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(54) Title: SOLAR PV AND AC SOURCE POWER BLENDING CONTROLLER

(57) Abstract: An energy blending device has a first input for alternating current, a second input for connection to a solar array, and an output, the energy blending device receiving energy from the first input, both inputs coupled to power an energy blending node. The device is in a configuration either with the solar array matching a voltage of the energy blending node, the blending node providing power through a DC-DC converter to a load interface device, and the solar array coupled through a DC-DC converter to the energy blending node, the energy blending node providing power to a load interface device. A microcontroller controls the DC-DC converter and a load interface device. The energy blending device has an energy storage system having a battery coupled either directly to the energy blending node or through a bidirectional energy storage interface to the energy blending node.



SOLAR PV AND AC SOURCE POWER BLENDING CONTROLLER**PRIORITY CLAIM**

[0001] The present document claims priority to United States Provisional Patent Application number 62/536,161 filed 24 July 2017, the entire content of that provisional patent application is incorporated herein by reference.

BACKGROUND

[0002] Residential and commercial electricity prices are increasing at annual rate of 5-10%. Two of the biggest loads in residential applications are air conditioning (HVAC) mainly used in southern states in US, and pumps. Both types of loads are in use during daylight hours, when the sun is at its peak.

[0003] The number of solar photovoltaic (PV) installs with AC grid connectivity (net metering) is increasing, giving utilities a problem with grid stability, so utilities are trying to decrease the number of new installed grid-tied solar systems. Another problem is that many distribution installations are not meant for bidirectional flow of power from solar to grid, which increases a risk of grid instability.

Summary:

[0004] Our proposed Power Blending Controller (PBC) combines power from solar PV sources with AC sources, such as the electrical grid, diesel, wind, gas or micro-hydro turbine or gasoline driven generators, and supplies an alternating current (AC) or direct current (DC) load with required power. With our PBC, power is “Blended” between solar and alternative AC sources, so that sum of the two provide 100% of required load power at any given time, hence the load operates without knowing where the power is coming from. Additional energy storage component can be added to the system to store energy from either the solar PV when available or AC sources when affordable, and used when needed later in a day, with a main purpose of keeping the load always in uninterrupted operation, and minimizing the use of electricity from the grid, especially during the peak hours when it’s the most expensive.

[0005] In an embodiment, an energy blending device has a first input for alternating current, a second input for connection to a solar array, and an output, the energy blending device receiving energy from the first input, both inputs coupled to power an energy blending node. The device is in a configuration either with the solar array matching voltage of the energy blending node, the blending node providing power through a DC-DC converter to a load interface device, and the solar array coupled through a DC-DC converter to the energy

blending node, the energy blending node providing power to a load interface device. A microcontroller controls the DC-DC converter and a load interface device. The energy blending device has an energy storage system having a battery coupled either directly to the energy blending node or through a bidirectional energy storage interface to the energy blending node.

[0006] In another embodiment, a method of combining energy from solar panels, an AC source, and an energy storage device to operate includes passing energy from each of the AC source and the solar panels to an energy blending node, and passing energy in a direction selected from the group consisting of from the energy storage device to the energy blending node and from the energy blending node to the energy storage device, the direction selected according to available energy at the energy blending node and energy needs of a load. The method also includes passing energy from the energy blending load through a load interface device to the load.

[0007] In another embodiment, an energy blending device has a first input configured for alternating current, a second input configured for connection to a solar panel, and an output, the energy blending device includes a rectifier receiving the first input, the rectifier coupled through a first DC-DC converter configured for power factor correction and having a DC output coupled to an energy blending node, the voltage of the energy blending node being regulated at a pre-set value by the first DC-DC converter to match a maximum power voltage of the solar PV panels. The energy blending device also includes an output driving circuit coupled to receive power from the energy blending node through a second DC-DC converter, the output driving circuit selected from the group consisting of a variable-frequency motor driver, a third DC-DC converter, and an inverter; and a microcontroller coupled to control the first and second DC-DC converters. The second DC-DC converter regulates an input voltage for the output driving circuit.

BRIEF DESCRIPTION OF THE FIGURES

[0008] Fig. 1 is a block diagram of an embodiment of a system incorporating a **Power Blending Controller (PBC) 103**.

[0009] Fig. 2 is a detailed diagram of an embodiment of the controller from Fig. 1.

[0010] Fig. 3 is a block diagram of another example of an embodiment of the power blending controller.

[0011] Fig. 4 illustrates typical voltage-current curves of a solar PV panel showing the maximum power point MPP.

[0012] Fig. 5 illustrates times of the daily operation of the system with **solar power** 602 and **AC source power** 603 sources controlled by power blending controller, when supplying power for a given **load power** 601.

[0013] Fig. 6 is a detailed diagram of another embodiment of a system incorporating a **Power Blending Controller (PBC)** 700 with a motor load output.

[0014] Fig. 7 is a detailed diagram of an embodiment from Fig. 6 with direct DC output port.

[0015] Fig. 8 is a block diagram of voltage levels used for blending node regulation.

[0016] Fig. 9 is a detailed control diagram of power blending algorithm that controls DC-DC boost converter interfacing solar source input.

[0017] Fig. 10 is a detailed control diagram of variable frequency converter algorithm that runs output motor load.

[0018] Fig. 11 is a flowchart illustrating a method used for controlling the embodiment shown in Fig. 6 and 7.

DETAILED DESCRIPTION OF THE EMBODIMENTS

[0019] Fig. 1 is a block diagram of a system 100 incorporating a **Power Blending Controller (PBC)** 103, configured to receive input power from inputs that may include a **solar PV system** having a solar array of one or more PV panels, connected in series or parallel configuration 101. The PBC also receives input power from an **AC source** 102 that can be a single, two or three phase configuration AC source, the AC source may be selected from: the electrical grid, diesel or gasoline driven generators, micro hydro or wind driven turbines, and other sources. The power flow from the AC source is unidirectional, always from the AC source to the PBC. Output of the PBC 103 feeds either a **DC or AC load** 104 that may differ in voltage, frequency and phase (AC only) from the AC source 102. There is an optional energy storage component 105 that can be connected to the PBC unit, acting as an energy buffer to enable uninterruptable power supply for load 104, and operation of loads while minimizing load on the AC source at peak price times.

[0020] Typically, there is a load-dependent cost associated with power from the AC source, such as a utility company bill according to a recording kilowatt hour meter if the AC source is the AC power grid, or a fuel bill if the AC source is a diesel or gas-turbine generator, the PBC uses available solar power to reduce power used from the AC source thereby reducing grid kilowatt hours or fuel bills.

[0021] Fig. 2 is an example, more detailed diagram of an embodiment of the controller from Fig. 1. Single, two or three phase **AC Source** 201 with its input voltage of

Vgrid 202 is one input to the **Power Blending Controller** 211. After **Vgrid** AC voltage is rectified using a passive **diode rectifier or active rectification circuit** 205, it provides **Vblend** 206, where it is merged with **solar PV source's** 203 output **Vpv** 204 through a blocking diode (not shown). Once the rectified AC source voltage and solar PV voltage are merged, power goes through **boost circuit** 207, to provide adequate higher **Vdc voltage** 208, than **Vblend** 206, which is an input for **Variable Frequency Drive (VFD) or Inverter** circuit 209. Single or multiphase VFD or Inverter circuit 209 adapts **Vdc** voltage 208 to provide proper power for **AC load** 210.

[0022] An optional **energy storage circuit** 216 through **Storage interface** 217 is coupled to the **Vblend** 206 voltage level to be coupled with both solar PV source 203 inputs and an output of the rectifier circuit 205, **Vblend** is then input for the boost circuit 207. Energy storage circuit 216 can be charged using rectified AC grid source in combination with Solar PV source power. It provides power to the boost circuit in combination with AC grid source and Solar PV source power, or solely when solar is not available, and AC source power is not affordable.

[0023] Energy storage 216 can be either a high voltage battery (battery voltage $V_b > 100V_{dc}$ like a high voltage Li-Ion battery), where storage interface 217, 317, 619 includes a battery charge management circuit, or energy storage 216 can be a lower voltage $V_b < 12-60V_{dc}$ battery, in which case the storage interface 217, 317, 619 includes a bidirectional DC-DC converter configured to step up battery voltage to the **Vblend** 206, 306, 607 voltage level when drawing power from the battery, and to step down power from **Vblend** 206, 306, 607 voltage to battery voltage when charging the battery, under control of microcontroller 215, 315, 615. In an alternative embodiment, storage interface 217, 317, 619 includes a first DC-DC converter adapted to charge the battery of energy storage 216, 316, 618 from energy blending node **Vblend** 608 307, 207 and a second DC-DC converter adapted to draw power from the battery of energy storage 216, 316, 618 and provide energy to energy blending node **Vblend** 206, 306, 607, the active DC-DC converter and amount of current drawn both under control of microcontroller 215, 315, 615. The microcontroller 215, 315, 615 has firmware configured to enable the microcontroller to determine an energy demand of the load and an availability of energy at **Vblend** the energy blending node, and to divert excess energy from **Vblend** to charge the battery of the energy storage, and to make up an energy deficit at **Vblend** by transferring energy from the battery to **Vblend**.

[0024] In an alternative embodiment a **DC/DC converter replaces VFD or Inverter** 209 and provides power to **DC load** 210. However, it is also possible to have a **Vdc**

being an output from **boost circuit** 207, directly feeding a load, without having VFD/Inverter, or DC-DC circuit. The VFD/Inverter or DC-DC circuit being a load interface device adapted to adapt power from the blending node to provide suitable voltage and frequency as needed to power the load. A **Microcontroller** 215 is integral part of the Power Blending Controller 211, with feedback and control signals to and from: rectifier 205, boost 207 and VFD/Inverter or DC/DC 209 circuits. Feedback signals that are inputs for microcontroller 215 include sensors for current, voltage, frequency, temperature, etc. while control signals from microcontroller 215 are controlling power switches (MOSFETS and IGBTs) that carry out power conversion between AC 201 and Solar source 203 on one side, and AC or DC load 210 on the other.

[0025] Fig. 3 illustrates another exemplary embodiment of the power blending controller. **AC Source** 301 with its input voltage of **Vgrid** 302 is input to the **Power Blending Controller** 311. Vgrid (grid supply voltage) is an input to the rectifier circuit 303, which is either single or three phase, depending on the AC source. In particular embodiments, rectifier 303 is connected to a Power Factor Correction (PFC) circuit 313 that aligns sinusoidal waveform of electrical grid voltage (Vgrid), with grid current; so that AC or DC loads 312 look to the grid as a resistive load during most operation. This PFC circuit includes a DC-DC converter having a selectable reference Vref 304 (provided by microcontroller) for regulating a Vblend voltage 307.

[0026] In a particular embodiment, this Vref voltage is chosen to match a solar voltage of coupled solar PV source in order to maximize solar power. The PFC circuit reads input AC Source 301 voltage waveforms, and controls its internal DC-DC converter 314 in order to overlay its AC current waveform against AC voltage waveform, to result in unity power factor, so that phase angle between the AC source 301 voltage and AC current waveforms is zero while providing pulsating DC onto Vblend 307. A filter capacitor 318 on Vblend may be provided to store energy between half cycles of the AC source 301 and permit boost circuit 308 and variable frequency drive 310 operation asynchronously to the AC source 301 frequency.

[0027] In some embodiments having a PFC circuit 310 with a boost-type DC-DC converter 314, the Vref signal at which PFC regulates the voltage is higher than a square root of two (SQRT(2)) times the root-mean-square (RMS) input AC voltage source. In some embodiments, it is possible to use either 120Vac or 230Vac source as an input to the PFC circuit. Hence, it's possible for 230Vac motor loads to be driven off of Power Blending Controller (PBC) even when connected to an 120Vac AC source, because the DC-DC

converter boost circuit inside the PBC adjusts the PFC output voltage to the higher voltage for VFD to control higher voltage motors.

[0028] In alternative embodiments, PFC circuit 310 may include a buck-boost DC-DC converter 314 and boost circuit 308 includes a voltage-increasing DC-DC converter, permitting greater flexibility of array voltage, output voltage, and AC supply voltage.

[0029] Solar PV source 305 has its output V_{pv} 306 coupled to V_{blend} , in embodiments through a blocking diode. V_{blend} in turn powers **boost circuit** 308 that powers **Variable Frequency Drive (VFD)** or **Inverter** circuit 309. VFD or inverter circuit 309 in embodiments can be a single or multiphase variable frequency drive to provide proper power for **AC load** 312. Circuit 309 can also be **DC/DC converter** adapted to provide power to **DC load** 312. It is also possible to directly connect some DC loads to **boost circuit** 308, directly feeding a load.

[0030] A **Microcontroller** 315 is an integral part of the Power Blending Controller 311 and has feedback and control signals to and from: PFC circuit 313, boost circuit 308 and VFD/Inverter or DC/DC 310 circuits. Feedback signals input to microcontroller 315 provide information of current, voltage, frequency (at AC load), temperature, etc. while control signals from microcontroller 215 control power switches (MOSFETS and IGBTs) that carry out power conversion between AC 201 and Solar source 203 on one side, and AC or DC load 210 on the other. Furthermore, control signals from microcontroller 315 to Rectifier with PFC circuit 303 set a reference for voltage regulation, which essentially regulates V_{blend} voltage - 307.

[0031] An energy storage circuit 316 and storage interface 317 have the same functionality as corresponding energy storage 216 and storage interface 217 in Fig. 2.

[0032] Fig. 4 illustrates typical voltage-current curve of one solar PV panel. Solar PV voltage is on X-axes, while solar PV current is on Y-axes. There are two different **solar PV curves** provided: 401 and 403. Curve 401 corresponds to higher solar irradiation, while 403 corresponds to a lower solar irradiation value. Maximum power point for 401 curve is at MPPT point 402 with current at maximum power point (**I_{mpp1}**) 405 value and voltage at maximum power point (**V_{mpp}**) 406 value, while a second maximum power point for curve 403 is shown at 404 with **I_{mpp2}** current 407 and same **V_{mpp}** 406 voltage value.

[0033] The microcontroller 215, 315, 615 periodically seeks for any adjusted maximum power point. In doing so, it tries drawing more or less current at a greater or lesser voltage from the array by adjusting factors such as V_{ref} . For example, it may try increasing V_{ref} so V_{blend} increase to V_{new} 409, testing operation at point 408. Point 408 is outside the

maximum power for curve 401, where solar voltage **Vnew** 409 has higher value than V_{mpp} , but solar current **Inew** 408 (the array current at V_{new}) has lower value than I_{mpp1} . As a result, power at point 408 results in lower power than power at point 402, although they are both on the same solar curve 401. And hence, a power at point 404 results in lower power than power at 402, because point 404 is on lower irradiance curve 403 than point 402. Should the microcontroller try a power point such as V_{new} , and find that power available is decreased while power is demanded by the load, the microcontroller backs off to its original V_{ref} .

[0034] Figure 5 shows daily operation of the system consisting of **solar power** 502 and **AC source power** 503 sources controlled by power blending controller, when supplying power for a constant **load power** 501. During intervals 504 when the sun is down, power to the load is provided by AC source only, while in intervals 505 where the sun is up, but solar output fails to meet full needs of the load, the power is blended between **AC source** 503 and **solar PV power** 502. Lastly, during time intervals 506 where plentiful solar power is available, the entire load power is provided by solar PV power 502, and excess power that is not utilized by the load is stored in energy storage 216, 316, 618 – as **stored power** 507.

[0035] Fig. 6 is a block diagram of an alternative embodiment of the power blender controller topology. Single phase **AC Source** 601 with its input voltage of **Vgrid** 602 is one input to the **Power Blending Controller** 600. V_{grid} is an input to the **rectifier** 603 and rectified voltage feeds **PFC circuit** 604. This PFC circuit 604 receives a reference signal for output voltage regulation V_{blend} 608, so that voltage is regulated at that value. At the same time **solar PV source's** 605 with its voltage **Vpv** 606 presents an input for **boost circuit** 607 including power switches, in most embodiments MOSFETs controlled to boost the voltage, from V_{blend} 608 voltage to a suitable input voltage for **Variable Frequency Drive (VFD)** or **Inverter** circuit 609, which can drive a single or multiphase **AC load** 610. A **Microcontroller** 615 is an integral part of the Power Blending Controller 600 and has feedback and control signals to and from: rectifier with PFC 604, boost 607 and VFD/Inverter or DC/DC 609 circuits, as well as V_{blend} 608 parameters. Feedback signals that input to microcontroller 615 provide information about current solar PV parameters: solar panel current (I_{pv}) and solar panel voltage (V_{pv}) 613, Boost inductor current (I_{ind}) 612, and load current (I_{load}) and load voltage (V_{load}) and load frequency (f_{load}) parameters. There are control signals from microcontroller 615, that control power switches (MOSFETS and IGBTs) that carry out power conversion between AC 601 and Solar source 605 on one side, and AC or DC load 610 on the other. A microcontroller signal that controls boost circuit

607 is duty 611, while microcontroller provides a reference voltage (Vref) that controls PFC circuit 616, defining a voltage level at which PFC circuit regulates the DC link voltage: Vblend 608. Lastly, microcontroller uses signal d for controlling operation of VFD/Inverter or DC/DC converter circuit 609, depending on the load 610 Power Blending Controller is attached to.

[0036] Microcontroller 215, 315, 615 is configured with a real time clock circuit and may be configured with user-entered data regarding scheduled times of low, medium, and peak electricity prices. The real time clock is compared to scheduled or broadcast times of peak electricity prices to determine whether stored energy from energy storage 618 or energy from the AC source 601 is to be used to make up energy deficits at Vblend 608 due to more energy being drawn by VFD/DC-AC Inverter/DC-DC converter circuits (load interface circuits) 609, 609A than provided by solar PV source 605.

[0037] In alternative embodiments, Vblend 608 may provide power to additional VFD/DC-AC Inverter/DC-DC converter circuits 609A adapted to provide power to additional loads 610A. In an exemplary embodiment, one VFD/DC-AC Inverter/DC-DC converter circuits 609 provides power to a load 610 including an AC motor through a variable-speed and variable-voltage drive, and a second VFD/DC-AC Inverter/DC-DC converter circuits 609A provides power to a load 610A at fixed frequency and voltage; in this embodiment load 610A includes desktop computers and lights where operation at reduced frequency or voltage (such as may be provided by VFD 609 to motor load 610) could cause undesired resetting of computers and flickering or dimming of lights.

[0038] In a particular embodiment, microcontroller 615 is configured with firmware in a memory of microcontroller 615 to prioritize loads and to drive intermittent-duty loads in a coordinated manner. For example, if two VFD converter circuits 609 are provided driving two motor loads 610, the microcontroller 615 may be configured to operate these loads alternately when available solar power is insufficient to operate these loads simultaneously. The microcontroller 615 may also be configured to operate a high-priority load whenever the load desires power, and to operate a second lower priority load only when solar power is sufficient to run both loads or when grid power is cheap.

[0039] It is anticipated that the embodiments illustrated in Fig. 2 and Fig. 3 may also power multiple loads having separate VFD/DC-AC inverter/DC-DC converters coupled to the output 209, 309 of boost circuit 208, 308, or through separate boost circuits to Vblend 207, 307.

[0040] In a particular exemplary embodiment of the embodiment of Fig. 6, a first VFD/DC-AC inverter/DC-DC converter load interface device 609 is adapted to run a 220V well pump configured to fill a cistern with variable voltage, variable frequency AC motor drive, a second load interface device 609A is a fixed-voltage, fixed-frequency DC-AC inverter adapted to run lights and a computer, a third load interface device (not shown) is a variable frequency AC motor drive adapted to run a 110V refrigerator motor, and a fourth load interface device is a DC-DC converter adapted to run a 12-volt boost pump from cistern to a water system. In this embodiment, microcontroller 315 is configured to prioritize loads, conserving sufficient charge in the energy storage 618, so that a high priority load such as the lights and computer always have power even when both AC power and solar power are unavailable for at least a predetermined backup power operating period, and to operate the well pump when AC power is cheap, solar power is plentiful, and the cistern is below full, or when the cistern is less than a minimum level despite pricing of AC power.

[0041] In order to conserve sufficient charge in the energy storage 618 so that the high priority load always has power even when both AC power and solar power is unavailable, the energy storage 615 is equipped with battery charge status monitoring devices coupled to provide a charge state to microcontroller 615,

[0042] An energy storage 618 and storage interface 619 can be added optionally with the same functionality as previously described with reference to energy storage and storage interface of Fig. 2 and 3.

[0043] It is also possible to couple a load directly to Vblend 608, in which case the load is connected directly to Vblend 708, as shown on Fig. 7.

[0044] Fig. 8 shows different voltage levels for blending voltage Vblend 801 regulation, depending on which controller is regulating the DC link blending voltage at which given time. At voltage level 1 802 the Vblend voltage is regulated at $V_{ref} - X$ value 803, where V_{ref} 805 is voltage level 2 804 at which the PFC circuit is regulating the V blend voltage. X is a constant which can vary depending on the load. At a voltage level 3 806 the Vblend voltage is regulated at $V_{ref} + X$ value 807.

[0045] Fig. 9 shows the control principle of the blending method implemented in the microcontroller 901. Inputs to the controller are solar PV voltage measurement 903, blending voltage measurement Vblend 907 and inductor current measured at the boost circuit interfacing the solar PV system 911.

[0046] Error between measured solar PV voltage V_{PV} 903 and reference voltage V^*_{PV} 902 is an input for the PI voltage controller 904, which uses certain proportional (P)

and integral (I) gains to calculate reference current I^* 905. Similarly, error between measured DC link blended voltage V_{blend} 907 and reference DC link voltage V_{ref+X} 906 is an input for the PI DC link voltage controller 908, which uses different proportional (P) and integral (I) gains to calculate reference current I^{**} 914.

[0047] Both reference currents I^* and I^{**} are inputs for MIN logical block 909, which outputs I^{*boost} reference 910, that is compared with input I_{ind} current 911. Error of the I^{*boost} and I_{ind} is run through another PI boost current controller 912, which results in duty ratio 913 signal that is used for controlling power switches of the boost circuit (607 of Fig. 6).

[0048] Fig. 10 illustrates how VFD circuit regulates DC link voltage V_{blend} at a voltage level 1 802 from Fig. 3 at a value of V_{ref-X} 803. The difference between V_{ref-X} 1002 and actual V_{blend} 1003 voltage is an input to the PI VFD DC link controller 1004, which provides reference frequency f^* 1005 for a voltage/frequency (V/f) VFD control method 1006 that results in duty cycle d 1007, which VFD uses to run the motor load.

[0049] Figure 11 is a flow chart used by the microcontroller to execute power a blending method for the topology described in Fig. 6 and 7 at the time of motor start. Microcontroller reads V_{blend} , V_{pv} and I_{boost} and calculates 1102 a duty-cycle signal d for boost circuit 607 using the method described above with reference to Fig. 9. Simultaneously, the PFC circuit tries to regulate V_{blend} voltage at V_{ref} and the VFD starts applying voltage to motor load to attempt rotation, according to the method describe above with reference to Fig. 10.

[0050] If 1104 the AC source is present, the VFD increases motor voltage and frequency to nominal voltages and frequency for the motor while the PFC circuit maintains V_{blend} 1106 as previously discussed with reference to Fig. 10. If 1104 the AC source is not present, the VFD applies available power to the motor 1108, effectively regulating V_{blend} at $V_{ref} - X$, until either the motor starts, or a timeout occurs. If a timeout occurs, the VFD shuts down and waits for a predetermined time before re-attempting motor start. In an alternative embodiment, the microcontroller may request that an AC generator used as AC source 601 start operation before next re-attempting motor start. Once the motor starts, motor operating frequency is increased until full nominal voltage and frequency are reached or the maximum available solar power is used.

[0051] As the motor starts, the boost circuit 607 operates 1112 in MPPT mode with duty cycle signal d as determined according to the method previously discussed with reference to Fig. 9. If 1114 the motor load is not solely operated by solar power, the PFC

circuit maintains V_{blend} 1106 as previously discussed with reference to Fig. 10; if 1114, the motor load can be solely supplied by solar power, boost circuit 607 regulates 1116 V_{blend} voltage at $V_{ref}+X$ level, while the motor load continues operating at either nominal frequency or the frequency at which power consumed by the motor matches the available power from the solar array.

[0052] Power blending controller (PBC) 103 (**Fig. 1**) has two inputs. First is solar photovoltaic power source 101, including an array of one or more photovoltaic panels coupled in series, parallel, or series-parallel to provide a DC (Direct Current) output to the PBC. The other input is from an AC source 102, which can be single or multiphase phase electrical grid, diesel or gasoline powered generator, or a micro hydro, gas, or wind turbine driven generator. AC source 102 in some embodiments is a generator configured to operate at request of a microcontroller, such as microcontroller 615 (Fig. 6), of power blending controller 103, and operates when solar power and energy storage reserve power together are insufficient to maintain a desired minimum standard of service of operating loads 104. Output of the power blending controller is adapted to drive one or more DC or single or multiphase AC loads 104.

[0053] **Figure 2** presents an option for power blending controller architecture where solar PV system 203 output is connected to the rectified AC source voltage V_{blend} 206. Solar PV panels 203 are connected in series and parallel to give a maximum power point voltage (V_{pv}) that matches rectified grid voltage V_{blend} 206. A solar array having a number of solar PV panels connected in series is determined as n (series panels) = $V_{blend} / \text{Maximum Power Point Voltage of a panel } (V_{mpp})$ 406 (Fig. 4) of the panels used in the Solar PV source array. If V_{mpp} of a given solar PV panel is X , and AC source voltage is 120Vac grid, then a minimum number of the solar PV panels used should be at least $1.41 \cdot 120/X$. This way rectified AC source voltage V_{blend} - 206 (in a particular embodiment: $1.41 \cdot 120$) fixes the solar PV voltage value, so that solar PV current is changing with solar irradiance. The number n of series solar PV panels can be higher than $1.41 \cdot 120/X$.

[0054] Optional energy storage can be added to the system, as shown in Fig. 2. The energy storage 216 is connected to the input of the boost circuit via bidirectional storage interface block 217 and can store excess power from solar PV source to feed boost circuit 207 in time periods when solar power from solar source 203 is insufficient to operate load 210 under control of microcontroller 215. Alternatively, microcontroller 215 can direct energy storage interface block 217 to use AC source power to charge the energy storage 216, so that power can be fed to boost circuit 207 at a later time. Such mechanism is useful for “peak

shaving” to reduce power consumption during the peak-priced hours of AC grid power, where a Power Blender Controller with energy storage can provide uninterrupted load operation while managing solar power and energy storage, making sure that overall power draw from the grid during peak hours is below a threshold that triggers unduly high demand charges for the customer.

[0055] Furthermore, the energy storage 216 can be used for uninterruptable power supply for the load by storing excess solar energy unused by the load during peak sun times and AC source 201 fails. In this embodiment, the microcontroller 215 of the power blending controller may be configured to maintain a minimum charge level in the energy storage 216 for providing uninterruptable power to high priority loads during power failures. Microcontroller 215 does so by configuring the power blending controller 103 and boost circuit 207 to draw power from AC source 205 as needed to operate the load when solar power is insufficient.

[0056] Storage interface 217 is a bidirectional DC-DC converter that enables use of low voltage batteries, as its DC-DC topology enables low voltage batteries to receive power from, and deliver power to the high voltage Vblend circuit level.

[0057] **Figure 3** shows another embodiment for a power blending controller architecture where solar PV 305 power is merged with rectified AC source 301 power on the output of the additional rectifier with Power Factor Correction - PFC 303 component. The PFC circuit has selectable reference 304 as an input for voltage regulation of PFC. That way, the voltage regulation level is chosen to match PV maximum power point voltage – V_{mpp} 506. As a result, an output of the PFC circuit - Vblend 307 is regulated by PFC circuit. Furthermore, reference voltage regulation set point 304 is controllable by either an external analog signal or from microcontroller 315 to track in realtime a maximum power point of panels. As a result, PFC circuit regulates Vblend 307 voltage at a set maximum power point voltage level. Microcontroller 315 also controls boost circuit 308 to regulate Vdc voltage 309 at level that matches the correct input for VFD/Inverter or DC-DC circuit 310 for a given load 312. It is also possible to directly couple a high voltage DC load to Vblend. Hence, DC loads can directly be connected to the output of the boost circuit 308 that is regulated Vdc voltage.

[0058] The number of Solar PV panels 305 connected in series is determined by the maximum power point voltage of the PV panels and AC source voltage. In an example, if V_{mpp} of a given solar PV panel is X, and AC source voltage is 120Vac grid and the rectifier has an output voltage $1.41*120$ Volts, then a minimum number N of the solar PV panels

should be at least $1.41 \cdot 120/X$. In this this way rectified AC source voltage V_{blend} - 307 (in a given example: $1.41 \cdot 120$) fixes the solar PV voltage value at a maximum power point level, so that all available solar PV current is used. The number of solar PV panels can be higher than $1.41 \cdot 120/X$. The selectable reference for voltage regulation is chosen so that regulated voltage V_{blend} 307 on the output of the PFC circuit 303 is adapted to the number of solar PV panels connected in series times the panels' V_{mpp} . The programmable power factor correction circuit, including a DC-DC converter, gives a rectified output voltage adjustable to match array V_{mpp} 506, and is controllable by microcontroller 315 where voltage regulation reference is set once for a given solar PV panels, or reference can change with solar irradiation, to match V_{mpp} 506 in real time. In an alternative embodiment dual-inline (DIP) switches may be used to configure the converter instead of a microcontroller.

[0059] Once solar PV power 305 is “blended” with rectified AC source power 302 at the V_{blend} 307 node, then boost circuit 308 accommodates an appropriate DC link voltage level 309 that VFD or inverter circuit 310 will be fed from to in turn power AC or DC loads 312. This way, the PFC circuit provides rectified AC source power at the correct voltage level for blending with Solar PV source at the maximum power point voltage of the solar array.

[0060] Again, an optional energy storage can be added to the system, as shown in the Fig. 3, in the same manner as in Fig. 2.

[0061] **Figure 5** shows power blending during the course of one cloudless day, where the X-axes represent the time of the day. Power blending controller is powered by solar PV 502 and AC source 503 while supplying power to the load with certain load power 501. At the beginning of the day, before sun comes out, the total load power 501 is supplied from AC source 503, which is shown during the time period 504. As the sun comes out, the solar power 502 contributes to the power blend, and solar PV voltage value – V_{mpp} 406 is dictated by the rectified AC source voltage V_{blend} while AC source is providing more than 50% of load power, for the topologies shown in the Fig. 2. However, for the power Blender topology shown in Fig. 3, 6 and 7, the blended voltage V_{blend} is regulated by PFC circuit powered by AC source. As the sun irradiance increases solar PV power contributes more to the load power, which is caused by solar PV current increasing its value from I_{mpp2} to I_{mpp1} .

[0062] As soon as solar PV source takes over the load power 501 and starts providing more than 50% of its power, the solar PV voltage changes from rectified AC source value to the new value determined by the solar PV curve - V_{new} 409, which is only

for topologies shown in the Fig. 2 and 3. At that point the new solar PV current is I_{new} 510, so that $I_{new} \cdot V_{new}$ is higher than load power 501. During the time 506 only solar PV is providing the power to the load, and V_{blend} voltage equals solar PV voltage, which is changing due to solar PV current change resulted by solar irradiance. At any given time, during the period 506, $I_{new} \cdot V_{new}$ is higher than load power 501. For topology shown in the Fig. 6 and 7, the blended voltage V_{blend} is regulated by boost circuit powered by solar.

[0063] If optional energy storage block is added to the system, excess solar power: $P_{excess} = I_{new} \cdot V_{new} - P_{load}$ is used to charge the energy storage during the period 506.

[0064] During the period 505 again, solar PV system start decreasing contribution in power blending, so that AC source power 503 takes over, and solar PV voltage value V_{blend} 206 drops back to rectified AC source value, which is same as the V_{mpp} 406 value of the solar PV system. As the sun irradiance decreases the V_{mpp} does not change much, but solar PV current drops from I_{mpp1} to I_{mpp2} , and eventually goes to zero, at which point AC source provides total power to the load again – period 504.

[0065] Solar PV system in this case is sized so that its V_{mpp} 406 voltage is the same value as rectified AC source voltage or 5% less for the topology from Fig. 2, while V_{mpp} 406 voltage can be higher for the solar PV system used in topology form Fig. 3. Solar PV system power 502 is sized based on the load power 501, which is applicable to the topologies from Fig. 2 and 3.

[0066] A control method for power blending topology shown in the Fig. 6 and 7 is described below. Solar PV and AC grid power are the inputs to the microcontroller operated power blender controller, with single/three phase AC output load 610, on Fig. 6, or DC output load 710, on Fig. 7.

[0067] Power blender controller 600 (Fig. 6) has three distinctive power conversion devices: Power factor correction (PFC) circuit 604 that interfaces AC source power via single phase diode bridge rectifier 603, a boost circuit 607 that is connected to the solar source on the input and single or three phase variable frequency drive - VFD 609 that is connected to the single or three phase motor load 610. The operation of all three circuits is controlled by microcontroller's 615 signals: PFC circuit is controlled by V_{ref} 616, boost circuit is controlled by duty 611, VFD is controlled by signal d 614, which are all a result of the power blending control algorithm, based on feedback signals: V_{pv} 613, I_{ind} 612, and V_{blend} 608.

[0068] Power Blending Controller 600 operates a load 610 by using Solar PV source 605 energy to offset energy from AC source 601. Operating principles of Power

Blending Controller (Blender) are described by the flowchart shown in Fig.11 and associated text above.

- A microcontroller that operates Power Blender Controller firstly reads the input signals: V_{blend} , V_{pv} and I_{boost} in order to generate a signal d for controlling the boost circuit using the control method from Fig. 9, and
- At the same time microcontroller provides V_{ref} voltage value to the PFC circuit that starts regulating V_{blend} at V_{ref} value, if AC power source is available
- At the same time VFD circuit starts applying the voltage output to the motor load per method described in the Fig. 10, in order to start motor's operation
- If the AC power source is present, PFC circuit will continue regulating V_{blend} at V_{ref} voltage level, while motor speed will increase as a result of VFD control method described by Fig. 10. Motor frequency/speed will reach maximum if AC power source is available. PFC circuit regulates a V_{blend} voltage 608 at V_{ref} voltage level 304, from Fig. 3. V_{ref} level is different for different motor types (example: for 120Vac phase voltage motors, V_{ref} can be 190Vdc, while for 240Vac motor types V_{ref} can be 370Vdc).
- As soon as V_{blend} voltage is regulated at V_{ref} , a VFD circuit 609 starts increasing output frequency and voltage, which starts a rotation of single or three phase motor load 610. Once VFD starts rotation of the motor, the VFD tries to regulate V_{blend} voltage at V_{ref-X} voltage value 303, from Fig. 3, which is lower than V_{ref} value that PFC circuit is regulating the V_{blend} voltage at. Because PFC circuit has infinite source of AC power (utility grid), it will maintain regulating V_{blend} voltage at V_{ref} , which is higher than V_{ref-X} level the VFD controller is trying to regulate at.
- VFD controller from Fig. 10 as a result of trying to regulate V_{blend} at V_{ref-X} increases the output motor frequency – $f^* 1005$, until it reaches maximum frequency.
- If however AC power is not available, then PFC circuit is off, and V_{blend} voltage is regulated by VFD at V_{ref-X} voltage level (X can be any suitable number, for example if $X=10$, and $V_{ref}=370V$, then $V_{ref-X}=360V$).
- A duty signal 913, from Fig. 9 for boost circuit 607 is actually obtained from PI boost current controller 912. A difference between measured inductor current – I_{ind} 911 of the boost circuit and reference I^*_{boost} current 910 is an input to the Boost current controller 912. I^*_{boost} reference current value 910 is obtained from MIN block 909 whose inputs are current references: I^* 905 – a result of PV voltage PI controller block 904 and I^{**} 914 – a result of DC link voltage PI controller block 908. PV voltage controller block performs maximum power point tracking (MPPT) algorithm of solar PV input panels, and

if I^* is of a smaller value than I^{**} , then boost circuit 607 will perform MPPT operation. If however, I^{**} is of a smaller value than I^* , then boost circuit 607 will perform DC link voltage regulation of DC link – Vblend voltage level at a reference voltage of $V_{ref}+X$, per Fig. 8.

- In MIN block, a minimum result of the two control loops 904 and 908 takes control, while the other loop gets knocked out. Because DC link voltage controller 908 output I^{**} 914 is resulting in higher value than PV voltage controller 904 output I^* 905 boost circuit will perform MPPT operation over solar PV input, while PFC circuit will continue regulating the Vblend voltage. As a result, boost circuit will extract maximum amount of power from input solar PV system, while AC source would be providing remaining amount of power to 100% motor load power, while regulating the Vblend voltage.
- If DC link voltage controller 908 overtake PV voltage controller 904, which would happen if all power for the motor load is provided by Solar PV source only, per DC link voltage controller loop 908, the solar PV source will NOT perform MPPT operation anymore and,
- Boost circuit will regulate DC link voltage Vblend at voltage level of $V_{ref}+X$, and motor will be operating at the maximum operating frequency.
- If the motor load is not entirely provided by solar PV source, but AC source is still providing portion of load power, then PFC circuit will regulate Vblend voltage, while boost circuit performs MPPT operation
- Ultimately, the VFD voltage control loop (Fig. 5) will adjust the motor frequency to match solar input PV power with motor output power. Hence, MPPT operation is still performed by boost circuit, while VFD is regulating DC link voltage Vblend at V^*PFC-X .

Combinations of Features

[0069] The features herein described can be collected in any combination, as necessary to meet a variety of applications. In particular the inventors anticipate the following particular combinations.

[0070] An energy blending device designated A has a first input configured for alternating current, a second input configured for connection to series-connected solar panels, and an output, the energy blending device including a rectifier receiving the first input, and having the rectifier output coupled to power an energy blending node; and a plurality of series-connected solar photovoltaic panels coupled to power the energy blending node. The device is in a configuration selected from the group consisting of the series-connected solar panels matching a voltage of and coupled to the energy blending node, the blending node

providing power through a DC-DC converter to a load interface device, and the series-connected solar panels coupled through a DC-DC converter to the energy blending node, the energy blending node providing power to a load interface device. The energy blending device further includes a microcontroller being coupled to control the DC-DC converter and load interface device; and an energy storage system selected from the group consisting of a battery coupled directly to the energy blending node and a battery coupled through an energy storage interface to the energy blending node.

[0071] An energy blending device designated AA including the energy blending device designated A where the series-connected solar panels couple through a DC-DC converter to the energy blending node, the energy blending node providing power to a load interface device, and the battery is coupled through an energy storage interface having DC-DC conversion capability to the energy blending node; and the energy storage interface is configured to operate under control of the microcontroller in modes including charging the battery from the energy blending node and drawing energy from the battery to provide energy to the energy blending node.

[0072] An energy blending device designated AB including the energy blending device designated A where the series-connected solar panels couple directly to the energy blending node and the load interface device is coupled to the energy blending node through a DC-DC converter.

[0073] An energy blending device designated AC including the energy blending device designated A, AA, or AB wherein the load interface device is selected from the group consisting of a variable frequency motor drive, a DC-DC converter, and a DC-AC inverter.

[0074] An energy blending device designated AD including the energy blending device designated A, AA, AB, or AC where the rectifier DC output is coupled to power an energy blending node through a second DC-DC converter configured to reduce power factor.

[0075] An energy blending device designated AE including the energy blending device designated A, AA, AB, AC, or AD wherein the load interface device is a variable frequency motor drive.

[0076] An energy blending device designated AF including the energy blending device designated A, AA, AB, AC, AD, or AE where the microcontroller is configured to start a generator if solar power is insufficient to start a motor coupled to the load interface device.

[0077] An energy blending device designated AG including the energy blending device designated A, AA, AB, AC, AD, AE, or AF the microcontroller is configured to start a generator if solar power is insufficient to start a motor coupled to the load interface device.

[0078] A method designated B of combining energy from solar panels, an AC source, and an energy storage device to operate includes passing energy from each of the AC source and the solar panels to an energy blending node, and passing energy in a direction selected from the group consisting of from the energy storage device to the energy blending node and from the energy blending node to the energy storage device, the direction selected according to available energy at the energy blending node and energy needs of a load. The method also includes passing energy from the energy blending load through a load interface device to the load.

[0079] A method designated BA including the method designated B wherein the step of passing energy from the energy blending node through the load interface device comprises passing energy through a DC-DC voltage converter.

[0080] A method designated BB including the method designated B or BA wherein the step of passing energy in a direction selected from the group consisting of from the energy storage device to the energy blending node and from the energy blending node to the energy storage device involves passing energy through a DC-DC voltage converter.

[0081] A method designated BC including the method designated B, BA, or BB wherein the step of passing energy from the AC source to the energy blending node comprises passing energy through a power factor correction unit comprising a DC-DC converter.

[0082] A method designated BD including the method designated B, BA, BB, or BC wherein the step of passing energy from the solar panels to the energy blending node comprises passing the energy through a DC-DC voltage converter.

[0083] A method designated BE including the method designated B, BA, BB, BC, or BD further including monitoring a voltage of the energy blending node and controlling at least one DC-DC voltage converter to maintain the voltage of the energy blending node within limits

[0084] A method designated BF including the method designated B, BA, BB, BC, BD, or BE wherein the load interface device includes a variable frequency motor drive.

[0085] An energy blending device designated C has a first input configured for alternating current, a second input configured for connection to a solar panel, and an output, the energy blending device includes a rectifier receiving the first input, the rectifier coupled

through a first DC-DC converter configured for power factor correction and having a DC output coupled to an energy blending node, the voltage of the energy blending node being regulated at a pre-set value by the first DC-DC converter to match a maximum power voltage of the solar PV panels. The energy blending device also includes an output driving circuit coupled to receive power from the energy blending node through a second DC-DC converter, the output driving circuit selected from the group consisting of a variable-frequency motor driver, a third DC-DC converter, and an inverter; and a microcontroller coupled to control the first and second DC-DC converters. The second DC-DC converter regulates an input voltage for the output driving circuit.

[0086] Changes may be made in the above methods and systems without departing from the scope hereof. It should thus be noted that the matter contained in the above description or shown in the accompanying drawings should be interpreted as illustrative and not in a limiting sense. The following claims are intended to cover all generic and specific features described herein, as well as all statements of the scope of the present method and system, which, as a matter of language, might be said to fall therebetween.

Claims:

What is claimed is:

1. An energy blending device having a first input configured for alternating current, a second input configured for connection to series connected solar panels, and an output, the energy blending device comprising:
 - a rectifier receiving the first input, and coupled to power an energy blending node;
 - a plurality of series-connected solar photovoltaic (PV) panels coupled to power the energy blending node;
 - the energy blending device in a configuration selected from the group consisting of:
 - the series-connected solar panels matching a voltage of and coupled to the energy blending node, the blending node providing power through a DC-DC converter to a load interface device, and
 - the series-connected solar panels coupled through a DC-DC converter to the energy blending node, the energy blending node coupled to provide power to a load interface device, the load interface device coupled to provide power to the output of the energy blending device;
 - a microcontroller being coupled to control the DC-DC converter and load interface device; and
 - an energy storage system selected from the group consisting of a battery coupled directly to the energy blending node and a battery coupled through an energy storage interface to the energy blending node.
2. The energy blending device of claim 1 wherein the series-connected solar panels couple through a DC-DC converter to the energy blending node, the energy blending node providing power to a load interface device, and the battery is coupled through an energy storage interface having DC-DC voltage conversion capability to the energy blending node; and
 - wherein the energy storage interface is configured to operate under control of the microcontroller in modes comprising charging the battery from the energy blending node and drawing energy from the battery to provide energy to the energy blending node.
3. The energy blending device of claim 1 wherein the series-connected solar panels couple directly to the energy blending node and the load interface device is coupled to the energy blending node through a DC-DC converter.

4. The energy blending device of claim 2 or 3 wherein the load interface device is selected from the group consisting of a variable frequency motor drive, a DC-DC converter, and a DC-AC inverter.
5. The energy blending device of claim 4 wherein the rectifier DC output is coupled to power an energy blending node through a second DC-DC converter configured to reduce power factor.
6. The energy blending device of claim 5 wherein the load interface device is a variable frequency motor drive.
7. The energy blending device of claim 6 wherein the microcontroller is configured to start a generator if solar power is insufficient to start a motor coupled to the load interface device.
8. The energy blending device of claim 7 wherein the energy blending device has a plurality of load interface devices and loads, and where the microcontroller is configured to prioritize a high priority load of a plurality of loads.
9. The energy blending device of claim 8 wherein the microcontroller is configured to reserve a portion of battery charge for the high priority load.
10. A method of combining energy from solar panels, an AC source, and an energy storage device to operate comprising:
 - passing energy from the solar panels to an energy blending node;
 - passing energy from the AC source to the energy blending node;
 - passing energy in a direction selected from the group consisting of from the energy storage device to the energy blending node and from the energy blending node to the energy storage device, the direction selected according to available energy at the energy blending node and energy needs of a load;
 - passing energy from the energy blending load through a load interface device to the load.
11. The method of claim 10 wherein the step of passing energy from the energy blending node through the load interface device comprises passing energy through a DC-DC voltage converter.

12. The method of claim 10 wherein the step of passing energy in a direction selected from the group consisting of from the energy storage device to the energy blending node and from the energy blending node to the energy storage device involves passing energy through a DC-DC voltage converter.
13. The method of claim 10 wherein the step of passing energy from the AC source to the energy blending node comprises passing energy through a power factor correction unit comprising a DC-DC converter.
14. The method of claim 10 wherein the step of passing energy from the solar panels to the energy blending node comprises passing the energy through a DC-DC voltage converter.
15. The method of claim 10, 11, 12, 13, or 14 further comprising monitoring a voltage of the energy blending node and controlling at least one DC-DC voltage converter to maintain the voltage of the energy blending node within limits
16. The method of claim 15 wherein the load interface device comprises a variable frequency motor drive.
17. An energy blending device having a first input configured for alternating current, a second input configured for connection to a solar panel, and an output, the energy blending device comprising:
 - a rectifier receiving the first input, the rectifier coupled through a first DC-DC converter configured for power factor correction and having a DC output coupled to an energy blending node;
 - the voltage of the energy blending node being regulated at a pre-set value by the first DC-DC converter to match a maximum power voltage of the solar PV panels; and
 - an output driving circuit coupled to receive power from the energy blending node through a second DC-DC converter, the output driving circuit selected from the group consisting of a variable-frequency motor driver, a third DC-DC converter, and an inverter; and
 - a microcontroller coupled to control the first and second DC-DC converters;wherein the second DC-DC converter regulates an input voltage for the output driving circuit.

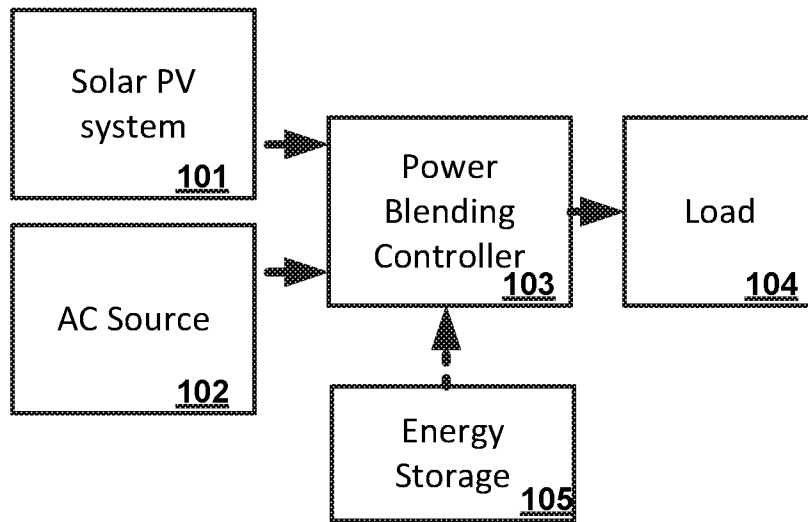


Fig. 1

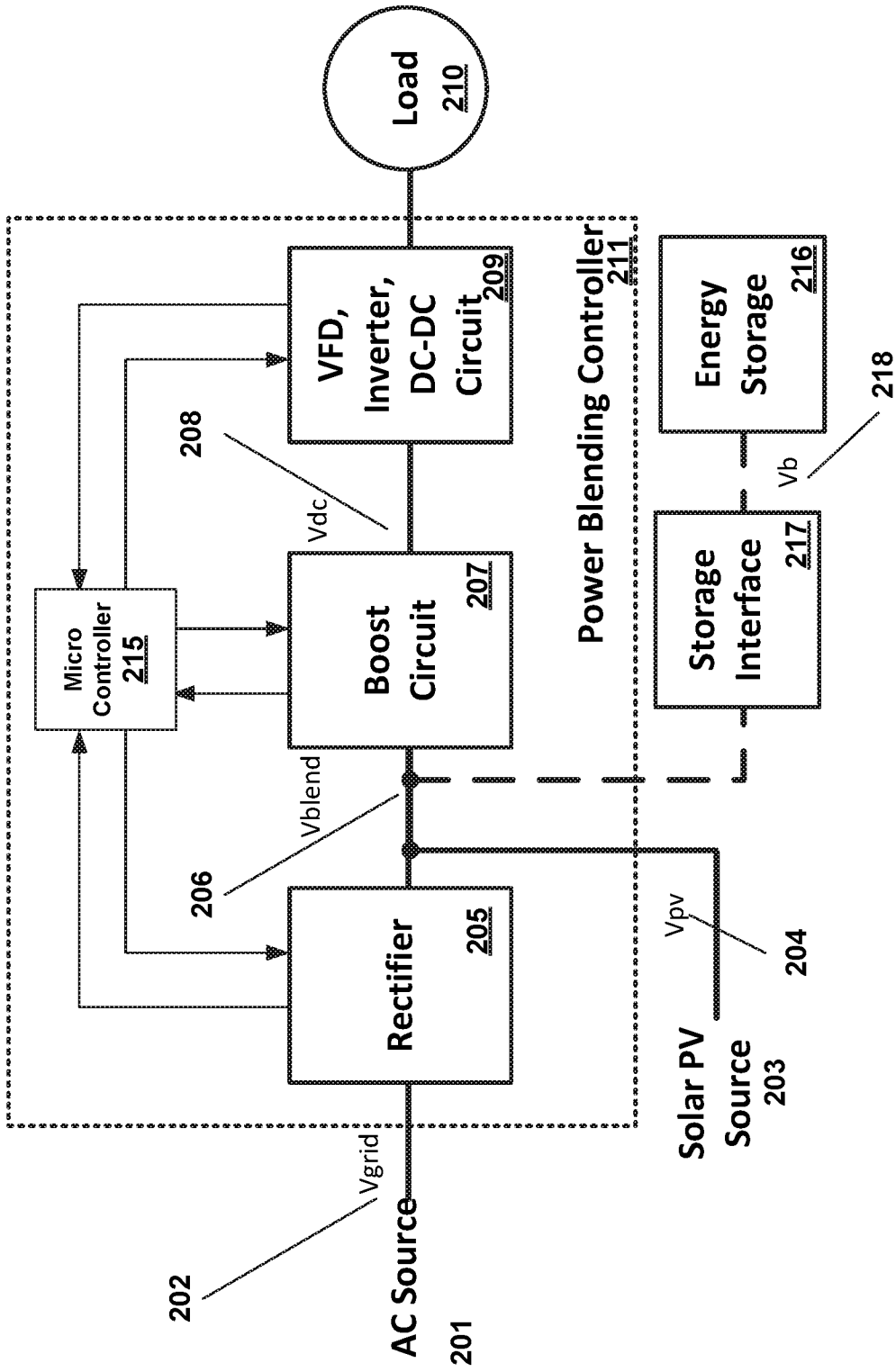


Fig. 2

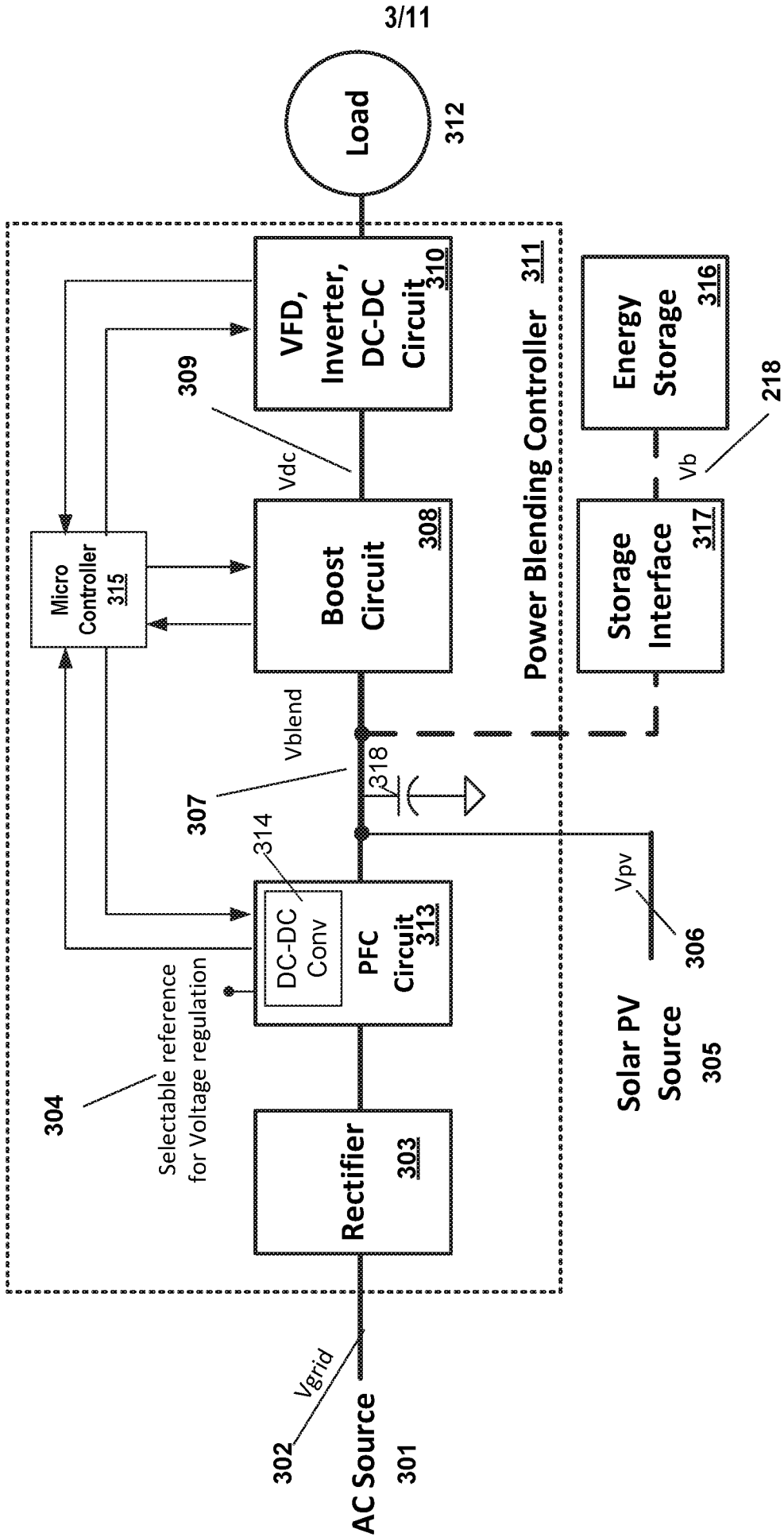


Fig. 3

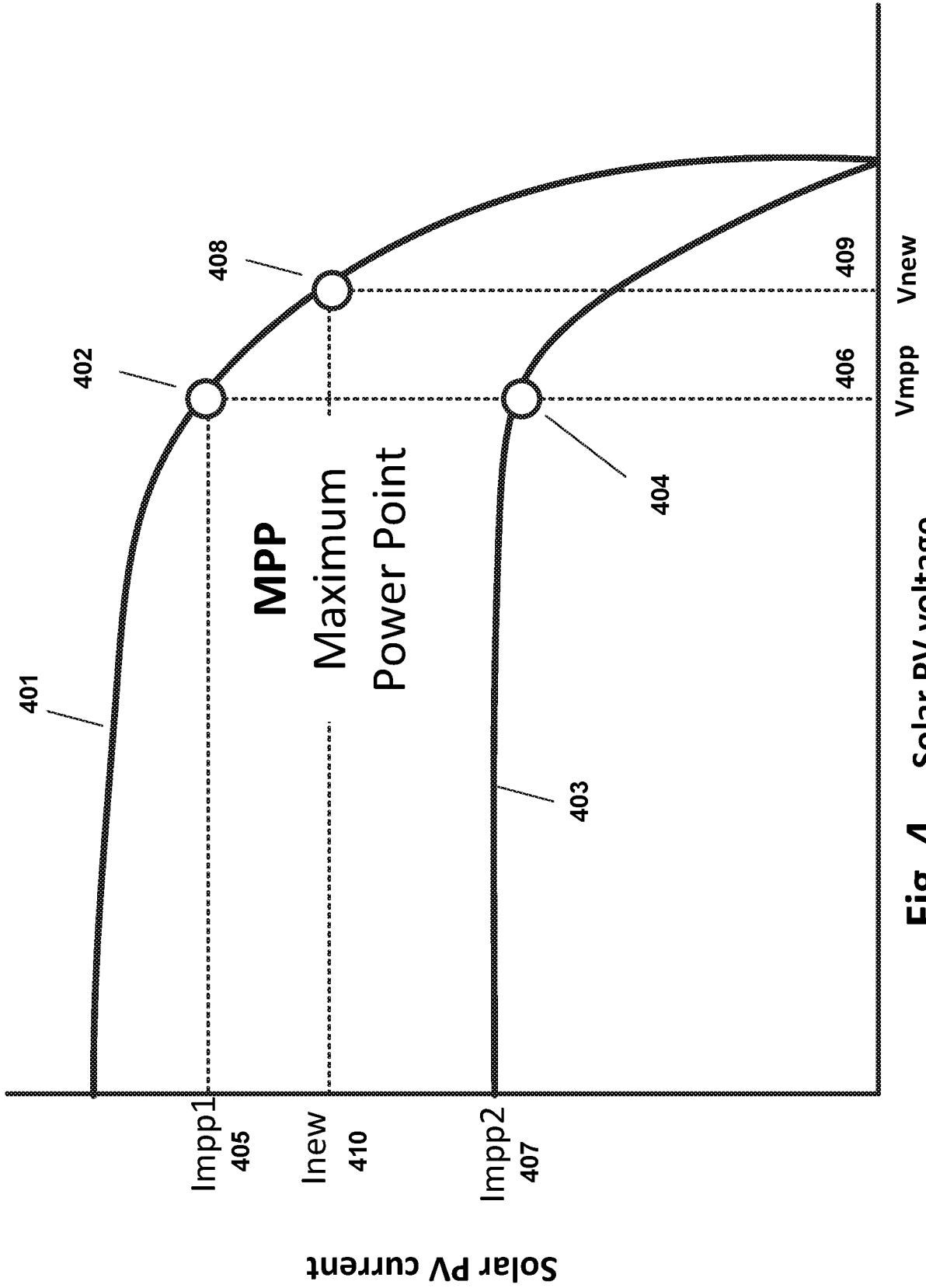


Fig. 4 Solar PV voltage

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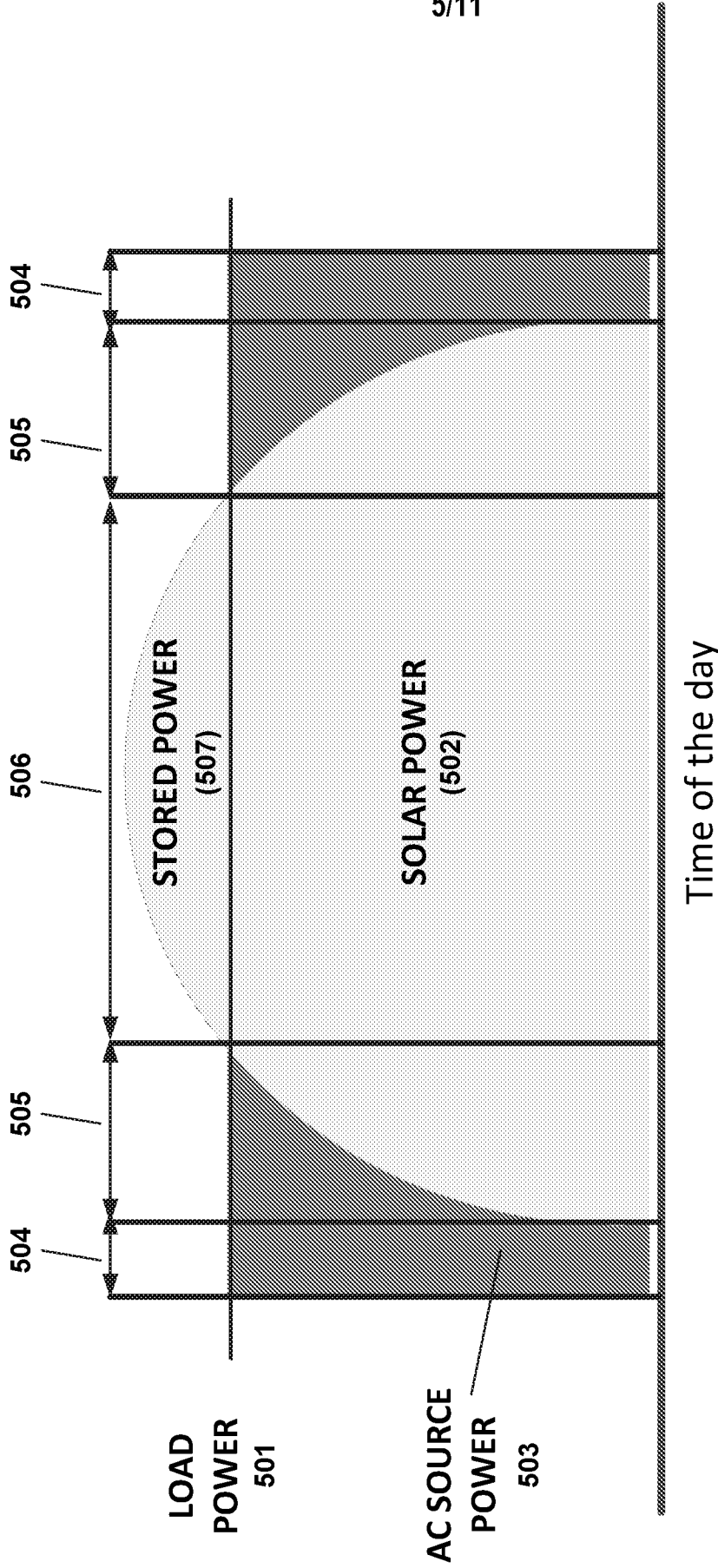


Fig. 5

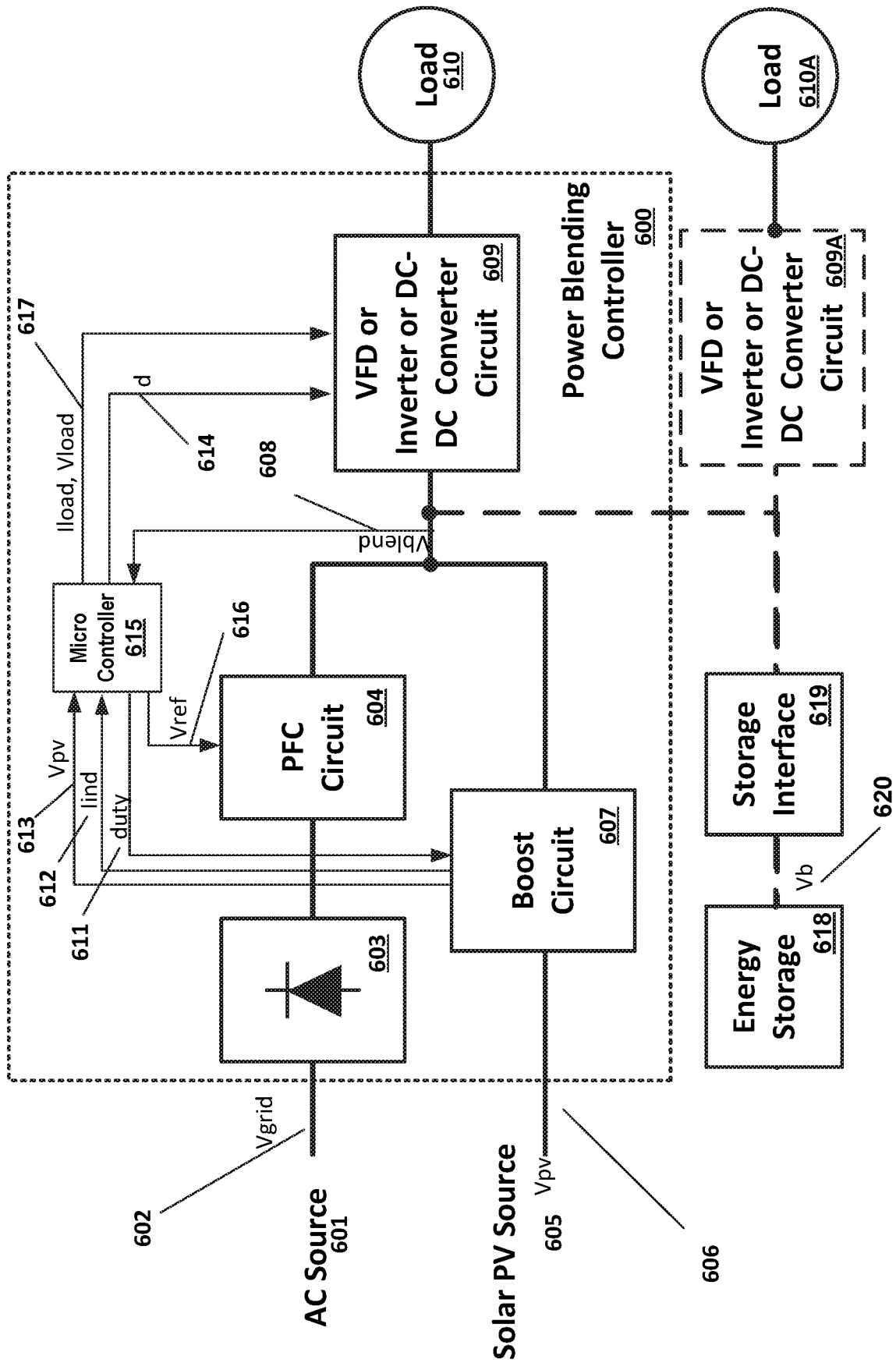


Fig. 6

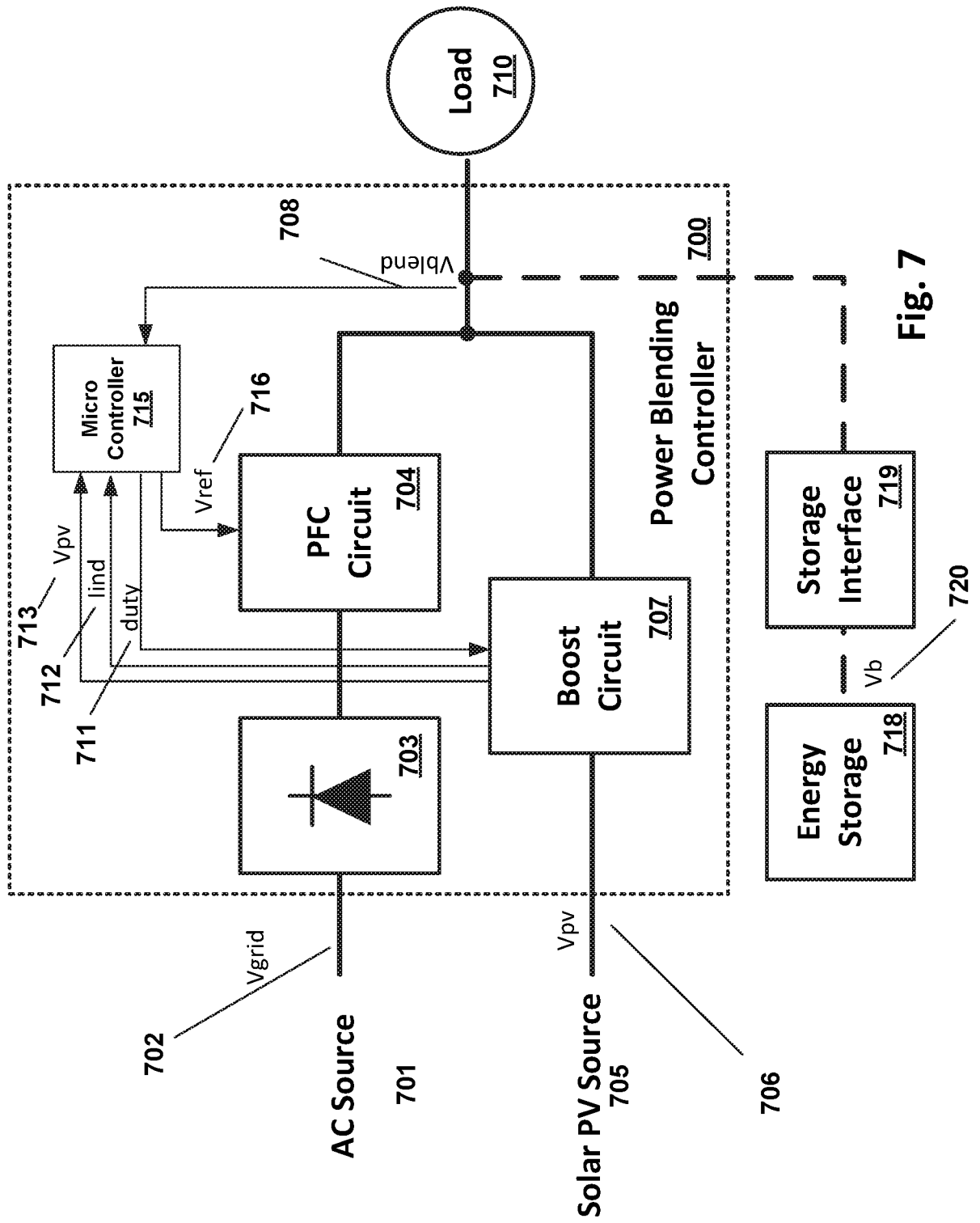


Fig. 7

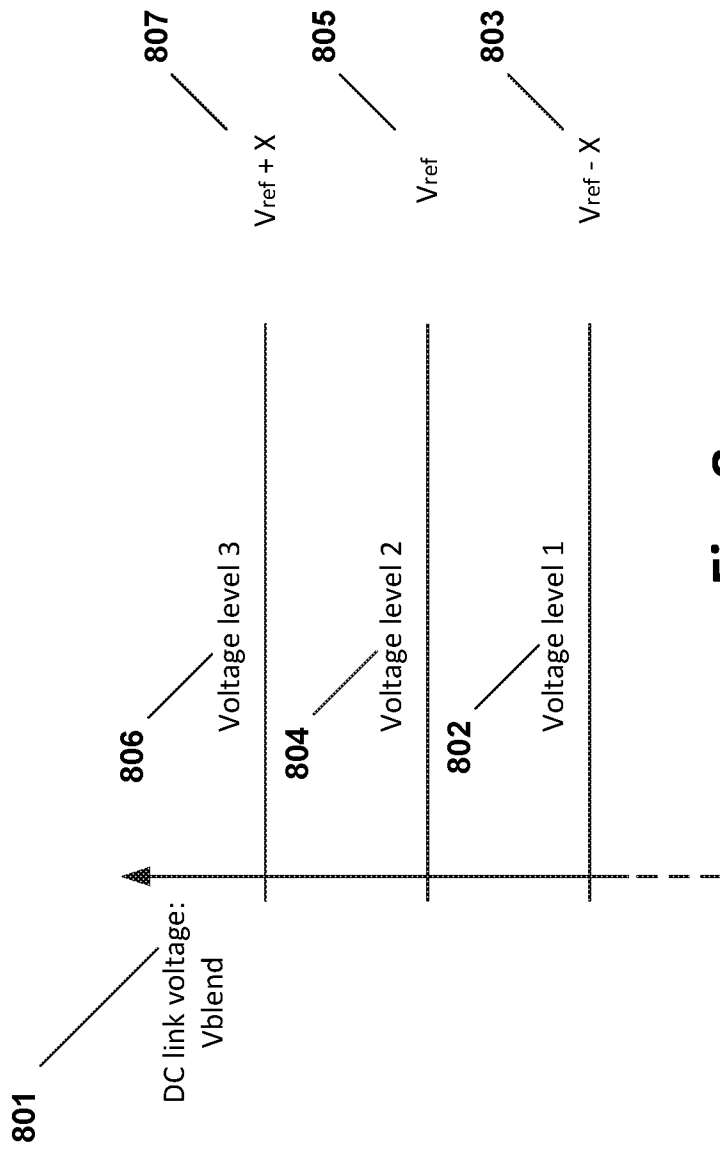
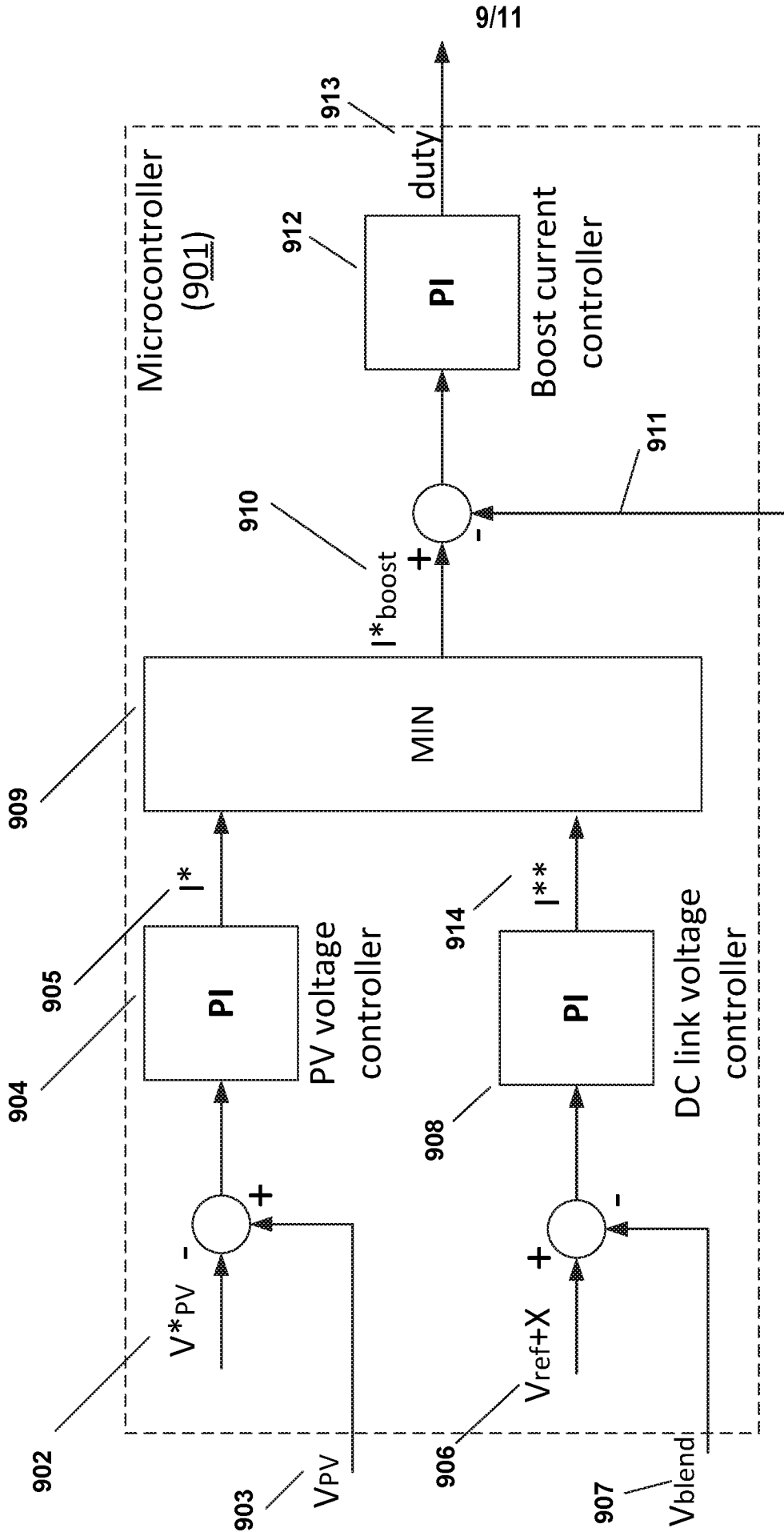


Fig. 8



I_{ind}

Fig. 9

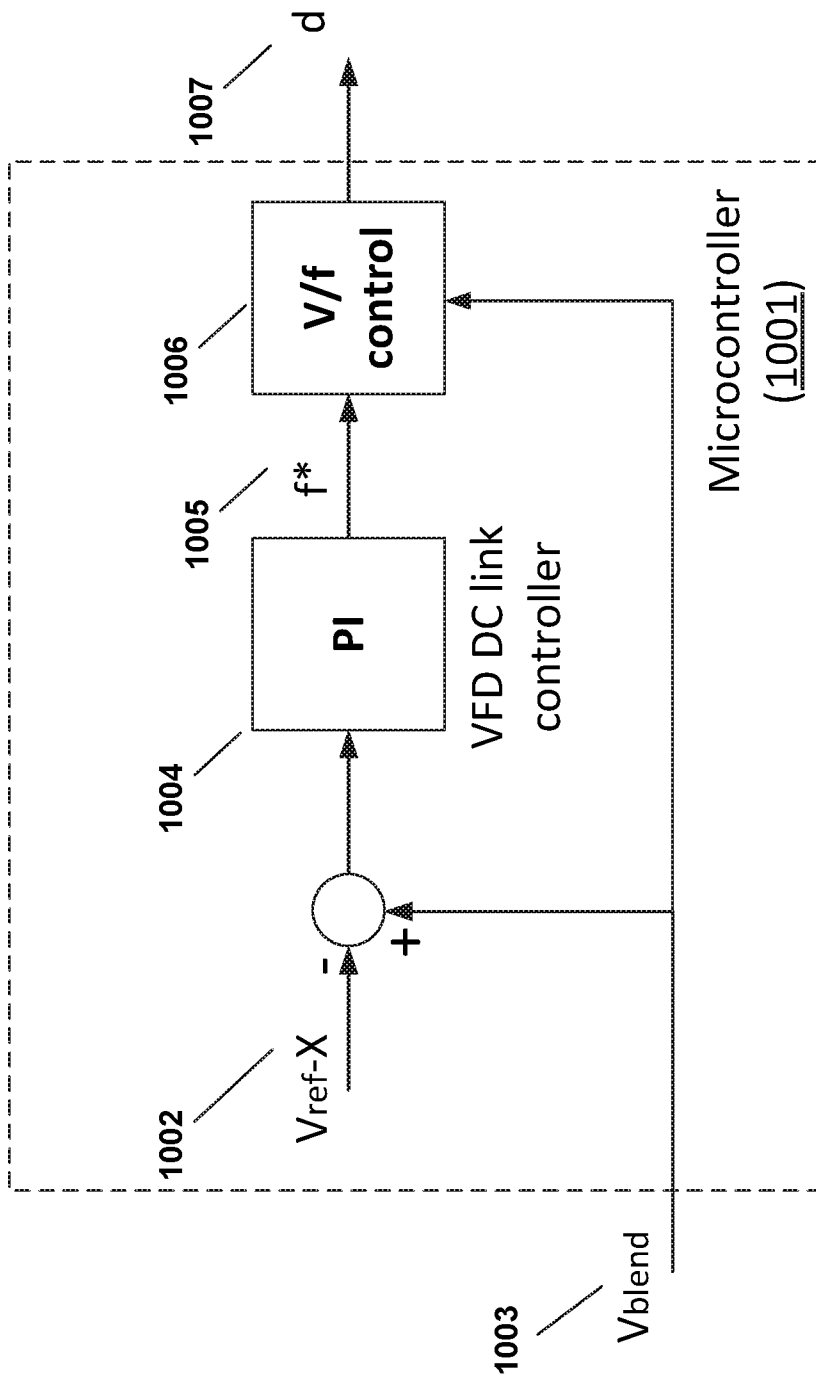


Fig. 10

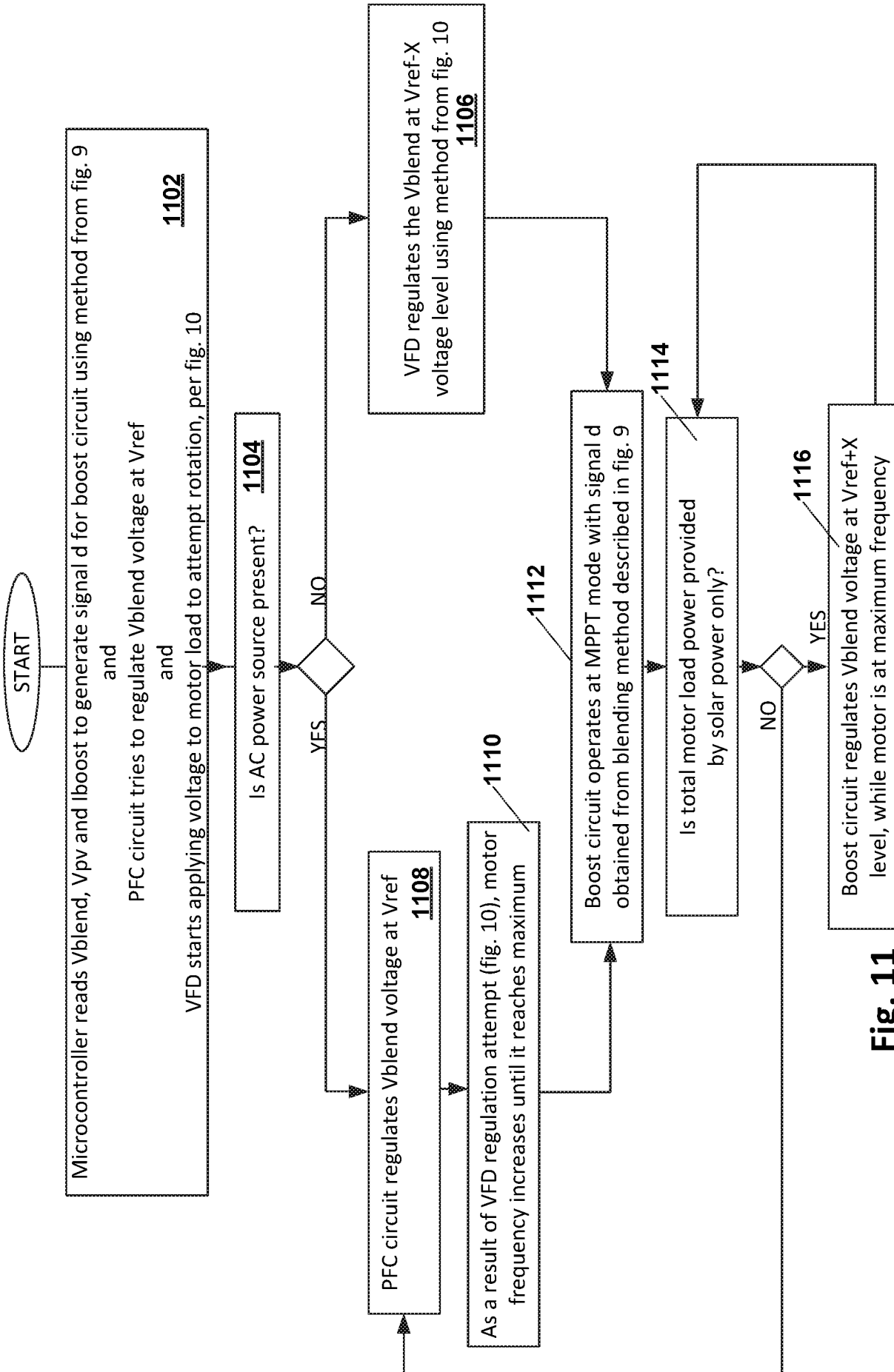


Fig. 11