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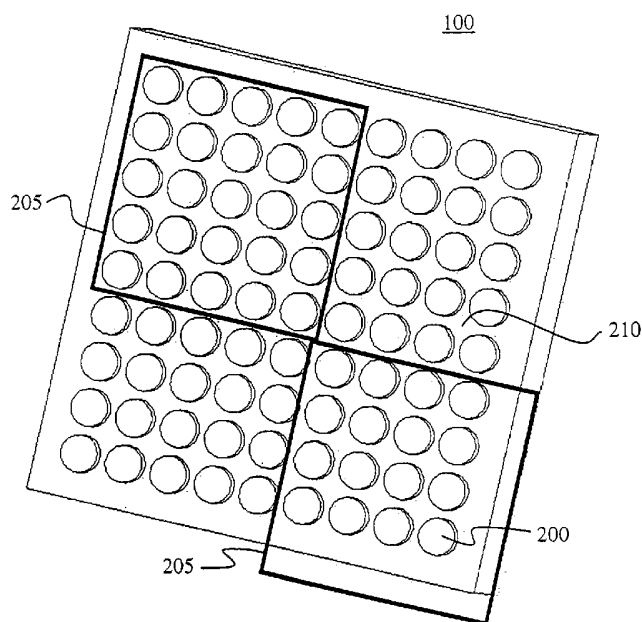
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(54) Title: DISPLAY DEVICE USING VERTICAL CAVITY LASER ARRAYS



(57) Abstract: A display apparatus for producing colored pixelated light includes a backlight unit for producing pump-beam light and a vertical cavity laser array device including a structure for modulating the properties of the device at spaced locations so as to provide an array of spaced laser pixels which have higher net gain than the interpixel regions, and an active region which includes portions for producing different colored light in response to the pump-beam light. The apparatus also includes a light shutter and a beam expander disposed over the light shutter for increasing the angular cone of view of the selected colored light.

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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

DISPLAY DEVICE USING VERTICAL CAVITY LASER ARRAYS

FIELD OF THE INVENTION

The present invention relates to a display device for producing colored light which uses a vertical cavity laser array.

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BACKGROUND OF THE INVENTION

In order to facilitate reading of the specification, the following terms are defined. Optic axis herein refers to the direction in which propagating light does not see birefringence. Polarizer and analyzer herein refer to elements that polarize electromagnetic waves. However, the one closer to the source of the light will be called a polarizer while the one closer to the viewer will be called an analyzer. Polarizing elements herein refers to both the polarizer and analyzer. Azimuthal angle ϕ and tilt angle θ are herein used to specify the direction of an optic axis. For the transmission axes of the polarizer and the analyzer, only the azimuthal angle ϕ is used, as their tilt angle θ is zero.

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FIG. 1 shows the definition of the azimuthal angle ϕ and tilt angle θ to specify the direction of the optic axis **1** with respect to the x-y-z coordinate system **3**. The x-y plane is parallel to the display surface **5**, and the z-axis is parallel to the display normal direction **7**. The azimuthal angle ϕ is the angle between the y-axis and the projection of the optic axis **9** onto the x-y plane. The tilt angle θ is the angle between the optic axis **1** and the x-y plane.

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There are a number of ways of producing pixelated colored light for display applications, such as for example, using a conventional passive or active matrix organic light emitting diode (OLED) device. Another way is to employ a liquid crystal display (LCD). In typical LCD systems, a liquid crystal cell is placed between a pair of polarizers. Light that enters the display is polarized by the initial polarizer. As the light passes through the liquid crystal cell, the molecular orientation of the liquid crystal material affects the polarized light such that it either passes through the analyzer or it is blocked by the analyzer. The orientation of the liquid crystal molecules can be altered by applying a voltage across the cell, thus enabling varying amounts of light intensity to pass through the LCD pixels. By employing this principle, minimal energy is required

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to switch the LCD. This switching energy is typically much less than that required for cathode ray tubes (CRT) employing cathodoluminescent materials, making a display that utilizes liquid crystal materials very attractive.

The typical liquid crystal cell contains a color filter array (CFA) comprised of red, green, and blue transmitting pixels. To transmit a large portion of the light from the backlight unit (BLU), the transmission spectra of each of the CFA pixels must have a large full-width at half maximum (FWHM). As a result of the large FWHM, the color gamut of the LCD is, at best, approximately 0.7 of the NTSC color gamut standard. Additionally, as light impinges on the CFA, more than two-thirds of that light is absorbed by the CFA, permitting for less than one-third to be transmitted. Correspondingly, this absorption of light outside of each pixel's transmission spectra results in a loss of overall display efficiency.

A transmissive LCD is illuminated by a backlight unit, including a light source, light guide plate (LGP), reflector, diffuser, collimating films, and a reflective polarizer. The reflective polarizer is used to recycle and reflect light of the undesired polarization. However, not all of the light of the undesired polarization is recycled and not all of the recycled light exits the BLU with the correct polarization state. Therefore, only a small portion of light reflected from the reflective polarizer is recycled into the correct polarization state. As a result, an unpolarized BLU light source results in nearly a factor of two efficiency loss upon passing through the bottom polarizer.

LCDs are quickly replacing CRTs and other types of electronic displays for computer monitors, televisions, and other office and household displays. However, LCD's suffer from poor contrast ratios at larger viewing angles. Unless the contrast ratio is improved at large viewing angles, the penetration of LCDs into certain markets will be limited. The poor contrast ratio is typically due to increased brightness of the display's dark state. LCDs are optimized such that the display has the highest contrast ratio within a narrow viewing cone centered on axis (at zero degrees viewing angle). As the display is viewed off-axis at larger viewing angles, the dark state experiences an increase in brightness, thus decreasing the contrast ratio. When viewing full color displays off axis, not only does the dark state increase in brightness, but also there is a shift

in color of both the dark and bright states. In the past there has been an attempt to improve this hue shift and loss of contrast ratio by various methods, such as the introduction of compensation films into the display or segmenting the pixel even further using multi-domains. However, these methods improve the hue shift and contrast ratio only slightly and for a limited viewing cone. Also, the manufacturing of compensation films and multi-domain liquid crystal cells is typically expensive, thus increasing the overall cost of the display.

Other flat panel displays try to solve the viewing angle problem by incorporating a photoluminescent (PL) screen on the front of the LCD, which is called a PL-LCD, as described in W. Crossland, SID Digest 837, (1997). This display employs a backlight unit of narrow band frequency, a liquid crystal modulator, and a photoluminescent output screen for producing color. The PL-LCD light source utilizes wavelengths that are in the UV, which would accelerate the breakdown of the liquid crystal materials. Also, the PL-LCD light source is much less efficient than the standard cold cathode fluorescent lamps (CCFLs) used in typical LCD displays.

In general, it would be beneficial to produce a display that did not suffer from the problems associated with typical LCD displays. As discussed above, these drawbacks are loss of efficiency (due to unpolarized backlights and usage of CFA's), poor color gamut, and loss of contrast and color at larger viewing angles. OLED displays overcome some of these disadvantages, however, they currently suffer from short lifetimes and higher manufacturing costs. Part of the higher manufacturing cost is inherent in the OLED design, such as the need to pixelate the OLED emitter region and the greater complexity of thin film transistors (TFTs) for current driven devices.

SUMMARY OF THE INVENTION

It is therefore an object of the present invention to provide a display that overcomes the disadvantages inherent in typical LCD displays, such as loss of efficiency, poorer color gamut, and lower contrast and color at larger viewing angles.

This object is achieved by a display apparatus for producing colored pixelated light, comprising:

- a) a backlight unit for producing pump-beam light;
- b) a vertical cavity laser array device including:
 - i) a structure for modulating the properties of the device at spaced locations so as to provide an array of spaced laser pixels which have higher net gain than the interpixel regions; and
 - ii) an active region which includes portions for producing different colored light in response to the pump-beam light;
- c) a light shutter; and
- d) a beam expander disposed over the light shutter for increasing the angular cone of view of the selected colored light.

ADVANTAGES

It is an advantage of the present invention to use a pixelated two-dimensional vertical cavity surface emitting laser (VCSEL) array as the light source for a liquid crystal display. Each color element contains thousands of micron-sized laser pixels, which are mutually incoherent. This leads to each color element producing multimode laser light. As a result of the pixel size being 3 to 5 microns in diameter, the divergence angle of the multimode laser light is on the order of 3-5°. This small divergence angle enables a 1:1 correspondence between the laser's color elements and the liquid crystal display's color elements. Correspondingly, it is no longer necessary to include the color filter array as one of the LCD film components.

Since the laser light passes through the LC switches on axis, the problems associated with contrast and color shifts for large viewing angles are limited. An additional feature of the near collimation of the light source is that the liquid crystal viewing angle compensation films can be removed from the display

structure. By including a birefringent layer as one of the VCSEL components, the multimode laser light output from the two-dimensional vertical cavity laser array can be polarized preferentially along one direction. As a result of the light source producing polarized light, the bottom polarizer element and its associated
5 reflective polarizer element can be deleted as elements of the LCD display. It is also common to include collimating films as part of the LCD components; however, these films can be removed since the laser output from the two-dimensional vertical cavity laser array is naturally collimated (3-5° divergence angle).

10 Additional advantages of the present invention come from the light output from each color element being nearly single wavelength. This property results in a large enhancement of the color gamut of the liquid crystal display. In applications that prefer a limited viewing angle, such as for privacy viewing, the near collimation of the light source results in a much enhanced on-axis viewing
15 brightness for the display compared to typical ones. This enhancement can either permit greatly increased display brightnesses or can be traded for greatly increased display power efficiency (enabling a large boost in the battery lifetime).

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 shows a perspective which is useful in understanding the
20 definition of the tilt and azimuthal angles to specify a direction of an optic axis;

FIG. 2 shows a side cross sectional schematic of an optically pumped two-dimensional VCSEL array device;

FIG. 3 shows a top view of a two-dimensional VCSEL array device containing red, green, and blue emitting elements in which each element is
25 composed of thousands of micron-sized laser pixels;

FIG. 4 shows a side view of another embodiment of an optically pumped two-dimensional VCSEL array device which includes absorbing elements;

FIG. 5 shows a side cross sectional view of another embodiment of
30 an optically pumped two-dimensional VCSEL array device which includes dyed photoresist absorbing elements;

FIG. 6 shows a side cross sectional view of another embodiment of an optically pumped two-dimensional VCSEL array device which includes planarized absorbing elements;

FIG. 7 shows a side cross sectional view of another embodiment of an optically pumped two-dimensional VCSEL array device which includes an etched dielectric stack;

FIG. 8 shows a side cross sectional view of another embodiment of an optically pumped two-dimensional VCSEL array device which includes an etched dielectric stack that has been planarized;

FIG. 9 is a simplified schematic of the display device containing the VCSEL array device;

FIG. 10 is a simplified schematic of a linear LED-array driven backlight unit pumping the VCSEL array device;

FIG. 11 is a simplified schematic of a planar LED-array driven backlight unit pumping the VCSEL array device;

FIG. 12 is a simplified schematic of a cold cathode fluorescent lamp driven backlight unit pumping the VCSEL array device;

FIG. 13 is simplified schematic of another embodiment of a cold cathode fluorescent lamp driven backlight unit pumping the VCSEL array device;

and

FIG. 14 is a simplified schematic of the liquid crystal cell and its components, including the analyzer.

DETAILED DESCRIPTION OF THE INVENTION

The invention is enabled by a light source that produces light output which is both nearly collimated and single wavelength. In addition, the light source must contain red, green, and blue emitting elements from a common substrate whose size is on the scale of $80 \times 240 \mu\text{m}$. A light source that meets these criteria is a two-dimensional vertical cavity surface emitting laser (VCSEL) array device **100**, as shown schematically in FIG. 2. FIG. 3 shows a top view of the two-dimensional VCSEL array device **100** where on the surface of the VCSEL needs to be defined red, green, and blue (RGB) emitting elements **205** which are composed of thousands of micron-sized laser pixels **200** separated by interpixel

regions **210**. In order to produce red, green, and blue laser light from a common substrate, it is preferred that an active region **130** be composed of organic-based gain media. However, recent research, R.N. Bhargava, Phys. Stat. Sol. 229, 897 (2002), points to the possibility of obtaining visible wavelength emission from
5 inorganic-based nanoparticles. Examples of these are ZnO nanoparticles (with preferred diameters less than 10 nm) either undoped or doped with impurities, such as, Mn^{2+} or Eu^{2+} .

If single mode lasing action were desired from each RGB emitting element **205**, then the emission from the various laser pixels **200** needs to be
10 phase-locked, i.e., intensity and phase information must be exchanged amongst the pixels (E. Kapon and M. Orenstein, U.S. Patent 5,086,430). In addition, the laser pixels **200** need to be the same size and positioned in a periodic array. However, having single mode laser output from each emitting element **205** would result in speckle, which is not desirable for display applications. As a result, it is
15 preferred that the individual laser pixels **200** be incoherent amongst themselves so as to result in multimode laser output from each emitting element **205**. Even though the laser pixels **200** do not exchange intensity and phase information between themselves, in order to obtain nearly collimated and single wavelength output from each emitting element **205**, each laser pixel needs to produce single
20 mode output. As a result, the preferred diameter of the laser pixels **200** is in the range of 2.5 to 4.5 μm , where smaller diameters result in increased scattering loss and larger diameters result in unwanted higher-order transverse modes.

The generalized methodology for producing a two-dimensional array of laser pixels is to modulate the net gain of the VCSEL device. This
25 modulation of the net gain can be obtained by a number of ways, such as selectively spoiling the emissive properties of the gain media in the active region **130**, selectively pumping the gain media in the active region **130**, and selectively etching one of the dielectric mirrors (stacks). A straightforward way to spoil the emissive properties of an organic-based gain media is to expose it to high levels of
30 UV radiation. In order to selectively pump the gain media in the active region **130**, an absorbing layer can be selectively deposited below the active region **130** (in the area underneath the interpixel regions **210**) such that it absorbs a pump-

beam light **180** prior to it entering the active region **130**. In both cases, the interpixel regions **210** are defined by where the net gain is lowered (through either spoiling the emissive properties or by absorbing the pump-beam light **180**), while the two-dimensional array of laser pixels **200** corresponds to the regions where the net gain is unmodified. For the case of selectively etching one of the dielectric stacks, the modulation is obtained by performing a two-dimensional etch of one of the dielectric stacks, such that, the interpixel regions **210** correspond to the etched areas (lower overall reflectance at the lasing wavelength) of the dielectric stack, whereas the unetched areas (higher overall reflectance at the lasing wavelength) correspond to the laser pixels **200**. For proper device operation, it is sufficient to etch either one or two periods of the dielectric stack. For the case of an organic-based gain media in the active region **130**, all device processing must be performed prior to depositing the organic components, since it is very difficult to perform micron-scale patterning on the laser structure once the organic layers have been deposited. As a result, the etching is performed on a bottom dielectric stack **120**. Even though weak confinement of the laser emission to the laser pixels **200** via net gain modulation can lead to phase-locked single mode lasing action in the best case, if phase-locking is only localized or if higher-order array modes are prevalent, then multimode lasing action will occur. In the present invention, multimode lasing action is preferred in order to prevent laser speckle. In such a case, in order to spoil even localized phase-locking, the size of the laser pixels **200** can be randomly varied from site to site, as well as placing the pixels on a randomly-arranged two-dimensional array.

Referring back to FIG. 2, the substrate **110** should be light transmissive. As a result, the substrate **110** can be transparent glass or plastic. On the substrate **110** is deposited the bottom dielectric stack **120**, which is composed of alternating high and low refractive index dielectric materials. In general, the bottom dielectric stack **120** is designed to be reflective to laser light over a predetermined range of wavelengths. Typical high and low refractive index materials are TiO_2 and SiO_2 , respectively. The bottom dielectric stack **120** can be deposited by plasma-enhanced chemical vapor deposition, electron-beam

(e-beam) deposition, or sputtering. Additional methodologies are polymeric extrusion, and sol-gel and colloidal depositions, as commonly practiced in the art.

As is well known in the art, the light output from VCSEL devices typically does not have a preferred orientation and can vary as a function of light intensity. Ways for fixing the polarization can be broken into two groups: 1) have the oscillator strength of the lasing transition be different for the transverse electric (TE) and transverse magnetic (TM) polarizations; and 2) have the dielectric stack reflectance be different for the two polarizations. The first approach is difficult to implement for gain media comprised of amorphous organic compounds. As a result, in one of the preferred embodiments the reflectance of either the top or bottom dielectric stacks is modified in order to make it birefringent. It has been shown for inorganic VCSEL devices that a 4% difference in the threshold modal gains between the TE and TM polarizations will result in greater than a 100:1 polarization mode suppression ratio (PMSR), Y. Ju, et al., Appl. Phys. Lett. 71, 741 (1997). The simplest route to enable this modal difference for amorphous organic laser systems is to replace one of the layers of the dielectric stack (preferably the stack with the lower peak reflectance) with a birefringent layer 126. As is well known in the art, these birefringent layers can have the index of refraction in the two polarization directions differing by as much as 0.25, with a 0.16 index difference being more common. It is simple to calculate using standard transfer matrix techniques that the modal difference between the two polarizations will be on the order of 22% if one of the stack layers (whose peak reflectance is on the order of 99%) is replaced by the birefringent layer 126, for which the index difference is 0.16. Since this modal difference is far greater than the one measured by Y. Ju, et al., Appl. Phys. Lett. 71, 741 (1997) for inorganic VCSELs, then the resulting PMSR should be much larger than 100:1. Even though the VCSEL array device 100 is described with reference to including a birefringent layer 126 in order to polarize the laser light 190, as is well known in the art, Y. Ju, et al., Appl. Phys. Lett. 71, 741 (1997), other ways can be employed to polarize the laser light 190 from the VCSEL array device 100.

The birefringent layer **126**, shown in FIG. 2, includes an alignment layer **128** and a birefringent material **129**, and is deposited over the bottom dielectric stack **120**. The birefringent layer **126** can also be disposed between the active region **130** and a top dielectric stack **140**. The birefringent layer **126** can also be disposed within one of the dielectric stacks. The alignment layer **128** can be oriented by the following techniques. The alignment layer contains a photo-orientable or photo-alignable material and can be oriented by a photo-alignment technique. Photo-orientable materials include, for example, photo-isomerization polymers, photo-dimerization polymers, and photo-decomposition polymers. In a preferred embodiment, the photo-orientable materials are cinnamic acid derivatives as disclosed in U.S. Patent 6,160,597. Such materials can be oriented and simultaneously crosslinked by irradiation with linearly polarized UV light. The alignment layer can also be oriented by mechanical rubbing, which is well known in the art. The photo-alignment process can be accomplished by using an apparatus as described in commonly assigned U.S. Patent Application Publication 2004/0008310 A1, the disclosure of which is herein incorporated by reference.

The birefringent material **129** is typically a liquid crystalline monomer when it is first disposed on the alignment layer **128**, and is crosslinked by UV irradiation, or polymerized by other ways such as heat. The birefringent material **129** can be a positive dielectric material, whose optic axis **1** has an average tilt angle between 0° and 20° . The birefringent material **129** can also be a negative dielectric material, whose optic axis **1** has an average tilt angle between 0° and 20° . In a preferred embodiment, the birefringent material **129** is comprised of diacrylate or diepoxide with positive birefringence as disclosed in U.S. Patent 6,160,597 (Schadt, et al.) and U.S. Patent 5,602,661 (Schadt, et al.). The optic axis **1** in the birefringent material **129** is usually untilted relative to the layer plane, and is uniform across the thickness direction.

The active region **130** is deposited over the bottom dielectric stack **120** or birefringent layer **126**, when it is included in the device. FIG. 2 shows that the active region **130** is not a bulk layer but a multilayer composite. The active region **130** contains one or more periodic gain regions **160**, which are separated by

spacer layers **170**. The thickness of the periodic gain regions **160** is typically less than 50 nm, with a preferred thickness of 5 to 30 nm. The thicknesses of the spacer layers **170** are chosen such that the periodic gain region(s) is aligned with the antinodes of the laser cavity's standing electromagnetic field (e-field).

5 Employing periodic gain region(s) **160** in the active region **130** results in larger power conversion efficiencies and a large reduction in the unwanted spontaneous emission. In summary, the active region **130** includes one or more periodic gain regions **160** and spacer layers **170** disposed on either side of the periodic gain region(s) and arranged so that the periodic gain region(s) is aligned with the
10 antinodes of the device's standing wave electromagnetic field.

The periodic gain region(s) **160** is composed of either small-molecular weight organic material, polymeric organic material, or inorganic-based nanoparticles, which fluoresce with a high quantum efficiency. The small-molecular weight organic material is typically deposited by high-vacuum
15 (10^{-6} Torr) thermal evaporation, while the conjugated polymers and inorganic nanoparticles are usually formed by spin casting.

Unless otherwise specifically stated, use of the term "substituted" or "substituent" means any group or atom other than hydrogen. Additionally, when the term "group" is used, it is meant that when a substituent group contains
20 a substitutable hydrogen, it is also intended to encompass not only the substituent's unsubstituted form, but also its form further substituted with any substituent group or groups as herein mentioned, so long as the substituent does not destroy properties necessary for device utility. Suitably, a substituent group can be halogen or can be bonded to the remainder of the molecule by an atom of
25 carbon, silicon, oxygen, nitrogen, phosphorous, sulfur, selenium, or boron. The substituent can be, for example, halogen, such as chloro, bromo or fluoro; nitro; hydroxyl; cyano; carboxyl; or groups which can be further substituted, such as alkyl, including straight or branched chain or cyclic alkyl, such as methyl, trifluoromethyl, ethyl, *t*-butyl, 3-(2,4-di-*t*-pentylphenoxy) propyl, and tetradecyl;
30 alkenyl, such as ethylene, 2-butene; alkoxy, such as methoxy, ethoxy, propoxy, butoxy, 2-methoxyethoxy, *sec*-butoxy, hexyloxy, 2-ethylhexyloxy, tetradecyloxy, 2-(2,4-di-*t*-pentylphenoxy)ethoxy, and 2-dodecyloxyethoxy; aryl such as phenyl,

4-*t*-butylphenyl, 2,4,6-trimethylphenyl, naphthyl; aryloxy, such as phenoxy, 2-methylphenoxy, alpha- or beta-naphthyloxy, and 4-tolyloxy; carbonamido, such as acetamido, benzamido, butyramido, tetradecanamido, alpha-(2,4-di-*t*-pentylphenoxy)acetamido, alpha-(2,4-di-*t*-pentylphenoxy)butyramido, alpha-(3-pentadecylphenoxy)-hexanamido, alpha-(4-hydroxy-3-*t*-butylphenoxy)-tetradecanamido, 2-oxo-pyrrolidin-1-yl, 2-oxo-5-tetradecylpyrrolin-1-yl, *N*-methyltetradecanamido, *N*-succinimido, *N*-phthalimido, 2,5-dioxo-1-oxazolidinyl, 3-dodecyl-2,5-dioxo-1-imidazolyl, and *N*-acetyl-*N*-dodecylamino, ethoxycarbonylamino, phenoxycarbonylamino, benzyloxycarbonylamino, hexadecyloxycarbonylamino, 2,4-di-*t*-butylphenoxycarbonylamino, phenylcarbonylamino, 2,5-(di-*t*-pentylphenyl)carbonylamino, *p*-dodecylphenylcarbonylamino, *p*-tolylcarbonylamino, *N*-methylureido, *N,N*-dimethylureido, *N*-methyl-*N*-dodecylureido, *N*-hexadecylureido, *N,N*-dioctadecylureido, *N,N*-dioctyl-*N'*-ethylureido, *N*-phenylureido, *N,N*-diphenylureido, *N*-phenyl-*N-p*-tolylureido, *N*-(*m*-hexadecylphenyl)ureido, *N,N*-(2,5-di-*t*-pentylphenyl)-*N'*-ethylureido, and *t*-butylcarbonamido; sulfonamido, such as methylsulfonamido, benzenesulfonamido, *p*-tolylsulfonamido, *p*-dodecylbenzenesulfonamido, *N*-methyltetradecylsulfonamido, *N,N*-dipropylsulfamoylamino, and hexadecylsulfonamido; sulfamoyl, such as *N*-methylsulfamoyl, *N*-ethylsulfamoyl, *N,N*-dipropylsulfamoyl, *N*-hexadecylsulfamoyl, *N,N*-dimethylsulfamoyl, *N*-[3-(dodecyloxy)propyl]-sulfamoyl, *N*-[4-(2,4-di-*t*-pentylphenoxy)butyl]sulfamoyl, *N*-methyl-*N*-tetradecylsulfamoyl, and *N*-dodecylsulfamoyl; carbamoyl, such as *N*-methylcarbamoyl, *N,N*-dibutylcarbamoyl, *N*-octadecylcarbamoyl, *N*-[4-(2,4-di-*t*-pentylphenoxy)butyl]carbamoyl, *N*-methyl-*N*-tetradecylcarbamoyl, and *N,N*-dioctylcarbamoyl; acyl, such as acetyl, (2,4-di-*t*-amylphenoxy)acetyl, phenoxycarbonyl, *p*-dodecyloxyphenoxycarbonyl methoxycarbonyl, butoxycarbonyl, tetradecyloxycarbonyl, ethoxycarbonyl, benzyloxycarbonyl, 3-pentadecyloxycarbonyl, and dodecyloxycarbonyl; sulfonyl, such as methoxysulfonyl, octyloxysulfonyl, tetradecyloxysulfonyl, 2-ethylhexyloxy-sulfonyl, phenoxysulfonyl, 2,4-di-*t*-pentylphenoxy-sulfonyl, methylsulfonyl, octylsulfonyl, 2-ethylhexylsulfonyl, dodecylsulfonyl, hexadecylsulfonyl,

phenylsulfonyl, 4-nonylphenylsulfonyl, and *p*-tolylsulfonyl; sulfonyloxy, such as dodecylsulfonyloxy, and hexadecylsulfonyloxy; sulfinyl, such as methylsulfinyl, octylsulfinyl, 2-ethylhexylsulfinyl, dodecylsulfinyl, hexadecylsulfinyl, phenylsulfinyl, 4-nonylphenylsulfinyl, and *p*-tolylsulfinyl; thio, such as ethylthio, 5 octylthio, benzylthio, tetradecylthio, 2-(2,4-di-*t*-pentylphenoxy)ethylthio, phenylthio, 2-butoxy-5-*t*-octylphenylthio, and *p*-tolylthio; acyloxy, such as acetyloxy, benzoyloxy, octadecanoyloxy, *p*-dodecylamidobenzoyloxy, *N*-phenylcarbamoyloxy, *N*-ethylcarbamoyloxy, and cyclohexylcarbonyloxy; amine, such as phenylanilino, 2-chloroanilino, diethylamine, dodecylamine; imino, such 10 as 1 (*N*-phenylimido)ethyl, *N*-succinimido or 3-benzylhydantoinyl; phosphate, such as dimethylphosphate and ethylbutylphosphate; phosphite, such as diethyl and dihexylphosphite; a heterocyclic group, a heterocyclic oxy group or a heterocyclic thio group, each of which can be substituted and which contain a 3 to 7 membered heterocyclic ring composed of carbon atoms and at least one hetero 15 atom selected from the group including oxygen, nitrogen, sulfur, phosphorous, or boron. such as 2-furyl, 2-thienyl, 2-benzimidazolyl or 2-benzothiazolyl; quaternary ammonium, such as triethylammonium; quaternary phosphonium, such as triphenylphosphonium; and silyloxy, such as trimethylsilyloxy.

If desired, the substituents can themselves be further substituted 20 one or more times with the described substituent groups. The particular substituents used can be selected by those skilled in the art to attain the desired properties for a specific application and can include, for example, electron-withdrawing groups, electron-donating groups, and steric groups. When a molecule can have two or more substituents, the substituents can be joined 25 together to form a ring such as a fused ring unless otherwise provided. Generally, the above groups and substituents thereof can include those having up to 48 carbon atoms, typically 1 to 36 carbon atoms and usually less than 24 carbon atoms, but greater numbers are possible depending on the particular substituents selected. Substitution can include fused ring derivatives such as but not limited to 30 benzo-, dibenzo-, naphtha-, or dinaphtho-fused derivatives. These fused ring derivatives can be further substituted as well.

The organic-based periodic gain region(s) **160** (or emissive material) can be comprised of a single host material, but more commonly includes a host material doped with a guest compound (dopant) or compounds where light emission comes primarily from the dopant and can be of any color. These host-dopant combinations are advantageous since they result in very small unpumped scattering/absorption losses for organic-based gain media (can be less than 1 cm^{-1}). The dopant is usually chosen from highly fluorescent dyes, but phosphorescent compounds, e.g., transition metal complexes as described for OLED applications in WO 98/55561, WO 00/18851, WO 00/57676, and WO 00/70655 are also useful. Dopants are typically coated as 0.01 to 10% by weight into the host material, wherein they can be selected to provide emitted light having hues of either red, green, or blue. An example of a useful host-dopant combination for red emitting layers is Alq as the host material and 1% L39 [4-(dicyanomethylene)-2-t-butyl-6-(1,1,7,7-tetramethyljulolidyl-9-enyl)-4H-pyran] as the dopant.

An important relationship for choosing a dye as a dopant is a comparison of the absorption of the dopant material and emission of the host material. For efficient energy transfer (via Forster energy transfer) from the host to the dopant molecule, a necessary condition is that the absorption of the dopant overlaps the emission of the host material. Those skilled in the art are familiar with the concept of Forster energy transfer, which involves a radiationless transfer of energy between the host and dopant molecules. An important relationship for choosing the host material is that the absorption of the host material significantly overlaps the emission spectrum of the pump-beam light **180**. In addition, it is preferred that the absorption of the host material or a host material plus a dopant is small at the laser emission wavelength of the VCSEL array device **100**. An acceptable level of absorption is that the absorption coefficient of the host plus dopant combination is less than 10 cm^{-1} at the wavelength of the laser emission.

Useful fluorescent emissive materials includes polycyclic aromatic compounds as described in I.B. Berlman, "Handbook of Fluorescence Spectra of Aromatic Molecules," Academic Press, New York, 1971 and EP 1 009 041.

Tertiary aromatic amines with more than two amine groups can be used including oligomeric materials.

Another class of useful emissive materials (for host or dopants) include aromatic tertiary amines, where the latter is understood to be a compound
 5 containing at least one trivalent nitrogen atom that is bonded only to carbon atoms, at least one of which is a member of an aromatic ring. In one form the aromatic tertiary amine can be an arylamine, such as a monoarylamine, diarylamine, triarylamine, or an oligomeric arylamine. Exemplary monomeric triarylamines are illustrated by Klupfel, et al. U.S. Patent 3,180,730. Other
 10 suitable triarylamines substituted with one or more vinyl radicals and/or comprising at least one active hydrogen containing group are disclosed by Brantley, et al. U.S. Patents 3,567,450 and 3,658,520.

A more preferred class of aromatic tertiary amines are those which include at least two aromatic tertiary amine moieties as described in U.S. Patents
 15 4,720,432 and 5,061,569. Such compounds include those represented by structural Formula A

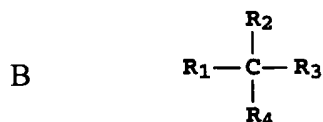


wherein:

Q₁ and Q₂ are independently selected aromatic tertiary amine moieties; and
 G is a linking group such as an arylene, cycloalkylene, or alkylene group
 20 of a carbon to carbon bond.

In one embodiment, at least one of Q₁ or Q₂ contains a polycyclic fused ring structure, e.g., a naphthalene. When G is an aryl group, it is conveniently a phenylene, biphenylene, or naphthalene moiety.

A useful class of triarylamines satisfying structural Formula A and
 25 containing two triarylamine moieties is represented by structural Formula B



where:

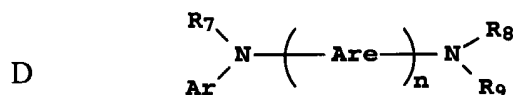
R₁ and R₂ each independently represent a hydrogen atom, an aryl group, or an alkyl group or R₁ and R₂ together represent the atoms completing a cycloalkyl group; and

R₃ and R₄ each independently represent an aryl group, which is in turn substituted with a diaryl substituted amino group, as indicated by structural Formula C



wherein R₅ and R₆ are independently selected aryl groups. In one embodiment, at least one of R₅ or R₆ contains a polycyclic fused ring structure, e.g., a naphthalene.

The host material can comprise a substituted or unsubstituted triarylamine compound. Another class of aromatic tertiary amines is the tetraaryldiamines. Desirable tetraaryldiamines include two diarylamino groups, such as indicated by Formula C, linked through an arylene group. Useful tetraaryldiamines include those represented by Formula D



wherein:

each Are is an independently selected arylene group, such as a phenylene or anthracene moiety;

n is an integer of from 1 to 4; and

Ar, R₇, R₈, and R₉ are independently selected aryl groups.

In a typical embodiment, at least one of Ar, R₇, R₈, and R₉ is a polycyclic fused ring structure, e.g., a naphthalene.

The various alkyl, alkylene, aryl, and arylene moieties of the foregoing structural Formulae A, B, C, D, can each in turn be substituted. Typical substituents include alkyl groups, alkoxy groups, aryl groups, aryloxy groups, and halogens such as fluoride, chloride, and bromide. The various alkyl and alkylene moieties typically contain from 1 to about 6 carbon atoms. The cycloalkyl moieties can contain from 3 to about 10 carbon atoms, but typically contain five,

six, or seven carbon atoms, e.g. cyclopentyl, cyclohexyl, and cycloheptyl ring structures. The aryl and arylene moieties are usually phenyl and phenylene moieties.

The emissive material can be formed of a single or a mixture of aromatic tertiary amine compounds. Specifically, one can employ a triarylamine, such as a triarylamine satisfying the Formula B, in combination with a tetraaryldiamine, such as indicated by Formula D. The host material can include a substituted or unsubstituted dicarbazole-biphenyl compound. Illustrative of useful aromatic tertiary amines is the following:

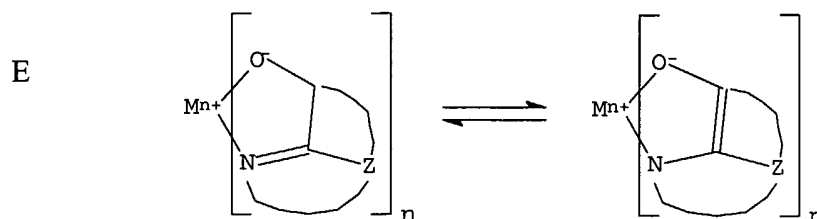
- 10 4,4'-*N,N'*-dicarbazole-1,1'-biphenyl (CBP) (D1);
 4,4'-Bis[N-(1-naphthyl)-N-phenylamino]biphenyl (D2);
 4,4'-Bis[N-(1-naphthyl)-N-(2-naphthyl)amino]biphenyl (D3);
 4,4'-Bis[N-(2-naphthyl)-N-*p*-tolylamino]biphenyl (D4);
 1,1-Bis(4-di-*p*-tolylaminophenyl)cyclohexane;
 15 1,1-Bis(4-di-*p*-tolylaminophenyl)-4-phenylcyclohexane;
 4,4'-Bis(diphenylamino)quadriphenyl;
 Bis(4-dimethylamino-2-methylphenyl)-phenylmethane;
 N,N,N-Tri(*p*-tolyl)amine;
 4-(di-*p*-tolylamino)-4'-[4(di-*p*-tolylamino)-styryl]stilbene;
 20 N,N,N',N'-Tetra-*p*-tolyl-4,4'-diaminobiphenyl;
 N,N,N',N'-Tetraphenyl-4,4'-diaminobiphenyl;
 N,N,N',N'-tetra-1-naphthyl-4,4'-diaminobiphenyl;
 N,N,N',N'-tetra-2-naphthyl-4,4'-diaminobiphenyl;
 N-Phenylcarbazole;
 25 4,4"-Bis[N-(1-naphthyl)-N-phenylamino]*p*-terphenyl;
 4,4'-Bis[N-(2-naphthyl)-N-phenylamino]biphenyl;
 4,4'-Bis[N-(3-acenaphthenyl)-N-phenylamino]biphenyl;
 1,5-Bis[N-(1-naphthyl)-N-phenylamino]naphthalene;
 4,4'-Bis[N-(9-anthryl)-N-phenylamino]biphenyl;
 30 4,4"-Bis[N-(1-anthryl)-N-phenylamino]-*p*-terphenyl;
 4,4'-Bis[N-(2-phenanthryl)-N-phenylamino]biphenyl;
 4,4'-Bis[N-(8-fluoranthryl)-N-phenylamino]biphenyl;

- 4,4'-Bis[N-(2-pyrenyl)-N-phenylamino]biphenyl;
 4,4'-Bis[N-(2-naphthacenyl)-N-phenylamino]biphenyl;
 4,4'-Bis[N-(2-perylenyl)-N-phenylamino]biphenyl;
 4,4'-Bis[N-(1-coronenyl)-N-phenylamino]biphenyl;
 5 2,6-Bis(di-*p*-tolylamino)naphthalene;
 2,6-Bis[di-(1-naphthyl)amino]naphthalene;
 2,6-Bis[N-(1-naphthyl)-N-(2-naphthyl)amino]naphthalene;
 N,N,N',N'-Tetra(2-naphthyl)-4,4''-diamino-*p*-terphenyl;
 4,4'-Bis{N-phenyl-N-[4-(1-naphthyl)-phenyl]amino}biphenyl;
 10 4,4'-Bis[N-phenyl-N-(2-pyrenyl)amino]biphenyl;
 2,6-Bis[N,N-di(2-naphthyl)amine]fluorene;
 1,5-Bis[N-(1-naphthyl)-N-phenylamino]naphthalene; and
 4,4',4''-tris[(3-methylphenyl)phenylamino]triphenylamine.

The host material can comprise a substituted or unsubstituted aza-
 15 aromatic compound. For example, the host material can comprise a substituted or
 unsubstituted acridine, quinoline, purine, phenazine, phenoxazine, or
 phenanthroline compound. Carbazole derivatives are useful hosts. Useful
 examples of phenanthroline materials include 2,9-dimethyl-4,7-diphenyl-1,10-
 phenanthroline and 4,7-diphenyl-1,10-phenanthroline.

20 Host and dopant molecules include, but are not limited to, those
 disclosed in U.S. Patents 4,768,292; 5,141,671; 5,150,006; 5,151,629; 5,405,709;
 5,484,922; 5,593,788; 5,645,948; 5,683,823; 5,755,999; 5,928,802; 5,935,720;
 5,935,721; and 6,020,078.

25 Metal complexes of 8-hydroxyquinoline and similar derivatives
 (Formula E) constitute one class of useful host materials capable of supporting
 electroluminescence, and are particularly suitable for light emission of
 wavelengths longer than 500 nm, e.g., green, yellow, orange, and red.



wherein:

M represents a metal;

n is an integer of from 1 to 3; and

- 5 Z independently in each occurrence represents the atoms completing a nucleus having at least two fused aromatic rings.

From the foregoing it is apparent that the metal can be monovalent, divalent, trivalent, or tetravalent metal. The metal can, for example, be an alkali metal, such as lithium, sodium, or potassium; an alkaline earth metal, such as
 10 magnesium or calcium; an earth metal, such aluminum or gallium, or a transition metal such as zinc or zirconium. Generally any monovalent, divalent, trivalent, or tetravalent metal known to be a useful chelating metal can be employed.

Z completes a heterocyclic nucleus containing at least two fused aromatic rings, at least one of which is an azole or azine ring. Additional rings, including both aliphatic and aromatic rings, can be fused with the two required
 15 rings, if required. To avoid adding molecular bulk without improving on function the number of ring atoms is usually maintained at 18 or less.

The host material can comprise a substituted or unsubstituted chelated oxinoid compound.

20 Illustrative of useful chelated oxinoid compounds are the following:

CO-1: Aluminum trisoxine [alias, tris(8-quinolinolato)aluminum(III)];

CO-2: Magnesium bisoxine [alias, bis(8-quinolinolato)magnesium(II)];

CO-3: Bis[benzo {f}-8-quinolinolato]zinc (II);

25 CO-4: Bis(2-methyl-8-quinolinolato)aluminum(III)- μ -oxo-bis(2-methyl-8-quinolinolato) aluminum(III);

CO-5: Indium trisoxine [alias, tris(8-quinolinolato)indium];

CO-6: Aluminum tris(5-methyloxine) [alias, tris(5-methyl-8-quinolinolato)aluminum(III)];

CO-7: Lithium oxine [alias, (8-quinolinolato)lithium(I)];

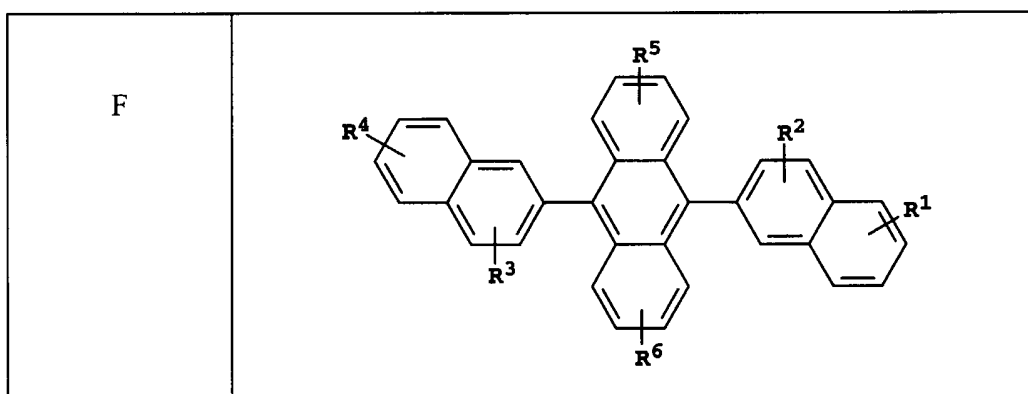
5 CO-8: Gallium oxine [alias, tris(8-quinolinolato)gallium(III)]; and

CO-9: Zirconium oxine [alias, tetra(8-quinolinolato)zirconium(IV)].

The host material can include a substituted or unsubstituted anthracene compound.

Derivatives of 9,10-di-(2-naphthyl)anthracene (Formula F)

10 constitute one class of useful hosts capable of supporting photoluminescence, and are particularly suitable for light emission of wavelengths longer than 400 nm, e.g. blue, green, yellow, orange or red.



wherein R^1 , R^2 , R^3 , R^4 , R^5 , and R^6 represent one or more substituents on each ring

15 where each substituent is individually selected from the following groups:

Group 1: hydrogen, or alkyl of from 1 to 24 carbon atoms;

Group 2: aryl or substituted aryl of from 5 to 20 carbon atoms;

Group 3: carbon atoms from 4 to 24 necessary to complete a fused aromatic ring of anthracenyl, pyrenyl, or perylenyl;

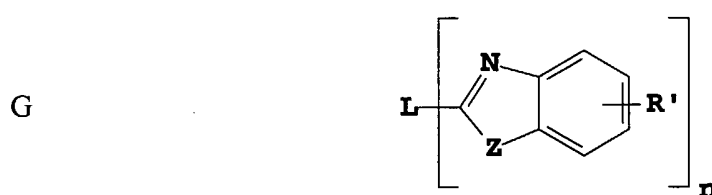
20 Group 4: heteroaryl or substituted heteroaryl of from 5 to 24 carbon atoms as necessary to complete a fused heteroaromatic ring of furyl, thienyl, pyridyl, quinolinyl or other heterocyclic systems;

Group 5: alkoxyamino, alkylamino, or arylamino of from 1 to 24 carbon atoms; and

25 Group 6: fluorine, chlorine, bromine or cyano.

Illustrative examples include 9,10-di-(2-naphthyl)anthracene (F1) and 2-*t*-butyl-9,10-di-(2-naphthyl)anthracene (F2). Other anthracene derivatives can be useful as a host, including derivatives of 9,10-bis-(4-(2,2'-diphenylethenyl)phenyl)anthracene.

5 Benzazole derivatives (Formula G) constitute another class of useful hosts capable of supporting photoluminescence, and are particularly suitable for light emission of wavelengths longer than 400 nm, e.g., blue, green, yellow, orange or red.



where:

10 n is an integer of 3 to 8;

Z is O, NR or S; and

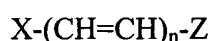
R and R' are individually hydrogen; alkyl of from 1 to 24 carbon atoms, for example, propyl, *t*-butyl, heptyl, and the like; aryl or hetero-atom substituted aryl of from 5 to 20 carbon atoms for example phenyl and naphthyl, furyl, thienyl, 15 pyridyl, quinolinyl and other heterocyclic systems; or halo such as chloro, fluoro; or atoms necessary to complete a fused aromatic ring; and

L is a linkage unit including alkyl, aryl, substituted alkyl, or substituted aryl, which conjugately or unconjugately connects the multiple benzazoles together. An example of a useful benzazole is 2, 2', 2''-(1,3,5-phenylene)tris[1- 20 phenyl-1H-benzimidazole].

The host material can comprise a substituted or unsubstituted benzoxazole compound, a substituted or unsubstituted benzothiazole compound, or a substituted or unsubstituted benzimidazole compound. The host material can comprise a substituted or unsubstituted oxazole compound, a substituted or 25 unsubstituted triazole compound, or a substituted or unsubstituted oxadiazole compound. Useful examples of oxazole compounds include 1,4-bis(5-phenyloxazol-2-yl)benzene, 1,4-bis(4-methyl-5-phenyloxazol-2-yl)benzene, and 1,4-bis(5-(*p*-biphenyl)oxazol-2-yl)benzene. Useful examples of oxadiazole

compounds include 2-(4-biphenyl)-5-phenyl-1,3,4-oxadiazole and 2-(4-biphenyl)-5-(4-tert-butylphenyl)-1,3,4-oxadiazole. Useful examples of triazole compounds include 3-(4-biphenyl)-4-phenyl-5-tert-butylphenyl-1,2,4-triazole.

Distyrylarylene derivatives are also useful as host materials or
 5 dopant materials. Many examples are described in U.S. Patent 5,121,029. Useful emissive materials (hosts and dopants) can have the general Formulae



where:

X and Z are independently a substituted or unsubstituted aromatic group or a substituted or unsubstituted aromatic complex ring group having one nitrogen atom;

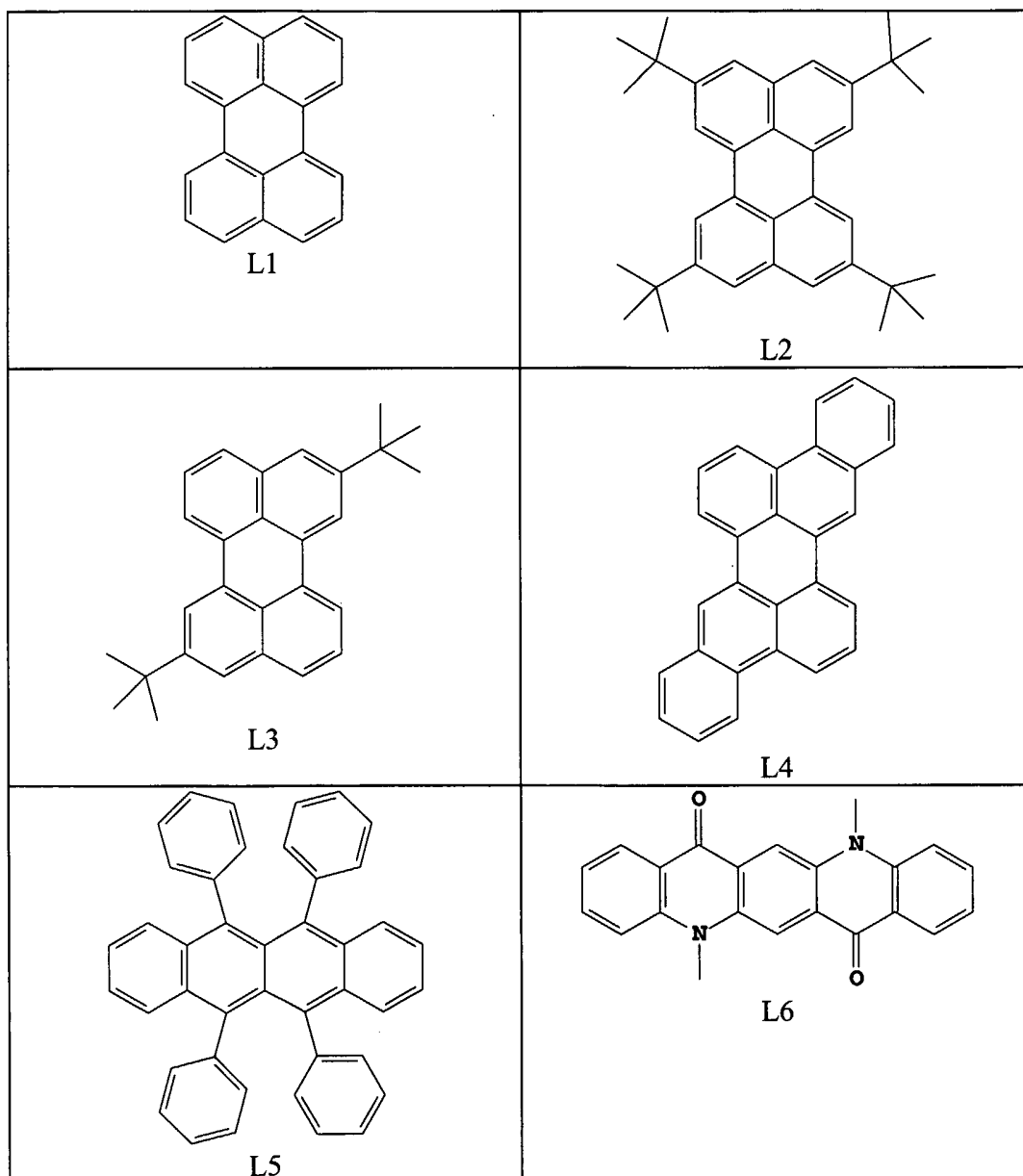
n equals 1, 2, or 3; and

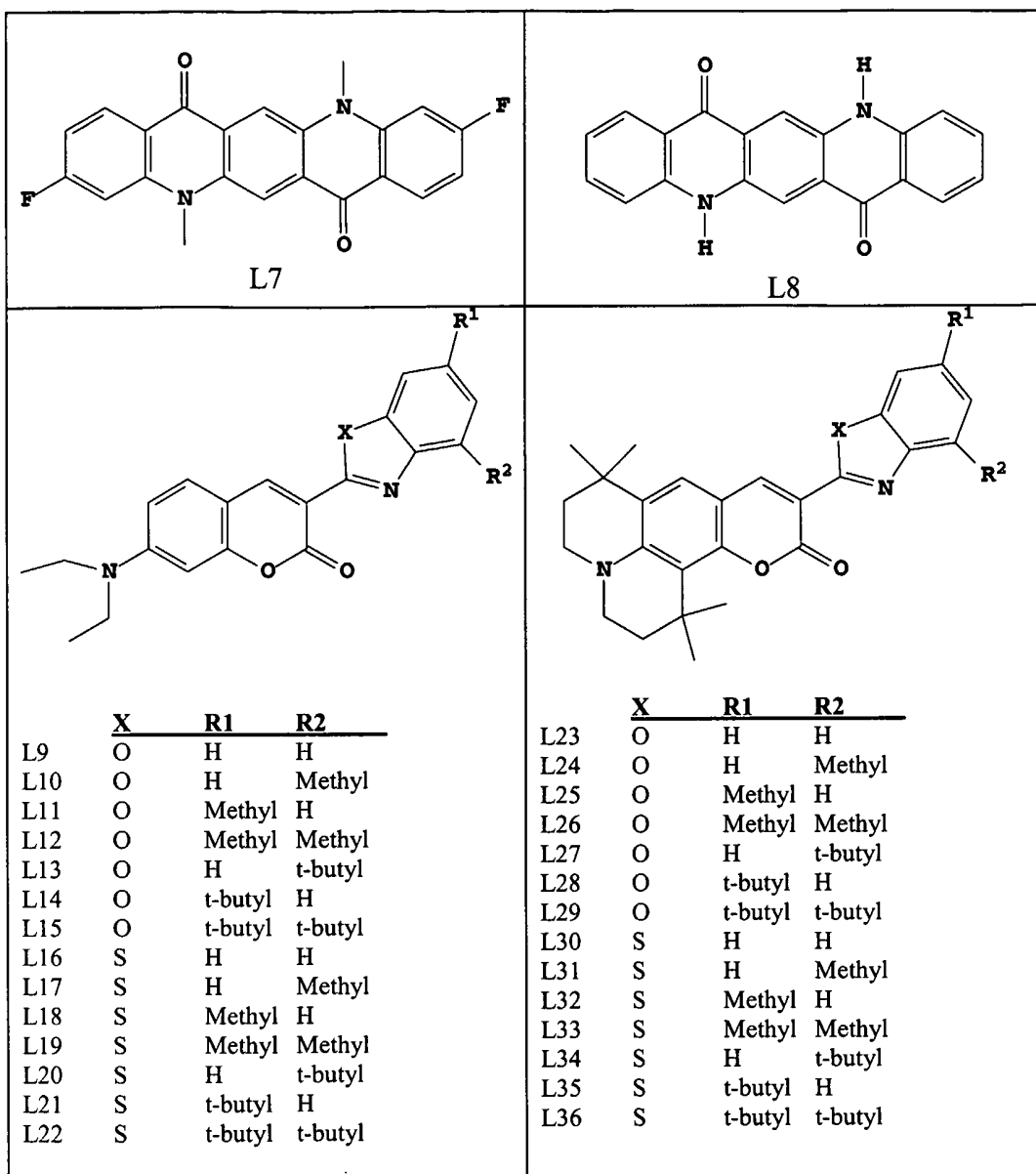
Y is a divalent aromatic group or a divalent aromatic complex ring group having one nitrogen atom. Useful examples include 1,4-bis(2-methylstyryl)-benzene, 4,4'-(9,10-anthracenediyl)-2,1-ethenediylbis(N,N-bis(4-methylphenyl)-benzenamine, 4,4'-(1,4-naphthalenediyl)-2,1-ethenediylbis(N,N-bis(4-methylphenyl)benzenamine, and 4,4'-(1,4-phenylenedi-2,1-ethenediyl)bis(N,N-(4-tolyl))benzenamine.

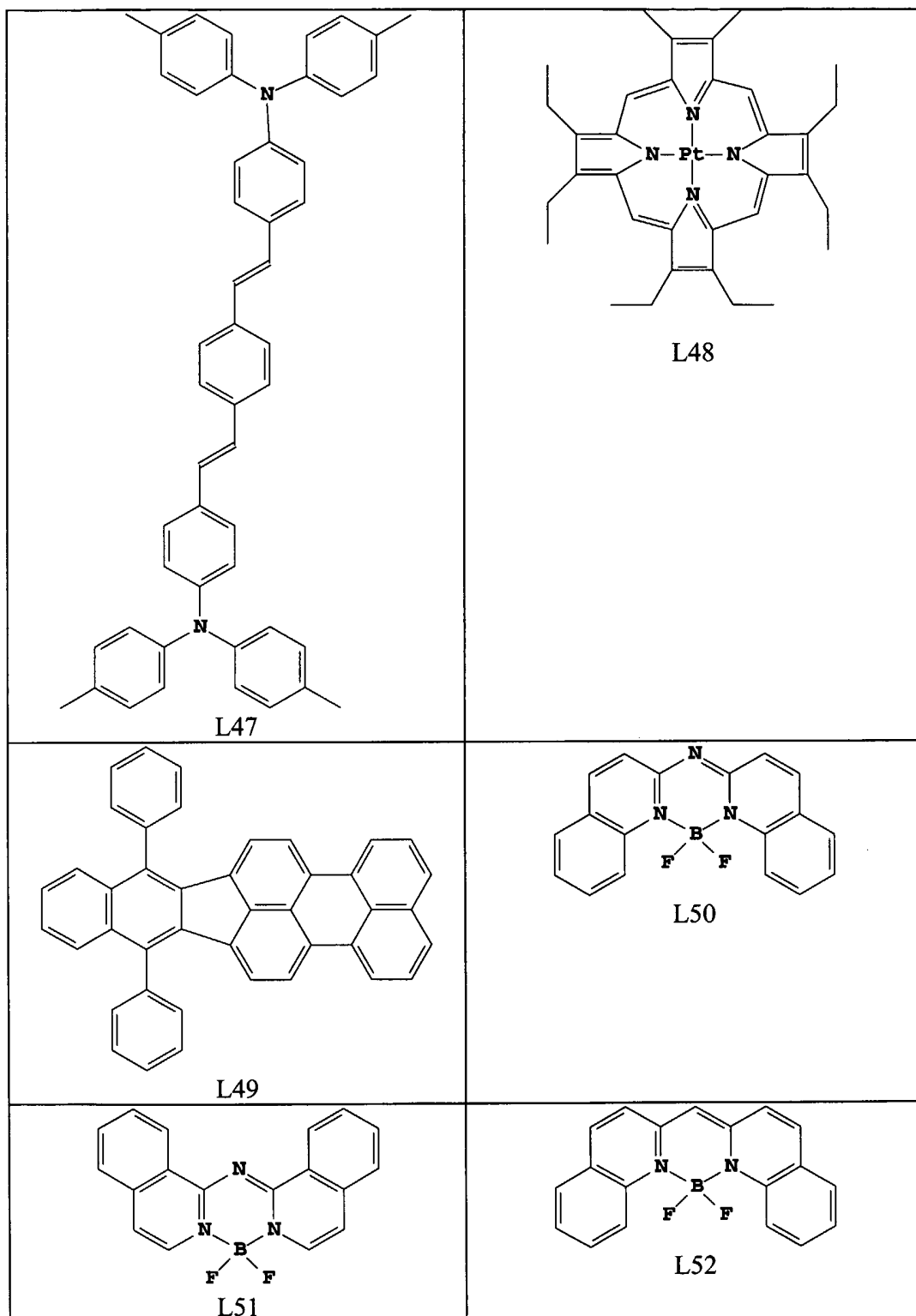
The organic-based dopant is selected to provide emission between
 10 300-1700 nm. The dopant can be selected from fluorescent or phosphorescent dyes. Useful fluorescent dopants include materials as described as host materials above. Other useful fluorescent dopants include, but are not limited to, derivatives of substituted or unsubstituted anthracene, tetracene, xanthene, perylene, rubrene, coumarin, rhodamine, and quinacridone,
 15 dicyanomethylenepyran compounds, thiopyran compounds, polymethine compounds, pyrilium and thiapyrilium compounds, fluorene derivatives, perflanthene derivatives, indenoperylene derivatives, bis(aziny)amine boron compounds, bis(aziny)methane compounds, naphthyridine, fluoranthene, furan, indole, thiaphene, benzoxanthene, pyrene, peropyrene, terphenyl, quaterphenyl,
 20 quinquephenyl, sexiphenyl, anthanthrene, bisanthrene compounds, N,N,N',N'-tetrasubstituted benzidene derivatives, N,N,N',N'-tetrylbenzidene derivatives

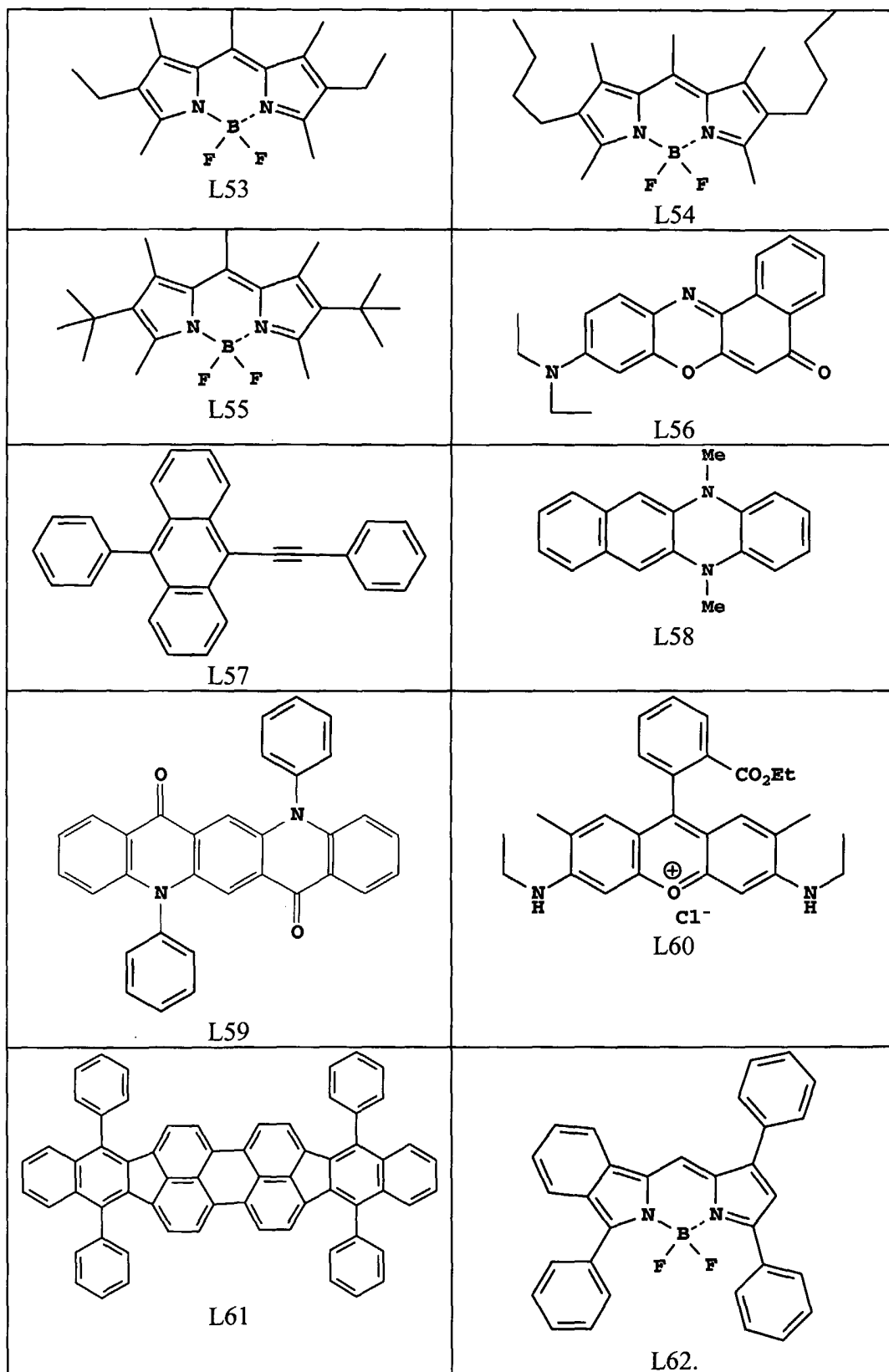
and carbostyryl compounds or combinations thereof. Derivatives of these classes of materials can also serve as useful host materials or combinations thereof. Host materials will often be compounds containing at least three phenylene moieties.

Illustrative examples of useful dopants include, but are not limited to, the following:









Other emissive materials include various heterocyclic optical brighteners as described in U.S. Patent 4,539,507.

The emissive material can also be a polymeric material, a blend of two or more polymeric materials, or a doped polymer or polymer blend. The emissive material can also include more than one nonpolymeric and polymeric material with or without dopants. Typical dopants are listed previously for nonpolymeric molecules. Nonpolymeric dopants can be molecularly dispersed into the polymeric host, or the dopant could be added by copolymerizing a minor constituent into the host polymer. Typical polymeric materials include, but are not limited to, substituted and unsubstituted poly(p-phenylenevinylene) (PPV) derivatives, substituted and unsubstituted poly(p-phenylene) (PPP) derivatives, substituted and unsubstituted polyfluorene (PF) derivatives, substituted and unsubstituted poly(p-pyridine), substituted and unsubstituted poly(p-pyridalvinylene) derivatives, and substituted, unsubstituted poly(p-phenylene) ladder and step-ladder polymers, and copolymers thereof as taught by Diaz-Garcia, et al. in U.S. Patent 5,881,083 and references therein. The substituents include but are not limited to alkyls, cycloalkyls, alkenyls, aryls, heteroaryls, alkoxy, aryloxy, amino, nitro, thio, halo, hydroxy, and cyano. Typical polymers are poly(p-phenylene vinylene), dialkyl-, diaryl-, diamino-, or dialkoxy-substituted PPV, mono alkyl-mono alkoxy-substituted PPV, mono aryl-substituted PPV, 9,9'-dialkyl or diaryl-substituted PF, 9,9'-mono alkyl-mono aryl substituted PF, 9-mono alkyl or aryl substituted PF, PPP, dialkyl-, diamino-, diaryl-, or dialkoxy-substituted PPP, mono alkyl-, aryl-, alkoxy-, or amino-substituted PPP. In addition, polymeric materials can be used such as poly(N-vinylcarbazole) (PVK), polythiophenes, polypyrrole, polyaniline, and copolymers such as poly(3,4-ethylenedioxythiophene)/poly(4-styrenesulfonate) also called PEDOT/PSS.

The organic materials mentioned above are suitably deposited through sublimation, but can be deposited from a solvent with an optional binder to improve film formation. If the material is a polymer, solvent deposition is usually preferred. The material to be deposited by sublimation can be vaporized from a sublimator "boat" often comprised of a tantalum material, e.g. as described

in U.S. Patent 6,237,529, or can be first coated onto a donor sheet and then sublimed in closer proximity to the substrate. Layers with a mixture of materials can utilize separate sublimator boats or the materials can be pre-mixed and coated from a single boat or donor sheet.

5 As shown in FIG. 3 and discussed above, the VCSEL array contains red, green, and blue emitting pixels with dimensions on the order of 80 x 240 μm . The emission color is determined by the combination of the length of the lasing path and the fluorescence spectrum of the gain media contained in the periodic gain region **160**. Patterned deposition of the gain media contained in
10 the periodic gain region **160** can be achieved using shadow masks, integral shadow masks (U.S. Patent 5,294,870), spatially-defined thermal dye transfer from a donor sheet (U.S. Patents 5,688,551; 5,851,709; and 6,066,357) and inkjet methods (U.S. Patent 6,066,357). If the periodic gain region **160** is more than one layer, then the patterned deposition needs to be repeated accordingly.

Most organic-based laser devices are sensitive to moisture or oxygen, or both, so they are commonly sealed in an inert atmosphere such as nitrogen or argon. Desiccant such as alumina, bauxite, calcium sulfate, clays, silica gel, zeolites, alkaline metal oxides, alkaline earth metal oxides, sulfates, or metal halides and perchlorates can be incorporated into the sealed device. Methods for encapsulation and desiccation include, but are not limited to, those described in U.S. Patent 6,226,890. In addition, barrier layers such as SiO_x, Teflon, and alternating inorganic/polymeric layers are known in the art for encapsulation.

15 For the spacer layer **170** it is preferred to use a material that is highly transparent to both the laser light **190** and the pump-beam light **180**. In this embodiment 1,1-Bis-(4-bis(4-methyl-phenyl)-amino-phenyl)-cyclohexane (TAPC) is chosen as the spacer material, since it has very low absorption throughout the visible and near UV spectrum and its index of refraction is slightly
20 lower than that of most organic host materials. This refractive index difference is useful since it helps in maximizing the overlap between the standing e-field antinodes and the periodic gain region(s) **160**. Besides organic spacer materials, the spacer layer **170** can also be composed of inorganic materials, such as SiO₂,

since it has low absorption and its index of refraction is less than that of organic host materials. When using inorganic-based spacer layers, the materials can be deposited either by thermal evaporation, e-beam at low deposition temperatures (around 70°C), or colloidal methods.

5 Following the deposition of the active region **130**, it is necessary to spatially pattern the net gain of the periodic gain region(s) **160** in order to form the lower net gain regions **150**. For the embodiment shown in FIG. 2, the lower net gain regions **150** are produced by locally spoiling the emissive properties of the periodic gain region(s) **160**. An effective way to form the lower net gain regions

10 **150** (for organic-based gain media) is to use standard photolithographic masks and UV exposing apparatus in order to produce a patterned UV exposure of the periodic gain region(s) **160**. Since organic media is sensitive to high intensity UV light (for example the mercury arc lamp's i-line at 365 nm), this technique works very effectively to lower the emissive intensity of the UV exposed areas of the

15 periodic gain region(s) **160**. As discussed above, the UV exposed areas (the lower net gain regions **150**) correspond to the interpixel region **210**, while the unexposed areas correspond to the laser pixels **200**. In the preferred embodiment the shape of the laser pixels **200** is circular; however, other pixel shapes are possible, such as rectangular. The size of the laser pixels **200** is in the range of 2.5 to 20 microns.

20 For single transverse mode laser operation, the preferred laser pixel **200** diameter is 2.5 to 4.5 μm . The interpixel spacing is in the range of 0.25 to 4 μm . In general, the spaced laser pixels **200** can have the same or different sizes and the spacings between pixels can have the same or different lengths to cause the output of the VCSEL array device **100** to produce locally single or multimode laser output. It

25 should be noted that the emissive intensity of the periodic gain region(s) **160** can be locally modulated by ways other than high intensity UV radiation, such as those ways commonly practiced in the art.

 Following the growth of the active region **130** and the production of the lower net gain regions **150** is the deposition of the top dielectric stack **140**.

30 The top dielectric stack **140** is spaced from the bottom dielectric stack **120** and reflective to light over a predetermined range of wavelengths. Its composition is analogous to that of the bottom dielectric stack. Since the top dielectric stack **140**

is deposited over an active region **130** that contains organics (for the case of organic-based gain media), its deposition temperature must be kept low in order to avoid melting the organics. As a result, a typical deposition temperature for the top dielectric stack **140** is 100°C or lower. The top dielectric stack can be
5 deposited by conventional ways, such as e-beam, low-energy sputtering, or colloidal deposition. In order to obtain effective lasing performance, it is preferred that the peak reflectivities of the top and bottom dielectric stacks be greater than 99%, where smaller values result in larger lasing linewidths.

The VCSEL array device **100** is optically driven by an incident
10 pump-beam light **180** and emits laser light **190**. As a result of the small lasing power density threshold of organic-based VCSEL laser cavities, the pump-beam can be incoherent LED light. FIG. 2 shows laser light **190** through the top dielectric stack **140**. Alternatively, the laser structure could be optically pumped through the top dielectric stack **140** with the laser light **190** through the substrate
15 **110** by proper design of the dielectric stack reflectance properties. The operation of the VCSEL array device **100** occurs by the following ways. The pump-beam light **180** transmits through the substrate **110** and the bottom dielectric stack **120** and is absorbed by the periodic gain region(s) **160**, wherein some fraction of the pump-beam energy is re-emitted as longer wavelength laser light at the position of
20 the laser pixels **200**. When the pump-beam light **180** enters through the substrate **110**, to ensure that the laser light **190** mainly exits through the top dielectric stack **140**, it is necessary to choose the top dielectric stack peak reflectance to be smaller than the bottom dielectric stack **120** peak reflectance. To improve the power conversion efficiency of the device, it is common practice to add additional
25 dielectric layers to both dielectric stacks, such that, the top dielectric stack **140** is highly reflective to the pump-beam light **180** and the bottom dielectric stack **120** is highly transmissive to the pump-beam light **180**.

As discussed above, another way for spatially modulating the net gain of the periodic gain region(s) **160** is to modulate the excitation of the periodic
30 gain region(s) **160** by the pump-beam light **180**. Another embodiment of the present invention is given in FIG. 4, laser array device **102**, which contains absorbing elements **155**. In order to form micron-sized laser pixel features and to

reduce diffraction effects, it is preferred that the absorbing elements **155** be placed adjacent to the active region **130**. As discussed above, performing photolithographic-based processing on laser devices is difficult once the organics have been deposited; accordingly, it is preferred to place the absorbing elements

5 between the birefringent layer **126** and the active region **130** as shown in FIG. 4. The composition of the absorbing elements **155** is any material that absorbs the pump-beam light **180** and only minimally absorbs and scatters the laser light **190**. It is preferred that at the emission wavelengths of the pump-beam light **180**, the absorbing elements' **155** absorption coefficient is greater than 10^4 cm^{-1} . The

10 thickness of the absorbing elements **155** is chosen such that a significant percentage of the pump-beam light **180** is absorbed by the elements. A preferred absorption fraction is greater than 25%. With regard to producing a patterned absorber layer, this can be accomplished by a number of ways. The first way is to deposit a uniform dye layer **157** and use patterned UV light to modify selectively

15 the absorption coefficient of the dye layer **157**. As discussed above with reference to FIG. 2, the UV light can be patterned using conventional photolithographic masks. With respect to modifying the absorption coefficient of the dye layer **157**, this can be accomplished either through bleaching the dye molecules (lowering the absorption selectively) or by dissociating the dye molecules to produce a

20 species, which more strongly absorbs the pump-beam light **180** (raising the absorption selectively). As stated above, it is preferred that both the dye layer **157** and the absorbing elements **155** only weakly absorb/scatter the laser light **190**. A nice feature of this way of producing the absorbing elements **155** is that it results in laser array device **102** being planar.

25 Another way for depositing the absorbing elements **155** is to use a dyed photoresist. The resulting laser array device **103** is illustrated in FIG. 5. These types of dyed photoresists are well known in the art, and are spin cast and patterned by standard photolithographic techniques. For either laser array device **102** or **103**, following the production of the spaced-apart absorbing elements **155**,

30 the active region **130** and the top dielectric stack **140** are deposited in sequence. Since the absorbing elements **155** need to be placed between the birefringent layer **126** and the active region **130**, and absorb a portion of the pump-beam light **180**, it

is necessary for the pump-beam light **180** to enter through the substrate **110**. There are also other ways, as commonly practiced in the art, to produce the absorbing elements **155**. For example, etched pits can be formed in a transparent layer (such as SiO₂), over which can be deposited the absorbing elements **155** material. Next, standard chemical mechanical polishing (CMP) techniques can be used to polish down the absorbing elements **155** material such that it only remains in the etched pit regions. As discussed above, the positions of the absorbing elements **155** correspond to the interpixel region **210**, while the remaining areas correspond to the laser pixels **200**. In the preferred embodiment the shape of the laser pixels **200** is circular; however, other pixel shapes are possible, such as rectangular. The size of the laser pixels **200** is in the range of 2.5 to 20 microns. For single transverse mode laser operation, the preferred laser pixel **200** diameter is 2.5 to 4.5 μm. The interpixel spacing is in the range of 0.25 to 4 μm. In general, the spaced laser pixels **200** can have the same or different sizes and the spacings between pixels can have the same or different lengths to cause the output of the laser array device **102** or **103** to produce locally single or multimode laser output.

FIG. 6 shows another embodiment of the present invention. This laser array device **104** is a variation of the one illustrated in FIG. 5. In FIG. 5 the active region **130** is grown directly on the absorbing elements **155**. As a result, the active region **130** and the top dielectric stack **140** are deposited on a non-planar (corrugated) surface for the case of the absorbing elements formed by dyed photoresist (note that the case of growing in the etch pits followed by CMP results in a planar surface). For certain multilayer stack combinations, such as TiO₂-SiO₂, deposition on a corrugated surface can lead to columnar growth of the stacks. As a result, there is enhanced scattering losses in the top dielectric stack **140**. To overcome this problem the absorbing elements **155** are planarized by a planarization layer **158**, using techniques well known in the art, prior to depositing the active region **130**. In one embodiment, following the production of the spaced apart absorbing elements **155**, the planarization layer **158** material is deposited by suitable processes. Next, using CMP techniques, which are well known in the art, the planarization layer **158** material is polished until it is flush (or within a couple

tens of nanometers) with the top surface of the absorbing elements **155**. A second embodiment of the planarization layer **158** is to use polymethyl-methacrylate (PMMA). In this case PMMA is spun cast over the spaced apart absorbing elements **155** to a thickness range of .5 to 3.0 μm , followed by a conventional
5 bake at 150 to 220°C. Scanning electron microscope (SEM) images reveal that a 3:1 or 4:1 PMMA thickness to absorbing element thickness ratio typically results in the planarization of the PMMA surface. Besides these three embodiments for planarization, other methodologies are possible as practiced by those skilled in the art. In summary, the addition of the planarization layer **158** following the
10 production of the spaced apart absorbing elements **155** and prior to the deposition of the active region **130**, leads to less scattering loss in the active region **130** and in the top dielectric stack **140** and results in higher power conversion efficiencies for the case of the absorbing elements **155** formed by dyed photoresist.

FIG. 7 shows another embodiment of the present invention, laser
15 array device **106**. In this case, the way for spatially modulating the net gain of the VCSEL device is to etch selectively (reflectance modulation) the bottom dielectric stack **120**. In order to reduce scattering losses and correspondingly boost the power conversion efficiency, it is preferred that the etched surface of the bottom dielectric stack be removed from the position of the active region **130** where the
20 intensity of the standing electromagnetic field (e-field) is highest. As a result, the bottom dielectric stack **120** is deposited in two parts, a first portion **121** and a second portion **125**, whereby the reflectance modulation is obtained by forming an etched region **151** in the surface of the first portion of the bottom dielectric stack
121. In order to distance the etched region **151** from the active region **130**, it is
25 preferred that the first portion of the bottom dielectric stack **121** contain at most 3 to 5 dielectric layers which reflect the laser light. For cases where additional dielectric layers are added to the bottom stack for reflecting the pump-beam light **180** back into the active region **130**, these layers are to be deposited first in the first portion of the bottom dielectric stack **121**.

30 The patterned etched region **151** is formed in the first portion of the bottom dielectric stack **121** by using standard photolithographic and etching techniques, thus forming a two-dimensional array of circular pillars on the surface

of the first portion of the bottom dielectric stack **121**. In the preferred embodiment the shape of the laser pixels is circular; however, other pixel shapes are possible, such as rectangular. The interpixel spacing is in the range of 0.25 to 4 μm . Via experimentation it has been determined that either one or two periods of the first portion of the bottom dielectric stack **121** should be removed to produce the etched region **151**. Etching deeper than this typically resulted in laser arrays with poorer performance. The second portion of the bottom dielectric stack **125** is deposited over the first portion of the bottom dielectric stack **121** after having formed the etched region **151**. As shown schematically in FIG. 7, the second portion of the bottom dielectric stack **125** fills the etched region **151**. The second portion of the bottom dielectric stack **125** is composed of alternating layers of high and low refractive index dielectric materials, such as TiO_2 and SiO_2 , respectively. As for the first portion, the second portion can be deposited by e-beam, PECVD, sputtering, sol-gel methods or colloidal deposition.

FIG. 8 shows another embodiment of the present invention, laser array device **108**. This device is a variation of the one illustrated in FIG. 7. In FIG. 7 the second portion of the bottom dielectric stack **125** is grown directly on the etched region **151**. As a result, the stack is deposited on a non-planar (corrugated) surface. For certain multilayer stack combinations, such as TiO_2 - SiO_2 , deposition on a corrugated surface can lead to columnar growth of the stacks. As a result, there is enhanced scattering losses in the second portion of the bottom dielectric stack **125**. To overcome this problem, the etched surface of the first portion of the bottom dielectric stack **121** is planarized by a planarization layer **158** prior to depositing the second portion of the bottom dielectric stack **125**. One embodiment of the planarization layer **158** is polyimide for the Ta_2O_5 - SiO_2 or TiO_2 - SiO_2 multilayer stack systems. Following the production of the etched regions **151**, 2 to 3 microns of polyimide are deposited on the surface of the first portion of the bottom dielectric stack **121** by spin casting and then hardened by a bake at temperatures ranging from 180 to 250°C. Next, using CMP techniques, which are well known in the art, the polyimide is polished until it is flush (or within a couple tens of nanometers) with the top surface of the first portion of the bottom dielectric stack **121** at the positions of the laser pixels **200**. Because of the

large difference in the polish rates of polyimide and oxides in standard CMP slurries, it is straightforward to have the polishing stop just as it begins to polish the oxide layers at the positions of the laser pixels **200**.

A second embodiment of the planarization layer **158** is SiO₂ for the
5 Ta₂O₅-SiO₂ multilayer dielectric stack system. In this case, the top layer of the first portion of the bottom dielectric stack **121** is a thin layer of Si₃N₄. The silicon nitride can be deposited by plasma-enhanced chemical vapor deposition (CVD) at a temperature range of 300-400°C and in a thickness range of 10 to 200 nm. Following the formation of the etched region **151** (where the etch goes through the
10 nitride layer and 1 to 2 periods of the first portion of the bottom dielectric stack **121**), the planarization layer **158** of SiO₂ is deposited at a thickness of 0.75 to 2.0 μm by either CVD or thermal evaporation. As for the polyimide embodiment, CMP is used with another common slurry to polish the SiO₂ until it is flush (or within a couple tens of nanometers) with the top of the silicon nitride layer. As a
15 result of a polish selectivity of greater than 3.5:1, it is again straightforward to stop the polishing as it begins to polish the top of the silicon nitride layer. A third embodiment of the planarization layer **158** is PMMA for any multilayer dielectric stack system. In this case, PMMA is spun cast over the etched surface of the first portion of the bottom dielectric stack **121** to a thickness range of .5 to 3.0 μm,
20 followed by a conventional bake at 150 to 220°C. Besides these three embodiments for planarization, other methodologies are possible as practiced by those skilled in the art. In summary, the addition of the planarization layer **158** following the production of the etched regions **151** and prior to the deposition of the second portion of the bottom dielectric stack **125**, leads to less scattering loss
25 in the active region **130** and in the bottom and top dielectric stacks and results in higher power conversion efficiencies.

With the invention of a display containing the VCSEL array device **100**, a simplified liquid crystal display can be made. The more simplified LCD, as shown in FIG. 9, typically contains a backlight unit **220**, the VCSEL array
30 device **100**, a polarizer layer **305**, a light shutter layer **310**, and a beam expander **320**. The backlight unit **220** provides the pump-beam light **180** for the VCSEL array device **100**. The VCSEL array device **100** provides a colored, pixelated

light source for the light shutter layer 310. If the VCSEL array device 100 includes the birefringent layer 126, then its output is also polarized and the polarizer layer 305 can be limited. Otherwise the polarizer layer 305 passes one polarization of the laser light 190 to the light shutter layer 310. The light shutter layer 310 either passes or blocks polarized light in a pixelated structure. The beam expander 320 takes the light exiting the light shutter layer 310 and expands its viewing cone.

The backlight unit 220, as shown in FIGS. 10-13 for producing the pump-beam light 180, is comprised of a diffuser 240 and either light emitting diodes (LEDs) 230 or a cold cathode fluorescent lamp (CCFL) 280. The diffuser 240 homogenizes the light incident on the VCSEL array device 100. The LEDs 230 are typically either in a linear array 250 illuminating the edge of a waveguide 260, which then redirects the light such that it is illuminating the VCSEL array device 100, or in a planar array 270 directly illuminating the VCSEL array device 100. The CCFL 280 is typically either illuminating the edge of the waveguide 260, which redirects the light such that it is illuminating the VCSEL array device 100, or oriented in rows 300 underneath the diffuser and directly illuminating the VCSEL array device 100.

The small divergence angle of the VCSEL array device 100 enables a 1:1 correspondence between the laser array's emitting elements 205 and the light shutter layer's 310 color elements. Correspondingly, it is no longer necessary to include a color filter array as one of the components of the light shutter layer 310. The light shutter layer 310 only needs to modulate the colored light incident from the VCSEL array device 100; thus, limiting the efficiency loss associated with color filter arrays. An additional feature of the near collimation of the light output from the VCSEL array device 100 is that the viewing angle compensation films can be removed from the display structure. Also due to the natural collimation (3-5° divergence angle) of the VCSEL array device 100 light output, is that the collimating films, which are typically included in the backlight unit 220, can be removed. As a result of the limitation of the viewing angle compensation films and the collimating films from the display structure, the cost of the liquid crystal display device can be reduced. However, to prevent light

leakage from neighboring pixels, the very small divergence of the VCSEL array device **100** light output must be accounted for. To prevent light of the incorrect color from escaping through a neighboring pixel, the size of the laser array's emitting elements **205** must be slightly reduced in order that the laser light upon
5 traversing into the light shutter layer **310** will subtend the proper pixel dimension of approximately $80 \times 240 \mu\text{m}$. The size of the emitting elements can be adjusted by selectively depositing metal between the bottom dielectric stack **120** and the substrate **110**. Preferred metals are Al or Ag which can be selectively deposited by well known evaporation techniques. These metals are highly reflective of the
10 pump-beam light **180** and will cause the recycling of the pump-beam light **180** until it passes between the metal depositions.

With the introduction of the birefringent layer **126** (or some other common means for affecting a preferred polarization of the VCSEL array light output) as a component in the VCSEL array device **100**, the multimode laser light
15 output from the two-dimensional vertical cavity laser array will be polarized preferentially along one direction. As a result, the bottom polarizer element and its associated reflective polarizer element are not needed in the backlight unit **220**. Removal of these elements from the display structure results in a cost savings. In another embodiment of the current invention, no effort can be made to
20 preferentially polarize the VCSEL output. In that case it will be necessary to add the polarizer layer **305** in between the top of the VCSEL array device **100** and the bottom of the light shutter layer **310**. As a result of the divergence of the VCSEL light output as discussed above, it is preferred that the added polarizer layer **305** be as thin as practical. For example, recent polarizers have thicknesses on the
25 order of $10 \mu\text{m}$.

The light shutter layer **310**, as shown in FIG. 14, is typically a liquid crystal cell **330** with an analyzer **340** on the side farthest from the VCSEL array device **100**. The liquid crystal cell **330** is analogous to conventional liquid crystal cells except that it does not contain a CFA. The liquid crystal cell **330**
30 does not require a CFA since the light output from the VCSEL array device **100** is pixelated into red, green, and blue laser light emission. The liquid crystal cell **330** comprises liquid crystal substrates **350** on the top and bottom. The liquid crystal

substrates **350** in the liquid crystal cell **330** can include either glass plates or plastic substrates. The thickness of the liquid crystal substrates **350** should be sufficiently thin to prevent parallax, which would result in light leakage through adjacent pixels. The thickness of the liquid crystal substrates **350** should preferably be less than 0.5 mm. Both of the liquid crystal substrates **350** are coated with a patterned transparent conductor layer **360**. Typical transparent conductors are indium tin oxide. On top of each of the transparent conductor layers **360** is coated an alignment layer **370**. Lastly, between the two alignment layers **370** is coated the liquid crystal material **380**. The liquid crystal cell **330** modulates the light intensity output from the VCSEL array device **100** by orienting the liquid crystal molecules upon selective application of voltages. The liquid crystal cell **330** can also contain thin film transistors at each pixel location, permitting the display to be driven actively. However, the invention does not require a specific drive scheme. The light shutter layer **310** also contains the analyzer **340** which resolves the polarized light output from the liquid crystal cell **330**.

Those skilled in the art will appreciate that other light shutters can be used with the present invention. An example is a light shutter produced by electrowetting. In this light switch, as demonstrated by Hayes, et al., Nature, **425**, 383 (2003), the application of an electric field changes the degree to which dye-containing oil droplets cover the surface of each pixel. In effect, the electric field modifies the hydrophobicity of the pixel surface. Hayes, et al., Nature, **425**, 383 (2003) envisioned their switch used for a reflective display, where the reflection is produced by a white reflector in back of the oil droplets. The electrowetting switch could also be used in transmission if the backplane is clear instead of reflective.

Since the light output of the VCSEL array device **100** is nearly collimated, it is necessary to include a beam expander **320** as the final element of the LCD device of FIG. 9 in order to increase the angular cone of the colored light output. Possible components comprising the beam expander **320** can be a diffuser element or a microlens array. The component should be such that it increases the viewing cone while preserving the sharpness of the display image. More

specifically, upon exiting the beam expander 320, each pixel should be as clearly distinguishable as prior to entering the beam expander 320. Depending on the intended application, the expansion of the viewing cone by the beam expander 320 can be adjusted accordingly.

- 5 The invention has been described in detail with particular reference to certain preferred embodiments thereof, but it will be understood that variations and modifications can be effected within the spirit and scope of the invention.

PARTS LIST

1	optic axis
3	x-y-z coordinate system
5	display surface
7	display normal direction
9	optic axis
100	VCSEL array device
102	laser array device
103	laser array device
104	laser array device
106	laser array device
108	laser array device
110	substrate
120	bottom dielectric stack
121	first portion of the bottom dielectric stack
125	second portion of the bottom dielectric stack
126	birefringent layer
128	alignment layer
129	birefringent material
130	active region
140	top dielectric stack
150	lower net gain regions
151	etched region
155	absorbing elements
157	dye layer
158	planarization layer
160	periodic gain region
170	spacer layers
180	pump-beam light
190	laser light

PARTS LIST (con't)

200	laser pixel
205	emitting element
210	interpixel region
220	backlight unit
230	light emitting diodes
240	diffuser
250	linear array
260	waveguide
270	planar array
280	cold cathode fluorescent lamp
300	rows
305	polarizer layer
310	light shutter layer
320	beam expander
330	liquid crystal cell
340	analyzer
350	liquid crystal substrates
360	transparent conductor
370	alignment layer for liquid crystal molecules
380	liquid crystal material
φ	azimuthal angle
θ	tilt angle

CLAIMS:

1. A display apparatus for producing colored pixelated light, comprising:
- 5 a) a backlight unit for producing pump-beam light;
- b) a vertical cavity laser array device including:
- i) a structure for modulating the properties of the device at spaced locations so as to provide an array of spaced laser pixels which have higher net gain than the interpixel regions; and
- 10 ii) an active region which includes portions for producing different colored light in response to the pump-beam light;
- c) a light shutter; and
- d) a beam expander disposed over the light shutter for increasing the angular cone of view of the selected colored light.
- 15
2. The display apparatus of claim 1 wherein a polarizing layer is provided between the vertical cavity laser array device and the light shutter.
3. The display apparatus of claim 1 wherein the vertical cavity laser array device further includes a birefringent layer disposed in the laser array device to ensure that the device produces polarized light having a predetermined polarization direction.
- 20
4. A display apparatus for producing colored pixelated light, comprising:
- 25 a) a backlight unit for producing pump-beam light;
- b) a vertical cavity laser array device having:
- i) a transparent substrate;
- ii) a bottom dielectric stack reflective to light over a predetermined range of wavelengths and being disposed over the substrate;
- 30

iii) means for modulating the properties of the device at spaced locations so as to provide an array of spaced laser pixels which have higher net gain than the interpixel regions;

iv) an active region which includes portions for
5 producing different colored light in response to the pump-beam light; and

v) a top dielectric stack spaced from the bottom dielectric stack and reflective to light over a predetermined range of wavelengths;

c) a light shutter for permitting selected colored light from the vertical cavity laser array device to pass therethrough; and

10 d) a beam expander disposed over the light shutter for increasing the angular cone of view of the selected colored light.

5. The display apparatus of claim 4 wherein a polarizing layer is provided between the vertical cavity laser array device and the light shutter.

15

6. The display apparatus of claim 4 wherein the vertical cavity laser array device further includes a birefringent layer disposed in the laser array device to ensure that the device produces polarized light having a predetermined polarization direction.

20

7. The display apparatus of claim 4 wherein the light shutter includes at least one layer having liquid crystals which are responsive to an applied field for permitting selected light to pass through.

25

8. The display apparatus of claim 4 wherein the light shutter includes at least one layer of polarizing film.

9. The display apparatus of claim 4 wherein the light shutter includes at least one layer having electrowetting switches.

30

10. The display apparatus of claim 4 wherein the backlight unit includes light emitting diodes or cold cathode fluorescent lamps.

11. The display apparatus of claim 4 wherein the active region includes one or more periodic gain region(s) and spacer layers disposed on either side of the periodic gain region(s) and arranged so that the periodic gain region(s) is aligned with the antinodes of the device's standing wave electromagnetic field.

5

12. The display apparatus of claim 11 wherein portions of the periodic gain region(s) produce red, green, or blue light.

13. The display apparatus of claim 11 wherein the periodic gain region(s) includes an organic host material and a dopant, and the spacer layers are substantially transparent to pump-beam light and laser light.

10

14. The display apparatus of claim 11 wherein the spacer layers include 1,1-Bis-(4-bis(4-methyl-phenyl)-amino-phenyl)-cyclohexane or silicon dioxide.

15

15. The display apparatus of claim 12 wherein the portions of the periodic gain region(s) producing green light include the host material of aluminum tris(8-hydroxyquinoline) and the dopant of [10-(2-benzothiazolyl)-2,3,6,7-tetrahydro-1,1,7,7-tetramethyl-1H,5H,11H-[1]Benzopyrano[6,7,8-ij]quinolizin-11-one].

20

16. The display apparatus of claim 12 wherein the portions of the periodic gain region(s) producing red light includes the host material of aluminum tris(8-hydroxyquinoline) and the dopant of [4-(dicyanomethylene)-2-tert-butyl-6-(1,1,7,7-tetramethyljulolidyl-9-enyl)-4H-pyran].

25

17. The display apparatus of claim 12 wherein the portions of the periodic gain region(s) producing blue light includes the host material of 2-tert-butyl-9,10-di-naphthalen-2-yl-anthracene and the dopant of 2,5,8,11-tetrakis(1,1-dimethylethyl)-perylene.

30

18. The display apparatus of claim 11 wherein the periodic gain region(s) includes polymeric materials.

5 19. The display apparatus of claim 11 wherein the periodic gain region(s) includes inorganic nanoparticles.

20. The display apparatus of claim 4 wherein the spaced laser pixels have the same or different sizes and the spacings between pixels have the same or different lengths to cause the output of the vertical cavity laser array
10 device to produce single or multimode laser output.

21. The display apparatus of claim 4 wherein the spacing between pixels is in the range of 0.25 to 4 microns.

15 22. The display apparatus of claim 4 wherein the size of the pixels is in the range of 2.5 to 20 microns.

23. The display apparatus of claim 4 wherein the pixels are arranged in a periodic two-dimensional array.
20

24. The display apparatus of claim 4 wherein the pixels are arranged randomly in a two-dimensional array.

25. The display apparatus of claim 4 wherein the array of spaced laser pixels includes a plurality of spaced apart absorbing elements selected to absorb the pump-beam light.
25

26. The display apparatus of claim 4 wherein the array of spaced laser pixels includes altering the emissive properties of the active region at
30 spaced apart locations.

27. The display apparatus of claim 26 wherein the emissive properties are altered by high intensity UV radiation.

5 28. The display apparatus of claim 4 wherein the array of spaced laser pixels includes selectively forming an etched region in the top surface of the bottom dielectric stack.

10 29. The display apparatus of claim 28 wherein a planarization layer is formed over the selectively etched bottom dielectric stack.

30. The display apparatus of claim 29 wherein the planarization layer includes polyimide or SiO₂ and is thinned by a chemical mechanical polishing system.

15 31. The display apparatus of claim 29 wherein the planarization layer includes polymethyl-methacrylate.

20 32. The display apparatus of claim 6 wherein the birefringent layer is disposed between the active region and either the bottom or top dielectric layers.

33. The display apparatus of claim 6 wherein the birefringent layer is disposed within one of the dielectric stacks.

25 34. The display apparatus of claim 6 wherein the birefringent layer includes an alignment layer disposed on at least one of the two sides of the birefringent layer.

30 35. The display apparatus of claim 34 wherein the alignment layer includes a material which permits orientation by a photo-alignment method.

36. The display apparatus of claim 34 wherein the alignment layer includes a material which permits orientation by mechanical rubbing.

37. The display apparatus of claim 6 wherein the birefringent layer includes a positive or negative birefringent material, whose optic axis has an average tilt angle between 0° and 20° .

38. The display apparatus of claim 37 wherein the birefringent material includes polymeric liquid crystals.

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39. The display apparatus of claim 4 wherein the pump-beam light is transmitted and introduced into the active region through at least one of the dielectric stacks.

15

40. A display apparatus for producing colored pixelated light, comprising:

- a) a backlight unit for producing pump-beam light;
- b) a vertical cavity laser array device including:
 - i) an etched region formed selectively in the top surface of the first portion of the bottom dielectric stack to provide an array of spaced laser pixels which have higher net gain than the interpixel regions; and
 - ii) an active region which includes portions for producing different colored light in response to the pump-beam light;
- c) a light shutter; and
- d) a beam expander disposed over the light shutter for increasing the angular cone of view of the selected colored light.

25

41. The display apparatus of claim 40 wherein a polarizing layer is provided between the vertical cavity laser array device and the light shutter.

30

42. The display apparatus of claim 40 wherein the vertical cavity laser array device further includes a birefringent layer disposed in the laser array device to ensure that the device produces polarized light having a predetermined polarization direction.

5

43. A display apparatus for producing colored pixelated light, comprising:

- a) a backlight unit for producing pump-beam light;
- b) a vertical cavity laser array device having:
 - 10 i) a transparent substrate;
 - ii) a first portion of the bottom dielectric stack reflective to light over a predetermined range of wavelengths and being disposed over the substrate;
 - iii) an etched region formed selectively in the top
 - 15 surface of the first portion of the bottom dielectric stack to provide an array of spaced laser pixels which have higher net gain than the interpixel regions;
 - iv) a second portion of the bottom dielectric stack formed over the etched first portion;
 - v) an active region which includes portions for
 - 20 producing different colored light in response to the pump-beam light; and
 - vi) a top dielectric stack spaced from the bottom dielectric stack and reflective to light over a predetermined range of wavelengths;
- c) a light shutter for permitting selected colored light from the vertical cavity laser array device to pass therethrough; and
- 25 d) a beam expander disposed over the light shutter for increasing the angular cone of view of the selected colored light.

44. The display apparatus of claim 43 wherein a polarizing layer is provided between the vertical cavity laser array device and the light

30 shutter.

45. The display apparatus of claim 43 wherein the vertical cavity laser array device further includes a birefringent layer disposed in the laser array device to ensure that the device produces polarized light having a predetermined polarization direction.

5

46. The display apparatus of claim 43 wherein the light shutter includes at least one layer having liquid crystals which are responsive to an applied field for permitting selected light to pass through.

10

47. The display apparatus of claim 43 wherein the light shutter includes at least one layer of polarizing film.

48. The display apparatus of claim 43 wherein the light shutter includes at least one layer having electrowetting switches.

15

49. The display apparatus of claim 43 wherein the backlight unit includes light emitting diodes or cold cathode fluorescent lamps.

50. The display apparatus of claim 43 wherein the active region includes one or more periodic gain region(s) and spacer layers disposed on either side of the periodic gain region(s) and arranged so that the periodic gain region(s) is aligned with the antinodes of the device's standing wave electromagnetic field

51. The display apparatus of claim 50 wherein portions of the periodic gain region(s) produce red, green, or blue light.

52. The display apparatus of claim 50 wherein the periodic gain region(s) includes an organic host material and a dopant and the spacer layers are substantially transparent to pump-beam light and laser light.

53. The display apparatus of claim 50 wherein the spacer layers includes 1,1-Bis-(4-bis(4-methyl-phenyl)-amino-phenyl)-cyclohexane or silicon dioxide.

5 54. The display apparatus of claim 51 wherein the portions of the periodic gain region(s) producing green light include the host material of aluminum tris(8-hydroxyquinoline) and the dopant of [10-(2-benzothiazolyl)-2,3,6,7-tetrahydro-1,1,7,7-tetramethyl-1H,5H,11H-[1]Benzopyrano[6,7,8-ij]quinolizin-11-one].

10

55. The display apparatus of claim 51 wherein the portions of the periodic gain region(s) producing red light includes the host material of aluminum tris(8-hydroxyquinoline) and the dopant of [4-(dicyanomethylene)-2-tert-butyl-6-(1,1,7,7-tetramethyljulolidyl-9-enyl)-4H-pyran].

15

56. The display apparatus of claim 51 wherein the portions of the periodic gain region(s) producing blue light includes the host material of 2-tert-butyl-9,10-di-naphthalen-2-yl-anthracene and the dopant of 2,5,8,11-tetrakis(1,1-dimethylethyl)-perylene.

20

57. The display apparatus of claim 50 wherein the periodic gain region(s) includes polymeric materials.

25

58. The display apparatus of claim 50 wherein the periodic gain region(s) includes inorganic nanoparticles.

59. The display apparatus of claim 43 wherein the spaced laser pixels have the same or different sizes and the spacings between pixels have the same or different lengths to cause the output of the vertical cavity laser array device to produce single or multimode laser output.

30

60. The display apparatus of claim 43 wherein the spacing between pixels is in the range of 0.25 to 4 microns.

5 61. The display apparatus of claim 43 wherein the size of the pixels is in the range of 2.5 to 20 microns.

62. The display apparatus of claim 43 wherein the pixels are arranged in a periodic two-dimensional array.

10 63. The display apparatus of claim 43 wherein the pixels are arranged randomly in a two-dimensional array.

64. The display apparatus of claim 43 wherein a planarization layer is formed between the first and second portions of the bottom dielectric stack.
15

65. The display apparatus of claim 64 wherein the planarization layer includes polyimide or SiO₂ and is thinned by a chemical mechanical polishing system.
20

66. The display apparatus of claim 64 wherein the planarization layer includes polymethyl-methacrylate.

67. The display apparatus of claim 45 wherein the birefringent layer is disposed between the active region and either the bottom or top dielectric layers.
25

68. The display apparatus of claim 45 wherein the birefringent layer is disposed within one of the dielectric stacks.

30 69. The display apparatus of claim 45 wherein the birefringent layer includes an alignment layer disposed on at least one of its two sides.

70. The display apparatus of claim 69 wherein the alignment layer includes a material suitable to permit orientation by a photo-alignment method.

5 71. The display apparatus of claim 69 wherein the alignment layer includes a material suitable to permit orientation by mechanical rubbing.

72. The display apparatus of claim 45 wherein the birefringent layer includes a positive or negative birefringent material, whose optic axis has an
10 average tilt angle between 0° and 20° .

73. The display apparatus of claim 72 wherein the birefringent material includes polymeric liquid crystals.

15 74. The display apparatus of claim 43 wherein the pump-beam light is transmitted and introduced into the active region through at least one of the dielectric stacks.

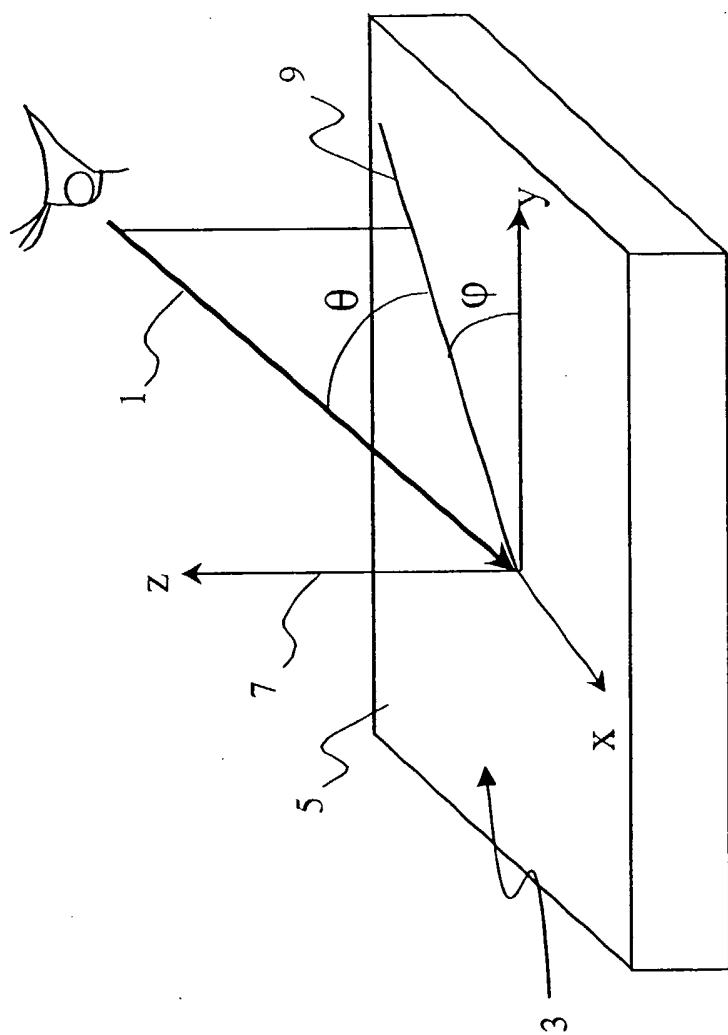


FIG.1

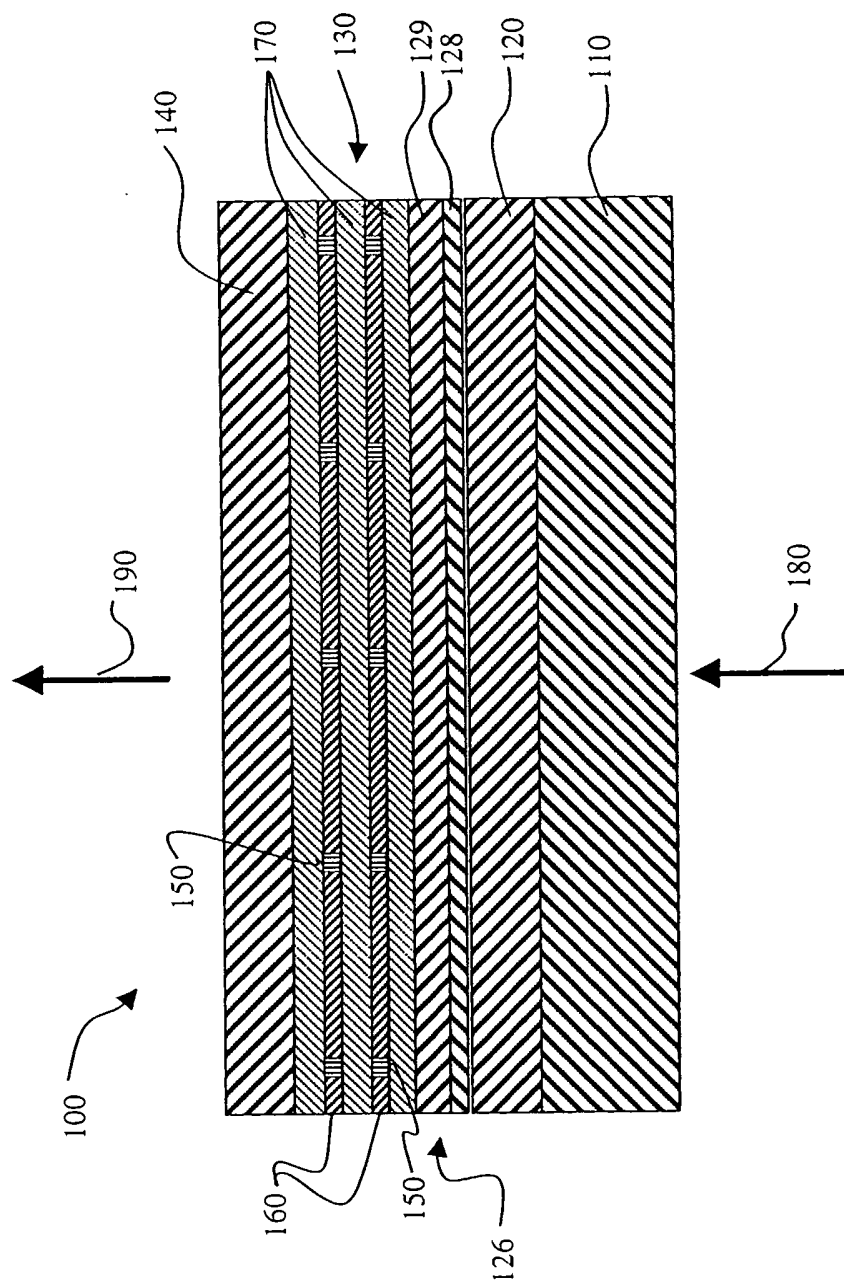


FIG. 2

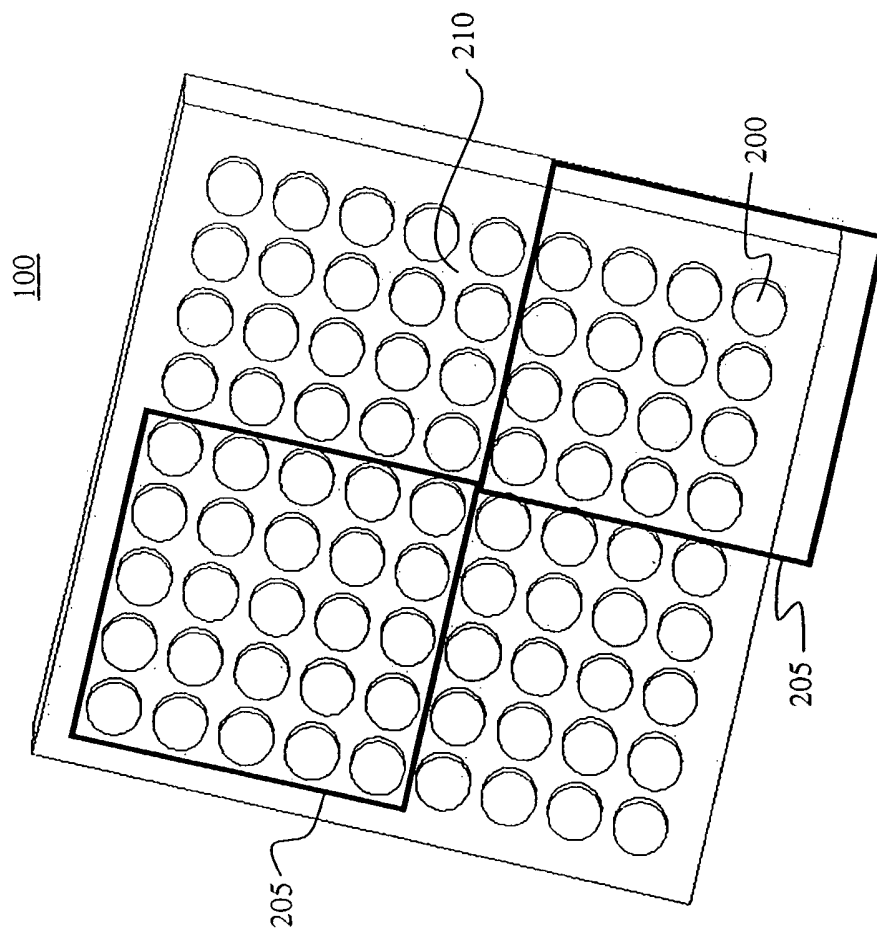


FIG. 3

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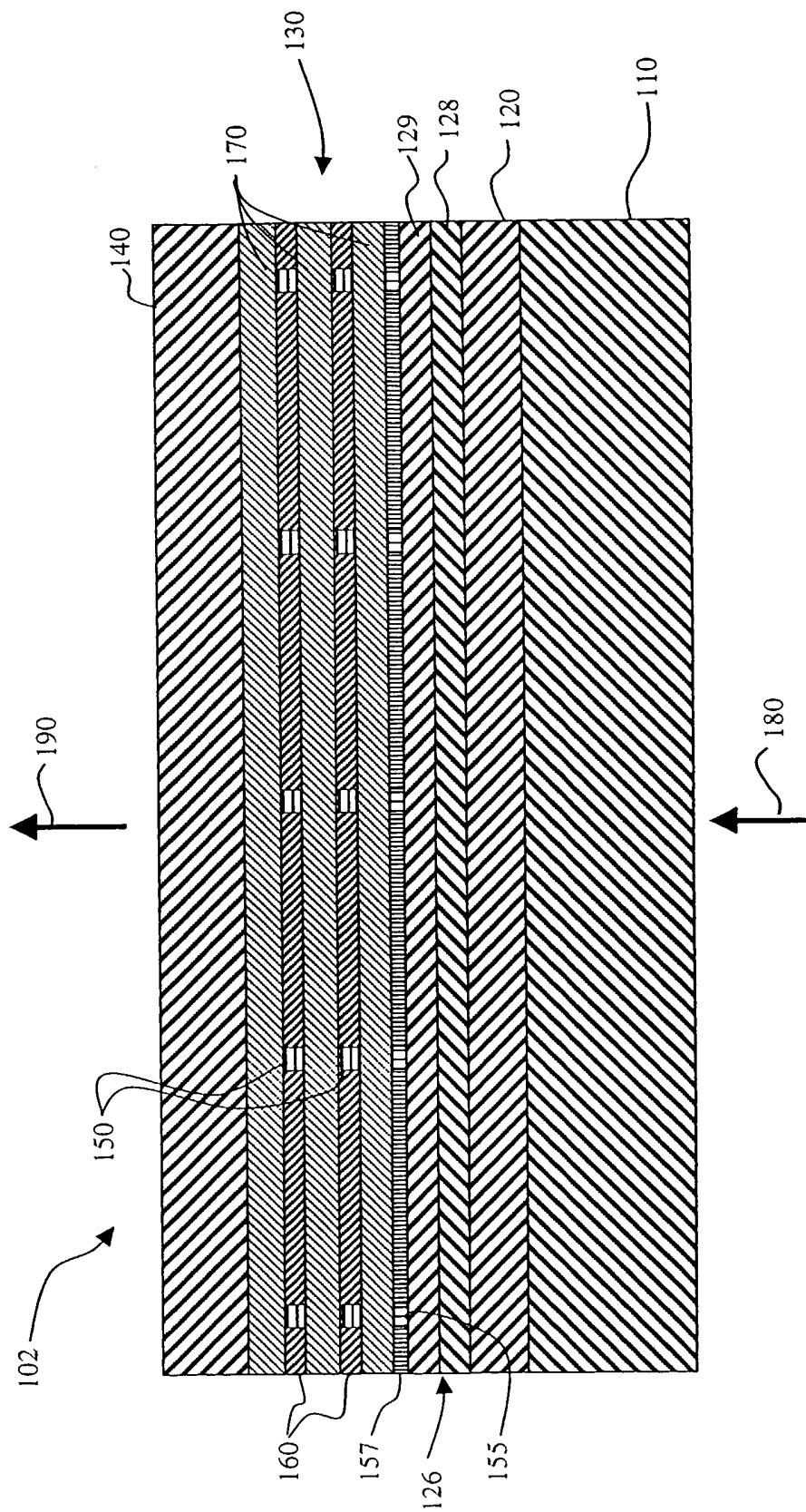


FIG. 4

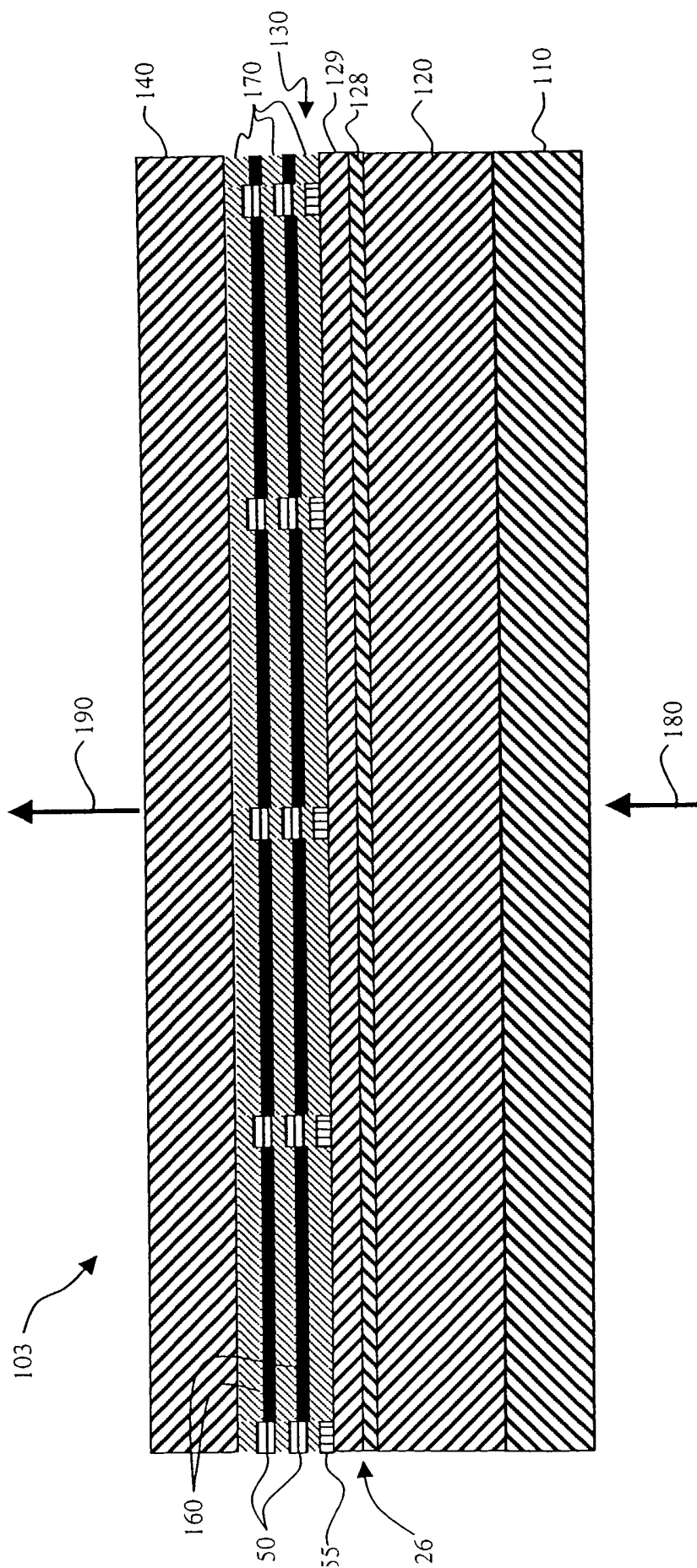


FIG. 5

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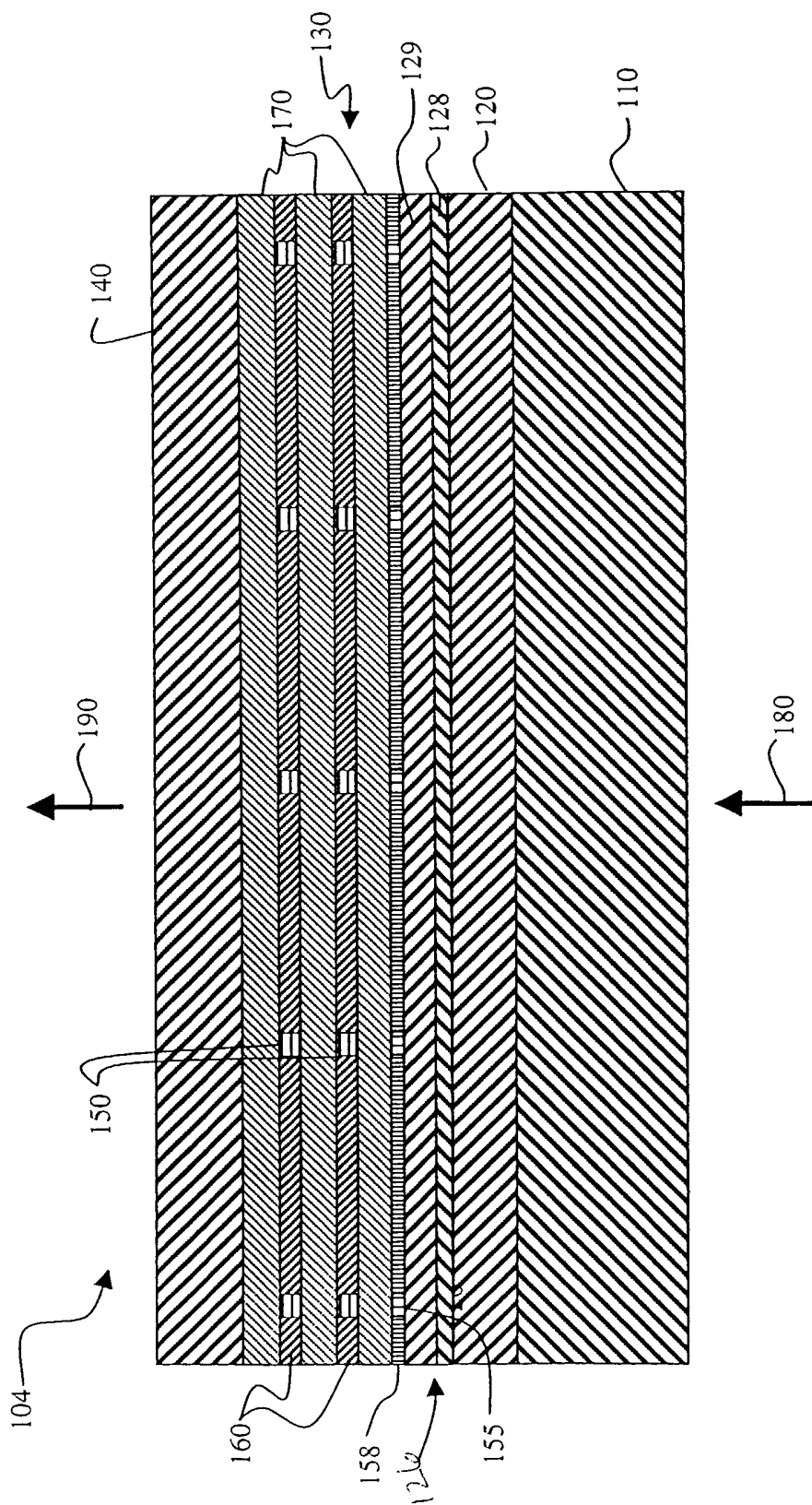


FIG. 6

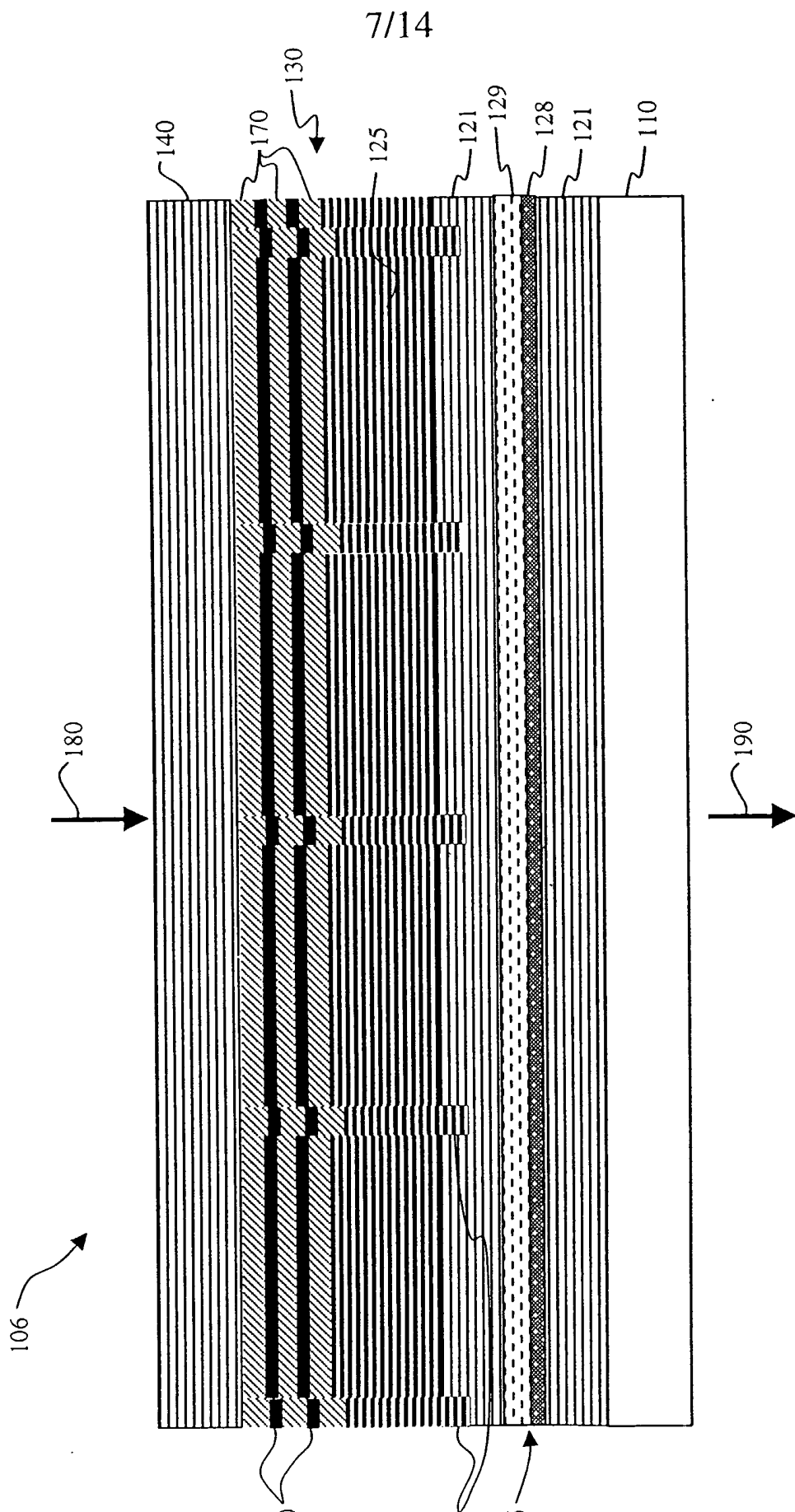


FIG. 7

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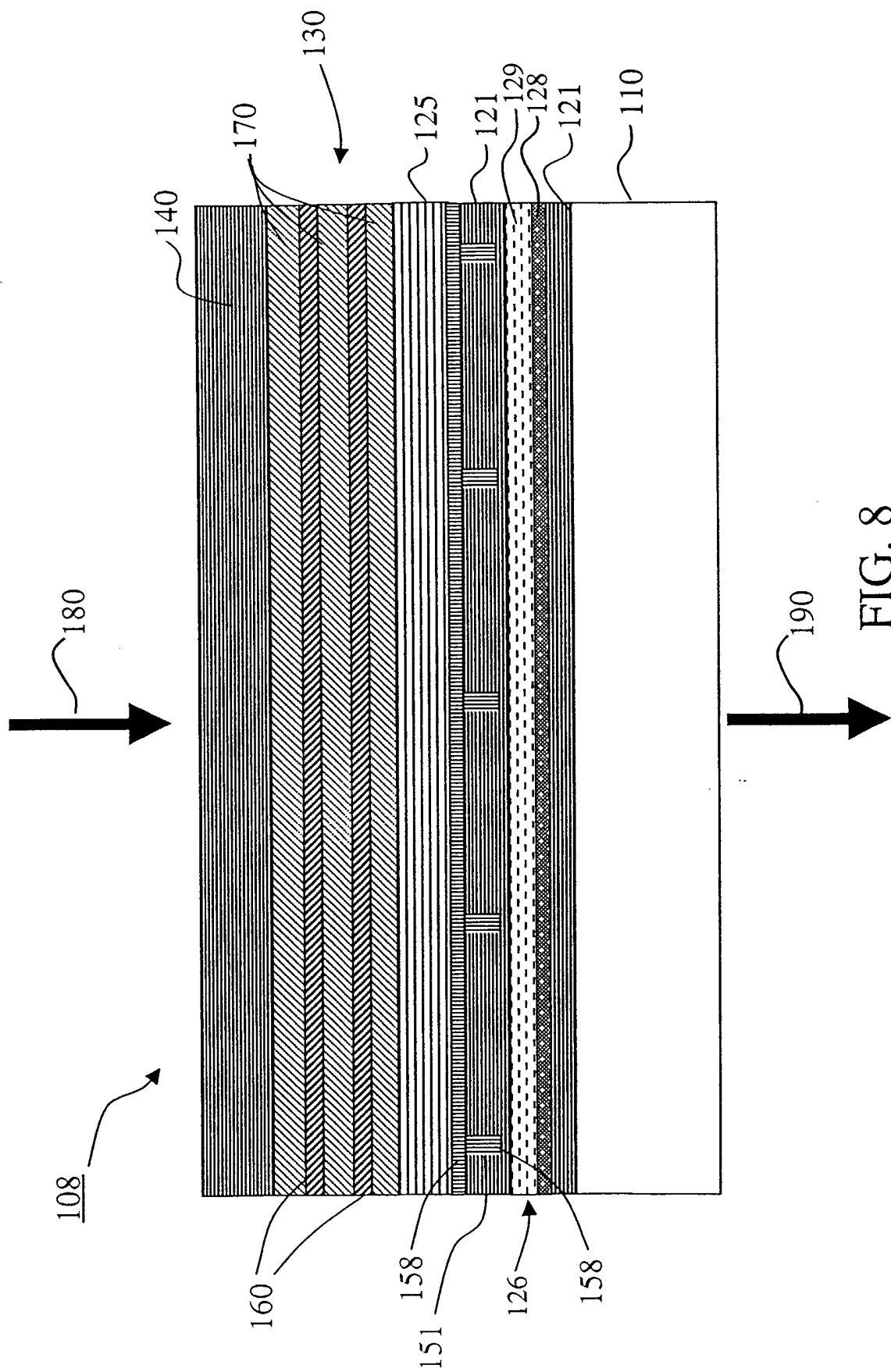


FIG. 8

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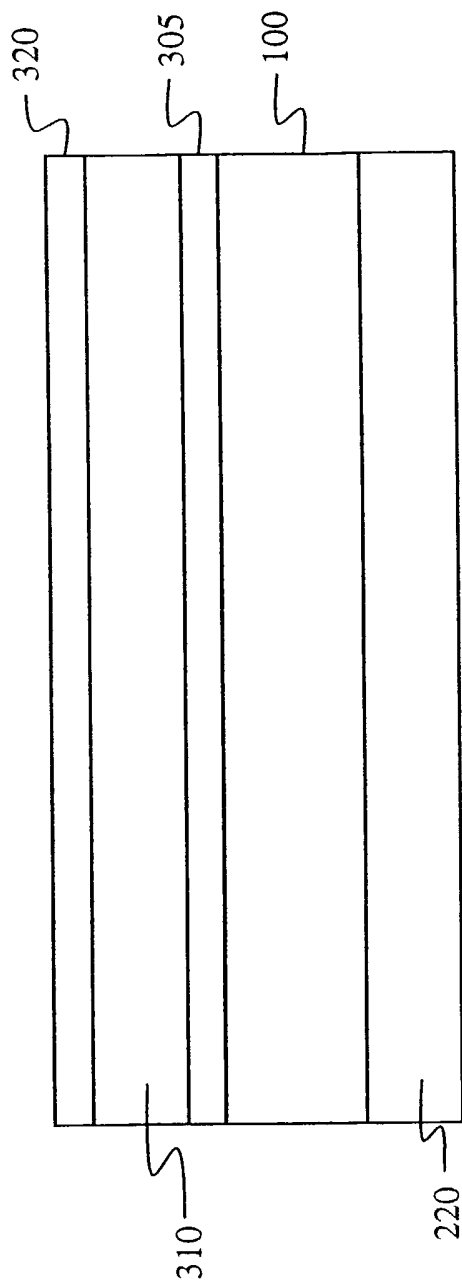


FIG. 9

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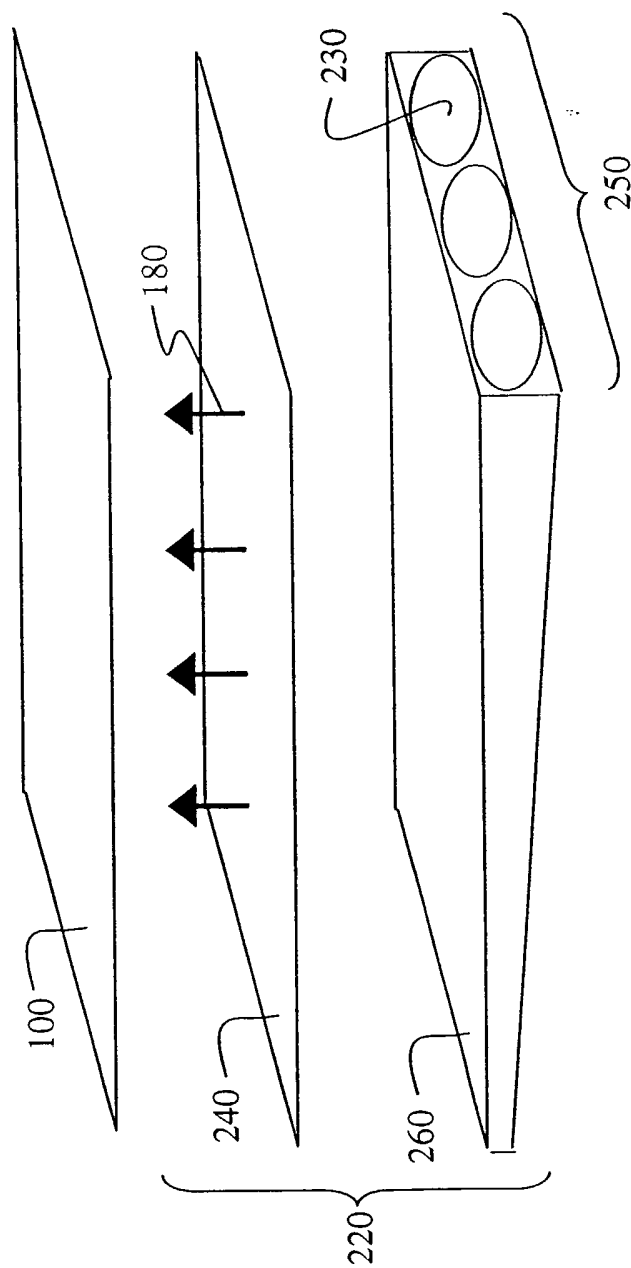


FIG. 10

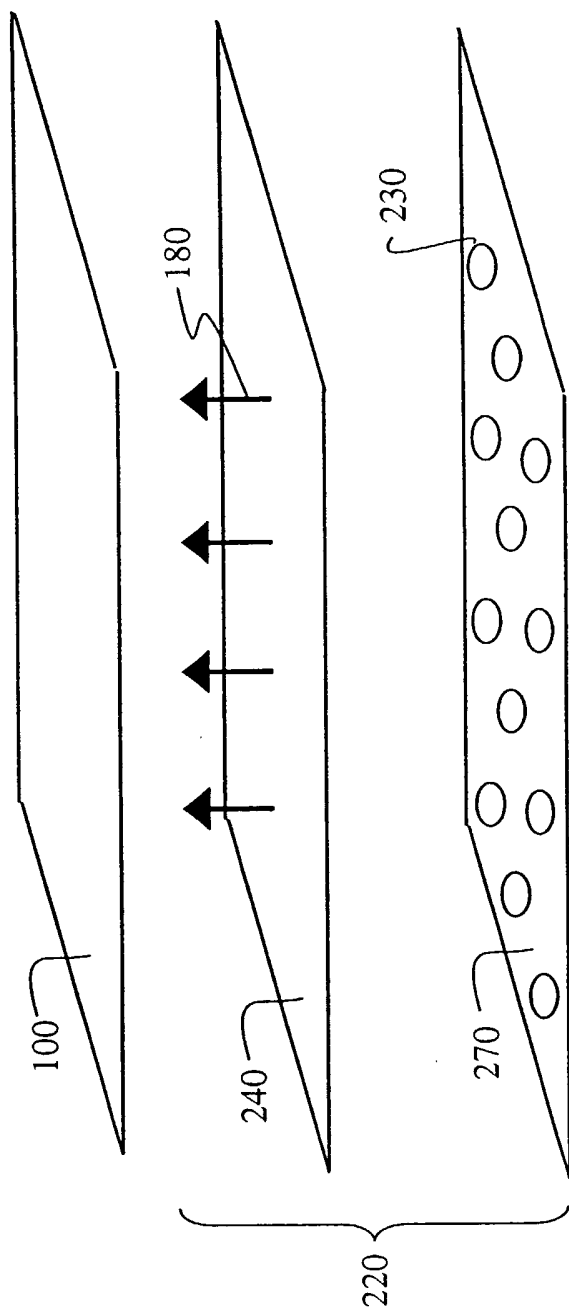


FIG. 11

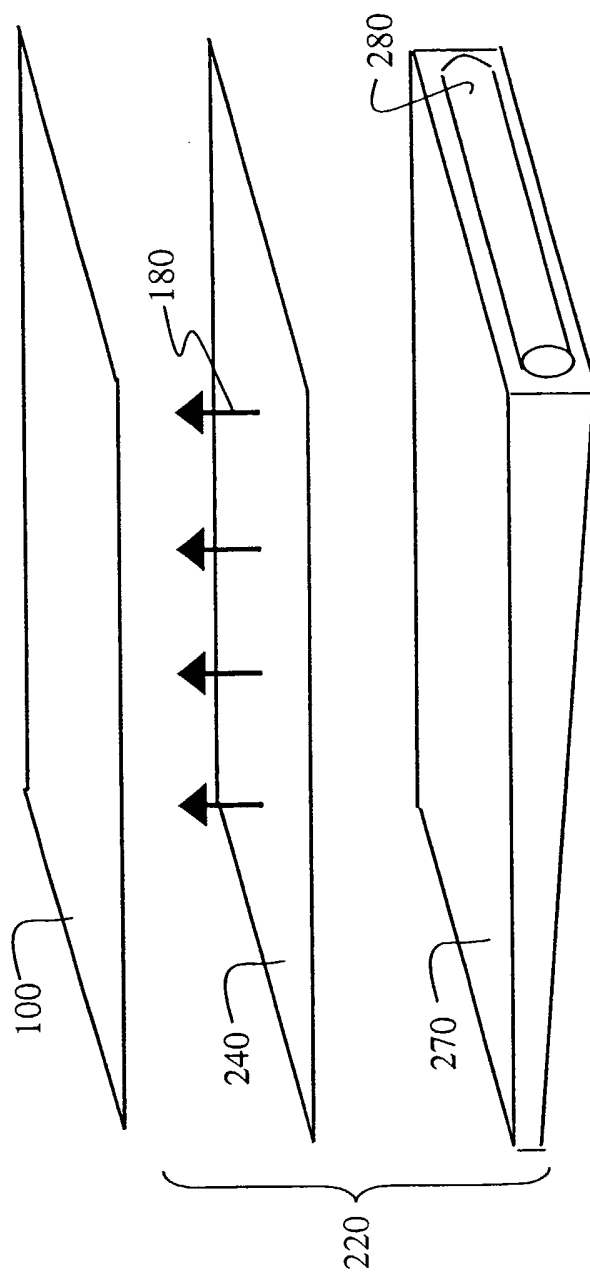


FIG. 12

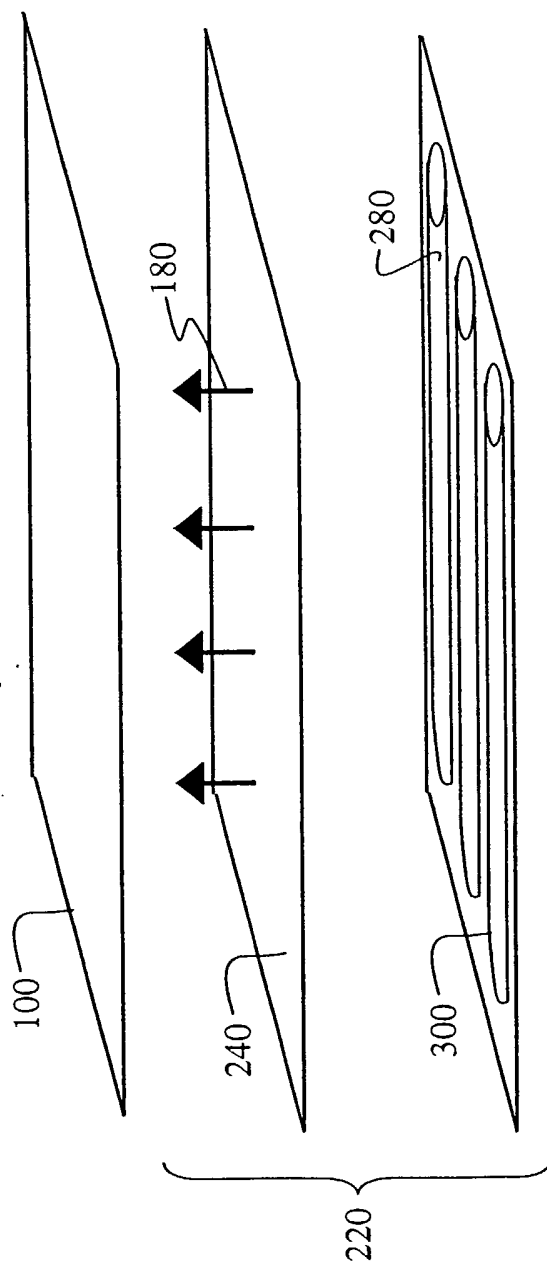


FIG. 13

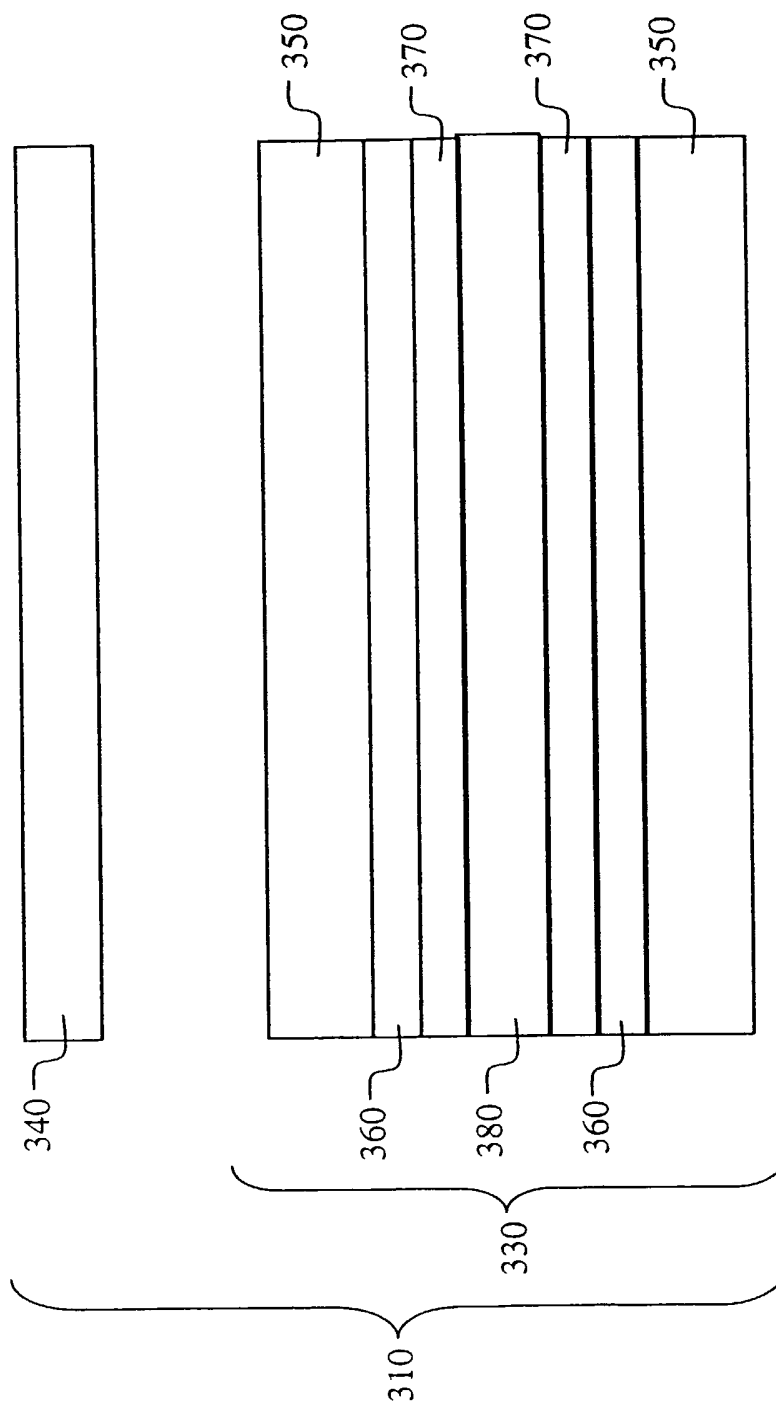


FIG. 14

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US2005/016885

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	EP 1 411 607 A (EASTMAN KODAK COMPANY) 21 April 2004 (2004-04-21)	1,2,4,5, 7,8, 10-18, 20-26, 28,39-41
A	paragraph '0007! - paragraph '0010!	43,
	paragraph '0014! - paragraph '0024!	49-55,
	paragraph '0031!; figures 1-3,5,6,8,10,13	57, 59-63,74
A	EP 0 818 769 A (SEIKO EPSON CORPORATION) 14 January 1998 (1998-01-14)	1,4,7,8, 11,12, 20-23, 26,40, 43,46, 47,50, 51,59-62
	column 5, line 25 - column 7, line 39	
	column 8, line 38 - line 41; figures 1,2	
A	US 2001/017674 A1 (YAMAGUCHI AKIRA) 30 August 2001 (2001-08-30)	1,4,40, 43
	paragraph '0005!	
	paragraph '0028!	
	paragraph '0074! - paragraph '0081!;	
	figures 1,5	
A	TOSHIKAZU MUKAIHARA ET AL: "POLARIZATION CONTROL OF VERTICAL-CAVITY SURFACE-EMITTING LASERS USING A BIREFRINGENT METAL/DIELECTRIC POLARIZER LOADED ON TOP DISTRIBUTED BRAGG REFLECTOR" IEEE JOURNAL OF SELECTED TOPICS IN QUANTUM ELECTRONICS, IEEE SERVICE CENTER, US, vol. 1, no. 2, 1 June 1995 (1995-06-01), pages 667-673, XP000521125 ISSN: 1077-260X	32,33, 67,68
	page 667, right-hand column, line 33 -	
	page 668, right-hand column, line 14;	
	figure 2	

INTERNATIONAL SEARCH REPORT

International Application No
PCT/US2005/016885

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
GB 2341973	A	29-03-2000	NONE
EP 1411607	A	21-04-2004	US 2004076201 A1 22-04-2004 EP 1411607 A2 21-04-2004 JP 2004140372 A 13-05-2004
EP 0818769	A	14-01-1998	JP 3671530 B2 13-07-2005 JP 10026944 A 27-01-1998 EP 0818769 A2 14-01-1998 KR 256708 B1 15-05-2000 US 6243148 B1 05-06-2001 US 6002458 A 14-12-1999
US 2001017674	A1	30-08-2001	JP 2001215501 A 10-08-2001