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(71) Applicant (for all designated States except US): **MAC-DONALD DETTWILER & ASSOCIATES INC.** [CA/CA]; 9445 Airport Road, Brampton, Ontario L6S 4J3 (CA).

(72) Inventor; and

(75) Inventor/Applicant (for US only): **GREGORIS, Dennis** [CA/CA]; 37-2385 Woodward Avenue, Burlington, Ontario L7R 1V2 (CA).

(74) Agent: **HILL & SCHUMACHER**; 264 Avenue Road, Toronto, Ontario M4V 2G7 (CA).

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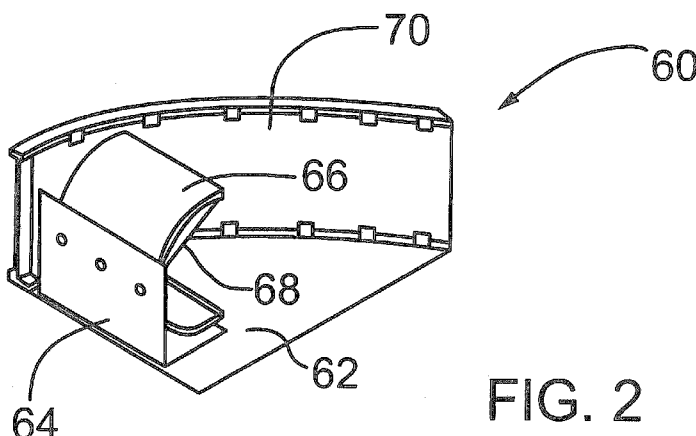


FIG. 2

(57) Abstract: The present invention provides an illuminator system comprising a dual reflector system and a linear light source. The dual reflector system comprises a primary and secondary generally cylindrical reflector, which collimate light from a linear light source in two planes. The linear light source may comprise many light emitting devices, and may emit light in a strobe or continuous fashion. The reflectors may be of many cylindrical shapes, and may include additional mirror segments to capture light otherwise not collimated. Further, the reflectors may be in various configurations of position and orientation with respect to one another, and may be adjustable in this respect. The system is more efficient than existing illuminators, is compact, all reflective (no colour), lightweight, simple and inexpensive to manufacture. The system has applications to many fields including machine vision, surveillance, spectroscopic inspection of materials, and converting linear light sources into rectangular beam spot lights.

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## **DUAL REFLECTOR SYSTEM FOR LINEAR LAMP ILLUMINATORS**

### **FIELD OF THE INVENTION**

This invention generally relates to illuminator systems, and more specifically a linear lamp illuminator system with a dual reflector system.

### **BACKGROUND OF THE INVENTION**

Flashlamps are often used as illumination sources for machine vision or surveillance cameras. However, the flashlamp emits light in all directions, so a collimating optical system must be used to concentrate the light onto the target of interest. Cylindrical parabolic or paraboloid reflectors are often used to collimate the light from linear flashlamps, sometimes in conjunction with a fresnel refractive lens. Unfortunately these standard methods have a number of drawbacks.

Cylindrical reflectors can only collimate the light in one plane and have a very wide beam in a plane orthogonal thereto, so most of the light generated by the lamp is wasted. Adding a cylindrical fresnel lens helps, but the lens must have a long focal length and large aperture which makes it heavy and expensive. Refractive elements can also separate the colours of the light due to dispersion, which is often undesirable in applications involving optical sensors.

Paraboloid reflectors may capture most of the light, but in order to function well the illumination source must fit entirely within the paraboloid. For long flashlamps, this imposes a large diameter for the reflector, making the reflector large and expensive. Examples of this configuration are

disclosed in U.S. Patent Nos. 5,037,191 and 5,235,470, which generally describe paraboloid reflectors for use with a linear light source. Further, some configurations of paraboloid reflectors such as the ones found in U.S. Patent Nos. 4,210,954 and 3,254,342 may produce a doughnut beam pattern which is often undesirable for imaging applications.

U.S. Patent No. 3,938,162 describes an antenna system for single or plural beams providing continuously variable beamwidth selectively in one or both of two orthogonal senses. The system includes two parabolic cylindrical reflectors, which are positioned with the focal axes thereof orthogonally. A point of multibeam feed is mounted adjacent the main reflector on the focal axis of the sub-reflector in the Airy disc of the system. Simultaneous operation of telescoping sections of the two reflectors provides bidirectional zooming of the beam.

U.S. Patent No. 4,208,661 describes an antenna system with two parabolic cylindrical reflectors with a point feed source located on the focal axis of one of the reflectors, wherein the directrix of the cylindrical wave front obtained by exposure of the first reflector coincides with the focal line of the second reflector, and the focal line of the first reflector is not parallel to the symmetry plane of the second reflector.

Therefore, it would be very advantageous to provide an improved reflector system for linear lamp illuminators.

## SUMMARY OF THE INVENTION

In general, embodiments of the present invention comprise an illuminator system comprising:

a dual reflector system comprising

a primary generally cylindrical reflector having a primary focal axis and oriented to collimate light in a first plane, and

a secondary generally cylindrical reflector having a secondary focal axis and oriented to collimate light in a second plane; and

a linear light source having an emission length disposed on the primary focal axis; wherein

said primary generally cylindrical reflector and said secondary generally cylindrical reflector are oriented relative to each other such that at least a portion of the light emitted by the linear light source is reflected and becomes collimated in both said first plane and said second plane.

In some embodiments of the invention, the primary and secondary generally cylindrical reflectors may be parabolic. In addition, in some embodiments, the secondary focal axis may lie at a distance from the primary vertex, and in some cases may be at a distance equal to the primary focal length from the primary vertex.

The generally cylindrical reflectors of the present invention may have vertices which are curved or linear.

In some embodiments of the invention, the secondary focal length will be greater than or equal to half of the emission length of the linear light source.

Many light sources are applicable for use in the present invention. Some exemplary useful light sources are flash lamps, continuous wave cylindrical linear light sources, tungsten halogen lamps, sodium lamps, metal halide lamps, and fluorescent lamps. In addition, the light sources may operate as a strobe light.

Some embodiments of the invention will include additional mirror segments located parallel to the primary generally cylindrical reflector and oriented with respect to said primary generally cylindrical reflector to reflect stray light back through said primary focal axis. Further, these mirror segments may be positioned such that light passing through said primary focal axis and reflecting from said primary generally cylindrical reflector does not reflect from said at least one mirror segment.

The dual reflector system of the present invention may include reflectors which are milled reflective material, and may include reflectors which are flexible reflective sheets mounted to inserts. Further, the reflectors may be mounted to a single base, and may be in the form of a parabola.

In some embodiments of the invention, the first and second planes in which the emitted light is collimated are mutually orthogonal.

Further, the position and orientation of the primary and secondary generally cylindrical reflectors with respect to one another may be adjustable. In some of these embodiments, the primary generally cylindrical reflector is able to translate and rotate relative to said secondary generally cylindrical reflector in a plane perpendicular to said secondary focal axis.

The primary focal axis, in some embodiments, may lie between a plane defined by two straight edges on the primary generally cylindrical reflector and the reflector itself.

Finally, some embodiments of the invention will include a primary generally cylindrical reflector comprising a parabolic portion and a portion which wraps around the light source. The portion which wraps around the linear light source may be circular in shape, and the linear light source may be disposed at the centre of the circle.

A further understanding of the functional and advantageous aspects of the invention can be realized by reference to the following detailed description and drawings.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

Embodiments of the invention will be more fully understood from the following detailed description thereof taken in connection with the accompanying drawings, which form a part of this application, and in which:

**Figure 1a** is a top view of a dual reflector system absent support structures for linear lamp illuminators constructed in accordance with the present invention;

**Figure 1b** is a side view of the dual reflector system of **Figure 1a**;

**Figure 2** is a perspective view of the focusing optics of the dual reflector system of **Figures 1a** and **1b**;

**Figure 3** is a top view of the focusing optics of the dual reflector of **Figure 1a** and **1b**;

**Figure 4** is a side view of the focusing optics of the dual reflector of **Figures 1a, 1b**;

**Figure 5** is a section along the line **5-5** of **Figure 3**.

**Figure 6** is a side view showing the primary reflector and reflector mount and mounting bracket of **Figure 7**;

**Figure 7** is a perspective view showing the primary reflector and reflector mount and mounting bracket;

**Figure 8** is a view taken along arrow **8** of **Figure 6**;

**Figure 8a** is a side view of an alternative embodiment of a primary reflector of the dual reflector system including a portion of the reflector that wraps around the linear illumination source to capture more emitted light.

**Figure 8b** is a front view of the alternative embodiment of **Figure 8a**.

**Figure 8c** is a side view of an alternative embodiment of a primary reflector of the dual reflector system including a mirror segment located parallel to the primary parabolic reflector to reflect stray light back through the mirror focus to improve the uniformity of the emitted beam;

**Figure 8d** is a side view of an alternative embodiment of a primary reflector of the dual reflector system including mirror segments located parallel to the primary parabolic reflector to reflect stray light back through the mirror focus to improve the light collection efficiency and the uniformity of the emitted beam. In the shown embodiment, the mirror segments are positioned such that they do not reflect any light which originally passed through the focal axis of and was reflected from the primary reflector;

**Figure 9** shows a cross-section geometry of the primary parabolic mirror and the cross-section of the linear light source, forming part of the

dual reflector system of the present invention, the figure only shows one-half of the parabolic mirror for simplicity;

**Figure 10** is a drawing showing the geometry of the secondary mirror and linear light source location forming part of the dual reflector system of the present invention;

**Figure 11** is a drawing showing the geometry of the linear light source of **Figure 9** and its reflected virtual source;

**Figure 12** shows a plot of normalized average Intensity as a function of secondary mirror focal plane position;

**Figure 13** is a perspective view showing the primary focal axis may be disposed between the primary generally cylindrical reflector and a plane defined by two straight edges on the primary generally cylindrical reflector; and

**Figure 14** is a side view of an embodiment of the invention in which the primary generally cylindrical reflector comprises a flexible sheet of reflective material affixed to a support bracket.

### **DETAILED DESCRIPTION OF THE INVENTION**

Generally speaking, the systems described herein are directed to a dual reflector system for linear lamp illuminators. As required, embodiments of the present invention are disclosed herein. However, the disclosed embodiments are merely exemplary, and it should be understood that the invention may be embodied in many various and alternative forms. The Figures are not to scale and some features may be exaggerated or minimized to show details of particular elements while related elements may

have been eliminated to prevent obscuring novel aspects. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting but merely as a basis for the claims and as a representative basis for teaching one skilled in the art to variously employ the present invention. For purposes of teaching and not limitation, the illustrated embodiments are directed to dual reflector system for linear lamp illuminators.

**Figures 1a** and **1b** show respectively a top and side view sketch of the dual reflector system **60**, absent supporting structures, to illustrate the basic concept. The dual reflector system includes a primary generally cylindrical mirror or reflector **68** with a linear illumination source, e.g. a cylindrical flash lamp **74** aligned along the length of the focal axis (at **74** in **Figure 1b**) of mirror **68**. A secondary generally cylindrical mirror or reflector **70** is oriented relative to the primary mirror **68** such that light emitted from the linear light source is reflected from the primary and secondary mirrors **68, 70** and is thereby collimated in two planes, forming a collimated beam. In some embodiments of the invention in which the reflectors **68, 70** are generally cylindrical parabolic, the primary and secondary reflectors **68, 70** have primary and secondary focal axes and primary and secondary vertices **122, 120**, respectively. Further, the distance between each focal axis and its respective vertex is called the focal length. In some embodiments, the secondary focal axis of the secondary mirror **70** ( $F_2$ ) preferably falls on or behind the vertex **122** of the primary mirror **68**. In the embodiment of the invention shown in **Figures 1a** and **1b**, the focal axis of the secondary mirror

**70** falls on the vertex **122** of the primary mirror **68**. Linear light source **74** has an overall length **L1** and an emission length **L2**.

**Figure 2** shows a perspective view of one embodiment of the invention including supporting structure and the assembled dual reflector system **60** focusing optics for producing the optical beam. In this embodiment, the primary parabolic mirror/reflector **68** is mounted to a cylindrical mounting bracket **66** which in turn is mounted to a mounting bracket **64**. Mounting bracket **64** is mounted on a base **62**. The mounting bracket **66** may include inserts between the bracket and the mirror **68** that form the mirror **68** in the shape of a parabola. The secondary parabolic reflector/mirror **70** is mounted to a mirror mount **72** which in turn is mounted to base **62**.

**Figure 14** shows a side view of one embodiment of the invention in which the primary generally cylindrical reflector **68** comprises a flexible sheet of reflective material. This sheet may be mounted to a base or other structure with inserts with the desired form. In the shown embodiment, the reflector **68** is formed in the shape of a parabola by the inserts **142** mounted to a mounting bracket **64**. In another embodiment of the invention, the primary generally cylindrical reflector **68** is milled from reflective material and does not require supporting structure to maintain its shape. One skilled in the art would appreciate that the secondary generally cylindrical reflector **70** may also be built in the described fashions.

**Figure 3** is a top view of the focusing optics of the dual reflector of **Figures 1a, 1b**. **Figure 4** is a side view of the focusing optics of the dual reflector of **Figures 1a, 1b**. **Figure 5** is a section along the line **5-5** of **Figure**

3. **Figure 7** is a perspective view showing the primary reflector **68**, reflector mount **66** and mounting bracket **64**. **Figure 6** is a side view showing the primary reflector **68**, reflector mount **66**, and mounting bracket **64** of **Figure 7**. **Figure 8** is a view taken along arrow **8** of **Figure 6**.

The two generally cylindrical reflectors **68** and **70** are used to collimate the light from the linear light source **74** into a narrow beam that, for instance, may match the field-of-view of a camera. The primary reflector **68** collimates the light in a first plane and the secondary reflector **70** collimates the light in a second plane. In preferable embodiments of the invention, the second plane is orthogonal to the first plane. In another preferable embodiment of the invention, the primary and secondary reflectors **68**, **70** are oriented such that as much as possible of the light which is not reflected by the first and second reflectors **68**, **70** is preferably already collimated in the desired direction upon emission from the linear lamp **74**.

Referring again to **Figures 1a** and **1b**, the focal length  $F_2$  of the secondary mirror **70** is preferably equal to, or greater than, half the linear light source emission length  $L_2$ . Typically the focal length  $F_2$  of secondary mirror **70** is made large enough so the secondary mirror **70** location accommodates the physical length  $L_1$  of the linear light source **74** i.e. it is equal to or greater than half the physical length  $L_1$  of the linear light source **74**.

The focal lengths ( $F_1$ ) of the primary mirror **68** and the secondary mirror **70** ( $F_2$ ) respectively are selected to achieve the desired illumination beam widths in the vertical and horizontal directions respectively given the diameter of the arc and the length of the arc.

While a preferable shape of the generally cylindrical primary reflector **68** is parabolic as shown in **Figure 1a**, other shapes may provide some advantageous features. As an example, the embodiment of a primary reflector **110** shown in **Figures 8a** and **8b** is a primary reflector of the dual reflector system **60** wherein a portion **112** of the reflector is parabolic to collimate light, and another cylindrical portion **114** wraps around the linear illumination source **74** to capture more emitted light. The cylindrical mirror **110** also has the effect of altering the intensity of the output beam light distribution in the vertical plane such that the intensity increases nearer the source throughout the aperture **A2**. The shape of the vertical intensity profile of the output beam is adjusted by the cylindrical mirror angular extent  $\alpha$  of cylindrical portion **114**, which determines the proportion of directly emitted to reflected light. Preferably, the cylindrical portion **114** that wraps around the linear illumination source **74** is circular in shape, and the linear illumination source **74** lies at the centre of the circle.

The advantages of this feature are: increased light collection efficiency, approximately 50% reduction in the illuminator volume and the ability to improve illumination uniformity when illuminating surfaces tilted at high angles to the illuminator.

The embodiment in **Figures 8c** and **8d** show two other configurations which capture stray light not initially directed to the primary reflector **68**; these include one or more mirror segments **80** located parallel to the primary reflector **68** which reflect stray light back through the mirror focal axis. As shown in **Figure 8d**, the mirror segments **80** may be located such that they

are not in the path of light which has passed through the primary focal axis and reflected from the primary reflector **68**.

In principle neither the primary mirror **68** nor the secondary mirror **70** has to be strictly cylindrical. Particularly, the primary and secondary mirror vertices may be curved to increase the amount of light collected in the orthogonal plane. Adding curvature may be used to decrease the size of the mirrors e.g. the primary mirror could be curved so that the secondary mirror can be shorter and likewise by adding a curvature to the secondary mirror. Similarly, the primary mirror **68** does not need to be a pure parabolic cylinder if there is a cylindrical mirror replacing one half of the mirror. Thus, when referred to as being "generally cylindrical", as used herein this phrase covers pure cylindrical in addition to these other configurations.

It will readily be appreciated by one skilled in the art that the linear light source **74** may comprise many different sources of light. For example, the linear light source **74** may comprise a flash lamp, a continuous wave cylindrical linear light source, a tungsten halogen lamp, a sodium lamp, a metal halide lamp, and a fluorescent lamp. Further, the linear light source **74** may be a strobe light or provide continuous illumination.

In some embodiments of the invention, it is preferable that as much of the emitted light as possible is collimated by the primary and secondary generally cylindrical reflectors **68, 70**. Therefore, the primary focal axis may be disposed between the primary generally cylindrical reflector **68** and a plane **136** defined by two straight edges **132, 134** on the primary generally cylindrical reflector **68**, as shown in **Figure 13**.

Further, adjustment of the beam emitted by the dual reflector system **60** is possible by providing the primary and secondary generally cylindrical reflectors **68, 70** in an adjustable configuration. To this end, the position and orientation of either one or both of the primary and secondary generally cylindrical reflectors **68, 70** may be adjustable. In some embodiments of the invention, for instance, the primary generally cylindrical reflector **68** may be able to translate and rotate on a plane perpendicular to the focal axis of the secondary generally cylindrical reflector **70**. However the position of linear light source **74** preferably remains on the focal axis of the primary mirror **68** as the primary mirror **68** position and orientation are adjusted.

### **Primary Mirror Design**

It is instructional to determine some of the basic design characteristics of a simple parabolic mirror. A simple geometric analysis can provide insight into what determines the average output beamwidth of the illuminator as a function of the parabola and linear light source characteristics. It should be noted that the analysis presented herein applies a simplified geometrical ray tracing and any design should include realistic models of the linear light source and mirror using more complex models and ray trace simulations.

**Figure 9** shows the cross-section geometry of the primary parabolic mirror **68** and the cross-section of the linear light source **74**. The **Figure 9** only shows one-half of the parabolic mirror **68** for simplicity. The linear light source **74** has an internal radius **R** and is located at the focal point  $y = F1$  of parabolic mirror **68**. The other half is to the left of  $X = 0$ . The linear light source **74** will always be at  $X = 0$ , on the axis of the parabola defined by

primary mirror **68**. In the example of **Figure 9**, the y axis location of the lamp is 0.5". In general, the y-axis location of the lamp **74** is  $y = Y$ . **Figure 9** shows, as a circle, the internal bore of the lamp, the area that generates light. The lamp has an internal bore diameter of  $2R$ . The active length of the lamp arc is 1 inch (but is not restricted to this length), not shown in **Figure 9**.

The equation for the parabola is given by

$$y = \frac{x^2}{4f} \quad (1)$$

where  $f$  is the focal length of the parabola. For this analysis it is assumed that the light produced by the arc is emitted within the internal radius  $R$ .

It is a property of parabolic mirrors that a ray of light emanating from parabola focal point  $f$  and incident to the parabolic surface at an arbitrary point  $P(x,y)$ , will reflect parallel to the optical axis of the parabola. The angle from this ray to the y axis is defined as  $\phi$ . Since it is assumed that light is radially and uniformly emitted from the linear light source, then  $\phi$  varies from zero degrees to a maximum angle  $\phi_{\max}$  determined by the half-aperture of the mirror  $W$ .

The distance from the focal point  $F_1$  to a point  $P(x,y)$  as a function of angle  $\phi$  is given by

$$D(\phi) = \sqrt{x^2(\phi) + (f - y(\phi))^2} \quad (2)$$

where

$$x(\phi) = 2f \left( \tan(\phi - 90) + \sqrt{\tan^2(\phi - 90) + 1} \right) \quad (3)$$

and

$$y(\phi) = \frac{x^2(\phi)}{4f} \quad (4)$$

Other rays emitted from the interior of the lamp diverge from the parabola surface 68 with an angular beam width  $\theta(\phi)$  determined by the bore radius  $R$  and its distance,  $D(\phi)$  from the point of reflection on the parabola surface where

$$\theta(\phi) = 2 \tan^{-1} \left( \frac{R}{D(\phi)} \right) \quad (5)$$

The maximum angle  $\phi_{\max}$  is determined when  $x$  is equal to the half aperture

$W$  so

$$y(\phi_{\max}) = \frac{W^2}{4f} \quad (6)$$

Therefore

$$\theta(\phi_{\max}) = 2 \tan^{-1} \left( \frac{R}{D(\phi_{\max})} \right) \quad (7)$$

where

$$\phi_{\max} = \frac{\pi}{2} + \tan^{-1} \left( \frac{W^2 - 4f^2}{4fW} \right) \text{ radians} \quad (8)$$

The average angular beam width,  $\theta_{\text{Average}}$ , is calculated by integrating over all the beam width angles values from  $\phi = 0$  to  $\phi_{\max}$ , then dividing by  $\phi_{\max}$ .

$$\theta_{\text{Average}} = \frac{\int_0^{\phi_{\max}} \theta(\phi) d\phi}{\phi_{\max}} \quad (9)$$

The model assumes that the total amount of collected light is fixed so that if it is spread over a wider beam, then the peak intensity must decrease.

In addition, the total amount of light collected by the mirror is proportional to the maximum subtended angle  $\phi_{max}$  and the peak light intensity is inversely proportional to angular beam width. Therefore, a relative measure of peak intensity is the maximum subtended angle  $\phi_{max}$  divided by the average angular beam width:

$$I_{peak} = \frac{\phi_{max}}{\theta_{Average}} \tag{10}$$

**Table 1** illustrates the results of the ray trace analysis for the cases of two illuminators with linear light source bore radii of 0.08 and 0.12 inches, and a total aperture width of 5 inches. The focal length is varied from 0.5 to 2 inches. The maximum angle  $\phi_{max}$  is shown as an indication of the amount of light collected by the parabolic reflector where amount collected is proportional to the value of  $\phi_{max}$ . The average angular beamwidth and the normalized peak intensity of the beam are also given. The central beam peak intensity is arbitrarily normalized to the smallest linear light source radius and focal length case for illustration.

**Table 1: Example results of a simple 2D geometrical ray trace**

		Linear light source Radius			
		0.08 inches		0.12 inches	
Focal Length (Inches)	Maximum angle $\phi_{max}$ (deg) W=2.5 inches	Average Beam Width (deg)	Normalized Peak Intensity $I_{peak}$	Average Beam Width (deg)	Normalized Peak Intensity $I_{peak}$
0.5	136.4	11.8	1	17.3	0.67
0.75	118	8.6	1.17	12.8	0.78
1	102.7	7.0	1.25	10.4	0.84
1.5	79.6	5.1	1.32	7.7	0.88
2	42.2	2.9	1.345	6.1	0.89

Several observations may be made in reference to **Table 1** that may be used as design guidance. The smaller the focal length, the greater the magnitude of collected light. As the radius of the linear light source **74** decreases relative to the focal length, the linear light source **74** becomes more point-like and consequently, the output beam becomes more collimated and more intense. Conversely, as the linear light source **R** radius becomes large compared to the focal length, the output beam widens and is less intense. Increasing the focal length decreases the total light but also decreases beam width more quickly.

### **Secondary mirror design**

**Figure 10** shows a plan view diagram of the illuminator with the primary mirror **68** and linear light source **74** located at the primary mirror **68** focal point  $F_1$ . The secondary mirror **70** is positioned such that its focal plane is parallel to the primary mirror axis and a distance **S** from the primary mirror **68** focal point  $F_1$ . The diagram is similar to **Figure 9** except that the light source is a linear source rather than an isotropic cylindrical source. The secondary mirror **70** collects direct light from along the length of the linear light source **74** and the light reflected from the primary mirror **68**, and reflects it towards the illuminated surface.

The analysis of the combined primary mirror **68** and secondary mirror **70** is complex but may be qualitatively understood by simplifying the geometries. Replacing the primary mirror **68** and linear light source **74** with a single linear source centered at the primary mirror **68** focal point **f** permits a simplified analysis similar to that done with the primary mirror **68**.

Referring to **Figure 10**, the geometry of the secondary mirror **70** and linear light source location are shown, in which the rays emitted from the ends of the linear light source **102** and incident at point  $P(y_p, z_p)$  on the parabolic mirror **70** with focal length  $f_s$ . The equation for the parabola is given by

$$z = \frac{y^2}{4f_s} \quad (11)$$

where  $f_s$  is the focal length of the parabola. As before, the distance from the focal point  $f_s$  to a point  $P(y, z)$  as a function of angle  $\phi_s$  is given by

$$D_s(\phi_s) = \sqrt{y^2(\phi_s) + (f_s - z(\phi_s))^2} \quad (12)$$

where

$$z(\phi_s) = 2f_s \left( \tan(\phi_s - 90) + \sqrt{\tan^2(\phi_s - 90) + 1} \right)$$

and

$$z(\phi_s) = \frac{y^2(\phi_s)}{4f_s}$$

Other rays emitted from the interior of the lamp diverge from the parabola surface of primary mirror **68** with an angular beam width  $\theta_s(\phi_s)$  determined by the source length  $l$  and its distance,  $D_s(\phi_s)$  from the point of reflection on the parabola surface where from the geometry,

$$\theta = \phi_s - 90 - \alpha$$

and

$$\gamma = \phi_s - 90 + \beta$$

and it can be shown that

$$\alpha(\phi_s) = \tan^{-1} \left( \frac{l_1 \cos(\phi_s - 90)}{D_s(\phi_s) - l_1 \sin(\phi_s - 90)} \right)$$

and

$$\beta(\phi_s) = \tan^{-1} \left( \frac{l_2 \cos(\phi_s - 90)}{D_s(\phi_s) + l_2 \sin(\phi_s - 90)} \right)$$

Therefore

$$\theta_s = \alpha(\phi_s) + \beta(\phi_s)$$

so the angular beamwidth is

$$\theta_s(\phi_s) = \tan^{-1} \left( \frac{l_1 \cos(\phi_s - 90)}{D_s(\phi_s) - l_1 \sin(\phi_s - 90)} \right) + \tan^{-1} \left( \frac{l_2 \cos(\phi_s - 90)}{D_s(\phi_s) + l_2 \sin(\phi_s - 90)} \right)$$

The maximum angle  $\phi_{max}$  is determined when x is equal to the half aperture

$W_s$ , so

$$z(\phi_{max}) = \frac{W_s^2}{4f_s}.$$

As before

$$\phi_{s \max} = 90 + \tan^{-1} \left( \frac{W_s^2 - 4f_s^2}{fW_s} \right)$$

and given the light distribution from a linear light source is given by the

approximate function

$$I(\phi) = \frac{2 \cos(\phi - 90)}{1 + \cos(\phi - 90)^2}$$

this can be combined with the geometrical beamwidth to provide a weighted beamwidth that is more physically representative. Therefore the weighted average angular beam width,  $\bar{\theta}_s$  is given by.

$$\bar{\theta}_s = \frac{\int_0^{\phi_{\max}} \theta_s(\varphi) \frac{2 \cos(\varphi - 90)}{1 + \cos(\varphi - 90)^2} d\varphi}{\phi_{\max}} .$$

These formulas can be used to perform a first-order design of the reflector based upon the linear light source emission length, desired average horizontal beamwidth and the reflector size constraints.

This analysis ignores the primary mirror **68** and linear light source **74** and assumes the light source is located at the secondary focal plane and the initial inclination is to have the primary mirror **68** and secondary mirror **70** focal planes coincide. However, this is a sub-optimal design from the standpoint of light collection efficiency and beam quality. Instead, in some embodiments of the invention, the secondary focal axis is located behind the vertex **122** of the primary mirror at a distance equal to the focal length of the primary mirror **68**,  $F_1$ . Doing so can increase the average intensity of the beam by more than 25%.

The reason for placing the secondary mirror **70** focus behind the primary mirror **68** can be seen by considering the reflection of the light from the linear light source **74** in the primary mirror **68**. **Figure 11** shows a drawing of the geometry of the linear light source and its reflected virtual source **74a**. Referring to **Figure 11**, light rays from the lamp **74** are incident at a point in the mirror  $P(x,y)$ . The incident rays are reflected and diverge away from the mirror **74** as disused in previous sections. The divergent rays may be considered to emanate from a virtual source **74a** which is a reflection of the original lamp perpendicular to the plane of the mirror surface tangent. The location of the virtual source **74a** varies along the parabola. The locus of the virtual sources **74a** can be determined by calculating the

intersection of the line between the source **74a** and its reflection **y** and the line  $X=Xp$ .

The line **y** is perpendicular to the parabola's tangent which has a slope  $m$  and the general equation for **y** is given by

$$y = \frac{-1}{m}x + f$$

The slope of the parabola

$$y = \frac{x^2}{4f}$$

is given by

$$m(x) = \frac{dy}{dx} = \frac{x}{2f}.$$

Substituting the slope into the equation for **y** and setting  $X=Xp$  produces  $y = -f$ . Consequently the locus of all the virtual sources lies on a line located behind the parabola vertex at a distance equal to the parabola focal length. This simplified analysis suggests that, to collect and focus as much light as possible from the real and virtual light sources **74** and **74a** respectively, the focal plane  $F_2$  of the secondary mirror **70** is preferably located at or behind the primary mirror vertex **122**, and more preferably is located at a distance equal to the primary mirror **68** focal length  $F_1$  behind the primary mirror **68** vertex.

To quantify the degree of improvement, a dual reflector system was simulated using a commercially available ray tracing analysis program. The secondary mirror **70** position was varied and the total normalized average light intensity within the beam spot was calculated. The results are shown in

**Figure 12** which shows normalized average intensity as a function of secondary mirror focal plane position.

The results shown in **Figure 12** indicate that the optimum amount of focused light occurs when the secondary mirror focal plane is located behind the primary mirror **68** vertex at a distance equal to the primary focal length  $F_1$ . The optimum location increases the average amount of focused light by over 25% compared to the primary focal point location. Increasing the distance from the vertex **122** further causes the output beam to defocus and the amount of light decreases.

The dual reflector system disclosed herein improves light collection efficiency and enables controlling of illumination beam size to best suit the application where illumination is needed. It improves the light uniformity of linear light sources such as linear arc lamps and strobed light. The system is more efficient than existing strobe flashlamp illuminators, is compact, all reflective (no colour), lightweight, simple and inexpensive to manufacture. These features result in increased illumination range, lower power requirements and better quality images from cameras that use this illuminator. The system has applications to machine vision, surveillance, spectroscopic inspection of materials, and converting linear light sources, such as tungsten halogen lamps, sodium lamps, metal halide lamps or fluorescent tubes, into rectangular beam spot lights (stage lights, projectors, vehicle headlights).

As used herein, the terms “comprises”, “comprising”, “including” and “includes” are to be construed as being inclusive and open ended, and not exclusive. Specifically, when used in this specification including claims, the

terms “comprises”, “comprising”, “including” and “includes” and variations thereof mean the specified features, steps or components are included. These terms are not to be interpreted to exclude the presence of other features, steps or components.

The foregoing description of the preferred embodiments of the invention has been presented to illustrate the principles of the invention and not to limit the invention to the particular embodiment illustrated. It is intended that the scope of the invention be defined by all of the embodiments encompassed within the following claims and their equivalents.

**THEREFORE WHAT IS CLAIMED IS:**

1. An illuminator system, comprising:
  - a dual reflector system comprising
    - a primary generally cylindrical reflector having a primary focal axis and oriented to collimate light in a first plane, and
    - a secondary generally cylindrical reflector having a secondary focal axis and oriented to collimate light in a second plane; and
    - a linear light source having an emission length disposed on the primary focal axis; wherein
    - said primary generally cylindrical reflector and said secondary generally cylindrical reflector are oriented relative to each other such that at least a portion of the light emitted by the linear light source is reflected and becomes collimated in both said first plane and said second plane.
  
2. The illuminator system according to claim 1 wherein
  - said primary generally cylindrical reflector is a primary generally cylindrical parabolic reflector having a primary vertex and a primary focal length between the primary vertex and said primary focal axis; and
  - said secondary generally cylindrical reflector is a secondary generally cylindrical parabolic reflector having a secondary vertex and a secondary focal length between the secondary vertex and said secondary focal axis.

3. The illuminator system according to claim 2 wherein the secondary focal axis is on or behind the primary vertex.
4. The illuminator system according to claim 3 wherein said secondary focal axis is at a distance equal to said primary focal length from said primary vertex.
5. The illuminator system according to claim 2 wherein said secondary focal length is greater than or equal to half of the emission length of said linear light source.
6. The illuminator system according to claim 2 wherein one of said primary vertex, said secondary vertex, and said primary and secondary vertices are curved.
7. The illuminator system according to claim 2 wherein one of said primary vertex, said secondary vertex, and said primary and secondary vertices are linear.
8. The illuminator system according to any one of claims 1 to 7 wherein said linear light source is one of a flash lamp, a continuous wave cylindrical linear light source, a tungsten halogen lamp, a sodium lamp, a metal halide lamp, and a fluorescent lamp.
9. The illuminator system according to claim 8 wherein said linear light source is a strobe light.

10. The illuminator system according to any one of claims 1 to 9 wherein said dual reflector system further includes at least one mirror segment located parallel to said primary generally cylindrical reflector and oriented with respect to said primary generally cylindrical reflector to reflect stray light back through said primary focal axis.

11. The illuminator system according to claim 10 wherein said at least one mirror segment is positioned such that light passing through said primary focal axis and reflecting from said primary generally cylindrical reflector does not reflect from said at least one mirror segment.

12. The illuminator system according to any one of claims 1 to 11 wherein one or both of said primary generally cylindrical reflector and said secondary generally cylindrical reflector comprise at least one flexible reflective sheet mounted to inserts.

13. The illuminator system according to claim 12 wherein said inserts are mounted to a single base.

14. The illuminator system according to claim 12 or 13 wherein said inserts form the flexible reflective sheet into the shape of a parabola.

15. The illuminator system according to any one of claims 1 to 11 wherein one or both of said primary generally cylindrical reflector and said secondary generally cylindrical reflector are milled from reflective material.

16. The illuminator system according to claim 15 wherein said milled reflective material is mounted to a single base.
17. The illuminator system according to claim 15 or 16 wherein a surface of said milled reflective material is in the shape of a parabola.
18. The illuminator system according to claim 1 wherein said first and second planes are mutually orthogonal.
19. The illuminator system according to any one of claims 1 to 18 wherein said primary generally cylindrical reflector and said secondary generally cylindrical reflector are positioned and oriented relative to each other in an adjustable manner.
20. The illuminator system according to claim 19 wherein said linear light source has a longitudinal axis along said emission length, and wherein said linear light source is fixed with respect to the primary mirror with its longitudinal axis aligned along the focal axis of the primary mirror.
21. The illuminator system according to claim 19 wherein said primary generally cylindrical reflector is able to translate and rotate relative to said secondary generally cylindrical reflector in a plane perpendicular to said secondary focal axis.
22. The illuminator system according to any one of claims 1 to 21 wherein said primary generally cylindrical reflector has two straight edges, and said

primary focal axis lies between said primary generally cylindrical reflector and a plane defined by the two straight edges.

23. The illuminator system according to any one of claims 1 to 22 wherein a portion of said primary generally cylindrical reflector is parabolic and a remaining portion of said primary generally cylindrical reflector wraps around the linear light source.

24. The illuminator system according to claim 23 wherein said portion of said primary generally cylindrical reflector that wraps around the linear light source is in the shape of a circle, and wherein said linear light source is disposed at a centre of said circle.

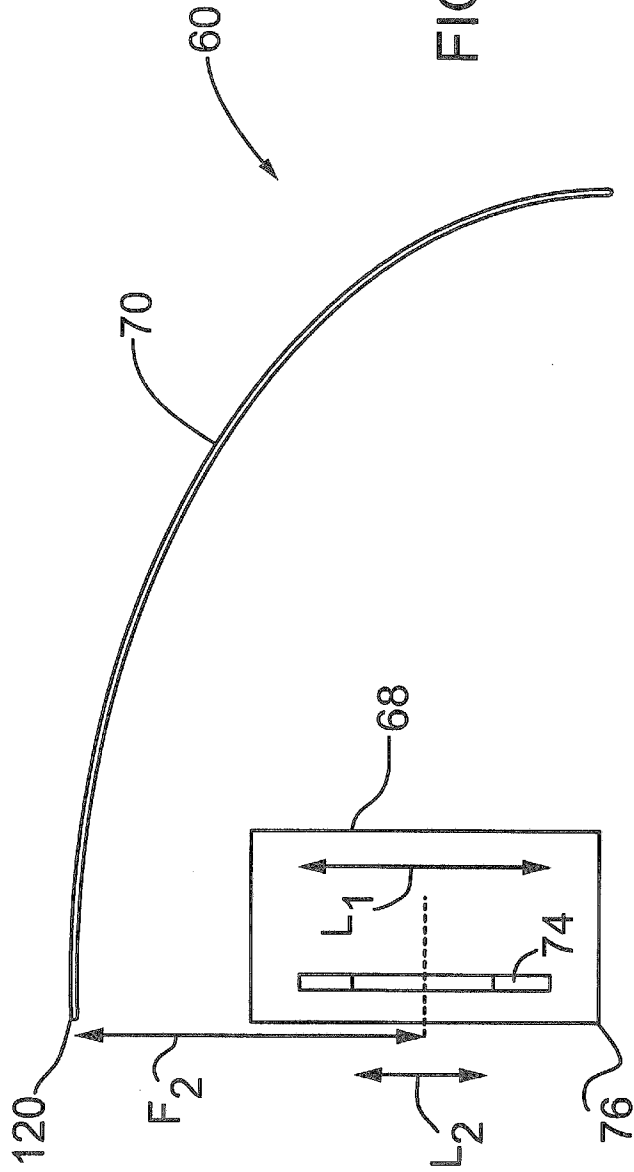


FIG. 1a

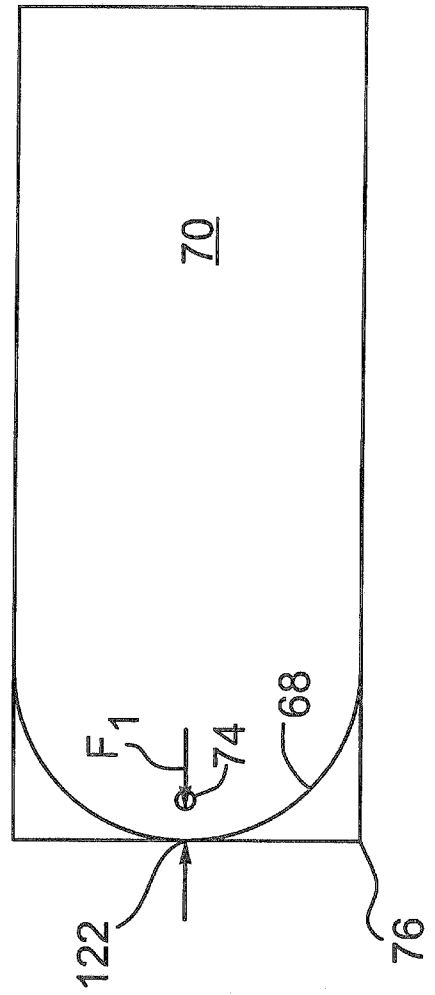


FIG. 1b

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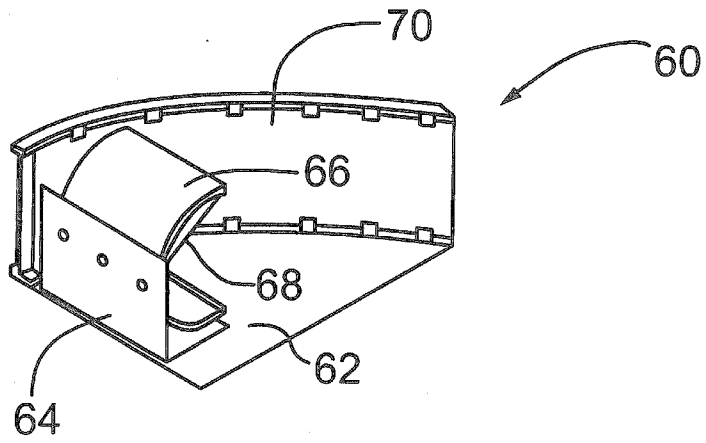


FIG. 2

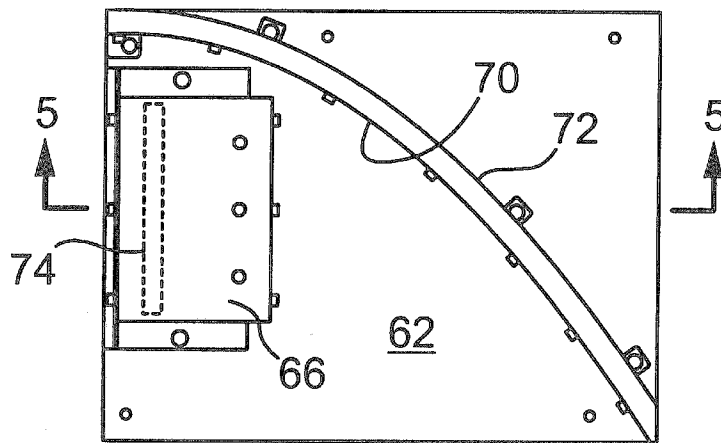


FIG. 3

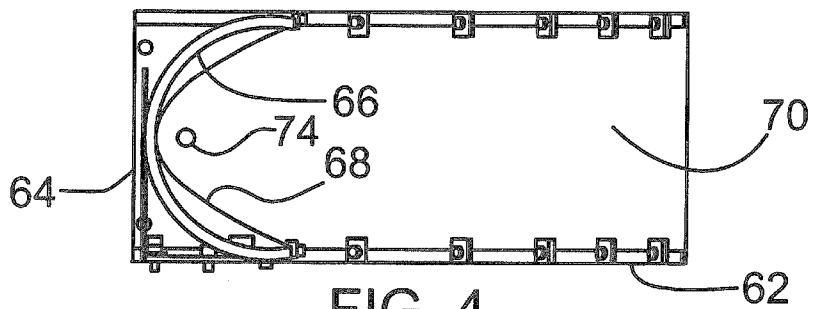


FIG. 4

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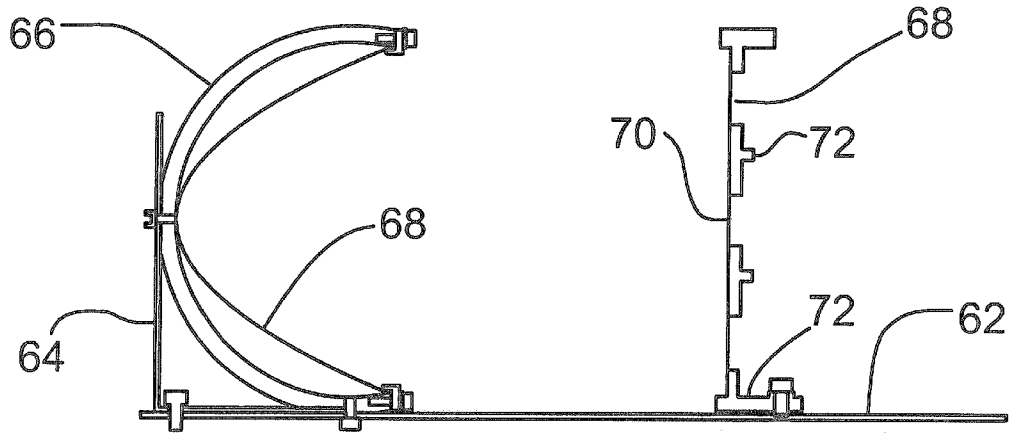


FIG. 5

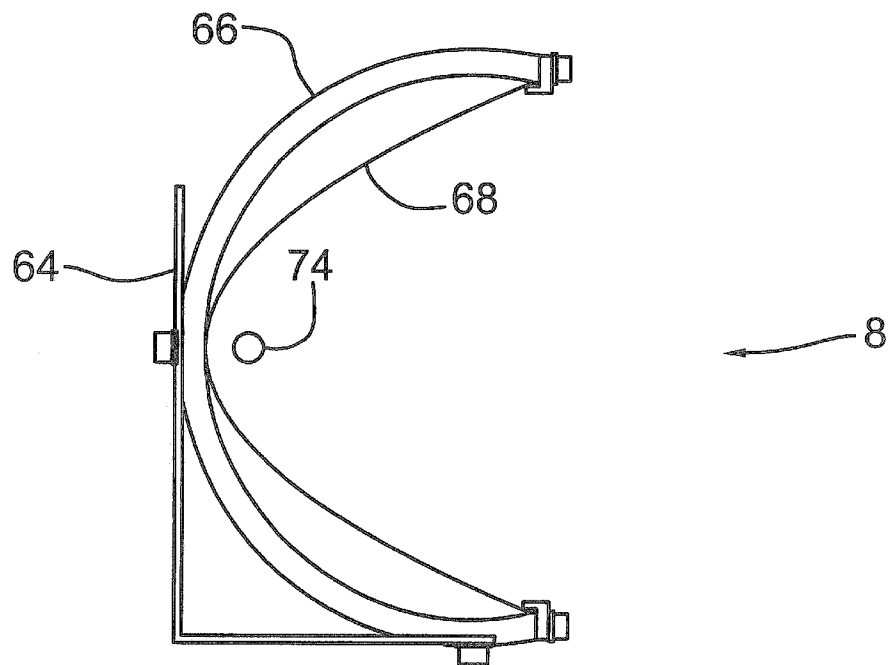
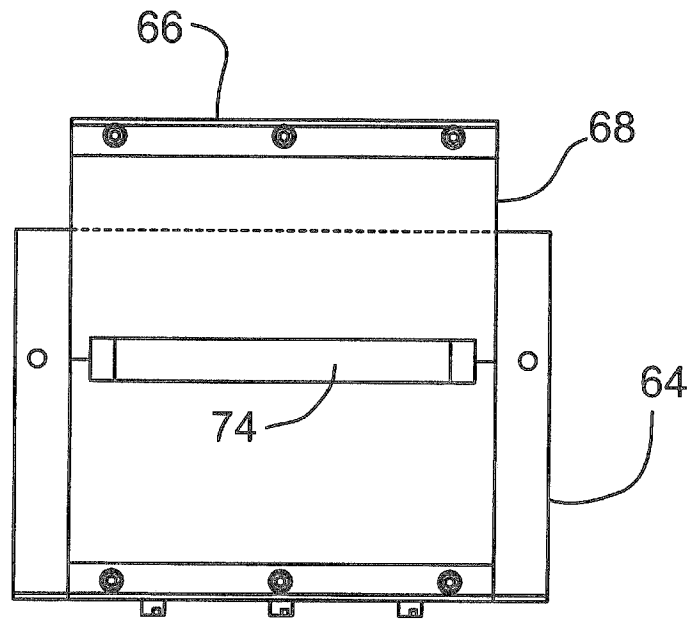
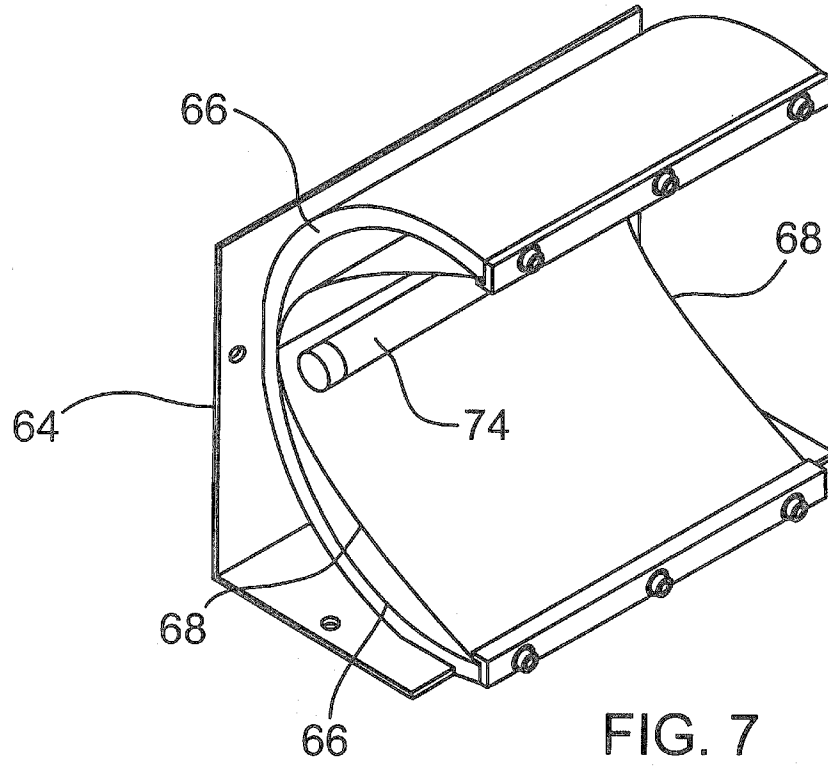
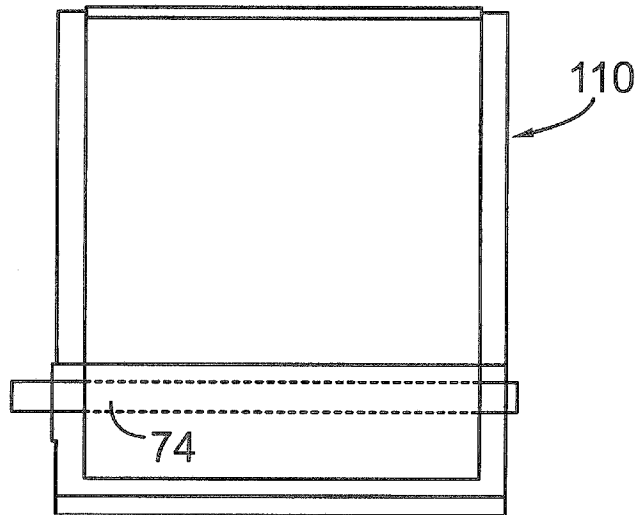
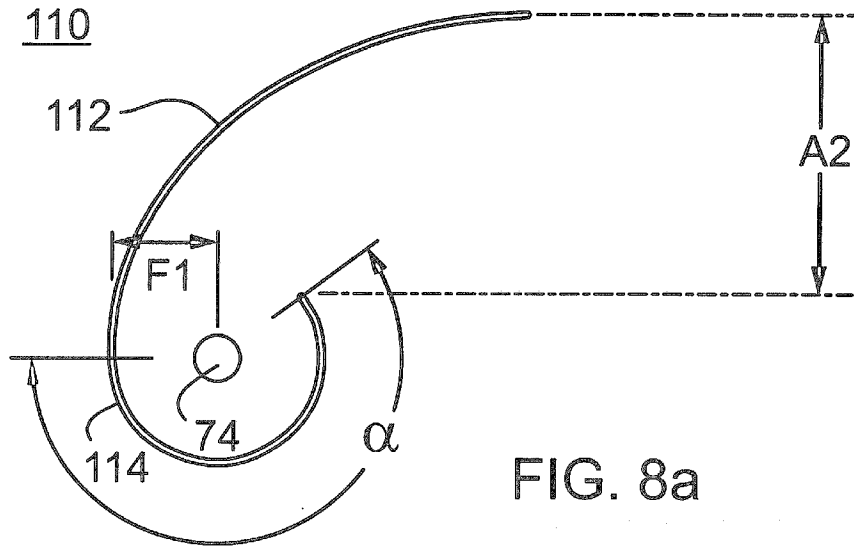


FIG. 6

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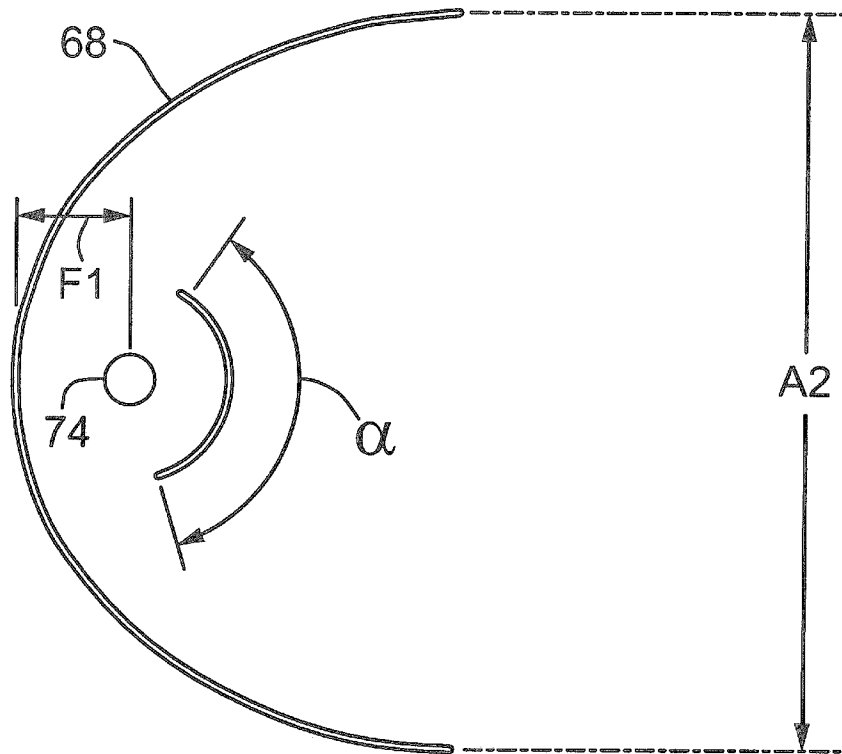


FIG. 8c

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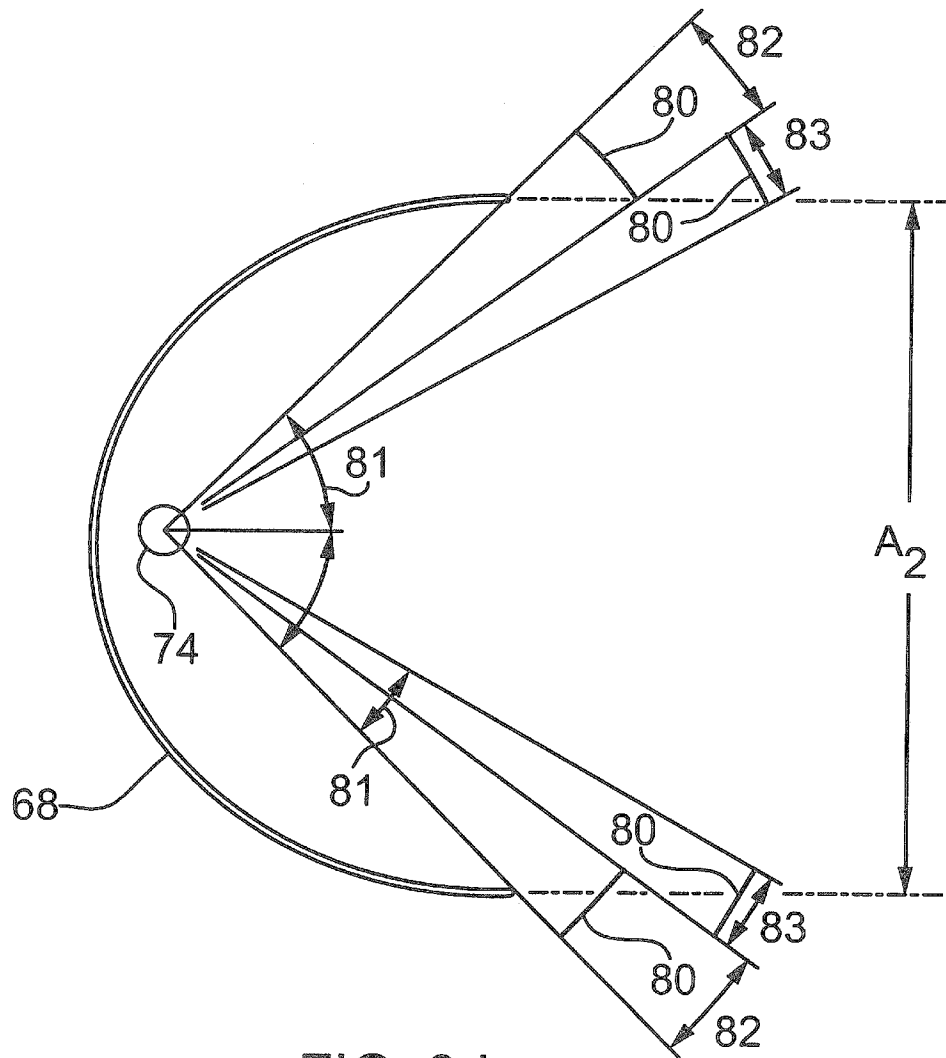


FIG. 8d

FIG. 9

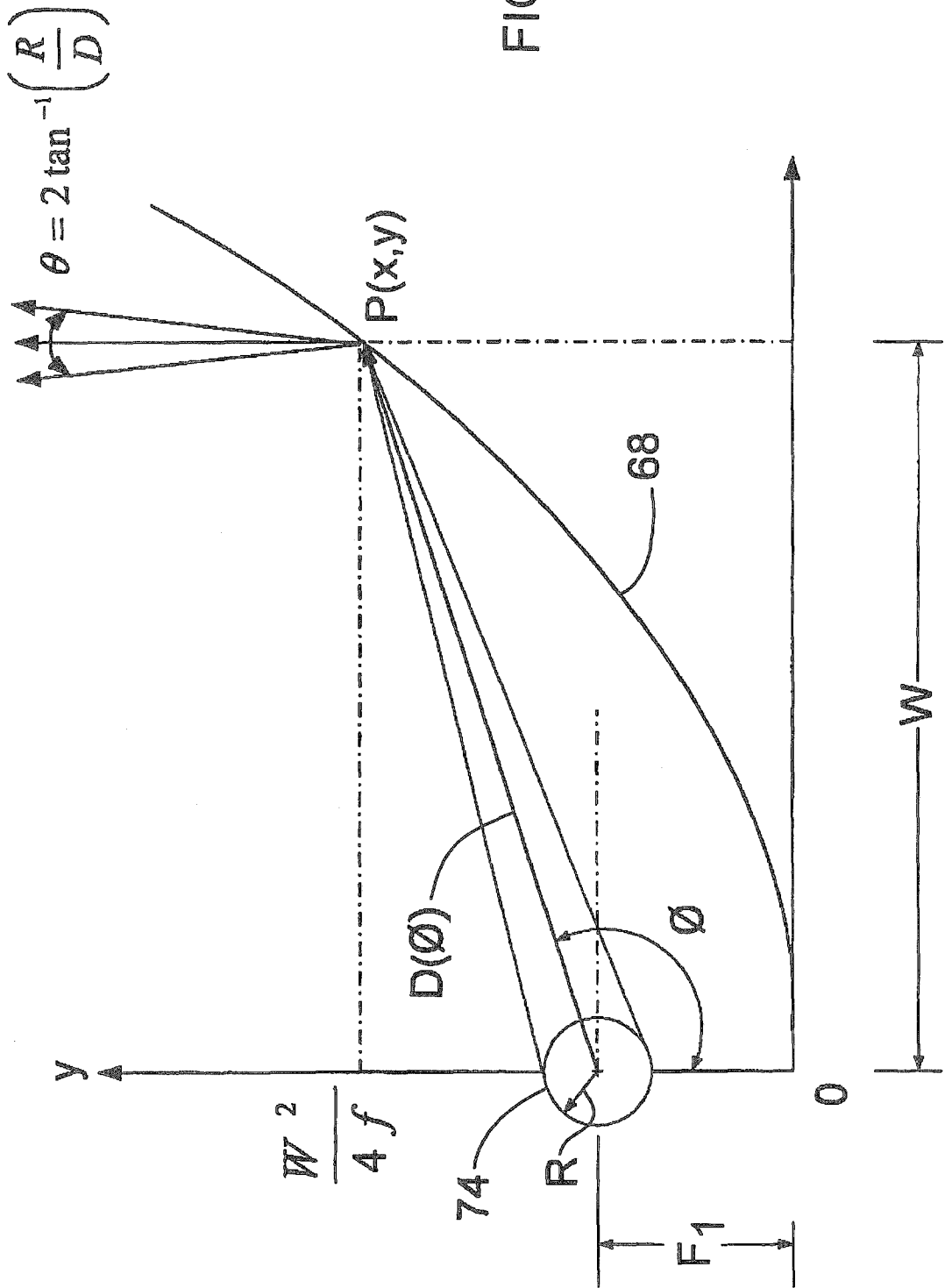
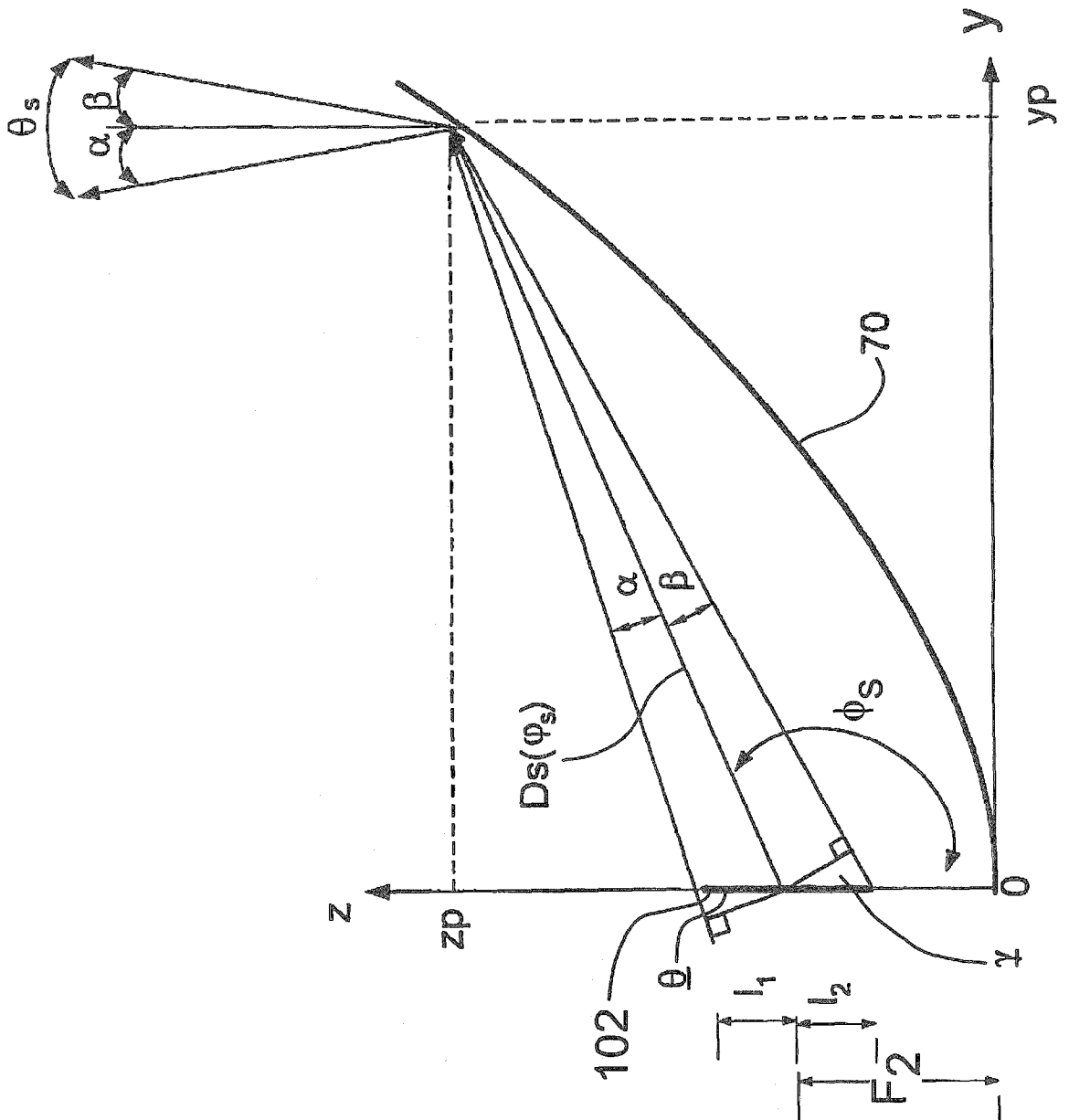


FIG. 10



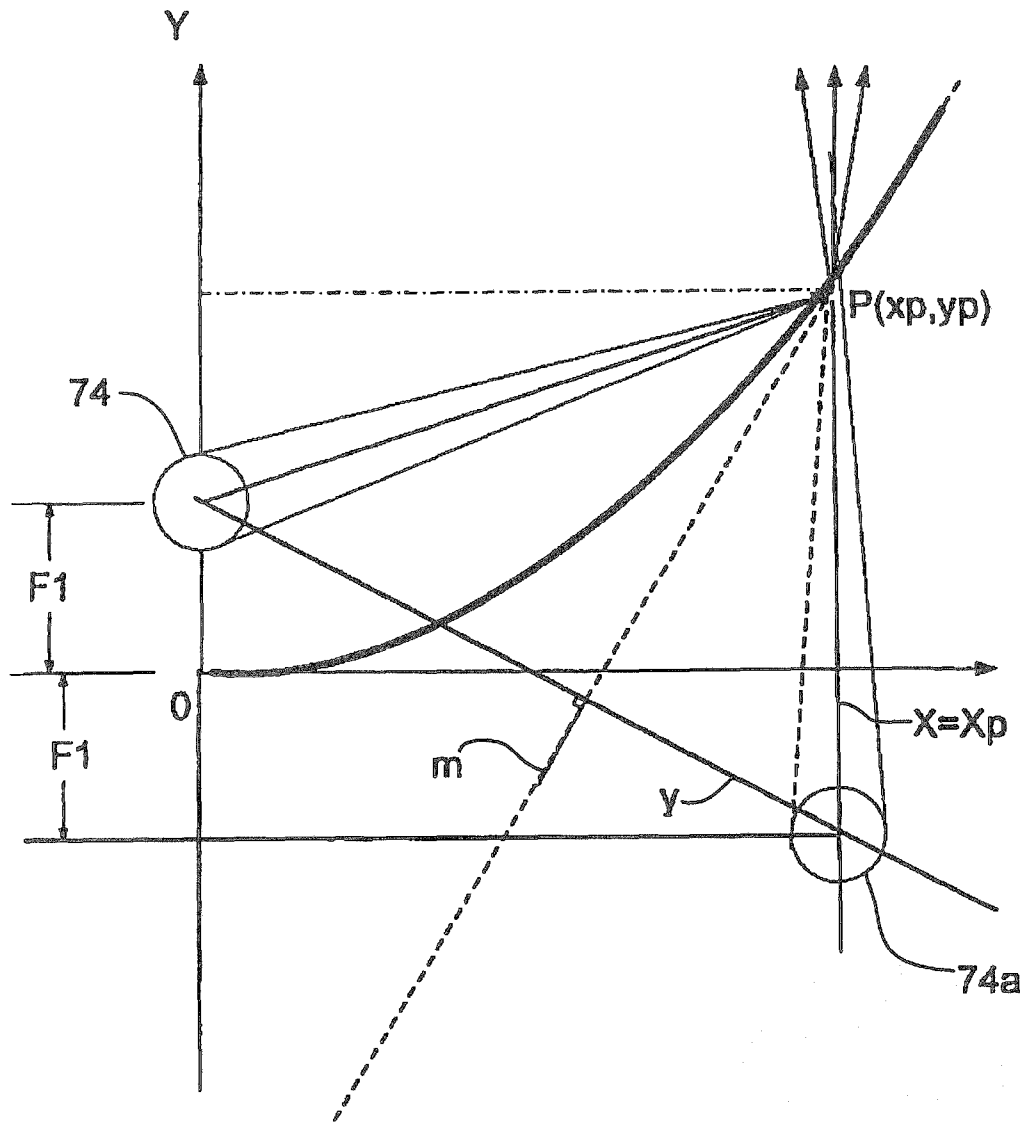


FIG. 11

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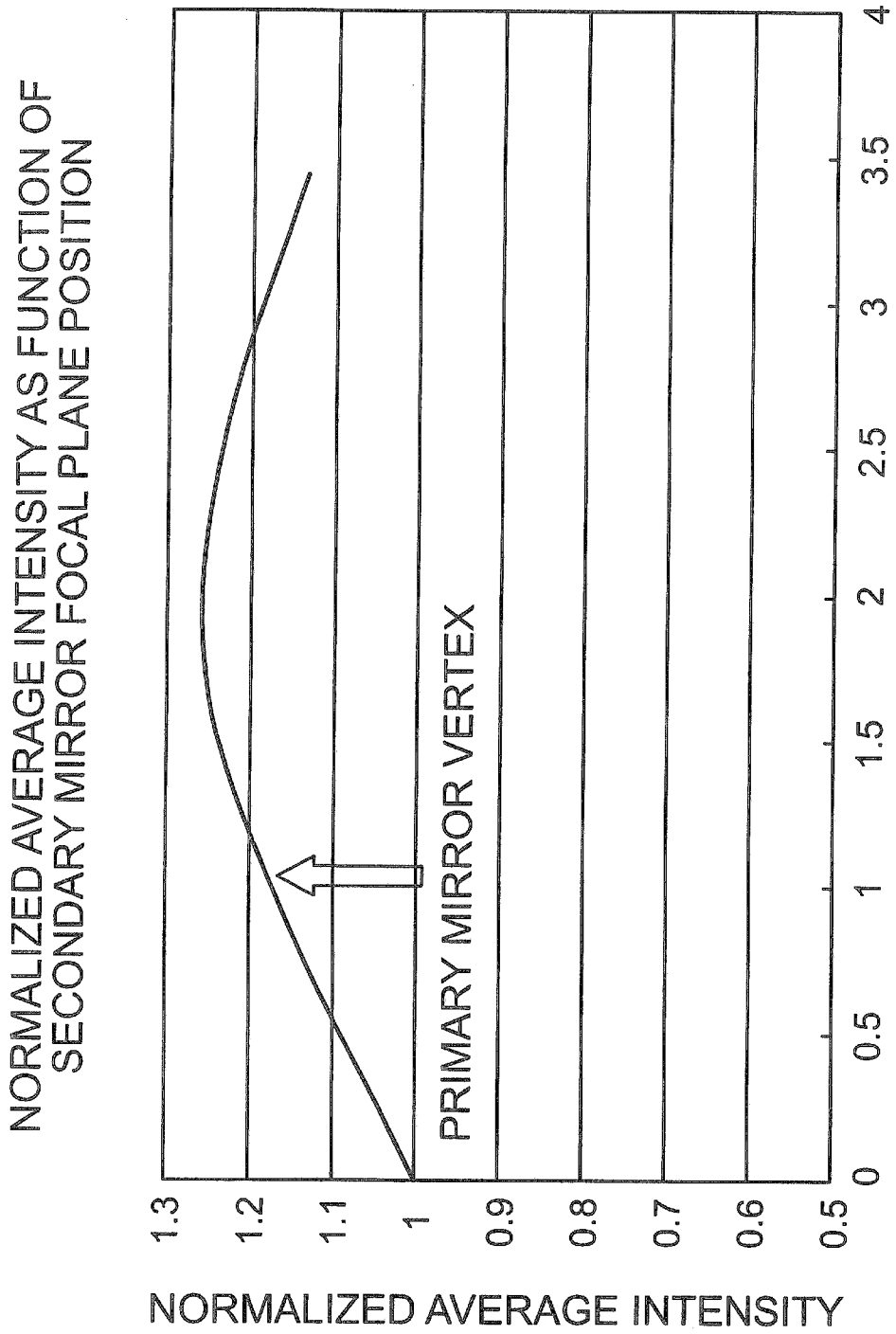


FIG. 12

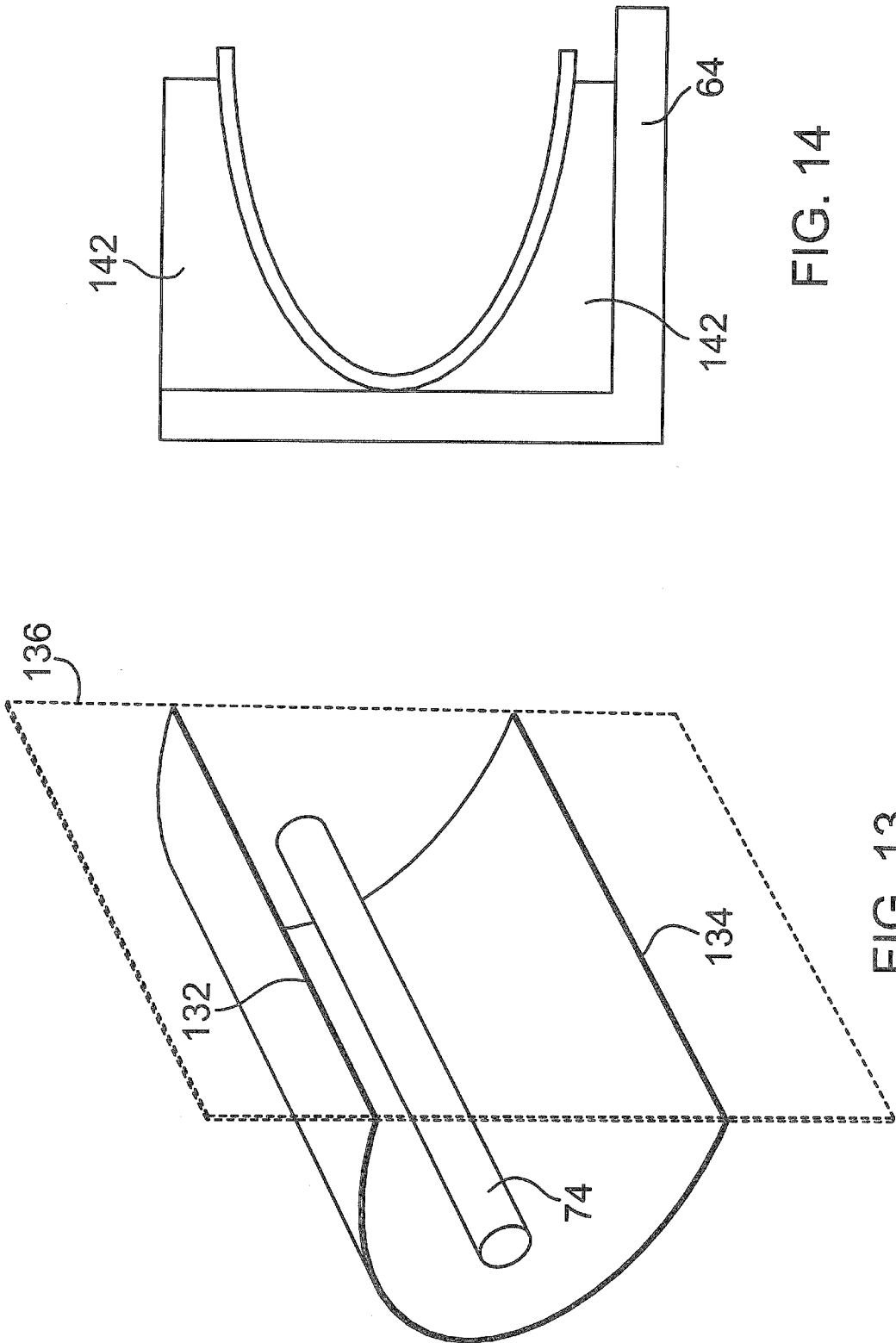


FIG. 14

FIG. 13

**INTERNATIONAL SEARCH REPORT**

International application No.  
PCT/CA2011/050659

A. CLASSIFICATION OF SUBJECT MATTER  
**IPC: F21V 7/09 (2006.01)**  
 According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
**IPC: F21V 7/09**

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic database(s) consulted during the international search (name of database(s) and, where practicable, search terms used)  
 Canadian Patent Data Base, EPODOC and Total Patent  
 keywords: reflector, dual, two, linear, collimate, cylind+ and lamp

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4755916 A (COLLINS, W.) the whole document	05 July 1988 (05-07-1988) 1 to 24
A	US 7556399 B1 (BAILEY, M. L.) the whole document	07 July 2009 (07-07-2009) 1 to 24
A	EP 1708513 A2 (JONG -HOI, K. et al.) the whole document	04 October 2006 (04-10-2006) 1 to 24
A	US 2006/0171160 A1 (MEYRENAUD, J.-L.) the whole document	03 August 2006 (03-08-2006) 1 to 24
A	US 6536921 B1 (SIMON, J. H.) the whole document	25 March 2003 (25-03-2003) 1 to 24

Further documents are listed in the continuation of Box C.       See patent family annex.

* Special categories of cited documents :	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier application or patent but published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 12 January 2012 (12-01-2012)	Date of mailing of the international search report 19 January 2012 (19-01-2012)
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Name and mailing address of the ISA/CA Canadian Intellectual Property Office Place du Portage I, C114 - 1st Floor, Box PCT 50 Victoria Street Gatineau, Quebec K1A 0C9 Facsimile No.: 001-819-953-2476	Authorized officer  <b>Malgorzata Samborski (819) 956-0759</b>
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**INTERNATIONAL SEARCH REPORT**  
Information on patent family members

International application No.  
PCT/CA2011/050659

Patent Document Cited in Search Report	Publication Date	Patent Family Member(s)	Publication Date
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