



(86) Date de dépôt PCT/PCT Filing Date: 2002/07/17

(87) Date publication PCT/PCT Publication Date: 2003/02/06

(85) Entrée phase nationale/National Entry: 2003/12/16

(86) N° demande PCT/PCT Application No.: EP 2002/008075

(87) N° publication PCT/PCT Publication No.: 2003/009952

(30) Priorité/Priority: 2001/07/25 (01306379.7) EP

(51) Cl.Int.⁷/Int.Cl.⁷ B21D 15/06, B21D 51/26

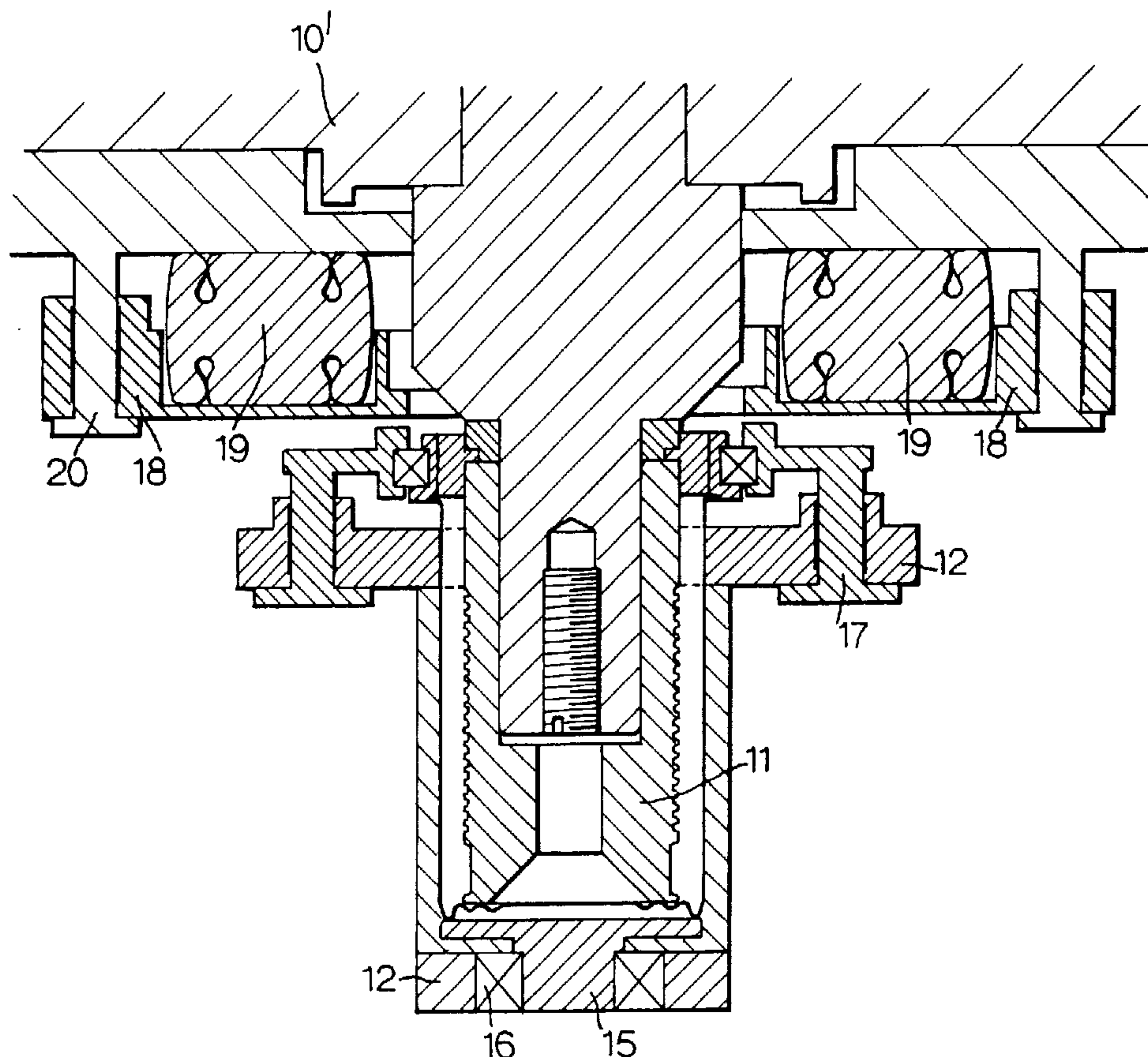
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(54) Titre : MOULURAGE DE RECIPIENTS

(54) Title: CONTAINER BEADING



(57) Abrégé/Abstract:

Beading of containers such as two and three piece can bodies by rolling the can body between tools, typically a roll/roll or a roll/rail of a rotary turret (10) system. During beading, a load is applied along the central axis of the can body, whereby axial and panel performance of the beaded can is improved. This load is applied for example by the use of miniature air bags (19) which are fixed to the turret.

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
6 February 2003 (06.02.2003)

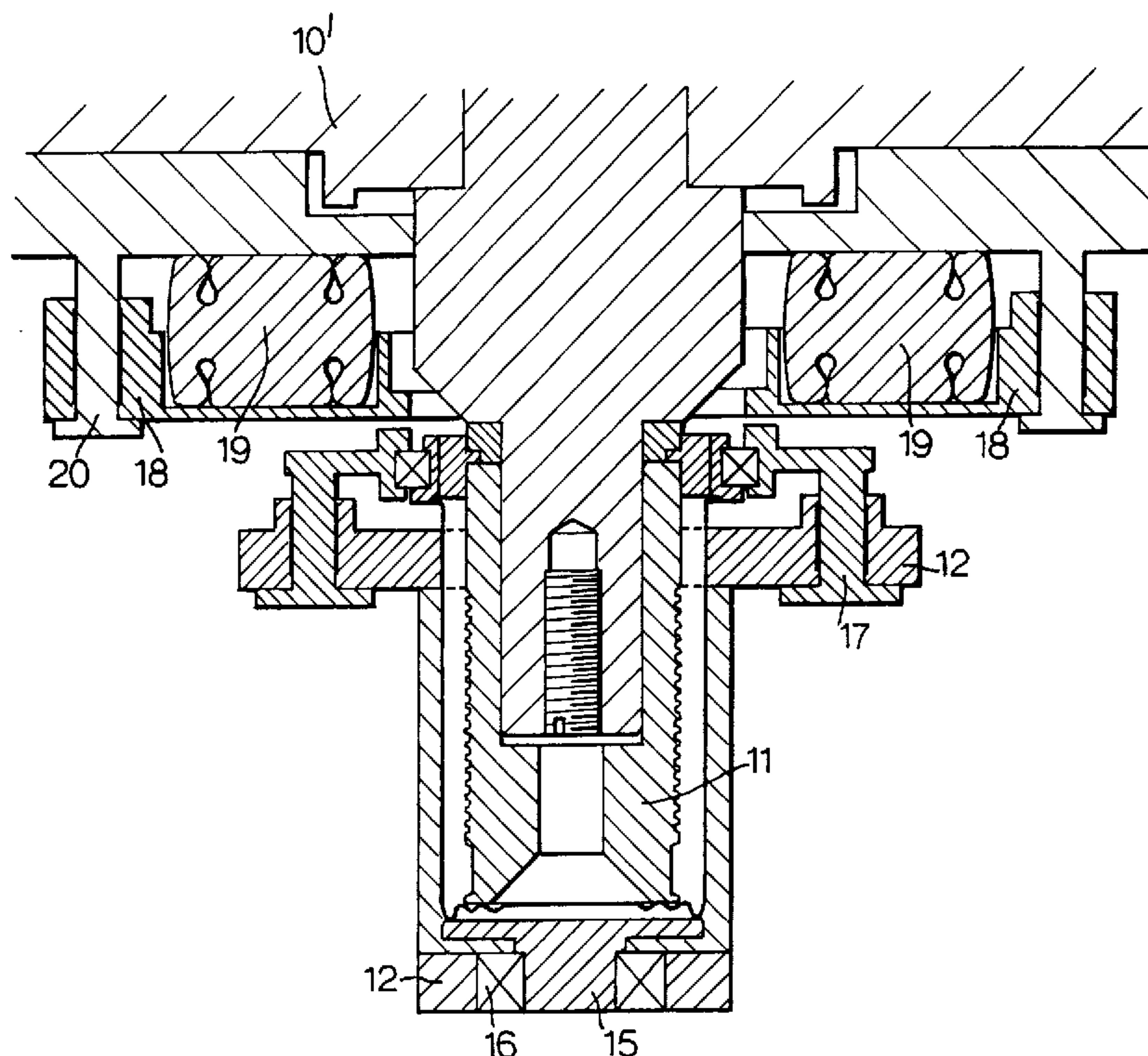
PCT

(10) International Publication Number
WO 03/009952 A1

- (51) International Patent Classification⁷: **B21D 15/06,** (72) Inventors; and
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- (21) International Application Number: PCT/EP02/08075
- (22) International Filing Date: 17 July 2002 (17.07.2002)
- (25) Filing Language: English (74) Agent: **RATLIFF, Ismay, Hilary**; Group Intellectual
Property, CarnaudMetalbox plc, Downsview Road, Wan-
tage, Oxfordshire OX12 9BP (GB).
- (26) Publication Language: English
- (30) Priority Data: 01306379.7 25 July 2001 (25.07.2001) EP (81) Designated States (*national*): AE, AG, AL, AM, AT, AU,
AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,
CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH,
GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC,
LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW,
MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG,
SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ,
VN, YU, ZA, ZM, ZW.
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[GB/GB]; Downsview Road, Wantage, Oxfordshire OX12
9BP (GB). KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW),
Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM),

[Continued on next page]

(54) Title: CONTAINER BEADING



(57) Abstract: Beading of containers such as two and three piece can bodies by rolling the can body between tools, typically a roll/roll or a roll/rail of a rotary turret (10) system. During beading, a load is applied along the central axis of the can body, whereby axial and panel performance of the beaded can is improved. This load is applied for example by the use of miniature air bags (19) which are fixed to the turret.



WO 03/009952 A1

WO 03/009952 A1



European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

Published:

— *with international search report*

CONTAINER BEADING

This invention relates to beading and, in particular but not exclusively, to the beading of cans using roll/rail and roll/roll beading systems.

Container body beads are formed by a beading machine
5 of, for example, the rotary turret type, in which a container is mounted on a mandrel and rolled over fixed rail segments progressively to form beads in the container side wall. The beading rail is profiled to form the beads as the can body is forced against the rail. The
10 internal mandrel, or alternative male tool element, has a complementary profile to that of the rail. Alternatively, beads may be formed by the relative motion of external rollers (also referred to simply as "rolls") and an internal mandrel, the container being mounted and freely
15 rotatable on the mandrel.

Can performance is typically quantified in terms of axial collapse and panel performance (distortion from the original, e.g. circular, cross-section under unbalanced external pressure). Whilst conventional beaded cans
20 provide acceptable axial and panel performance, there is a need to improve performance still further in order to enable additional metal savings to be made.

According to the present invention, there is provided a method of beading a container, the method
25 comprising: mounting a can body on a first tool such that the can body is freely rotatable; moving the can body and first tool into contact with a second tool, such that the can body is clamped between the tools, at least one of the tools including a beading profile; applying a load
30 along the central axis of the can body; and forming

-2-

circumferential beads in the can body side wall by rolling the can body between the tools, whilst maintaining the positive axial load on the can body.

The Applicant has found that by applying a positive axial load to the can body during the beading operation, axial collapse and panel performances are improved by around 10% over standard beading without compromising can geometry. By a "positive" axial load, it is meant that that load is directed along the longitudinal axis of the can and is a net compressive load, rather than being balanced out by an opposite force, such as a locating force.

Usually the can body has a flange and the method may further comprise holding the flange in a freely rotatable flange support ring. This ring prevents the flange from collapsing and/or overgrowing when under load.

The axial load may be applied either to the flange end of the can body, or to the opposite end. Clearly the opposite end could be the integral base of the can body in a so-called "two-piece" can body, open in a tubular "three-piece" can body, or the can end of a three-piece can body with one closed, typically seamed-on end. Although loading the can body from both ends is, in theory, possible and may generate further benefits in can performance, loading at one end is more practical as this enables conventional bead-ers to be used.

For can bodies of from 60 to 250 mm in diameter and having a wall thickness of between 40T (0.102mm) and 60 T (0.152mm), where "T" is tenths of thou (thousandths of an inch), the axial load applied may be between 0 N and 900

-3-

N, performance benefits being realised over all levels of axial load. However, high loads may lead to unacceptable pull down (reduction in can height) and/or flange growth so that ideally the load may be 600 N or less. Preferably
5 for a can body having a 48T (0.123mm) wall thickness, the applied load is from 300 N to 600 N, and for optimum performance benefit may be 600 N. Applied load varies in direct proportion to the wall thickness and clearly applied load may be greater for larger containers having
10 bigger, deeper beads.

In a preferred embodiment for the same 73 mm diameter can body of 48T (0.123mm) wall thickness, the bead forming step comprises forming beads of up to 0.0215" (0.546mm) with a maximum pull-down of
15 approximately 0.04" (1 mm).

According to a further aspect of the present invention, there is provided an apparatus for beading a container, the apparatus comprising: a mandrel for internal support of the can body; a tool for external
20 engagement with the can body, the mandrel and external tool having complementary bead profiles; and means for applying a load along the central axis of the can body during beading of the can body side wall.

The apparatus usually includes a can body carrier, such as a cradle, and a plate for supporting the base of
25 a two piece can body or one end of a three piece can body. The load may be applied via the base plate or, for ease of changing the load to be applied, the load application means may include at least one air bag at the
30 end opposite to the plate, such that the applied load is

-4-

in line with the central axis of the mandrel. In the latter case, load may be applied by axial movement of the plate whereby the air bags are compressed and provide a reactive axial load on the can body.

5 A preferred embodiment of the invention will now be described, by way of example only, with reference to the drawings, in which:

Figure 1 is a schematic perspective view of a prior art apparatus for beading a can body;

10 Figure 2 is a partial side section of a beader with a can body mounted on a profiled mandrel for bead forming;

Figure 3 is a partial side section of the beader, perpendicular to the view of figure 2;

15 Figures 4 to 9 are partial side sections of the can carrier during a typical beading sequence.

The prior art beader of figure 1 is of the type described in EP-0006321 and comprises a rotary turret 10 carrying heads, each of which comprises a profiled mandrel 11 which is rotatably mounted on the turret on a shaft (not shown). Can bodies 1 are fed onto the mandrels 11 by infeed star wheel 14 and are initially held in position by cradles 12. As the turret rotates in the direction of the arrow, the can bodies engage a beading rail 13. The shafts of the mandrel are driven so that the mandrels and can bodies mounted thereon roll along the rail 13.

25 In this prior art beader, metal is drawn in tension from plain wall sections at either end of the can bodies
30 thereby progressively forming one or more beads or

-5-

clusters of beads 4 and, for two piece can bodies, a rolling bead 5, in the can side wall as bead depth is increased. Beaded cans are discharged by a further starwheel (not shown), leaving the can carrier 12 free to
5 receive the next can body blank.

Figure 2 is a first side view of the axial loading system and shows a two piece can body 1, having an integral base 2 and flange 3 at its open end and mounted on mandrel 11. Bead cluster 4 is formed in the can side
10 wall in conventional manner by rolling the profiled mandrel 11 and can body 1 along the bead forming rail 13. Rolling bead 5 adjacent the can base 2, enables the can body to roll in a straight line during labelling or processing in a reel and spiral cooker, for example and
15 is not required for three piece can bodies.

The base 2 of the can is supported by base plate 15 which is mounted via bearings 16 for free rotation on can carrier cradle 12. During beading, the flange 3 of the can body 1 engages a flange support ring 17 which is
20 connected to the can carrier 12 (best seen in figure 2a).

Figure 3 is a second side view of the axial loading system, perpendicular to the view of figure 2 and showing the rotary turret 10' and air bags 19, which are held in position by means of yoke plate 18. The can is loaded
25 through its central axis by twin air bags 19 which transfer the load via yoke plate 18 when the plate is engaged by the rotary flange support ring 17 during canming of the can carrier or cradle 12. Movement of the air bags is limited by height stops 20 but both the yoke

-6-

plate and flange support ring are fully floating in order to ensure evenly distributed load around the can flange.

In contrast with the prior art beader of figure 1, in the beader of the present invention, metal from the plain wall sections is drawn in compression due to the applied axial load. Whilst the embodiment shown in the drawings uses air bags to load the system, clearly other biasing devices could be used within the scope of the invention. By using air bags, loads can be easily changed if desired, remain constant throughout the life of the air bag and, by linking each head of the rotary turret machine to a common air supply, are equal on each head.

The progression of movement of the can carrier, flange support ring and yoke plate for application of an axial load to the can body is set out in figures 4 to 9.

During rotation of the turret, the can carrier 12 and flange support ring 17 cam back towards the turret (upward arrows in the figures) over the profiled mandrel until the flange support ring contacts the yoke plate 18 which retains the air bags in position (figures 4 and 5). In order to clamp the can in position, the carrier continues camming backwards, thereby reducing in height, until the position shown in figure 6. The can body which is held in the carrier then engages flange support ring 17. No movement of the yoke plate has occurred at this stage and consequently no loading of the can body.

Once the can is clamped in the carrier, the carrier continues camming backwards by typically 3 mm, thereby moving the yoke plate the same distance (figure 7). The movement of the yoke plate initiates loading of the can

-7-

by transferring of the axial load from the air bags. This movement of the yoke plate 18 compresses the air bags 19 and also takes up any slack in the system.

When the can carrier is fully back, as shown in figure 7, beading commences. During beading, the can body reduces in height due to the bead formation and the air bags and flange support ring 17 move forward to follow this movement by typically 1 mm to compensate for the pull down (figure 8).

After the completion of beading, the carrier 12, and flange support ring mounted on the carrier cam forward (figure 9) to discharge the can body. It is clear from figure 9 that the carrier 12 has completely disengaged from flange support ring 17.

In the present invention, the compression of the air bags 19 during beading causes the can body to be loaded along its central axis via yoke plate 18 and flange support ring 17, by virtue of the location of the can body flange in the flange support ring.

In the figures 4 to 9, backward movement towards the turret is denoted by an upward arrow and forward movement, away from the turret, by a downward arrow on the relevant moving parts of the apparatus.

25

Example 1

A roll/roll single headed beader was used to quantify the axial and panel performance of a set of cans having a beading profile formed whilst applying an axial

30

-8-

load. Each can was free to rotate while being clamped and beaded and a flange support ring prevented the can flange from collapsing and overgrowing when under load.

Twenty 73 mm diameter x 108.5 mm cans of 48T
5 (0.114mm) side wall gauge were beaded for each setting, that is:

- (i) three different bead depths (shallow 0.016" (0.406mm), standard 0.0205" (0.521mm) and deep 0.025" (0.635mm)); and
- 10 (ii) axial clamping loads of from 0 to 900N.

A gain of 10% in axial and panel performance over standard beading was found for all given bead depths at 400N axial load. It is believed that by beading under compression, local thinning of the metal was reduced,
15 thereby improving performance. Performance improvements may, however, also be due to geometrical changes. A gain of up to 25% was achieved with high clamping loads but exhibited unacceptable pull down and flange growth above 600N.

20

Example 2

In order to mimic production conditions more closely, the experiment of example 1 was conducted using
25 a rotary turret roll/rail beader similar to that shown in figure 1. The present example loaded the can at the flange end only, using the air bag loading system of figures 2 to 8. Can sizes were as in example 1 (i.e. 73 mm diameter x 108.5 mm cans, side wall gauge of 48T

-9-

(0.213mm)). 50 samples were tested for each beader setting as follows:

(i) three bead depths (0.018" (0.457mm), 0.021" (0.533mm) and 0.024" (0.61mm)); and

5 (ii) axial loads of 0, 300N, 450N, 600N and 900N.

Axial and panel performance benefits were realised at all levels of axial load, with maximum overall gain of approximately 3-4% over zero load being generated at 600N. Performance gains were more sensitive at shallower
10 bead depths. At a target bead depth of 0.021" (0.533mm), axial strength increased with axial load to a peak at about 600N load. Panel performance mirrored this improvement in axial performance when an axial load was applied during beading.

15 Variability of both axial and panel failure was considerably reduced by all axial loading, irrespective of value. Axial loading resulted in increased levels of pull-down than without such loading but this remained within acceptable limits at 0.04" (1mm) pulldown at 600N
20 axial load. Flange growth at loads up to 600N (inclusive) was insignificant but some growth was experienced at 900N.

The invention has been described by way of example only and changes may be made to the apparatus within the
25 scope of the invention. For example, other methods of loading the system may be used although ideally loading should be carried out through the central axis of the can body. The load may be applied via the flange end or base (opposite to the flange end), or both ends of the can

-10-

body. The invention is equally applicable to two and three piece can bodies.

-11-

CLAIMS:-

1. A method of beading a container, the method comprising:

mounting a can body on a first tool such that the can body is freely rotatable;

moving the can body and first tool into contact with a second tool, such that the can body is clamped between the tools, at least one of the tools including a beading profile;

applying a load along the central axis of the can body; and

forming circumferential beads in the can body side wall by rolling the can body between the tools;

characterised by applying a load which is a positive axial load and maintaining the positive axial load on the can body during bead formation.

2. A method according to claim 1, in which the can body has a flange and the method further comprises holding the flange in a flange support ring.

3. A method according to claim 2, in which the axial load is applied to the flange end, the opposite end, or to both ends of the can body.

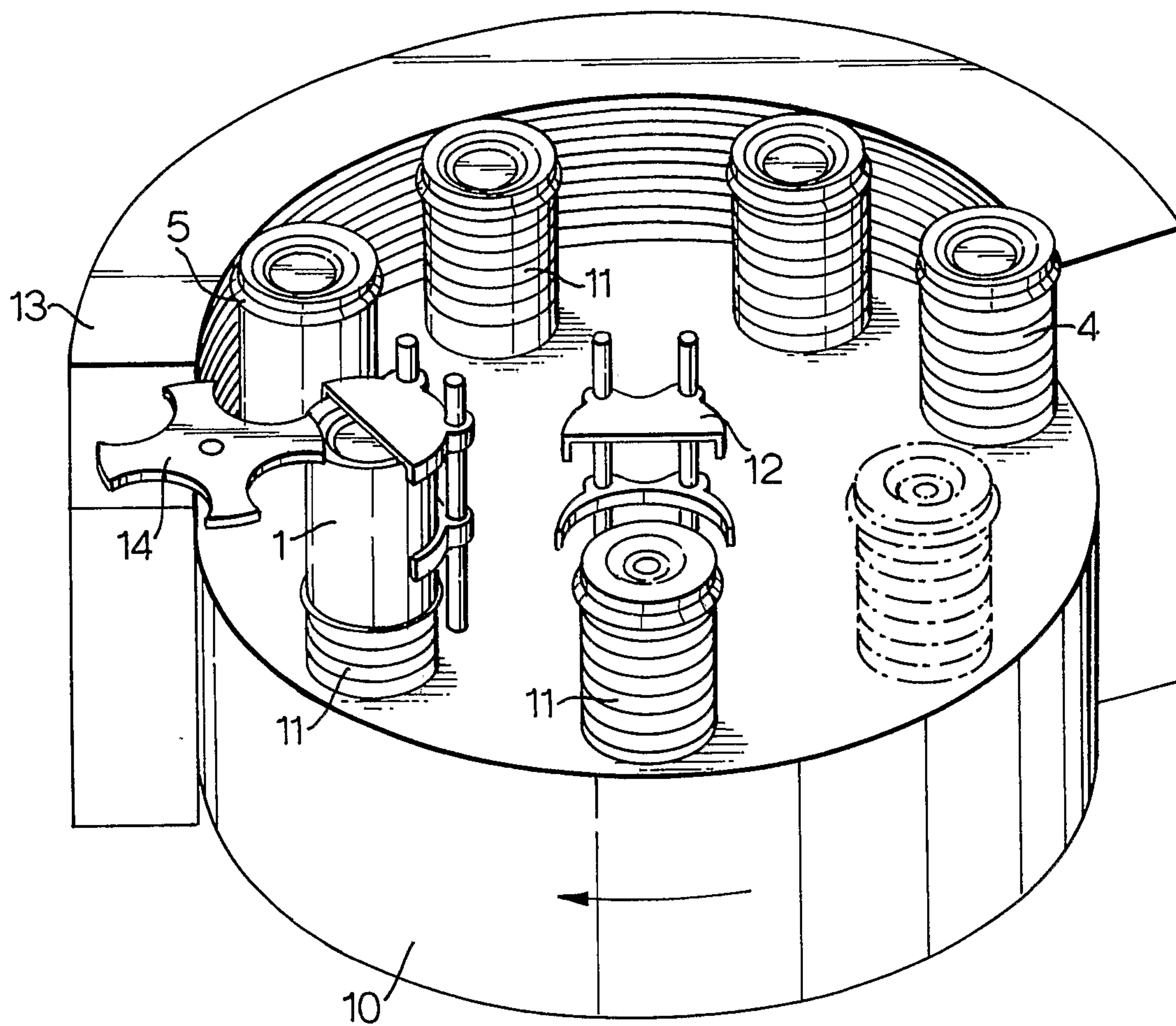
4. A method according to any one of claims 1 to 3, in which the can body diameter is from 60 to 250 mm, can wall thickness is between 40T (0.102mm) and 60T (0.152mm) and the axial load applied is between 0 N and 900 N.

-12-

5. A method according to claim 4, in which the wall thickness is from 40T (0.102mm) to 60T (0.152mm) and the axial load is 600 N or less.
6. A method according to claim 5, in which the axial load is from 300 N to 600 N.
7. A method according to any one of claims 4 to 6, in which the bead forming step comprises forming beads of up to 0.0215" (0.546mm) with a maximum pull-down of approximately 0.04" (1 mm).
8. An apparatus for beading a container, the apparatus comprising:
a first roll for supporting a can body such that the can body is freely rotatable on the roll; and
a fixed rail or second roll, the first roll and fixed rail or second roll having complementary bead profiles;
characterised by means for applying a positive axial load of from 300 N to 600 N along the central axis of the can body during beading of the can body side wall.
9. An apparatus according to claim 8, in which the load application means includes at least one air bag in line with the central axis of the can body.

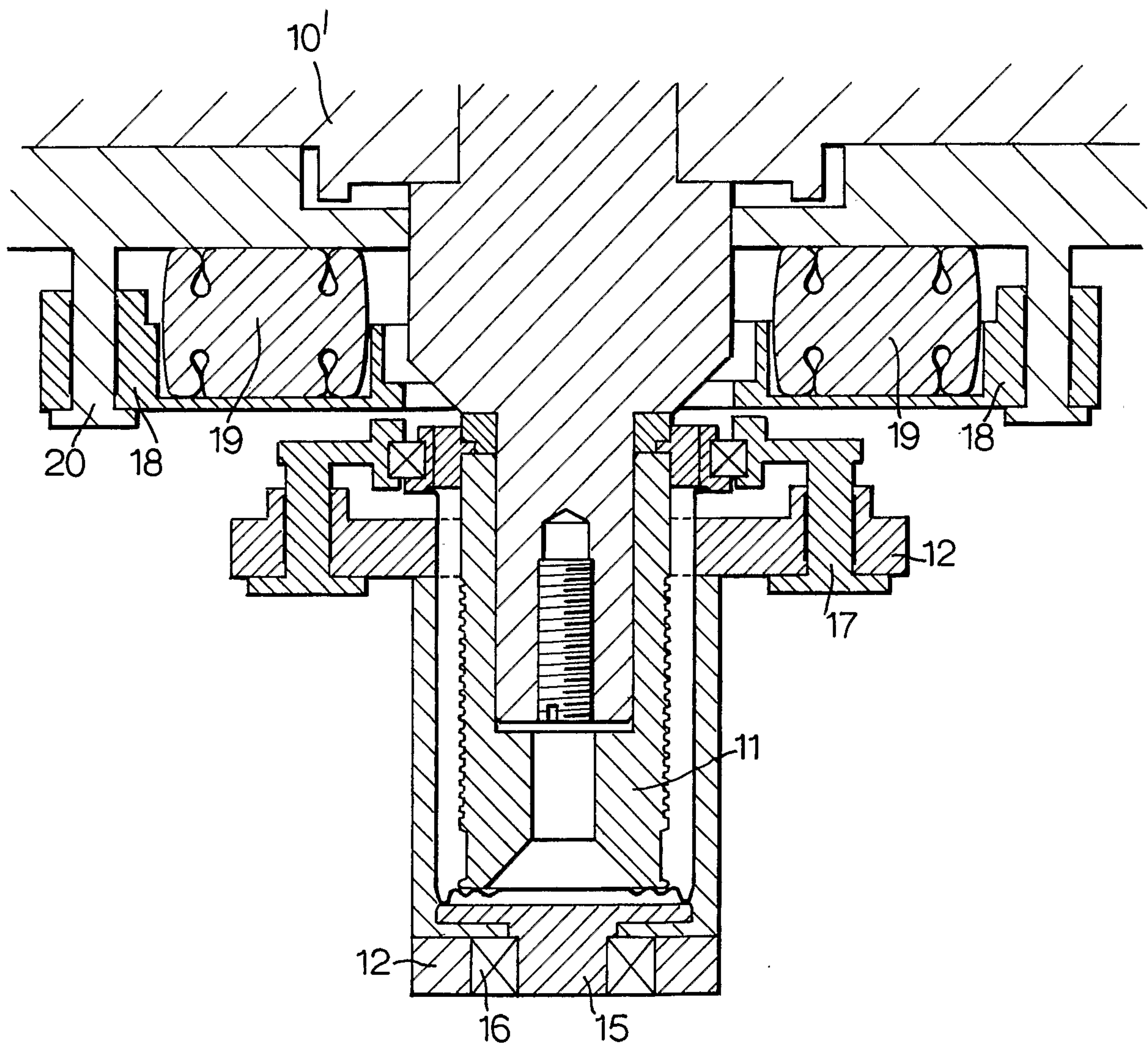
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Fig.1.
PRIOR ART



3/5

Fig.3.



4/5

Fig.4.

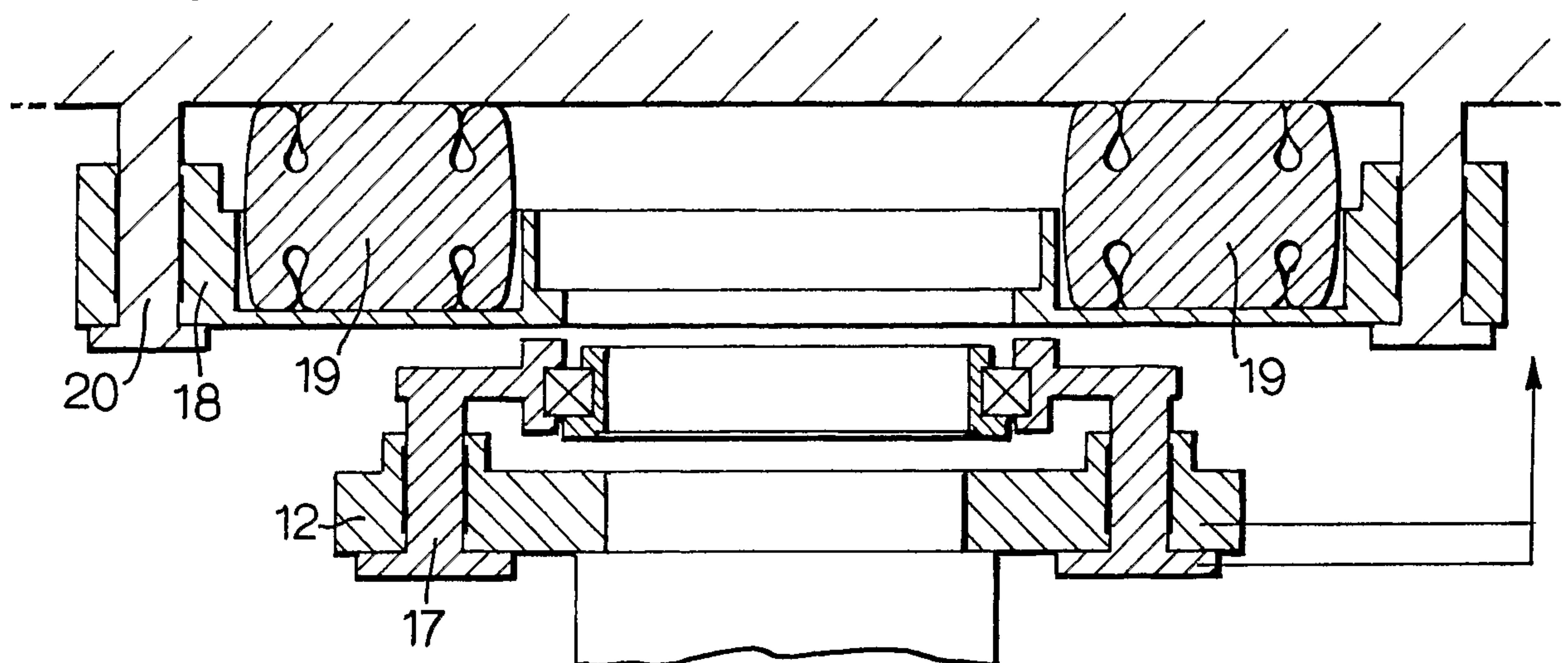


Fig.5.

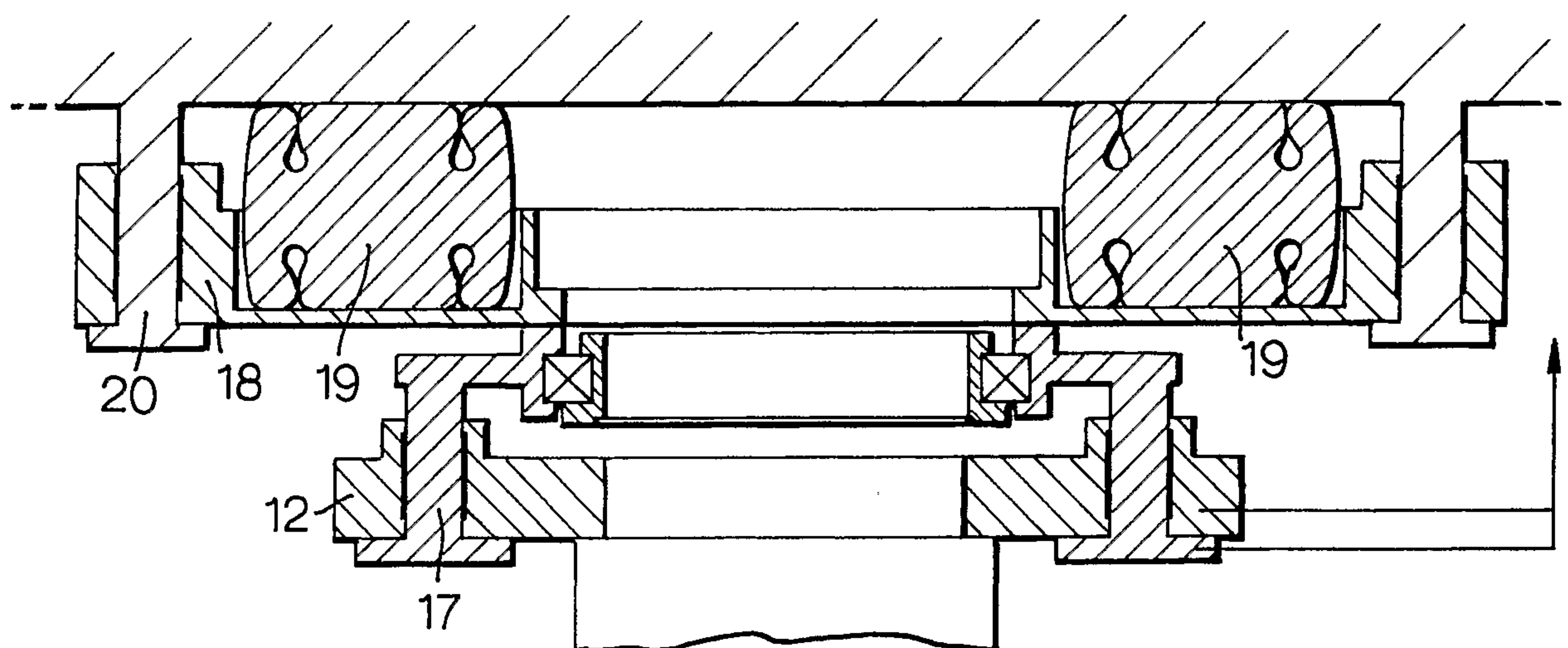
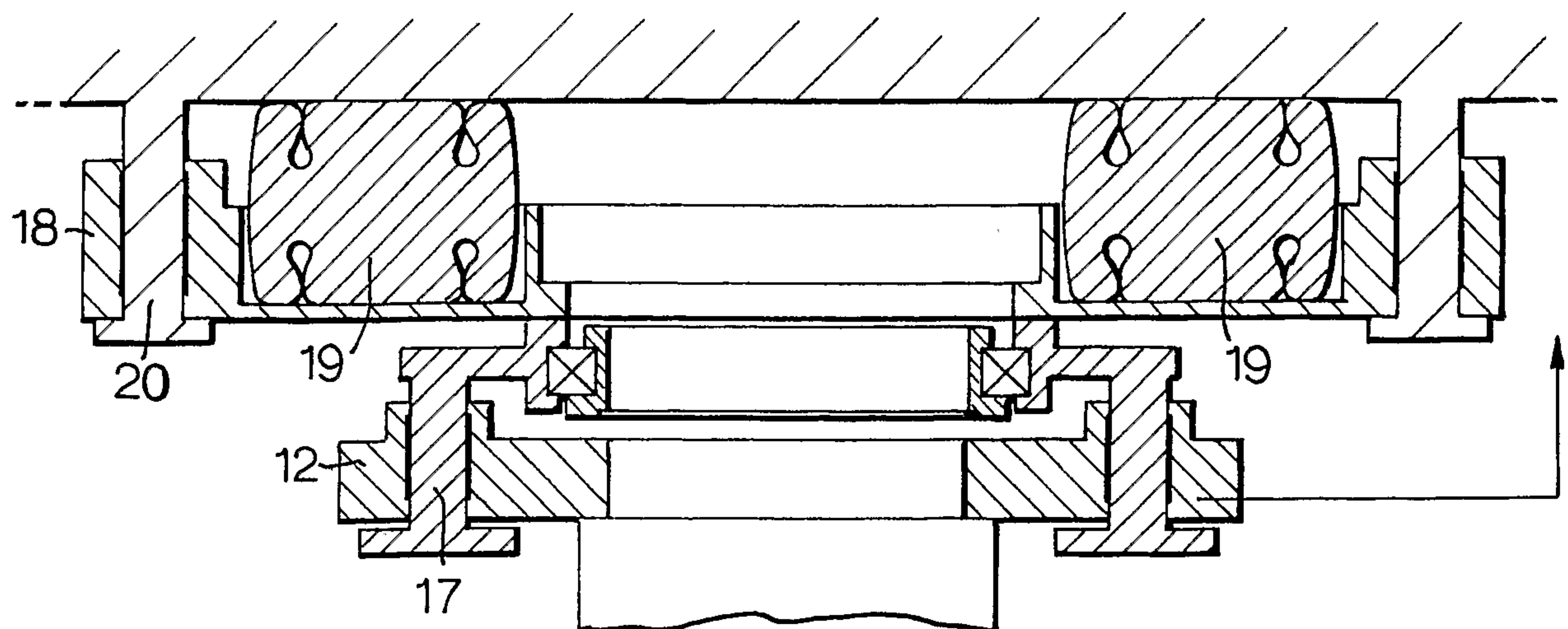


Fig.6.



5/5

Fig.7.

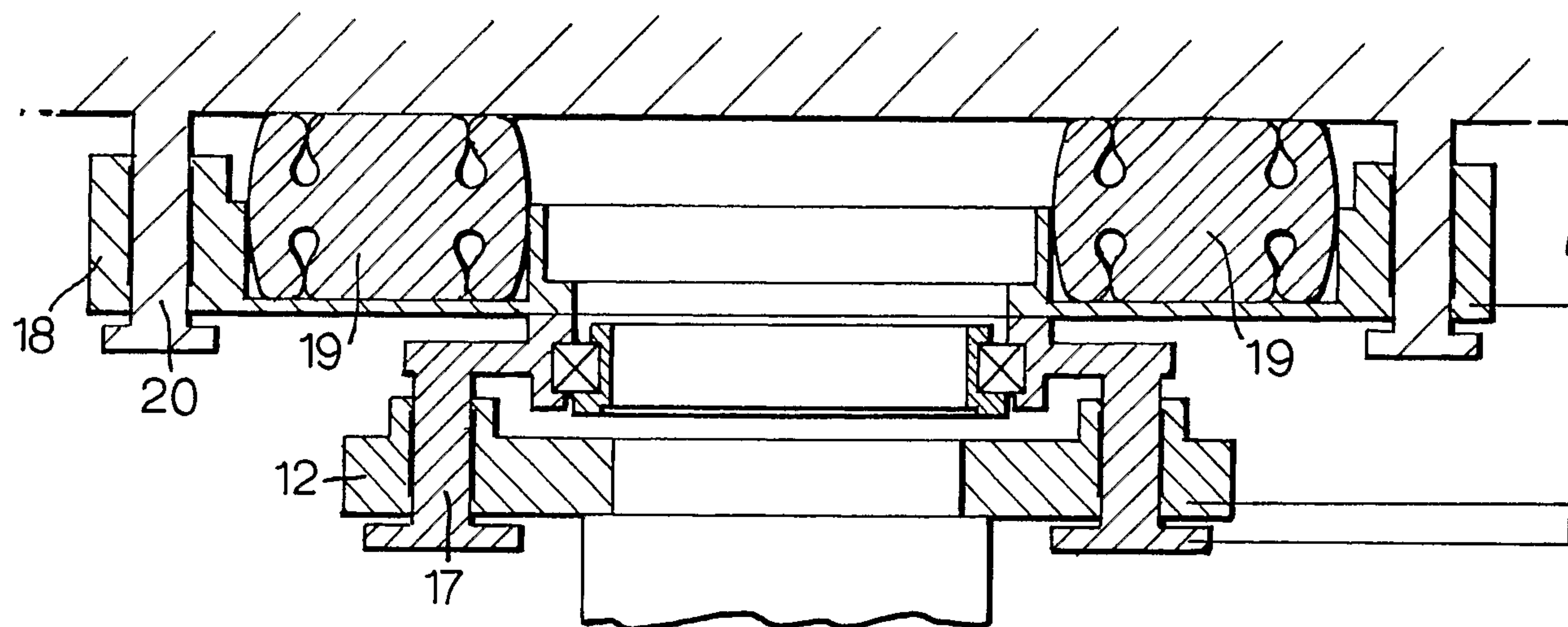


Fig.8.

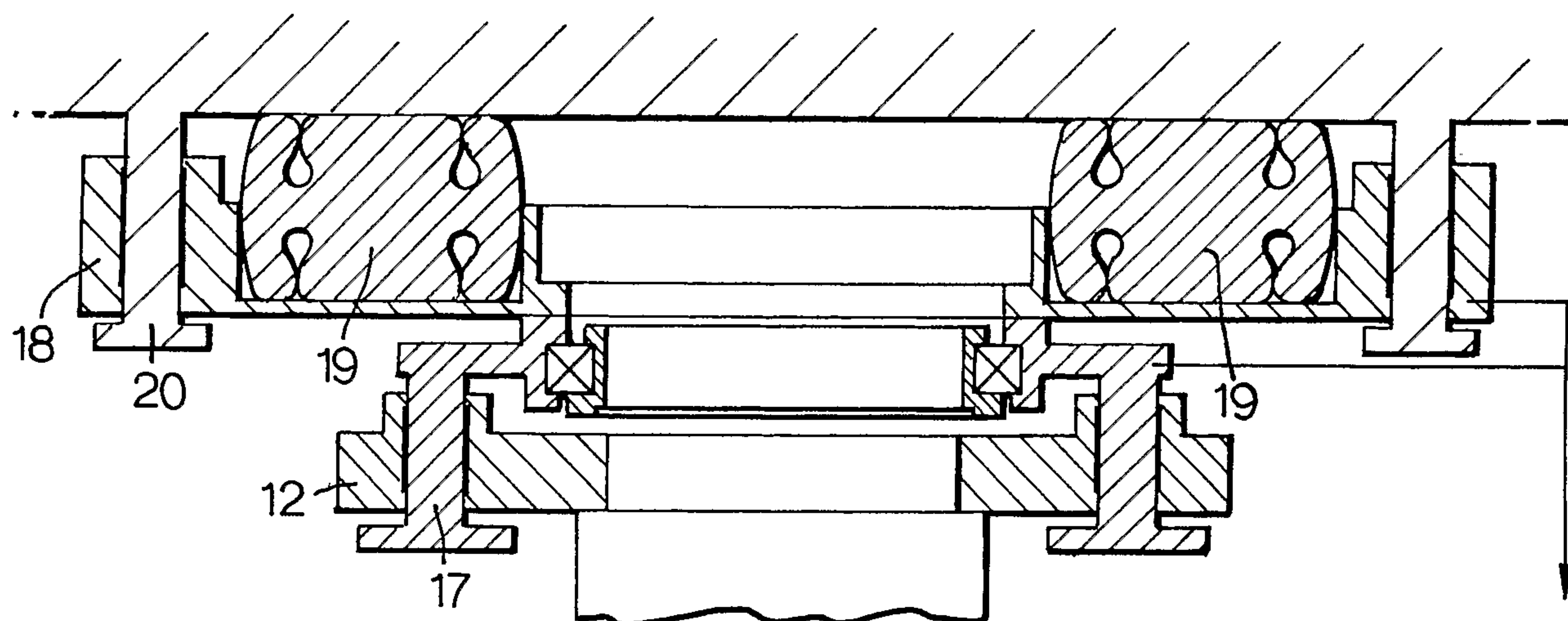


Fig.9.

