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DESCRIPTION

Field of invention

[0001] The present invention relates to a thrust bearing for a wind turbine.

Art Background

[0002] The increasing size of wind turbines and trend towards offshore turbines puts high demands on serviceability and robustness that the current rolling element bearing systems cannot provide. Also, due to fact that large wind turbines have large dynamic shaft deflections, high loads and low speeds makes it difficult for plain bearings to work and last in the demanded lifetime.

[0003] Conventional wind turbine designs use conventional roller bearings or ball bearings for carrying the drive train, the generator on direct drive turbines and hub with blades require. When such conventional roller bearings or ball bearings have to be replaced, for example at the end of their life cycle, this can be performed only by disassembling the drive train, the generator and/or the hub with blade. These operations require the use of a costly crane capacity. Such costs are especially high for wind turbines located offshore, for which a jackup vessel has to be used.

[0004] One solution to the above problem is the use of fluid bearings instead of roller bearings or ball bearings.

[0005] Another solution to the above problem is to enhance the serviceability of the roller bearings or ball bearings to a higher level. In particular, it is known that the structural integrity of ball or roller bearings is significantly compromised by any axial movement caused by axial thrust forces.

[0006] Therefore, serviceability of the roller bearings or ball bearings may be improved by completely or at least in part by absorbing such axial thrust forces.

[0007] In addition, it is further important in wind turbines to know the value of such axial thrust force. Measurement of the thrust force on the wind turbine rotor provides a significant amount of information about the operational state of the turbine. The information can be used by the control system to reduce loading on main components e.g. tower, blades etc.

[0008] A common way of measuring the rotor thrust is by measuring the strain in the individual blade roots and transforming the measurement to collective rotor thrust. The strain measurement is typical performed using strain gauges or most recently fiber Bragg sensors.

Another method is measuring strain on a main support structure on the turbine e.g. the main shaft.

[0009] The main issue with these approaches is that strain gauges need maintenance during the lifetime and for complex structures like the main shaft of a direct drive turbine the strain distribution is complex making the placement of the strain gauges and strain to thrust transformations a critical problem.

[0010] It is a purpose of the present invention to provide a thrust bearing for a wind turbine, which absorbs the axial thrust forces, acting on ball or roller or fluid bearings, in order to enhance the serviceability of the wind turbine. It is desirable that the thrust bearing itself provides an enhanced level of serviceability by allowing easy maintenance and replacement of the thrust bearing. US 2,778,696 discloses a thrust bearing with bearing pads according to the preamble of claim 1.

[0011] It is a further purpose of the present invention to provide a thrust bearing for a wind turbine, which allows a simple robust and cheap method for measuring the thrust force acting on the thrust bearing.

Summary of the Invention

[0012] This need may be met by the subject matter according to the independent claims. Advantageous embodiments of the present invention are described by the dependent claims.

[0013] According to the invention there is provided a thrust bearing for a wind turbine according to claim 1.

[0014] This design enhances the serviceability of the main bearing (ball or roller or fluid bearing) to a higher level, with respect to known solutions, by allowing replacement without the use of a major crane (or jackup vessel) or even special tools installed in the turbine. When the springs are worn or broken the wind turbine can continue to operate and the replacement can be done during a planned maintenance service. Each bearing pad may be removed, inspected and serviced individually and without moving the shaft to unload thrust bearing.

[0015] Any thrust force acting on the bearing pad results in a small axial movement until the equilibrium is reached between the thrust force and the opposite spring force in the spring element. This means that the thrust force can be measured by the deformation of the spring element.

[0016] Measurement of a deformation for deriving the value of the thrust force is a much simpler and robust than measuring strain.

[0017] In embodiments of the present invention the bearing pad comprises a low friction layer

contacting the thrust surface of the thrust collar.

[0018] Advantageously, this enable the low friction contact between the pad and the thrust collar, thus reducing wear.

[0019] In embodiments of the present invention, the bearing pad is preferably annularly shaped about the longitudinal axis of the thrust bearing.

[0020] Alternatively, the bearing pad may be of another shape or may be not continuously distributed around the longitudinal axis of the thrust bearing.

[0021] In embodiments of the present invention at least a portion of the bearing pad is tapered with respect to the pad seat. In particular, at least a portion of the bearing pad may have a conical section. Advantageously, this prevents locking of the bearing pad with respect to the pad seat.

[0022] According to the invention, the bearing pad comprises a male element and a female element coupled to one another with backlash, the male element being inserted in a pocket of the female element allowing relative tilting between the male element and the female element about an axis orthogonal to the longitudinal axis. Advantageously, this permits correcting misalignment of the bearing pad with respect to the thrust collar and the longitudinal axis of the thrust bearing.

[0023] According to embodiments of the invention, the spring element comprises at least a steel or a polymer spring. Particularly, the spring element comprises at least an helicoidal spring or a Belleville spring or an elastomer layer.

[0024] Any type of spring element may be associated to a system for measuring the deformation for determining the thrust force acting on the thrust bearing.

[0025] Particularly, according to embodiments of the present invention, the elastomer layer is attached to a steel discs.

[0026] More particularly, according to a specific embodiment of the present invention, the spring element includes a stack having a plurality of elastomer layers attached to respective steel discs. Each elastomer layer may be glued to the respective steel discs to improve adhesion.

[0027] The aspects defined above and further aspects of the present invention are apparent from the examples of embodiment to be described hereinafter and are explained with reference to the examples of embodiment. The invention will be described in more detail hereinafter with reference to examples of embodiment but to which the invention is not limited.

Brief Description of the Drawing

[0028]

Figure 1

shows a schematic sectional view of a first embodiment of thrust bearing for a wind turbine according to the present invention.

Figure 2

shows a schematic sectional view of an example of thrust bearing for a wind turbine not part of the present invention.

Figure 3

shows a schematic sectional view of a second example of thrust bearing for a wind turbine not part of the present invention.

Figure 4

shows a schematic sectional view of a third example of thrust bearing for a wind turbine not part of the present invention.

Detailed Description

[0029] The illustrations in the drawings are schematic. It is noted that in different figures, similar or identical elements or features are provided with the same reference signs. In order to avoid unnecessary repetitions elements or features which have already been described with respect to an embodiment or example are not described again further in the description.

[0030] Figure 1 shows an embodiment of a thrust bearing 10 for a wind turbine, according to the present invention. Figures 2 to 3 show examples of thrust bearings not part of the present invention. The thrust bearing 10 comprises a thrust collar 11 rotatable around a longitudinal axis Y of the thrust bearing 10. The thrust collar 11 is a disc attached to a shaft 13 of the wind turbine. The shaft 13 extends longitudinally with respect to the longitudinal axis Y and is subject to rotate around the longitudinal axis Y.

[0031] In the following the terms "longitudinal", "radial" and "circumferential" are referred, when not differently specified, to the longitudinal axis Y of the thrust bearing 10.

[0032] The thrust collar 11 comprises two main circular plane surfaces 12, 14, including a first thrust surface 12 for transferring a thrust force of the thrust bearing 10 to other components of the thrust bearing 10, as better detailed in the following, and a second opposite surface 14. The two main surfaces of the thrust collar 11 are transversally oriented with respect to the longitudinal axis Y. In particular, the two main circular plane surfaces 12, 14 may be radially oriented with respect to the longitudinal axis Y.

[0033] The thrust bearing 10 further comprises:

a support structure 20 fixed with respect to the longitudinal axis Y of the thrust bearing 10, and

a bearing pad 30 contacting the thrust surface 12 of the thrust collar 11 and movable on a pad seat 18 provided on the support structure 20.

[0034] The bearing pad 30 is annularly shaped about the longitudinal axis Y of the thrust bearing 10.

[0035] The thrust bearing 10 further comprises at least a spring element 40 is interposed between the bearing pad 30 and the support structure 20.

[0036] According to other embodiments of the present invention (not shown) the bearing pad 30 has a different shape. In all the embodiments of the present invention the bearing pad 30 provides transferring of a thrust force between the thrust collar 11 and the spring element 40.

[0037] The pad seat 18 has a shape corresponding to the shape of the bearing pad 30 and allowing the bearing pad 30 to translate at least along a direction parallel to the longitudinal axis Y.

[0038] On a side of the spring element 40 opposite to the bearing pad 30, the spring element 40 contacts a thrust plate 45, which is fixed to the support structure 20 by means of a plurality of screws 46.

[0039] The spring element 40 is interposed between the bearing pad 30 and thrust plate 45, in such a way that the thrust force from the thrust collar 11 is transferred to the thrust plate 45 through the spring element 40.

[0040] The thrust force causes the spring element 40 to deform. The thrust bearing 10 includes a system (not shown) for measuring such deformation and consequently calculating the thrust force acting on the thrust collar 11.

[0041] The bearing pad 30, on a face contacting the thrust surface 12 of the thrust collar 11, comprises a low friction layer 35 for reducing friction caused by the contact between the bearing pad 30 and the thrust collar 11 and due to the rotation of the thrust collar 11.

[0042] With reference to the embodiment and examples of **Figures 1 to 3**, the pad seat 18 comprises a first portion 18a and a second portion 18b, longitudinally adjacent to each other. The first portion 18a has a first radial extension R1 while the second portion 18b has a second radial extension R2, greater than the first radial extension R1. The first portion 18a is adjacent to the thrust collar 11 while the second portion 18b is adjacent to the thrust plate 45 and houses the spring element 40.

[0043] Consequently, the bearing pad 30 comprises a first portion 30a coupled with the first portion 18a of the pad seat 18 and a second portion 30b coupled with the second portion 18b of the pad seat 18. The shoulder 18c between the first portion 18a and the second portion 18b of the pad seat 18 prevents the bearing pad 30 from exiting the pad seat 18 in the longitudinal direction towards the thrust collar 11.

[0044] The shoulder 18c also allows preloading the spring element 40 when assembling it in the thrust bearing. If the spring element 40 is a too long it will be preloaded when bolting plate 45 to the support structure 20 with bolts 46.

[0045] With specific reference to the embodiment of **Figure 1**, the bearing pad 30 comprises a male element 31 and a female element 32 coupled to one another with backlash for correcting misalignment of the bearing pad 30 with respect to the thrust collar 11 and to the longitudinal axis Y.

[0046] The male element 31 includes a longitudinal protrusion 31a inserted in a pocket 33 of the female element 32 allowing relative tilting between the male element 31 and the female element 32 about an axis orthogonal to the longitudinal axis Y.

[0047] The bearing pad 30 is oriented in such a way that the male element 31 contacts the thrust surface 12 of the thrust collar 11 and the female element 32 contacts the spring element 40. The second portion 30b of the bearing pad 30 is provided on the female element 32, which is coupled with both the first portion 18a and the second portion 18b of the pad seat 18.

[0048] With specific reference to the example of **Figure 2**, the bearing pad 30 is made of a single solid element, wherein both the first portion 30a and the second portion 30b extends in the longitudinal direction parallel to the respective first portion 18a and second portion 18b of the pad seat 18.

[0049] With specific reference to the example of **Figure 3**, the bearing pad 30 is made of a single solid element, wherein the first portion 30a extends in the longitudinal direction parallel but distanced to the respective first portion 18a of the pad seat 18. The second portion 30b is tapered with respect to the respective second portion 18b of the pad seat 18. In particular, second portion 30b is conical in the section view of **Figure 3**. Such design of the bearing pad 30 prevents locking with respect to the pad seat 18.

[0050] In the embodiment and examples of **Figures 1 to 3** the spring element 40 comprises a plurality of elastomer layers 41 and a plurality of steel discs 42. Elastomer layers 41 and steel discs 42 are interposed to one another to create a stack where each elastomer layers 41 is interposed between two respective steel discs 42 or between a steel disc 42 and the bearing pad 30 or between a steel disc 42 and the thrust plate 45.

[0051] Each elastomer layer 41 is attached by gluing to a respective steel disc 42 to improve

adhesion.

[0052] In the example of **Figure 4**, the bearing pad 30 includes a longitudinal protrusion 36 extending towards the thrust plate 45 but longitudinally distanced from the thrust plate 45. The spring element 40 includes a steel or a polymer spring housed in the pad seat 18 around the longitudinal protrusion 36 and active between a shoulder 37 of the bearing pad 30 and the thrust plate 45.

[0053] The steel or polymer spring 40 in the example of **Figure 4** may be an helicoidal spring or a Belleville spring or another type of spring capable of transferring the thrust force from the thrust collar 11 to the thrust plate 45.

[0054] A polymer spring may be preferred in some embodiments of the present invention considering that such type of spring yields a reaction force even in case of breakage, wear or slow degeneration.

[0055] It should be noted that the term "comprising" does not exclude other elements or steps and the use of articles "a" or "an" does not exclude a plurality. It should also be noted that reference signs in the claims should not be construed as limiting the scope of the claims.

REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

- [US2778696A \[0010\]](#)

Patentkrav

1. Aksialleje (10) til en vindmølle omfattende:

5 en trykring (11), der er drejelig omkring en længdeakse (Y) af aksiallejet (10) og har en trykflade (12), der er orienteret på tværs i forhold til længdeaksen (Y),

en støttestruktur (20), der er fastgjort i forhold til aksiallejets (10) længdeakse (Y),

10 et lejesegment (30), der berører trykfladen (12) af trykringen (11) og er bevægelig på et segmentsæde (18), der er tilvejebragt i støttestrukturen (20), hvor segmentsædet (18) omfatter et første afsnit (18a), der grænser op til trykringen (11), og et andet afsnit (18b), der grænser op til det første afsnit (18a) i længderetningen, hvor det første afsnit (18a) har en første radial udstrækning (R1),

15 og det andet afsnit (18b) har en anden radial udstrækning (R2), der er større end den første radiale udstrækning (R1), hvor den første radiale udstrækning (R1) og den anden radiale udstrækning (R2) er orienteret på tværs i forhold til længdeaksen (Y), hvor lejesegmentet (30) omfatter et første afsnit (30a), der er forbundet med det første afsnit (18a) af segmentsædet (18), et andet afsnit (30b), der er forbundet med det andet afsnit (18b) af segmentsædet (18), og

20 en skulder (18c), der er dannet mellem det første afsnit (18a) og det andet afsnit (18b) af segmentsædet (18), hvorved lejesegmentet (30) forhindres i at komme ud af segmentsædet (18) i længderetningen mod trykringen (11),

en trykplade (45), der er fastgjort til støttestrukturen (20), modsat lejesegmentet (30), hvor mindst et fjederelement (40) er anbragt inde imellem lejesegmentet (30) og trykpladen (45),

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kendetegnet ved

at lejesegmentet (30) omfatter et hanelement (31) og et hunelement (32), der er forbundet med hinanden med frigang, hvor hanelementet (31) er indsat i en udsparring (33) af hunelementet (32), hvorved der muliggøres en relativ kipning

30 mellem hanelementet (31) og hunelementet (32) omkring en akse, der er ortogonal med længdeaksen (Y).

2. Aksialleje (10) ifølge krav 1, hvor lejesegmentet (30) omfatter et lavfriktionslag (35), der berører trykfladen (12) af trykringen (11).

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3. Aksialleje (10) ifølge krav 1 eller 2, hvor lejesegmentet (30) er ringformet omkring aksiallejets (10) længdeakse (Y).
- 5 4. Aksialleje (10) ifølge et af de foregående krav, hvor mindst et afsnit af lejesegmentet (30) er tilspidset i forhold til segmentsædet (18) med henblik på at forhindre låsning af lejesegmentet (30) i forhold til segmentsædet (18).
- 10 5. Aksialleje (10) ifølge krav 4, hvor mindst et afsnit af lejesegmentet (30) har en konisk sektion.
6. Aksialleje (10) ifølge krav 1, hvor hanelementet (31) berører trykfladen (12) af trykringen (11), og hunelementet (32) berører fjederelementet (40).
- 15 7. Aksialleje (10) ifølge et af de foregående krav, hvor fjederelementet (40) i det mindste omfatter en stål- eller en polymerfjeder.
8. Aksialleje (10) ifølge krav 7, hvor fjederelementet (40) omfatter mindst en spiralformet fjeder eller en Belleville-fjeder.
- 20 9. Aksialleje (10) ifølge et af de foregående krav, hvor fjederelementet (40) omfatter mindst et elastomerlag (41).
- 25 10. Aksialleje (10) ifølge krav 9, hvor elastomerlaget (41) er fastgjort til en stålskive (42).
11. Aksialleje (10) ifølge krav 10, hvor fjederelementet (40) omfatter en stabel af en flerhed af elastomerlag (41) fastgjort til respektive stålskiver (42).
- 30 12. Aksialleje (10) ifølge et af de foregående krav, yderligere indbefattende et system til måling af deformationen af fjederelementet (40).
13. Aksialleje (10) ifølge krav 12, yderligere indbefattende et system til måling af deformationen af fjederelementet (40) med henblik på at beregne den aksialkraft, der indvirker på trykringen (11).

FIG 2

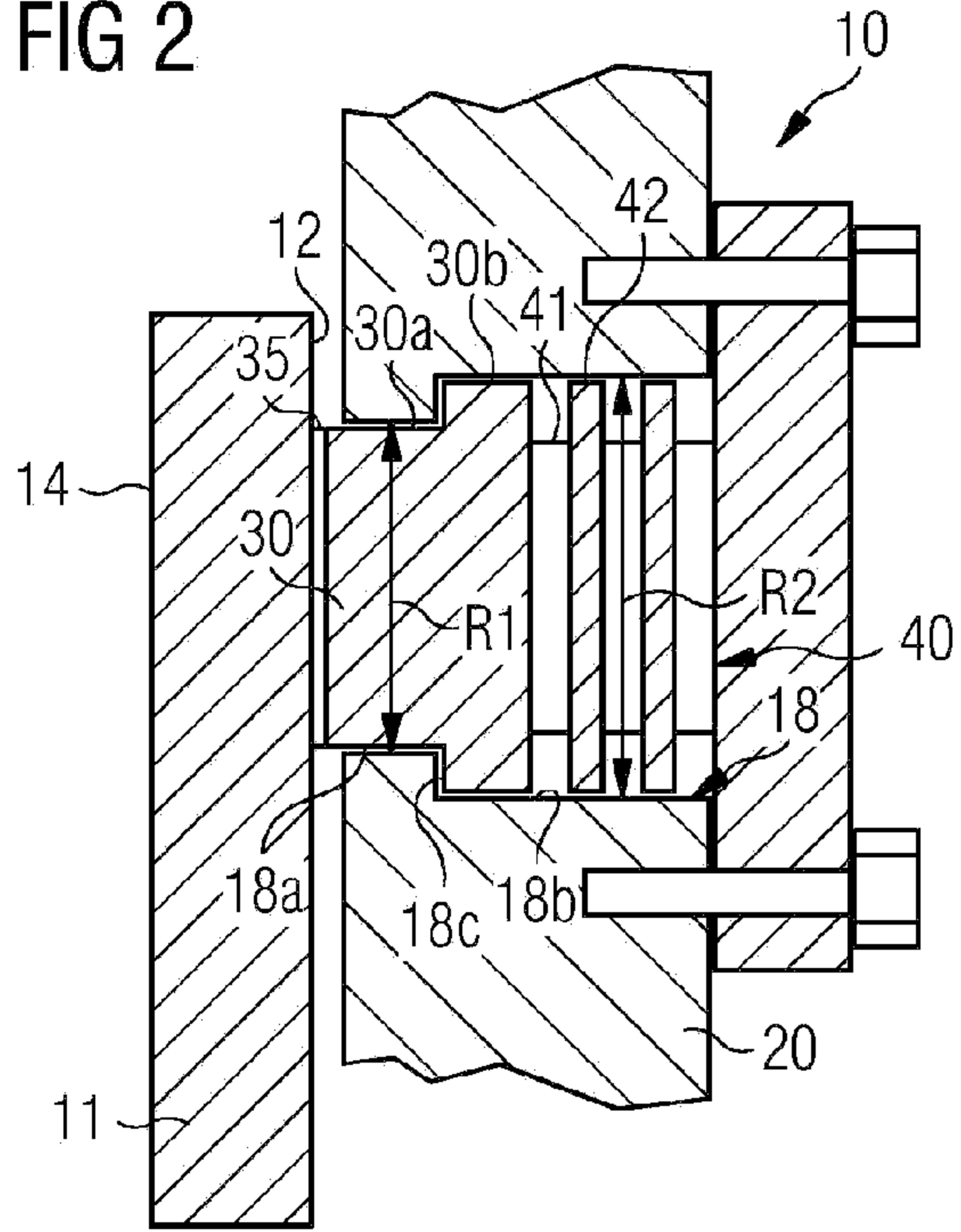


FIG 3

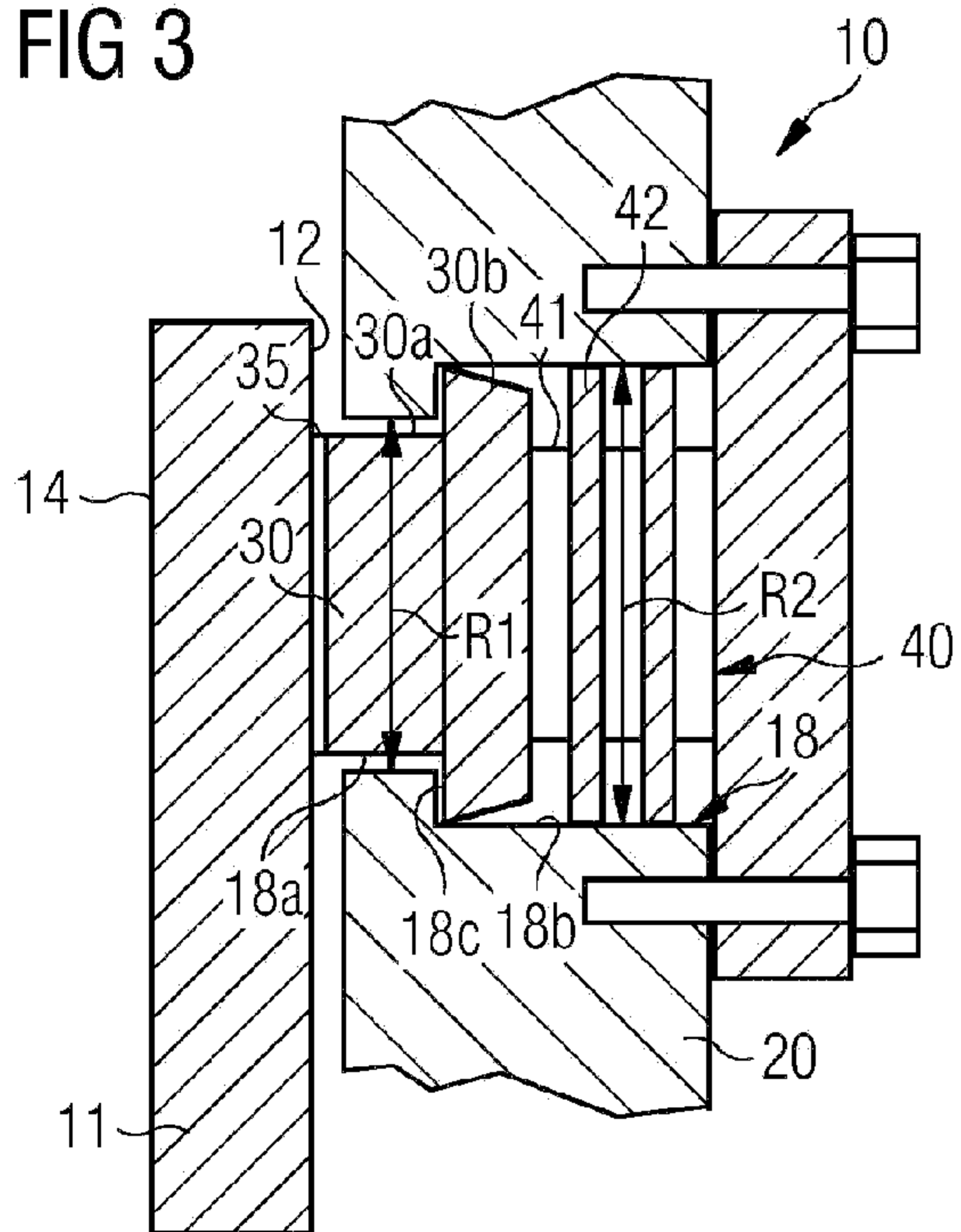


FIG 4

