

(19) **DANMARK**

(10) **DK/EP 3818331 T3**



(12) **Oversættelse af
europæisk patentskrift**

Patent- og
Varemærkestyrelsen

-
- (51) Int.Cl.: **G 01 B 9/02 (2022.01)** **G 01 D 5/353 (2006.01)** **G 02 B 6/26 (2006.01)**
G 02 B 6/34 (2006.01)
- (45) Oversættelsen bekendtgjort den: **2024-07-29**
- (80) Dato for Den Europæiske Patentmyndigheds bekendtgørelse om meddelelse af patentet: **2024-04-24**
- (86) Europæisk ansøgning nr.: **19830499.0**
- (86) Europæisk indleveringsdag: **2019-07-04**
- (87) Den europæiske ansøgnings publiceringsdag: **2021-05-12**
- (86) International ansøgning nr.: **IL2019050742**
- (87) Internationalt publikationsnr.: **WO2020008464**
- (30) Prioritet: **2018-07-04 US 201862693941 P**
- (84) Designerede stater: **AL AT BE BG CH CY CZ DE DK EE ES FI FR GB GR HR HU IE IS IT LI LT LU LV MC MK MT NL NO PL PT RO RS SE SI SK SM TR**
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- (54) Benævnelse: **METODE OG SYSTEM TIL BESTEMMELSE AF GITTERFORSTYRRELSER VED HJÆLP AF MODULERET LYS**
- (56) Fremdragne publikationer:
WO-A1-2012/033718
KR-B1- 100 496 554
US-A- 5 426 297
US-A- 5 680 489
US-A- 5 748 312
US-A1- 2002 041 722
US-A1- 2002 063 866
US-A1- 2008 204 747
US-A1- 2018 003 551
US-B1- 6 285 806
US-B2- 9 025 157

DESCRIPTION

Description

FIELD AND BACKGROUND OF THE INVENTION

[0001] The present invention, in some embodiments thereof, relates to a sensor system and, more particularly, but not exclusively, to a method and a system for sensing by reflection of modulated light, e.g., by a fiber Bragg grating (FBG).

[0002] FBGs are a well-known component used in the fields of optical fiber sensing and communications, and typically comprise a repeating pattern written into a photosensitive optical fiber. When illuminated, a Bragg grating reflects a component of light at wavelengths within a range whose central wavelength and bandwidth depend on the properties of the grating (e.g., pitch, refractive index, length of the grating). The central wavelength and bandwidth of this range are referred to as the Bragg wavelength and FBG bandwidth, respectively. A perturbation of the grating, for example, by temperature, pressure, strain, vibration or the like, results in a shift in the Bragg wavelength (referred to as "Bragg shift"), which can be detected in the reflected spectrum. This shift can then be compared with the unperturbed Bragg wavelength to determine the extent of the perturbation.

[0003] Thus, an FBG can serve as a sensor. FBG sensors are particularly useful as embedded sensors for smart structures where the sensors can be used for real time evaluation of temperature, pressure, strain, vibration and the like. Since many gratings can be written into a length of fiber and addressed using multiplexing techniques, FBG sensors can provide quasi-distributed sensing capabilities.

[0004] Conventionally, the shift in Bragg wavelength is measured with the aid of spectral analysis techniques such as interferometers, tunable optical filters, tunable lasers or diffraction elements [Chen et al., "Review of fiber Bragg grating sensor technology", Front. Optoelectron. China 4 204 (2011)].

[0005] In the field of large distance optical communication, it is known to measure dispersion in an optical fiber by linearly dispersing ultra-short pulses in the fiber and mapping their spectrum to the time domain. This allows mapping the dispersion by measuring the delay between two spikes in the dispersed pulse's temporal profile [Tong et al., "Fibre dispersion or pulse spectrum measurement using a sampling oscilloscope", Electronics Lett. 33(11) 983-985 (1997)].

[0006] U.S. Published Application No. 20020063866 discloses interrogation of fiber optic

sensors that non-intrusively sense fluid flow within a pipe. A series of discrete light pulses are directed at sensors positioned between pairs of low reflectivity fiber Bragg gratings. Successive light pulses are split so that ones of the pulses are delayed relative to the other ones of pulses. The light pulses are combined and the phase shifts between the pulses are determined.

[0007] U.S. Patent No. 5,748,312 discloses sensing strain between fiber Bragg grating sensors inscribed in an optical fiber. The strain is detected between the two fiber Bragg grating sensors based on the optical propagation times of light reflected by the individual fiber sensors, by calculating the differences between the phase shifts induced by successive sensors.

[0008] U.S. Patent No. 6,285,806 discloses a fiber optic sensor with multiple segments for detecting a physical condition. The segments are separated by Bragg gratings. Light from a light source is input into the input end of the array. Light reflected by each of the reflectors has a phase shift representing the effects of the physical condition on all of the segments from the input end to that reflector. The return light is demultiplexed by modulating the light input with a pseudo-random bit sequence and correlating the output with a time-shifted version of the pseudo-random bit sequence.

SUMMARY OF THE INVENTION

[0009] The present invention provides method of determining perturbation of a grating formed in an optical fiber according to claim 1, a system for determining perturbation of a grating formed in an optical fiber according to claim 12.

[0010] According to an aspect of some embodiments of the present invention there is provided a method of determining perturbation of a grating formed in an optical fiber. The method comprises: modulating and transmitting a light beam through the optical fiber, measuring at least one phase shift in a modulation of light reflected off the grating, and determining the perturbation of the grating based on the phase shift(s).

[0011] According to some embodiments of the invention the modulation is applied before the transmitting. According to some embodiments of the invention the modulation is applied after the light beam is reflected off the grating. According to some embodiments of the invention the modulation is applied before the transmitting as well as after the light beam is reflected off the grating.

[0012] According to some embodiments of the invention the optical fiber is formed with a plurality of gratings, wherein two or more of the gratings are characterized by different Bragg wavelengths.

[0013] According to some embodiments of the invention the invention the method comprises de-multiplexing the reflected light beam into two or more channels, respectively corresponding to the different Bragg wavelengths, prior to the measurement of the phase shift(s).

[0014] According to some embodiments of the invention the method comprises scanning a frequency of the modulation over a plurality of modulation frequencies, wherein the method comprises measuring a modulation phase shift and modulation magnitude of light reflected off the gratings for each modulation frequency, and determining an individual optical wavelength or optical frequency shift for each of the two or more gratings, based on the measured modulation phase shifts and measured modulation magnitudes.

[0015] According to the invention the method comprises dispersing the reflected light beam prior to the measurement of the phase shift(s).

[0016] According to some embodiments of the invention dispersing is performed by a chirped grating formed in an optical fiber.

[0017] According to some embodiments of the invention dispersing is performed by an optical fiber spool.

[0018] According to some embodiments of the invention the measurement of the phase shift is characterized by a predetermined phase resolution, and the dispersing is characterized by a predetermined dispersion parameter describing pulse broadening per unit wavelength, wherein a frequency of the modulation is at least a ratio between the phase resolution and a multiplication of the dispersion parameter by a predetermined spectral resolution threshold.

[0019] According to some embodiments of the invention the predetermined spectral resolution threshold is less than 0.1 picometer and the measurement of the phase shift(s) is at a sampling rate of at least 1 kHz.

[0020] According to some embodiments of the invention the dispersion is characterized by a dispersion coefficient, wherein the method comprises varying a value of the coefficient over a plurality of dispersion coefficient values, measuring a modulation phase shift and modulation magnitude of light reflected off the grating for each value of the dispersion coefficient, and determining an individual optical wavelength or optical frequency shift for each of the two or more gratings, based on the measured modulation phase shifts and measured modulation magnitudes.

[0021] According to some embodiments of the invention the modulation comprises radiofrequency modulation. According to some embodiments of the invention the modulation comprises sinusoidal modulation.

[0022] According to some embodiments of the invention the method comprises amplifying the light beam prior to the transmission.

[0023] According to some embodiments of the invention the determination of the perturbation of the grating is not on an optical power of the reflected light beam.

[0024] According to some embodiments of the invention the method is executed without determining an optical power of the reflected light beam.

[0025] According to some embodiments of the invention the determination of the perturbation of the grating comprises expressing the perturbation as a shift in a Bragg wavelength characterizing the grating.

[0026] According to some embodiments of the invention the method comprises using the shift in the Bragg wavelength for calculating at least one physical quantity effecting the perturbation of the grating.

[0027] According to some embodiments of the invention the determination of the perturbation of the grating comprises expressing the perturbation as at least one physical quantity effecting the perturbation of the grating.

[0028] According to some embodiments of the invention the physical quantity(ies) is selected from the group consisting of ambient temperature, pressure applied to the fiber, strain of the fiber, and accelerative motion of the fiber.

[0029] According to an aspect of some embodiments of the present invention there is provided a system for determining perturbation of a grating formed in an optical fiber. The system comprises: an optical modulation system for modulating a light beam; an optical coupler for coupling the light beam into the optical fiber and receiving light reflected off the grating; and an optical and electrical analysis system configured for measuring at least one phase shift in a modulation of light reflected off the grating, and determining the perturbation of the grating based on the phase shift(s).

[0030] According to an aspect of some embodiments of the present invention there is provided a sensor system. The sensor system comprises: an optical modulation system for modulating a light beam; an optical coupler for coupling the light beam into the optical fiber and receiving light reflected off the grating; and an optical and electrical analysis system configured for measuring at least one phase shift in a modulation of light reflected off the grating, and determining at least one physical quantity effecting a perturbation of the grating.

[0031] According to some embodiments of the invention the physical quantity(ies) is selected from the group consisting of ambient temperature, pressure applied to the fiber, strain of the fiber, and accelerative motion of the fiber.

[0032] According to some embodiments of the invention the optical modulation system is configured to modulate the light beam before the transmission. According to some embodiments of the invention the optical modulation system is configured to modulate the light beam after the light beam is reflected off the grating. According to some embodiments of the invention the optical modulation system is configured to modulate the light beam before the

transmitting as well as after the light beam is reflected off the grating.

[0033] According to some embodiments of the invention the optical fiber is formed with a plurality of gratings, wherein two or more of the gratings are characterized by different Bragg wavelengths.

[0034] According to some embodiments of the invention the analysis system comprises an optical de-multiplexing system for de-multiplexing the reflected light beam into two or more channels, respectively corresponding to the different Bragg wavelengths, prior to the measurement of the phase shift(s).

[0035] According to some embodiments of the invention the analysis system comprises a plurality of light detectors, one for each of the channels.

[0036] According to some embodiments of the invention the optical modulation system is configured for scanning a frequency of the modulation over a plurality of modulation frequencies, wherein the optical and electrical analysis system is configured for measuring a modulation phase shift and modulation magnitude of light reflected off the grating for each modulation frequency, and for determining an individual optical wavelength or optical frequency shift for each of the two or more gratings, based on the measured modulation phase shifts and measured modulation magnitudes.

[0037] According to some embodiments of the invention the analysis system comprises a single light detector.

[0038] According to some embodiments of the invention the analysis system comprises a dispersive optical device configured for dispersing the reflected light beam prior to the measurement of the phase shift(s).

[0039] According to some embodiments of the invention the dispersive optical device comprises a chirped grating formed in an optical fiber. According to some embodiments of the invention the dispersive optical device comprises an optical fiber spool.

[0040] According to some embodiments of the invention the analysis system comprises a signal processing system configured for measuring the phase shift(s) at a predetermined phase resolution, wherein the dispersive optical device is configured for effecting dispersing according to a predetermined dispersion parameter describing pulse broadening per unit wavelength, wherein the optical modulation system is configured for modulating the light beam at a frequency which is at least a ratio between the phase resolution and a multiplication of the dispersion parameter by a predetermined spectral resolution threshold.

[0041] According to some embodiments of the invention the predetermined spectral resolution threshold is less than 10 picometers.

[0042] According to some embodiments of the invention the predetermined spectral resolution threshold is less than 0.1 picometer, wherein the signal processing system is configured for measuring the phase shift(s) at a sampling rate of at least 1 kHz.

[0043] According to some embodiments of the invention the dispersive optical device is controllable, wherein the system comprises a dispersion controller for controlling the dispersive optical device so as to vary a value of a dispersion coefficient characterizing the dispersive optical device, wherein the optical and electrical analysis system is configured for measuring a modulation phase shift and modulation magnitude of light reflected off the grating for different values of the dispersion coefficient, and determining an individual optical wavelength or optical frequency shift for each of the two or more gratings, based on the measured modulation phase shifts and measured modulation magnitudes.

[0044] According to some embodiments of the invention the method comprises an optical amplifier for amplifying the light beam prior to the transmission.

[0045] According to an aspect of some embodiments of the present invention there is provided a method of determining perturbation of a plurality of gratings formed in an optical fiber. The method comprises: modulating and transmitting a light beam through the optical fiber, wherein the modulation comprises scanning a frequency of the modulation over a plurality of modulation frequencies; measuring a modulation phase shift and modulation magnitude of light reflected off the grating for each modulation frequency; and determining perturbation of two or more of the gratings based on the measured modulation phase shifts and measured modulation magnitudes.

[0046] According to some embodiments of the invention the method comprises dispersing the light reflected off the grating using a controllable dispersive optical device, wherein the dispersing comprises controlling the dispersive optical device so as to vary a value of a dispersion coefficient characterizing the dispersive optical device, wherein the method comprises measuring the modulation phase shift and modulation magnitude also for different values of the dispersion coefficient.

[0047] According to an aspect of some embodiments of the present invention there is provided a method of determining perturbation of a plurality of gratings formed in an optical fiber. The method comprises: modulating and transmitting a light beam through the optical fiber; dispersing light reflected off the grating using a controllable dispersive optical device, wherein the dispersing comprises controlling the dispersive optical device so as to vary a value of a dispersion coefficient characterizing the dispersive optical device; measuring a modulation phase shift and modulation magnitude of light reflected off the grating for different values of the dispersion coefficient; and determining perturbation of two or more of the gratings based on the measured modulation phase shifts and measured modulation magnitudes.

[0048] According to some embodiments of the invention the modulation is executed before the transmitting.

[0049] According to some embodiments of the invention the modulation is executed after the light beam is reflected off the grating.

[0050] According to some embodiments of the invention the modulation is executed before the transmitting as well as after the light beam is reflected off the grating.

[0051] According to some embodiments of the invention the determining the perturbation comprises calculating an optical wavelength or optical frequency shift caused by a respective grating.

[0052] Unless otherwise defined, all technical and/or scientific terms used herein have the same meaning as commonly understood by one of ordinary skill in the art to which the invention pertains. Although methods and materials similar or equivalent to those described herein can be used in the practice or testing of embodiments of the invention, exemplary methods and/or materials are described below. In case of conflict, the patent specification, including definitions, will control. In addition, the materials, methods, and examples are illustrative only and are not intended to be necessarily limiting.

[0053] Implementation of the method and/or system of embodiments of the invention can involve performing or completing selected tasks manually, automatically, or a combination thereof. Moreover, according to actual instrumentation and equipment of embodiments of the method and/or system of the invention, several selected tasks could be implemented by hardware, by software or by firmware or by a combination thereof using an operating system.

[0054] For example, hardware for performing selected tasks according to embodiments of the invention could be implemented as a chip or a circuit. As software, selected tasks according to embodiments of the invention could be implemented as a plurality of software instructions being executed by a computer using any suitable operating system. In an exemplary embodiment of the invention, one or more tasks according to exemplary embodiments of method and/or system as described herein are performed by a data processor, such as a computing platform for executing a plurality of instructions. Optionally, the data processor includes a volatile memory for storing instructions and/or data and/or a non-volatile storage, for example, a magnetic hard-disk and/or removable media, for storing instructions and/or data. Optionally, a network connection is provided as well. A display and/or a user input device such as a keyboard or mouse are optionally provided as well.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

[0055] Some embodiments of the invention are herein described, by way of example only, with reference to the accompanying drawings. With specific reference now to the drawings in detail, it is stressed that the particulars shown are by way of example and for purposes of illustrative discussion of embodiments of the invention. In this regard, the description taken with the

drawings makes apparent to those skilled in the art how embodiments of the invention may be practiced.

[0056] In the drawings:

FIG. 1 is flowchart diagram of a method suitable for determining perturbation of a grating formed in an optical fiber, according to some embodiments of the present invention;

FIG. 2 is a schematic illustration of a system suitable for determining perturbation of a grating formed in an optical fiber, according to some embodiments of the present invention;

FIG. 3 is a schematic illustration of an experimental setup used in experiments performed according to some embodiments of the present invention;

FIG. 4 shows monitored Bragg wavelength shift due to periodic strain on a FBG, obtained in experiments performed according to some embodiments of the present invention;

FIG. 5 shows Fourier analysis of ultrasonic waves in water for different values of vibration power, obtained in experiments performed according to some embodiments of the present invention;

FIG. 6 shows Fourier analysis of a signal returning from an FBG wound around a piezoelectric fiber stretcher vibrating at about 200 kHz;

FIG. 7 shows resolution as a function of speed, obtained in experiments performed according to some embodiments of the present invention;

FIG. 8 is a flowchart diagram of a method suitable for amplifying a phase shift, according to some embodiments of the present invention; and

FIG. 9 is a schematic block diagram illustration of a system for amplifying a phase shift, according to some embodiments of the present invention.

DESCRIPTION OF SPECIFIC EMBODIMENTS OF THE INVENTION

[0057] The present invention, in some embodiments thereof, relates to a sensor system and, more particularly, but not exclusively, to a method and a system for sensing by reflection of modulated light, *e.g.*, by a fiber Bragg grating (FBG).

[0058] Before explaining at least one embodiment of the invention in detail, it is to be understood that the invention is not necessarily limited in its application to the details of construction and the arrangement of the components and/or methods set forth in the following description and/or illustrated in the drawings and/or the Examples. The invention is capable of other embodiments or of being practiced or carried out in various ways.

[0059] In conventional FBG sensors the Bragg shift caused by a perturbation in an FBG is typically measured by spectral analysis techniques such as spectrometers, interferometers, tunable optical filters, tunable lasers or diffraction elements. The inventors realized that these techniques are complicated, and require expensive equipment for achieving adequate accuracy. The inventors also realized that techniques that rely on the need to employ laser frequency sweep limits the measurement speed, especially if the sweep is done mechanically. Other systems measure the time response of a pulse passing through a dispersive element. The Inventors found that this type of technique also requires expensive tools such as modulators capable of modulating ultrashort pulses and fast electronic detection devices. The Inventors also found that this technique has additional disadvantages such as the need to resolve the temporal response in the frequency domain, which limits the spectral resolution.

[0060] In a search for a technique that optionally and preferably overcomes the above problems, and/or for a technique that is optionally and preferably more accurate and/or executable at higher speeds, the Inventors devised a method and a system that acquire interrogator data from the grating(s) directly from the modulation of light reflected off the grating(s). The inventors found that such direct acquisition benefits from many advantages, and at the same time is overcomes one or more of the aforementioned drawbacks. Firstly, the technique enjoys high noise rejection and high-speed measurements, since it does not require a spectral sweep. Secondly, the technique can be executed using relatively low cost equipment compared to the equipment required for fast time-domain measurements. Thirdly, unlike conventional techniques for resolving the temporal response in the frequency domain, for which the resolution is bounded by the fading effect, the technique according to some embodiments of the present invention selects the working frequency in accordance with the periodicity in the fading effect, thereby improving the resolution.

[0061] Referring now to the drawings, FIG. 1 is flowchart diagram of a method suitable for determining perturbation of a grating formed in an optical fiber, and FIG. 2 is a schematic illustration of a system **30** suitable for determining perturbation of a grating formed in an optical fiber, according to some embodiments of the present invention. In a preferred embodiment, system **30** can be used for executing at least a few of the operations of the method.

[0062] It is to be understood that, unless otherwise defined, the operations described hereinbelow can be executed either contemporaneously or sequentially in many combinations or orders of execution. Specifically, the ordering of the flowchart diagrams is not to be considered as limiting. For example, two or more operations, appearing in the following description or in the flowchart diagrams in a particular order, can be executed in a different order (e.g., a reverse order) or substantially contemporaneously. Additionally, several operations described below are optional and may not be executed.

[0063] The method begins at **10** and optionally and preferably continues to **11** at which a light beam is generated, and to **12** at which the light beam is modulated to provide a modulated light beam **34**. The light can be infrared light, visible light or ultraviolet light as desired.

Preferably, the light is infrared light.

[0064] The generation **11** and modulation **12** can be executed by an optical modulation system **40**. The modulation can be either a direct modulation or an external modulation, and of any type known in the art. When direct modulation is employed, a light source **36** receives a modulation signal from a controller **42** and generates modulated light beam **34**. When external modulation is employed, an unmodulated light beam **32** is generated by light source **36** and is modulated by an optical modulator **38** that receives the modulation signal from controller **42**. Controller **42** can include a dedicated circuit for generating the modulation signal.

[0065] The modulation can be at any frequency range, such as, but not limited to, radiofrequency. When radiofrequency modulation is employed the modulation frequency is optionally and preferably from about 1 kHz to about 40 GHz. In various exemplary embodiments of the invention the modulation is a sinusoidal modulation, but modulation waveforms other sinusoidal are also contemplated in some embodiments. Also contemplated are embodiments in which a multi-frequency modulation is employed, for example, by a sum of sinusoidal signals, each at a different frequency. The modulation can be executed to modulate any of the amplitude, frequency and phase of the light beam, including modulations of two or more of the amplitude, frequency and phase. In a preferred embodiment, at least amplitude modulation is employed, and in a more preferred embodiment, only amplitude modulation is employed wherein the frequency and phase are not modulated.

[0066] The present embodiments also contemplate modulation scanning, wherein a frequency of the modulation is scanned over a plurality of modulation frequencies. The advantage of these embodiments is explained below. It is to be understood, however, that it is not necessary to employ modulation scanning, and that the method according to some embodiments of the present invention can be practiced also when the modulation is without frequency scanning.

[0067] In some optional embodiments of the present invention the method proceeds to **13** at which light beam **34** is amplified. This can optionally and preferably be achieved by an optical amplifier **50**, such as, but not limited to, an erbium-doped fiber amplifier (EDFA), an ytterbium-doped fiber amplifier (YDFA), a Raman amplifier, a hybrid Raman/erbium-doped amplifier, a hybrid Raman/ytterbium-doped amplifier, an erbium-ytterbium co-doped fiber amplifier, a neodymium-doped fiber amplifier, a thulium-doped fiber amplifier, and the like.

[0068] The method can proceed to **14** at which the modulated light beam **34** is transmitted through an optical fiber **44** having one or more gratings **46** formed therein, and to **15** at which light reflected off the grating(s) **46** is coupled out of optical fiber **44**. The grating(s) can be fabricated within the entire or part of the core's cross-section or at the core-cladding interface of fiber **44**, or in other fiber sections as known in the art. The optical fiber **44** is optionally and preferably an optical fiber with a FBG sensor or an array of FBG sensors. The grating **46** is constituted to selectively reflect a component of the light that has wavelengths within a particular Bragg bandwidth centered at a particular Bragg wavelength, and to allow other components to continue to propagate in the fiber **44**. When optical fiber **44** has a plurality of

gratings, each of at least two of the gratings, more preferably each of the gratings formed in fiber **44**, is constituted to selectively reflect a different component of the light. Thus, each grating **46** of fiber **44** is characterized by a Bragg wavelength (and a corresponding Bragg bandwidth), wherein at least two of the gratings are characterized by a different Bragg wavelength. Shown in FIG. 2, is a fiber with N gratings, characterized by a set of N different respective Bragg wavelengths, denoted $\lambda_1, \lambda_2, \dots, \lambda_N$. The gratings need not to be ordered according to their λ values.

[0069] In various exemplary embodiments of the invention optical fiber **44** is deployed on or embedded within a structure such as, but not limited to, an airplane wing, a fence, a wind turbine blade, a building, a bridge, a culvert, a tunnel lining, a pipeline, a river, a flood control reservoir, a well, and the like.

[0070] The in-coupling and out-coupling of light into- and out of- fiber **44** is optionally and preferably via one or more optical couplers **48** which provide optical coupling between system **40** and fiber **44**, and optionally and preferably also between fiber **44** and an optical and electrical analysis system generally shown at **52**. In the schematic illustration shown in FIG. 2, which is not to be considered as limiting, optical coupler **48** is shown as an optical circulator having three or more input/output (I/O) ports (three shown in the present example), wherein at least one port is in optical communication with system **40** and at least one port is in optical communication with fiber **44**. In FIG. 2, light beam **34** enters circulator **48** through its first port **(1)** and exits through its second port **(2)** into fiber **44**. Light reflected off the grating(s) **46** propagates backwards in fiber **44**, enters circulator **48** through its second port **(2)** and exits through its third port **(3)**. From the third port the reflect light optionally and preferably enters system **52** for performing processing and analysis as further detailed hereinbelow.

[0071] In some optional embodiments of the present invention modulation **12** is executed after the light exits fiber **44**. In these embodiments, it is not necessary to carry out modulation **12** before transmitting the light to the fiber. Yet, embodiments in which modulation **12** is applied two or more times (e.g., before the light is coupled into the fiber, and after the light exits the fiber) are also contemplated.

[0072] In some embodiments of the present invention the method proceeds to **16** at which the reflected light beam is dispersed. Operation **16** is executed so as to increase the group velocity dispersion (GVD) of the reflected light beam. Preferably, following operation **16**, the magnitude of the GVD of the light beam is larger (e.g., 2 times or 4 times or 8 times or 10 times larger) than the magnitude of the combined effective GVD of all the other components in system **52**. Operation **16** is optionally and preferably performed by a dispersive optical device **54**, which in some embodiments of the present invention is a component of system **52**. Alternatively, or additionally, operation **16** can be performed also by the grating(s) of the fiber itself.

[0073] Representative examples of dispersive optical devices suitable to be used as device **54** include, without limitation, a chirped grating formed in an optical fiber (e.g., a chirped FBG, such as, but not limited to, the chirped FBG marketed by Teraxion, Canada), a dispersion

compensating fiber (DCF), and an optical fiber spool.

[0074] It is expected that during the life of a patent maturing from this application many relevant optical devices that disperse light will be developed and the scope of the term dispersive optical device is intended to include all such new technologies *a priori*.

[0075] The dispersion provided by dispersive optical device **54** is typically characterized by a dispersion coefficient \check{D} . The \check{D} parameter describes the amount of broadening of an optical pulse propagating in the dispersive optical device per unit of wavelength, typically in units of ps/nm. Suitable for the present embodiments are dispersive optical devices capable of effecting dispersion characterized by a positive or negative dispersion parameter \check{D} having an absolute value of at least 100 ps/nm or at least 300 ps/nm or at least 1000 ps/nm or at least 1500 ps/nm or at least 2000 ps/nm or at least 2500 ps/nm.

[0076] In some embodiments of the present invention dispersive optical device **54** is controllable, wherein the dispersion coefficient \check{D} can be varied, for example, by means of a dispersion controller **55**. Variation of the dispersion coefficient can be achieved, for example, by effecting a strain on device **54** (e.g., by applying stress or tension thereto) and/or by changing its temperature. Dispersion controller **55** is preferably a structure configured for applying stress and/or tension and/or temperature to device **45**. The present embodiments also contemplate dispersion scanning, wherein the dispersion coefficient \check{D} is scanned over a plurality of the dispersion coefficients. The advantage of these embodiments is explained below. It is to be understood, however, that it is not necessary to employ dispersion scanning, and that the method according to some embodiments of the present invention can be practiced also when dispersive optical device **54** is characterized by a fixed value of the dispersion coefficient.

[0077] When fiber **44** comprises two or more gratings **46** the method optionally and preferably proceeds to **17** at which a de-multiplexing is applied to the reflected light beam. The de-multiplexing **17** is preferably executed to provide two or more spatially separated optical channels, each corresponding to a Bragg wavelength that characterizes a different grating of fiber **44**. The de-multiplexing **17** can be executed using an optical de-multiplexing system **56**, which can also be a component of system **52**. De-multiplexing system **56** can be of any type, including, without limitation, an arrayed waveguide grating, a photonic crystal fiber and the like. Shown in FIG. 2 is an optical de-multiplexing system which produces N channels each corresponding to one Bragg wavelength of the aforementioned set $\lambda_1, \lambda_2, \dots, \lambda_N$.

[0078] It is to be understood that it is not necessary to de-multiplex the reflect light even when fiber **44** comprises a plurality of gratings **46**. For example, when modulation scanning is employed, the multiplicity of modulation frequencies can provide sufficient information regarding the contribution of more than one grating, as is further explained below. Another example is when dispersion scanning is employed, in which case the multiplicity of values of the dispersion coefficients can provide sufficient information regarding the contribution of more than one grating, as is further explained below.

[0079] At **18** the light is preferably converted into electrical signals, for example, by using an optical detector (e.g., a selector having a single optical sensor), or an array of optical detectors **58** (one for each optical channel, in embodiments in which the light is de-multiplexed into channel), and at **19** at least phase shifts in a modulation of the reflected light off the grating(s) **46** are measured, for example, by a signal processing system **60**, as illustrated in FIG. 2. In some embodiments of the present invention operating **19** also includes measuring the magnitude of the signal.

[0080] The present Inventors found that the modulation phase shift is indicative of a perturbation in the grating, and can therefore improve sensing since the phase shift is determined directly from the modulation of the light, without the need to determine a time-domain response of the signal.

[0081] The modulation phase shifts can be determined by processing system **60** using any technique known in the art. A representative example of a suitable technique for determining a phase shift is provided in the Example section that follows (see Example 2). Alternatively, or additionally, signal processing system **60** can comprise a network analyzer and/or a spectrum analyzer. When processing system **60** comprises a network analyzer, it can serve both for processing the electrical signals provided by detector array **58** to determine the phase shifts, and for generating the modulation signal that is received by light source **36** or modulator **38**. Thus, the same network analyzer can serve both as controller **42** and as signal processing system **60**.

[0082] In embodiments in which the fiber has a plurality of gratings and modulation scanning is employed, the individual phase, wavelength or frequency shift caused by each of gratings can be determined from the information provided by the multiplicity of modulation frequencies. In these embodiments, the method preferably measures, for each modulation frequency, the global phase shift and global magnitude of the reflected light. This provides a plurality of global phase shifts and a plurality of global magnitudes. Each global phase shift and global magnitude describes a wave formed of a plurality of partial waves, respectively corresponding to the plurality of gratings in the fiber. Thus, each global phase shift and global magnitude carries information regarding the individual phase, wavelength or frequency shifts caused by the gratings in the fiber. According to some embodiments of the present invention the number of different modulation frequencies that are employed is sufficient to extract the individual phase, wavelength or frequency shifts, and optionally also the individual magnitudes, from the global phase shifts and global magnitude. This can be done, for example, by solving a set of equations, where the unknowns are the individual phase, wavelength or frequency shifts, and the coefficients and known terms are the global phase shifts and global magnitudes. It was found by the Inventors, that for a fiber having N gratings, it is sufficient to employ $N/2$ different modulation frequencies. Representative example of a set of equations and a technique for automatically solve these equations is provided in the Examples section that follows (see Example. 3).

[0083] In embodiments in which the fiber has a plurality of gratings and dispersion scanning is employed, the individual phase, wavelength or frequency shift caused by each of gratings can be determined from the information provided by the multiplicity of dispersion coefficient values. In these embodiments, the method preferably measures, for each dispersion coefficient value, the global phase shift and global magnitude of the reflected light. This provides a plurality of global phase shifts and a plurality of global magnitudes, as further detailed hereinabove. According to some embodiments of the present invention the number of different dispersion coefficients that are employed is sufficient to extract the individual phase, wavelength or frequency shifts, and optionally also the individual magnitudes, from the global phase shifts and global magnitude. This can be done, for example, by solving a set of equations, as further detailed hereinabove, and exemplified below.

[0084] In some embodiments of the present invention, system **60** also receives a signal from a reference light detector **62**. Reference light detector **62** can receive a light beam that is reflected off the grating(s) but is not subjected to further dispersion and/or de-multiplexing. For example, a beam splitter **57** can be placed on the optical path of the light beam exiting fiber **44** such that one beam continues as further detailed hereinabove and another beam, serving as a reference beam, is directed to detector **62**.

[0085] From **19** the method can proceed to **20** at which the perturbation of the grating is determined based on the phase shifts. For example, suppose that system **40** provides a light beam that is sinusoidally modulated according to $\cos(\Omega t)$, where Ω is the angular modulation frequency (e.g., within a radiofrequency range). Dispersive optical device **54** disperses the light so that each component arrives separately into optical de-multiplexing system **56**. Suppose further that when fiber **44** is unperturbed, the light component reflected from the i th grating exits dispersive optical device **54** acquiring an overall modulation phase ϕ_i , so that it is modulated according $\cos(\Omega t + \phi_i)$. System **56** directs each component into a separate channel, wherein the light component reflected from the i th grating is directed to the i th optical channel. The respective optical detector converts the i th optical channel into an electrical signal that is in turn processed by signal processing system **60** to determine its modulation parameters.

[0086] Suppose now that a perturbation occurs at the i th grating so that it selectively reflects light component at wavelength $\lambda_i + \Delta\lambda_i$, where λ_i is the wavelength (within the optical range) of the light component that would have been reflected from the i th grating had this grating been unperturbed. Following the dispersion by dispersive optical device **54**, the i th component acquires a modulation phase $\phi_i + \Delta\phi_i$ so that it is modulated according $\cos(\Omega t + \phi_i + \Delta\phi_i)$. Thus, the optical phase shift $\Delta\phi_i$ in the modulation is a proxy to the optical wavelength shift $\Delta\lambda_i$ (or, equivalently, an optical frequency shift $\Delta f_i = c\Delta\lambda_i / \lambda_i^2$, where c is the speed of light).

[0087] When de-multiplexing system **56** is employed, de-multiplexing system **56** directs this component into the i th optical channel, the respective optical detector converts this component into an electrical signal received by signal processing system **60**. When signal processing system **60** determined that the phase of the signal generated by the i th detector is shifted, the

method determines that perturbation occurred at the i th grating.

[0088] Alternatively, signal processing system **60** can determine the value of the optical wavelength shift $\Delta\lambda_i$ without de-multiplexing and without measuring its modulation phase shift proxy, for example, by employing modulation scanning as described herein. When signal processing system **60** determined that $\Delta\lambda_i$ is non-zero the method determines that perturbation occurred at the i th grating.

[0089] Thus, the method and system optionally and preferably successfully determine the perturbation based on the phase shift, without relying on the optical power of the reflected light beam. This is unlike conventional techniques that require complicated optical power processing operations in order to determine the perturbation.

[0090] The perturbation as determined at **20** can be expressed in more than one way. In some embodiments, the perturbation is expressed as a shift in the respective Bragg wavelength ($\Delta\lambda_i$, in the above example). The Bragg shift can be determined, for example, using an empirically generated lookup table that relates between the modulation phase shift $\Delta\phi_i$ and the Bragg shift $\Delta\lambda_i$. From the expressed value of the Bragg shift the method can determine a value of a physical quantity effecting the perturbation of the grating, for example, as known in the art of FBG sensors.

[0091] Also contemplated are embodiments in which the perturbation is expressed as the value of the physical quantity without actually determining the Bragg shift. The value of the physical quantity can be determined using an empirically generated lookup table that relates between the modulation phase shift and the value of the physical quantity.

[0092] Representative examples of physical quantities that can be determined include, without limitation, ambient temperature, pressure applied to the fiber, strain of the fiber, accelerative motion of the fiber (e.g., vibration). Another physical quantity that is contemplated is a depth of the respective grating that can be determined based on the pressure applied thereto.

[0093] The present Inventors found that the resolution of the sensing of the Bragg shift (hence also of the value the physical quantity to be determined) can be improved by a judicious selection of the frequency of the modulation and/or the resolution of the measurement of the modulation phase shift. Specifically, denoting the resolution of the measurement of the modulation phase shift by $\Delta\phi_{res}$, the dispersion parameter that characterizes the dispersion by \check{D} , and the modulation angular frequency by Ω , at least one of Ω , $\Delta\phi_{res}$ and \check{D} is preferably selected to satisfy the relation: $\Delta\phi_{res}/(\check{D}\times\Omega) \leq \Delta\lambda_{res}$, where $\Delta\lambda_{res}$ is a predetermined spectral resolution threshold. For example, for a signal processing system **60** capable of measuring the phase at a phase of resolution of $\Delta\phi_{res}$, and dispersive optical device **54** capable of effecting dispersion characterized by a dispersion coefficient the dispersion parameter of \check{D} , controller **42** can be configured to generate a modulation signal characterized by an angular modulation frequency Ω which is at least $\Delta\phi_{res}/(\check{D}\times\Delta\lambda_{res})$.

[0094] Typically, but not necessarily, $\Delta\lambda_{\text{res}}$ is less than 10 picometers or less than 1 picometers or less than 0.1 picometers or less than 0.05 picometers, e.g., 0.01 or less.

[0095] The Inventors found that the improvement in the spectral resolution $\Delta\lambda_{\text{res}}$ (hence also the improvement in the ability to determine the value the physical quantity) can be achieved without or with small compromise on the speed of the measurement. The speed of the measurement is typically expressed in terms of the sampling rate employed by signal processing system 60 in determining the modulation phase shifts. According to some preferred embodiments of the present invention at least one of Ω , $\Delta\phi_{\text{res}}$ and \check{D} is selected to provide spectral resolution of $\Delta\lambda_{\text{res}}$ that less than 0.1 picometer or less than 0.05 picometers, e.g., 0.01 or less, at a sampling rate signal processing system 60 that is at least 1 kHz or at least 10 kHz or at least 100 kHz or at least 1 MHz or at least 10 MHz.

[0096] The method ends at 21.

[0097] As used herein the term "about" refers to $\pm 10\%$.

[0098] The word "exemplary" is used herein to mean "serving as an example, instance or illustration." Any embodiment described as "exemplary" is not necessarily to be construed as preferred or advantageous over other embodiments and/or to exclude the incorporation of features from other embodiments.

[0099] The word "optionally" is used herein to mean "is provided in some embodiments and not provided in other embodiments." Any particular embodiment of the invention may include a plurality of "optional" features unless such features conflict.

[0100] The terms "comprises", "comprising", "includes", "including", "having" and their conjugates mean "including but not limited to".

[0101] The term "consisting of" means "including and limited to".

[0102] The term "consisting essentially of" means that the composition, method or structure may include additional ingredients, steps and/or parts, but only if the additional ingredients, steps and/or parts do not materially alter the basic and novel characteristics of the claimed composition, method or structure.

[0103] As used herein, the singular form "a", "an" and "the" include plural references unless the context clearly dictates otherwise. For example, the term "a compound" or "at least one compound" may include a plurality of compounds, including mixtures thereof.

[0104] Throughout this application, various embodiments of this invention may be presented in a range format. It should be understood that the description in range format is merely for

convenience and brevity and should not be construed as an inflexible limitation on the scope of the invention. Accordingly, the description of a range should be considered to have specifically disclosed all the possible subranges as well as individual numerical values within that range. For example, description of a range such as from 1 to 6 should be considered to have specifically disclosed subranges such as from 1 to 3, from 1 to 4, from 1 to 5, from 2 to 4, from 2 to 6, from 3 to 6 etc., as well as individual numbers within that range, for example, 1, 2, 3, 4, 5, and 6. This applies regardless of the breadth of the range.

[0105] Whenever a numerical range is indicated herein, it is meant to include any cited numeral (fractional or integral) within the indicated range. The phrases "ranging/ranges between" a first indicate number and a second indicate number and "ranging/ranges from" a first indicate number "to" a second indicate number are used herein interchangeably and are meant to include the first and second indicated numbers and all the fractional and integral numerals therebetween.

[0106] It is appreciated that certain features of the invention, which are, for clarity, described in the context of separate embodiments, may also be provided in combination in a single embodiment. Conversely, various features of the invention, which are, for brevity, described in the context of a single embodiment, may also be provided separately or in any suitable subcombination or as suitable in any other described embodiment of the invention. Certain features described in the context of various embodiments are not to be considered essential features of those embodiments, unless the embodiment is inoperative without those elements.

[0107] Various embodiments and aspects of the present invention as delineated hereinabove and as claimed in the claims section below find experimental support in the following examples.

EXAMPLES

[0108] Reference is now made to the following examples, which together with the above descriptions illustrate some embodiments of the invention in a non limiting fashion.

Example 1

Experimental Study

[0109] This Example demonstrates a high speed and high sensitivity FBG interrogator based on radio frequency (RF) phase-shift measurement. Using a sinusoidally modulated source and a chromatic dispersion element, Bragg-wavelength shifts are converted directly to RF phase shifts. Interrogation speeds of more than 1 MHz with spectral sensitivity of less than 1 pm, and sensitivity of less than 0.01 pm at speed of 100 Hz are demonstrated. The excellent resolution-

speed tradeoff is demonstrated over a speed range of 5 orders of magnitude. An overall sensitivity vs. speed dependence of $0.34 \text{ fm}/\sqrt{\text{Hz}}$, which is equivalent to $0.3 \text{ nanostrain}/\sqrt{\text{Hz}}$, is demonstrated. This Example uses direct RF phase-shift measurements as the basis for the interrogation of wavelength shifts in an FBG sensor. The unique potential of this method for achieving an excellent resolution-speed tradeoff, e.g, 10 MHz speed with 1 pm spectral resolution, is demonstrated.

[0110] A light source is modulated by a sinusoidal RF signal at frequency $f_{mod} = \Omega/2\pi$ and modulation index m , giving a power:

$$P(t) = P_0[1 + m\cos(\Omega t)] = P_0 + P_{AC}(t) \quad (1)$$

where P_0 and $P_{AC}(t)$ are the average power and signal envelope respectively. After passing through a dispersive medium with a dispersion coefficient $D[\text{ps/nm/km}]$ and length L , the signal acquires a group delay τ_g which can be expressed as an additional phase ϕ in the AC term:

$$P_{AC,out}(t) = P_0 \cos[\Omega(t - \tau_g)] = P_0 \cos(\Omega t - \phi) \quad (2)$$

[0111] Since the group delay is dependent on the carrier wavelength, a slight shift $\Delta\lambda$ of the center wavelength will cause a shift in the RF phase $\Delta\phi$ which can be approximately expressed as:

$$\Delta\phi \approx \Omega \check{D} \Delta\lambda \quad (3)$$

[0112] By measuring $\Delta\phi$, $\Delta\lambda$ is determined. The minimum detectable phase-shift $\Delta\phi_{res}$ is limited by the phase-noise that accompanies the signal. Therefore, the spectral resolution is defined as:

$$\Delta\lambda_{res} = \Delta\phi_{res} / \Omega \check{D} \quad (4)$$

so that the spectral resolution improves for lower values of phase-shift resolution, higher RF modulation frequency and higher dispersion.

[0113] The experimental setup used in this demonstration is illustrated in FIG. 3. A superluminescent diode (SLED) in the c-band was directly modulated with an RF signal of a vector network analyzer (VNA) having a tunable RF filter. In the present example, the modulation frequency was $f_{mod}=923 \text{ MHz}$. The modulated light was amplified by an EDFA and directed with a circulator into a sensing channel having three FBGs with different Bragg wavelengths. The reflected light was directed into a dispersion component, which was either a dispersion compensating module (DCM) consisting of a circulator and a chirped FBG (Teraxion DCML-C0100-160k) having a dispersion parameter $\check{D} = -2680 \text{ ps/nm}$ (used for the first three experiments described below), or a dispersion compensating fiber (DCF) a dispersion parameter with $DL = -680 \text{ ps/nm}$ (used for a portion of the fourth experiment described below). A demultiplexer split the light into three spectral regimes corresponding to the Bragg wavelengths of the three FBGs, and the detected signals were then routed back to the VNA for RF phase-shift measurement. The average detected optical power was approximately -16 dBm .

[0114] In a first experiment, the system's performance with weak strain was demonstrated. One of the FBGs was periodically strained with a motorized high-precision mechanical stage at a frequency of approximately 1 Hz, and the signal was sampled at a rate of 10 Hz. The pk-pk strain on the FBG was approximately $0.09 \mu\epsilon$, giving a spectral shift of about 0.1 pm in the Bragg wavelength. The output signal is shown in FIG. 4, demonstrating the capability of the system of the present embodiments to acquire weak strain signals with good SNR. The shown resolution capability is below 0.1 pm. In this experiment, the intermediate frequency bandwidth (IF_{BW}) of the VNA was set to $IF_{BW}=10$ Hz, allowing a speed acquisition of approximately 10 samples per second, since the sampling rate of the VNA is proportional to the IF_{sw} .

[0115] A second experiment demonstrated the system response in an ultrasonic region between 20-100 kHz. A second FBG was immersed in a water-filled container, together with an ultrasonic probe (Sonics Vibra-Cell) which gives a fixed vibration at 20 kHz. The Fast Fourier transform (FFT) of the acquired signal is shown in FIG. 5 for three different values of the ultrasonic-wave intensity. In FIG. 5, the green line corresponds to 20% ultrasonic power, the red line corresponds to 60% ultrasonic power, and the black line corresponds to 80% ultrasonic power. The red and black lines are offset for clarity. Note that as the intensity increases, the second harmonic at 40 kHz appears, and for higher intensity other frequencies appear, due to the nonlinearity of the probe. The y-axis wavelength-shift values ($\Delta\lambda$) refer only to the low intensity level experiment (20%), the others are at the same scale, but shifted for clarity. The speed acquisition was about 70 kHz for the low level experiment and about 96 kHz for the higher levels, in order to record the higher harmonic vibrations.

[0116] FIG. 6 shows the results of a third experiment, where a third FBG was wound around a piezoelectric fiber stretcher (Optiphase) driven by a sinusoidal signal at 200 kHz. The acquisition speed was set at about 1.4 MHz. A graph of the signal FFT shows the 200 kHz peak, corresponding to an about 3.5 pm shift in the Bragg wavelength, with an SNR of about 7.

[0117] Throughout these experiments there no cross-talk between the RF signals of the different FBG reflections was observed, enabling a clean detection of each FBG sensor.

[0118] In a fourth experiment, consisted of four different runs, the overall dependence of the system resolution on the IF_{BW} (which limits the speed of the measurement) was characterized for different values of the \check{D} parameter and/or modulation frequency f_{mod} . In each experimental run, the IF_{BW} of the VNA was gradually increased and the minimum (SNR = 1) wavelength-shift resolution was measured, using the same third FBG used in the third experiment. The results are plotted in FIG. 7. In the first run, a standard dispersion compensating fiber (DCF) with $\check{D} = -680$ ps/nm was used (blue dots in FIG. 7). In the second run the DCF was replaced with the DCM used above ($\check{D} = -2680$ ps/nm, red dots in FIG. 7). For both runs f_{mod} was 133 MHz. In the third and fourth runs, the DCM remained, and the modulation frequency was first increased to 913 MHz (green dots in FIG. 7) and then decreased to 635 MHz (black dots in FIG. 7). In the present Example, this latter frequency was preferred, giving 17 dB more RF

power. The solid lines in FIG. 7 are fits to a resolution that is proportional to the square root of the speed.

[0119] As demonstrated in FIG. 7 that for any given dispersion parameter \tilde{D} and modulation frequency, the trade-off between speed and sensitivity depends only on the IF_{BW} . Increasing the dispersion coefficient by a factor of 4, for example, by replacing the DCF (blue line) with the DCM (red line), improves the all-over performance by the same factor as predicted by EQ. 4. Increasing f_{mod} by a factor of 8 (red line to green line) improved the sensitivity by a lower factor of 5.3. It is assumed that this is due to a combination of increased phase noise with increasing frequency as well as the combined RF dependence of the system's various components. This is borne out from the final run at 635 MHz (black line) where the system performance peaked due to the overall RF response of the system. This suggests that the performances described in this Example can be enhanced even further.

[0120] This Example demonstrates an overall sensitivity vs. speed dependence of about 0.34

$$fm/\sqrt{Hz}$$

, which in terms of strain measurement is equivalent to 0.3

$$n\epsilon/\sqrt{Hz}$$

. These results outperform conventional FBG interrogators. The technique of the present embodiments is robust and can be used for dynamic measurements as well as for quasi-static monitoring without the need for additional compensation techniques which increase cost and complexity. Due to its reliance on frequency domain measurements and electronic RF processing, the technique of the present embodiments is more flexible than conventional methods, particularly those that rely on time-domain measurements. This Example demonstrates that the operating point can be selected anywhere in the region between ultra-high sensitivity or ultra-high speed, by adjusting the RF filter bandwidth or other equivalent signal processing parameters.

[0121] The spectral dynamic range (ratio between spectral bandwidth and resolution) of the exemplified technique is about 35dB for phase resolution of 2 mrad, within the 2π phase ambiguity constraint. As for the measurable wavelength range, the flexibility of the technique of the present embodiments is an advantage, since decreasing the modulation frequency decreases the wavelength-shift to phase-shift ratio (see EQ. 3), allowing for large wavelength range measurements. The phase can in some embodiments of the present invention be unwrapped by digital signal processing if the sampling rate is at least twice as fast as the signal measurement speed, enabling an increase of the dynamic range. The large spectral dynamic range and flexible wavelength range measurement, allow for high-speed and high-resolution interrogation. Another advantage of the exemplified technique is that fluctuations of the source power do not affect the measurement. This feature is particularly useful for amplified spontaneous emission (ASE) light sources such as an as SLED, where the broadband spectrum appears to be stable over a long time scale, but fluctuates at RF time scales.

[0122] A further advantage of the technique of the present embodiments is the ability to simultaneously interrogate cascaded FBG sensors by routing the different spectral regions of

each FBG sensor to different detectors (for example, using a demultiplexer) and measuring all the phase-shifts in parallel. This capability is particularly useful for applications such as machine condition monitoring, especially at MHz sampling rates.

Example 2

Exemplified Phase Shift Measurement

[0123] FIG. 8 is a flowchart diagram of a method suitable for amplifying a phase shift of a signal relative to a reference signal, according to some embodiments of the present invention. The method is suitable for improving the resolution of phase shift measurement. The phase shift can be amplified by a predetermined factor to a value that is within the detection resolution of a phase shift detector. The amplified phase shift can then be measured by the phase shift detector as known in the art, and the result of the measurement can be divided by the predetermined factor, thereby allowing the determination of the unamplified phase shift even if its extent is less than the available resolution of the phase shift detector.

[0124] The method begins at **600** and continues to **601** at which a signal S is generated or received, and to **602** at which a reference signal S_{ref} is generated or received. For example, one of the signals (e.g., signal S) can be the signal reflected off the grating(s) in the fiber of the present embodiments, and the other signal (e.g., signal S_{ref}) can be received via a path that does not allow it to interact with the grating(s). The method continues to **603** at which the modulation of at least one of the signals is varied. The variation is optionally and preferably with respect to the modulation amplitude such that the modulation amplitudes of the signal and the reference signal are sufficiently close to each other. Preferably, a ratio between modulation amplitudes of the signal and the reference signal is from about 0.9 to about 1.1, or from about 0.95 to about 1.05, or from about 0.99 to about 1.01, or from about 0.995 to about 1.005, or from about 0.999 to about 1.001 or from about 0.9995 to about 1.0005 or from about 0.9999 to about 1.0001. The variation is optionally and preferably also with respect to the modulation phase, such that the phase difference θ_{in} between the phase θ_1 of the reference signal and the phase θ_2 of the signal is sufficiently small or sufficiently close to π radians, as further detailed hereinabove. Optionally, one of signals S and S_{ref} is generated by selected operations of method **100** so as to ensure that the phase difference θ_{in} is sufficiently small or sufficiently close to π radians. The amplitude(s) and phase(s) employed for the modulation variation can be selected by the method or be stored or encoded in a circuit that vary the modulation.

[0125] The method preferably continues to **604** at which an output signal S_{out} which is a linear combination of the signals is formed. This can be done electronically, using an electric circuit, or optically using an optical assembly. The combination **604** can be done either directly, for

example, using a signal summing circuit, or indirectly, for example, by signal multiplication followed by extraction of signal components that are linearly proportional to each of the signals, as further detailed hereinabove.

[0126] The linear combination can be generally written as $S_{out} = p(S+qS_{ref})$, where p is a normalization parameter, q is a linear combination coefficient and S and S_{ref} are, respectively, the signal and reference signal following the modulation variation **603**. The normalization parameter p can be set to any number, e.g., 1. The linear combination coefficient reflects the weight ratio of the two signal and is optionally and preferably selected based on the sign of $\cos(\theta_{in})$, where θ_{in} is the phase difference between the modulation phases of the signals.

[0127] Generally, q is about 1 when $\cos(\theta_{in})$ is negative and about -1 when $\cos(\theta_{in})$ is positive. This can be written mathematically as $q \approx -NINT(\cos(\theta_{in}))$, where NINT is the nearest integer function and the \approx sign is to be understood as within 10%. In other words, q optionally and preferably satisfies the conditions $\text{sign}(q) = -\text{sign}(\cos(\theta_{in}))$ and $0.9 \leq |q| \leq 1.1$.

[0128] It was found by the present Inventors that the above procedure can ensure that the phase difference of the output signal relative to the reference ($\theta_{out} - \theta_1$) is amplified relative to the phase difference θ_{in} . It was found that the amplification extent can reach the value of $1/\alpha$, where α is the absolute value of the difference between 1 and the ratio between modulation amplitudes of the signals. According to some embodiments of the present invention α can be at most 0.1 or at most 0.05 or at most 0.01 or at most 0.005 or at most 0.0001 or less, so that θ_{out} can be 10 times larger or 20 times larger or 100 times larger or 200 times larger or 1000 times larger or 2000 times larger or 10000 times larger than θ_{in} , where θ_{out} is the phase of S_{out} .

[0129] In some embodiments of the present invention the method continues to **605** at which the phase of the output signal relative to the reference signal is measured. This can be done using any phase measuring technique known in the art. Representative examples including, without limitation, phase detectors that are commercially available from Mini-Circuits[®], USA, and On Semiconductors[®], USA.

[0130] In some embodiments of the present invention, the method continues to **606** at which a change over time of the phase of the output signal relative to the reference signal is measured. Operation **606** can be executed whether or not the phase of the output signal is known, since a change in a phase of a signal can be measured even when the signal's phase itself is not known. Thus, in some embodiments **605** is executed and **606** is not executed, in some embodiments both **605** and **606** are executed, in some embodiments **605** is not executed and **606** is executed, and in some embodiments none of **605** and **606** is executed.

[0131] The method ends at **607**.

[0132] Once the change of the phase is measured, it can be multiplied by α to determine the unamplified phase shift.

[0133] FIG. 9 is a schematic block diagram illustration of a system 700 for amplifying a phase shift of a signal relative to a reference signal, according to some embodiments of the present invention. System 700 is optionally and preferably configured for executing one or more operations of method 600 above. System 700 comprises a modulation circuit 702, configured for varying a modulation of at least one of the signals as further detailed hereinabove. The amplitude(s) and phase(s) employed for the modulation variation performed by circuit 702 can be selected by system 700, for example, using an amplitude selection circuit, or be stored or encoded in circuit 702.

[0134] System 700 can also comprise a signal combiner 704, configured for forming an output signal S_{out} which is a linear combination of the signals, as further detailed hereinabove. In some embodiments, combiner 704 comprises a signal adder circuit. These embodiments are useful when the linear combination coefficient is positive (e.g., $q=1$). In some embodiments, combiner 704 comprises a signal subtractor circuit. These embodiments are useful when the linear combination coefficient is negative (e.g., $q=-1$). In some embodiments, combiner 704 comprises a signal multiplier circuit. These embodiments are useful when the linear combination is obtained by multiplication followed by extraction of linear components as further detailed hereinabove.

[0135] In some embodiment combiner 704 is an optical assembly configured for performing a linear combination of two signals as known in the art.

[0136] In some embodiments of the present invention, system 700 comprises a detector circuit 706, which can be configured as phase detector for measuring a phase of the output signal relative to the reference signal, or as a phase-change detector for measuring a change of phase of the output signal over time, or as a combined phase detector and phase-change detector for measuring both the phase of and its change.

Example 3

Calculation of phase-shifts by solving a system of equations

[0137] This Example describes a technique for numerically calculating the wavelength-shift caused by each grating, by scanning the modulation frequency. The advantage of this technique is that it does not need a physical element (such as a de-multiplexer) to separate between the channels. Since the light reflected off the gratings (and optionally and preferably passed through the dispersive optical device) is a summation of the different signals returning from the different gratings the total signal at the modulation frequency Ω can be written as:

$$a_1 e^{i\Delta\varphi_1} + a_2 e^{i\Delta\varphi_2} + \dots + a_N e^{i\Delta\varphi_N} - h e^{i\xi}$$

$$a_1 e^{-j\phi_1} + a_2 e^{-j\phi_2} + \dots + a_N e^{-j\phi_N} = b e^{-j\phi}$$

where a_i and $\Delta\phi_i \equiv \check{D}\Omega\Delta\lambda_i$ are respectively the magnitude and the phase-shift reflected off the i th grating, and b and ϕ are respectively the global magnitude and the global phase-shift of the total signal as measured by an optical detector having a single optical sensor.

[0138] Assuming the magnitudes a_i are known from preliminary measurements, by scanning different modulation frequencies Ω_j (preferably at least $N/2$, where N is the number of gratings in the fiber), one can obtain a system of N equations with N unknowns (the Bragg-wavelength-shifts $\Delta\lambda_i$). The scanning can be serial or in parallel. Parallel scanning can be achieved by simultaneously modulating the RF signal with several frequencies, and measuring, e.g., by a signal processing system, each frequency by itself simultaneously, for example, using RF filters. A suitable system of N equations can be written as:

$$\sum_{i=1}^N a_{i,\Omega_1} \cos(\check{D}\Omega_1\Delta\lambda_i) = b(\Omega_1) \cos(\xi(\Omega_1))$$

$$\sum_{i=1}^N a_{i,\Omega_1} \sin(\check{D}\Omega_1\Delta\lambda_i) = b(\Omega_1) \sin(\xi(\Omega_1))$$

$$\sum_{i=1}^N a_{i,\Omega_2} \cos(\check{D}\Omega_2\Delta\lambda_i) = b(\Omega_2) \cos(\xi(\Omega_2))$$

$$\sum_{i=1}^N a_{i,\Omega_2} \sin(\check{D}\Omega_2\Delta\lambda_i) = b(\Omega_2) \sin(\xi(\Omega_2))$$

$$\sum_{i=1}^N a_{i,\Omega_{N/2}} \cos(\check{D}\Omega_{N/2}\Delta\lambda_i) = b(\Omega_{N/2}) \cos(\xi(\Omega_{N/2}))$$

$$\sum_{i=1}^N a_{i,\Omega_{N/2}} \sin(\check{D}\Omega_{N/2}\Delta\lambda_i) = b(\Omega_{N/2}) \sin(\xi(\Omega_{N/2}))$$

[0139] A solution or partial solution of this system of equations can provide the values of $\Delta\lambda_i$, $i=1, 2, \dots, N$. This system of equations can be automatically solved using any technique known in the art. Representative examples include, without limitation the 'Trust-region' method [26] and the 'Levenberg-Margardt' technique [27,28].

[0140] Although the invention has been described in conjunction with specific embodiments thereof, it is evident that many alternatives, modifications and variations will be apparent to those skilled in the art. Accordingly, it is intended to embrace all such alternatives, modifications and variations that fall within the scope of the appended claims.

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Krav

- 5 1. En metode (10) til bestemmelse af forstyrrelse af et gitter (46), der er dannet i en optisk fiber (44), idet metoden omfatter:

10 modulation (12) og transmission (14) af en lysstråle (34) gennem den optiske fiber (44), måling (19) af mindst en faseforskydning $\Delta\phi_i$ i en modulation af lys, der reflekteres fra gitteret (46), for direkte at konvertere en bølgelængdeforskydning af lysstrålen (34) til faseforskydningen i modulationen, og bestemmelse (20) af forstyrrelsen af gitteret (46) baseret på den mindst ene faseforskydning;

15 hvor faseforskydningen $\Delta\phi_i$ er defineret som en forskel mellem en samlet modulationsfase $\phi_i + \Delta\phi_i$, der er opnået af lysstrålen (34), når gitteret (46) er forstyrret, og en samlet modulationsfase ϕ_i , der ville være opnået af lysstrålen (34), hvis gitteret (46) havde været uforstyrret; og

hvor metoden omfatter spredning (16) af den reflekterede lysstråle (34) forud for målingen (19) af den mindst ene faseforskydning $\Delta\phi_i$.
- 20 2. Metoden (10) i krav 1, hvor moduleringen (12) udføres før overførslen (14).
3. Metoden (10) i et hvilket som helst af kravene 1 og 2, hvor moduleringen (12) udføres, efter at lysstrålen (34) er reflekteret af gitteret (46).
- 25 4. Metoden (10) ifølge et hvilket som helst af kravene 1-3, hvor den optiske fiber (44) er dannet med en flerhed af gitre (46), og hvor mindst to af de nævnte gitre (46) er **karakteriseret ved** forskellige Bragg-bølgelængder ($\lambda_1, \lambda_2, \dots, \lambda_N$).
- 30 5. Metoden (10) ifølge krav 4, der yderligere omfatter de-multiplexing (17) af den reflekterede lysstråle (34) i mindst to kanaler, der henholdsvis svarer til de forskellige Bragg-bølgelængder ($\lambda_1, \lambda_2, \dots, \lambda_N$), før målingen (19) af den mindst ene faseforskydning.
- 35 6. Metoden (10) ifølge krav 4, hvor modulationen (12) omfatter scanning af en frekvens af modulationen over en flerhed af modulationsfrekvenser, hvor metoden omfatter måling (19) af en modulationsfaseforskydning og modulationsstørrelse af lys, der reflekteres af de mindst to gitre for hver modulationsfrekvens, og bestemmelse (20) af en individuel optisk bølgelængde eller optisk frekvensforskydning for hver af de mindst to gitre baseret på de målte modulationsfaseforskydninger og de målte modulationsstørrelser.
- 40 7. Metoden (10) ifølge et hvilket som helst af kravene 1-6, hvor målingen (19) af den mindst ene faseforskydning er kendetegnet ved en forudbestemt faseopløsning, og dispergeringen (16) er kendetegnet ved en forudbestemt dispersionsparameter, der beskriver pulsbredelse pr. bølgelængdeenhed, og hvor en frekvens af moduleringen mindst er et forhold mellem faseopløsningen og en multiplikation af dispersionsparameteren med en forudbestemt spektralopløsningstærskel.
- 45 8. Metoden (10) ifølge et hvilket som helst af kravene 1-6, hvor dispergeringen (16) er karakteriseret ved en dispersionskoefficient, hvor metoden omfatter variation af en værdi af koefficienten over en flerhed af dispersionskoefficientværdier, måling af en modulationsfaseforskydning og modulationsstørrelse af lys, der reflekteres fra gitteret, for hver værdi af dispersionskoefficienten, og bestemmelse (20) af en individuel optisk bølgelængde eller optisk frekvensforskydning for hvert af de mindst to gitre, baseret på de målte modulationsfaseforskydninger og målte modulationsstørrelser.
- 50

9. Metoden (10) ifølge et hvilket som helst af kravene 1-8, hvor den nævnte bestemmelse (20) af forstyrrelsen af gitteret (46) omfatter at udtrykke forstyrrelsen som et skift i en Bragg-bølgelængde ($\lambda_1, \lambda_2, \dots, \lambda_N$), der karakteriserer gitteret (46).
- 5 10. Metoden (10) ifølge krav 1, hvor bestemmelsen (20) af forstyrrelsen af gitteret (46) omfatter at udtrykke forstyrrelsen som mindst en fysisk størrelse, der påvirker forstyrrelsen af gitteret (46).
- 10 11. Metoden (10) ifølge krav 10, hvor den mindst ene fysiske størrelse er valgt fra gruppen bestående af omgivelsestemperatur, tryk påført fiberen (44), belastning af fiberen (44) og accelerativ bevægelse af fiberen (44).
12. Et system (30) til bestemmelse af forstyrrelse af et gitter (46), der er dannet i en optisk fiber (44), idet systemet (30) omfatter:
- 15 et optisk modulationssystem (40) til modulation af en lysstråle (34);
 en optisk kobler (48) til at koble den nævnte lysstråle (34) ind i den optiske fiber (44) og modtage lys, der reflekteres fra gitteret (46); og
 et optisk og elektrisk analysesystem (52), der er konfigureret til at måle mindst en faseforskydning i en modulation af lys, der reflekteres fra gitteret (44), for direkte at konvertere en bølgelængdeforskydning af lysstrålen (34) til faseforskydningen $\Delta\phi_i$ modulationen, og bestemme forstyrrelsen af gitteret (46) baseret på den mindst ene faseforskydning;
- 20 hvor faseforskydningen $\Delta\phi_i$ er defineret som en forskel mellem en samlet modulationsfase $\phi_i + \Delta\phi_i$, der er opnået af lysstrålen (34), når gitteret (46) er forstyrret, og en samlet modulationsfase ϕ_i , der ville være opnået af lysstrålen (34), hvis gitteret (46) havde været uforstyrret; og
 hvor systemet (30) omfatter en dispersiv optisk anordning (54), der er konfigureret til at sprede den reflekterede lysstråle (34) forud for målingen af den mindst ene faseforskydning $\Delta\phi_i$.
- 30 13. Systemet (30) ifølge krav 12, hvor den optiske fiber (44) er dannet med en flerhed af gitre (46), og hvor mindst to af de nævnte gitre (46) er karakteriseret ved forskellige Bragg-bølgelængder ($\lambda_1, \lambda_2, \dots, \lambda_N$).
- 35 14. Systemet (30) ifølge krav 13, hvor analysesystemet (52) omfatter et optisk de-multiplexingssystem (56) til de-multiplexing af den reflekterede lysstråle (34) i mindst to kanaler, der henholdsvis svarer til de forskellige Bragg-bølgelængder ($\lambda_1, \lambda_2, \dots, \lambda_N$), før målingen af den mindst ene faseforskydning $\Delta\phi_i$.
- 40 15. Systemet (30) ifølge krav 14, hvor det optiske modulationssystem (40) er konfigureret til at scanne en frekvens af modulationen over en flerhed af modulationsfrekvenser Ω_i , hvor det optiske og elektriske analysesystem (52) er konfigureret til at måle en modulationsfaseforskydning $\Delta\phi_i$ og modulationsstørrelse a_i af lys (34), der reflekteres fra gitteret (46), for hver modulationsfrekvens Ω_i , og til bestemmelse af en individuel optisk bølgelængdeforskydning $\Delta\phi_i$ eller optisk frekvens Δf_i -forskydning for hver af de mindst to gitre (46), baseret på de målte modulationsfaseskift $\Delta\phi_i$ og målte modulationsstørrelser a_i .
- 45

DRAWINGS

Drawing

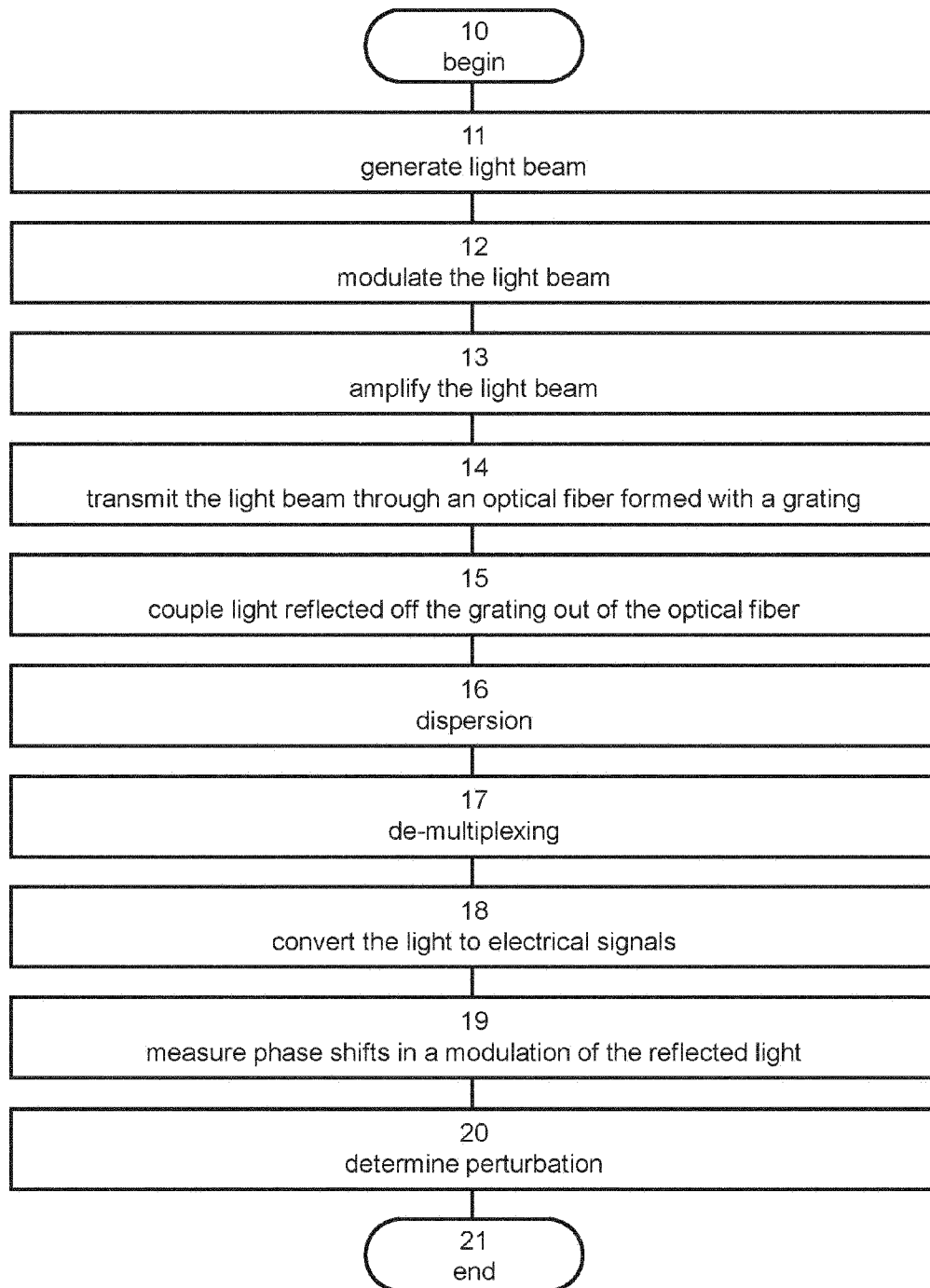


FIG. 1

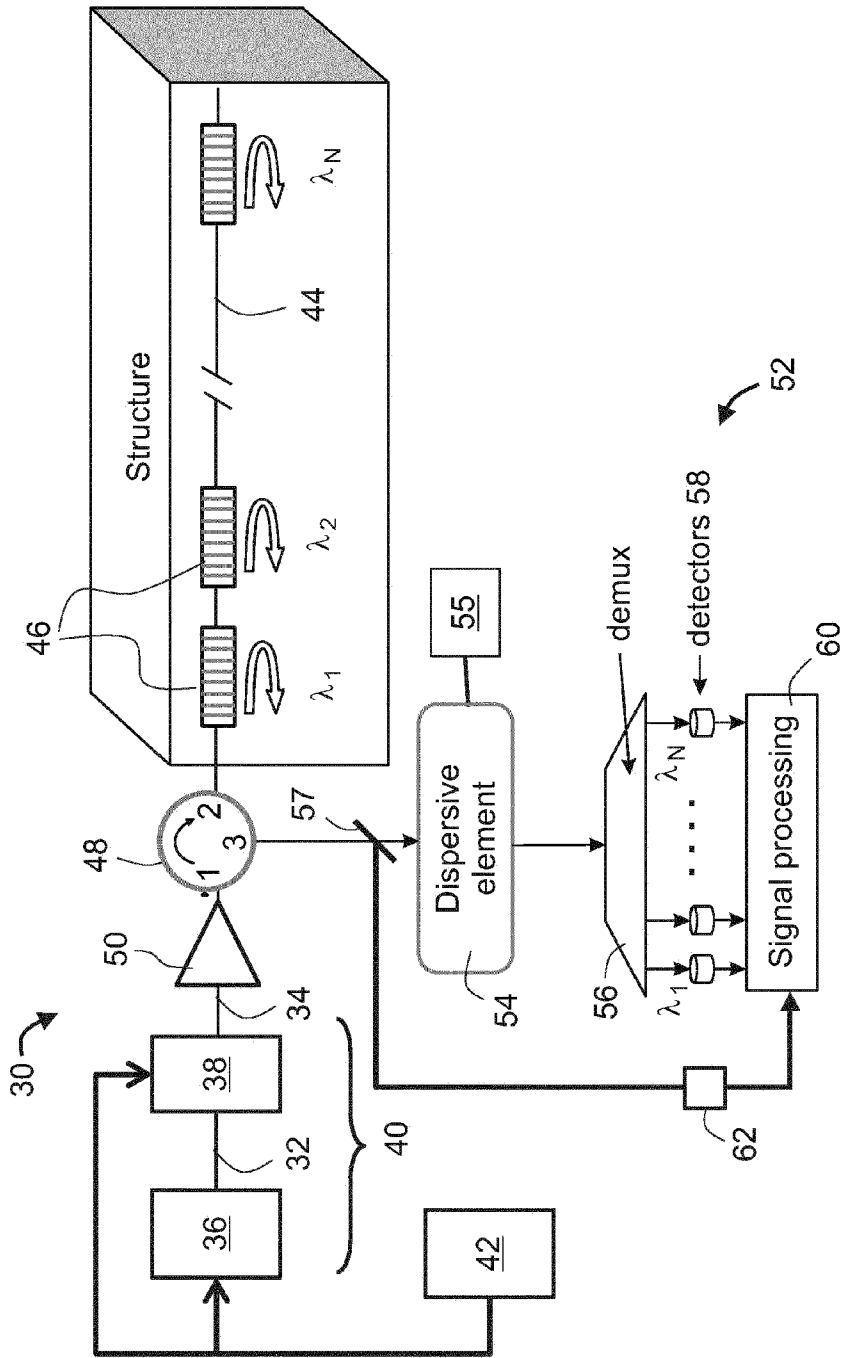


FIG. 2

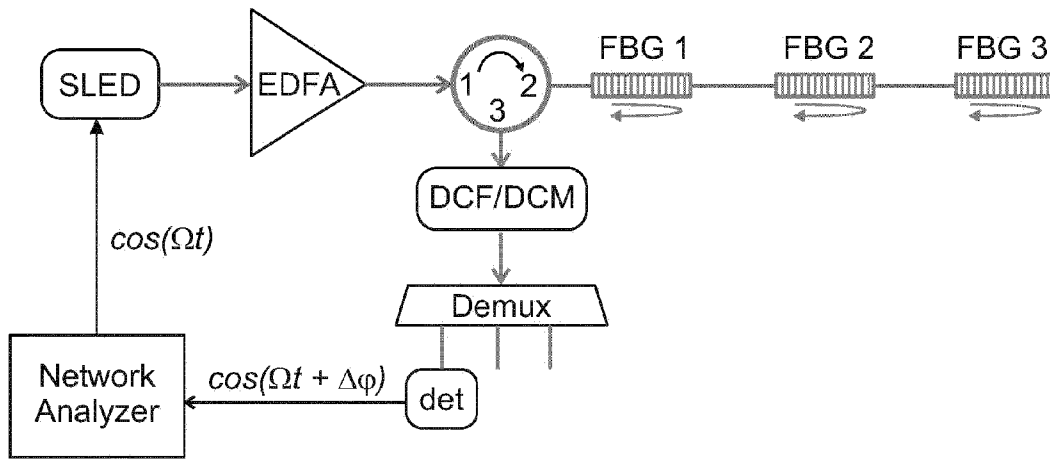


FIG. 3

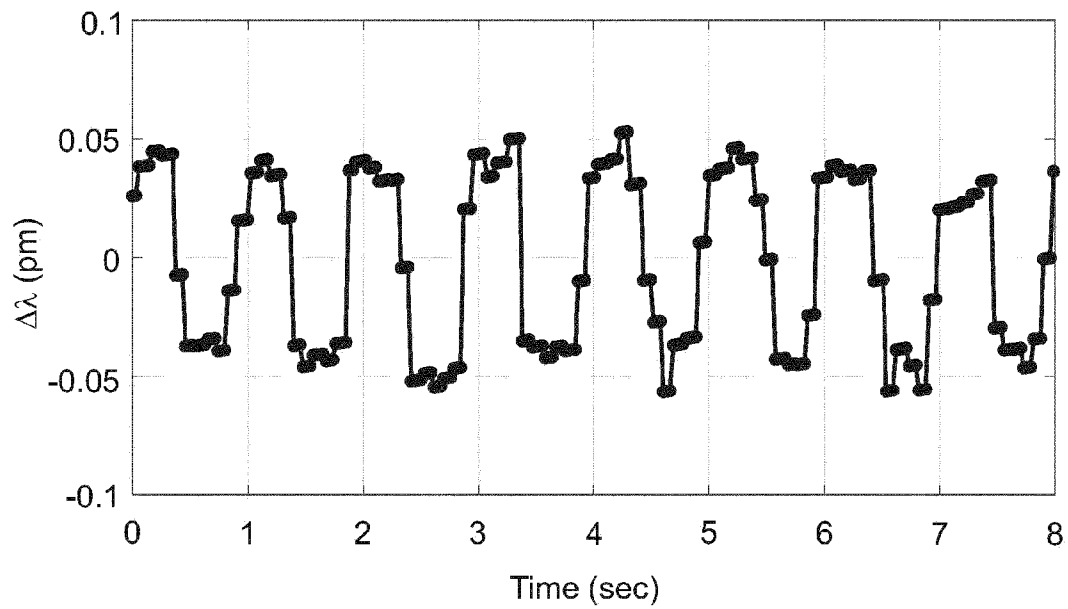
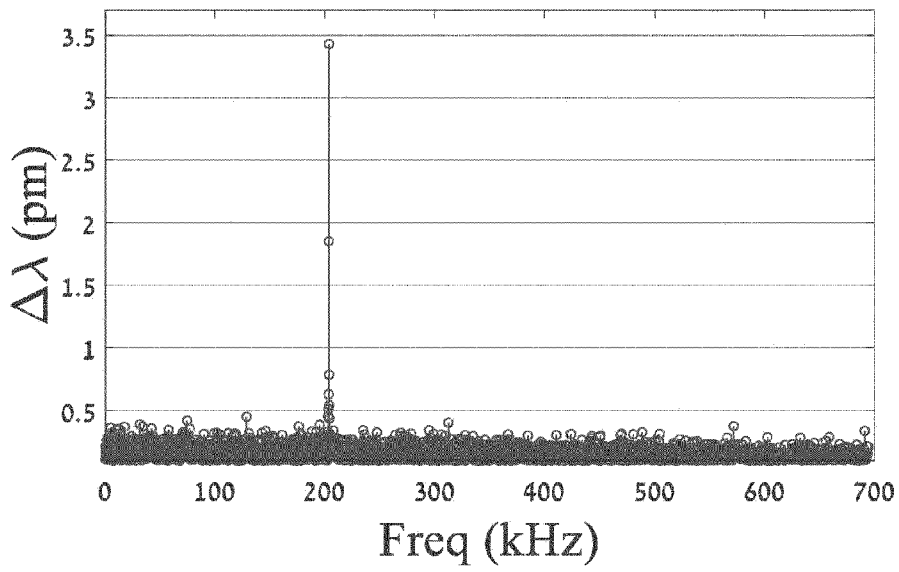
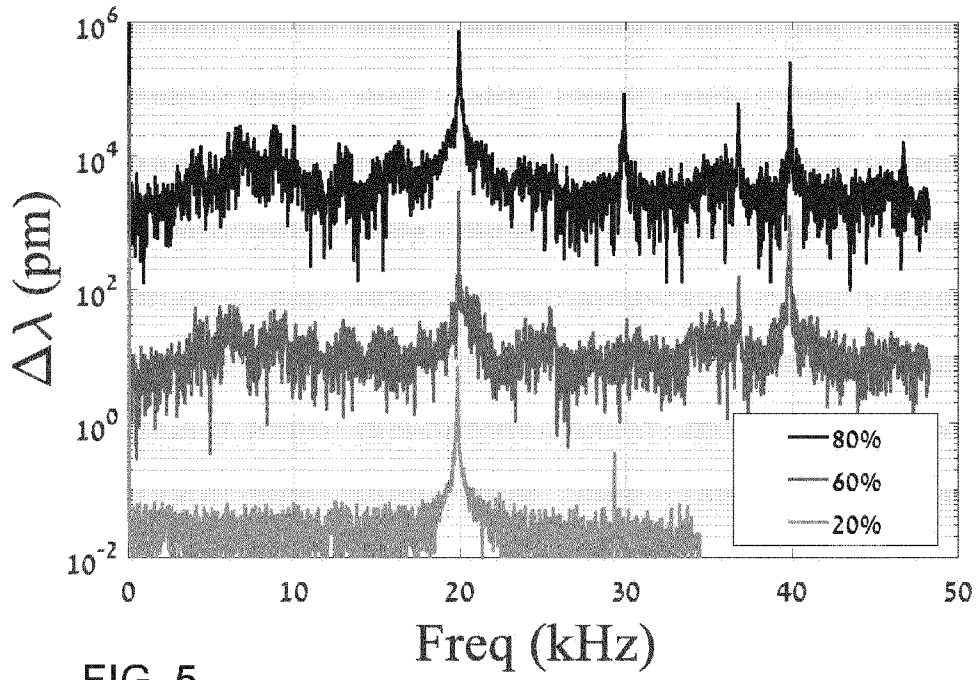


FIG. 4



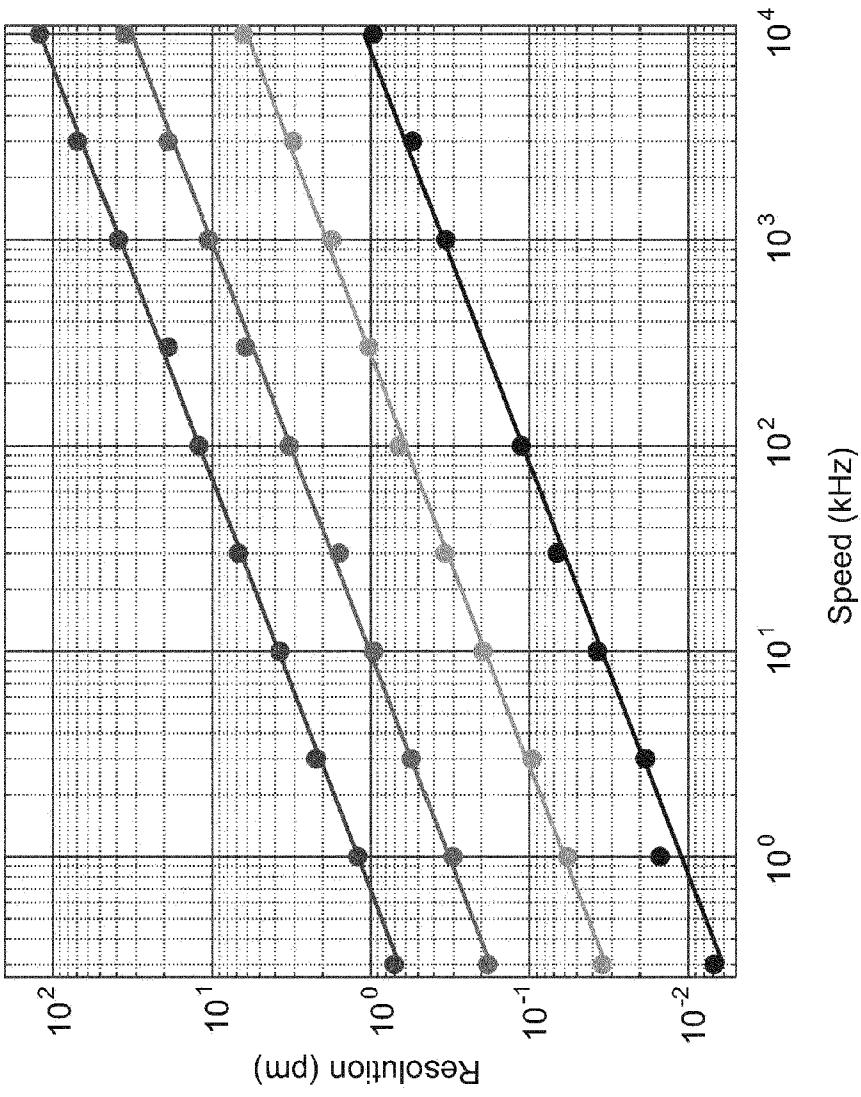


FIG. 7

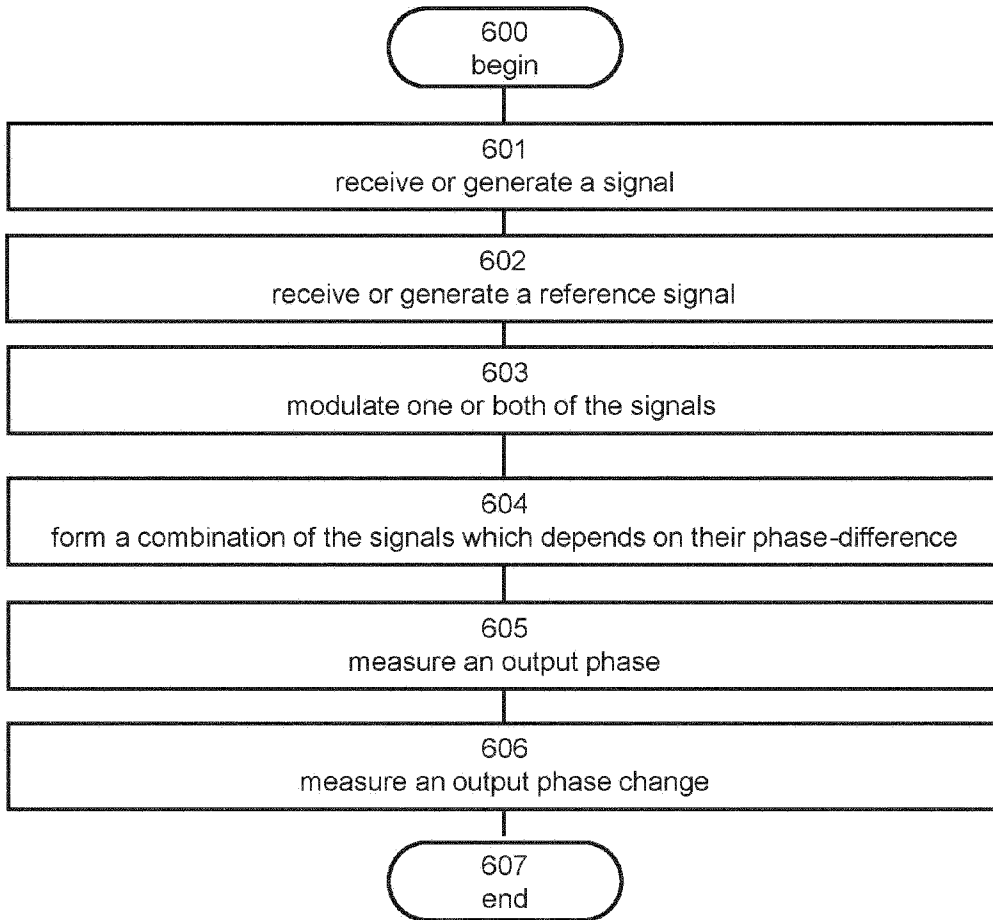


FIG. 8

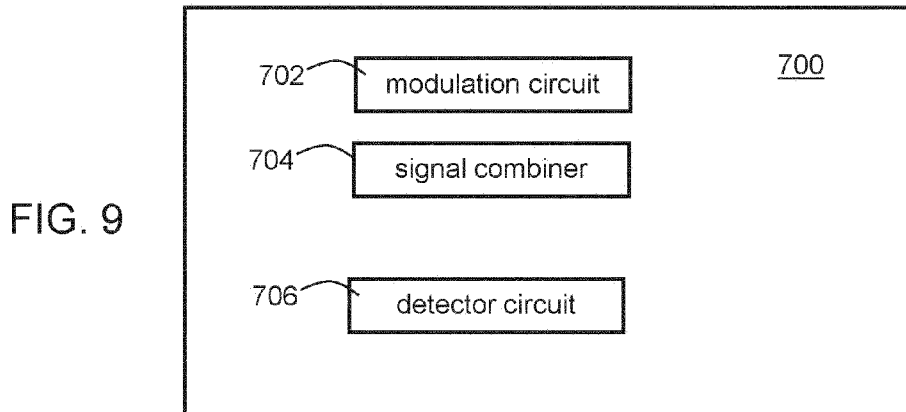


FIG. 9