



(51) International Patent Classification:

G01P 3/36 (2006.01) **G06T 7/20** (2006.01)
G01P 3/50 (2006.01) **G01S 11/12** (2006.01)

(21) International Application Number:

PCT/EP2009/067252

(22) International Filing Date:

16 December 2009 (16.12.2009)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

08172123.5 18 December 2008 (18.12.2008) EP

(71) Applicant (for all designated States except US): **UNI-
VERSITÄT ZÜRICH** [CH/CH]; Protektorat Forschung,
Rämistrasse 71, CH-8006 Zürich (CH).

(72) Inventor; and

(75) Inventor/Applicant (for US only): **ROHRSEITZ, Nicola**
[CH/CH]; Limmatstrasse 267, CH-8005 Zürich (CH).

(74) Agent: **FISCHER, Michael**; Siemens AG, Postfach 22
16 34, 80506 München (DE).

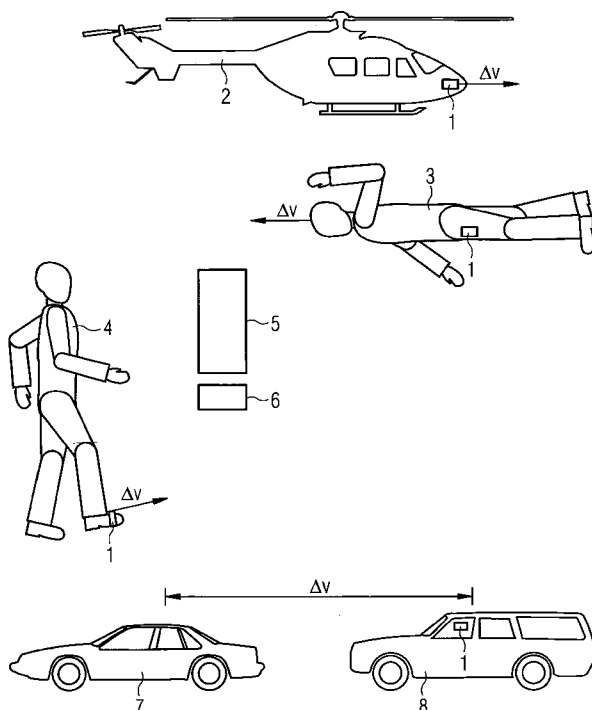
(81) Designated States (unless otherwise indicated, for every
kind of national protection available): AE, AG, AL, AM,
AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ,
CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO,
DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT,
HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP,
KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD,
ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI,
NO, NZ, OM, PE, PG, PH, PL, PT, RO, RS, RU, SC, SD,
SE, SG, SK, SL, SM, ST, SV, SY, TJ, TM, TN, TR, TT,
TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every
kind of regional protection available): ARIPO (BW, GH,
GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM,
ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ,
TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE,
ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV,
MC, MK, MT, NL, NO, PL, PT, RO, SE, SI, SK, SM,
TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW,
ML, MR, NE, SN, TD, TG).

[Continued on next page]

(54) Title: PASSIVE TRANSLATIONAL VELOCITY MEASUREMENT FROM OPTICAL INFORMATION

FIG 1



(57) Abstract: The invention is a passive method to measure the translational speed of a visual scene using the distribution of light intensities. Measuring the speed of translation is useful for control, safety, management of resources, fuel efficiency, and many more application fields. It is however technically challenging because a wide-field translating scene projects on an image plane as a heterogeneous field of apparent speeds. The invention solves this problem by combining two principles: perspective distortion matching over a broad field of view, and temporal filtering variation. In conventional systems, an acquired image is calibrated to obtain linear coordinates. Instead, the invention uses the perspective distortion of the image to sample the visual scene at different linear wavelengths over the visual field. The result is a spatial sensitivity map of the visual scene. The obtained signal is then temporally filtered with cutoff frequencies proportional to the spatial sensitivity. The final result is the wide-spectrum computation of the ratio between temporal and linear spatial frequencies, in other words linear speed. The technique is passive because it does not require the emission of a reference signal. This is an advantage over active speed sensors mainly because of reduced power consumption, but it is an enabling factor for other applications. Where it is difficult or impossible using standard device-centered techniques, like on aircrafts or in fluids, the invention enables measuring absolute linear speed. The advantage over non-device-centered techniques—like GPS—is the independence from external infrastructures. The small computational overhead makes it ideal for mobile applications.



Published:

— *with international search report (Art. 21(3))*

Passive translational velocity measurement from optical information

The present invention relates to a method and a system for
5 determining a linear speed of an object, in particular in a Cartesian frame of reference.

Linear speed computation could benefit applications such as self-guided vehicles (at 2 in FIG. 1), mobile robotics, smart
10 vision systems, and body movement control for therapy (at 3 in Fig. 1) and entertainment (at 4 in Fig. 1). In general, the measurement of linear speed from optical information is useful to technical applications because it operates in the frame of reference of translating movements.

15 Moreover, linear speed can be used to compute the distance traveled. This requires multiplying the linear speed signal by the appropriate time interval.

20 The passive measurement of the linear speed from a visual scene relies on the light distributions generated by a translation. It is a technically challenging task mainly because a wide-field scene moving at constant translational speed projects on an image plane as a heterogeneous field of
25 apparent speeds that depends on the distribution of spatial frequencies (FIG. 2). This field is called optical flow, and is what the existing visual speed sensors measure.

Each velocity vector of the optical flow field is a projection
30 of the translational speed. These vectors can thus render the translational speed by means of a spherical-to-cartesian transformation. This requires, besides the intensity, direction and location of the vector in the spherical field, also the distance between the sensing entity and the projected
35 moving object. This principle is applied in the so-called "V/H" sensors. These have commonly a narrow field of view, pointed perpendicularly to the direction of translation.

Unfortunately, the computation of speed using the V/H sensor is not as robust as it would be desirable in terms of accuracy.

5

It is therefore an objective of the present invention to provide a method to measure linear speed using an optoelectronic device.

10 Contrary to V/H sensors, the present invention computes speed over a wide-field of view, and therefore it is more robust over a broad range of spatial frequencies (the inverse of linear wavelength). Moreover, contrary to conventional optical flow sensors, the spatial and temporal filtering properties of
15 the invention can be adapted to the requirements of the target application.

Industry standard systems on the other hand rely on computationally intensive feature-matching algorithms (e.g.,
20 "block matching"). Contrary to these, the invention is computationally lightweight.

The aim of the invention is therefore to measure speed in the cartesian frame of reference with little computational
25 overhead.

This aim is achieved by the features given in claim 1 for the method and in claim 4 for the system.

30 According to claim 1, the method for determining a linear speed of an object comprises the steps of:
a) sampling a series of light intensity courses $I(t)$ over the time t ; each light intensity courses $I(t)$ covering a different azimuthal direction, each different azimuthal direction
35 thereby defining a detection length of a series of detection lengths as seen in the direction of the linear speed to be determined;

- b) transforming the series of detection lengths for the azimuthal directions into a series of linear spatial frequencies;
- c) defining for each azimuthal direction a band pass or a high pass filter, thereby relating for each detection length the characteristic filter frequencies to the respective linear spatial frequencies;
- d) filtering the sampled light intensity for each azimuthal direction with the respective band pass or high pass filter to obtain a set of filtered light intensities;
- e) calculating the linear speed by dividing the characteristic filter frequencies through the spatial frequencies for at least one of azimuthal directions for which the filtered light intensity exceeds a predefined threshold; and
- f) determining the linear speed by correlating the calculated linear speeds for those azimuthal directions for which the filtered light intensity exceeds the predefined threshold.

With respect to the technical terms used above, some detailed information is given below on how to interpret these terms. Azimuthal direction means a spatial angle between two angles. For example, the total azimuth of 90° is divided into 18 azimuthal directions meaning every azimuthal direction to cover 5° of the total azimuth of 90° . The detection length or also called herein linear wavelength is the length of each azimuthal direction in the direction of the linear speed. The detection length is therefore a function of the azimuthal direction and the distance to the physical structures perpendicular to the linear speed vector. The transformation of these detection lengths leads to the inverse of the detection lengths which is called hereinafter the spatial frequencies. The characteristic filter frequencies are those frequencies that are related to the throughput frequencies of the filter. The throughput frequencies are related to the spatial frequencies of each of the azimuthal directions. The more perpendicular the azimuthal direction is oriented, the higher are the characteristic filter frequencies. In a

preferred embodiment, the average of the lower and upper cut-off frequency of a band pass filter specified for a distinct azimuthal direction matches with the periodic time of the substantially sinusoidal intensity pulse occurring for this specific detection length. When the intensity structure of the light source does not match with the detection length of the respective azimuthal direction the intensity pulse deviates more from the substantial sinusoidal form; either broadens and becomes flatter in terms of intensity or tapers and becomes higher in terms of intensity. Consequently, the intensities $I(t)$ measured for these azimuthal directions are filtered out and these azimuthal directions can therefore not contribute to the determination of the linear speed. Therefore, a predefined threshold for the intensity signal after filtering has to be defined. When a filtered intensity will exceed this threshold, the temporal frequencies TF (the range of the throughput frequencies) have to be divided by the spatial frequencies for each specific azimuthal direction delivering a course of a normalized response over the velocity $v=TF/SF$ wherein the peaks of these normalized responses for a plurality of azimuthal directions deliver finally the linear speed.

The invention therefore does the determination of the linear speed spoken in general terms by combining two principles: perspective distortion matching and temporal filtering variation. The process of passively extracting the velocity from a visual scene using the invention requires a set of photoreceptors (i.e., light intensity encoders) with defined angular aperture, and variable band-pass filtering. These two components allow exploiting the three crucial concepts required for measuring speed from passive visual information:

- Every instantaneous natural visual scene is separable in a series of linear spatial frequencies.
- Every point in a natural visual scene is separable in a series of temporal frequencies.
- Speed is the ratio between temporal and spatial frequency ($v = TF/SF$).

From a point-like, radial perspective, any linear wavelength projects on a circle as a combination of increasing angular wavelengths. This trivial phenomenon is known as perspective distortion. The opposite situation is to project an angular wavelength on a line, which results in increasingly long linear wavelengths. Using this last principle to sample identical angular wavelengths over a broad ($\sim 90^\circ$) angular opening means acquiring a multitude of linear wavelengths. As every instantaneous natural visual scene is separable in a series of linear spatial frequencies (i.e., the inverse of a linear wavelength), each angular receptor sensitive to an angular wavelength will be able to sample a different linear spatial component. This means that the perspective distortion from linear to angular creates a linear spatial filter that depends on the direction of sampling. The combination of a set of identical angular photoreceptors directed on different coplanar axes creates therefore a sensitivity map for a broad range of linear spatial frequencies.

The spatial sensitivity must be matched by an adequate temporal sensitivity that results in the encoding of speed. The domain of temporal filters has been extensively studied, and has a wide range of industrial applications. The appropriate filter to apply to the spatial sensitivities is either high-pass or band-pass. The temporal cut-off frequencies must be proportional ($v = TF/SF$) to those created by the spatial filters, to result in sensitivity to linear speed which range has to be contemplated upon when designing the azimuthal resolution.

The gist of the invention is thus divided in two:

- Broadband spatial filtering using perspective distortion
- Matching temporal filtering variation to obtain linear velocity measurement

These features provide a robust and computationally lightweight method of measuring speed in a linear frame of reference. The method is largely independent of the precise details of implementation (software, electronic, digital, analog,...). These affect the performance and quality of the computation, making the method adaptable to different kinds of applications. Because of the small computational overhead, the method can be embedded in portable devices.

10

Brief description of the drawings

FIG. 1 presents schematical representations of a range of applications of the invention;

15

FIG. 2 is a representation of the perspective distortion concept as exploited in the invention;

20

FIG. 3 is a representation of the division of the invention in subsystems;

FIG. 4 illustrating the data of different subsets and the determination of the translational speed;

25

FIG. 5 is a schematic representation of the general implementations of the present invention;

30

FIG. 6 shows schematically the equivalence of angularly arranged photoreceptors and a system composed of a planar photoreceptor array and a fisheye lens;

FIG. 7 presents three examples of sampling modes on a planar imaging sensor.

35

FIG. 8 is a schematic representation of the preferred embodiment of each of the subsystems with respect to the calculation of the linear speed for each of the subsystems;

FIG. 9 shows an output of a preferred embodiment in terms of its spatio-temporal sensitivity and its velocity dependence as well as in the subfigures the spatio-temporal plots of individual subsystems.

Detailed description of the invention

Translating movements are present in a large variety of occurrences: human bodies, helicopters, airplanes, cars, videogame controls, robots et cetera. An embodiment 1 of the present invention can be placed on each one of these applications.

FIG. 1 shows four examples of applications. 2 is an autonomous helicopter that uses an embodiment 1 of the invention to measure its own translational speed. 3 is a person swimming wearing the embodiment 1 of the invention. 4 is a person playing videogames (e.g., soccer simulation) on a console system 6 that wirelessly receives movement speed from the embodiment 1 of the invention, giving feedback in real-time on a display system 5. 7 and 8 are cars travelling at different speeds, which is measured on 8 by the embodiment 1 of the invention.

The invention makes use of two principles:

- Perspective distortion matching
- Temporal filtering variation

Perspective distortion maps different linear wavelengths (detection lengths) to different angular positions. FIG. 2 shows this principle: from a point-like perspective 11, two objects 9 and 10 having different linear sizes λ_1 and λ_2 can project the same angular size (angle (azimuthal direction) between 12 and 13 for object 9, and angle (azimuthal direction) between 14 and 15 for object 10) according to the sampling azimuth and a perpendicular distance 16

(perpendicular to the direction of the speed vector to be determined).

A set of photoreceptors with identical angular aperture
5 pointed in different azimuthal directions thus samples a wide spectrum of linear wavelengths. Each linear wavelength is mapped onto an azimuthal position.

The invention computes linear velocity using frequencies by
10 means of the formula

$$v = TF/SF$$

where TF and SF are the temporal and spatial frequencies,
15 respectively. The computation is done by matching the spatial filtering with an appropriate temporal filtering; the cutoff frequencies vary thus with the azimuth.

FIG. 3 shows a conceptual overview of the invention. It is
20 composed of a set of subsystems 19, each of which has different spatio-temporal filtering properties. The subsystems use the information 17 from an array of photoreceptors 18 to each compute linear speed in a narrow spatio-temporal frequency band. Combined, these narrow bands provide uniform
25 speed computation capabilities over broad range of frequencies.

Each subsystem 19 is identical, up to the spatial sampling axis, and the temporal filtering properties. The subsystem can
30 be designed according to the performance needs of the final application. FIG. 4 shows the conceptual data form. 20, 21, 22, 23 show the spatio-temporal frequency bands of four subsystems, showing the shift in temporal and spatial sensitivity. Only by summing the sensitivities of these
35 subsystems at 24, the invention provides velocity computing over a broad range of frequencies at 25.

FIG. 5 shows the two general embodiments of the subsystems of the invention. The first subsystem is composed of a set of photoreceptors 26, a preprocessing stage 27, spatial bandpass filters 28, temporal filters 29, directional filters 31, a postprocessing stage 32, and a read-out system 33. It works as follows: the light intensity distribution generated by a translation is captured by the photoreceptors 26, and passed to the preprocessing stage 27 that calibrates and possibly decimates it to reduce the stream of incoming information. The resulting array is hence filtered, first spatially 28, then temporally 29 (or viceversa). The direction of the visual stimulus is determined from the spatio-temporally filtered signal. A postprocessing stage arbitrates the output of the subsystems, and calibrates the speed signal. The result of this general embodiment provides a speed signal using 33 that is dependent on the distance to the moving objects (16 in FIG. 2). For determining the absolute speed, either a fixed reference or a distance sensor can be used.

In the second general embodiment, the distance is computed by combining the spatial and temporal information at 30.

Both the general embodiments can have hardware, software of mixed implementations.

FIG. 6 shows that the required angular spatial sampling (angle between optical axes 34 and 35) can be achieved using angularly-arranged photoreceptors 36 or also a wide-angle fisheye lens 37 over a planar array of photoreceptors 38.

The invention described this far computes the translating speed in one direction. To measure translating speed in different directions requires to appropriately placing the photoreceptor arrays. This can be done by exploiting the perspective distortion principle in different directions. FIG. 7 shows that the image 44 coming through a fisheye lens projects on a planar imaging sensor 42 with a bidimensional

linear array of pixels 43. Sampling along order 45 allows generating different speed sensing modes (examples 39, 40, 41). These modes allow measuring speed in different directions of space, and with different spatial properties because of the optical properties of the lens.

One preferred embodiment (FIG. 8) of the first general embodiment shown in FIG. 5 is composed of eighteen ($n + 2 = 18$) photoreceptors 18 for sixteen identical ($n = 16$), parallel subsystems 19 (processing lines). Each of these sixteen subsystems 19 points radially in a different azimuthal direction of an angular field of view, receiving input from 3 photoreceptors, and performs four scalar operations (wiring diagram shown in FIG. 8).

Three photoreceptors o_1 , o_2 , o_3 in Figure 8 are arranged one next to the other, and sample the light intensity on a narrow aperture (e.g., 5° with $n = 16$), each in three adjacent azimuthal directions of the angular field of view. Each photoreceptor o_1 , o_2 , o_3 receives a signal that can be decomposed, using the Fourier Transform, into:

$$I(t) = I_0 \cdot \sin(2\pi \cdot t \cdot TF + \varphi_x),$$

where I_0 is the Fourier amplitude, TF is the temporal frequency and φ_x is the phase shift between the signals on each photoreceptor o_1 , o_2 , o_3 .

The phase shift φ_x depends on the aperture between photoreceptors $\Delta\varphi$ and the spatial frequency SF :

$$\varphi_x = 2\pi \cdot \Delta\varphi \cdot SF.$$

The inputs 47, 49 from the photoreceptors at the extremes o_1 , o_3 of each subsystem 19 are subtracted at 50 one from another, resulting in a first difference signal s_{13} :

$$s_{13} = o_1 - o_3 = 2\sin(-\phi_x) \cdot \cos(2\pi \cdot t \cdot TF)$$

The amplitude of this first difference signal s_{13} is dependent on the linear spatial frequency content of the input signals, and it peaks at an angular wavelength of 20° : $SF_{a,peak} = 1/4\Delta\phi$. Pointing in different directions, the sub-systems 19 are thus sensitive to different linear wavelengths (as shown in FIG. 9 for different azimuths).

10 The next step is to temporally filter the signal s_{13} , using appropriate cutoff frequencies to match the spatial filtering properties. The resulting signal t_{13} can be obtained using any industrial grade filter (e.g., Bessel or Chebychev) on the signal s_{13} . One simple method to implement the temporal filter
15 for a specific range of speeds is to subtract two temporally phase-shifted signals. Thus, the resulting first difference signal s_{13} from the first stage subtraction 50 is split on two lines, one of which has a temporal delay τ 51. The phase-shifted, split signals are subtracted one from the other to
20 obtain a second difference signal ts_{13} :

$$ts_{13} = s_{13} - \text{delayed } s_{13} = -4\sin(-\phi_x) \cdot \sin(-\tau/2) \cdot \sin(2\pi \cdot t \cdot TF + \tau/2)$$

25 The amplitude of this signal ts_{13} is dependent on the temporal frequency content of the input signals, and it peaks at a temporal period (inverse of the temporal frequency) equal to the amount of temporal delay τ . Each subsystem 19_i has a different temporal delay that matches the spatial
30 characteristics: to create the speed dependent signal, τ must be inversely proportional to the spatial sensitivity. With $\Delta\phi = 5^\circ$, for instance, a velocity-dependent signal is generated using $\tau = 5$ ms for the subsystem 19₁ pointing perpendicularly to the speed vector, with a fixed increase of 0.5 ms for the
35 each of the other subsystems, culminating with $\tau = 13$ ms for the sixteenth subsystem 19₁₆.

The amplitude of the resulting signal from the temporal filtering stage (ts_{13}) is proportional to the speed of the input of the photoreceptors 18_1 to 18_{n+2} . To resolve the ambiguity of direction, and to provide an output under the form of mean offset, the second difference signal ts_{13} is multiplied at 53 by the signal 48 incoming from the central photoreceptor o_2 .

This operation generates the output of a single subsystem sso , whose mean value presents bandpass filtering properties over the spatial and temporal frequency:

$$sso = ts_{13} \cdot o_2 = -2\sin(-\phi_x) \cdot \sin(-\tau/2) \cdot (\cos(\tau/2) - \cos(4\pi \cdot t \cdot TF + \tau/2))$$

The narrow spatio-temporal filtering means that sso is proportional to the linear speed vector in the range of the considered subsystem (not visible in the expression of sso because it describes only part of the result). The maximum value of all subsystems 19_1 to 19_n provides a speed-dependent signal over a broad range of temporal and spatial frequencies. This example implementation is based on a distance reference, which can be used to measure the distances to other objects in the field of view. The dependency of speed on the TF , SF , the distance d , and the azimuth α is visible in:

$$v = TF \cdot d \cdot \arctan(\cos^2\alpha / (d + \cos\alpha \cdot \sin\alpha / SF) / SF)$$

FIG. 9 shows an output of the preferred embodiment. 54 shows its spatio-temporal sensitivity and 55 its velocity dependence. The subfigures below show the spatio-temporal sensitivity plots of individual subsystems, pointing at the indicated azimuths.

Examples

Measuring linear speed visually has many potential technical applications. The flagship application of the passive, visual linear speed sensor (VLSS) is self-control in physical exercises. The effectiveness of physical training for therapy and performance improvement depends on the speed of the movements. Muscle tone, bone strength, and joint wear all require appropriate speeds of execution that vary over the period of exercise. The VLSS can provide the adequate feedback on the execution, allowing the exerciser to adjust its movements for an optimal training. Being independent of physical contact and lightweight, the VLSS for physical training can be used anywhere and without further equipment.

Furthermore, the VLSS has potential applications in the transportation, sport, entertainment, medicine, surveillance, and manufacturing industries. The following is a short list of applications where the introduction of the invention would be useful:

- Using the VLSS on a car allows measuring its absolute speed, and the relative speed of the surrounding traffic (e.g., speed difference between car 7 and 8 in FIG. 1).
- Using the VLSS on professional sports fields allows easier measurement of the movements of the players (e.g., for swimmers, as 3 in FIG. 1) or of other parts of the competition (e.g., ball, discus).
- Using the VLSS in human-machine interfaces allows having a more precise reading of the movements of the body in three dimensions. This information can be used to guide virtual objects for entertainment (e.g., soccer videogame, as played by 4 using console 6 and display 5 of FIG. 1) or rehabilitation purposes.
- Using the VLSS on a small flying robot allows it to move autonomously indoors or when GPS is not available or does not have the required resolution (e.g., autonomous helicopter as in 2 of FIG. 1).

- Using the VLSS in a portable phone or photocamera allows adding speed information to static pictures or video.
- Using the VLSS on rail freight cars allows for higher speed and security when automatically arranging cargo on dead tracks.
- Using the VLSS on manufacturing lines reduces the costs of automation.

Engineering considerations

Hereinafter some information is listed on the engineering of the proposed method and the proposed system. It has to be emphasized that the design of the system has to consider the range of velocity to be measured in order to dimension to size of the azimuthal direction resolution and the appropriate filter characteristics for each of the azimuthal directions. Table 1 below therefore gives an example on the linear spatial resolution as a function of the distance to the object and of the angular azimuthal resolution.

$d/\Delta\phi$	0.1°	1.0°	5.0°	10.0°
0.1 m	0.2	1.8	8.7	17.6
1.0 m	1.8	17.5	87.5	176.3
10.0 m	17.5	174.6	874.9	1763.3

Table 1: spatial resolution (i.e., minimal detectable linear wavelength) in mm for three distances (d) and four angular resolutions ($\Delta\phi$; i.e., size of the photoreceptors). The value is calculated using $l_{min} = d \cdot \tan(\Delta\phi)$

Table 2 illustrates the relationship between the spatial resolution and the temporal resolution. The table 2 shows the translational speed resolution as a function of the temporal frequency filter resolution and of the angular resolution.

$\Delta TF/\Delta\phi$	0.1°	1.0°	5.0°	10.0°
0.1 Hz	0.2	1.8	8.7	17.6
1.0 Hz	1.8	17.5	87.5	176.3
5.0 Hz	8.8	87.3	437.5	881.7

10.0 Hz	17.5	174.6	874.9	1763.3
---------	------	-------	-------	--------

Table 2: speed resolution in mm/s for 4 temporal frequency resolutions (ΔTF), and 4 angular resolutions ($\Delta\phi$), at a distance of 1.0 m. The value is calculated using $v_{min} = \Delta TF \cdot l_{min} = \Delta TF \cdot d \cdot \tan(\Delta\phi)$

5

Maximum measurable speed

The maximum measurable speed depends highly on the specific technology used for the temporal filters. In general, an homogeneous resolution of the measurement at high speeds (i.e., above 3 m/s) calls for higher spatial resolution.

Asymptotical dependence on speed

The formula of the dependency of speed on page 12, line 5:

$$v = TF \cdot d \cdot \arctan(\cos^2\alpha / (d + \cos\alpha \cdot \sin\alpha / SF) / SF)$$

20

is of the form $y = x \cdot \arctan(1/x)$, which is asymptotical over x , and conserves its dependence on the spatial frequency SF . This means that the higher the distance d , the less the computation of translational speed using the invention depends on it.

25

The drawback of this is that it is not sufficient to increase the distance to increase the maximum measurable speed (this would have been the case if d was not contained in the tangent).

30

Partial application of the method

The method can also be only partially applied to measure translating speed. If the distance and the spatial-frequency content of the environment is known, it might be sufficient to

35

use only part of the subsystems: those sensible to the said spatial frequencies at the considered distance. This method can contribute to a fast calculation of the translating speed in terms of evaluating only those signals stemming from a
5 determined region of interest.

Claims

1. A method for determining a linear speed (Δv) of an object, comprising the steps of:

- 5 a) sampling a series of light intensity courses $I(t)$ over the time t ; each light intensity courses $I(t)$ covering a different azimuthal direction (12, 13, 14, 15), each different azimuthal direction (12, 13, 14, 15) thereby defining a detection length (λ_i ; $i=1, \dots, k$) of a series of detection lengths (λ_i) as seen in
10 the direction of the linear speed (Δv) to be determined;
b) transforming the series of detection lengths (λ_i) for the azimuthal directions (12, 13, 14, 15) into a series of linear spatial frequencies (SF_i);
c) defining for each azimuthal direction (12, 13, 14, 15) a
15 band pass or a high pass filter, thereby relating for each detection length (λ_i) the characteristic filter frequencies to the respective linear spatial frequencies (SF_i);
d) filtering the sampled light intensity for each azimuthal direction (12, 13, 14, 15) with the respective band pass or
20 high pass filter to obtain a set of filtered light intensities;
e) calculating the linear speed by dividing the characteristic filter frequencies through the spatial frequencies (SF_i) for at least one of azimuthal directions (12, 13, 14, 15) for which
25 the filtered light intensity exceeds a predefined threshold;
and
f) determining the linear speed by correlating the calculated linear speeds for those azimuthal directions (12, 13, 14, 15) for which the filtered light intensity exceeds a predefined
30 threshold.

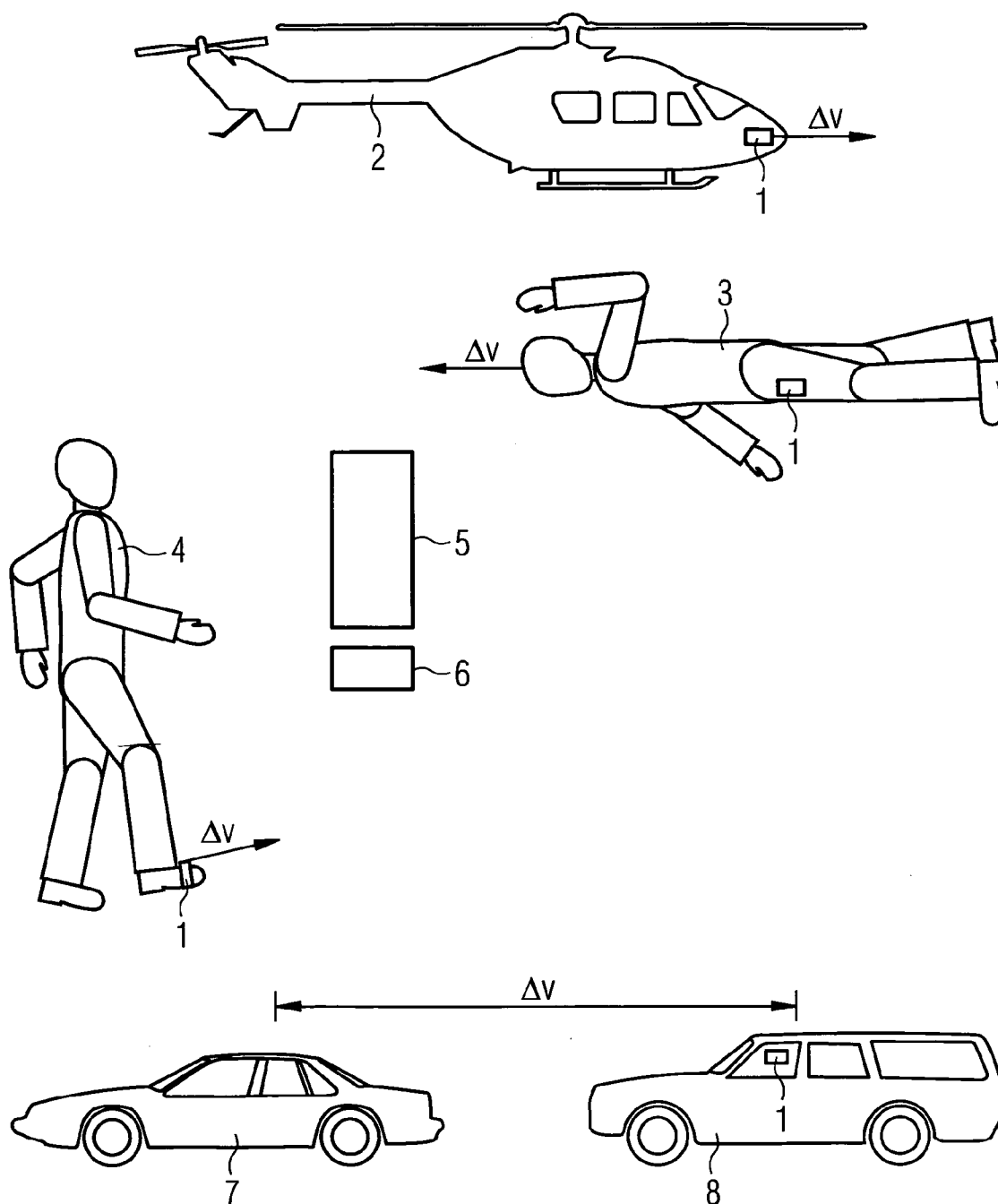
2. The method according to claim 1, wherein each azimuthal direction (12, 13, 14, 15) covers a range of detection lengths ($\lambda_i + \Delta\lambda_i$) yielding a range of linear spatial frequencies (SF_i).

3. The method according to claim 1 or 2, wherein each band pass or high pass filter assigned to an azimuthal direction (12, 13, 14, 15) covers a range of throughput frequencies.

- 5 4. A system for determining a linear speed (Δv) of an object, comprising:
- a) a set of photoreceptors disposed on the object, composed of subsets of 3 photoreceptors; said subset of photoreceptors ($35_i, o_1, o_2, o_3$) measuring light intensities $I(t)$ and being
- 10 arranged to cover identical angular apertures pointing in different azimuthal directions (12, 13, 14, 15), each different azimuthal direction (12, 13, 14, 15) thereby defining a detection length ($\lambda_i; i=1, \dots, k$) of a series of detection lengths (λ) as seen in the direction of the linear
- 15 speed (Δv) to be determined;
- b) means (C) for calculation the linear speed (Δv) for evaluation subsets ($36_j; j=1, \dots, k-1$), each evaluation subset (36_j) comprising the intensity inputs of three adjacent photoreceptors (o_1, o_2, o_3), by performing for at least part of
- 20 the subsets (36_j):
- c) subtracting the light intensities inputs from the two extreme photoreceptors (o_1, o_3) of each evaluation subset (36_j) to receive a first difference signal (s_{13});
- d) splitting the first difference signal (s_{13}) on two lines;
- 25 one line delaying the difference signal (s_{13}) by a temporal delay (τ);
- e) subtracting the signals (s_{13} , delayed s_{13}) from the two lines to receive a second difference signal (ts_{13});
- f) multiplying the second difference signal (ts_{13}) with the
- 30 input from the central photoreceptor (o_2) to achieve an output signal (s_{so}) being indicative for the linear speed (Δv).

1/6

FIG 1



2/6

FIG 2

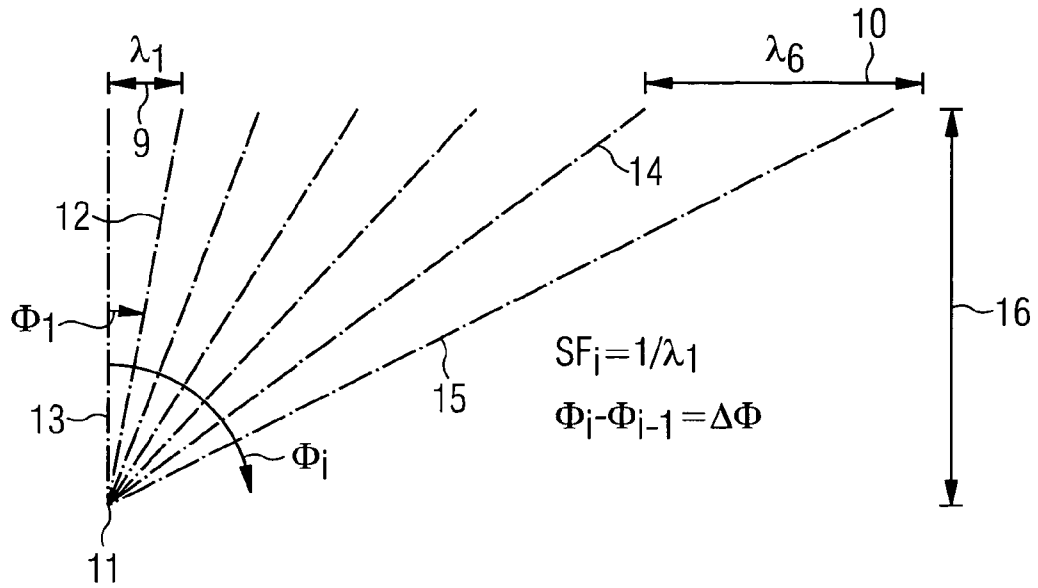
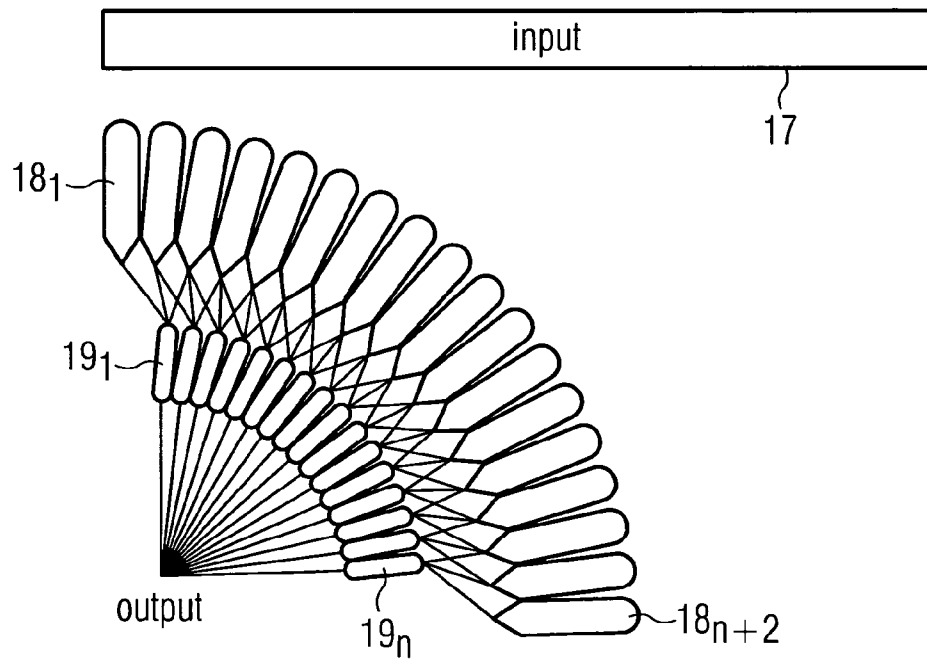
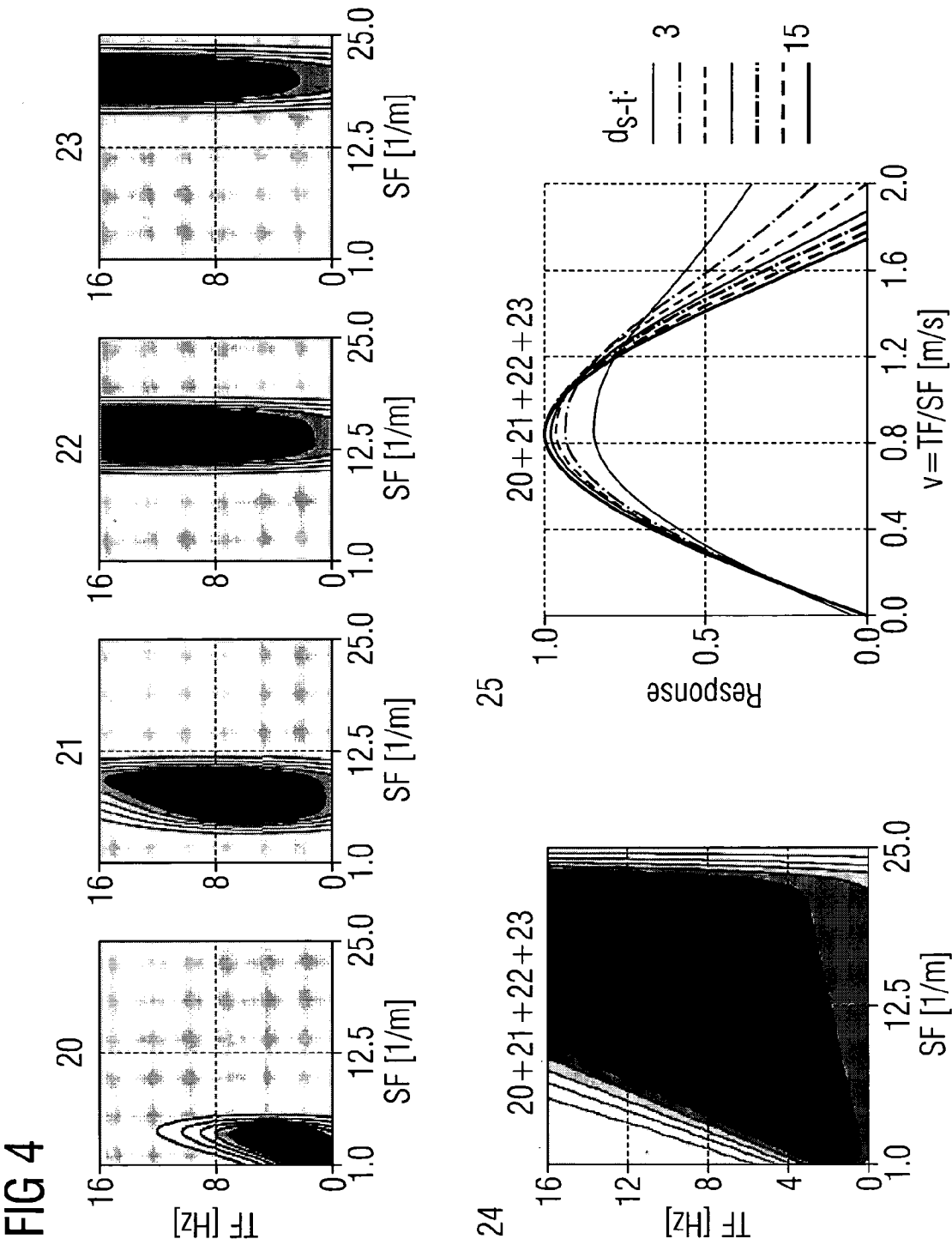


FIG 3





4/6

FIG 5

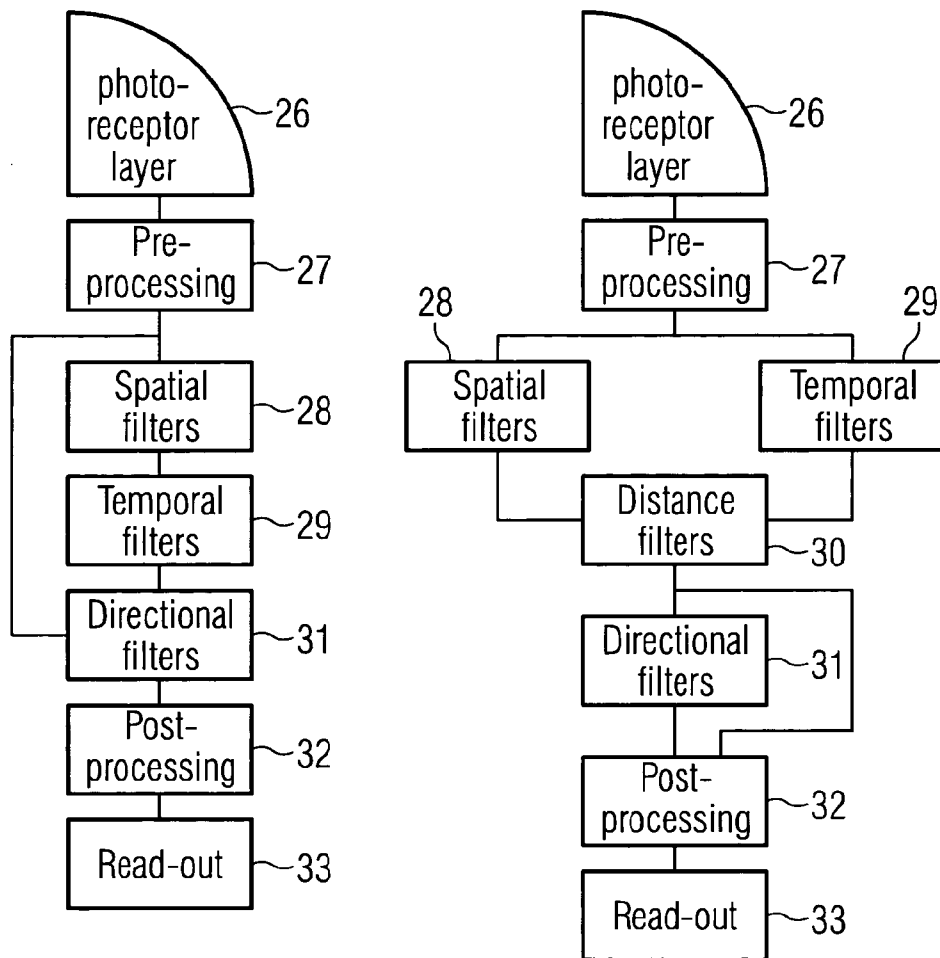
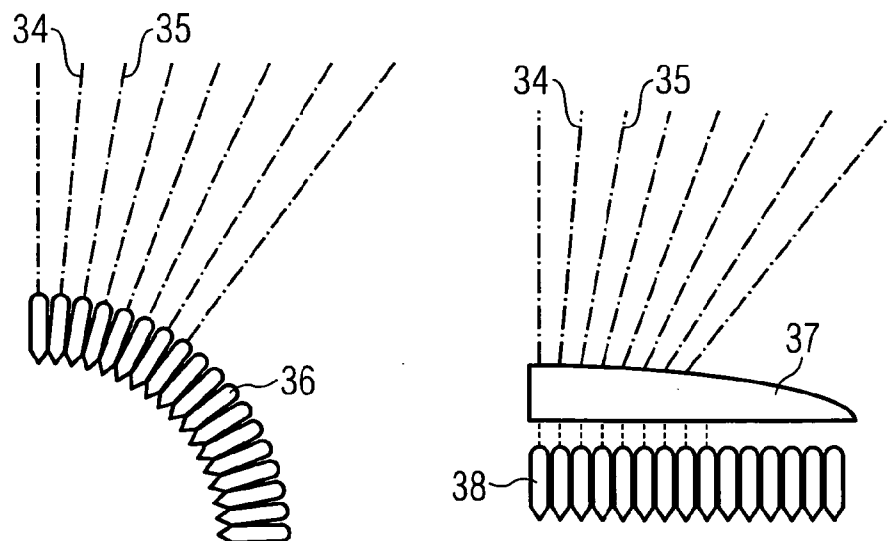


FIG 6



5/6

FIG 7

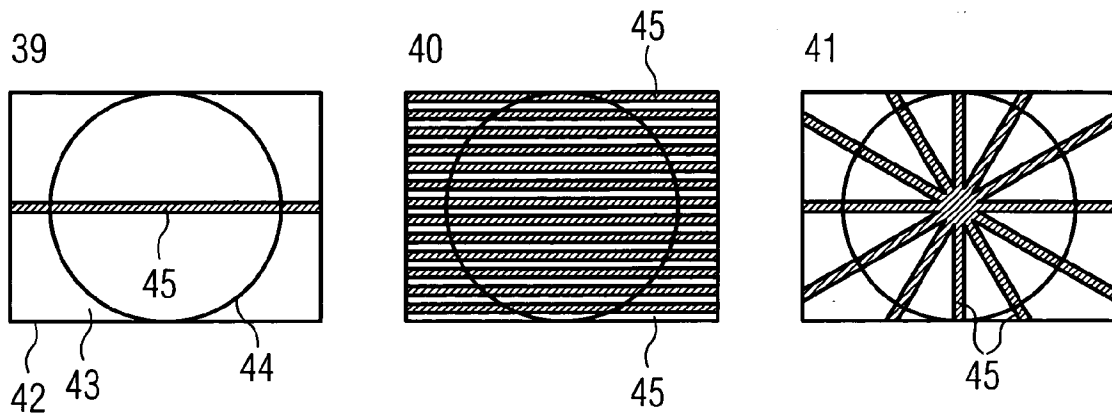
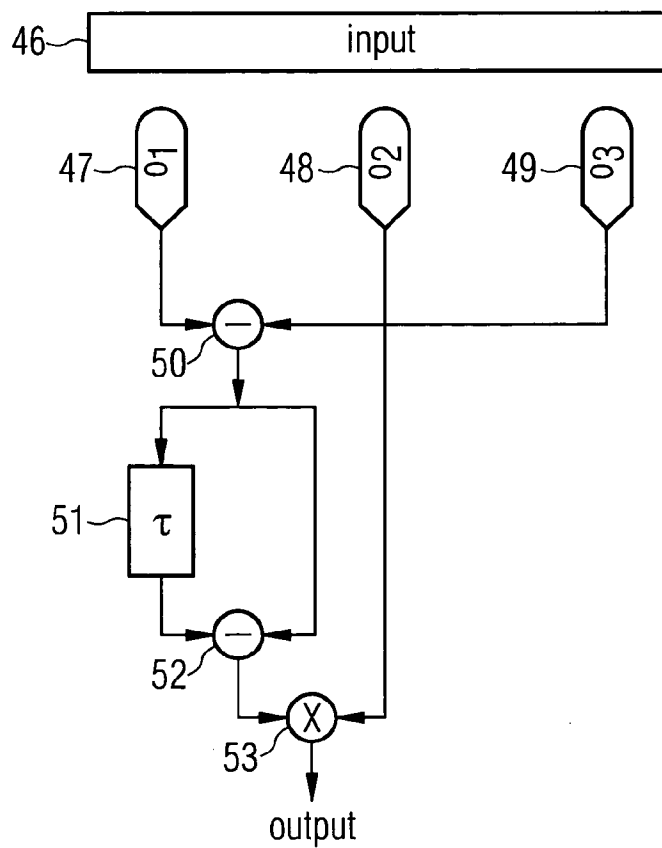
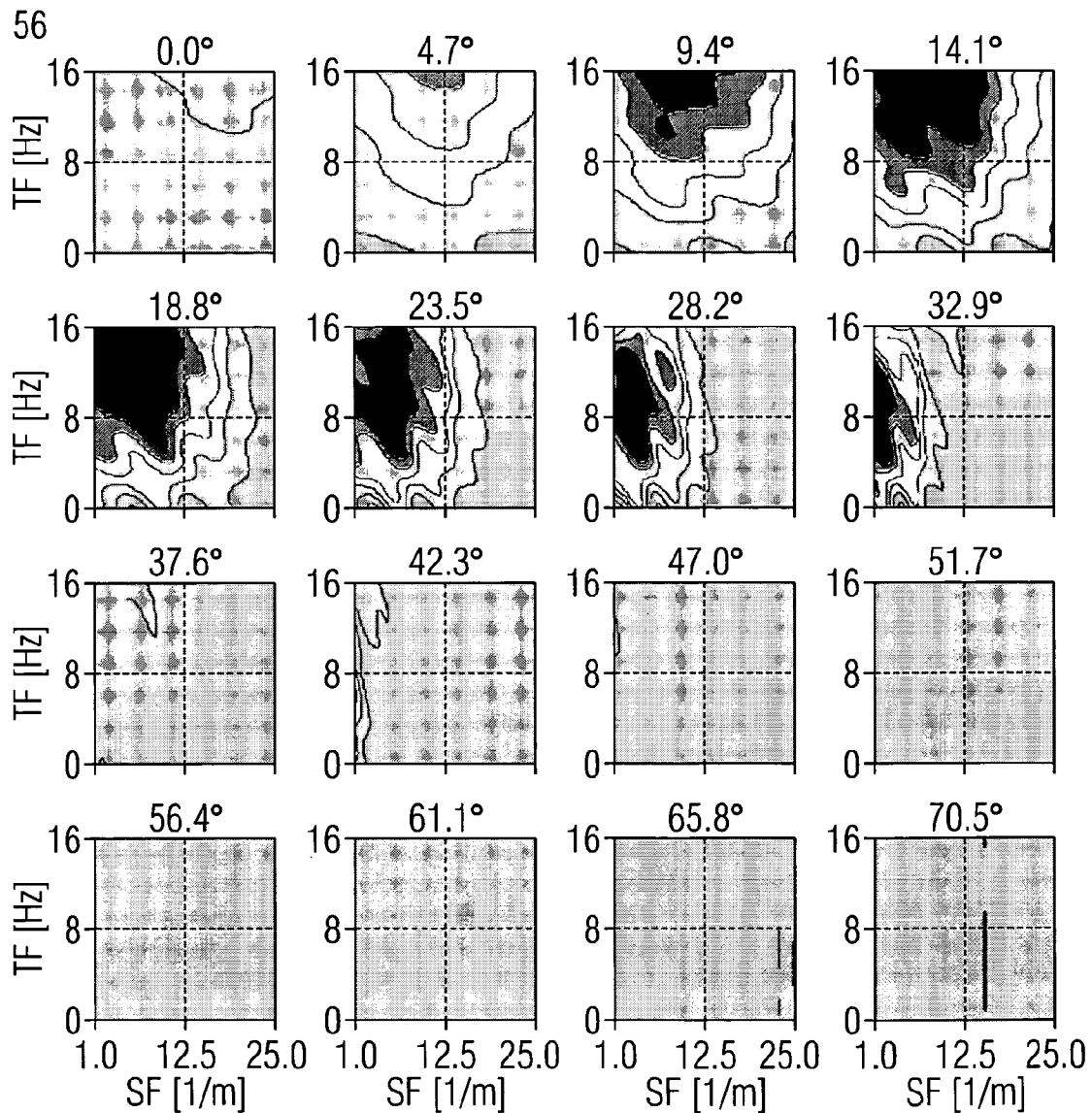
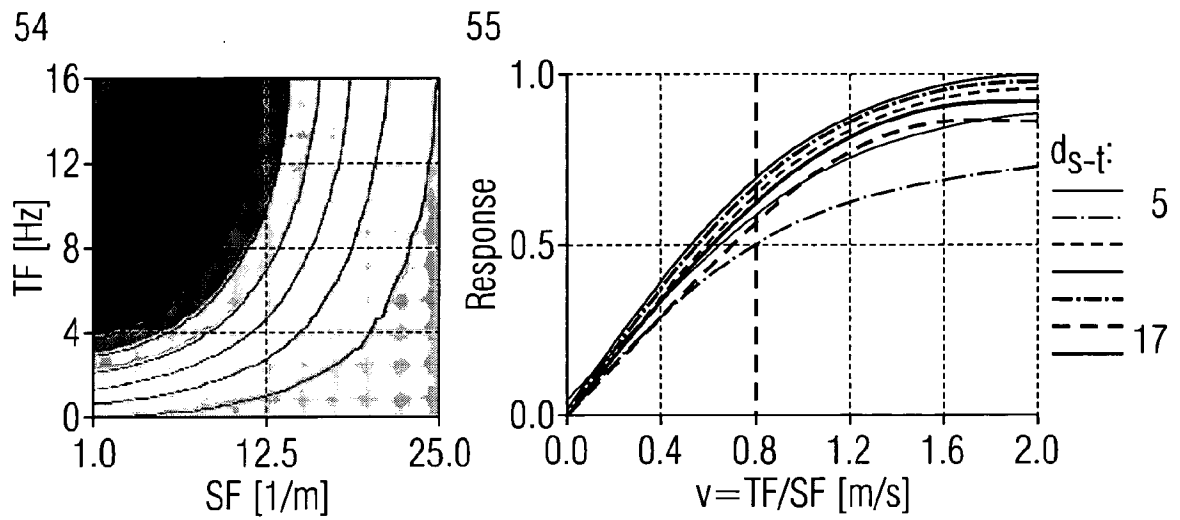


FIG 8



6/6

FIG 9



SUBSTITUTE SHEET (RULE 26)

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2009/067252

A. CLASSIFICATION OF SUBJECT MATTER

INV. G01P3/36 G01P3/50 G06T7/20 G01S11/12

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

G01P G06T G01S

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	GB 2 298 919 A (NIPPON ELECTRIC CO [JP]) 18 September 1996 (1996-09-18) the whole document	1-4
A	US 6 384 905 B1 (BARROWS GEOFFREY L [US]) 7 May 2002 (2002-05-07) the whole document	1-4
A	JP 2000 155125 A (TOYOTA CENTRAL RES & DEV) 6 June 2000 (2000-06-06) abstract	1-4

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

9 March 2010

Date of mailing of the international search report

19/03/2010

Name and mailing address of the ISA/

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040,
Fax: (+31-70) 340-3016

Authorized officer

Reto, Davide

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/EP2009/067252

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
GB 2298919	A	18-09-1996	JP 2780658 B2	30-07-1998
			JP 8248045 A	27-09-1996
			US 5828444 A	27-10-1998
US 6384905	B1	07-05-2002	NONE	
JP 2000155125	A	06-06-2000	JP 3546296 B2	21-07-2004