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(54) IMPROVEMENTS IN AND RELATING TO HYDRAULIC APPARATUS FOR CONTROLLING SUBSEA OIL OR GAS WELL OPERATIONS

(71) We, FMC CORPORATION, a corporation organised and existing under the laws of the State of Delaware, United States of America, of 200 E. Randolph Drive, Chicago, Illinois, United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—

This invention relates to the hydraulic control of a subsea device, and more particularly to hydraulic apparatus for the individual control of a relatively large number of subsea well devices using only a few hydraulic pressure source lines from a surface vessel to the seafloor.

The production of oil and gas from offshore wells has developed into a major endeavour of the petroleum industry. Wells are commonly drilled several hundred or even several thousand feet below the surface of the ocean, substantially beyond the depth at which divers can work efficiently. As a result, the drilling and operating of a subsea well must be controlled from a surface vessel or from an offshore platform. The testing, production and shutting down of the subsea well is regulated by a subsea Christmas tree which is positioned on top of the subsea wellhead. The Christmas tree includes a plurality of valves having operators which are biased to a non-active position by spring returns, and it has been found convenient to actuate these operators by hydraulic fluid which is directly controlled from the surface vessel. For this purpose, a plurality of hydraulic lines are commonly run from the surface vessel to the wellhead to open and close these valves, and to actuate other devices in the well and the wellhead during installation, testing and operating the subsea well equipment, and also during workover procedures being performed on the well.

There is a need for apparatus which can be used to control a large number of subsea operators with only a few hydraulic source lines between the surface vessel and the wellhead.

According to the present invention there is provided apparatus for remote individual control of a plurality of hydraulically-actuated subsea operators using a smaller number of hydraulic lines between a surface control centre

and a subsea device containing said operators, said apparatus comprising a source of hydraulic fluid under pressure, a plurality of hydraulic source lines, a plurality of hydraulic switches, means connecting each of said switches between said source of fluid and a corresponding one of said source lines, a multiple-position valve having a plurality of sections, each of said sections having an inlet port and a plurality of outlet ports, means connecting each of said source lines to a corresponding one of said inlet ports of said valve, and means for connecting each of said subsea operators to a corresponding one of said outlet ports of said valve.

The present invention also provides apparatus for remote individual control of a plurality of hydraulically-operated subsea operators wherein a smaller number of hydraulic lines are contained in a riser extending between a surface control centre and a subsea device containing said operators, said apparatus comprising a hydraulic pump mounted on said control centre, a plurality of hydraulic source lines, a plurality of hydraulic switches mounted on said control centre, each of said switches being connected between said hydraulic pump and a corresponding one of said source lines, a multiple-position valve having a plurality of sections, each of said sections having an inlet port and a plurality of outlet ports, said valve being mounted at the lower end of said riser, said source lines extending through said riser and the lower end of each of said source lines being connected to a corresponding one of said inlet ports of said valve, and means for connecting each of said subsea operators to a corresponding one of said outlet ports of said valve.

According to another aspect, the present invention provides a method for remotely controlling a plurality of hydraulically-actuated subsea devices using a smaller number of hydraulic lines between a surface control centre and a subsea station interconnected to said devices, said method comprising the steps of 1) installing a multiple-section hydraulically-operated valve at said subsea station, each of said sections including an input port and a plurality of output ports, 2) providing control means for selectively switching said valve sections between a plurality of functional positions, 3) connecting each of said valve output ports to a

corresponding one of said devices, 4) connecting a plurality of hydraulic lines between said control centre and said valve with each of said hydraulic lines being connected to a corresponding one of said input ports, and 5) connecting a plurality of hydraulic switches between a source of pressurized hydraulic fluid and said hydraulic lines with each of said switches being connected to a corresponding one of said hydraulic lines.

According to another aspect, the present invention provides a method for remotely and selectively controlling a plurality of hydraulically-actuated subsea devices by means of hydraulic pressure conducted by hydraulic lines extending between a surface control centre and a subsea station, said station including a hydraulically-actuated multiple-section valve, each valve section being movable between a plurality of functional positions, each valve section having an input port and a plurality of output ports with each input port connected to one of said hydraulic lines, and each output port connected to a corresponding one of said devices, and valve control means connected to said valve to change the position of the valve sections in response to a hydraulic signal received from said control centre, said method comprising the steps of 1) conducting a hydraulic signal to said valve control means to move said valve sections to a desired position, 2) directing hydraulic fluid pressure to the input ports of selected valve sections, 3) conducting said hydraulic fluid pressure through said valve sections to selected output ports thereof, and 4) conducting said hydraulic fluid pressure from said selected output ports to their corresponding subsea devices.

The invention will now be particularly described, by way of example, with reference to the accompanying drawings in which:—

Figure 1 is a diagrammatic view, partly in elevation and partly in perspective with portions broken away, of a subsea wellhead system in which the apparatus of the present invention is used.

Figure 2 is a schematic of the switching and valve circuitry of the present invention.

Figures 3A and 3B comprise a table which shows the positions of the valves and switches as related to the various operations at the subsea well.

Figure 4 comprises a table which illustrates the correlation between the operator which is energized, the source line used, and the position of the multiple-position valve.

Figure 5 comprises a table which illustrates the correlation between the function of each subsea operator and the designation number of that operator.

Figures 6A and 6B comprise a schematic of the subsea valve.

Figure 7 is an isometric view of one embodiment of the subsea valve and valve actuator embodying the features of the present inven-

tion.

Figure 8 is an enlarged plan view of a portion of the subsea valve of Figure 7.

Figure 9 is a vertical section taken along line 9-9 of Figure 8.

Figure 10 comprises a schematic of the section of the valve shown in Figure 8.

Figure 11 is a diagrammatic view of a portion of the valve actuator illustrating the positions of the actuator corresponding to different operating modes of the valve.

Figure 12 comprises a schematic of the valve actuator.

Figure 13 comprises a schematic of a mode-indicator section of the subsea valve.

Figure 14 is a horizontal section of the subsea valve with a portion broken away.

Figure 15 is a vertical section taken along line 15-15 of Figure 14.

Figure 16 is a horizontal section taken along line 16-16 of Figure 15.

Figure 17 is a horizontal section taken along line 17-17 of Figure 15.

Figure 18 is a side elevation taken in the direction of the arrows 18-18 of Figure 14.

Figures 1 and 2 diagrammatically illustrate hydraulic apparatus for controlling many valves or other subsea wells while using only a few hydraulic pressure source lines. The present invention is diagrammatically illustrated in Figures 1 and 2 as employed with a completion/workover riser or other type of riser 11 having its upper end connected to a control center 12a on a surface vessel 12, and the riser's lower end connected to a valve container 15 that is mounted on a subsea well Christmas tree diagrammatically illustrated at 10. Within and extending between the valve container 15 and the vessel 12 are a plurality of hydraulic pressure source lines E, F, G, H, I, J, K, L, M, N, O and P (not all shown) and three tubing runs 16a, 16b and 16c. The upper ends of the source lines E-P are each connected to a corresponding one of a plurality of hydraulic switches 17e, 17f, 17g, 17h, 17i, 17j, 17k, 17l, 17m, 17n, 17o and 17p (not all shown), and each of the switches 17e-17p are connected to a hydraulic pump 20 which provides pressurized hydraulic fluid to the source lines when these switches are closed. The lower end of each of the source lines E-P is connected to a corresponding one of a plurality of inlet ports on a pair of multiple-position hydraulic valves 21a, 21b, each valve having a larger number of outlet ports. A plurality of outlet lines 24a-25b (Figures 2, 6a, 6b) are each connected between a corresponding one of the outlet ports of the valves 21a, 21b and one of a plurality of wellhead operators 26a-27b. These operators are used to open and close valves, connect and disconnect tree caps, control pods, etc., and provide installation, testing and operation of the well.

The schematic diagram of Figure 2 discloses hydraulic circuitry for controlling a total of twenty-eight subsea operators using only twelve

hydraulic lines between the hydraulic pump 20 (on the surface vessel) and the valves 21a, 21b (located on the seafloor). It should be noted that some of the outlet ports from the valve 21a are not used, so a few more operators could be controlled by the apparatus if these operators were needed.

The various steps of installing, testing and maintaining a typical subsea wellhead are listed in Figures 3A, 3B where these steps have been grouped together under three modes of operations or groups of steps. Figures 3A and 3B comprise a single chart in which the various operations to be performed are listed in a single column at the left of the chart while across the top of the chart (Figure 3A) are listed the various subsea operators which need to be controlled from the surface vessel. At the intersection of the rows which list the operations and the column which lists the operator is a letter (P,B,E) which indicates that hydraulic pressure or lack of hydraulic pressure is required by the operator during the operation in question. The letter P indicates that the operator requires pressure for a given operation while the letter B indicates that the operator is to be bled or a lack of pressure is required. For example, in step 2, when a subsea tree is being connected, operator 26c must be pressurized and operator 26d must be bled. Some operators may be either pressurized or bled as represented by the letter "E". Due to space limitations on the chart (Figures 3A, 3B) letters are used to represent the various operators which are identified in the function identification list of Figure 5. For example, operator 26a is a control line to the 1 surface controlled subsea safety valve (SCSSV).

The first four steps of the operation listed in the chart (Figures 3A, 3B) include the steps for connecting the subsea tree to the well and for removing plugs from the tubing. These four steps have been labelled "mode A" (Figures 2, 3, 6A, 6B) and the valve sections 30a-30n are in the "A position" during these four steps of operation. Steps 5-12 of the operation (Figure 3A) include the steps for testing the subsea tree and the wellhead after the installation and these steps have been labelled "mode B" (Figures 2, 4, 6A, 6B) and the valve sections 30a-30n are in the "B position" during these steps of the operation. The steps 13-27 (Figure 3B) include the various workover operations; these steps have been labelled "mode C" (Figures 2, 4, 6A, 6B) and the valve sections 30a-30n are in the "C position" during these steps of the operation. The various steps of the operation are controlled directly by the hydraulic switches 17e-17p (Figures 1 and 2) on the surface vessel 12. The modes A, B and C have been used as basis for designing the member of sections and the number of positions needed in the multiple-position valves 21a, 21b.

For example, when the valves 21a, 21b

(Figures 2, 6A, 6B) are in the A position the switch 17f controls the hydraulic power for the operator 26b. At the same time the switch 17g controls the hydraulic power for the operators 26c, 26j, 26k, 26m, 26n, 26p, 26q and 26s. When the valves 21a, 21b are in the B position the switch 17f controls the hydraulic power for the operator 26a and the switch 17g controls the power for the operator 26c only. The control of the other operators at the various positions of the valves may be best seen by referring to Figure 2. The vent or bleed connections of the valve are not shown in Figure 2 in order to more clearly show the hydraulic input control circuitry; however, these vent connections may be seen in Figures 6A, 6B.

The system is preferably vented to sea with liquid from the various vents being discharged directly into the sea. In a vent-to-sea hydraulic system the hydraulic fluid contains a large percentage of water, for example, it may be 95% water. This results in a hydraulic fluid having a specific gravity of approximately 1 so that a pressure balance is achieved at the outlet of the subsea valve. The valve vents may also be connected back to the surface, but this requires at least one additional hydraulic line between the valve and a surface vessel, to return the hydraulic fluid to the hydraulic pump.

Figures 6A, 6B and 7 disclose details of a 3-position, pilot-operated hydraulic valve 21 having a plurality of sections 30a-30n with each section being operable in the three different modes. These sections may be placed end-to-end to form a single valve if the container 15 (Figure 1) is long enough to contain such a valve or these sections may be arranged to form two or more valves. The embodiments disclosed in Figures 1 and 2 connects the sections into a pair of valves 21a and 21b. The various sections 30a-30n of the valves 21a, 21b are shown in more detail in Figures 6A and 6B and with a portion of one of the valves being shown in Figure 7. Each of the valves 21a, 21b includes a pilot section 28 which shifts the valve from one operating position to the next operating position each time that a predetermined minimum pressure is applied to the pilot input line P. Details of the operation of the pilot section will be discussed in connection with the physical construction of the valves as shown in Figures 7-18.

One embodiment of the valve 21 as shown in Figures 7-12 comprises a linear-slide, multiple-section flat valve having external programmable jumpers so that the configuration of the valve can readily be changed. The valve sections 30a-30n are mounted on a base 33 (Figure 7) with the larger section 30n being mounted directly on the base 33 and the smaller sections 30a-30n having a spacer 34 mounted between the base and each of the sections. Each of the sections includes a lower valve block 37 (Figures 7-9) which is connected to the base 33 by a plurality of machine screws 38. Each section

includes a sliding jumper block 40 which is slidably connected to the lower valve block 37 by a dove-tail joint to insure a tight, yet movable fit between the jumper block 40 and the valve block 37.

The lower valve block 37 (Figure 9) includes a plurality of passageways 41a-41n (only a portion of which are shown) which interconnect a plurality of inlet-outlet ports 44a-44n with corresponding ones of a plurality of internal ports 45a-45n. The jumper block 40 (Figure 9) includes a plurality of vertical passageways 47a-47n, only two of which are shown, each connected between an internal port 48a-48n and a corresponding one of a plurality of jumper ports 49a-49n. An annular shear-seal ring 52 and a wave spring 53, both positioned in an annular recess 54 about each of the internal ports 35a-45n, provide a fluid-tight seal between each of the vertical passageways 47a-47n in the jumper block 40, and the corresponding vertical passageways 41b-41c in the valve block 37.

A plurality of programmable jumper lines 57a-57n (Figures 7-10) are connected between the various jumper ports 49a-49n of the jumper block 40 to provide various combinations of connections between the outlet lines *i, p, y* and the source and vent lines L, V1, V2. The ends of the jumper lines 57a-57n are each provided with a tube fitting 58 which is threaded into the upper end of a corresponding one of the jumper ports 49a-49n. The ends of the outlet lines *i, p, y* and the lines L, V1, V2 are each threaded into a corresponding one of the inlet/outlet ports 44a-44n.

The jumper block 40 (Figure 8) can be moved into any one of the modes A, B or C to provide the various combinations of outlet to source and vent connections shown in Figure 10. The jumper blocks 40 are moved from one mode or position to another by an actuator section 28 (Figure 7) that includes a pair of hydraulic cylinders 58a, 58b and a pilot control section 29 having a plurality of switching valves 59a-59d (Figure 12) with each of the valves 59a-59d shown in the deenergized position. The valves 59b, 59c switch from the deenergized position to the energized position whenever a pressure of more than 1000 psi is applied to the pilot line P, and the valves 59a, 59d switch to the energized position whenever a pressure of more than 2000 psi is applied to the same pilot line P.

The hydraulic cylinders 58a, 58b are positioned (Figure 7) at one end of the valve 21 with the cylinder 58b fixed to a spacer 34a by a clevis 61 and pin 62. The cylinder 58a is supported above the spacer 34a by a pair of rods 65a, 65b (Figures 7, 11, 12). The rod 65a interconnects the cylinder 58a and a piston P2 inside the cylinder 58b, and the rod 65b interconnects the sliding jumper block 40n and a piston P1 inside the cylinder 58a. Thus, although the cylinder 58b is fixed relative to

the spacer 34a and the base 33 (Figure 7), the pistons P1, P2 and the cylinder 58a are free to move along the length of the spacer 34a. A plurality of hydraulic lines 66a-66d between the pilot control section 29 and the cylinders 58a, 58b provide the hydraulic power to move the pistons P1, P2. A plurality of rods or connecting links 60 rigidly interconnect the jumper blocks 40 so that each section of the switch is always in the same mode of operation.

When the hydraulic pressure from the surface vessel applied to the source line P (Figures 6A, 7, 12) is somewhat less than 1000 psi, fluid flows through the valve 59a and line 66a to the chamber *a* of the cylinder 58a, forcing the piston P1 (Figure 12) to the right and moving fluid from the chamber *b* through line 66d and the valve 59d to the vent V. At the same time, fluid flows through the valve 59b and line 66b to the chamber *c* of the cylinder 58b, forcing the piston P2 to the right and moving fluid from the chamber *d* through the line 66c and the valve 59c to the vent V. This places both pistons P1, P2 in their fully retracted position, designated mode C in Figure 11, with the jumper blocks 40 (Figures 7, 8) above the right portion of each of the lower valve blocks 37, so that the mode C jumper lines 57a-57c (Figure 8) are connected between the outlet lines *p, i, y*, and the vent and source lines V1, V2, L, respectively.

When the hydraulic pressure from the source line P (Figure 12) is increased to between 1000 psi and 2000 psi the valves 59b and 59c switch to their energized position wherein fluid flows through the valve 59c and line 66c to the chamber *d* of the cylinder 58b, thereby forcing the piston P2 to the left and fluid from the chamber *c* through the line 66b and valve 59b to the vent V. As the piston Ps moves to the left, the rod 65a (Figures 7, 11) is extended from the cylinder 58b, thereby moving the cylinder 58a to the left and the jumper blocks 40 into the mode B as shown in Figures 8, 10, 11.

When the hydraulic pressure from the source line P (Figure 12) is increased to above 2000 psi the valves 59a, 59d are also switched to their energized position wherein fluid flows through the valve 59d and line 66d to the chamber *b* of the cylinder 58a, forcing the piston P1 to the left and moving fluid from the chamber *a* through the line 66a and the valve 59a to the vent V. This extends both the rods 65a, 65b, and moves the jumper blocks 40 into the mode A (Figures 8, 10, 11). Thus, the mode of operation of the linear-slide valve can be controlled from a remote position by applying different hydraulic pressures to the pilot valve 29.

Another embodiment of valve for use in the apparatus of the invention is shown in Figures 13-18 that illustrate a rotary type valve 70 with internal passageways instead of the external jumpers of the first embodiment illustrated in

Figures 7-12. These internal passageways can be drilled or otherwise formed to provide the same passageway system provided by the external jumpers, so that the ultimate function of both valves is the same. The valve 70 comprises a plurality of sections 30a-30n (Figure 18) each having a cylindrical outer housing 67 with a flange 67a (Figures 14, 15) at one end thereof, and a wall 68 that encloses the other end thereof. The wall 68 includes a central bore 68a having an annular shaft 69 rotatably mounted therein. The sections are each bolted to at least one adjacent section by a plurality of bolts 72 (Figures 14, 16-18) extending through bores 73 in the flanges 67a.

Each section (Figures 14, 15) includes an annular rotor 75 mounted between the wall 68 and a cap 76 which is threaded to the upper end of the housing 67. The shaft 69 is rotatably mounted through an annular bore 92 in the center of the cap 76, and the shaft is secured to the rotor 75 (Figure 14) by a key 83. A thrust bearing 77 (Figure 15), positioned in an annular groove 79 in the bottom of the cap 76, provides a bearing surface which rests against the top surface of the rotor 75 to limit upward movement of the rotor. The wall 68 (Figure 15) includes a plurality of passageways 80a-80n which interconnect a plurality of inlet/outlet ports 81a-81n (Figures 14, 15) with corresponding ones of a plurality of internal ports 82a-82n (Figure 15). An annular shearing 52 and a wave spring 53, both positioned in an annular recess 85 about each of the internal ports 82a-82n, provide a fluid-tight seal between each of the vertical passageways 86a-86n in the wall 68, and the corresponding vertical passageways 87a-87n in the rotor 75.

A plurality of horizontal passageways 90a-90n (Figures 14-16) interconnect the various vertical passageways 87a-87n in the rotor 75 and connect other vertical passageways 87a-87n with a chamber 91, between the outer housing 67 and the rotor 75. This chamber 91 is vented to the sea by a vent V (Figure 14) so that only a single vent is needed instead of the pair of vents employed in the embodiment of Figures 7-12. A pair of annular seals 95 (Figure 15) mounted around the shaft 69, and an annular seal 96 mounted between the housing 67 and the cap 76, prevent leakage of fluid from the chamber 91.

The upper end of the shaft 69 (Figure 18) is attached to a mechanism 98 which rotates the multiple-position valve 70 into the positions or modes A, B, C. The mechanism 98 includes a lower ratchet section 99 having a plurality of teeth 99a, and an upper ratchet section 100. The upper ratchet section 100 is biased against the lower ratchet section 99 by a spring 103 which is wound about a shaft 104. The shaft 104 is connected between the upper ratchet section 100 and a spur gear 108 which is connected to a movable rack 108. The rack 108 is connected to a piston 109 by a rod 112 which

is mounted inside a cylinder 113. The piston is biased toward the left end of the cylinder 113 by a spring 114.

Each time the hydraulic cylinder 113 is energized by hydraulic fluid from the pilot input line P, the rack 108 moves toward the right (Figure 18) thereby causing the spur gear 108, the ratchet sections 100, 99, the shaft 69 and each of the rotors 75 (Figure 15) to rotate 120 degrees in a clockwise direction (as viewed from above) with the vertical passageways 87a-87n in the rotors stopping at a position adjacent the vertical passageways 86a-86n in the wall 68 (Figure 15). When the hydraulic cylinder 113 (Figure 18) is deenergized the spring 114 causes the piston 109, the rod 112 and the rack 108 to move to the left and causing the upper ratchet section 100 to rotate counterclockwise. However, the lower ratchet section remains stationary due to the friction between the seals 95 (Figure 15) and the shaft 69 and due to the shape of the teeth on the ratchet sections 99 and 100 which permit the upper ratchet section 100 to rotate counterclockwise while the lower ratchet section 99 remains in a fixed position. Each 120 degree rotation of the shaft 69 causes the valve to change from mode A to mode B, or from mode B to mode C, or from mode C to mode A.

The various connections between the inlet ports and the outlet ports can be seen in Figures 2, 6a and 6b. For example, when the valve is in mode A, in section 30b of the valve the inlet line F is connected to the outlet line 24b and to the operator 26b. When the valve is moved into mode B, the inlet line F is connected to the outlet line 24a and to the operator 26a. The section 30n (Figures 2, 6b) of the valve connects all of the operators 26j, 26k, 26m, 26n, 26p, 26q and 26s in parallel when the valve is in mode A so that power to these operators is all controlled by the switch 17g. In the B and C modes of the valve, each of these operators is controlled by an individual one of the switches 17j-17p. It may be noted that the "B" and "C" portions of the 30n section of the valve are identical, but both portions are needed as all of the sections of the valve change from mode B to mode C when the pilot valve causes the rotors 75 (Figure 16) to rotate from position B to position C.

The details of the connections for one of the sections of the rotary switch can be seen in Figures 10, 14, 16 and 17. As shown in the mode A, the inlet line K is connected to the outlet line i by the horizontal passageways 80c, 90h, 80b (Figure 14) and the vertical passageways 86c, 86h (Figure 17), 87h, 87c (Figure 16). The inlet/outlet line p is connected to the vent V by the horizontal passageways 80a (Figures 14, 15, 17), 90a (Figures 14-16), the vertical passageways 86a (Figures 15, 17), 87a (Figures 15, 16) and the chamber 91 (Figures 14-16). In the mode B, the rotor 75 (Figure 16) is moved 120 degrees clockwise from the position shown in

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Figure 16 so that the inlet line K is connected to the inlet/outlet line *p* by the horizontal passageways 80a, 80c (Figure 17), 90c (Figures 15-16) and the vertical passageways 86a, 86c (Figure 17), 87e, 87d (Figures 15-16).

5 A mode-indicator section 117 of the rotary switch 21 as disclosed in Figure 13 provides means for remotely checking the position or mode in which the switch of Figures 14-18 is  
 10 operating. The mode-indicator section 117 includes a plurality of pressure-relief valves 118a-118c and a valve section 30y (Figure 13) which is preferably connected to the lower end of the shaft 69 (Figure 18) although the section 30y  
 15 could be connected anywhere along the length of the shaft. Each of the pressure-relief valves (Figure 13) prevents the pressure drop across the valve from exceeding the value shown in the Figure 13. For example, the maximum pressure  
 20 drop between the inlet port 119a and the vent port V of the valve 118a is 1500 psi.

Each of the pressure-relief valves 118a-118c is connected to the source line P in a corresponding one of the modes A, B, C and prevents  
 25 the pressure in the source line P from raising above the pressure drop across the relief valve. A pressure gauge (not shown) mounted on the surface vessel 12 (Figure 1) and connected to the line P is used to indicate the pressure on the  
 30 line P and thereby indicate the mode of operation of the rotary switch 21. When the pressure in the source line P increases above 750 psi, the piston 109 (Figures 13, 18) moves the rack 108, spur gear 107 and the shaft 69 a total of 120  
 35 degrees so that the rotary switch moves into one of the modes A, B or C and connects one of the pressure-relief valves to the source line P. For example, in mode B (Figure 13) the pressure-relief valve 118b is connected to the  
 40 source line P through the valve section 39y so that the pressure in the source line P cannot increase above 2000 psi. In mode A the pressure-relief valve 118a is connected to the line P so that the pressure in the source line P cannot  
 45 increase above 1500 psi and in mode C the valve 118c is connected to the line P and the pressure in the line P cannot increase above 2500 psi.

The present invention provides a means for  
 50 controlling the operation of a relatively large number of subsea operators while using a much smaller number of hydraulic control lines between a surface vessel or a surface platform and a multiple-position subsea valve which is positioned near the subsea operators. The multiple-  
 55 position valve has a plurality of sections with each section having an input port, a vent port and a plurality of output ports. Connected between each of the input ports and a source of hydraulic power on the surface vessel is a source line having a hydraulic switch connected therein. A separate subsea operator may be individually controlled by a corresponding one of the hydraulic switches at each position of the  
 60 subsea valve.  
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Certain features of the apparatus described herein form the subject of our copending patent applications Nos. 23272/78 and 26051/80. serial no's 1 601 582 and 1 601 583

WHAT WE CLAIM IS:

1. Apparatus for remote individual control of a plurality of hydraulically-actuated subsea operators using a smaller number of hydraulic lines extending between a surface control center and a subsea device containing said operators, said apparatus comprising
  - a source of hydraulic fluid under pressure,
  - a plurality of hydraulic source lines,
  - a plurality of hydraulic switches,
  - means connecting each of said switches between said source of fluid and a corresponding one of said source lines,
  - a multiple-position valve having a plurality of sections, each of said sections having an inlet port and a plurality of outlet ports,
  - means connecting each of said source lines to a corresponding one of said inlet ports of said valve, and
  - means for connecting each of said subsea operators to a corresponding one of said outlet ports of said valve.
2. Apparatus for remote individual control of subsea operators as claimed in Claim 1 including means for mounting said multiple-position valve to said subsea device, and means for mounting said hydraulic switches at said surface control center.
3. Apparatus for remote individual control of subsea operators as claimed in Claim 1 wherein said means for connecting each of said subsea operators to said outlet ports of said valve includes a plurality of outlet lines each connected between one of said operators and a corresponding one of said outlet ports.
4. Apparatus for remote individual control of subsea operators as claimed in any preceding claim wherein each of said inlet ports is connected to a corresponding outlet port being connected to a different outlet port at each of the different positions of said valve.
5. Apparatus for remote individual control of subsea operators as claimed in any preceding claim wherein said multiple-position valve includes a pilot port, and wherein the valve position is changed each time a predetermined value of pressure is applied to said pilot port.
6. Apparatus for remote individual control of subsea operators as claimed in Claim 5 wherein a sequence of pulses of pressure applied to said pilot port causes said multiple-position valve to dequentially move through a predetermined series of valve positions.
7. Apparatus for remote individual control of subsea operators as claimed in any preceding claim wherein said multiple-position valve includes a cylindrically-shaped rotary portion having a plurality of passageways therein, each of said passageways being connected between one of said inlet ports and a corresponding one of said outlet ports when said rotary portion is

stopped at one of said multiple positions.

8. Apparatus for remote individual control of subsea operators as claimed in Claim 7, wherein a different set of passageways is connected to said inlet ports at each of the different positions of said rotary portion of said valve, and a different set of outlet ports is connected to said passageways at each of the different positions of said rotary portion of said valve.

9. Apparatus for remote individual control of subsea operators as claimed in Claim 1 wherein each of said sections of said multiple-position valve includes a lower valve block having a plurality of inlet/outlet ports, a plurality of internal valve ports and a plurality of passageways interconnecting each of said internal valve ports with a corresponding one of said inlet/outlet ports, a jumper block having a plurality of jumper ports, a plurality of internal ports and a plurality of passageways interconnecting each of said internal ports with a corresponding one of said jumper ports, a plurality of programmable jumper lines, means for connecting each end of said jumper lines to a selected pair of said jumper ports to selectively interconnect said passageways in said jumper block, and means mounting said jumper block in slocing contact with said lower valve block to interconnect said internal valve ports with corresponding ones of said internal ports in said jumper block.

10. Apparatus for remote individual control of a plurality of hydraulically-operated subsea operators wherein a smaller number of hydraulic lines are contained in a riser extending between a surface control centre comprising a hydraulic pump mounted on said control centre, a plurality of hydraulic source lines, a plurality of hydraulic switches mounted on said control centre, each of said switches being connected between said hydraulic pump and a corresponding one of said source lines, a multiple-position valve having a plurality of sections, each of said sections having an inlet port and a plurality of outlet ports, said valve being mounted at the lower end of said riser, said source lines extending through said riser and the lower end of each of said source lines being connected to a corresponding one of said inlet ports of said valve, and means for conencting each of said subsea operators to a corresponding one of said outlet ports of said valve.

11. Apparatus for remote individual control of subsea operators as claimed in Claim 10 wherein said outlet ports are divided into a plurality of groups, each of said inlet ports being coupled to a corresponding one of said outlet ports in a first group when said multiple-position valve is in a first position and each of said inlet ports being coupled to a corresponding one of said outlet ports in a second group when said multiple-position valve is in a second position.

12. Apparatus for remote individual control of subsea operators as claimed in Claim 10 or

Claim 11 wherein said multiple-position valve includes a pilot port and means for changing the valve position each time a pressure is applied to said pilot port of said valve.

13. Apparatus for remote individual control of subsea operators as claimed in Claim 12 including a pilot control switch mounted on said control centre said pilot control switch being connected between said hydraulic pump and said pilot port.

14. Apparatus for remote individual control of subsea operators as claimed in Claim 12 or Claim 13 wherein said valve is moved through a predetermined sequence of valve positions in response to a series of pressure pulses applied to said pilot port.

15. A method for remotely controlling a plurality of hydraulically-actuated subsea devices using a smaller number of hydraulic lines between a surface centre and a subsea station interconnected to said devices said method comprising the steps of

1) installing a multiple-section hydraulically-operated valve at said subsea station, each of said sections including an input port and a plurality of output ports,

2) providing control means for selectively switching said valve sections between a plurality of functional positions,

3) connecting each of said valve output ports to a corresponding one of said devices,

4) connecting a plurality of hydraulic lines between said control centre and said valve with each of said hydraulic lines being connected to a corresponding one of said input ports, and

5) connecting a plurality of hydraulic switches between a source of pressurized hydraulic fluid and said hudraulic lines with each of said switches being connected to a corresponding one of said hydraulic lines.

16. A method for remotely and selectively controlling a plurality of hydraulically-actuated subsea devices by means of hydraulic pressure conducted by hydraulic lines extending between a surface control centre and a subsea station, said station including a hydraulically-actuated multiple-section valve, each volve section being movable between a plurality of functional positions, each output ports with each inpur port connected to one of said hydraulic lines, and each output port connected to a corresponding one of said devices, and valve control means connected to said valve to change the position of the valve sections in response to a hydraulic signal received from said control centre, said method comprising the steps of

1) conducting a hydraulic signal to said valve control means to move said valve sections to a desired position,

2) directing fluid pressure to the input ports of selected valve sections,

3) conducting said hydraulic fluid pressure through said valve sections to selected output ports thereof, and

4) conducting said hydraulic fluid pressure

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from said selected output ports to their corresponding subsea devices.

17. A method as claimed in Claim 16 including the step of bleeding hydraulic fluid  
5 pressure from selected subsea devices by conducting said pressure from said devices to their corresponding valve sections and thence to a reduced pressure atmosphere.

18. A method and apparatus for hydraulic-

ally controlling subsea well equipment substantially as hereinbefore described with reference to the accompanying drawings. 10

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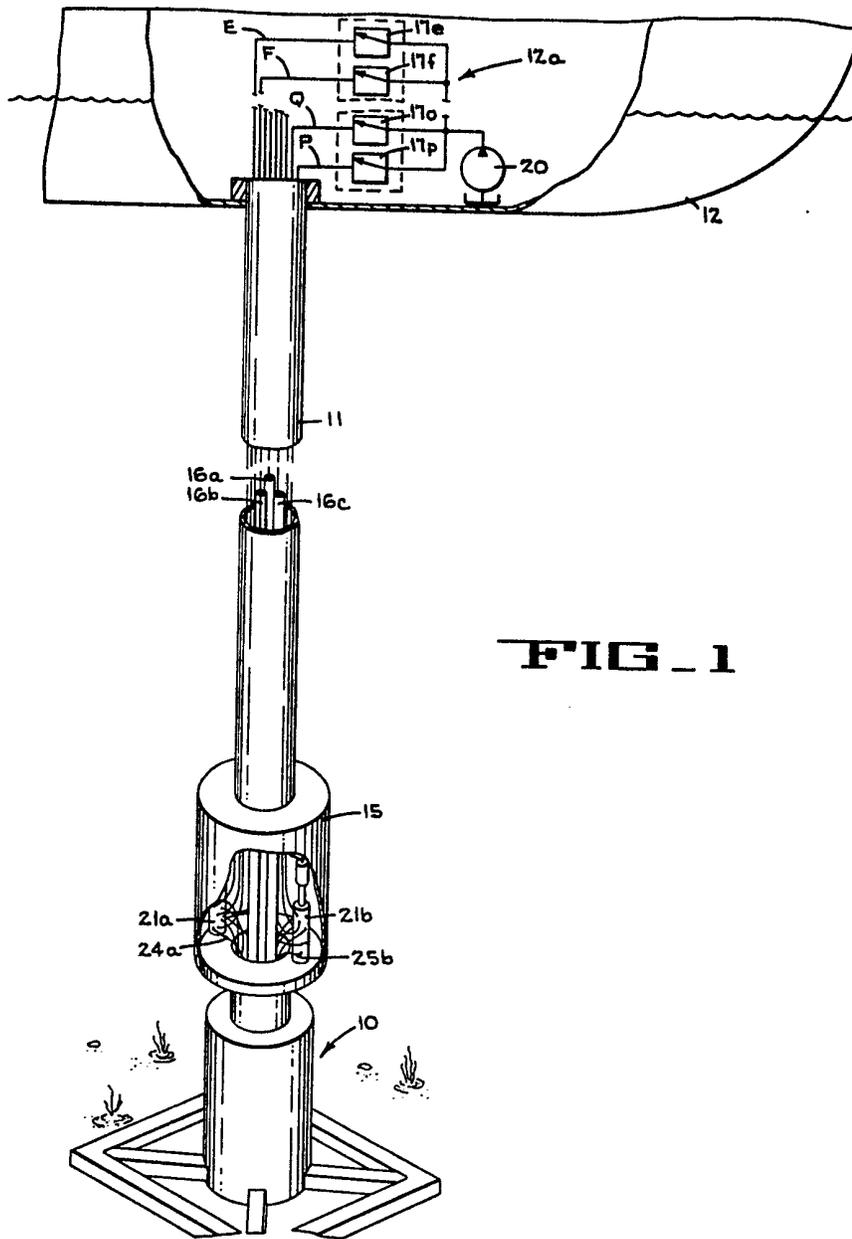
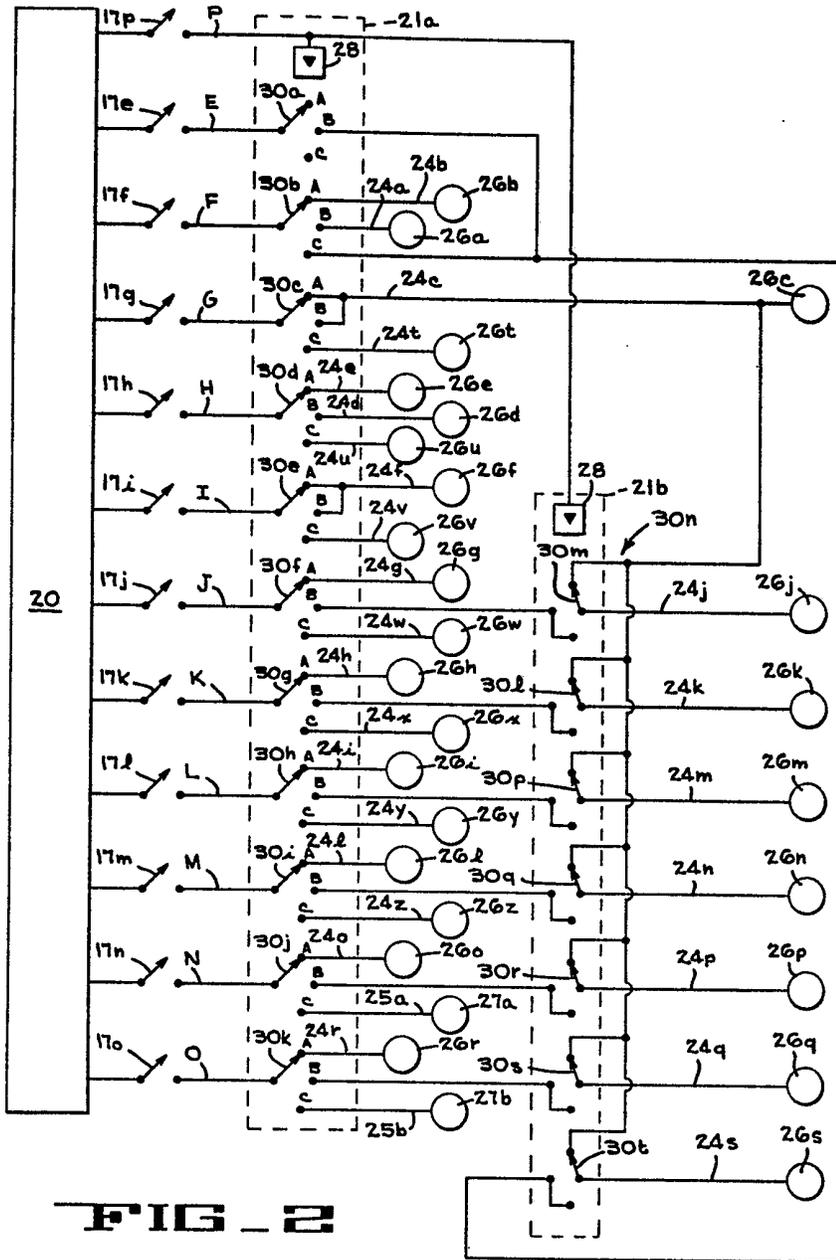


FIG. 1





**FIG-3B**

- 13. CLOSE TREE B<sub>2</sub> B<sub>2</sub> B B<sub>2</sub> B<sub>2</sub> B B B B B B B B B B B B P B B P B B E E E B B B B
- 14. RELEASE TREE B<sub>2</sub> B<sub>2</sub> B B<sub>2</sub> B<sub>2</sub> B B B B B B B B B B B B P E E E P B B B P  
 RUNNING TOOL B<sub>2</sub> B<sub>2</sub> B B B B B B B B B B B B P E E E P B B B P
- 15. STROKE UP B B B B B B B B B B B B B B B B P E E E P B B E B<sub>3</sub>
- 16. STROKE DOWN B B B B B B B B B B B B B B B B P E B B P B B B P
- 17. LATCH ONTO TREE CAP OR POD B B B B B B B B B B B B B B B B P B B B P B B B P
- 18. UNLATCH CAP OR POD (GRAB RELEASE FAN) B B B B B B B B B B B B B B B B P B<sub>4</sub> B<sub>4</sub> P<sub>4</sub> P<sub>4</sub> B B P
- 19. UNLOCK CAP OR POD B B B B B B B B B B B B B B B B P B<sub>5</sub> P<sub>5</sub> B<sub>5</sub> B B P
- 20. STROKE UP W/ CAP OR POD B B B B B B B B B B B B B B B B P B B P B B B E B<sub>3</sub>
- 21. STROKE UP W/ CAP OR POD B B B B B B B B B B B B B B B B P B B P B B B B P
- 22. LATCH CAP OR POD B B B B B B B B B B B B B B B B P B<sub>6</sub> B<sub>6</sub> P<sub>6</sub> B B P
- 23. RELEASE CAP OR POD B B B B B B B B B B B B B B B B P B B B P B B B P
- 24. RELEASE FM CAP OR POD (SAME AS #14) B<sub>2</sub> B<sub>2</sub> B B B B B B B B B B B B P E E E P B B B P
- 25. RELEASE FLOW-LINE & ELECT. CONNECTOR B B B B B B B B B B B B B B B B P B B E E B B B B
- 26. REENTRY RELEASE TOOL B B B B B B B B B B B B B B B B P E E E B P<sub>7</sub> P<sub>7</sub> B
- 27. TREE RUNNING TOOL STAB HOLD B B B B B B B B B B B B B B B B P E B B B B B B E

## FIG. 5

### FUNCTION IDENTIFICATION

OPERATOR #	OPERATOR FUNCTION
26a	SCSSV #1, CONTROL LINE
26b	SCSSV #1, BALANCE LINE
26c	SCSSV's, ONE INCH VALVES
26d	SCSSV #2, CONTROL LINE
26e	SCSSV #2, BALANCE LINE
26f	TREE CONNECTOR LOCK
26g	TREE CONNECTOR UNLOCK
26h	TREE CONNECTOR SECONDARY UNLOCK
26i	TREE CONNECTOR TEST (1" VALVE PORTING TO ANNULUS RUN)
26j	LOWER MASTER #1
26k	LOWER MASTER #2
26l	LOWER MASTER ANNULUS
26m	UPPER MASTER #1
26n	UPPER MASTER #2
26o	UPPER MASTER ANNULUS
26p	SWAB VALVE #1
26q	SWAB VALVE #2
26r	SWAB VALVE ANNULUS
26s	RUNNING TOOL LATCH
26t	RUNNING TOOL UNLATCH
26u	RUNNING TOOL SECONDARY UNLATCH
26v	TREE CAP AND CONTROL POD ACTUATION LOCK
26w	TREE CAP AND CONTROL POD ACTUATION UNLOCK
26x	TREE CAP AND CONTROL POD ACTUATION TOOL RELEASE
26y	TREE CAP AND CONTROL POD ACTUATION TEST
26z	REENTRY TOOL RELEASE
27a	REENTRY TOOL HYDRAULIC CYLINDER UP
27b	REENTRY TOOL HYDRAULIC CYLINDER DOWN

# FIG. 4

(numbers not shown are vented to sea)

Mode A

SURFACE ACCESS NECESSARY TO OPERATOR:

ACCESS ACHIEVED THROUGH SOURCE LINE

26c	-----	G
26j	-----	G
26k	-----	G
26l	-----	M
26m	-----	G
26n	-----	G
26o	-----	N
26p	-----	G
26q	-----	G
26r	-----	G
26s	-----	O
26b	-----	F
26e	-----	H
26f	-----	I
26h	-----	J
26i	-----	K
	-----	L

{ 26c, 26j, 26k, 26l, 26m, 26n, 26o, 26p, 26q, 26r } PRESSURE ALL TIME DURING THIS MODE.

Mode B

SURFACE ACCESS NECESSARY TO OPERATOR:

ACCESS ACHIEVED THROUGH SOURCE LINE

26a	-----	F
26c	-----	G
26f	-----	I
26s	-----	E
26d	-----	H
26j	-----	J
26k	-----	K
26m	-----	L
26n	-----	M
26p	-----	N
26q	-----	O

{ 26a, 26c, 26f, 26s } PRESSURE ALL TIME DURING THIS MODE.

Mode C

SURFACE ACCESS NECESSARY TO OPERATOR:

ACCESS ACHIEVED THROUGH SOURCE LINE

26s	-----	F
26t	-----	G
26u	-----	H
26v	-----	I
26w	-----	J
26x	-----	K
26y	-----	L
26z	-----	M
27a	-----	N
27b	-----	O

**FIGS**

## FUNCTION IDENTIFICATION

OPERATOR #	OPERATOR FUNCTION
26a	SCSSV #1, CONTROL LINE
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26l	LOWER MASTER ANNULUS
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26p	SWAB VALVE #1
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26r	SWAB VALVE ANNULUS
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26t	RUNNING TOOL UNLATCH
26u	RUNNING TOOL SECONDARY UNLATCH
26v	TREE CAP AND CONTROL POD ACTUATION LOCK
26w	TREE CAP AND CONTROL POD ACTUATION UNLOCK
26x	TREE CAP AND CONTROL POD ACTUATION TOOL RELEASE
26y	TREE CAP AND CONTROL POD ACTUATION TEST
26z	REENTRY TOOL RELEASE
27a	REENTRY TOOL HYDRAULIC CYLINDER UP
27b	REENTRY TOOL HYDRAULIC CYLINDER DOWN

FIG. 6A

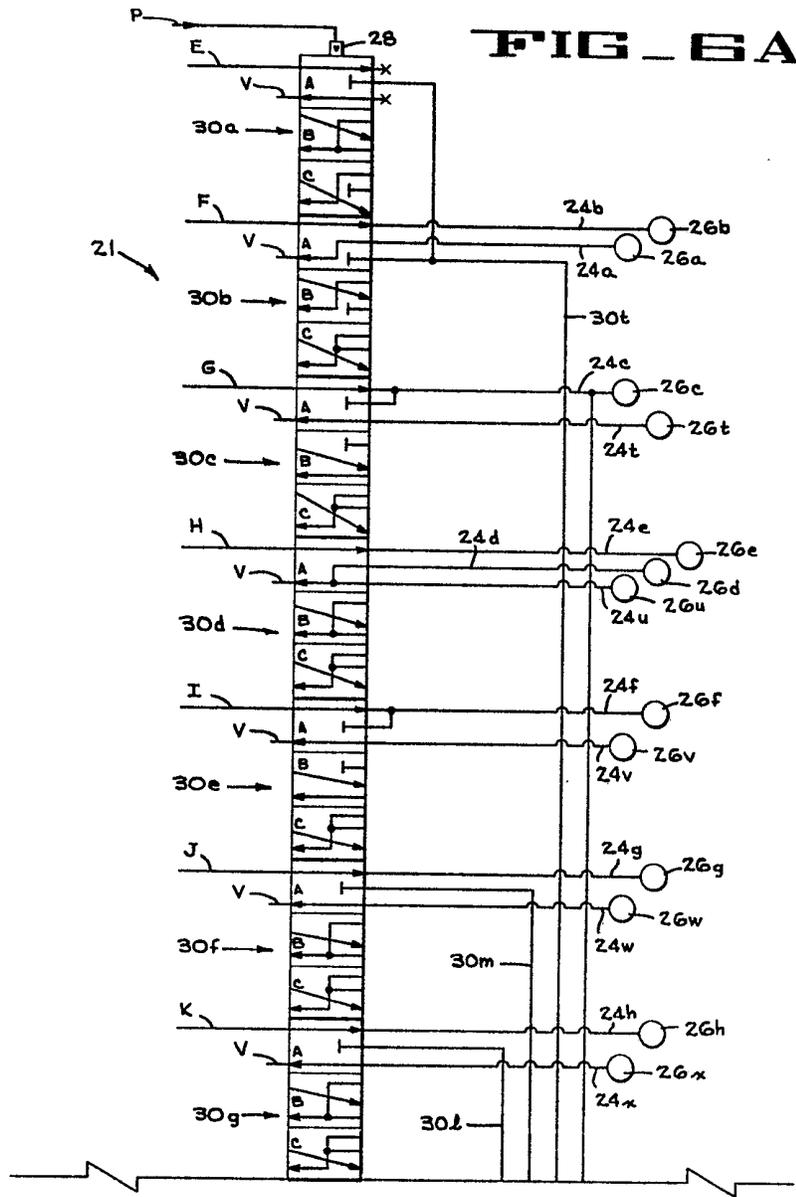


FIG. 6B

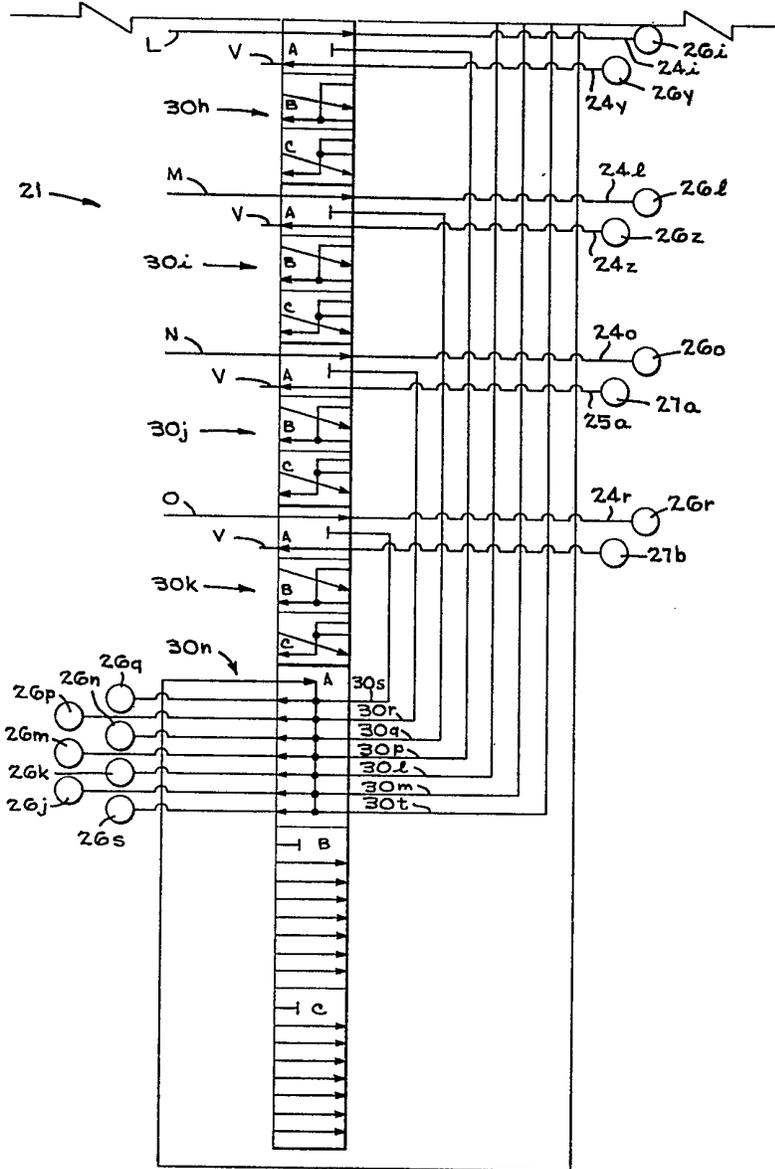
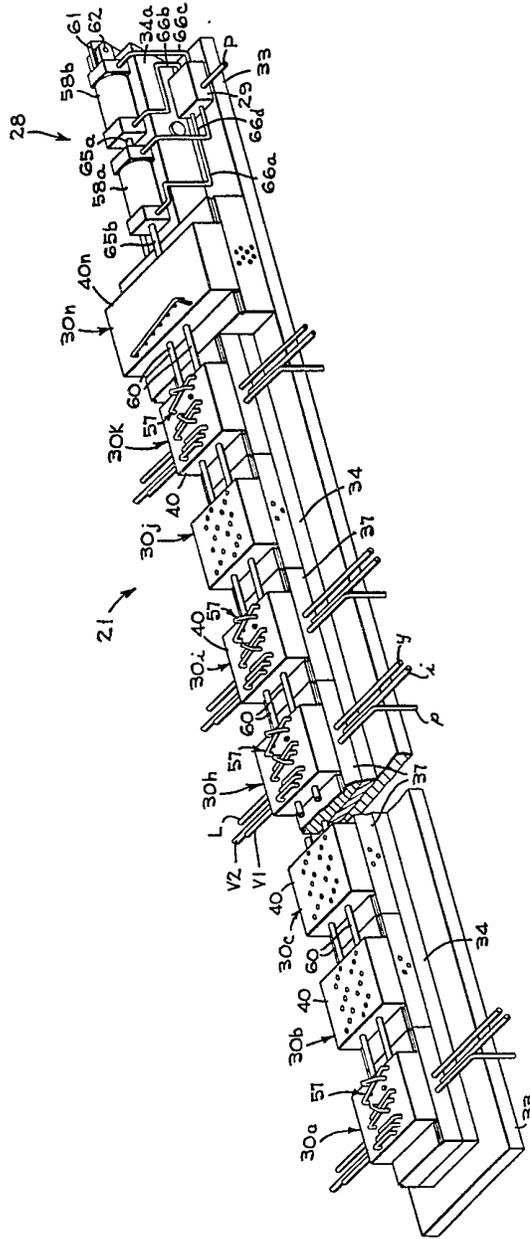
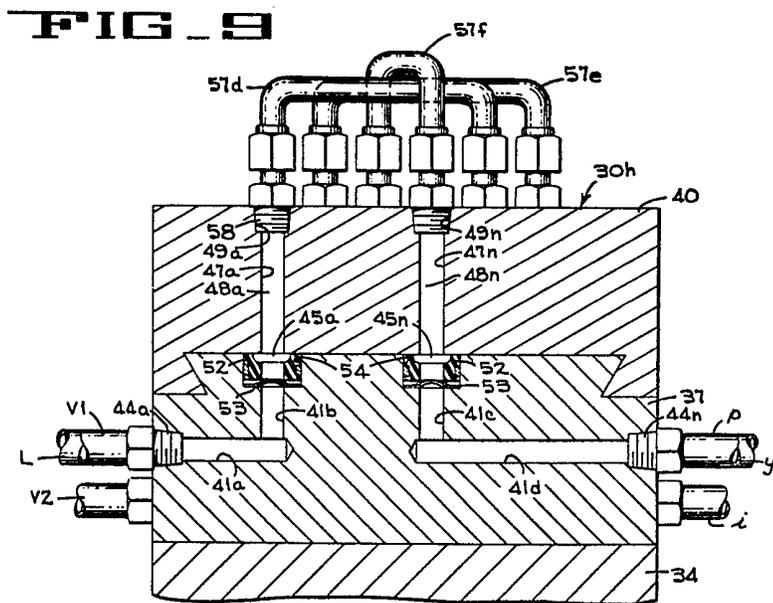
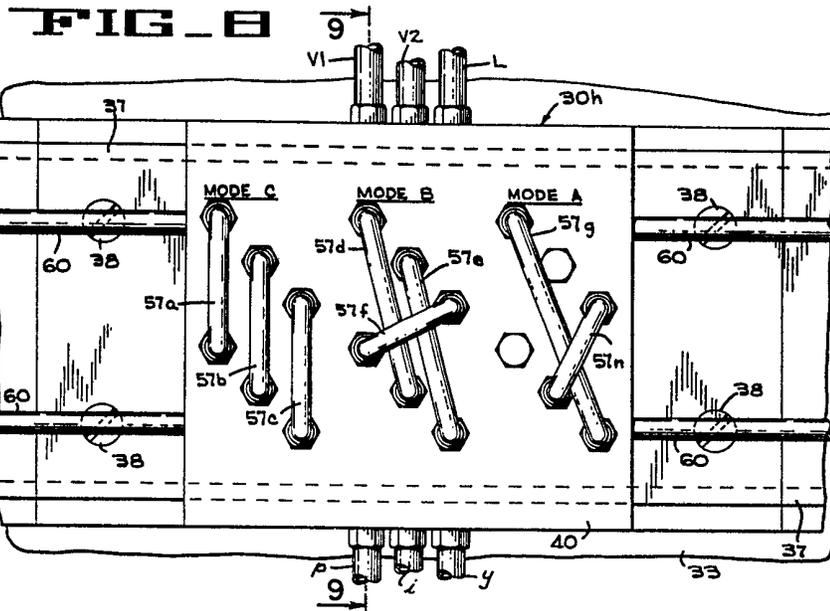


FIG. 7





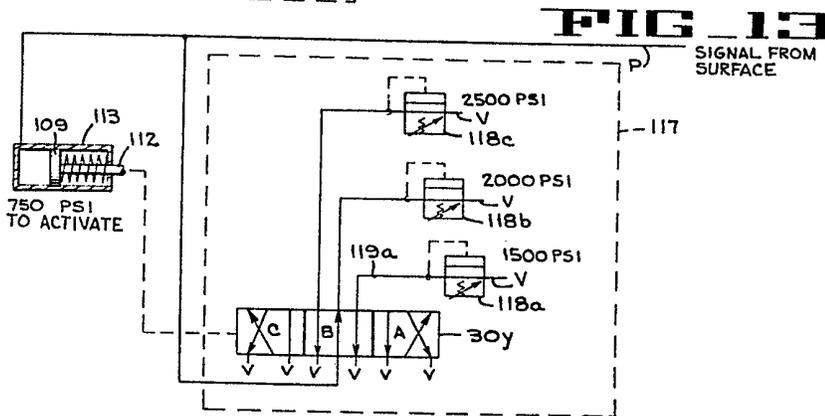
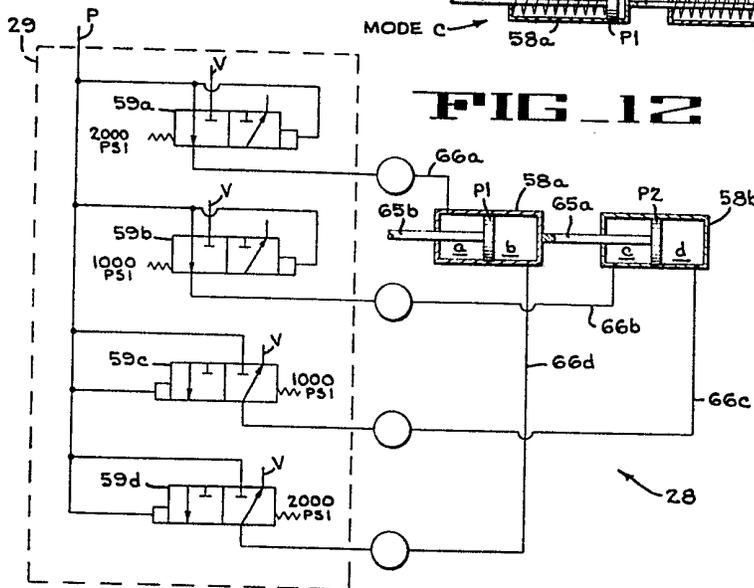
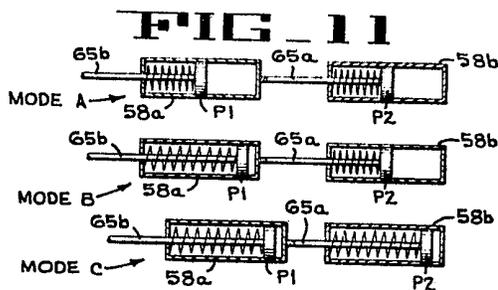
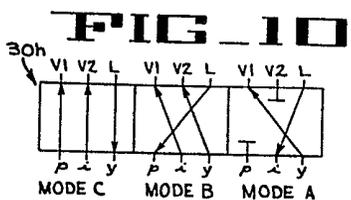


FIG 14

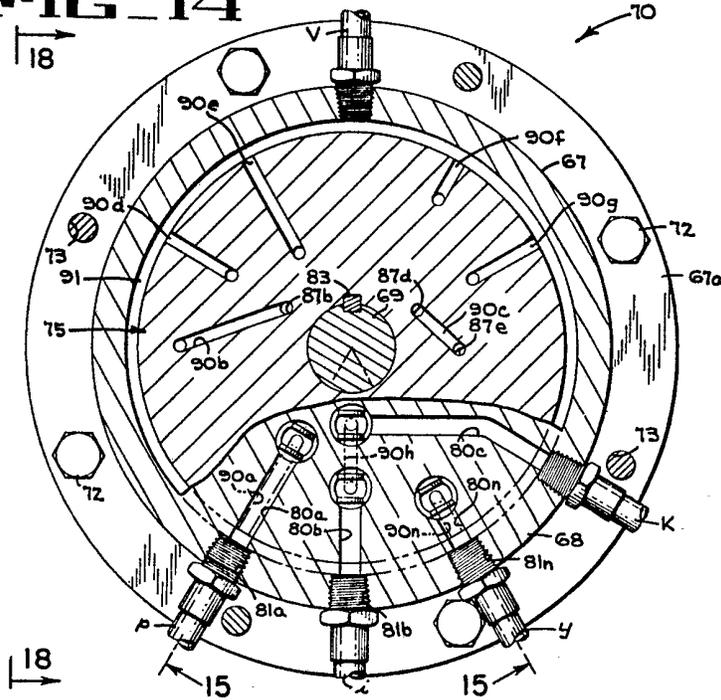


FIG 15

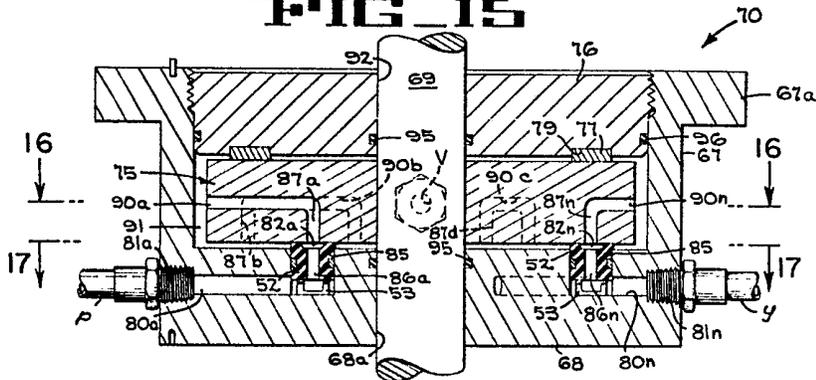


FIG. 16

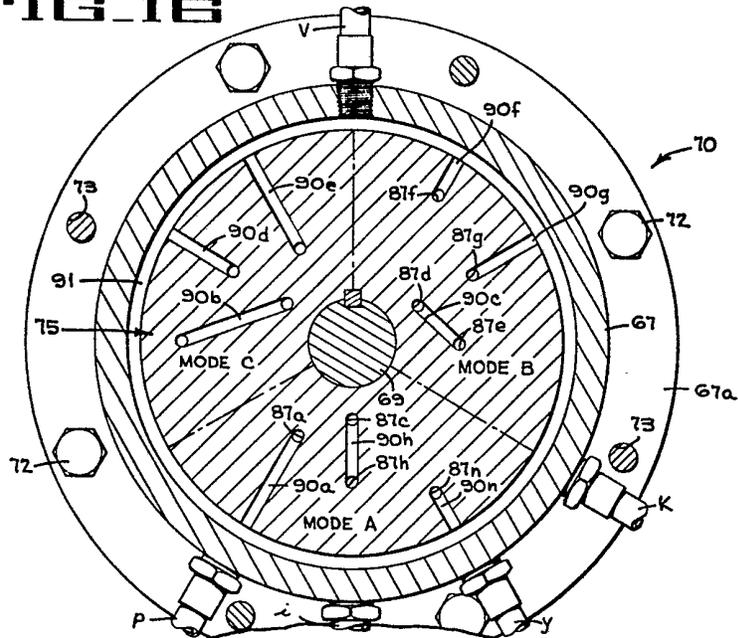


FIG. 17

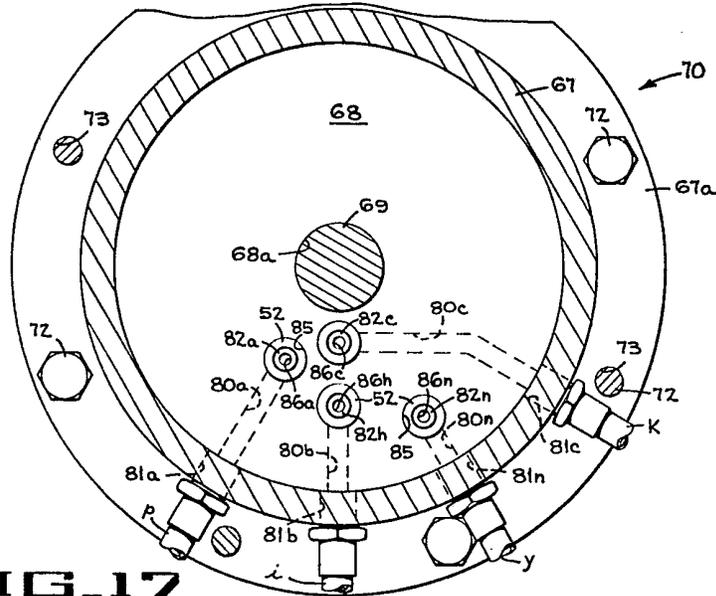


FIG. 18

