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#### IMPROVEMENTS IN OR RELATING TO COMPOSITE MATERIALS

The present invention relates to improved laminar composite structures and to a process for their manufacture. In particular the present invention relates to high strength light weight, rigid, composite materials and to their manufacture. The invention further relates to the production of high strength, light weight articles from such composites. Steel is typically used in structures where high strength is required. However steel tends to be heavy and thus adds excess weight to the article. Although there are a few light weight materials which are stronger than steel they are extremely expensive.

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We have found that the light weight, rigid composites of the present invention are particularly useful as materials in the furniture, construction and sporting, goods industries. In recent years there has been a trend to replace traditional steel and wooden components with lighter materials of comparable strength such as aluminium, fibre reinforced polymeric materials, foam materials and composites particularly composites containing foamed layers. There is however a continuing need for materials of increased strength and reduced weight.

The composites of the present invention have a wide variety of uses in additional applications in which high strength combined with light weight is required and in particular it can provide an inexpensive light weight material with comparable or improved strength relative to steel and wood. In addition, the structures can be used to improve the strength of articles in which lighter materials such as aluminium are used. Other uses include as raw materials in the production of sporting goods such as skis and in line skates and in the production of furniture.

The strength required of a material will depend upon the use to which it is to be put. For example the important characteristics can be high tensile strength and high flexural modules as measured by ASTM D790/ISO 178 norm or alternatively it can be resistance to impact, compression strength or torsional strength and in certain uses a combination of these properties may be required.

We have found that particularly desirable properties and in particularly the combination of low weight and high strength and stiffness can be obtained from composites sandwich structures consisting of at least two surface layers of wood enclosing a layer of rigid epoxy foam.

Composite sandwich structures with a foam core are known and have been proposed as materials having significant strength and stiffness together with an advantage derived from weight considerations. For example the abstract of Japanese Patent publication JP 58049223 A2 discloses sandwich structures comprising epoxy foam sandwiched between two metal plates. Two articles by S. Venkatraman and Kishore, the first in the Journal of Reinforced Plastics and Composites Vol 16 No. 7/1997 and the second in the Journal of Reinforced Plastics and Composites Vol 17 No. 8/1998 disclose composites comprising a thin layer of flexible foam sandwiched between two thick layers of glass-epoxy resin materials. The first of these articles relates to impact studies on the glass/epoxy laminates and the second to Investigations on the role of foam layers in the Failure of Glass-Epoxy composite subjected to repeated impacts. In both articles the layer of flexible epoxy foam is provided as a prefoamed flexible layer and is adhered to the glass/epoxy layer by means of an adhesive. The later article concludes that the way the sheet layers of flexible foam are arranged with respect to the direction of impact influences the spread of the crack path on repeated impact.

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Untied States Patent 3598671 discloses a method of preparing foam plastic laminated structures in which at least one component of a foam forming material is applied as a coating onto the surface of one sheet of a base material. A further component of the foam forming material is applied as a coating onto the surface of a second sheet of the base material. The sheets are then brought together so that the components of the foam forming materials are brought together so that they foam and produce a foamed core plastic laminated structure. Example 2 of US 3598671 produces such a laminate comprising a layer of epoxy foam ¼ inch thick sandwiched between two layers of fiberglass each approximately 1/8 inch thick. Accordingly the combined thickness of the two layers of fiberglass is substantially the same as the thickness of the foam. The foam is also extremely heavy, having a density of 7.5 lbs per square foot. United States Patent 3598671 does not therefore envisage the high strength light weight materials of the present invention.

Heat activatable foamable epoxy materials are known and are used in the production of structural reinforcement in automobiles. For instance the foamable material may be applied to the surface of a metal or plastic carrier to produce a component which is inserted into a part of the vehicle structure which requires reinforcement. The heat activatable foamable epoxy material may be formulated so that it will foam under the

conditions that prevail in the electrocoat (e-coat) process used to provide an anticorrosion coating to the metal surfaces of the vehicle structure or in any other painting operations. Such foamable epoxy materials and their uses are described in United States Patents 4922596; 4978562; 5124186 and 5884960. We have now found that improved light weight high strength composite materials can be obtained comprising a core of foamable epoxy materials of this type sandwiched between two layers of wood. United States Patent Application 09/939152 discloses structurally reinforced panels comprising a metal panel, a woven roving and bonded to one side of a matrix material which may be an epoxy foam.

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The present invention therefore provides a composite structure comprising an epoxy foam between two surface layers at least one of which is wood.

In a further embodiment, the present invention provides a composite comprising a sandwich structure comprising at least two surface layers at least one of which is wood attached to a central layer of rigid epoxy foam wherein the layer of epoxy foam is at least 1.5 times the combined thickness of the two surface layers and the foam has a density of from 0.2 to 1.5 gram/cc preferably between 0.4 and 1.5 gram/cc. In particular we prefer that the foam have a density of 0.3 to 0.6 gram/cc.

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In a further embodiment the invention provides a composite comprising at least two surface layers at least one of which is wood each layer having a thickness of from 0.2 to 10 millimetres and a core layer of a rigid epoxy foam having a thickness of from 2 to 200 millimetres.

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It is preferred that both the surface layers are of wood.

In a further embodiment of the present invention the composites of the present invention have a density in the range of from 0.1 to 2.0 gram/cc preferably 0.1 to 1.0 gram/cc; the density depending on the nature of the wood and optionally other material used for the surface layers. In yet a further embodiment a composite of the present invention which is from 5 to 8 millimeters thick has a flexural modulus of from 100 mPa to 700 mPa preferably 200 mPa more preferably 200 mPa to 700 mPa as measured by ASTM D 790/ISO 178 norm.

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It is preferred that both the surface layers of the composites of the present invention are of wood. However if only one layer is of wood the other layer may be of any

suitable material. Examples of suitable material include metal, including metal foil such as aluminium or steel foil, plastic film or sheeting such as polypropylene or polyethylene film or polyethylene terephthalate film. It is preferred however that the material be a fibrous material, a particularly preferred material is the material available from Saint Gobain under the trademark Twintex. It is particularly preferred that the surface layers be porous so that the epoxy material can penetrate the pores in the surface layers so that the surface layers become embedded in the epoxy foam.

Where fibrous material is used it may be of any suitable material and its selection will depend upon the use to which the composite material is to be put. Examples of fibrous materials that may be used include woven and non woven textile webs such as webs derived from polyester, polyamide, polyolefin, paper, carbon and kevlar fibre. These webs may be woven or obtained by non woven web manufacturing techniques such as needle punching and point bonding. Metallic fibrous webs may also be used although we prefer to use glass fibre which may also be woven or non-woven. In particular we prefer to use glass fibre web having a weight of from 40 gram/sq metre to 400 gram/sq metre. Other preferred fibrous materials include carbon fibre and Kevlar. The surface layers may themselves be produced by the laying up of two or more layers of material which may be the same or different.

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The term embedded is used to describe a composite in which the surface layer, although at the surfaces of the composite is largely enveloped by epoxy material. This may be determined from electron micrograph photographs of a cross section of the material such as Figure 4, which shows a substantially continuous layer of epoxy material extending into and at times through the surface layer. It will be appreciated that in order to be embedded it is not essential that all of the surface material be encased with the epoxy material. The epoxy material that extends into and sometimes through the surface layer may be the same as the epoxy foam although in a preferred embodiment of the present invention it is a separate unfoamed epoxy material that is compatible with the foamable epoxy material and forms a substantially continuous matrix with the foamable material, taking into account the voids formed due to the foaming of the epoxy material. The surface layer material is therefore embedded in this epoxy matrix.

35 The wood that is used as one or both of the surface layers is preferably a thin layer such as those typically available as plywood. Typical thicknesses that can be used

are from 0.4 to 2 millimeters preferably from 0.4 to 1.0 millimeters. Any form of wood may be used.

The foam layer is of a rigid epoxy foam. Rigid meaning that it is hard to the touch and resistant to manually applied pressure. It is preferred that the foam layer have a thickness of from 5 to 15 millimetres, preferably from 7 to 13 millimetres and most preferably from 8 to 13 millimetres. In the production of the composite materials of the present invention it is preferred that the foamable material from which the foam is produced have a thickness in the unfoamed state of from 1 to 5 millimetres, preferably 2 to 4 millimetres more preferably 2 to 3.5 millimetres.

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The present invention further provides a process for the production of composite materials comprising providing a first layer, laying a layer of heat activatable foamable epoxy material thereon and providing a second surface layer on the surface of the layer of heat activatable foamable epoxy material remote from the first layer and heating to activate the epoxy material to cause it to foam and cure and to thereby form a rigid foamed epoxy material bonded to the surface layers wherein at least one of the surface layers is wood.

In one further embodiment the present invention provides another process for the production of composite materials comprising spraying a foamable epoxy material between two surface layers and allowing the foamable material to expand and cure and bond to the surface layers wherein at least one of the surface layers is wood.

In one embodiment the surface layers are coated and/or impregnated with an epoxy material prior to heating. Preferably when such an epoxy material is used it is compatible with the heat activatable foamable epoxy material, so as to form a substantially continuous matrix therewith, as hereinbefore described. In this way when the surface layers are porous they can become embedded in the epoxy material. Preferably the epoxy material also cures under the same conditions as the heat activatable foamable epoxy material cures. In this embodiment the heating step of the process of the present invention will cure both epoxy resins. Conveniently the epoxy material with which the porous layers are coated and/or impregnated is the same epoxy material as is used as the basis for the heat activated foamable material although it need not be foamable.

The various embodiments of the present invention envisage in addition, sandwich composites containing four or more layers, their production and materials made therefrom. For example in addition to three layer sandwich structures the composite may comprise five layers consisting of two outer layers such as fibrous, metallic or plastic layers and an inner layer of fibrous, metallic or plastic material with two layers of epoxy foam or heat activatable epoxy foam forming material interposed between the layers. Composites containing a greater number of layers are also envisaged providing, however, that the two surface layers of the composite are according to the present invention.

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Foamable epoxy materials typically contain an epoxy resin, a blowing agent and a curing agent and frequently also contain a filler. The blowing agent and the curing agent can be selected so that foaming and curing (hardening) occur within the desired temperature range. The materials should therefore be chosen so that the temperature required for foaming and curing does not damage the surface layers. The epoxy resin may be chosen according to the degree of stiffness that is required in the product. Amine curing agents are frequently used in which case curing temperatures of at least 100°C are generally required. It is preferred that the blowing agent and curing agent be chosen so that foaming starts at a temperature slightly below the curing temperature. The foamable epoxy resin may be applied as a liquid typically through use of a solvent such as an alcohol. In this embodiment the epoxy resin may be sprayed or painted onto one or both of the surface layers. The solvent may then be removed by evaporation to provide a continuous or discontinuous layer of foamable epoxy material. Alternatively the foamable epoxy material may be extruded and cut into pieces for use in the invention or alternatively extruded onto one of the surface layers conveniently between the two surface layers.

The heat activated epoxy foam forming material should be chosen according to the application to which the composite is to be put. However the heat-activated epoxy-based resin should have foamable characteristics upon activation through the use of heat whereby it expands, cross-links to produce hard, rigid foam and cures to bond to the surface layers. An example of a preferred formulation is an epoxy-based material that may include polymer modifiers such as an ethylene copolymer or terpolymer that is commercially available from L & L Products, Inc of Romeo, Michigan, under the designations L-5204, L-5206, L-5207, L-5208, L-5209, L-5214 and L-5222 and from Core Products as core 5207,5214, 5234 and 5231. These products may also include fillers such as glass microspheres, calcium carbonate and talc which can reduce the

density of the foam. One advantage of these preferred heat activated foamable materials is that they can be processed in several ways to produce the heat activatable foamable layer of the present invention. The layer of foamable activatable epoxy material may be continuous or discontinuous. Possible techniques for the provision of the layer of foamable activatable material include the provision of sheet material, injection molding, blow molding, thermoforming, direct deposition of palletized materials, extrusion or extrusion with a mini-applicator extruder. The preferred epoxy materials are flexible prior to activation and this flexibility enables the creation of designs that allow the production of complex shapes and which exceed the design flexibility capability of most prior art high strength materials.

The heat activatable foamable epoxy resin whether it be as strips or spots is thermally expandable. That is, upon the application of heat they will expand, typically by a foaming reaction and preferably to at least 130%, more preferably at least 150%, the volume of the unexpanded state, but more preferably to at least twice the volume of the expanded state. The material also cures to provide a rigid epoxy foam bonded to the surface layers. The foamable material is preferably not tacky to the touch at room temperature and it is such that it will soften and then expand due to the activation of the blowing agent, the epoxy will then begin to cure and develop adhesive properties so that it will bond to the surface layers and finally the curing will be completed to harden the foamed epoxy resin. The resulting product being a sandwich structure comprising the surface layers bonded to the hard, rigid epoxy foam.

Epoxy resin preferably forms about 5% to about 75% by weight and more preferably from about 15% to 65% by weight of the activatable foamable epoxy material composition. Filler preferably forms from about 0% to about 70% by weight and more preferably from about 20% to about 50% by weight of the composition. A blowing agent preferably forms from about 0.5% to about 10% by weight and more preferably from about 0.2% to 5% by weight of the composition. A curing agent preferably forms from about 0% to about 10% by weight and more preferably from about 0.5% to 5% by weight of the composition. An accelerator preferably forms from about 0% to about 10% by weight and more preferably from about 0.3% to 5% by weight of the composition. A preferred formulation is set out in the following table.

Ingredient	% by weight 15% to 65%		
Epoxy Resin			
Ethylene Copolymer	0% to 20%		
Blowing Agent	0.2% to 5%		
Curing Agent	0.5% to 5		
Accelerator 0.3% to 5%			
Filler	20% to 50%		

In the preferred embodiment of the process of the present invention one or more of the surface layers is coated and/or impregnated with an epoxy material prior to heating to foam and cure the heat activatable epoxy material. In this embodiment it is preferred that the epoxy material used to coat and/or impregnate the surface layer cure under the same conditions as those under which the heat activatable foamable material cures. In a particularly preferred embodiment the epoxy material is the same as the epoxy material upon which the heat activated foamable material is based. This embodiment is particularly preferred when the surface layers are porous so that they may be impregnated with epoxy material. Alternatively the impregnation may be accomplished through the application of the foamable epoxy material in liquid form.

Epoxy resins that are preferably used in the foamable material have an epoxy equivalents value of about 200 to 5000, more preferably 300 to 3000, since these resins have suitable curing reactivity and melting points. Therefore, foams having satisfactory rigidity can be prepared. More preferably, the epoxy resin contains about 500 to 2500 and most preferably contains about 500 to 1500 epoxy equivalents.

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Epoxy resins having suitable epoxy equivalents are not restricted to a single type of epoxy resin. Rather, combinations of epoxy resins may be used. Representative epoxy resins include, but are not limited to, bisphenol A, bisphenol F, brominated bisphenol A, hydrogenated bisphenol A, bisphenol S, bisphenol AF, biphenyl, naphthalene, fluorine, phenol novolac, ortho-cresone novolac, DPP novolac, trifunctional, tris-hydroxyphenylmethane, tetraphenolethane and other glycidyl ether types are preferred.

The curing agent is material that is capable of curing epoxy resins. Preferably, the curing agent can co-exist at room temperature or usual storage temperatures with

the epoxy resin in unexpanded form without reacting with the epoxy resin, while at the same time, maintaining its curing reactivity. The curing agent preferably cures the epoxy resin at a temperature above the melting point of the epoxy resin and accordingly the curing reactivity of the curing agent should not be diminished when the foamable epoxy resin formulation is compounded and/or extruded.

Preferably, the curing agent retains sufficient reactivity during the production and storage of the foamable material in order to cure the epoxy resin when desired. Therefore, while some limited curing of the epoxy resin may occur during the production and storage of the foam precursor material, such curing should not substantially affect the curing reactivity of the curing agent. Accordingly, the curing agent also preferably has low reactivity with the epoxy resin when stored at room or usual storage temperatures in order to allow the foamable material to be stored for a long-term. Preferably, a curing agent is utilised that initiates curing in the temperature range of about 100°C to 200°C. More preferably, the curing temperature is from about 130°C to 180°C.

Preferred curing agents include polyaddition type, catalyst type and condensation type curing agents. The polyaddition type curing agents include, but are not limited to, polyamine-based dicyandiamide and the acid anhydride-based methyl nadic acid anhydride. The catalyst type curing agents include, but are not limited to, Imidazole-based 2-methyllmidazole, 2-ethyl 4-methyllmidazole and 2-heptadecyl Imidazole, Lewis acid-based monoethylamine boron trifluoride, piperazine boron trifluoride and other related compounds.

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The amount of curing agent used in the foam precursor materials will differ depending on the epoxy equivalents of the epoxy resin and will be sufficient to provide the rigid foam structure. Generally, an amount of curing agent is utilized that will effectively cure the epoxy resin. Preferable amounts are 1 to 25 parts by weight to 100 parts by weight of the epoxy resin and more preferably 1 to 10 parts by weight.

The foaming agent decomposes and expands at a temperature that is higher than the melting point of the epoxy resin that is used and does not decompose during the compounding and production of the foamable material such as during compounding and/or extrusion.

A foaming agent is selected that decomposes, and thus expands the epoxy resin, in a prescribed heating temperature range, depending on the curing agent used. The temperature range in which the curing agent can cure the epoxy resin should preferably overlap the temperature range in which the foaming agent decomposes and expands. Specifically, the foaming (decomposition) temperature is preferably about 100°C or higher, and more preferably 120°C or higher.

Preferably, organic decomposing-type foaming agents are utilised. For example, azodicarbonamide, azobisformamide, azobisisobutyronitrile, barium azodicarboxylate, N,N¹-dinitrosopentamethylene tetramine, N, N¹-dinitroso-N,N¹-dimethylteraphthalamide, para-toluensulfonyl hydrazide, benzenesulfonyl hydrazide, 4,4¹-oxybenzenesulfonyl hydrazide and other related compounds may be used. Any one or a combination of two or more of these foaming agents may be used. Azodicarbonamide is particularly preferred.

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The foaming agent is preferably added in an amount to provide a foaming ratio of about 30% to 100%, preferably 50% to 400%, and more preferably about 100% to 300%. That is, the amount of foaming agent utilised will produce a foam material having a volume 1.3 to 10 times larger than the volume of the foam precursor material, preferably 1.5 to 5 times larger and more preferably about 2 to 4 times larger. While specific amounts will depend upon the particular epoxy resin that is selected, the foaming agent may be added at about 0.5 to 15 parts by weight to 100 parts by weight of the epoxy resin and more preferably 0.5 to 10 parts by weight.

Various other additives may be added to the foamable composition, such as other resin components including for example, thermosetting resins and/or thermoplastic resins, inorganic additives including, for example, calcium carbonate, talc or mica, reactive dilutive compositions, curing accelerators, foaming aids, flame retardants, colouring agents and reinforcing materials (in powder form, chip form, fibre form bead form, etc) including, for example, glass, metal, ceramic or similar materials.

A thermosetting resin, other than an epoxy resin, may be added, including for example, polyester resins, melamine resins, urea resins and phenol resins. If such thermosetting resins are used, the amount of thermosetting resin can be appropriately determined based upon on the curing agent. If a thermoplastic resin is added, the resulting foam is generally more resilient than when a thermosetting resin alone is used. Thus, by changing the amount of thermoplastic resins and

thermosetting resins that are included in the foam precursor material, foam materials having different qualities may be produced. For example, adding such additives can increase the toughness of the foam material.

If a thermoplastic resin is added as an additive, the resin component is preferably polyethylene, polyvinyl acetate or a copolymer of ethylene and an alkyl acrylate. The copolymers of ethylene and alkyl acrylates can include ethylene-methyl acrylate polymer, ethylene-ethyl acrylate polymer, ethylene-butyl acrylate polymer etc, and preferred copolymers are of ethylene and alkyl acrylates with about 1 to 4 carbon atoms in the alkyl group. The thermoplastic resin may be a single compound or composition of matter or a combination of two or more compounds or compositions of matter.

If a thermoplastic resin is added, a polymerizable monomer may also be added. Suitable polymerizable monomers include triallyl cyanurate, triallyl isocryanurate, trimethylolpropane trimethacrylate and similar compounds.

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By adding a reinforcing material (in powder form, chip form, fibre form, bead form etc) such as glass, metal or ceramic, the rigidity of the resulting foam material can be increased. Specifically, if a fibre-formed material is added, the resiliency of the resulting foam material can be increased. The amount of such reinforcing materials to be added is preferably 1 to 300 parts by weight to 100 parts by weight of the resin component and more preferably 1 to 100 parts by weight.

In the embodiment of the invention where the surface layers are coated and/or impregnated with an epoxy material comprising epoxy resin preferably from about 5% to about 75% by weight and more preferably from about 15% to 65% by weight of the composition. Filler preferably forms from about 0% to about 70% by weight and more preferably from about 20% to about 50% by weight of the composition. Curing agent preferably forms from about 0% to about 10% by weight and more preferably from about 0.5% to 5% by weight of the composition. Accelerator preferably forms from about 0% to about 10% by weight and more preferably from about 0.3% to 5% by weight of the composition. A preferred coating formulation is set out in the following table.

Ingredient	% by weight		
Epoxy Resin	15% to 65%		
Ethylene Copolymer	0% to 20%		
Curing Agent	0.5% to 5		
Accelerator	0.3% to 5%		
Filler	20% to 50%		

The foamable epoxy material may be provided between the surface layers which are held apart by suitable means to allow the desired expansion of the foamable material.

The temperatures that should be used for the heating to foam and cure the epoxy materials will depend upon the choice of blowing agent and curing agent however, we have found that temperatures in the region of 100°C to 240°C are particularly useful although epoxy resin systems that foam upon mixing the components at lower temperatures are known. Alternatively one can use a system which foams at lower temperatures, such as those in which two or more components are provided and mixed at ambient temperature. A benefit of the process of the present invention is that external pressure may not be required during moulding in order to achieve a desired surface finish in that the foaming of the heat activatable foamable epoxy resin can itself produced sufficient internal pressure.

We have found that composites of the present invention have high flexural strength combined with low weight. Typically a composite having a thickness of from 5 millimetres to 8 millimetres has a flexural strength of from 100 mPa to 700 mPa typically 300 mPa to 700 mPa at a density of from 0.1 to 1.0 grams/cc which compares favourably with current light weight aluminium, based materials of similar weight per unit area which have a flexural modulus of about 10% that of the composite of the present invention products of comparable weight per unit area.

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The composites of the present invention find a wide range of uses where high strength and light weight are required. For example they may be used in the construction industry, in transportation industries including the automobile, aircraft, aerospace and shipping vessel industries and in the furniture and sporting goods industries. The composites may also be used as components in buildings, vehicles, sporting goods and furniture. We particularly prefer that the composites are in the

form of panels and as such they may be used in the construction industry as building panels or as facing sheets for the casting of concrete.

If the composites are to be attached to other components within the finished article attachment means may be provided within the composite to enable assembly. In this embodiment of the invention the attachment may be located within the activatable foamable material prior to heating to foam and cure. In this way the foamable material can expand around the attachment to hold it firmly in place as the epoxy material cures. Typical attachment means comprise clips, studs, bolts and the like which may be of any material providing they retain their strength under the conditions used for activation and foaming.

The present invention is further illustrated by reference to the following Examples.

### Example 1

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An extruded foamable epoxy material available from Core Products as CORE-5234 is placed between two layers of 0.6 millimetre thick three ply plywood. The three layers are then placed in a mould and cured at 175°C for 45 minutes and at normal pressure to form a composite 5.4 millimetres thick.

### **CLAIMS**

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 A composite comprising a sandwich structure comprising an epoxy foam between two surface layers in which at least one of the surface layers is wood.

- 2. A composite according to Claim 1 in which bother surface layers are wood.
- 3. A composite comprising a sandwich structure according to Claim 1 or Claim 2 comprising at least two surface layers attached to a central layer of rigid epoxy foam wherein the layer of epoxy foam is at least 1.5 times the combined thickness of the two surface layers and the foam has a density of from 0.2 to 1.5 gram/cc.
- 15 4. A composite according to any of the preceding claims in which the foam has a density of between 0.4 and 1.5 gram/cc.
  - 5. A composite according to claim 4 in which the foam has a density of 0.3 to 0.6 gram/cc.
- 6. A composite comprising at least two surface layers each layer having a thickness of from 0.2 to 10 millimetres and a core layer of a rigid epoxy foam having a thickness of from 2 to 200 millimetres wherein at least one of the surface layers is wood.
  - 7. A composite according to Claim 6 in which both surface layers are wood.
  - 8. A composite according to any of the preceding claims having a flexural modulus as measured by ASTM D790/ISO 178 from 200 mPa to 700 mPa.
  - 9. A composite according to any of the preceding claims having a density of from 0.1 to 1 gram/cc.
- The use of a composite according to any of the preceding claims to provide structures in the construction, furniture or transportation industries.

11. A process for the production of composite materials comprising providing a first surface layer, laying a layer of heat activatable foamable epoxy material thereon and providing a second surface layer on the surface of the layer of heat activatable foamable epoxy material remote from the first layer of fibrous material and heat activating the epoxy material so that it foams and bonds to the surface layers wherein at lest one of the surface layers is wood.

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12. A process for the production of composite materials comprising spraying a foamable epoxy material between two surface layers and allowing the foamable material to expand and cure and bond to the surface layers wherein at lest one of the surface layers is wood.

#### INTERNATIONAL SEARCH REPORT

International application No PCT/EP2006/007644

CLASSIFICATION OF SUBJECT MATTER NV. B32B5/18 B32B2 B32B21/04 B32B27/38 According to International Patent Classification (IPC) or to both national classification and IPC B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) B32B Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched Electronic data base consulted during the international search (name of data base and, where practical, search terms used) EPO-Internal, WPI Data C. DOCUMENTS CONSIDERED TO BE RELEVANT Category\* Citation of document, with indication, where appropriate, of the relevant passages Relevant to claim No. χ US 4 581 186 A (LARSON ROGER E [US]) 1-10.128 April 1986 (1986-04-08) column 1, line 57 - line 61 column 2, line 28 - line 42 column 4, line 9 - line 14 claim 1 χ US 4 146 251 A (TANAHASHI RYOJI) 1 - 1127 March 1979 (1979-03-27) column 1, line 5 - line 9 column 2, line 22 - line 30 column 3, line 32 - line 44 column 4, line 5 - line 66 column 5, line 9 - line 15 claims 1,6,7,9,19-21,23Further documents are listed in the continuation of Box C. See patent family annex. Special categories of cited documents: "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the \*A\* document defining the general state of the art which is not considered to be of particular relevance invention "E" earlier document but published on or after the international "X" document of particular relevance; the claimed invention filing date cannot be considered novel or cannot be considered to document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such docu-"O" document referring to an oral disclosure, use, exhibition or other means ments, such combination being obvious to a person skilled document published prior to the international filing date but later than the priority date claimed "&" document member of the same patent family Date of the actual completion of the international search Date of mailing of the international search report 23 October 2006 07/11/2006 Name and mailing address of the ISA/ Authorized officer European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Girard, Sarah Fax: (+31-70) 340-3016

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Information on patent family members

International application No
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Patent document cited in search report		Publication date		Patent family member(s)	Publication date
US 4581186	A	08-04-1986	NONE		
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