



(51) International Patent Classification:

B64C 9/38 (2006.01) B64C 21/10 (2006.01)
B64C 15/14 (2006.01) B64C 29/00 (2006.01)

(21) International Application Number:

PCT/KZ2015/000008

(22) International Filing Date:

9 July 2015 (09.07.2015)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

2014/1053.1 4 August 2014 (04.08.2014) KZ

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(81) Designated States (unless otherwise indicated, for every

kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM,

DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, JP, KE, KG, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

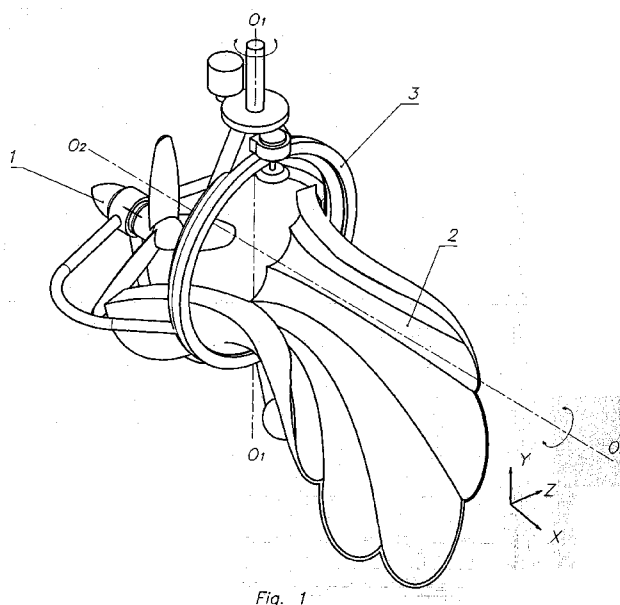
Declarations under Rule 4.17:

— of inventorship (Rule 4.17(iv))

Published:

— with international search report (Art. 21(3))

(54) Title: AERODYNAMIC DEVICE



(57) Abstract: The invention relates to aviation equipment. An object of this invention is to develop a new aerodynamic device which can extend the range of aerodynamic devices for aviation, increase the efficiency of the air flow power use, increase the efficiency of the lifting force and improve the efficiency of controlling the wing resultant forces. For this purpose, the aerodynamic device has an aerodynamic wing (2) with a blower (1) of gaseous working fluid (such as air) mounted above the wing (2), in accordance with the invention, the aerodynamic wing (2) has a specific shape it is designed in the form of a double-curved open surface made up by a system of longitudinal grooves (7,8) along the whole wing surface. The wing (2) has a convergent segment (4) and a divergent segment (6); between the convergent and the divergent segments there is a smooth transitional segment (5). The wing outlines have end elements (11). In the convergent and the divergent segments of the wing lower surface which is not blown by air, there is a controlled drive system (10) for the wing surface cambering and area changing. The divergent segment tip on the wing trailing edge has a deflatable controlled element (9). The structural parts of the present invention meet special conditions.

AERODYNAMIC DEVICE

Technical Field

The invention relates to aviation equipment.

Background Art

5 The conventional aerodynamic device used in aircraft in the form of a lift generating airfoil is a wing. The working fluid - air or another gas - flowing around the wing, creates different in magnitude pressures on its upper and lower surfaces caused by different speeds of streams above and below the wing and resulting in creating the lifting force (New Polytechnic Dictionary ed. by A.U. Ishlinsky. - Moscow: Research Publishing "Bolshaya
10 Rossiyskaya Entsiklopediya", 2000. - p. 36, 252). For instance, a fan blower generates air flow, while a turbojet blower generates gas flow which contains (along with air) other gaseous combustion products. In the following, for the purpose of clarity of the present object disclosure, air is taken to mean gas, because the cases of other gaseous working fluids, such as end gases (exhaust gases), are identical.

15 The air flow around the wing is a three-dimensional nonlinear process. The lifting force of the wing depends on its area, shape, planform shape, as well as on the angle of attack, air speed, viscosity and density, and on other physical factors. When a wing is moving in the air flow, the air layers interact with the wing upper and lower surfaces. The air flow moving along the wing upper surface gets attracted to it and moves along it even
20 after the profile inflection due to the effect of viscosity forces, which is known as the Coanda effect (see, for example: 1) Loytsyansky, L.G., Fluid Mechanics. - Moscow: Drofa Publishing, 2003, 7th edition, p. 504-507; 2) Reba I., Wohlthausen E. Applications of the Coanda Effect // Scientific American, volume 214, June 1966, pp. 84-92 (http://www.laesieworks.com/ifo/how/Coanda_effect-P1.html)). The increase of the wing
25 lifting force due to the Coanda effect is possible by virtue of the forced increase of the air flow rate on the wing upper surface.

One of the well-known is the aerodynamic device consisting of a Custer channel wing and a propeller engine (See: 1) Bowers P. Unconventional Aircraft / P. Bowers - Blue Ridge Summit, PA: 1990 (Eng). - Moscow: Mir, 1991 (Rus). pp. 137-138. 2) US Patent №
30 2,691,494, Cl. 244-12, 10.06.1954). The Custer channel wing is a semi-circular airfoil of a channel or "half barrel" shape. Furthermore, in its section along the airflow, the channel wing has an aerodynamic contour. Above the Custer channel wing, there is a propeller

engine, while the prop plane is located at the airfoil trailing edge. The propeller sucks the air into the channel creating the increase of the air flow rate above airfoil and thus increases the wing lifting force.

The closest analogous solution is an aerodynamic device in the form of a chute-type wing with a turbojet mounted on its front upper surface. This aerodynamic device was proposed in RU Patent №2288137, IPC B64C21/00, B64C3/00, 30.05.2005, according to which the chute-type wings are mounted underneath the fuselage. When the turbojet is working, the end gases are moving along the wing upper surface thus creating a low pressure area on the wing upper surface which results in additional wing lift.

The technical result of the well-known analogs with an unconventional wing, is creating the lifting force by employing the Coanda effect.

A common drawback of the above aerodynamic devices is underutilization of air viscosity and compressibility and insufficiently effective choice of the wing upper surface shape, which is interacting with the air flow and acts as an underlying surface in relation to the air flow, which results in low efficiency of the air flow power use, in reduced lifting force and in low efficiency of controlling the wing resultant forces.

Summary of Invention

An object of this invention is to develop a new aerodynamic device which can obviate the above drawbacks of conventional devices, increase efficiency of the air flow power use, increase the efficiency of the lifting force, and improve the efficiency of the wing resultant forces control process by virtue of:

1) improved efficiency of the air flow power utilization in the process of air flow around the wing due to reduced energy scattering in space by means of using air viscosity forces and compressibility;

2) improved efficiency of the underlying surface specific shape utilization for attached flow about the airfoil;

3) improved efficiency of utilizing the Coanda effect to increase the reaction force impulse projection value in the vertical direction, determined by the interaction between the structural components and the air flow;

4) improved efficiency of the wing resultant lifting forces control process by virtue of forces generated by the wing.

It is another object of the present invention to extend the range of aerodynamic devices for aviation through providing a new specific unconventional device.

For this purpose, the aerodynamic device has an aerodynamic wing with a gaseous

working fluid (such as air) blower mounted above the wing and connected to the wing by mechanical components (or connecting system); in accordance with the invention, the aerodynamic wing has a specific form: the wing is designed in the form of a double-curved open surface made up by a system of longitudinal grooves along the entire wing surface and with a vertical longitudinal plane of symmetry. Along the trajectory of the gaseous working fluid flow, the wing has a convergent segment and a divergent segment; between the convergent and the divergent segments there is a smooth transitional segment. To prevent the air flowing from the lower surface to the upper surface, the wing outlines have end elements. In the convergent and the divergent segments of the wing lower surface which is not blown by air, there is a controlled drive system for the wing surface cambering and area changing. The divergent segment tip on the wing trailing edge has a deflectable controlled element whose purpose is similar to that of the conventional wing plain flap.

The structural parts of the present invention have the following distinguishing features. The system of longitudinal grooves consists of the central grooves provided in the wing central part and of the lateral grooves provided in the wing side parts. The central grooves go along the whole wing, starting from the convergent segment, continuing in the transition segment and finishing in the divergent segment. The lateral grooves start in the convergent segment and, depending on the position in relation to the wing vertical plane of symmetry, may end in the transitional segment or in the divergent segment, which is established by experiments or by calculation, depending on the specific purpose of the wing. The vertices of the central and lateral grooves are rounded, in so doing, the generatrix curvature radii r for the groove vertices are smaller than the generatrix curvature radii R for the groove lower parts (as is known, a generatrix is a line whose motion generates a surface). The number of the central and lateral grooves depends on the required (needed or necessary) wing area, which is determined in accordance with the specific purpose of the wing.

The central and lateral grooves are made on the wing underlying surface in such a way that the cross-sectional area of each groove along the flow is either constant or monotonically increasing. The convergent segment of the wing is actually a sectorial part of a symmetrical conical surface provided with grooves along the flow. The geometry variables and relationships for the convergent segment of the wing are characterized in that the opening angle of the whole sectorial part of the wing convergent segment γ_k lies in the range from 150° to 220° . The relation between the sectorial angle of the central part of the wing convergent segment and the opening angle of the entire sectorial part of the wing

convergent segment γ_{kc} / γ_k lies in the range from 0.5 to 0.8. In the longitudinal plane of symmetry, the relation between the convergent segment length projected on the rolling axis of symmetry and the wing chord length with its maximum value L_k / L_{max} lies in the range from 0.1 to 0.4. (As is known from Aerodynamics (see, for example: GOST 22833-77.

5 Aircraft Geometry Variables), the wing chord length is equal to the distance between the points of the wing leading and trailing edges in the vertical plane of symmetry. From this definition follows the meaning of value L_{max}). The wing transitional segment is actually a sectorial symmetrical double-curved saddle-shaped surface with longitudinal grooves. The transitional segment comprises the wing throat which has the minimum cross-sectional area
10 and is perpendicular to the wing vertical longitudinal plane of symmetry. In the longitudinal plane of symmetry, the relation between the transitional segment length projected on the rolling axis of symmetry and the wing length chord with its maximum value L_t / L_{max} lies in the range from 0.1 to 0.4. The divergent segment of the wing is actually a sectorial part of a symmetrical conical surface with longitudinal grooves. The divergent segment is made with
15 a provision of the positive increment of the wing underlying surface area over the wing length, longitudinally along the flow. The opening angle of the entire sectorial part of the wing divergent segment γ_d lies in the range from 150° to 220° . The relation between the sectorial angle of the wing divergent segment and the opening angle of the entire sectorial part of the wing divergent segment

20 γ_{dc} / γ_d lies in the range from 0.5 to 0.8. In the longitudinal plane of symmetry, the relation between the divergent segment length projected on the rolling axis of symmetry and the wing length chord with its maximum value L_d / L_{max} lies in the range from 0.2 to 0.8. The wing section cambering and area changing result in changing the relation between the projected lengths of these sections and the chord value with its maximum value L_{max} ; in so
25 doing the particular relationship values lie within the above ranges. The deflection angle for the deflectable controlled element θ lies in the range from 0° to 40° .

The invention is illustrated, by way of example, in the accompanying scheme drawings which show one of the preferred embodiments of the invention. These drawings have sufficient detail for understanding the essence of the invention.

30 Brief Description of Drawings

The figures show an air blower 1, an aerodynamic wing 2, a connecting system 3 (in other words, these are mechanical elements 3, connecting the blower 1 with the wing 2), the wing convergent segment 4, the transitional segment 5, the wing divergent segment 6, central grooves 7, lateral grooves 8, the deflectable controlled element 9, the controlled

drive system 10 for cambering and area changing of the wing transitional and divergent segments, the end elements 11. It should be noted that in the following, for the sake of clarity of the disclosure of the invention, each separate figure shows primarily only those device elements which are necessary for illustrating the essence of this or that part of the invention description (without extra elements which can be conceptually omitted).

Fig. 1 and Fig. 2 are a structure of the whole device (Fig. 1 is a visual image of the device, Fig. 2 is the side view of the device) and its main elements: the propeller blower 1, the aerodynamic wing 2, the connecting system 3 (of mechanical type, connecting the blower 1 with the wing 2), the controlled drive system 10 for cambering and area changing of the wing transitional and divergent segments.

Fig. 3 is an aerodynamic wing, axonometric drawing. Fig. 3 shows the shape of the aerodynamic wing 2, the central and lateral grooves 7 and 8, the deflectable controlled element 9, the end elements 11.

Fig. 4 is an aerodynamic wing, side view, with the longitudinal section A-A in the longitudinal plane of symmetry. Fig. 4 shows the following values: aerodynamic chord L , which can be changed to the maximum value L_{\max} ; the convergent segment length projected on the longitudinal plane of symmetry L_k ; the divergent segment length projected on the longitudinal plane of symmetry L_d ; the transitional segment length projected on the longitudinal plane of symmetry L_t .

Fig. 5 is an aerodynamic wing, B view (convergent segment view). Fig. 5 shows the aerodynamic wing 2 (by the example of the wing with three central grooves 7 and two lateral grooves 8 on each side), the end elements 11.

Fig. 6 is a section of the convergent segment C-C. Fig. 6 shows the following values: the generatrix curvature radius for vertices r , the generatrix curvature radius for the lower part of groove R , the opening angle for the whole sectorial part of the wing convergent segment γ_k , the sectorial angle of the central part of the wing convergent segment γ_{kc} , the sectorial angle of the lateral part of the wing opening angle γ_{ks} , the cross-sectional area of the central groove S_{1k} , the cross-sectional area of the lateral groove S_{2k} . It should be noted, that in Fig. 6 and further in the application materials, if the value symbols have additional superscripts « i » or « j », they indicate the i -th or j -th grooves.

Fig. 7 is an aerodynamic wing, D view (the divergent segment view). Fig. 7 shows the aerodynamic wing 2 (by the example of the wing with three central grooves 7 and two lateral grooves 8 on each side), the deflectable controlled element 9, the end elements 11.

Fig. 8 is a section of the divergent segment $C_n - C_n$. Fig. 8 shows the following

values: the generatrix curvature radius for vertices r , the generatrix curvature radius for the lower part of groove R , the opening angle for the whole sectorial part of the wing divergent segment γ_d , sectorial angle of the central part of the wing divergent segment γ_{dc} , the sectorial angle of the lateral part of the wing divergent segment γ_{ds} , the cross-sectional area of the central groove S_{ld} , the cross-sectional area of the lateral groove S_{2d} .

Fig. 9 is an aerodynamic wing, top view. Fig. 9 shows the aerodynamic wing 2, the deflectable controlled element 9, the end elements 11.

Fig. 10, Fig. 11, Fig. 12, Fig. 13 show the aerodynamic wing with different shapes of the divergent segment in the longitudinal plane of symmetry (the arrows show the movement of the particles of the air flow). In so doing, Fig. 11, Fig. 12 and Fig. 13 show the controlled drive system 10 for wing divergent segment cambering and area changing.

Fig. 14 is a deflectable controlled element 9 in various positions, θ is the deflection angle for the deflectable controlled element.

Fig. 15 is an unmanned aircraft option.

Modes for Carrying out the Invention

The proposed aerodynamic device operates in the following way (Fig. 1-14).

From the blower 1 the flow passes above the aerodynamic wing 2 and interacts with the same (Fig. 1, Fig. 2). The aerodynamic flow from the blower 1 flows around the wing 2 only on the upper side. In this case, the wing 2 upper surface acts as the underlying surface in relation to the flow and the flow actively interacts with the underlying surface which is then defined as a viscous interaction underlying surface (hereinafter referred to as VIUS).

The occurrence of the aerodynamic lifting force is caused by the force interaction between the incoming gaseous working fluid (such as air) from the blower 1 and the wing 2 aerodynamic surface of a special shape. The high-energy flow of the gaseous working fluid can be generated by the work of a propeller, jet engine or rocket engine, an axial-flow or a radial-flow blower, etc.

When the air flow passes from the blower 1 to the wing convergent segment 4, the surrounding air particles are ejected by the high-energy air flow from the blower 1, which adds the number of air particles involved in flowing around the wing 2.

The underlying surface of the convergent segment 4, due to deflection and deceleration of the air flow from the blower 1, in immediate proximity to the wing 2 surface in the central part of the convergent segment 4, can create a high-pressure zone (as compared to the pressure at the periphery of the convergent segment 4). As has been shown by model-based exploratory tests, a high-pressure zone can cover from 0 (zero) to 30% of

the convergent segment 4 surface area.

The air flow is distributed between grooves 7 and 8 of the convergent segment 4 and afterwards passes along grooves 7 and 8 toward the transitional segment 5. Due to a special shape of the convergent surface grooves, the particles move toward the transitional segment 5 with simultaneous flow redistribution in such a way that the air flow gets attracted to the surface of the convergent segment 4 as a result of compressibility and viscous force effect in the flow of air particles.

The area of the high-pressure zone depends both on the air flow energy and the angle between the resultant velocity speed of the air flow from the blower 1 and the symmetry axis of the conical surface making the wing convergent segment 4. The optimum value of this angle maintains the most efficient "attraction" and holding of the flow to the VIUS, thus ensuring the attached flow of air particles toward the wing transitional segment 5.

Low-pressure zones occur on the VIUS of the transitional 5 and divergent 6 wing segments flown by the air flow; this determines the occurrence of forces of aerodynamic nature on the surface of wing 2.

The entire viscous interaction underlying surface (VIUS) of the aerodynamic wing is covered with grooves. The central part of the wing has central grooves 7, and the lateral parts of the wing have lateral grooves 8. The grooves on the aerodynamic wing have the following functions.

In the central grooves 7 the basic process of the interaction between the flow and the VIUS takes place. The lateral grooves 8 provide for keeping the air flow above the VIUS in the wing central part and perform the restrictive function. The central grooves 7 go along the whole length of the aerodynamic wing 2, starting from the convergent segment 4, continuing in the transitional segment 5 and finishing in the divergent segment 6. The grooves are made on the VIUS in such a way that the cross-sectional area of each groove along the flow motion is either constant or monotonically increasing. The lateral grooves 8 start in the convergent segment 4 and, depending on the position in relation to the wing 2 vertical plane of symmetry, may end in the transitional segment 5 or in the divergent segment 6, which is established by experiments or by calculation, depending on the specific purpose of the aerodynamic wing.

The structural components of the wing surface which are formed by the vertices of the adjacent grooves, cut the flow and direct the same along the wing generatrix thus increasing the VIUS area.

The vertices of the central and lateral grooves are rounded with the generatrix

curvature radii for the groove vertices r are smaller than the generatrix curvature radii for the lower parts of the groove R .

The number and the shape of the central and lateral grooves depends on the required wing area, which is determined in accordance with the specific purpose of the wing.

5 The central and lateral grooves are made on the wing underlying surface in such a way that the cross-sectional area of each groove along the flow is either constant or monotonically increasing. The optimum shape and size of the central grooves 7 on the convergent segment 4 are determined by calculation (using numerical methods) and by experiments taking account various physical parameters (air flow rate, kinematic coefficient
10 of air viscosity, etc.) and are established depending on the specific purpose of the aerodynamic wing.

The segments of the aerodynamic wing 2 are characterized as follows.

The convergent segment 4 of the wing is actually a sectorial part of a symmetrical conical surface provided with longitudinal grooves along the flow. The geometry variables
15 and relationships for the convergent segment of the wing are given below.

The opening angle of the entire sectorial part of the wing convergent segment γ_k lies in the range from 150° to 220° (Fig. 6). The relation between the sectorial angle of the central part of the wing convergent segment and the opening angle of the entire sectorial part of the wing convergent segment γ_{kc} / γ_k lies in the range from 0.5 to 0.8 (Fig. 6).

20 In the longitudinal plane of symmetry, the relation between the convergent segment length projected on the rolling axis of symmetry and the wing chord length with its maximum value L_k / L_{\max} lies in the range from 0.1 to 0.4 (Fig. 4).

The transitional segment 5 serves for connecting the convergent 4 and divergent 6 wing segments. The wing transitional segment 5 is actually a sectorial symmetrical double-
25 curved saddle-shaped surface. The transitional segment 5 is provided with longitudinal grooves along the flow. The lifting force arises at the transitional segment 5 of the aerodynamic surface. Moreover, the transitional segment 5 comprises the wing 2 throat which has the minimum cross-sectional area. The throat section is perpendicular to the wing 2 vertical longitudinal plane of symmetry. The lifting force arises at the transitional segment
30 5 of the aerodynamic surface. In the longitudinal plane of symmetry, the relation between the transitional segment length projected on the rolling axis of symmetry and the wing chord length with its maximum value L_t / L_{\max} lies in the range from 0.1 to 0.4 (Fig. 4).

The divergent segment 6 of the wing is actually a sectorial part of a symmetrical conical surface. It is also provided with longitudinal grooves along the air flow.

To ensure the continuous flow around the underlying surface, the divergent segment is made with a provision of the positive increment of the wing underlying surface area over the wing length, longitudinally along the flow. Meeting this condition can reduce the build-up rate of the boundary layer which contributes to separation of the flow from the surface.

5 The lifting force arises at the divergent segment 6 of the aerodynamic surface.

The opening angle of the entire sectorial part of the wing divergent segment γ_d lies in the range from 150° to 220° (Fig. 8). The relation between the sectorial angle of the central part of the wing divergent segment and the opening angle of the entire sectorial part of the wing divergent segment γ_{dc} / γ_d lies in the range from 0.5 to 0.8 (Fig. 8).

10 In the longitudinal plane of symmetry, the relation between the divergent segment length projected on the rolling axis of symmetry and the wing length chord with its maximum value L_d / L_{\max} lies in the range from 0.2 to 0.8 (Fig. 4).

The design of the divergent segment 6 of the wing 2 allows to change the direction of the retroactive force arising from the air flow jet coming off the surface of the divergent
15 segment 6, as well as the direction and the magnitude of the total resultant aerodynamic force. This property of the wing 2 can be used for generating control forces and moments during flight control, for example, for an unmanned flying vehicle which could employ one or more proposed wings 2 (Fig. 15).

Cambering and area changing of the transitional segment 5 and the divergent
20 segment 6 is achieved by a special design and/or by using special elastic and resilient materials. In the proposed device, the aerodynamic wing 2 is provided with a system of controlled drives 10 for the wing surface cambering and area changing, which ensures meeting the condition of the positive increment of the wing underlying surface area over the wing length, longitudinally along the flow, as well as for generating control forces and
25 moments during various flight modes and conditions.

The divergent segment 6 tip on the wing trailing edge has a deflectable controlled element 9 which is responsible for increasing or decreasing the deflection of the air flow coming off the wing 2 in the vertical plane. The deflection angle θ for the deflectable controlled element 9 (the flap) lies in the range from 0° to 40° (Fig. 14). The deflectable
30 controlled element 9 makes it possible to increase the wing lifting force during take-off.

Since the air flow around the wing is a three-dimensional nonlinear process and depends on a number of physical factors, it is impossible to foresee and justify optimisation of its design characteristics. Therefore, optimisation of some of the proposed design characteristics was carried out by means of the conventional design-theoretical methods and

model tests established in fluid mechanics (Encyclopedic Dictionary of Physics / ed. by A.M. Prokhorov. – Moscow: Sovetskaya Entsiklopedia, 1983. – 928 p.; Krasnov, N.F., Aerodynamics. Part I. Theoretical Framework. Airfoil and Wing Aerodynamics. Technical college textbook. - Moscow, Vysshaya Shkola, 1976. - 384 p.; Krasnov, N. F.,

- 5 Aerodynamics. Part II. Aerodynamics Technology. Textbook for technical college students. — 3rd edition, revised and enlarged. — Moscow, Vysshaya Shkola, 1980. — 416 p.). In so doing, it was found that the proposed ranges are optimal. In other cases, beyond these optimal ranges, the efficiency of utilizing the air flow power normally used for generating the wing resultant lifting force, declines by at least 10%.

- 10 Due to the special wing shape and to the blowing of the wing upper surface by the blower, the proposed device makes it possible to design various aircrafts with one or more special-shape wings, as well as to combine conventional wings in the aircraft design. For instance, it is possible to develop unmanned aircrafts performing vertical take-off and landing as well as level flight (Fig. 15).

CLAIMS

1. An aerodynamic device which has an aerodynamic wing (2) with a gaseous working fluid blower (1) mounted above the wing (2) and connected to the wing by mechanical components (3) characterized in that the aerodynamic wing (2) has a specific form of a double-curved open surface made up by a system of longitudinal grooves (7, 8) along the entire surface of the wing (2) surface and with a vertical longitudinal plane of symmetry; along the trajectory of gaseous working fluid flow, the wing (2) has a convergent segment (4) and a divergent segment (6); between the convergent (4) and the divergent (6) segments there is a smooth transitional segment (5); the wing (2) outlines have end elements (11); in the transitional (5) and the divergent (6) segments on the wing (2) lower surface which is not blown by air, there is a controlled drive system (10) for the wing (2) surface cambering and area changing; the divergent segment (6) tip on the wing (2) trailing edge has a deflectable controlled element (9).

2. The aerodynamic device of claim 1 wherein the device structural parts are characterized in that the system of longitudinal grooves (7, 8) consists of the central grooves (7) provided in the wing (2) central part and of the lateral grooves (8) provided in the wing (2) side parts; the central grooves (7) go along the whole length of the aerodynamic wing (2), starting from the convergent segment (4), continuing in the transitional segment (5) and finishing in the divergent segment (6); the lateral grooves (8) start in the convergent segment (4) and, depending on the position in relation to the wing (2) vertical plane of symmetry may end in the transitional segment (5) or in the divergent segment (6), which is determined depending on the specific purpose of the wing (2); the vertices of the central (7) and lateral (8) grooves are rounded, with the generatrix curvature radii for the groove (7, 8) vertices smaller than the generatrix curvature radii for the groove (7, 8) lower parts; the number of the central (7) and lateral (8) grooves depends on the required wing area, which is determined in accordance with the specific purpose of the wing (2); the central (7) and the lateral (8) grooves are made on the wing (2) underlying surface in such a way that the cross-sectional area of each groove (7, 8) along the flow is either constant or monotonically increasing; the wing convergent segment (4) is actually a sectorial part of the symmetrical conical surface provided with grooves (7, 8) along the flow; the geometry variables and relationships for the convergent segment (4) of the wing are characterized in that the opening angle of the entire sectorial part of the wing convergent segment (4) γ_k lies in the range

$150^0 < \gamma_k < 220^0$, the relation between the sectorial angle of the central part of the wing convergent segment (4) γ_{kc} and the opening angle of the entire sectorial part of the wing convergent segment (4) γ_k lies in the range $0.5 < \gamma_{kc} / \gamma_k < 0.8$, in the longitudinal plane of symmetry, the relation between the convergent segment (4) length projected on the rolling axis of symmetry L_k and the wing (2) chord length with its maximum value L_{max} lies in the range $0.1 < L_k / L_{max} < 0.4$; the wing transitional segment (5) is actually a sectorial symmetrical double-curved saddle-shaped surface with longitudinal grooves (7, 8), the transitional segment (5) comprises the wing (2) throat which has the minimum cross-sectional area and is perpendicular to the wing (2) vertical longitudinal plane of symmetry, in the longitudinal plane of symmetry, the relation between the transitional segment (5) length projected on the rolling axis of symmetry L_t and the wing (2) chord length with its maximum value L_{max} lies in the range $0.1 < L_t / L_{max} < 0.4$; the divergent segment (6) of the wing is actually a sectorial part of a symmetrical conical surface with longitudinal grooves (7, 8), the divergent segment (6) is made with a provision for the positive increment of the wing (6) underlying surface area over the wing (6) length, longitudinally along the flow, the opening angle of the entire sectorial part of the wing (6) divergent segment γ_d lies in the range $150^0 < \gamma_d < 220^0$, the relation between the sectorial angle of the wing (6) divergent segment γ_{dc} and the opening angle of the entire sectorial part of the wing divergent segment γ_d lies in the range $0.5 < \gamma_{dc} / \gamma_d < 0.8$, in the longitudinal plane of symmetry, the relation between the divergent segment (6) length projected on the rolling axis of symmetry L_d and the wing (2) length chord with its maximum value L_{max} lies in the range $0.2 < L_d / L_{max} < 0.8$; the deflection angle for the deflectable controlled element (9) θ lies in the range from $0^0 < \theta < 40^0$.

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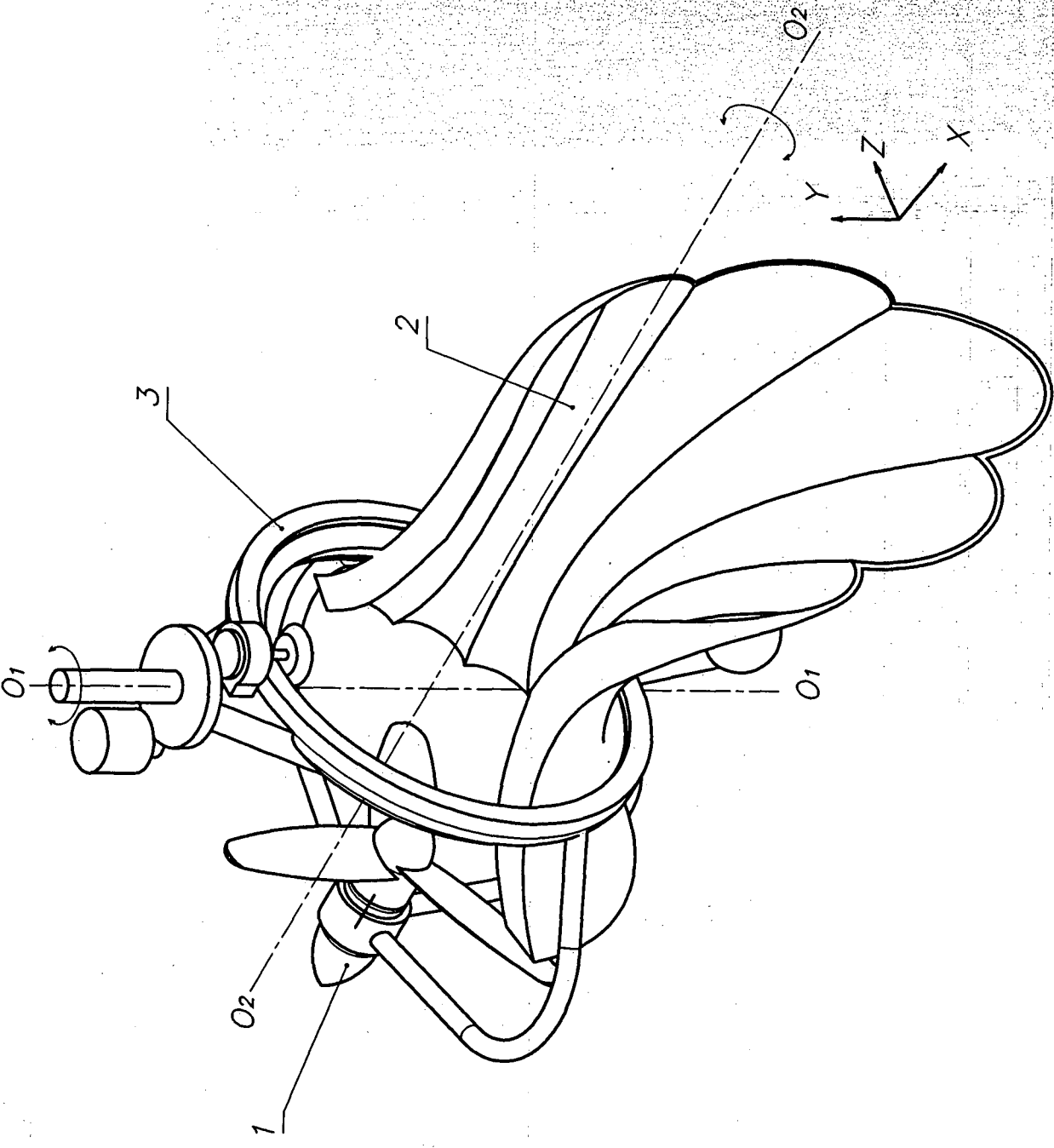


Fig. 1

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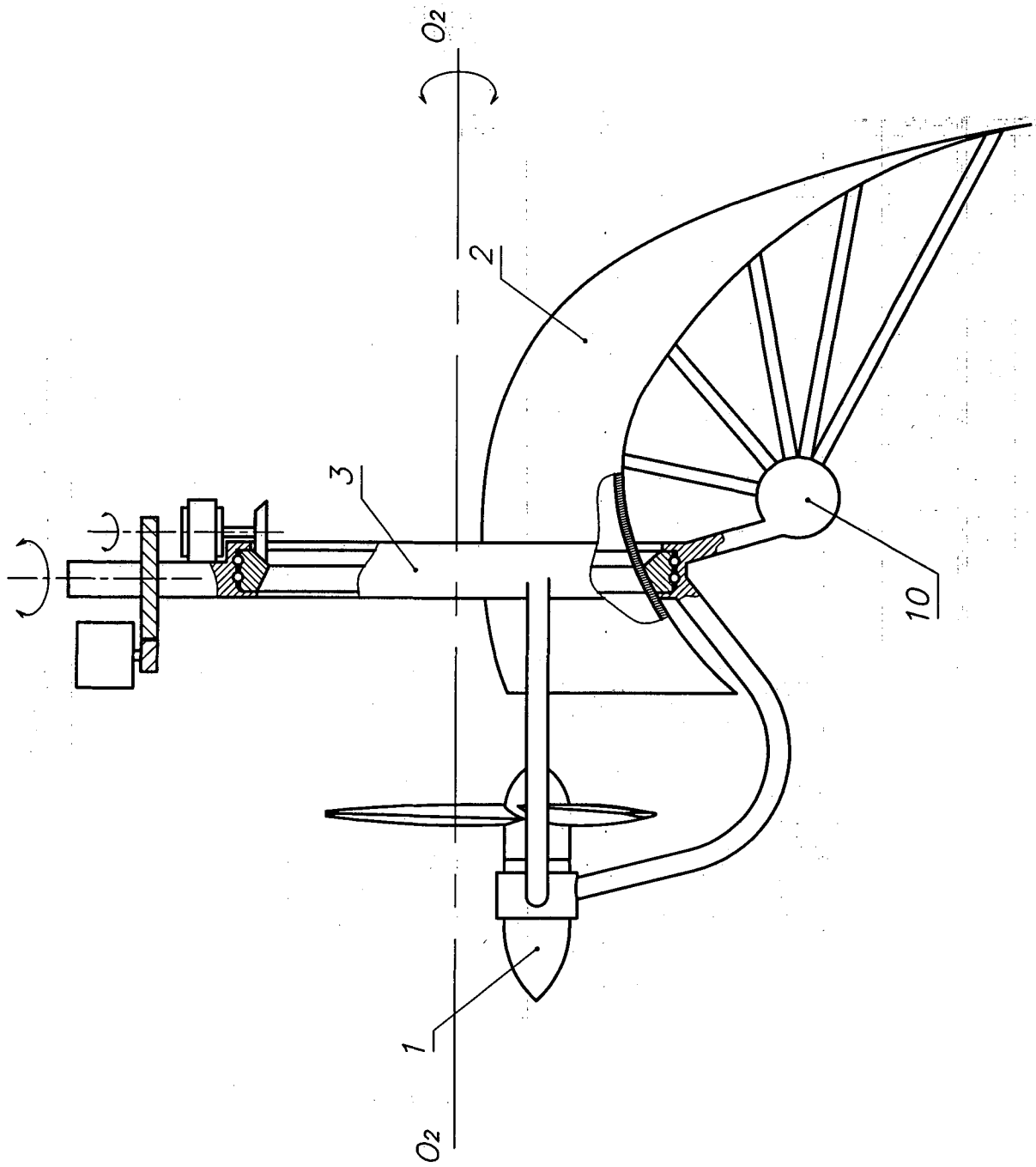


Fig. 2

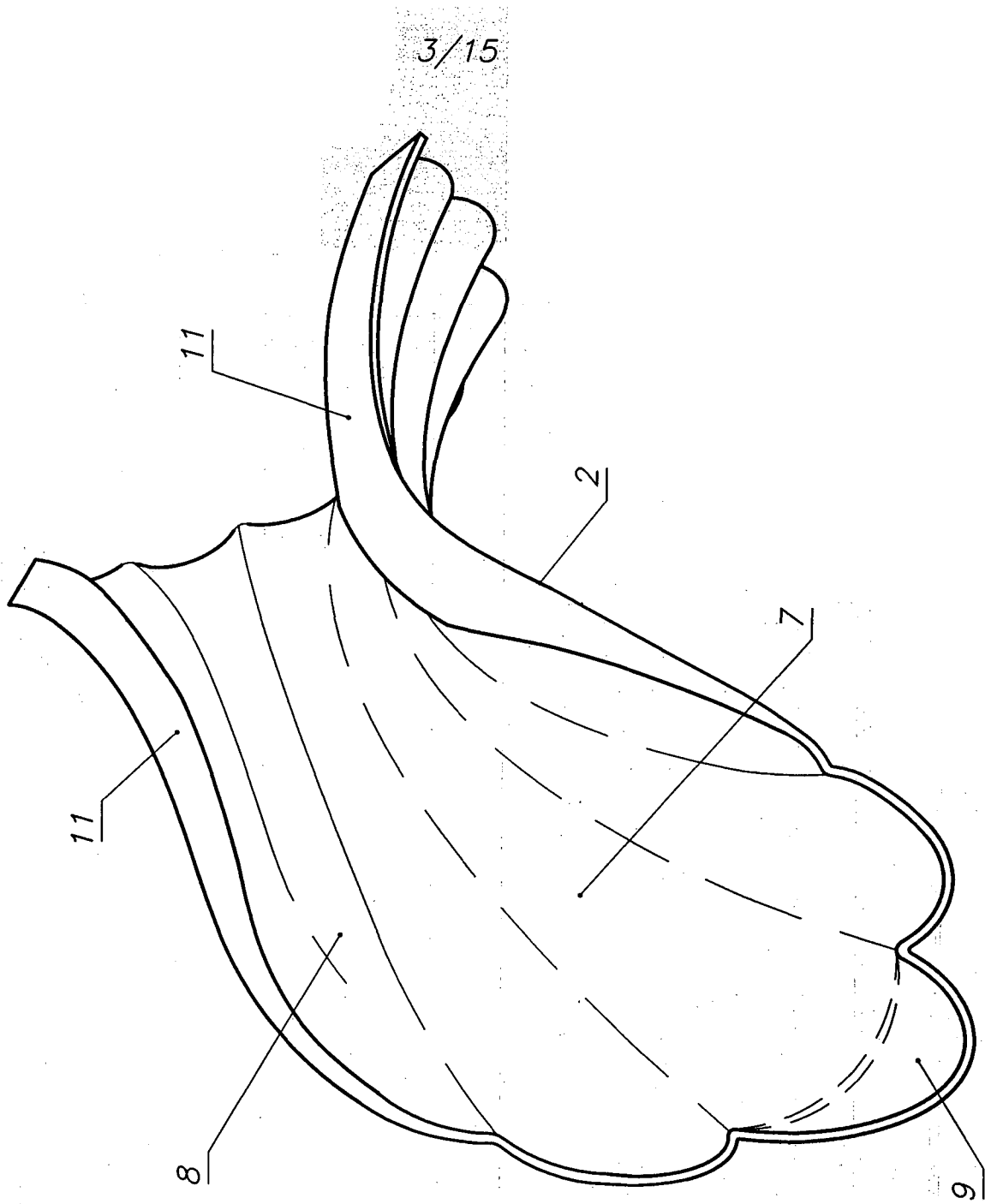


Fig. 3

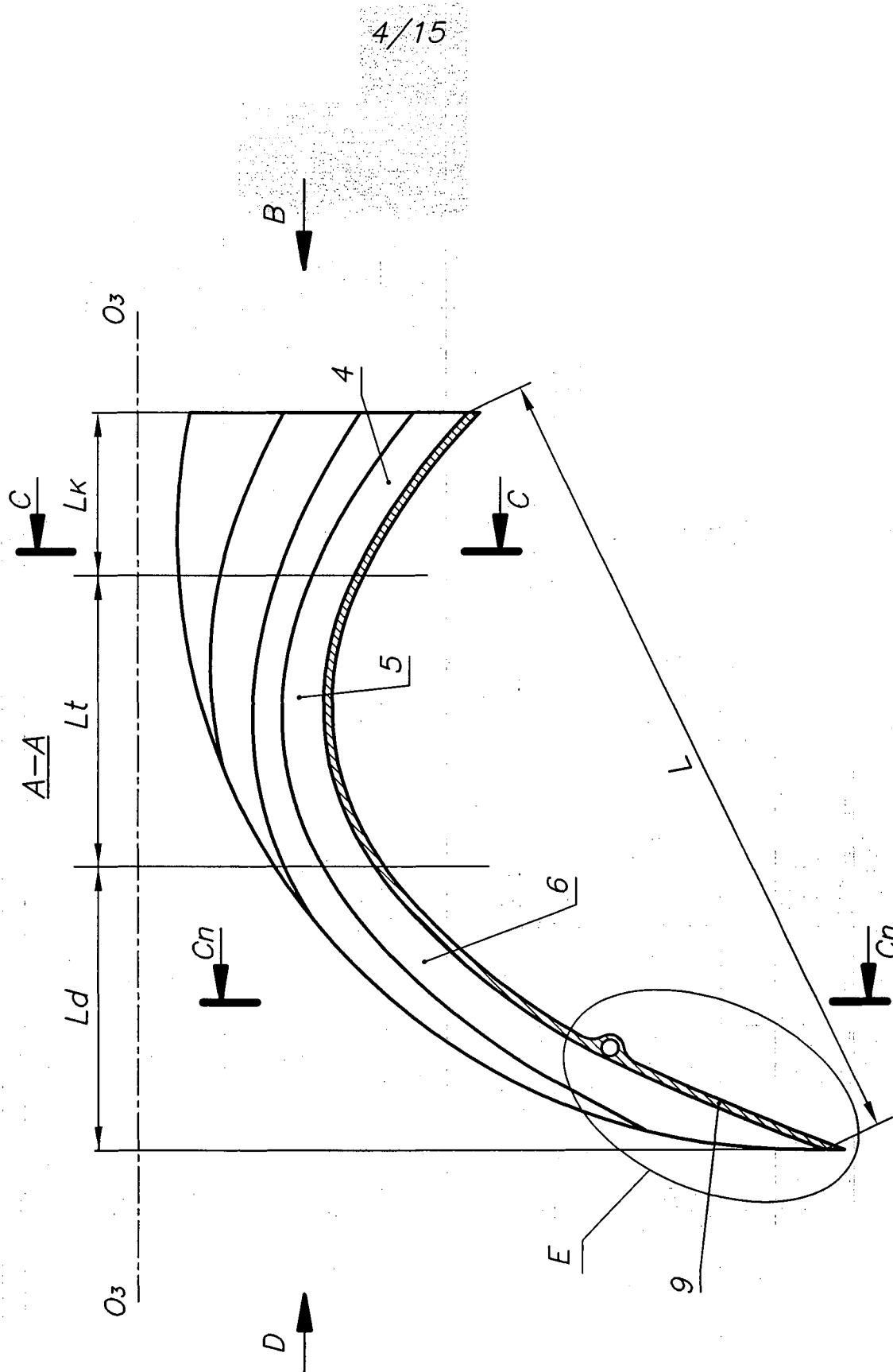


Fig. 4

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View B

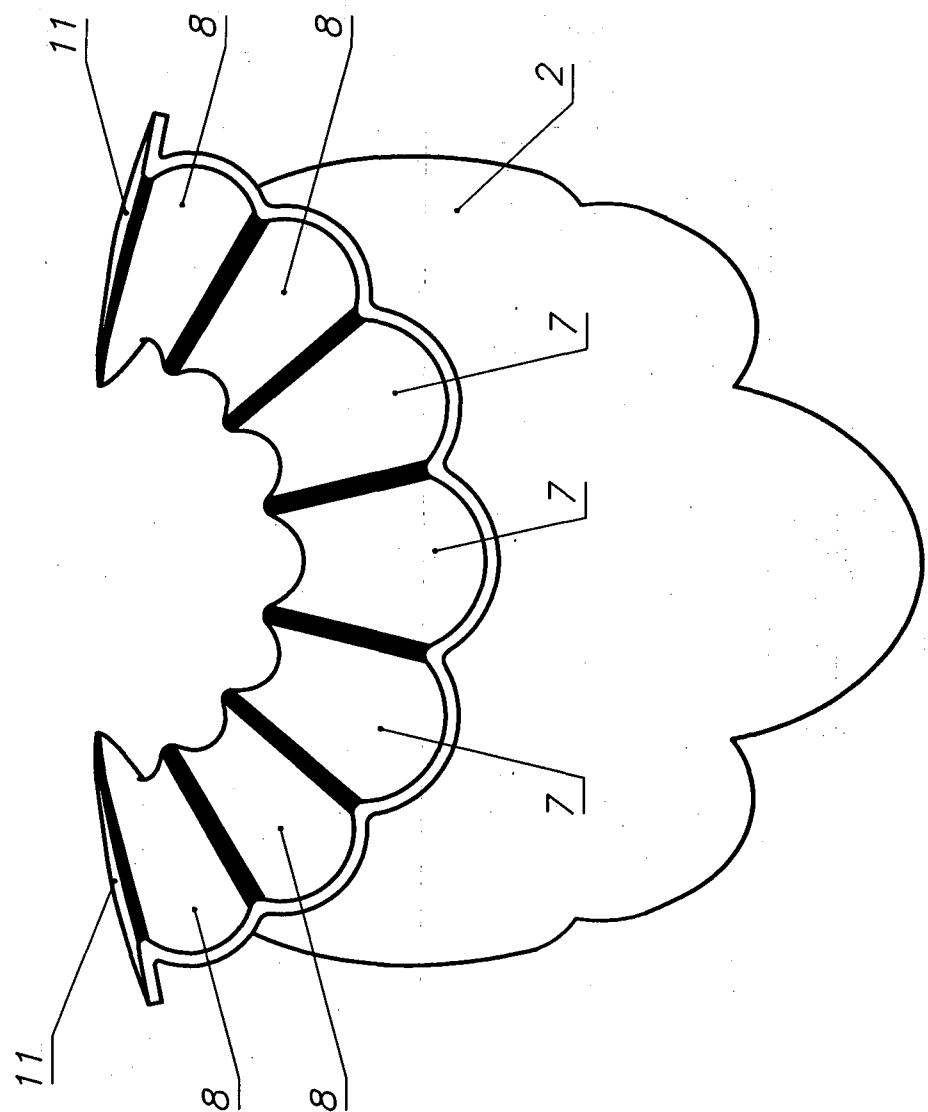


Fig. 5

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C-C

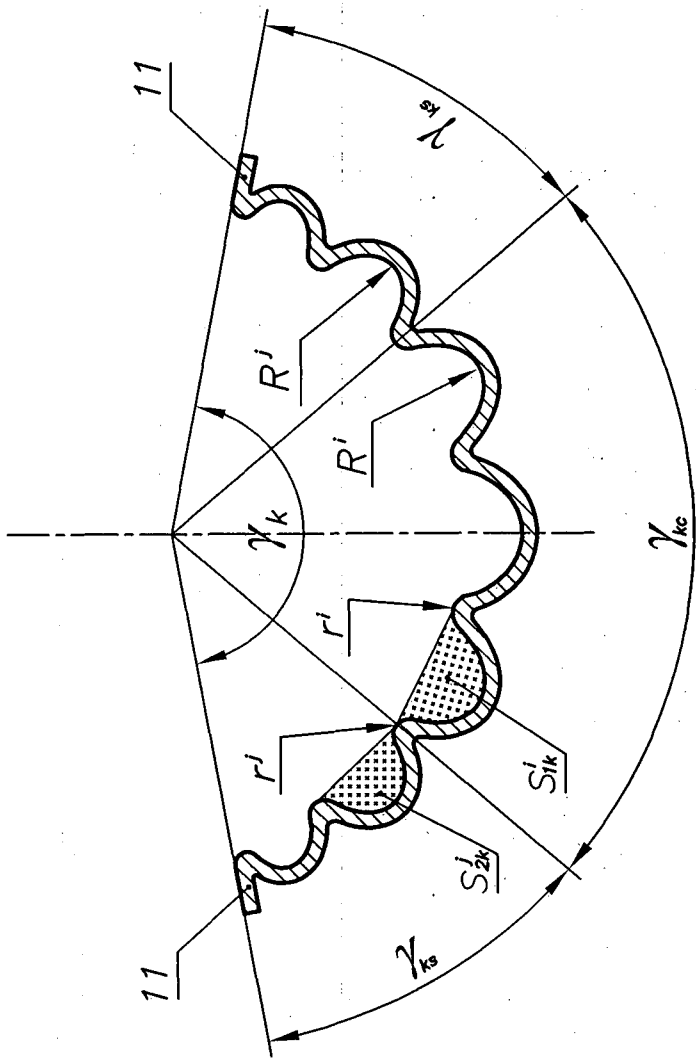


Fig. 6

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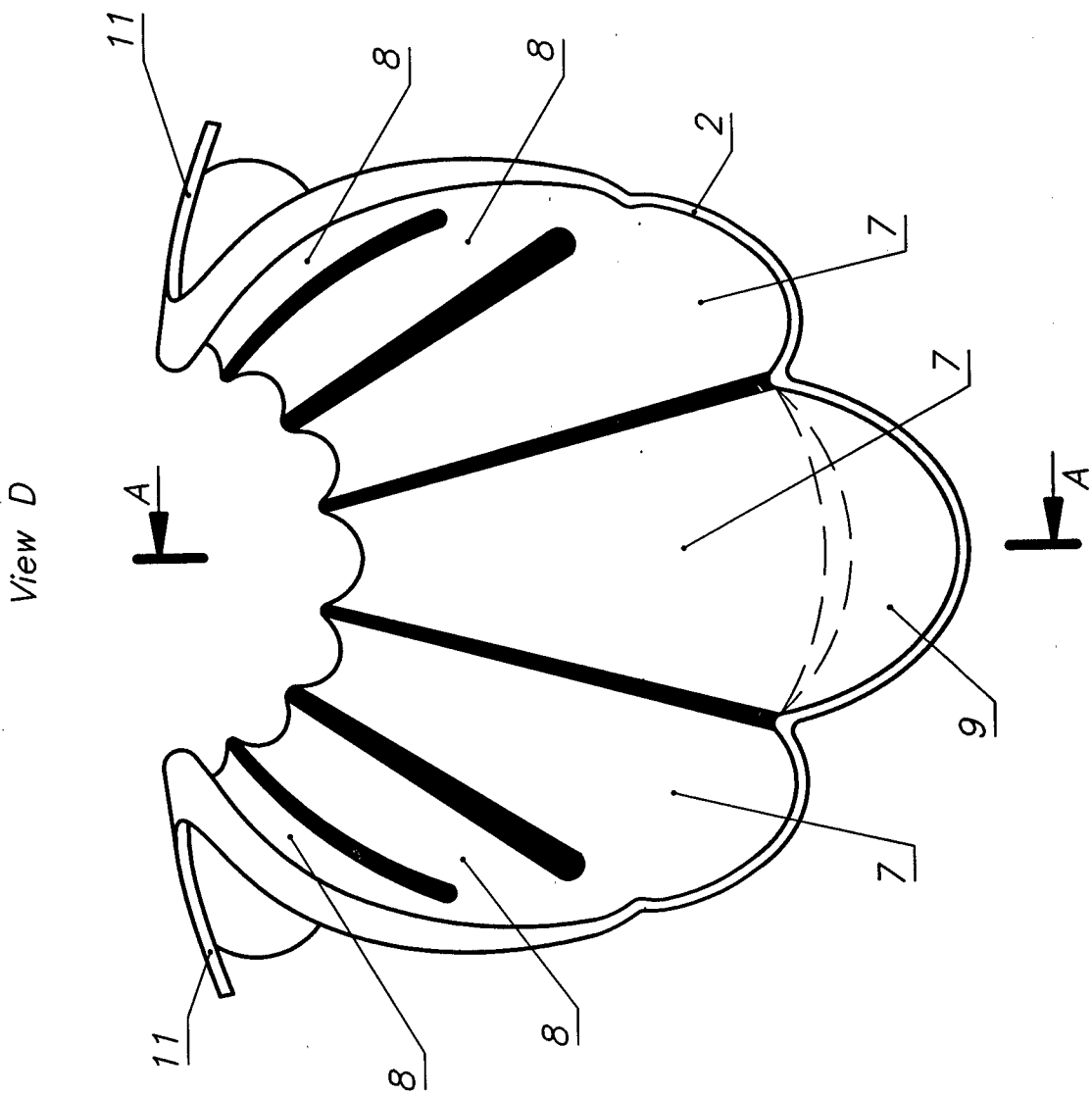


Fig. 7

$Cn - Cn$

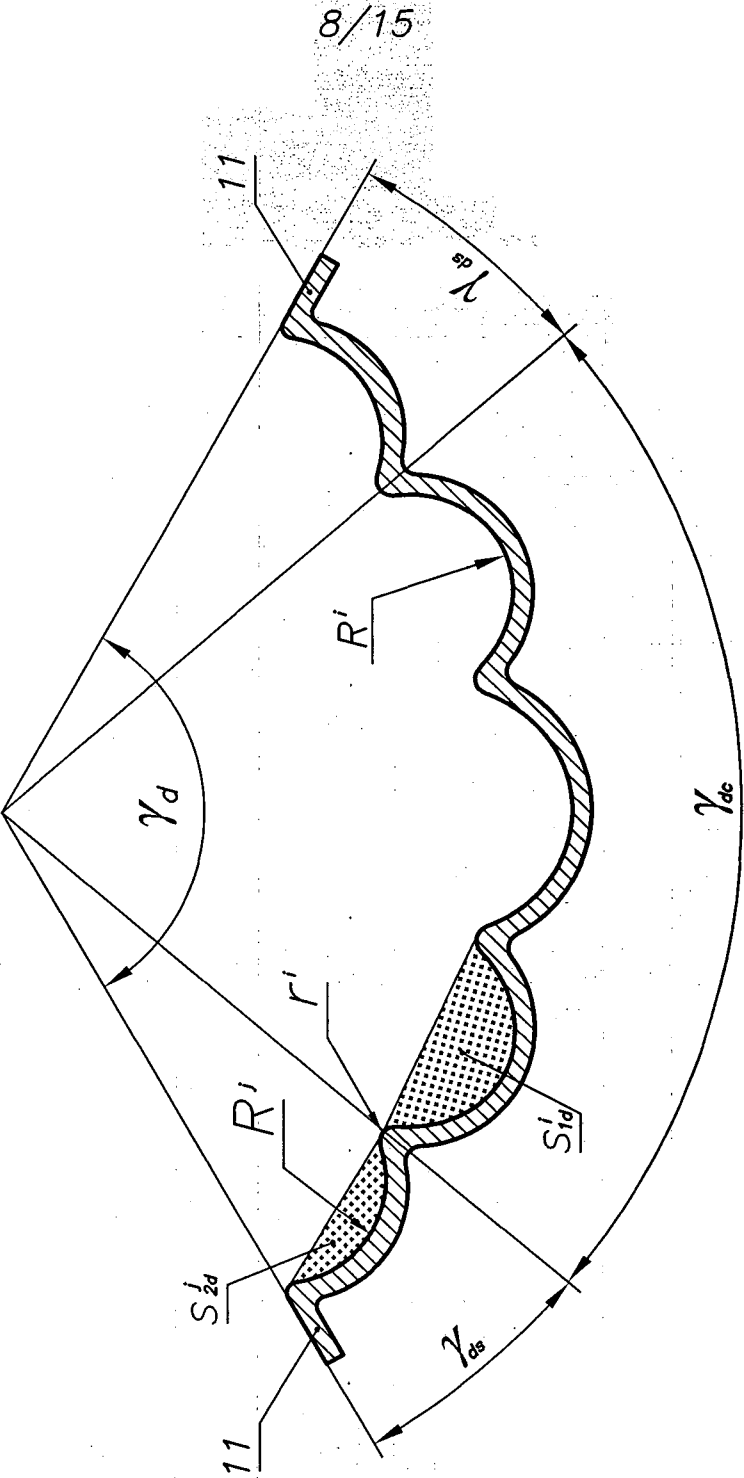


Fig. 8

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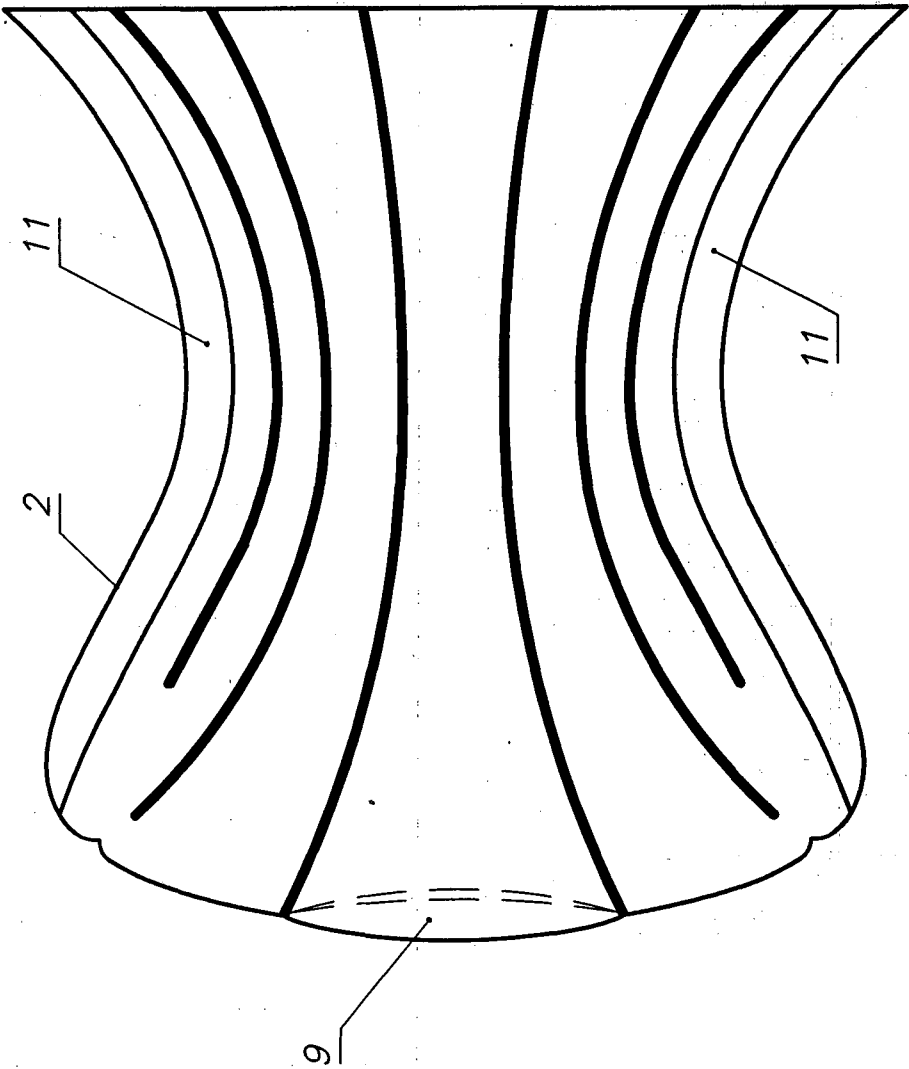


Fig. 9

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Figure 10

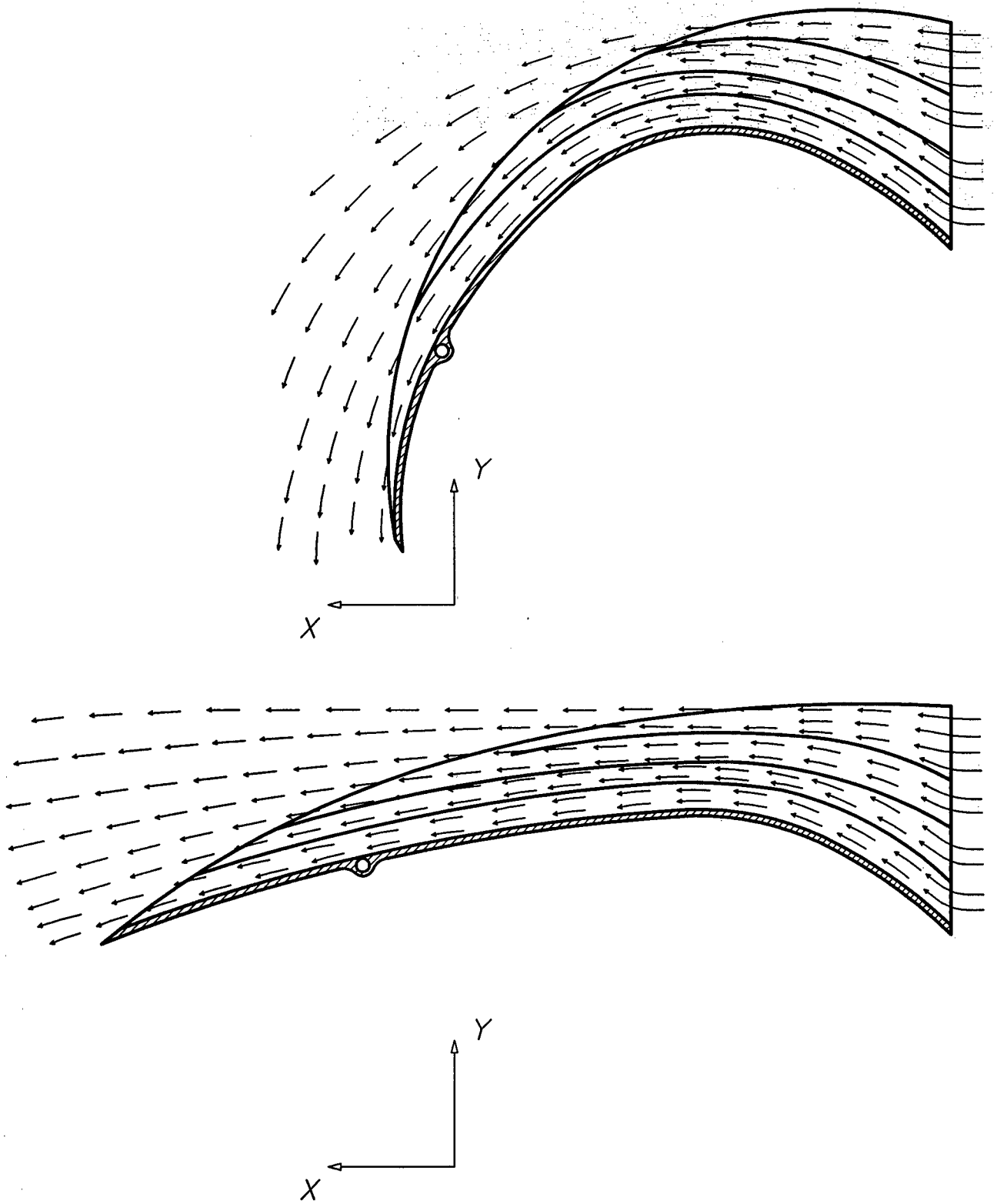


Fig. 10

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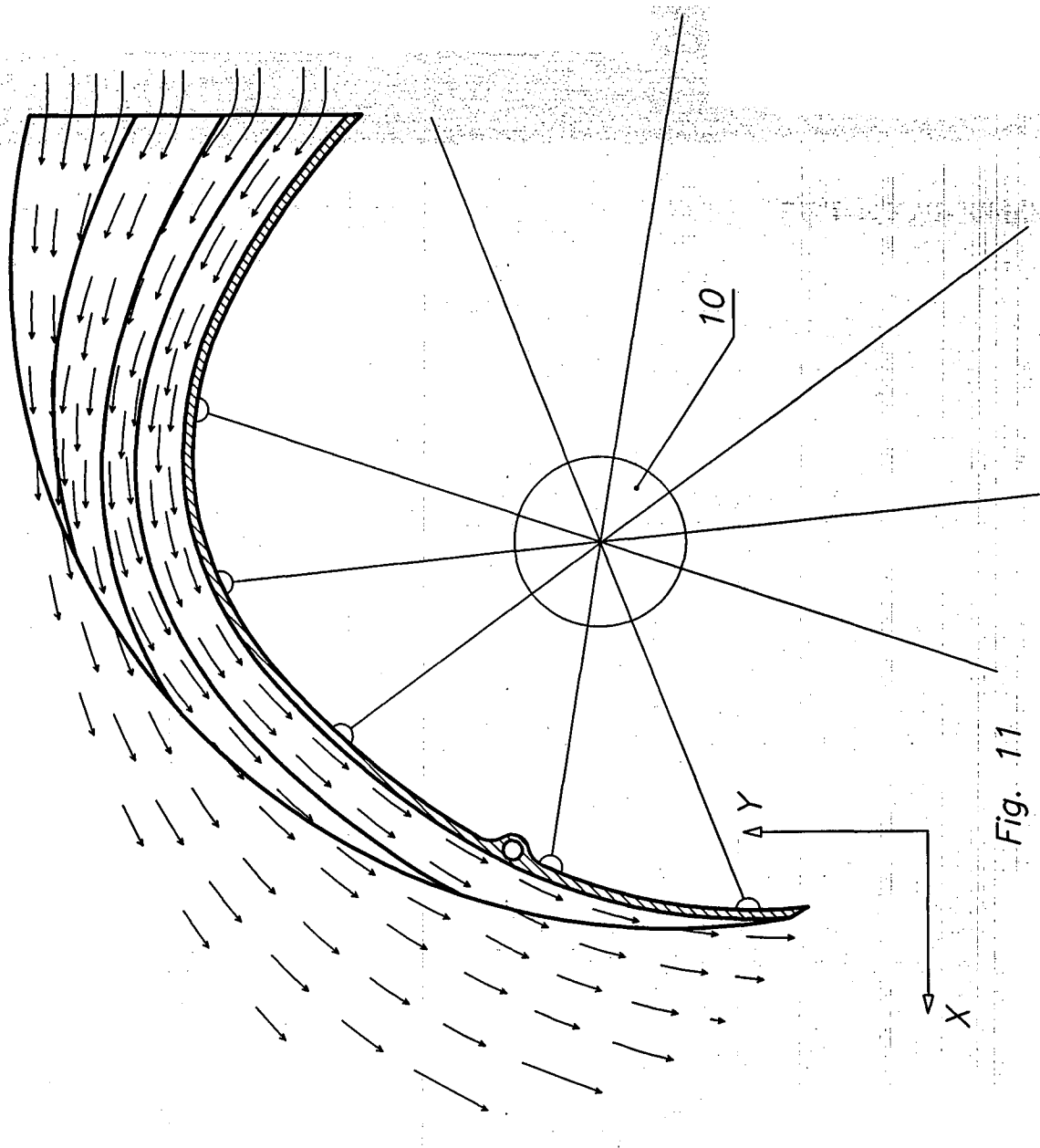
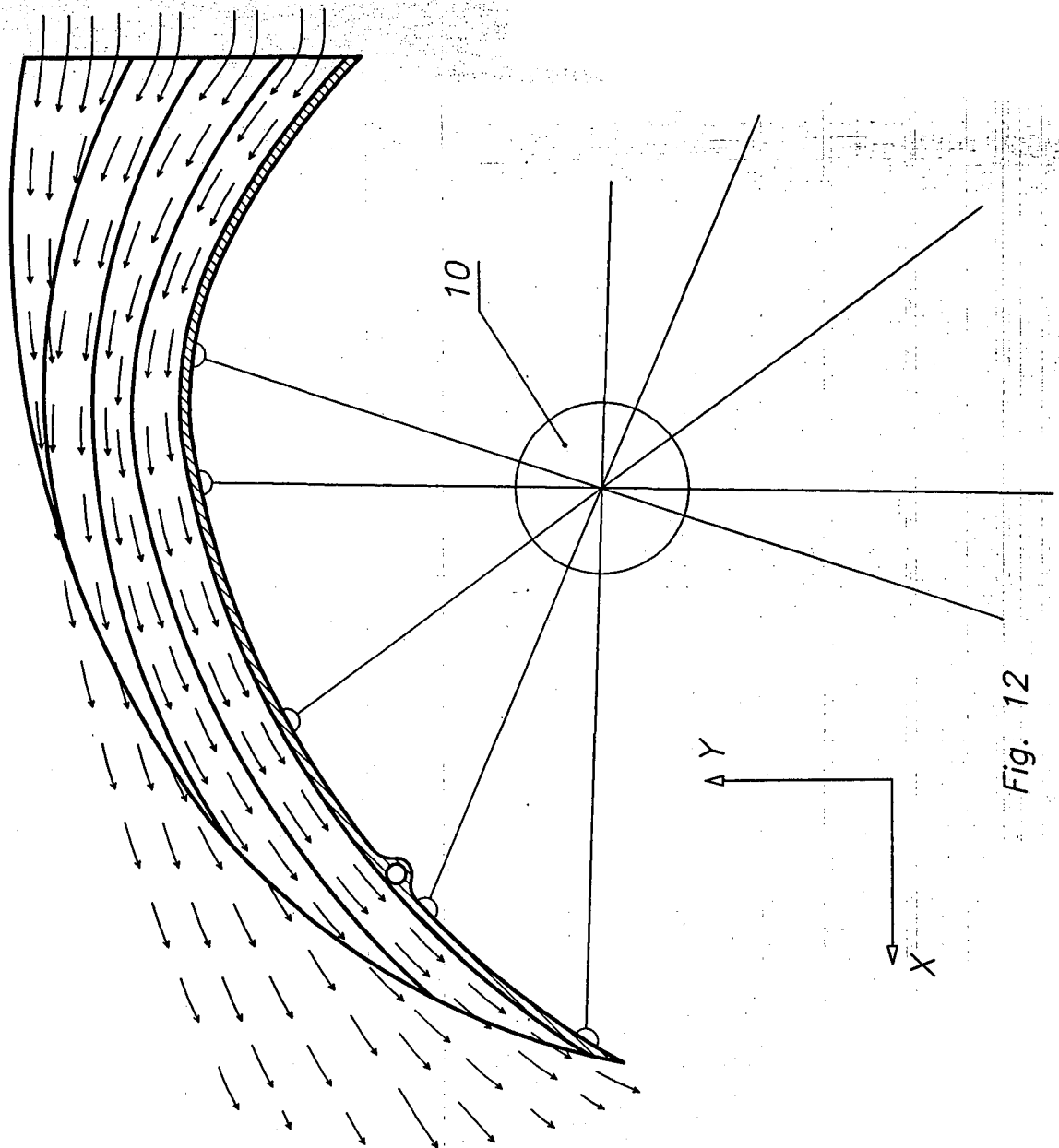
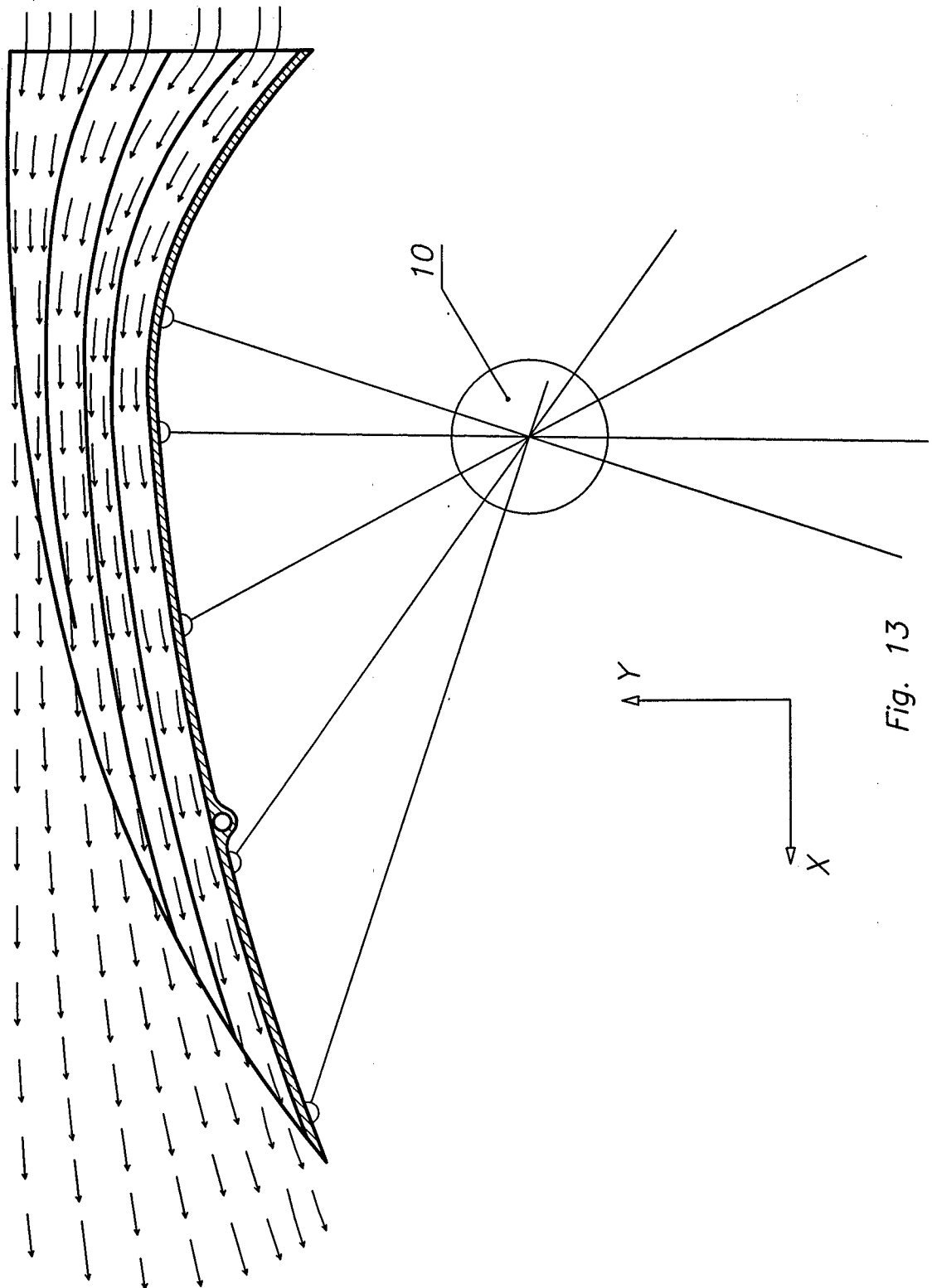


Fig. 11

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View E

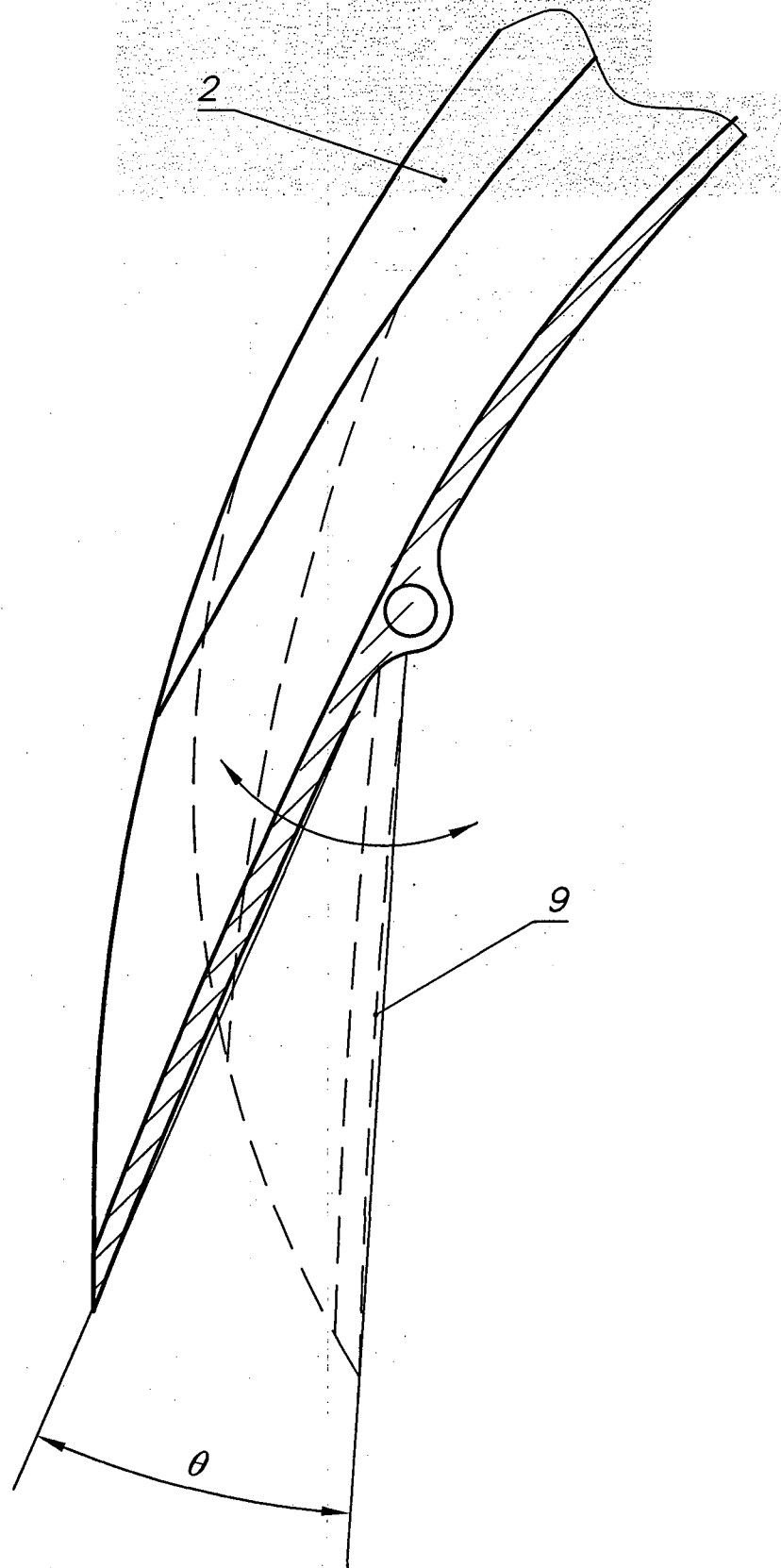


Fig. 14

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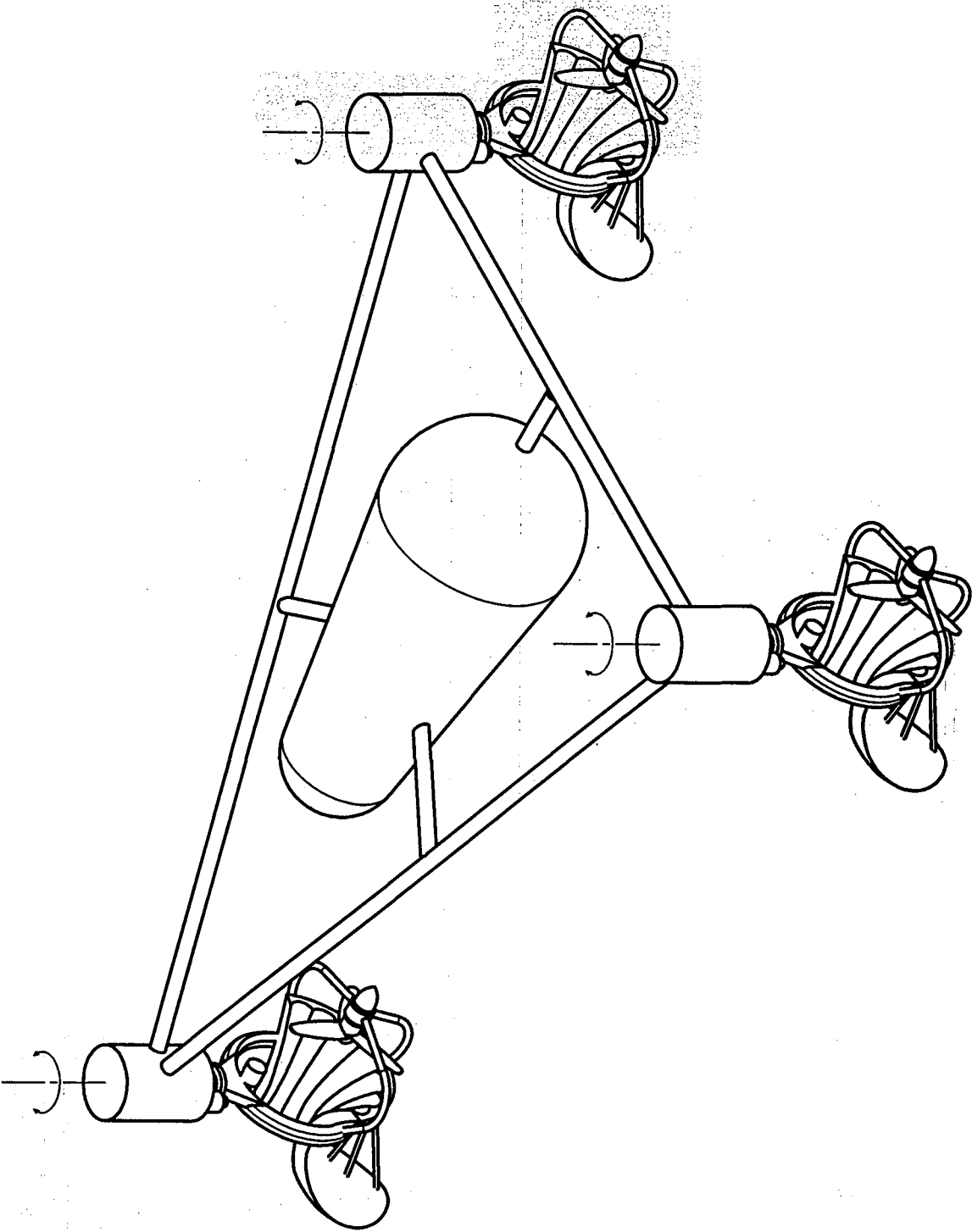


Fig. 15

INTERNATIONAL SEARCH REPORT

International application No
PCT/KZ2015/000008

A. CLASSIFICATION OF SUBJECT MATTER INV. B64C9/38 B64C15/14 B64C21/10 B64C29/00 ADD.		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) B64C		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) EPO-Internal, PAJ, WPI Data		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2 691 494 A (CUSTER WILLARD R) 12 October 1954 (1954-10-12) cited in the application column 1, line 41 - column 2, line 34; figures 1-3	1,2
A	----- EP 2 597 037 A2 (ROLLS ROYCE PLC [GB]) 29 May 2013 (2013-05-29) paragraphs [0017] - [0021]; figure 2	1,2
A	----- US 4 830 315 A (PRESZ JR WALTER M [US] ET AL) 16 May 1989 (1989-05-16) column 6, line 58 - column 7, line 39; figures 2-5 -----	1,2
<div style="display: flex; justify-content: space-between;"> <input type="checkbox"/> Further documents are listed in the continuation of Box C. <input checked="" type="checkbox"/> See patent family annex. </div>		
<div style="display: flex;"> <div style="flex: 1;"> <p>* Special categories of cited documents :</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier application or patent but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="flex: 1;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&" document member of the same patent family</p> </div> </div>		
Date of the actual completion of the international search <div style="text-align: center; font-size: 1.2em;">4 November 2015</div>		Date of mailing of the international search report <div style="text-align: center; font-size: 1.2em;">24/11/2015</div>
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016		Authorized officer <div style="text-align: center; font-size: 1.2em;">Busto, Mario</div>

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/KZ2015/000008

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2691494	A	12-10-1954	NONE
EP 2597037	A2	29-05-2013	EP 2597037 A2 29-05-2013
		US 2013336781 A1	19-12-2013
US 4830315	A	16-05-1989	NONE