

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
19 April 2012 (19.04.2012)

(10) International Publication Number
WO 2012/050424 AI

(51) International Patent Classification:
A61B 17/68 (2006.01)

(21) International Application Number:
PCT/MY20 11/000213

(22) International Filing Date:
21 September 2011 (21.09.2011)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
PI201000485 1 14 October 2010 (14.10.2010) MY

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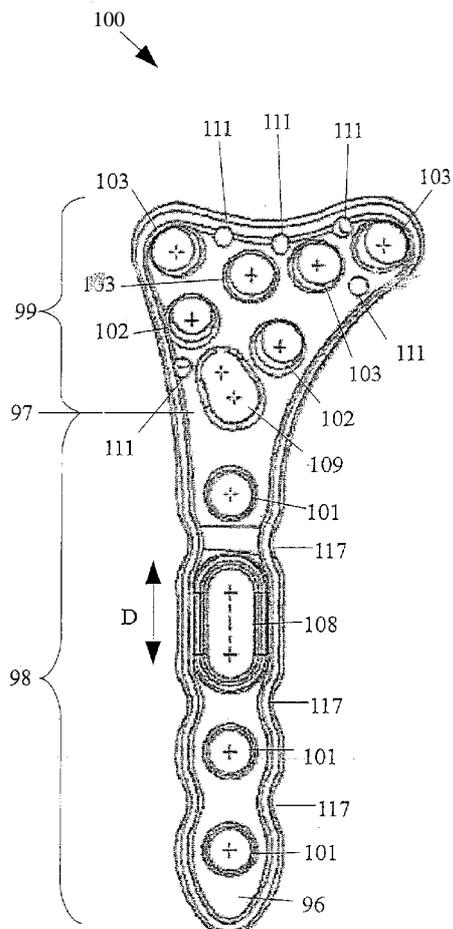
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[Continued on nextpage]

(54) Title: A DISTAL RADIUS PLATING SYSTEM

Figure 1

(57) Abstract: A bone plate (100) for fixing distal radius (405) fracture comprising a volar-shaped head (99) to be positioned at the distal radius (405); a shaft (98) inclinedly extending from the head (99); a plurality of K-wire openings (111) distributed over the head (99) for receiving K-wires (118) to temporarily secure the plate (100); and a plurality of fastening means openings (101, 102, 103, 108) distributed over the head (99) and the shaft (98) for receiving fastening means (104, 105, 106, 107) to fix the plate (100) to the distal radius (405); characterized by an insertion cavity (109) formed at the junction of the head (99) and the shaft (98) in such a manner as to provide an accessible space for efficient insertion of bone graft material.



WO 2012/050424 A1

(81) **Designated States** (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) **Designated States** (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH,

GM, KE, LR, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

- with international search report (Art. 21(3))
- before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments (Rule 48.2(h))

A DISTAL RADIUS PLATING SYSTEM

FIELD OF INVENTION

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The present invention relates to a plating system for internal fixation of bone fracture. In more particular, the present invention provides a bone plate for the fracture fixation and management of intra or extra-articular fracture of the distal radius bone, which effectively promotes the healing of the bone fracture.

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BACKGROUND OF THE INVENTION

A distal radius fracture is a common bone fracture occurred at the radius of the forearm, which is positioned proximately to the wrist joint. It is sometimes known as Colles's fracture, Smith's fracture, Barton's fracture or Chauffeur's fracture, or generally known as wrist fracture. As the distal end of human radius is made up of cancellous bone, any fracture occurred at this region will usually give rise to the collapse of this structure in the later phase. Therefore, proper treatment methods are necessary to be applied for fixing and managing the fracture.

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One of the contemporary treatment options for distal radius fracture is the surgery approach. During the orthopedic surgery, an internal fixator, such as a bone plate, can be implanted into the bone at the fracture region. This internal fixation technique is capable of facilitating the healing of the fracture. Therefore, the configuration and performance of a bone plate is vital to the cure of this injury.

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There are several patented technologies disclosed in the prior arts relating to the distal radius plating systems. Of interest in connection with a distal radius plate is disclosed in U.S. Patent No. 2007265629. The distal radius plate comprises a head portion and a

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proximal plate portion, wherein the head portion has a palm shaped profile having a complex topography that is substantially free from any planar areas. The plate also has at least one fixed peg hole which is threaded and at least one variable angle peg hole with a locking mechanism that permits a variable angle peg to be locked into a
5 desired position.

Another highly-versatile variable-angle bone plate system is disclosed in U.S. Patent No. 2008140130. This bone plate system includes a plurality of holes constructed to receive either a non-locking, locking, or variable-angle locking bone screw. The holes
10 have discrete columns of teeth or thread segments arranged around the inner surface of the hole for engaging threads on the heads of locking and variable-angle locking bone screws. Variable-angle locking bone screws can engage the bone plate at within a range of selectable angles. The head of the variable-angle locking screw is at least partially spherical, and the thread thereon has a profile that follows the arc-shaped
15 radius of curvature of the spherical portion of the screwhead.

U.S. Patent No. 2006004362 also discloses a distal radius bone plating system with locking and non-locking screws. This bone plate can be applied for the fixation of distal or proximal ends of long bones. It also has a head portion and a shaft portion
20 having a plurality of plate holes and a plurality of locking and non-locking screws. The locking bone screws can be threaded and the non-locking cancellous bone screws are configured and dimensioned to have a particularly useful dimensional relationship.

25 There is another U.S. Patent No. 2005065524 relating to an anatomical distal radius fracture fixation plate with fixed-angle Kirschner wire (K-wire) holes which define a three-dimensional surface. This fixation plate includes a set of threaded peg holes adapted to individually receive fixation pegs therethrough and non-threaded alignment holes having a relatively smaller diameter than the peg holes and preferably
30 sized to closely receive a K-wire. The alignment holes are located between the peg

holes, in which one alignment hole is configured for aligning the plate, while other alignment holes are configured for use after fracture reduction and receive K-wires to temporarily stabilize the fracture and secure the plate to the bone. The head of the plate has a shape and contour which provide bone support and a low profile which
5 minimizes the potential for soft tissue irritation.

To further strengthen the fixation bone fracture, bone graft can be applied together with the bone plate as a filler material. Generally, there are several types of bone grafts used, namely autograft, allograft, xenograft and synthetic bone graft. Autograft
10 and synthetic bone graft are commonly used in distal radius fracture. The bone graft can be inserted and packed into the fracture region. The bone graft will fill up the gaps and spaces caused by the fracture and interdigitate the spaces within the cancellous bone. However, the process of packing the bone graft after fixing the
15 fracture with plate and screws can be challenging. This is because the screw holes on the bone plate are usually small and not designed to adapt for the efficient insertion of bone graft. Thus, the volume of bone graft that can be inserted at the fracture region are limited and wastage of bone graft can occur as most of the bone graft, especially the paste form, will spill out from the fracture region.

20 As revealed by the patented technologies, most of the prior arts disclose a low profile design of the bone plate. Besides, various types of screws including fixed angle and variable angle screws have also been described by the existing technologies. However, none of the existing technologies discloses a distal radius bone plate which is designed and configured to adapt for the efficient insertion of bone graft during the
25 internal fixation process. It is therefore desirable for the present invention to provide a distal radius bone plate having innovative design and configuration which are capable of overcoming the drawbacks of the prior arts and providing a more efficient surgery treatment for distal radius fracture.

SUMMARY OF INVENTION

The primary object of the present invention is to provide an innovative bone plate for fixing distal radius fracture which is designed and configured to allow and to ease the
5 insertion and packing of bone graft into the fracture region during the internal fixation process, thus enhancing the fixation of the bone fracture and promoting healing thereof.

Another object of the present invention is to provide a distal radius bone plate which
10 has anatomic low profile design that matches with the topography of the distal radius, and comparable with the existing distal radius bone plating technologies.

Still another object of the present invention is to provide a distal radius bone plate with optimum fixed angle construct for maximum fracture stability.

15 Yet another object of the present invention is to provide a distal radius bone plating system which is incorporated with specifically-designed screws that are capable of reducing stress within the bone of the patient and providing ease of screw purchasing for the surgeon.

20 Further object of the present invention is to provide a kit for fixing distal radius fracture which includes an innovative bone plate and variable effective fastening and fixing means.

25 At least one of the preceding objects is met, in whole or in part, by the present invention, in which one of the embodiments of the present invention describes a bone plate (100) for fixing distal radius (405) fracture comprising a volar-shaped head (99) to be positioned at the distal radius (405); a shaft (98) inclinedly extending from the head (99); a plurality of K-wire openings (111) distributed over the head (99) for
30 receiving K-wires (118) to temporarily secure the plate (100); and a plurality of

fastening means openings (101, 102, 103, 108) distributed over the head (99) and the shaft (98) for receiving fastening means (104, 105, 106, 107) to fix the plate (100) to the distal radius (405); characterized by an insertion cavity (109) formed at the junction of the head (99) and the shaft (98) in such a manner as to provide an accessible space for efficient insertion of bone graft material.

One of the preferred embodiments of the present invention is a bone plate (100) wherein the head (99) has a thickness of 1.5 mm to 2.5 mm, and is tapered from the junction of the head (99) and the shaft (98), towards the distal end of the plate (100).

Another preferred embodiment of the present invention discloses that the shaft (98) has a thickness of 2.0 mm to 3.0 mm. Preferably, the shaft (98) has at least one waisted region (117) for uniform distribution of stresses.

Still another preferred embodiment of the present invention discloses that the pre-bended angle of inclination between the head (99) and the shaft (98) lies within the range of 20° to 30°, most preferably 23°.

Yet another preferred embodiment of the present invention discloses that the plurality of K-wire openings (111) and fastening means openings (101, 102, 103, 108) are chamfered outwardly towards the bottom surface of the plate (100) to allow flexible movement of the K-wires (118) and the fastening means (104, 105, 106, 107).

In yet another preferred embodiment of the present invention, it is disclosed that the fastening means (104, 105, 106, 107) are locking screws (104), cortical screws (105), smooth pegs (106), threaded pegs (107) or a combination of any two or more thereof.

Preferably, the plurality of fastening means openings (103) at the distal end of the head (99) are aligned in an arc (400) to allow the fastening means (104, 105, 106, 107) to engage subchondral regions of the distal radius (405). Further, others of the

fastening means openings (102) are aligned on the head (99) in such a manner as to allow the fastening means (104, 105, 106, 107) to engage volar and medial subchondral regions of the distal radius (405).

5 Another preferred embodiment of the present invention also discloses that still further fastening means openings (101, 108) are aligned along the longitudinal axis of the shaft (98). Preferably, the plurality of fastening means openings (101, 102, 103, 108) are round or oblong in shape.

10 According to another preferred embodiment of the present invention, the insertion cavity (109) is gourd-shaped, pear-shaped or kidney-shaped. Preferably, a chamfer (200) is outwardly formed around the insertion cavity (109) toward its bottom surface (95) to allow maximum reach of a bone graft syringe at any angle through the cavity (109).

15

Further embodiment of the present invention is a bone plate (100) for fixing distal radius (405) fracture which is made of titanium, titanium alloy or stainless steel.

Still further embodiment of the present invention is a kit (300) for fixing distal radius
20 (405) fracture comprising a plurality of K-wires (118); a plurality of fastening means (104, 105, 106, 107) and a bone plate having a volar-shaped head (99) to be positioned at the distal radius (405); a shaft (98) inclinedly extending from the head (99); a plurality of K-wire openings (111) distributed over the head (99) for receiving K-wires (118) to temporarily secure the plate (100); and a plurality of fastening means
25 openings (101, 102, 103, 108) distributed over the head (99) and the shaft (98) for receiving fastening means (104, 105, 106, 107) to fix the plate (100) to the distal radius (405); characterized by an insertion cavity (109) formed at the junction -of the head (99) and the shaft (98) in such a manner as to provide an accessible space for efficient insertion of bone graft material.

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One skilled in the art will readily appreciate that the present invention is well adapted to carry out the objects and obtain the ends and advantages mentioned, as well as those inherent therein. The embodiments described herein are not intended as limitations on the scope of the invention.

5

BRIEF DESCRIPTION OF THE DRAWINGS

For the purpose of facilitating an understanding of the invention, there is illustrated in the accompanying drawing the preferred embodiments from an inspection of which when considered in connection with the following description, the invention, its construction and operation and many of its advantages would be readily understood and appreciated.

15 Figure 1 is a top view of the distal radius bone plate (100) as described in one of the preferred embodiments of the present invention.

Figure 2 is a bottom view of the distal radius bone plate (100) of Figure 1 showing the longitudinal A-A axis of the plate (100).

20

Figure 3 is a perspective view of the distal radius bone plating kit (300) as described in one of the preferred embodiments of the present invention, showing the positioning of the K-wires (118) and various types of fastening means (104, 105, 106, 107) on the plate (100).

25

Figure 4 is a front view of the distal radius bone plating kit (300) of Figure 3, showing the head (99) of the plate (100) and the angulations of the fastening means (104, 106, 107).

30 Figure 5 is a side view of the distal radius bone plating kit (300) of Figure 3,

showing the angle of inclination, α , formed between the head (99) and the shaft (98).

Figure 6(a) is a partial top view of the distal radius bone plate (100) of Figure 1.

5

Figure 6(b) is a cross-sectional view through the B-B axis of Figure 6(a), showing the head inclination angle, β , of the head (99) of the bone plate (100).

Figure 7 shows the top view of the distal radius bone plate (100) of Figure 1 when it is positioned on the distal radius (405).

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Figure 8(a) is a top view of the distal radius bone plate (100) of Figure 1 showing the angular definition of the fastening means openings (101, 102, 103, 108).

15

Figure 8(b) is a cross-sectional perspective view through the C-C axis of Figure 8(a) showing the contact threads between the fastening means (104, 106, 107) and the plate (100).

Figure 9(a) is a side view of a locking self-tapping screw of the distal radius bone plating kit (300) as described in one of the preferred embodiments of the present invention.

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Figure 9(b) is a top view of the locking self-tapping screw of Figure 9(a).

25

Figure 9(c) is a cross-sectional view of the locking self-tapping screw of Figure 9(a).

Figure 9(d) is a side perspective view of the locking self-tapping screw of Figure 9(a).

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Figure 10(a) is a side view of a cortical self-tapping screw of the distal radius bone plating kit (300) as described in one of the preferred embodiments of the present invention.

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Figure 10(b) is a top view of the cortical self-tapping screw of Figure 10(a).

^{3/4} Figure 10(c) is a cross-sectional view of the cortical self-tapping screw of Figure 10(a).

10

Figure 10(d) is a side perspective view of the cortical self-tapping screw of Figure 10(a).

Figure 11(a) is a side view of a locking self-tapping threaded peg of the distal radius bone plating kit (300) as described in one of the preferred embodiments of the present invention.

15

Figure 11(b) is a top view of the locking self-tapping threaded peg of Figure 11(a).

20 Figure 11(c) is a cross-sectional view of the locking self-tapping threaded peg of Figure 11(a).

Figure 11(d) is a side perspective view of the locking self-tapping threaded peg of Figure 11(a).

25

Figure 12(a) is a side view of a locking smooth peg of the distal radius bone plating kit (300) as described in one of the preferred embodiments of the present invention.

30 Figure 12(b) is a top view of the locking smooth peg of Figure 12(a).

Figure 12(c) is a cross-sectional view of the locking smooth peg of Figure 12(a).

Figure 12(d) is a side perspective view of the locking smooth peg of Figure 12(a).

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DETAILED DESCRIPTION OF THE INVENTION

The present invention relates to a plating system for internal fixation of bone fracture.

10 In more particular, the present invention provides a bone plate for the fracture fixation and management of intra or extra-articular fracture of the distal radius bone, which effectively promotes the healing of the bone fracture.

Hereinafter, the invention shall be described according to the preferred embodiments
15 of the present invention and by referring to the accompanying description and drawings. However, it is to be understood that limiting the description to the preferred embodiments of the invention and to the drawings is merely to facilitate discussion of the present invention and it is envisioned that those skilled in the art may devise various modifications without departing from the scope of the appended claim.

20

The present invention discloses a bone plate (100) for fixing distal radius (405) fracture comprising a volar-shaped head (99) to be positioned at the distal radius (405); a shaft (98) inclinedly extending from the head (99); a plurality of K-wire openings (111) distributed over the head (99) for receiving K-wires (118) to temporarily secure the plate (100); and a plurality of fastening means openings (101,
25 102, 103, 108) distributed over the head (99) and the shaft (98) for receiving fastening means (104, 105, 106, 107) to fix the plate (100) to the distal radius (405); characterized by an insertion cavity (109) formed at the junction of the head (99) and the shaft (98) in such a manner as to provide an accessible space for efficient insertion
30 of bone graft material.

Figure 1 and Figure 2 respectively show a top view and a bottom view of the distal radius bone plate (100) as described in one of the preferred embodiments of the present invention. This bone plate (100) is designed and configured into a unique anatomic low profile that provides optimum fixation support for the distal volar radius (405). The bone plate (100) shown in Figure 1 and Figure 2 is designed and configured for the right volar. It is to be noted that a left distal radius bone plate shall be substantially a mirror image of the plate (100) shown in Figure 2 which is having a longitudinal A-A axis.

10

As shown in Figure 1 and Figure 2, the distal radius bone plate (100) is made up of a head (99) and a shaft (98). The junction of the head (99) and the shaft (98) is considered as a neck (97). The wide V-shaped neck (97) with a radius curvature is capable of providing substantial strength to support the head (99) from the shaft (98).

15

One of the preferred embodiments of the present invention is a bone plate (100) in which the head (99), which is also known as the buttress head, has a thickness of 1.5 mm to 2.5 mm in order to maintain low profile of the plate (100). This design is capable of easing contouring or bending of the plate (100), thus reducing soft tissue irritation. Preferably, the thickness of the head (99) is gradually tapered from the junction of the head (99) and the shaft (98), towards the distal end of the plate (100), in which the shaft (98) has a thickness of 2.0 mm to 3.0 mm. The width of the head (99) is preferred to be approximately 20 mm to 30 mm, depending on the size of the user's volar. Most preferably, a standardized width of 25mm is generally made.

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However, the present invention does not intend to limit the width of the head (99), even though a wider plate is generally preferred for larger bone at a scale approximately 15% to 35% depending on the underlying bone size.

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According to the preferred embodiment of the present invention, the length of the plate (100) is preferably 55 mm to 65 mm, most preferably 60 mm, for a shaft (98)

with 4 fastening means openings (101, 102, 103, 108). However, it is to be noted the present invention does not intend to limit length of the plate (100). A longer plate (100) with more number of fastening means openings (101, 102, 103, 108) is preferred depending on the surgeon discretion on fracture pattern. Preferably, the shaft (98) has a few waisted regions (117) therealong for uniform distribution of stresses. More preferably, the edge of the shaft (98) volar shaped head (99) are fabricated into a smooth round shaped in order to reduce soft tissue irritation.

Still another embodiment of the present invention is a kit (300) for fixing distal radius (405) fracture comprising a plurality of K-wires (118); a plurality of fastening means (104, 105, 106, 107) and a bone plate as set forth in the foregoing description. Illustrated in Figure 3 is a perspective view of the distal radius bone plating kit (300) as described in the preferred embodiment, showing the positioning of the plurality of K-wires (118) and various types of fastening means (104, 105, 106, 107). The K-wire openings (111) are configured and dimensioned to receive K-wires (118) for temporarily stabilizing the fracture and securing the plate position during the fracture fixation process. As shown in Figure 4 and Figure 5, the K-wires (118) can be rotatably fitted on the plate (100) at the K-wire openings (111) in variable angles which provides flexibility to the movement of the K-wire during the positioning of the plate (100).

According to another preferred embodiment of the present invention, the plurality of fastening means openings (101, 102, 103, 108) are retrofittable for various types of fastening means (104, 105, 106, 107). It is also disclosed in the preferred embodiment that these fastening means (104, 105, 106, 107) can be locking screws (104), cortical screws (105), locking smooth pegs (106), locking threaded pegs (107) or a combination of any two or more thereof. The dimensions of these fastening means (104, 105, 106, 107) are further illustrated in Figure 9(a)-(d), 10(a)-(d), 11(a)-(d) and 12(a)-(d). Figure 4 shows the optimum exclusive angulations of the different types of fastening.

As illustrated in Figure 5, an angle of inclination, α , is formed between the head (99) and the shaft (98) at their junction, or the neck (97). According to the preferred embodiment of the present invention, the angle of inclination, α , is ranging from 20° to 27°. Most preferably, the pre-bended angle of inclination is 23°. However, the present invention does not intend to limit the size of the angle α as it can be varied depending on the underlying bone. In one of the preferred embodiments, the head (99) of the plate (100) can be inclined or skewed approximately 1° to 5° at the radial side in order to rest perfectly near to the volar ridge of the radial styloid. However, the present invention does not intend to limit the size of the angle, β , as it can be varied depending on the underlying bone. A cross-sectional view of the bone plate (100) showing the head inclination angle, β , of the head (99) is illustrated in Figure 6(b), which is obtained from the partial top view of the bone plate (100) through the B-B axis of Figure 6(a).

15

Referring to Figure 7, the plurality of fastening means openings (103) at the distal end of the head (99) are aligned in an arc (400), forming a first set of fastening means openings (103), to allow the fastening means (104, 106, 107) to engage subchondral regions of the distal radius (405). The fastening means (104, 106, 107) applied at this first set of fastening means openings (103) are primary supporting screws, angled specifically in the longitudinal and lateral direction, which as the first set of angular definitions (500, 501, 503, 507) as shown in Figure 8(a) which perfectly engage the entire subchondral regions of the distal radius (405), including the area of radial styloid, palmarulnar and dorsoulnar.

25

Further, a second set of fastening means openings (102) is also formed on the head (99) and preferably positioned in a in an oblique line (403) as shown in Figure 7, in such a way that it provides secondary support to the first set of fastening means (104, 106, 107) as set forth in the foregoing description. The second set of fastening means (104, 106, 107) can be placed at the second set of fastening means openings (102)

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located close to the neck (97) of the plate (100) to cover the volar and medial aspect of the subchondral regions of the distal radius (405). The second set of angular definitions (502, 508) are also shown in Figure 8(a).

5 Another preferred embodiment of the present invention also discloses that the plurality of fastening means openings (101, 108) are aligned along the longitudinal axis of the shaft (98), which is the A-A axis as shown in Figure 1. The fastening means (104, 105) to be placed at this third set of fastening means openings (101, 108) are meant for low profile locking and low profile cortical screws (105). Several
10 shapes of the fastening means openings (101, 102, 103, 108) can be provided. Preferably, these fastening means openings (101, 102, 103, 108) are round in shape, as shown by the first fastening means openings (101) of the shaft (98); or oblong in shape, as shown by the second fastening means openings (108) of the shaft (98) in Figure 1 to Figure 3. Oblong openings (108) allow the fixation and longitudinal
15 translation of low profile cortical screw (105) in the direction D as illustrated in Figure 1 for plate positioning. This opening (108) also allows the low profile cortical screw (105) to translate within 15° laterally (left-right), and approximately 50° longitudinally.

20 Accordingly, the screws threads and combination angle of screw angulations provide a minimum of 2 to 3 threads intact (514) in all the fastening means openings (101, 102, 103), thus resulting in a strong locking mechanism. Figure 8(b) is a cross-sectional view through the C-C axis of Figure 8(a) showing the contact threads between the fastening means (104, 106, 107) and the plate (100). Locking smooth
25 pegs (106) and locking threaded pegs (107) are preferred for plate head (99) on osteoporotic bones. However, low profile locking screws (104) can be used on the same location as well.

Yet another preferred embodiment of the present invention discloses that the plurality
30 of K-wire openings (111) and fastening means openings (101, 102, 103, 108) are

chamfered outwardly toward the bottom surface (95) of the plate (100) to avoid sharp edges, thus to reduce interference with ligaments and soft tissue, in order to avoid tissue irritation. Besides, there is a limited contact base of the shaft (98) designed, therefore the periosteal vascularity underneath the bone plate (100) can be improved.

5 In other words, the design and configuration of this bone plate (100) is capable of avoiding devascularization.

¾ As set forth in the preferred embodiment, the present invention is characterized by the incorporation of an insertion cavity (109) at the neck (97) of the plate (100). This
10 insertion cavity (109) is preferably gourd-shaped, pear-shaped or kidney-shaped. This uniquely shaped cavity (109) formed on the plate median allows option for easy and accessible space for the insertion of bone graft, positioned in the longitudinal and lateral direction as shown in the angle definitions (504, 505, 506) in Figure 8(a). Preferably, a wide bottom chamfer (200) is provided and outwardly formed around
15 the insertion cavity (109) toward its bottom surface (95) to allow maximum reach of a bone graft syringe at any angle through the cavity (109).

The insertion cavity (109) is specially designed to ease the surgeon in inserting the bone graft. This cavity (109), with its flexible shape, is sufficiently large and
20 convenient for the accession of the surgeon to create the window for bone graft insertion and packing during the internal fixation process. It is also capable of preventing the wastage of the bone graft material. Moreover, the presence of this cavity (109) does not compromise the overall strength of the plate structure.

25 Further embodiment of the present invention is a bone plate (100) for fixing distal radius (405) fracture which is made of titanium, titanium alloy or stainless steel. An example for titanium alloy which can be used is Ti6Al4V; whereas the stainless steel preferably applied is 316LVM. The materials used for fabricating the plate (100), as well as the fastening means (104, 105, 106, 107) coupled therewith, are to be
30 sterilized. However, the present invention does not intend to limit the use of other

suitable bio compatible materials in the aforementioned fabrication.

Figure 9(a) to 9(d) shows a custom designed locking screw (104) which can be used with the distal radius plate (100). The locking screw (104) is made up of a locking head (618) and a threaded shaft (617). The threaded shaft (617) of the locking screw (104) is preferably having a core diameter (612) which is approximately 70% to 80% of the major diameter (620) which maintains the core strength of the locking screw (104). The thread of the locking screw (104) has a thrust face (605) that forms an angle of approximately 30° to 40° to a plane transverse to the longitudinal axis of the locking screw (104). This thread has a trailing face (604) which has an angle of approximately 5° to 11° to the same plane. This self tapping locking screw (104) has a tip with a radius (609) of approximately 0.5mm to 1.5mm and a point angle (621) of approximately 117° to 123° . The neck of the screw has a reinforced profile with a combination of chamfer (610) which increases the stiffness and a radius (611) that improve the deflection; resulting in a fastening means with optimum strength.

On the other hand, Figure 10(a) to 10(d) shows a custom designed low profile cortical screw (105) which contains a low profile screw head (718) designed with a combination of 3 different radiuses (701, 702, 703) and a threaded shaft (717). The threaded shaft has a core diameter (712) which is approximately 63% to 73% of the major diameter (720). The thread of the low profile cortical screw (105) also has a thrust face (705) that forms an angle of approximately 30° to 40° to a plane transverse to the longitudinal axis of the screw, similar to that of the locking screw (104). This thread has a trailing face (704) angled approximately 0° to 6° to the same plane. This self tapping cortical screw's tip has a radius (709) of approximately 0.5mm to 1.5mm with a point angle (721) of approximately 85° to 95° . The neck of the screw has a reinforced profile with a radius (711) that improve the deflection; resulting in a fastening means with optimum strength.

As shown in Figure 11(a) to 11(d) is a locking threaded peg (107) which can be used with the plate (100). This locking threaded peg (107) is also having a locking head (818) and a threaded shaft (817), wherein the core diameter (812) of the shaft (817) is approximately 50% to 60% of the major diameter (820). The thread has a thrust face (805) that forms an angle of approximately 20° to 30° to a plane transverse to the longitudinal axis of the screw, and it has a trailing face (804) which has an angle of approximately 2° to 8° to the same plane. The self tapping threaded peg tip has a radius (809) of approximately 0.5mm to 1.5mm with a point angle (821) of approximately 117° to 123°. The neck of the screw has a reinforced profile with a combination of chamfer (810) which increases the stiffness and a radius (811) that improve the deflection; resulting in a fastening means with optimum strength.

Illustrated in Figure 12(a) to 12(d) is a custom designed locking smooth peg (106). This locking smooth peg (106) possesses a locking head (918) and smooth shaft (917). The smooth peg shaft (917) has a core diameter which is in the same dimension as the major diameter (920) a tip (909) radius similar to the radius of the peg's diameter. The neck of the screw has a reinforced profile with a combination of chamfer (910) which increases the stiffness and a radius (911) that improve the deflection; resulting in a fastening means with optimum strength.

20

Preferably, the locking heads of all the locking screw (104), the cortical screw (105), threaded peg (107) and smooth peg (106) have the hexalobe recesses (616, 716, 816, 916) for receiving a hexalobe screwdriver. The locking heads of these screws (104, 106, 107) also have external taper threads with a preferred taper angle of approximately 5° to 15° relative to the longitudinal axis of the screw, and a symmetrical included thread angle (602 & 603, 802 & 803, 902 & 903) of approximately 60°. The threads generally have a crest width (601, 801, 901) of approximately 0.02mm to 0.08mm.

25

According to the preferred embodiment of the present invention, the helical threads of the shafts of the locking screw (104), the cortical screw (105) and threaded peg (107) can have helical threads (625, 725, 825) with a helix angle of approximately 78° to 88° . They can have a crest width (606, 706, 806) of the major diameter which is preferably to be 0.03mm to 0.15mm in order to keep a good strength on the wing of screw thread (624, 724, 824). These can be shown in Figure 9(c), 10(c) and 11(c).

These self tapping screws (104, 105, 107) are preferably 3-fluted and having tips with unique geometry such as a substantially straight flute (613, 713, 813) and taper relieved thread (614, 814) for stress reduction during the self tapping process on the bone. The flute can have a core diameter (622, 722, 822) of 40-50% relative to the core diameter of the thread (612, 712, 812), with a core taper angle (623, 723, 823) of 15° to 25° . As shown in Figure 9(b), 10(b) and 11(b), the rake angle of the screws (615, 715, 815) is preferably 0° to 10° , whereas the taper thread relief angle (619, 819) is preferably 4° to 12° and the helix angle of the flute (613, 713, 813) is preferred to be approximately within the range of 0° to 10° . Minimum of 1 to 2 full turn taper thread (607, 707, 807) at the screw tip is substantially preferred with a taper angle (608, 708, 808) of approximately 10° for the locking screw (104) and the cortical screw (105), or 25° to 35° for the threaded peg (107), per side relative to the longitudinal axis of the screw to ensure easy entry of the screws into the drilled hole during the fixation process.

The bone plate (100) is used in an open reduction internal fixation system for fracture management of the distal radius (405). According to the preferred embodiment of the present invention, the bone fracture fixation process can be initiated by making an incision and dissection, followed by retraction of tendon and arteries. The fracture region is visualized and reduced.

An appropriate size of the implant, which is the distal radius bone plate (100) shall be chosen according to the bone anatomy of the patient. Preferably, the plate (100) is

positioned according to the optimum position, which is preferably 5 mm from the distal edge of the radius, or the pronator quadratus line (404) as demonstrated in Figure 7. However, the suitable position can be determined depending on the surgeon's discretion. K-wires (118) can be used for temporarily fixation of the plate (100) while evaluating the placement of the plate (100). A hole of approximately 2.5 mm to 2.7 mm can be drilled on the diaphyseal part of the bone through the oblong-shaped opening (108) of the plate (100) using an appropriate drill guide.

Preferably, the length of the fastening means (104, 105, 106, 107) or the screws applied can be determined using an appropriate depth gauge. For example, a non-locking cortical screw (105) can be placed in the oblong-shaped opening (108) but not completely tightened to allow adjustment of the plate (100) in distal or proximal directions. Under an image intensifier, the correct position of the plate (100) can be determined and the cortical screw (105) can be tightened. Based on the fracture pattern and preference, the procedures of drilling, measuring and placement of other types of fastening means such as the locking threaded pegs (107), locking smooth pegs (106) or locking screws (104) can be repeated by using a drill, a drill sleeve, a measuring gauge and a torque screwdriver. The selection of fastening means (104, 105, 106, 107) are depending on the bone characteristics. Preferably, an approximately 1.9 mm to 2.1 mm drill hole is applied for the coupling of aforementioned screws on the rows of fastening means openings (102, 103) on the head, and preferably a 2.1 mm to 2.7 mm drill hole is used for the remaining openings (101, 108) on the shaft (98).

The bone graft materials are preferably applied through the insertion cavity (109) as an optimal bone void filler. The suitable types of bone graft materials applied herein can be an autogenous bone graft in paste, patty or granule form. Besides, both autograft or allograft also can be used in the present invention. It is vital to ensure under the image intensifier that all the fastening means (104, 105, 106, 107) are secured in good position, without penetrating the any of the joints. Then, the incision

can be closed to complete the fixation process.

The present disclosure includes as contained in the appended claims, as well as that of the foregoing description. Although this invention has been described in its preferred
5 form with a degree of particularity, it is understood that the present disclosure of the preferred form has been made only by way of example and that numerous changes in the details of construction and the combination and arrangements of parts may be resorted to without departing from the scope of the invention.

CLAIMS

1. A bone plate (100) for fixing distal radius (405) fracture comprising:
a volar-shaped head (99) to be positioned at the distal radius (405);
5 a shaft (98) inclinedly extending from the head (99);
a plurality of K-wire openings (111) distributed over the head (99) for receiving
K-wires (118) to temporarily secure the plate (100); and
a plurality of fastening means openings (101, 102, 103, 108) distributed over the
head (99) and the shaft (98) for receiving fastening means (104, 105, 106, 107) to
10 fix the plate (100) to the distal radius (405);
characterized by an insertion cavity (109) formed at the junction of the head (99)
and the shaft (98) in such a manner as to provide an accessible space for efficient
insertion of bone graft material.
- 15 2. A bone plate (100) according to claim 1, wherein the head (99) has a thickness
of 1.5 mm to 2.5 mm and is tapered from the junction of the head (99) and the
shaft (98), towards the distal end of the plate (100).
3. A bone plate (100) according to claim 1, wherein the shaft (98) has a thickness
20 of 2.0 mm to 3.0 mm.
4. A bone plate (100) according to claim 1, wherein the shaft (98) has at least one
waisted region (117) for uniform distribution of stresses.
- 25 5. A bone plate according to claim 1, wherein the angle of inclination between
the head (99) and the shaft (98) lies within the range of 20° to 30°.
6. A bone plate (100) according to claim 1, wherein the fastening means (104,
105, 106, 107) are locking screws (104), cortical screws (105), locking smooth
30 pegs (106), locking threaded pegs (107) or a combination of any two or more

thereof.

- 5 7. A bone plate (100) according to claim 1, wherein the plurality of fastening means openings (103) at the distal end of the head (99) are aligned in an arc (400) to allow the fastening means (104, 106, 107) to engage subchondral regions of the distal radius (405).
- 10 8. A bone plate (100) according to claim 7, wherein others of the fastening means openings (102) are aligned on the head (99) in such a manner as to allow the fastening means (104, 106, 107) to engage volar and medial subchondral regions of the distal radius (405).
- 15 9. A bone plate (100) according to claim 8, wherein still further fastening means openings (101, 108) are aligned along the longitudinal axis of the shaft (98).
10. A bone plate (100) according to claim 1, wherein the plurality of fastening means openings (101, 102, 103, 108) are round or oblong in shape.
- 20 11. A bone plate (100) according to claim 1, wherein the insertion cavity (109) is gourd-shaped, pear-shaped or kidney-shaped.
- 25 12. A bone plate (100) according to claim 1, wherein a chamfer (200) is outwardly formed around the insertion cavity (109) toward its bottom surface (95) to allow maximum reach of a bone grafting device at any angle through the cavity (109).
13. A bone plate (100) according to claim 1 made of titanium, titanium alloy or stainless steel.
- 30 14. A kit (300) for fixing distal radius (405) fracture comprising:

a bone plate having a volar-shaped head (99) to be positioned at the distal radius (405); a shaft (98) inclinedly extending from the head (99); a plurality of K-wire openings (111) distributed over the head (99) for receiving K-wires (118) to temporarily secure the plate (100); and a plurality of fastening means openings (101, 102, 103, 108) distributed over the head (99) and the shaft (98) for receiving fastening means (104, 105, 106, 107) to fix the plate (100) to the distal radius (405); characterized by an insertion cavity (109) formed at the junction of the head (99) and the shaft (98) in such a manner as to provide an accessible space for efficient insertion of bone graft material;

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10 a plurality of K-wires (118); and
a plurality of fastening means (104, 105, 106, 107).

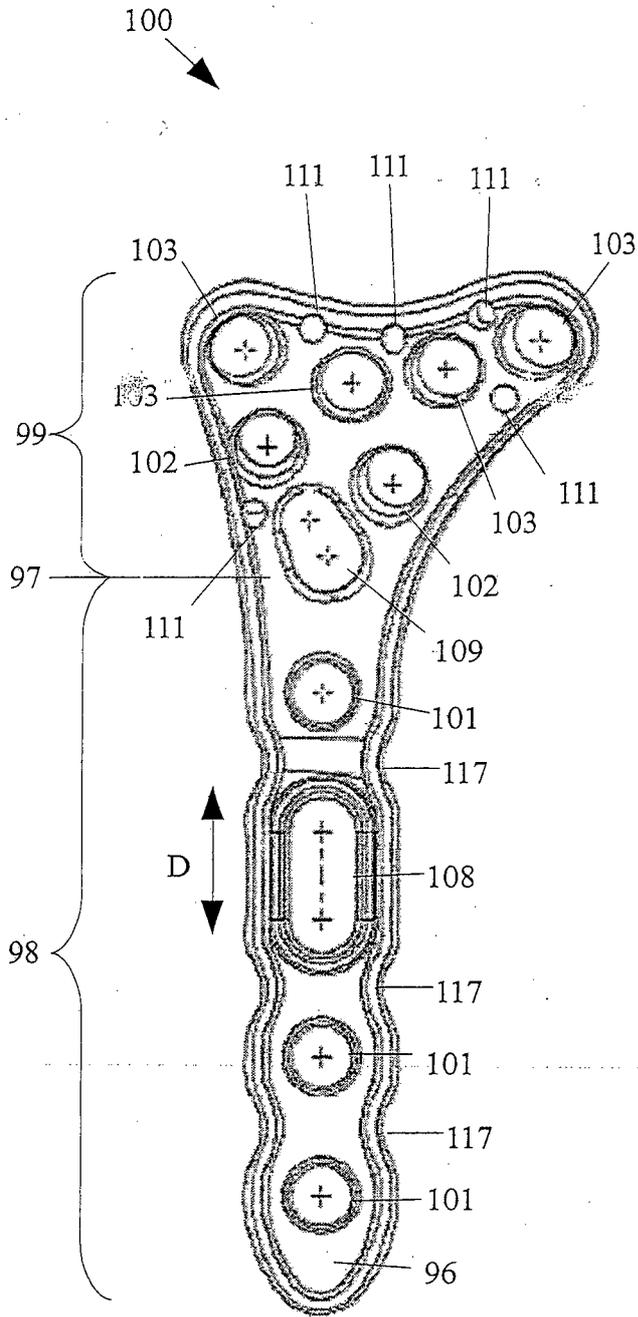


Figure 1

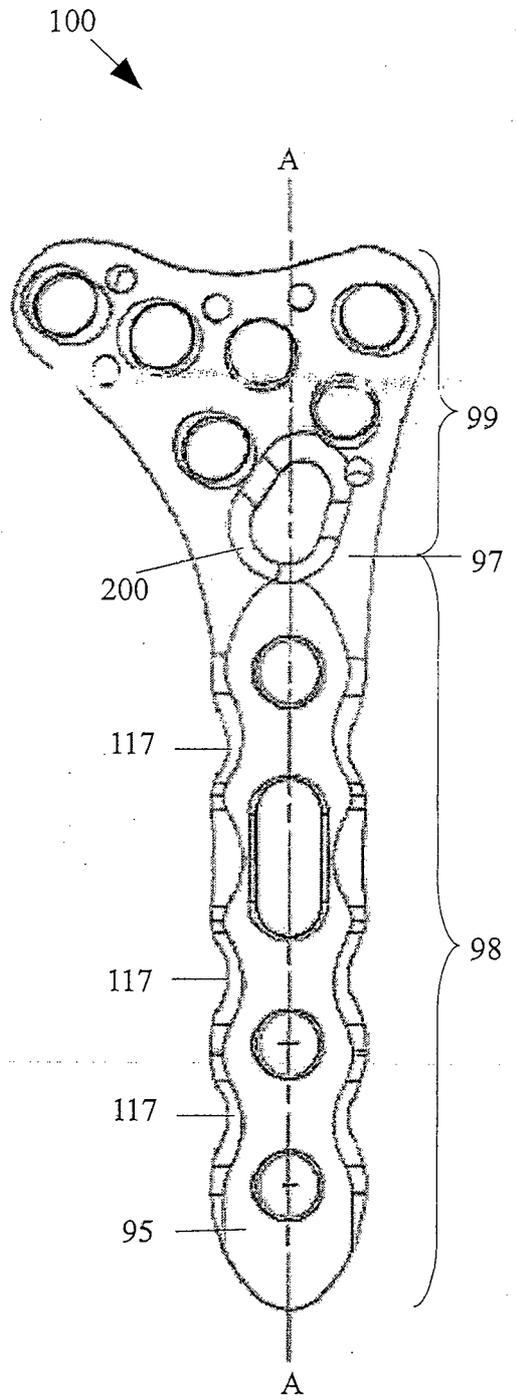


Figure 2

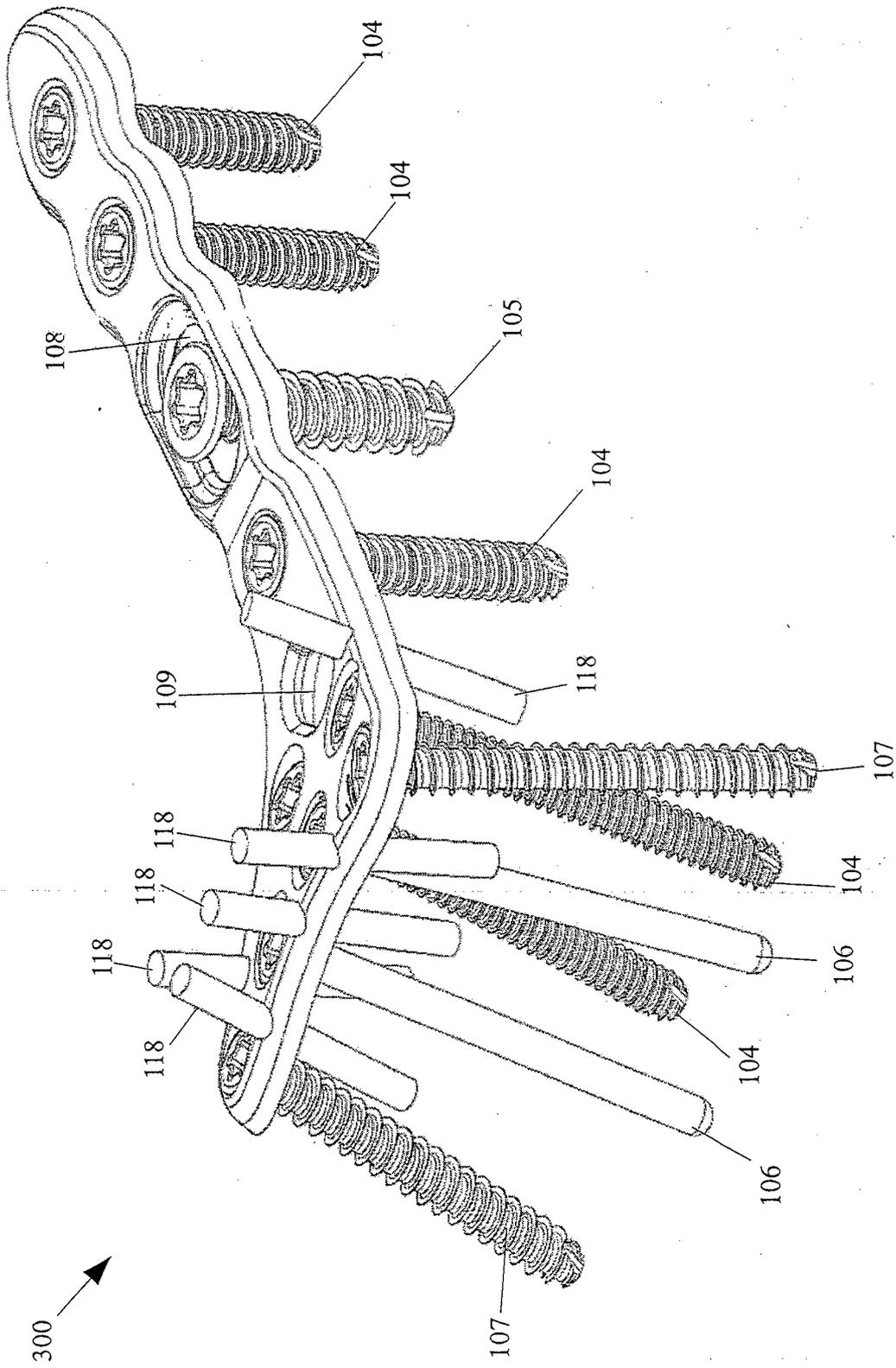


Figure 3

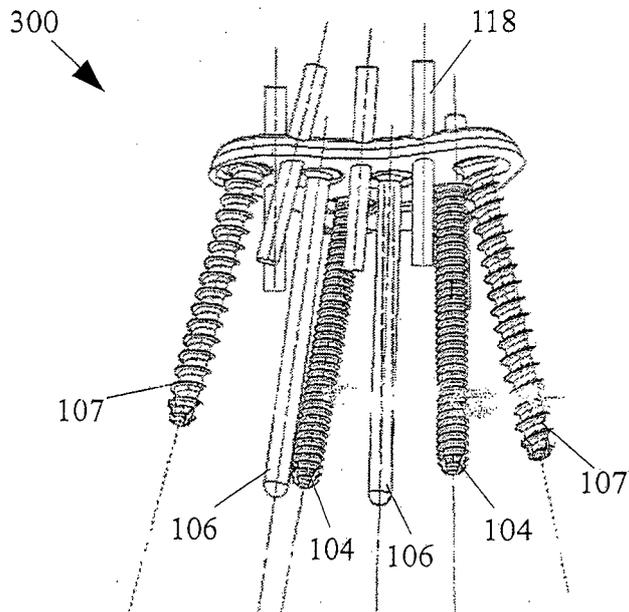


Figure 4

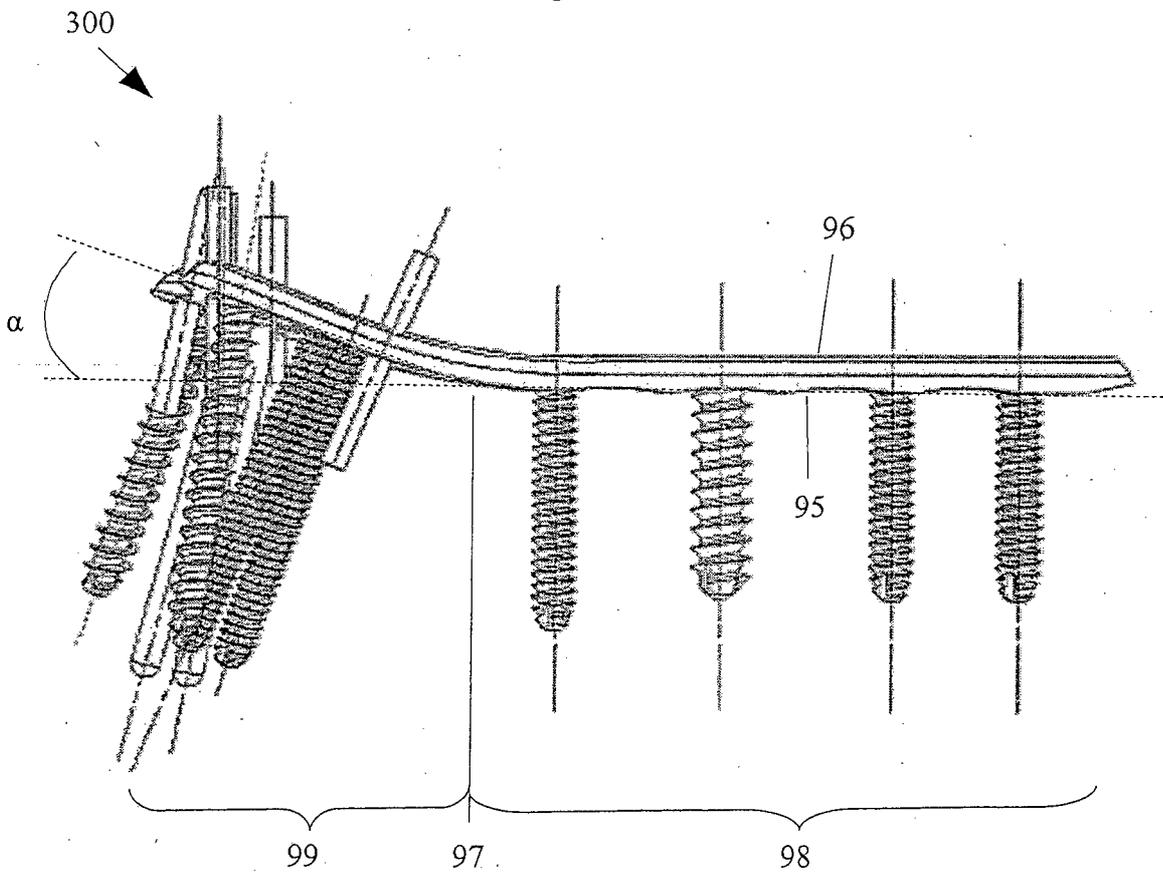


Figure 5

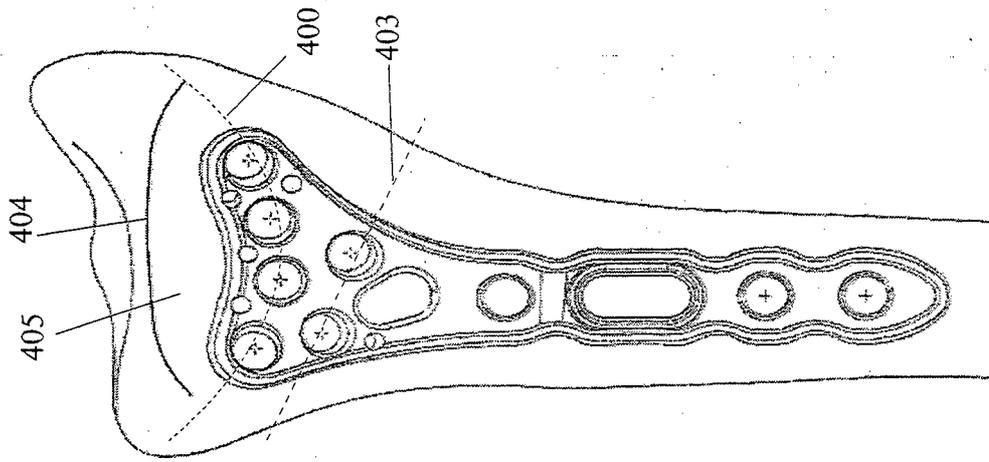


Figure 7

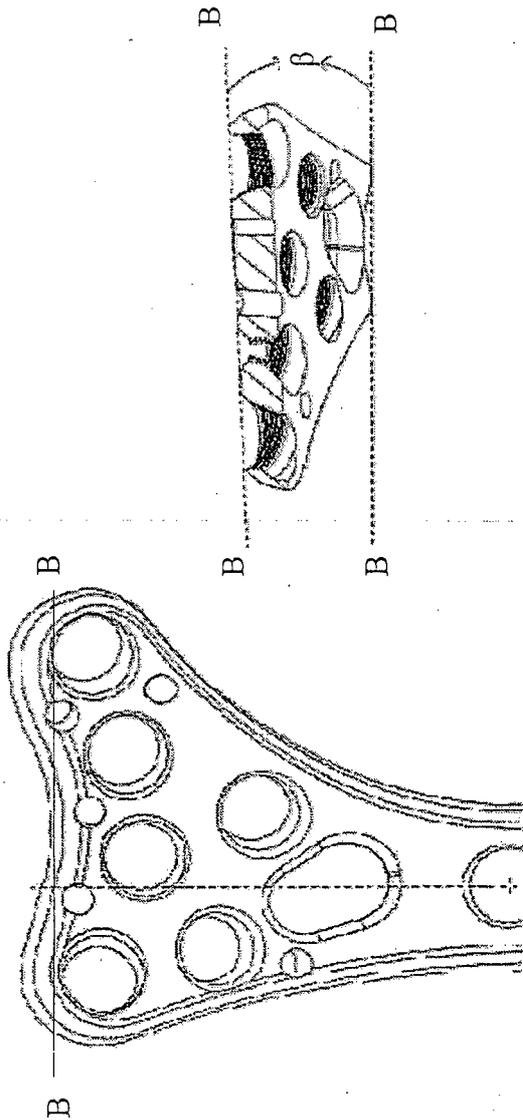


Figure 6(a)

Figure 6(b)

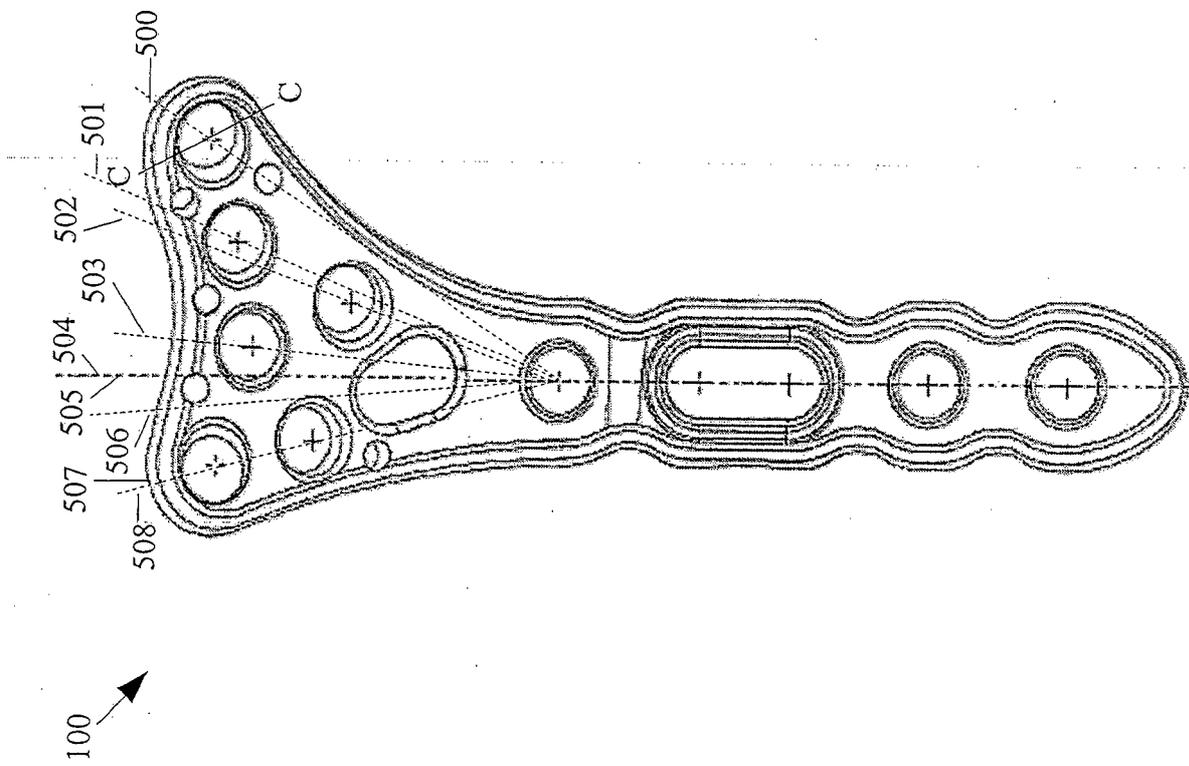


Figure 8(a)

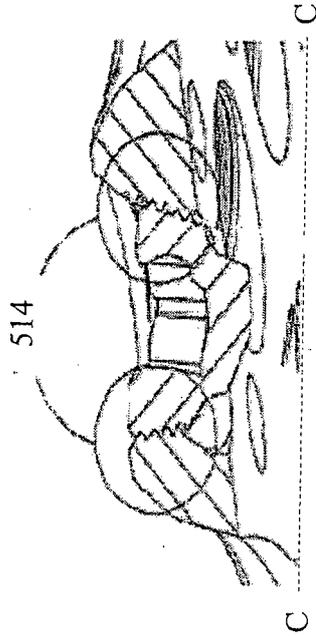


Figure 8(b)

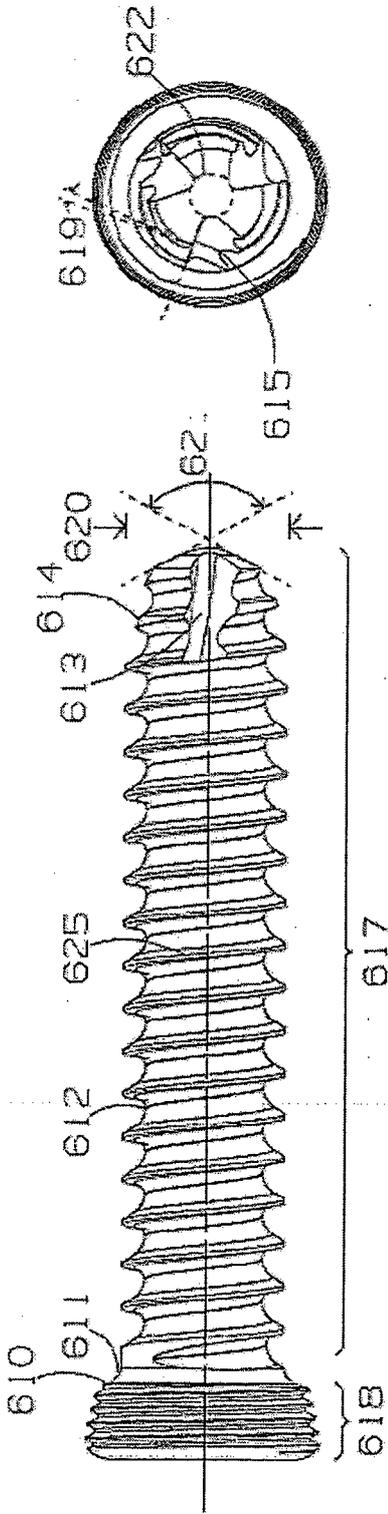


Figure 9(b)

Figure 9(a)

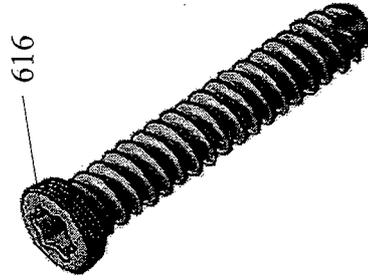


Figure 9(d)

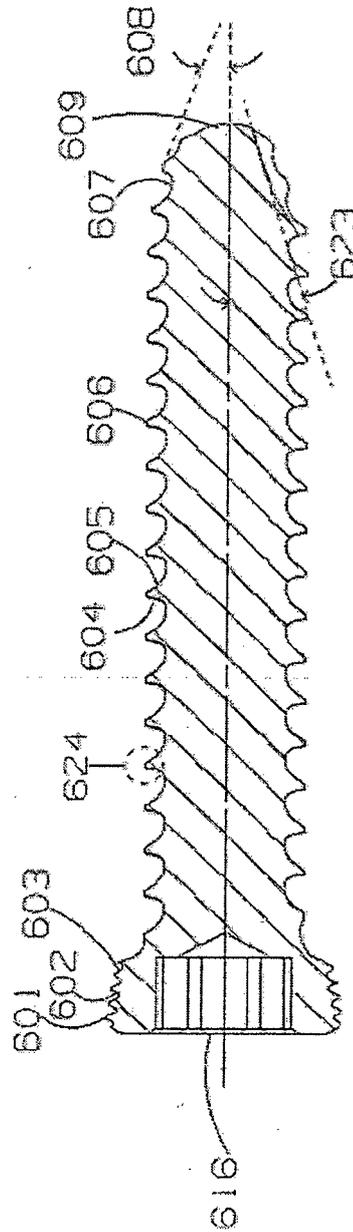


Figure 9(c)

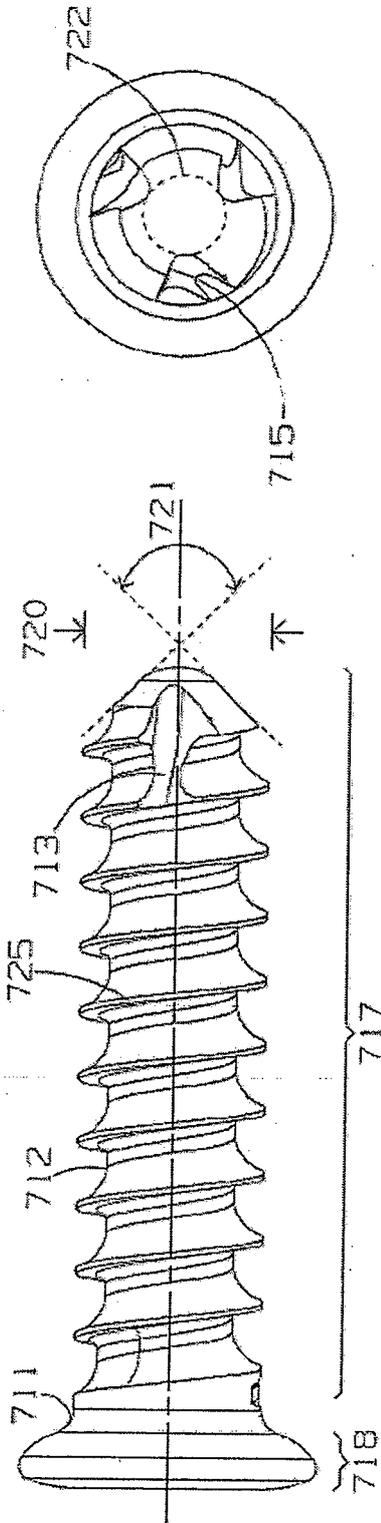


Figure 10(b)

Figure 10(a)

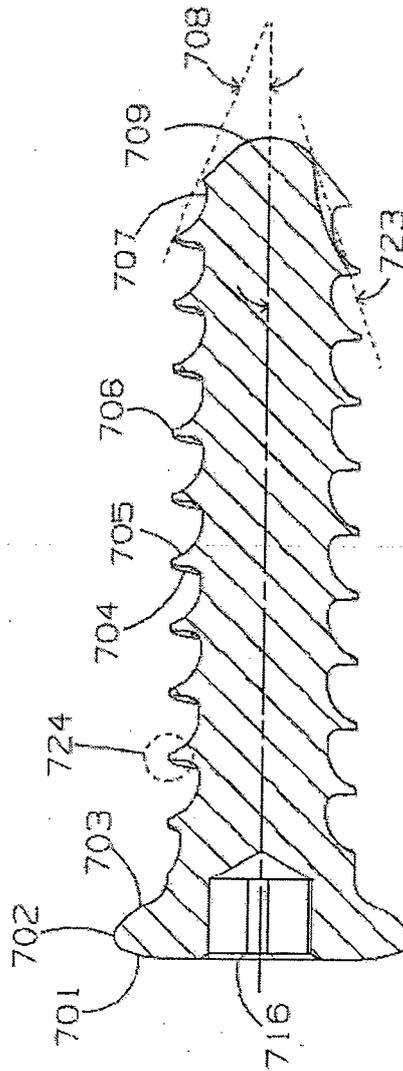


Figure 10(c)

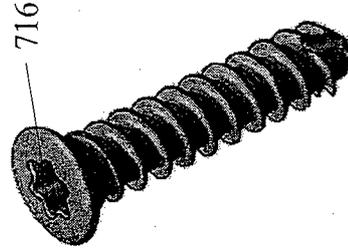


Figure 10(d)

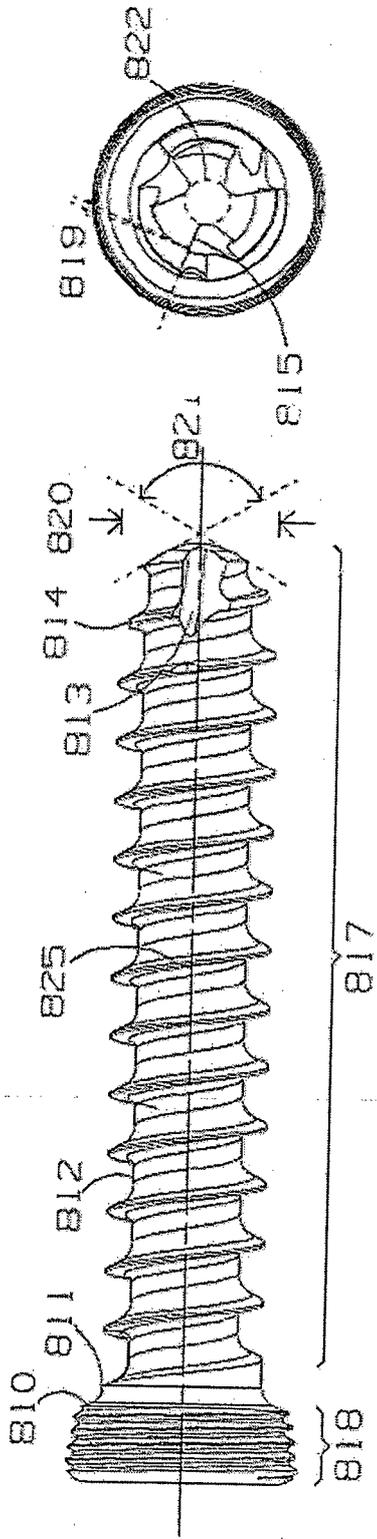


Figure 11(a)

Figure 11(b)

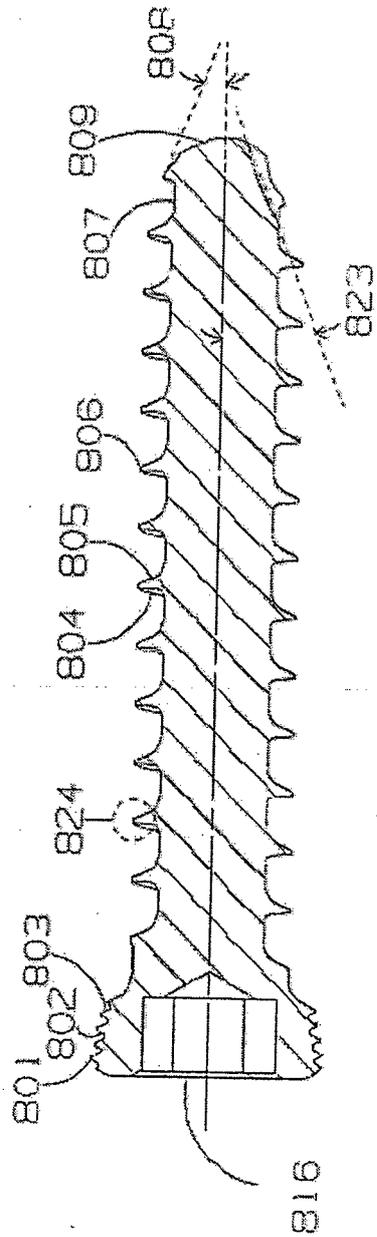


Figure 11(c)

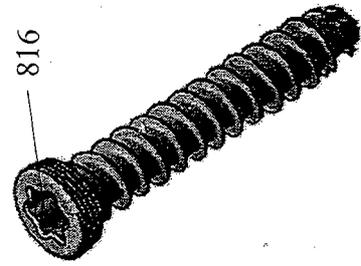
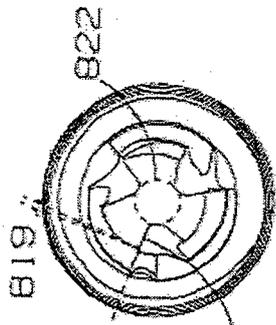


Figure 11(d)



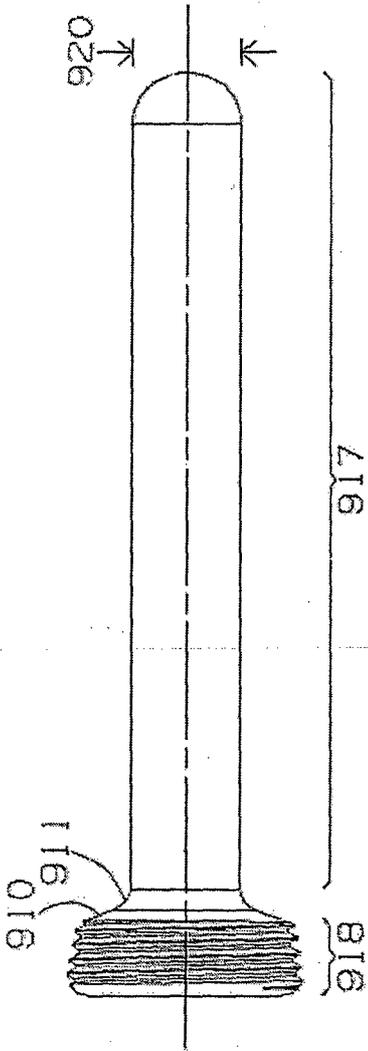


Figure 12(a)

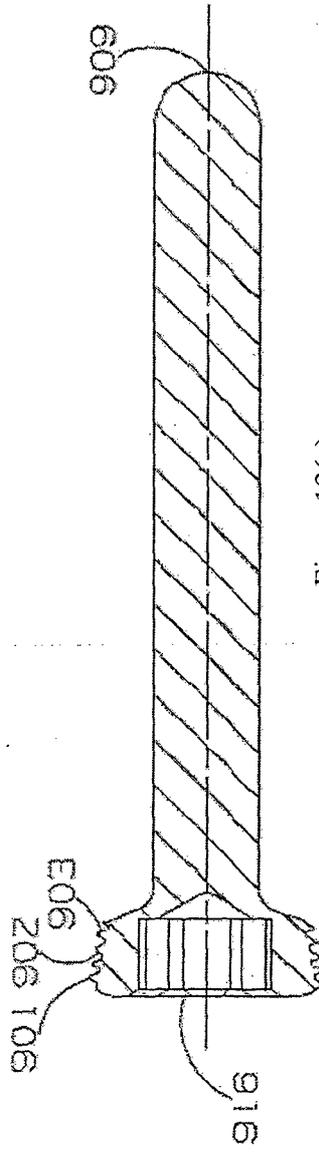


Figure 12(c)

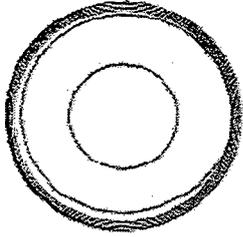


Figure 12(b)

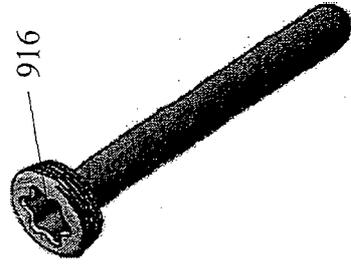


Figure 12(d)

A. CLASSIFICATION OF SUBJECT MATTER		
Int. Cl.		
A61B 17/68 (2006.01)		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) WPI, EPODOC, IPC A61B 17/58, A61B 17/56, A61B 17/68 & KEYWORDS VOLAR, Y, SHAPE, HOLE, OPENING, APERTURE, PASSAGE, GRAFT, MATERIAL, FILLER & OTHERS		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2008/0140127 A1 (VASTA ET AL) 12 June 2008 see entire specification and figures 1-7	1-14
A	US 2005/0065524 A1 (ORBAY) 24 March 2005 see abstract & figure 2	
A	US 2007/0265629 A1 (MARTIN ET AL) 15 November 2007 see abstract & figure 2 1	
A	US 2005/0085818 A1 (HUEBNER) 21 April 2005 see abstract & figures 2 & 5	
<input type="checkbox"/> Further documents are listed in the continuation of Box C <input checked="" type="checkbox"/> See patent family annex		
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family		
Date of the actual completion of the international search 09 February 2012		Date of mailing of the international search report 16 February 2012
Name and mailing address of the ISA/AU AUSTRALIAN PATENT OFFICE PO BOX 200, WODEN ACT 2606, AUSTRALIA E-mail address: pct@ipaaustralia.gov.au Facsimile No. +61 2 6283 7999		Authorized officer M.S. HAYNES AUSTRALIAN PATENT OFFICE (ISO 9001 Quality Certified Service) Telephone No : +61 2 6283 2170

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT7MY2011/000213

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w o	2004045384	w o	2004045389	w o	2004045455
w o	2004080344	w o	20041 12587	w o	20050371 14
w o	2005046494	w o	2005074580	w o	2005102193
W o	2007009124	w o	2007048038	w o	2007082004
w o	2007127994	w o	2007146165	w o	2008048684
w o	2008057404	w o	2010054400		

Due to data integration issues this family listing may not include 10 digit Australian applications filed since May 2001.

END OF ANNEX