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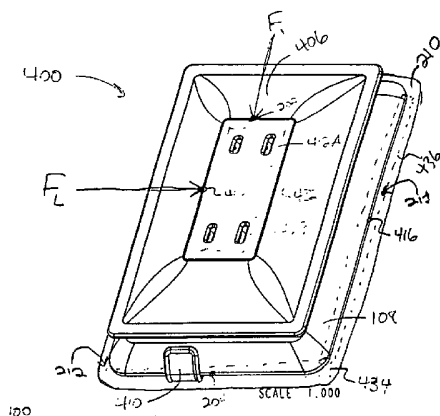
(43) International Publication Date
26 February 2004 (26.02.2004)

PCT

(10) International Publication Number
WO 2004/016292 A1

- (51) International Patent Classification⁷: **A61L 9/03**
- (21) International Application Number:
PCT/US2003/025243
- (22) International Filing Date: 13 August 2003 (13.08.2003)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data:
10/222,070 16 August 2002 (16.08.2002) US
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- (81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.
- (84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).
- Published:**
- with international search report
 - before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments
- For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: VAPOR DISPENSING DEVICE HAVING IMPROVED TRANSVERSE LOADING STABILITY



(57) Abstract: A vapor dispensing device having a high transverse loading stability includes a relatively low profile with respect to the supporting wall or electrical receptacle such that the frequency and impact of accidental physical contact with the device are appropriately reduced. To achieve a low profile, the housing of a vapor dispensing device is designed such that the distance from the outlet face of the wall receptacle to a worst-case transverse loading point (d_L) is less than the distance from the plug to a worst-case support point (d_S).

VAPOR DISPENSING DEVICE HAVING IMPROVED TRANSVERSE LOADING STABILITY

Field of Invention

This invention generally relates to vapor dispensing devices such as air fresheners.
5 More particularly, the invention relates to electrically-powered vapor dispensing devices.

Background of the Invention

Electrically-operated vapor dispensing devices have been used for several years and have become common household products. These devices are typically inserted into a
10 conventional electrical receptacle to obtain electricity for heating a perfumed fluid, wax, paraffin, or other fuel to produce a pleasing aroma that is dispersed within a room or other confined space. Examples of electric vapor dispensers include the RENUZIT products available from The Dial Corporation of Scottsdale, Arizona. One such product is shown in U.S. Design Patent Serial No. D449,101 which issued on October 9, 2001 to Wolpert et al.

15 Many conventional vapor dispensing devices exhibit a marked disadvantage, however, in that the size of the dispenser housing frequently extends outwardly from the wall receptacle for a significant distance. Because of this distance, an outcropping from the wall is produced that can become bumped, jostled or otherwise accidentally placed into contact with people or objects. Such contact may have the effect of pushing the dispenser
20 out of the wall receptacle, and may potentially break or deform the device. Accordingly, it is desirable to produce an electric vapor dispenser that is resilient to accidental contact that may produce breakage or displacement of the dispenser.

Summary of the Invention

25 A vapor dispensing device having a high transverse loading stability is provided in accordance with various embodiments of the invention. Such a device includes a relatively low profile with respect to the supporting wall or electrical receptacle such that the frequency and impact of accidental physical contact with the device are appropriately reduced. According to an exemplary embodiment, the housing of a vapor dispensing device
30 is designed such that the perpendicular distance from the outlet face of the wall receptacle to a worst-case transverse loading point (d_L) is less than the distance from the plug to a worst-case support point (d_S) such that a transverse loading coefficient $\eta = d_S/d_L$ is greater than

one. These and other aspects of the invention shall become more apparent when read in conjunction with the accompanying drawing figures and the attached detailed description of exemplary embodiments.

5

Brief Description of the Drawing Figures

The features and advantages of the present invention are hereinafter described in the following detailed description of exemplary embodiments to be read in conjunction with the accompanying drawing figures, wherein like reference numerals are used to identify the same or similar parts in the similar views, and:

10

Figure 1 is a side view of a conventional vapor dispensing device;

Figure 2 is a side view of an exemplary vapor dispensing device with a high transverse loading stability;

Figure 3 is a side view of an exemplary vapor dispensing device having two plugs and a high transverse loading stability;

15

Figures 4A-D are top, front, side and perspective views, respectively, of an exemplary vapor dispensing device having a high transverse loading stability; and

Figures 5A-5C depict various refill configurations in accordance with the present invention.

20

Detailed Description of Exemplary Embodiments

With reference to Figure 1, a conventional vapor dispensing device **100** typically includes a housing **108** coupled to a plug **106** that is capable of being inserted into a conventional electrical receptacle in a wall or other structure **110**. Housing **108** typically retains a vapor-producing material such as a perfumed fluid, wax, paraffin or the like that can be combusted, electrolyzed or otherwise processed by a resistance heater or other appropriate device to produce a vapor that can be dispersed through a room, vehicle or other confined space.

25

30

Due to the relatively large profile of vapor dispensing device **100** with respect to wall **110**, however, forces impacting on the vapor dispensing device **100** suitably produce rotational moments about a support point along the wall. For example, force **F** applied at point **102** on housing **108** suitably produces a rotational moment about point **104** that is equal to the magnitude of force **F** multiplied by the distance d_L from the effective point of

force **F** to the front face of the outlet. This loading distance d_L is defined as the distance from the effective point of force **F** from an axis that is perpendicular to the front face of the outlet and that runs through a support point **104**. In the vapor-dispensing device **100** shown in Figure 1, support point **104** is the point on device **100** that bears the greatest impact of force **F**.

Application of force **F** produces a reactive force **R** between plug **106** and wall **110**. Reactive force **R** appropriately maintains vapor-producing device **100** in contact with the outlet receptacle, and produces a counter-balancing rotational moment upon support point **104**. The moment produced by the stabilizing force **R** about support point **104** is equal to the magnitude of reactive force **R** multiplied by the distance from force **R** to support point **104**. This distance is referred to herein as support distance d_S and is typically measured along an axis parallel to the outlet face. Because vapor dispensing device **100** remains rigidly fixed in position and does not move in response to the application of force **F**, the sum of the moments about point **104** suitably equates to zero. The sum of the moments about point **104** may therefore be expressed as:

$$R d_S - F d_L = 0 \quad (\text{Equation 1})$$

Manipulating these terms algebraically shows that the resulting force **R** produced into the wall by force **F** is as follows:

$$R = F \frac{d_L}{d_S} = \eta \quad (\text{Equation 2})$$

wherein η is a transverse loading coefficient defined as the ratio of the support distance d_S to the load distance d_L . In vapor dispensing device **100** shown in Figure 1, it is clear that lateral distance d_L is relatively large compared to d_S , thereby indicating that the transverse loading coefficient η is less than 1. Accordingly, it can be readily shown from Equation 2 that a load force **F** upon point **102** effectively produces a resultant force **R** that has a greater magnitude than that of force **F** when the transverse loading coefficient η is less than one.

Figure 2 is a side view of a vapor dispensing device having an improved transverse loading stability. With reference now to Figure 2, a vapor dispensing device **200** suitably includes a housing **108** coupled to a plug **106** that is capable of being inserted into the outlet face **212** of a conventional electrical receptacle **210** housed in a wall or other surface **110**. Housing **108** may also include a conventional device outlet **206** electrically coupled to the

plug that provides electrical power from plug 106 to a light or other electrically-powered device such as a hairdryer, curling iron, electric razor, kitchen appliance, or the like.

Figure 2 depicts a force **F** impinging upon a worst-case transverse loading point 202 along housing 108. Worst-case loading point 202 is any point along the edge of device 200 that is furthest from the outer face 212 of the electrical receptacle. Worst-case loading point 202 corresponds to locations on housing 108 where the impinging force produces a maximum rotational moment about a worst-case support point 204, which is defined as the points on housing 108 wherein the moment produced by reactive force **R** is maximized. Worst-case support points 204 typically reside on an edge of housing 108 that is in physical contact with the front face of the receptacle and that is on a side of housing 108 opposite plug 106 from the impinging point of the force **F**. Accordingly, device 200 may exhibit multiple worst-case support points along an edge of housing 108 that provide equal reactive moments to external forces. Similarly, forces impinging upon each point along certain edges of housing 108 may produce identical moments in the various support points. Accordingly, the precise locations of worst-case loading and support points on device 400 vary widely depending upon the particular embodiment and forces applied.

In the device shown in Figure 2, worst-case support point 204 is defined near the bottom of vapor dispensing device 200 at the point on housing 108 that bears the greatest loads from applied external forces. Worst-case transverse loading point 202 corresponds to the point on vapor dispensing device 200 whereupon application of a force **F** produces the greatest resultant force **R** between plug 106 and the surrounding receptacle 210. Using Equation 2 above, the resultant force **R** is:

$$R = F \, d_L/d_S = \frac{F}{\eta}$$

In this case, however, the transverse loading coefficient η is greater than one because support distance d_S from plug 106 to support point 204 along outlet face 212 is designed to be greater than the lateral distance d_L from outlet face 212 to loading point 202. Correspondingly, then, force **F** applied at worst-case transverse loading point 202 produces a resulting force **R** with a magnitude that is less than the magnitude of force **F**, thereby reducing the impact of force **F** on plug 106 and improving the overall transverse loading stability of vapor dispensing device 200.

Figure 3 is a side view of a vapor dispensing device having more than one plug which can be inserted into an electrical receptacle. With reference now to Figure 3, a vapor dispensing device **300** suitably includes housing **108** coupled to two plugs **106a** and **106b**. Either or both of the plugs **106a-b** may be an electrical communication with one or more device outlets **206** to provide electrical power from receptacle **210** (Figure 2) to external devices such as lamps, hair dryers or the like.

In the embodiment shown, the worst-case transverse loading point remains at point **202**, which is the greatest perpendicular distance d_L from the face of the outlet. Similarly, worst-case support point **204** remains at the edge of housing **108** at a distance furthest from plugs **106A-B** and opposite worst-case transverse loading point **202**. Because two plugs **106A-B** are provided, two resultant forces R_1 and R_2 are produced. Accordingly, the rotational moments about point **204** are appropriately expressed as:

$$R_1 d_{S2} + R_2 d_{S1} - F d_L = 0. \quad (\text{Equation 3})$$

Algebraically manipulating Equation 3 results in:

$$F = R_1 d_{S1}/d_L + R_2 d_{S2}/d_L = R_1 \eta_1 + R_2 \eta_2 \quad (\text{Equation 4})$$

wherein $\eta_1 = d_{S1}/d_L$ and $\eta_2 = d_{S2}/d_L$. Evaluating Equation 4 shows that force F applied at point **202** is appropriately counterbalanced by two resultant forces R_1 and R_2 . In each case, the transverse loading coefficients η_1 and η_2 are designed to be greater than one such that the support distance d_S is greater than the loading distance d_L for each plug **106A-B**. Because R_1 and R_2 are inversely proportional to η_1 and η_2 , respectively, it may be readily shown that relatively large values for η_1 and η_2 result in correspondingly smaller reactive forces R_1 and R_2 for a constant value of F . Further, because unusually high values of R_1 and R_2 can cause breakage or movement of device **300**, higher values for η_1 and η_2 thereby allow device **300** to produce lower reactive forces and to thereby withstand greater forces F without breakage or movement. Accordingly, the transverse loading stability of device **300** is improved.

Figures 4A-D are top, front, side and perspective views, respectively, of another exemplary embodiment of a vapor-dispensing device. With reference to Figures 4A-D, vapor dispensing device **400** suitably includes a housing **108** connecting to one or more plugs **106A-B**. Housing **108** and plugs **106A-B** are appropriately configured to correspond with the front face **212** of a wall-mounted outlet receptacle **210** (Figure 4D) to provide device stability and electrical power.

In the exemplary embodiment shown in the drawings, housing 108 suitably includes two optional device outlets 412A-B that allow the user to connect other appliances to plugs 106A-B to obtain electrical power while device 400 remains in use. Each of the plugs 106A-B has two prongs 404A-B as best seen in Figure 4A. To simplify the discussion
5 below, however, the reactive forces produced by each prong 404A-B are analyzed as a combined reactive force **R** for the entire plug 106. Plug 106 may conform to any electrical convention such as the 60 Hertz, 110 Volt alternating-current standard commonly used in North America. Alternatively, plug 106 may be configured to operate using direct current (e.g. current supplied by a battery) or any other electrical convention.

10 Fragrance is produced in device 400 by any conventional technique and structure. In an exemplary embodiment, device 400 suitably uses electrical resistance to heat a fragrance-producing fuel such as a perfumed fluid, wax or other substance maintained in a reservoir within or coupled to housing 108. In a further exemplary embodiment, device 400 suitably interfaces to an optional replaceable fragrance cartridge (or "refill component") 406 to
15 replenish the supply of fuel as needed. The cartridge may be discarded and replaced when the fuel is spent, when the user desires an alternate fragrance or as otherwise appropriate. An optional flat lamp, night light or other lighting feature may also be provided within fragrance-producing device 400. The term "housing" as used herein is intended to broadly include features such as removable cartridges, lamps and the like that may be coupled or
20 otherwise attached to device 400.

Housing 108 may also include or interface with an optional fragrance intensity slider 410. Slider 410 allows users to adjust the intensity of fragrance produced by device 400 by moving slider 410 to a desired linear position corresponding to the rate by which fragrance is allowed to diffuse or move into the surrounding space. Alternate embodiments may use a
25 rotary dial, switch or other control in place of slider 410 to adjust the fragrance intensity, or may eliminate fragrance intensity adjustment altogether.

Figures 4A-D depict two separate forces F_1 and F_L impinging upon worst-case transverse loading points 202 and 414, respectively. Worst-case loading points 202 and 414 correspond to locations on housing 108 where the impinging forces F_1 and F_L produce
30 maximum rotational moments upon device 400. Accordingly, the worst case loading points on device 400 are the points furthest from the outlet face along outer ridge 432 of device 400 as shown in Figure 4D.

Worst case support points **204** and **416** lie along the outer edge of housing **108** facing the electrical receptacle and opposite plugs **106A-B**, since the rotational moments produced by reactive forces \mathbf{R}_1 and \mathbf{R}_2 are maximized along edges **434** and **436** (Figure 4D), respectively. To simplify discussion, points **204** and **416** are considered as worst case support points for forces \mathbf{F}_1 and \mathbf{F}_L , respectively, although other points along edges **434** or **436** would produce similar results.

With continued to Figures 4A-D, force \mathbf{F}_1 is shown applied to worst-case loading point **202**, which is located along the upper edge of housing **108** at a point furthest outward from the outlet face. Force \mathbf{F}_1 is therefore applied a distance of d_L (Figs. 4A and 4C) from the outlet face to produce a moment of magnitude $F \times d_L$ about worst case support point **204**. Plugs **106A** and **106B** effectively produce reactive forces \mathbf{R}_1 and \mathbf{R}_2 at distances d_{S1} and d_{S2} from support point **204**, respectively, to generate rotational moments about point **204** equal to $R_1 \times d_{S1}$ and $R_2 \times d_{S2}$, respectively. Applying the analysis of equation 4 set forth above, the transverse loading stability of device **400** is suitably improved by designing distances d_{S1} and d_{S2} to be relatively long compared to distance d_L . Stated another way, stability is improved by designing the maximum thickness of device **400** to be less than the shortest distance from either plug **106A-B** to any loading edge (e.g. edges **434** and **436**) of housing **108** that is in contact with outlet face **212**.

Similarly, force \mathbf{F}_L is shown applied to worst-case loading point **414**, which (like point **202**) is located along the upper edge of housing **108** at a point furthest outward from the outlet face. Force \mathbf{F}_L is therefore applied a distance of d_L (Figs. 4A and 4C) from the outlet face to produce a moment of magnitude $F_L \times d_L$ about worst case support point **204**, which lies along edge **436** as described above. Plugs **106A** and **106B** effectively produce reactive forces \mathbf{R}_1 and \mathbf{R}_2 at a distance d_{SL} from support point **204**. In this case, \mathbf{R}_1 and \mathbf{R}_2 are produced at an equal distance from support point **204** along an axis parallel to the outlet face as best seen in Figure 4C. Accordingly, \mathbf{R}_1 and \mathbf{R}_2 generate rotational moments about point **204** with magnitudes equal to $R_1 \times d_{SL}$ and $R_2 \times d_{SL}$, respectively. Again applying the analysis of equation 4 set forth above, the transverse loading stability of device **400** is suitably improved by designing distance d_{SL} to be relatively long compared to distance d_L .

Regardless of the type of volatilizable material used, the material delivery system may employ any form of controller to modulate the delivery of vapor into the environment. To the extent that the rate at which the vapor is introduced into the environment is a function of

both the temperature of the volatilizable material and the environmental convection conditions in the vicinity of the volatilizable material, any suitable control mechanism may be employed to modulate these two factors. For example, the convection conditions may be controlled through the use of adjustable convection inhibitors (e.g., one or more vents) one
5 or more convection enhancers (e.g., fans, chimney structures, etc.), or other structures that modify the vapor pressure in and around the material delivery system. Similarly, the temperature of the volatilizable material and/or the temperature of the environment in the vicinity of the material delivery system may be controlled through any convenient method, including resistive heating (described above), or through proximity of the device to a
10 preexisting heat source.

Notwithstanding the nature of receptacle 210 -- i.e., whether and to what extent the receptacle is configured to supply electrical current -- the device may be passive, active, or selectably switched between active and passive modes. The term "passive" in this context, as applied to delivery devices, refers to those devices which substantially depend upon ambient
15 conditions to deliver a fragrance or otherwise give rise to a modification of the environment. Such ambient conditions include, for example, ambient thermal conditions (e.g., wall surface temperature and air temperature) and ambient air flow, (e.g., air flow resulting from free convection as well as the movement (if any) of fans, individuals, and other entities within the environment). The term "active" in this context refers to devices that are not
20 passive, e.g., devices which employ integrated fans, heating elements, and other such devices.

In the event that the vapor dispensing device is an active device, any power source required by the device may be intrinsic to receptacle 210, e.g., the 120 V source of a standard wall outlet, or extrinsic to receptacle 210, e.g., supplied by a battery, solar cell, or
25 other such device incorporated into or otherwise associated with delivery device 100. Alternatively, power may be supplied by a combination of intrinsic and extrinsic sources and/or may be incorporated into a refill component.

Delivery device 100 suitably includes one or more removeably attached refill components as briefly mentioned above. That is, referring to Figs. 5A-5C, it may be
30 advantageous for the delivery device to include components that are integral to housing 108 of the delivery system itself as well as one or more refill components 406 (or simply "refills") that can be replaced by the user. In the event delivery system 100 is an air

freshener device, for example, a depleted refill component 406 may be removed from system 100 and replaced by a new refill containing fragrant oil, wax, gel, or the like. The refill suitably includes a refill body and a volatilizable material provided therein.

In accordance with one aspect of the present invention, a refill component is provided which allows a vapor-dispensing device to mimic an electrical receptacle. For example, a refill component comprising a refill body having a volatilizable material provided therein may be configured to be inserted behind the front surface of the device such that it is substantially concealed by the front surface. In accordance with one aspect of the present invention, the refill has a perimeter that is encompassed by the perimeter of the housing.

In accordance with another aspect of the present invention, refill 406 is configured such that it does not significantly obstruct the receptacle's outlet pattern (comprising, for example, two outlets 412A and 412B). In one embodiment, for example, this is accomplished by providing a refill component 406 that at least partially surrounds one or more outlets on the receptacle (variously shown in Figs. 5A-5C). In the event that the delivery device is used in connection with a standard electrical receptacle, it is desirable for refill 406 to encompass two or more sides of the outlet pattern (Fig. 5A). To the extent that it is advantageous to supply the greatest possible volume of volatilizable material, the refill may be configured as a rectangular ring that completely surrounds the outlet pattern (Fig. 5B). Alternatively, the refill may be configured in a 'U' shape to allow refill 406 to be slideably removed from the device (Fig. 5C).

For the sake of brevity, conventional electrical and mechanical design techniques used in developing various vapor-dispensing devices (and the various components thereof) are not described in detail herein. Accordingly, devices disclosed herein may be readily modified to create equivalent embodiments through application of general electrical and mechanical principles. Although the embodiments described herein show vapor dispensing devices that are generally quadrilateral in shape, for example, other design styles could be formulated. Vapor dispensing devices could be readily formulated with angular, round, oval or other shapes, for example, as well as with combinations of multiple shapes and structures. In a further embodiment, the vapor dispensing device may be adorned with an ornamental design such as a floral design, an outdoor scene, a cartoon or movie character, or the like. Moreover, the general concepts of improving transverse loading stability described herein

may be applied to other electrical devices such as air filters, nightlights, audio speakers, wireless control devices, timers and the like.

The particular implementations shown and described herein are examples of the invention and are not intended to otherwise limit the scope of the invention in any way. The
5 connecting lines shown in the various figures contained herein are intended to represent exemplary functional relationships and/or physical couplings between the various elements. It should be noted that many alternative or additional functional relationships, physical connections or logical connections may be present in a practical vapor-dispensing device. The corresponding structures, materials, acts and equivalents of all elements in the claims
10 below are intended to include any structure, material or acts for performing the functions in combination with other claimed elements as specifically claimed. The scope of the invention should be determined by the appended claims and their legal equivalents, rather than by the examples given above. No item or component is essential to the practice of the invention unless the element is specifically described herein as "critical", "essential" or
15 "required".

Claims

1. A vapor-dispensing device having a high transverse loading stability when connected to an electrical receptacle having an outlet face, said vapor-dispensing device comprising:

- 5 a housing;
 a device outlet provided within said housing;
 a plug electrically coupled to said device outlet and configured to be inserted into said outlet face;
 said housing having a worst-case transverse loading point a distance d_L from
10 said outlet face along an axis through said worst-case transverse loading point and substantially perpendicular to said outlet face;
 said housing having a worst-case support point a distance d_S from said plug along an axis through said worst-case support point and substantially parallel to said outlet face;
15 said transverse loading stability of said vapor dispensing device characterized by a transverse loading coefficient η , defined as:
 $\eta \equiv d_S/d_L$
 wherein said vapor dispensing device has a transverse loading coefficient $\eta >$
1.0.

20

2. A vapor dispensing device configured to be connected to an electrical receptacle having an outlet face, said vapor dispensing device comprising a housing and a plug configured to be inserted into the outlet face, wherein the housing comprises a worst-case transverse loading point a perpendicular distance d_L from the outlet face and a worst-
25 case support point a distance d_S from the plug, and wherein the distance d_S is greater than the distance d_L .

3. The vapor dispensing device of claim 2 further comprising a first device outlet electrically coupled to the plug.

30

4. The vapor dispensing device of claim 3 further comprising a second plug electrically coupled to the plug.

5. The vapor dispensing device of claim 2 wherein the worst case transverse loading point is defined as a point on the housing having a maximum distance from the outlet face.

6. The vapor dispensing device of claim 5 wherein the worst case support point is defined as a point along a loading edge of the housing adjacent the front face and opposite the plug from the worst case transverse loading point.

7. The vapor dispensing device of claim 6 wherein the thickness of the housing is less than the shortest distance from the plug to the loading edge of the housing.

8. The vapor dispensing device of claim 1, further including a refill component removeably attached to said housing.

9. The apparatus of claim 8, wherein said refill component at least partially surrounds the outlet.

10. The apparatus of claim 8, wherein said refill is generally "U"-shaped.

11. The apparatus of claim 10, wherein said refill is configured to slideably attach to the environment-altering apparatus.

12. The apparatus of claim 8, wherein said refill component is a rectangular ring.

13. The apparatus of claim 1, wherein the vapor-delivery device is passive.

14. The apparatus of claim 1, wherein the vapor-delivery device is active.

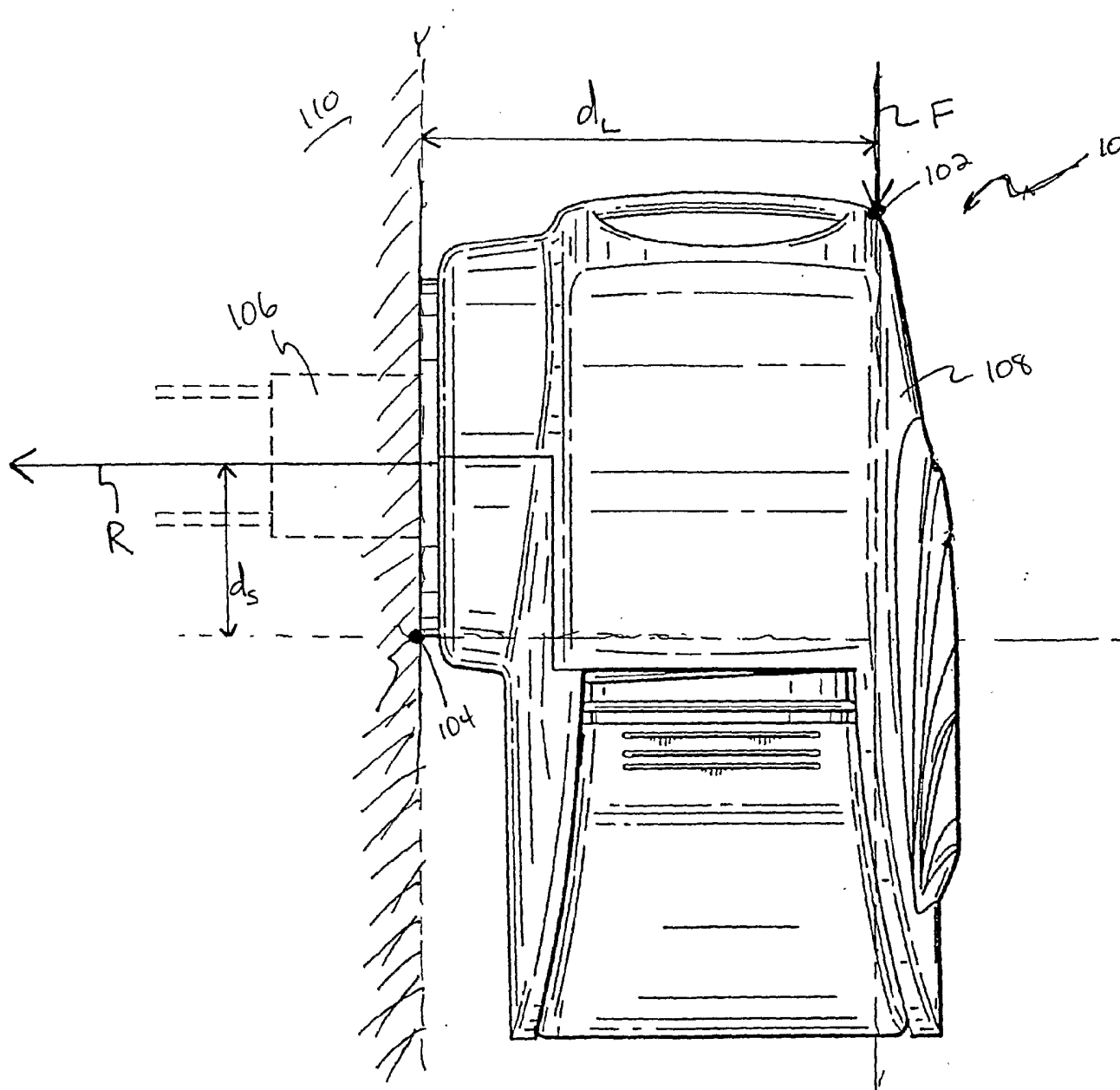


FIG. 1
(Prior Art)

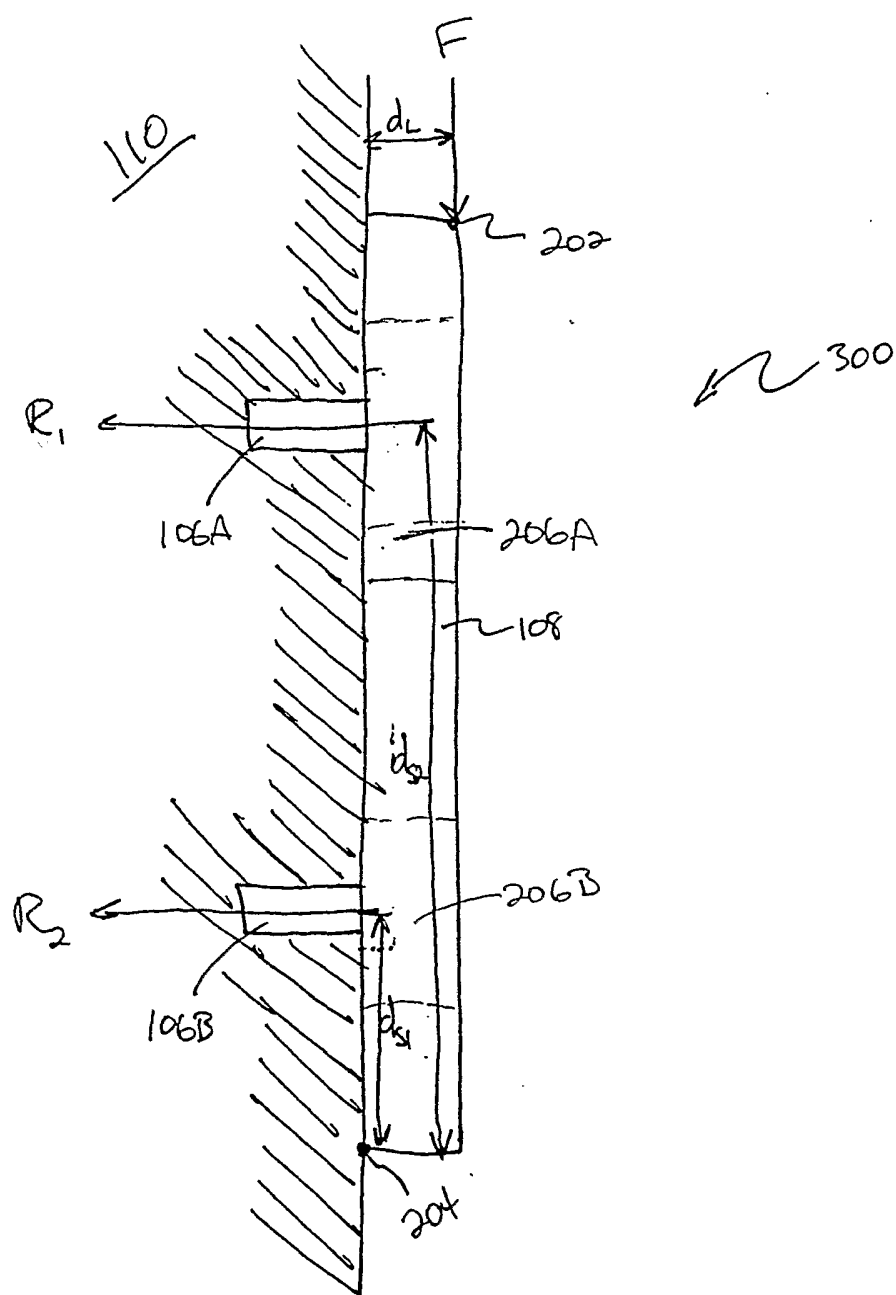


FIGURE 3

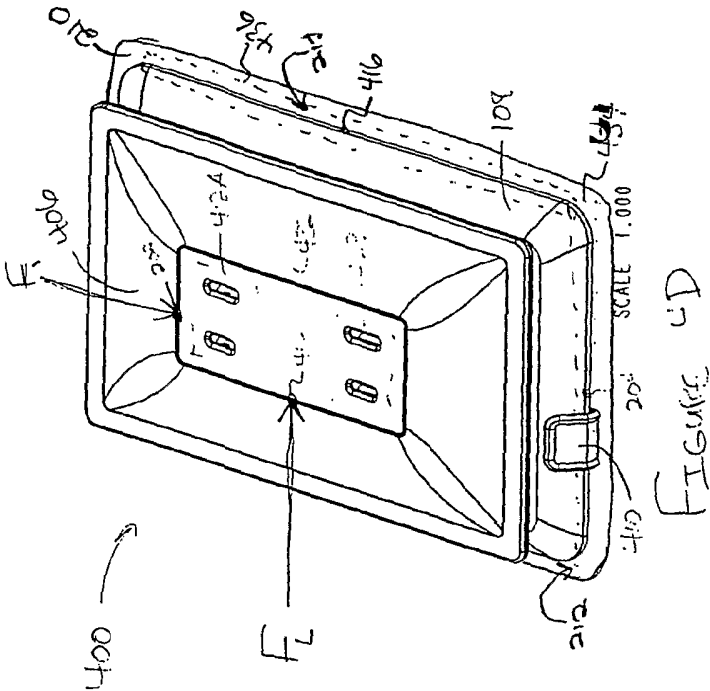


FIGURE 4D

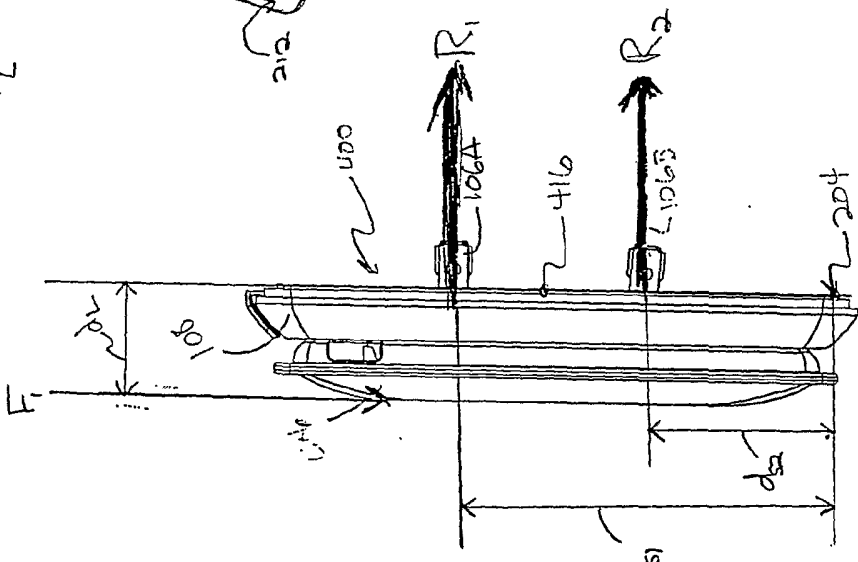


FIGURE 4C

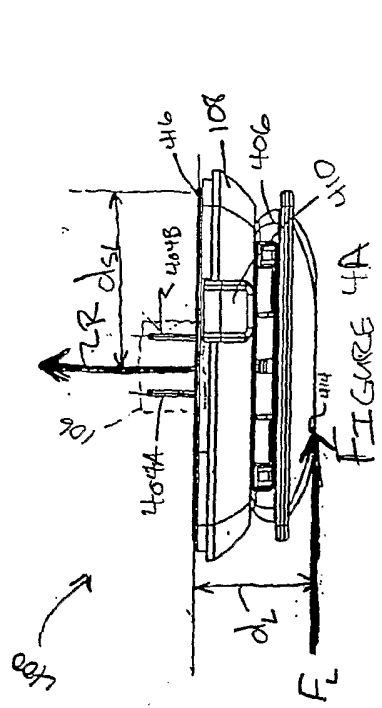


FIGURE 4A

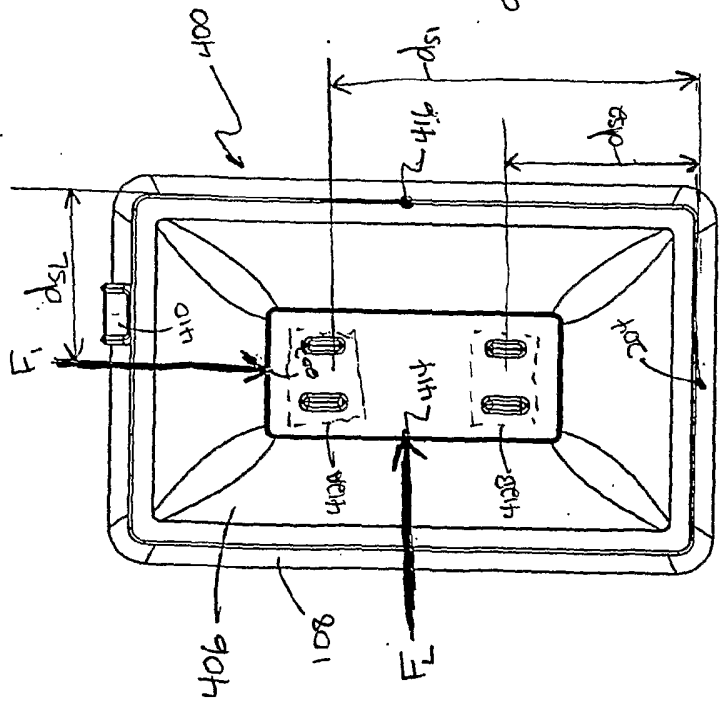
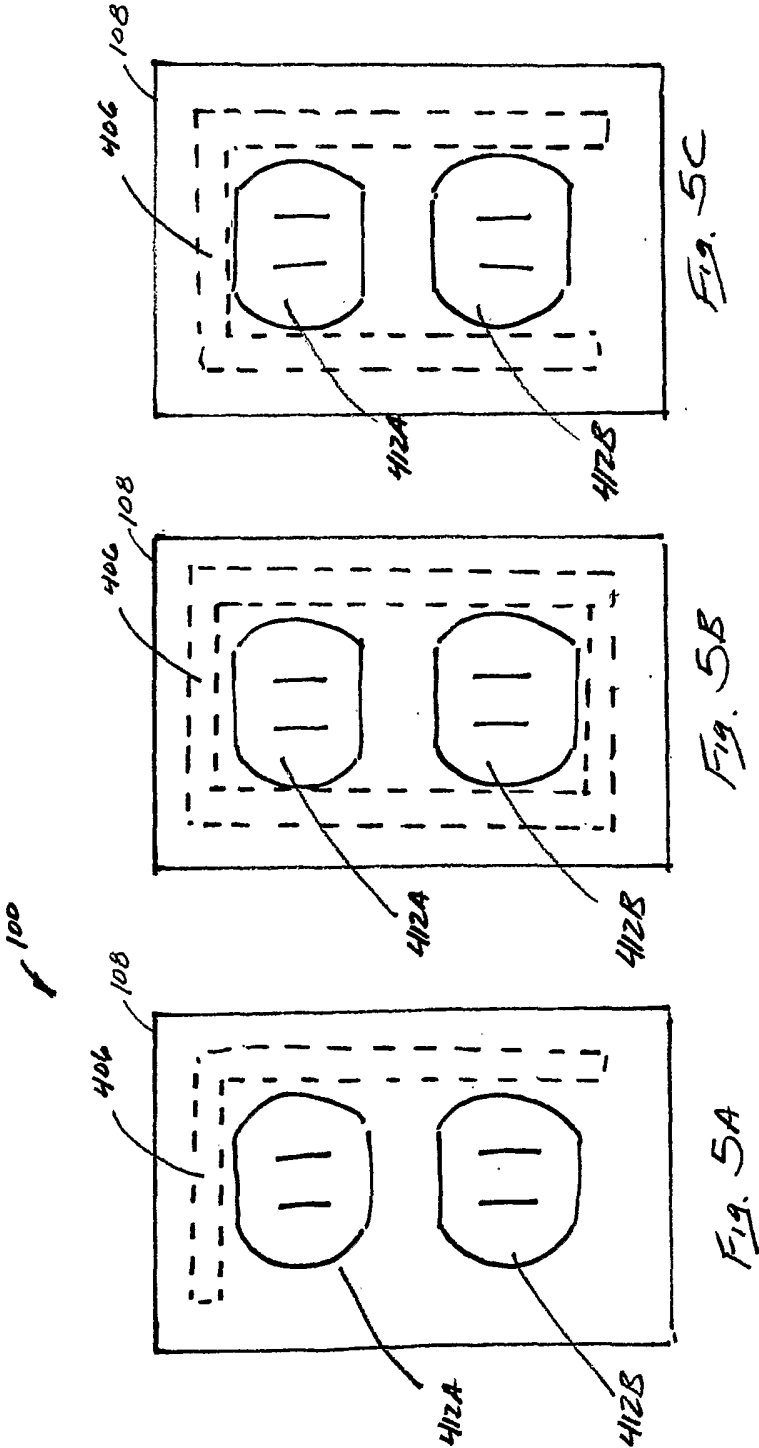


FIGURE 4B



INTERNATIONAL SEARCH REPORT

Internat Application No

PCT/US 03/25243

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 A61L9/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 A61L A01M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 804 821 A (GLUCKSMAN DOV Z) 14 February 1989 (1989-02-14) column 6, line 11 -column 7, line 60; figures 7,9	1-3,5-8, 14
X	DE 41 31 613 A (GLOBOL GMBH) 25 March 1993 (1993-03-25) column 1, line 20 - line 58; figures 1,13,16	2,5-7
A	column 2, line 64 -column 3, line 30 column 8, line 13 - line 39	8,10,11, 14
X	US 6 085 026 A (HAMMONS RANDALL LEE ET AL) 4 July 2000 (2000-07-04) figures 1,3	2,5-7
	-/--	

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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Date of the actual completion of the international search

10 December 2003

Date of mailing of the international search report

19/12/2003

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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

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