



(12) **DEMANDE DE BREVET CANADIEN
CANADIAN PATENT APPLICATION**

(13) **A1**

(86) **Date de dépôt PCT/PCT Filing Date:** 2016/01/25
(87) **Date publication PCT/PCT Publication Date:** 2017/08/03
(85) **Entrée phase nationale/National Entry:** 2018/07/19
(86) **N° demande PCT/PCT Application No.:** RU 2016/000020
(87) **N° publication PCT/PCT Publication No.:** 2017/131546

(51) **Cl.Int./Int.Cl. G01K 1/14** (2006.01),
G01K 13/02 (2006.01), **G01K 17/06** (2006.01)
(71) **Demandeur/Applicant:**
ROSEMOUNT INC., US
(72) **Inventeurs/Inventors:**
KUZNETSOV, YURI NICKOLAYEVICH, RU;
RUD, JASON H., US;
GARIPOV, SAIT SAITOVICH, RU;
KRIVONOGOV, ALEKSEY ALEKSANDROVICH, RU;
FOMCHENKO, SERGEY ANDREYEVICH, RU;
REPYEVSKY, VLADIMIR VICTOROVICH, RU
(74) **Agent:** MARKS & CLERK

(54) **Titre : SYSTEME NON INTRUSIF DE CALCUL DE TEMPERATURE DE FLUIDE DE TRAITEMENT**
(54) **Title: NON-INTRUSIVE PROCESS FLUID TEMPERATURE CALCULATION SYSTEM**

(57) **Abrégé/Abstract:**

A process fluid temperature calculation system includes a first temperature sensor disposed to measure an external temperature of a process fluid conduit. The process fluid temperature calculation system has a stem portion having a known thermal impedance. A second temperature sensor is spaced from the first temperature sensor by the stem portion. Measurement circuitry is coupled to the first and second temperature sensors. A microprocessor is coupled to the measurement circuitry to receive temperature information from the measurement circuitry and to provide an estimate of temperature of process fluid within the process fluid conduit using a heat flux calculation.

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property
Organization
International Bureau(43) International Publication Date
3 August 2017 (03.08.2017)(10) International Publication Number
WO 2017/131546 A1

(51) International Patent Classification:

G01K 1/14 (2006.01) *G01K 17/06* (2006.01)
G01K 13/02 (2006.01)

(21) International Application Number:

PCT/RU2016/000020

(22) International Filing Date:

25 January 2016 (25.01.2016)

(25) Filing Language:

English

(26) Publication Language:

English

(71) Applicant: ROSEMOUNT INC. [US/US]; 8200 Market Boulevard, Chanhassen, Minnesota 55317 (US).

(72) Inventors: KUZNETSOV, Yuri Nickolayevich; 16-1 Sverdlova st., Snezhinsk, 546770 (RU). RUD, Jason H.; 2307 Coldwater Crossing, Mauer, MN 55360 (US). GARISOV, Sait Saitovich; 25-29 Pobedy ave., Kopeysk, 456604 (RU). KRIVONOGOV, Aleksey Aleksandrovich; 29-32 Agalakova st., Chelyabinsk, 454010 (RU). FOMCHENKO, Sergey Andreyevich; 112-214 Komarova st., Chelyabinsk, 454071 (RU). REPYEVSKY, Vladimir Victorovich; 23a-8 Moldavskaya st., Chelyabinsk, 545021 (RU).

(74) Agent: LAW FIRM "GORODISSKY & PARTNERS" LTD; MITS Alexander Vladimirovich, POPOVA Eliza-

veta Vitalievna, B. Spasskaya str., 25, bldg 3, Moscow, 129090 (RU).

(81) Designated States (*unless otherwise indicated, for every kind of national protection available*): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, JP, KE, KG, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.(84) Designated States (*unless otherwise indicated, for every kind of regional protection available*): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

Published:

— with international search report (Art. 21(3))

(54) Title: NON-INTRUSIVE PROCESS FLUID TEMPERATURE CALCULATION SYSTEM

(57) Abstract: A process fluid temperature calculation system includes a first temperature sensor disposed to measure an external temperature of a process fluid conduit. The process fluid temperature calculation system has a stem portion having a known thermal impedance. A second temperature sensor is spaced from the first temperature sensor by the stem portion. Measurement circuitry is coupled to the first and second temperature sensors. A microprocessor is coupled to the measurement circuitry to receive temperature information from the measurement circuitry and to provide an estimate of temperature of process fluid within the process fluid conduit using a heat flux calculation.



WO 2017/131546 A1

NON-INTRUSIVE PROCESS FLUID TEMPERATURE CALCULATION SYSTEM

BACKGROUND

[0001] The process industry employs process variable transmitters to monitor process variables associated with substances such as solids, slurries, liquids, vapors, and gases in chemical, pulp, petroleum, pharmaceutical, food and other fluid process plants. Process variables includes pressure, temperature, flow, level, turbidity, density, concentration, chemical composition, and other properties.

[0002] A process fluid temperature transmitter provides an output related to a process fluid temperature. The temperature transmitter output can be communicated over a process control loop to a control room, or the output can be communicated to another process device such that the process can be monitored and controlled.

[0003] Traditionally, process fluid temperature transmitters were coupled to or employed thermowells which provided a temperature sensor in thermal communication with a process fluid but otherwise protected the temperature sensor from direct contact with the process fluid. The thermowell is positioned within the process fluid in order to ensure substantial thermal contact between the process fluid and the temperature sensor disposed inside the thermowell. Thermowells are typically designed using relatively robust metal structures such that the thermowell can withstand a number of challenges provided by the process fluid. Such challenges can include physical challenges, such as process fluid flowing past the thermowell at a relatively high rate; thermal challenges, such as extremely high temperature; pressure challenges, such as the process fluid being conveyed or stored at a high pressure; and chemical challenges, such as those provided by a caustic process fluid. Further, thermowells can be difficult to design into a process installation. Such thermowells require a process intrusion where the thermowell is mounted to and extends into a process vessel such as a tank or pipe. This process intrusion itself must be carefully designed and controlled such that the process fluid does not leak from the vessel at the intrusion point.

[0004] There are a number of factors that can compromise the structural integrity of a thermowell. In some cases, not all factors may be fully considered and thermowells have sometimes bent or even broken off thus causing the process installation to be shut

down for a significant period of time. This is highly undesirable. For some applications, a thermowell simply cannot be used without potential damage. In such applications, it may be beneficial, or even required, to use a non-invasive process fluid temperature calculation system. With such a system, a pipe clamp sensor is used to couple a temperature sensor to a process vessel, such as a pipe. While such a non-invasive process fluid temperature calculation provides the benefit of not requiring a process intrusion, nor subjecting a thermowell directly to the process fluid, there is a tradeoff. Specifically, a non-invasive temperature calculation system is typically less accurate in detecting the process fluid temperature than a thermowell which extends into the process fluid and measures the temperature directly.

[0005] Providing a non-invasive process fluid temperature calculation system that could more accurately reflect the temperature of the process fluid would reduce some of the tradeoff required by users of such systems and also potentially provide more accurate temperature calculation and process control in situations where thermowells were not desired or possible.

SUMMARY

[0006] A process fluid temperature calculation system includes a first temperature sensor disposed to measure an external temperature of a process fluid conduit. The process fluid temperature calculation system has a stem portion having a known thermal impedance. A second temperature sensor is spaced from the first temperature sensor by the stem portion. Measurement circuitry is coupled to the first and second temperature sensors. A microprocessor is coupled to the measurement circuitry to receive temperature information from the measurement circuitry and to provide an estimate of temperature of process fluid within the process fluid conduit using a heat flux calculation.

BRIEF DESCRIPTION OF THE DRAWINGS

[0007] FIG. 1 is a chart of process fluid temperature versus pipe clamp temperature illustrating error associated with a non-invasive temperature calculation system.

[0008] FIG. 2 is a diagrammatic view of a non-invasive temperature calculation system coupled to a process fluid vessel in accordance with one embodiment of the present invention.

[0009] FIG. 3 is a diagrammatic view illustrating heat flow through a non-invasive process fluid temperature calculation system in accordance with an embodiment of the present invention.

[0010] FIG. 4 is a block diagram of a non-invasive process fluid temperature calculation system in accordance with an embodiment of the present invention.

[0011] FIG. 5 is a flow diagram of a method of estimating process fluid temperature in a non-invasive temperature measurement system in accordance with an embodiment of the present invention.

[0012] FIGS. 6A and 6B are charts illustrating corrected temperature and compensation error, respectively, of a non-invasive process fluid temperature calculation system in accordance with an embodiment of the present invention.

DETAILED DESCRIPTION

[0013] As set forth above, selecting a non-invasive temperature calculation system has traditionally required a tradeoff in accuracy. FIG. 1 is a chart of process fluid temperature versus pipe clamp temperature illustrating error of a non-invasive temperature calculation system as the process fluid temperature changes. The left axis of the chart shows both process fluid temperature and pipe clamp temperature, while the right axis shows error in degrees Celsius. At the initial time, the process fluid temperature and pipe clamp temperature are each at approximately 25 degrees Celsius and the error is approximately zero degrees Celsius. As the process fluid temperature increases, the pipe clamp temperature also increases, but at a lesser rate. Additionally, as the process fluid temperature changes, the pipe clamp also changes, but does not quite match the process fluid temperature. This generates an error that fluctuates between approximately 14 and 16 degrees Celsius. This indicates that the pipe clamp temperature is reading approximately 14 to 16 degrees below the temperature of the process fluid.

[0014] FIG. 2 is a diagrammatic view of a non-invasive process fluid calculation system in accordance with an embodiment of the present invention. System 100 is illustrated as coupled to process fluid vessel 102, which, in the illustrated example, is a pipe or conduit. As such, system 100 includes a clamp 104 that secures around the outer surface of pipe 102. While the embodiment shown in FIG. 2 employs a threaded fastener to secure clamp 104 about pipe 102, any suitable clamping mechanism can be employed.

Clamp 104 includes a temperature sensor (shown in FIG. 3) that is placed in direct thermal contact with the outside skin surface of pipe 102. This temperature sensor is electrically coupled to electronics disposed within housing 108 such that the electronics within housing 108 can measure the temperature of the pipe 102. System 100 also includes a stem portion 110 that couples clamp 104 to housing 108. Stem portion 110 conducts heat from clamp 104 to housing 108. However, the material selected for manufacturing stem 110; the length of stem 110; and/or the thickness of the material comprising stem 110 can be designed to provide a specific thermal impedance of stem 110. As set forth herein, thermal impedance is defined as the degree to which a structure, such as stem 110, resists heat flow. Thermal impedance may generally be thought of as the reciprocal of thermal conductance. Since some process fluid pipes 102 may be provided at relatively high temperatures, it may be beneficial for stem 110 to have a higher thermal impedance in order to protect electronics within housing 108 from such elevated temperatures.

[0015] In accordance with some embodiments of the present invention, an additional temperature sensor is provided a certain distance away from pipe 102. In one embodiment, the additional temperature sensor is disposed within housing 108. However, embodiments of the present invention can be practiced where the additional temperature sensor is provided within a fixed location inside stem portion 110. As set forth in greater detail below, sensing the skin temperature of pipe 102 and the spaced temperature from the additional temperature sensor can provide an indication of heat flow. Moreover, since environmental effects, such as wind chill and ambient temperature can affect the degree to which heat is removed from stem 110 as it flows therethrough, at least some embodiments of the present invention include thermal insulation as shown in phantom in FIG. 2. This thermal insulation can be provided about pipe 102 and clamp 104 as shown at reference numeral 112. Moreover, in one embodiment the thermal pipe insulation can extend a minimum distance in both directions (upstream and downstream) from pipe clamp 104. In one embodiment, this minimum distance is at least six inches. Additionally, thermal insulation can be provided about stem portion 110 as illustrated at reference numeral 114. For embodiments that employ insulation 112 and/or 114, the insulation should be at least ½ inch thick, and should preferably be selected to reduce or

potentially eliminate any external thermal absorption. For example, ideally the outer surface of the thermal insulation would be white or reflective.

[0016] FIG. 3 is a diagrammatic view of a non-invasive process fluid temperature calculation system where heat flow is modeled in terms of electrical components. Specifically, the temperature of the process fluid is illustrated as node 150 and is coupled to temperature sensor 152 via the thermal impedance of the pipe material (R_{pipe}) indicated diagrammatically as resistor 154. It should be noted that the thermal impedance of the pipe material can be known either by virtue of the material of the pipe itself and the thickness of the pipe wall such that a suitable impedance parameter could be entered into circuitry within housing 108. For example, a user configuring the system may indicate that the pipe is constructed from stainless steel and is $\frac{1}{2}$ inch thick. Then, suitable lookup data within memory of the non-invasive process fluid temperature calculation system identifies a corresponding thermal impedance that matches the selected material and wall thickness. Moreover, embodiments may be practiced where the pipe material is simply selected and the thermal impedance can be calculated based on the selected material and the selected wall thickness. Regardless, embodiments of the present invention generally leverage knowledge of the thermal impedance of the pipe material. Further, in embodiments where the thermal impedance of the pipe material cannot be known ahead of time, it is also possible that a calibration operation can be provided where a known process fluid temperature is provided to the non-invasive process fluid temperature calculation system and the thermal impedance is set as a calibration parameter.

[0017] As indicated in FIG. 3, heat may also flow from temperature sensor 152 out the sidewall of stem portion 110 to the ambient environment illustrated at reference numeral 156 and this thermal impedance (R_2) is indicated diagrammatically at reference number 158. As set forth above, the thermal impedance to ambient from the skin temperature sensor 152 can be increased by providing an insulation material, in some embodiments. Heat will flow from the external surface of pipe 102 through stem portion 110 to housing 108 via conduction through stem portion 110. The thermal impedance of stem portion 110 (R_{sensor}) is illustrated diagrammatically at reference numeral 160. Finally, heat may also flow from the temperature sensor 162, coupled to a terminal block within housing 108, to the ambient environment via thermal impedance 164 (R_1).

[0018] When the non-invasive process fluid temperature calculation system is connected, by virtue of pipe clamp 104, to a process fluid conduit, such as pipe 102, both the skin temperature of the process fluid conduit and the transmitter terminal temperature 162 can be measured and used in a heat flux calculation to accurately infer or otherwise approximate the process fluid temperature 150 within conduit 102.

[0019] When the process fluid temperature changes, it will affect both the reading from temperature sensor 152 and the reading from terminal temperature sensor 162 since there is a rigid mechanical interconnection between them (heat conduction through stem portion 110) with relatively high thermal conductance. The same applies to the ambient temperature. When the ambient temperature changes, it will impact both of these measurements as well, but by a much lesser extent.

[0020] For slow changing conditions, the basis heat flux calculation can be simplified into:

$$T_{\text{corrected}} = T_{\text{sensor}} + (T_{\text{sensor}} - T_{\text{terminal}}) * (R_{\text{pipe}} / R_{\text{sensor}}).$$

A non-insulated clamp assembly or fast-changing process/ambient conditions can be further corrected by dynamically adjusting the R_{sensor} coefficient using the rate of change in the terminal temperature versus the rate of change in the conduit skin temperature. If the conduit skin temperature is changing quickly, additional correction may be applied during this time in order to minimize time constants. Similarly, if ambient temperature is changing quickly in relation to the conduit skin temperature, less correction may be applied.

[0021] FIG. 4 is a diagrammatic view of a non-invasive process fluid temperature measurement in accordance with an embodiment of the present invention. As shown in FIG. 4, housing 108 contains microprocessor 250, first A/D converter 252, second A/D converter 254, and memory 256. First A/D converter 252 and second A/D converter 254 are analog-to-digital converters. While the example shown in FIG. 4 employs two discrete analog-to-digital converters, embodiments of the present invention can be practiced with a single analog-to-digital converter and suitable switching circuitry, such as a multiplexer, to couple the single analog-to-digital converter to multiple temperature sensors.

[0022] Microprocessor 250 is coupled to first temperature sensor 152 via first analog-to-digital converter 252. First analog-to-digital converter 252 is electrically coupled to wires of temperature sensor 152 to convert the analog electrical signals from temperature sensor 152 to a digital signal for microprocessor 250. Temperature sensor 152 and/or temperature sensor 162 can be any suitable temperature sensing device or component including a Resistance Temperature Device (RTD), a thermocouple, thermistor, or any other suitable device that has an electrical characteristic that varies with temperature. Second analog-to-digital converter 254 couples microprocessor 250 to second temperature sensor 162. Second temperature sensor 162 can also be any suitable temperature sensing device, but, in one embodiment, is the same type of temperature sensor as temperature sensor 152. Second analog-to-digital converter 254 is electrically coupled to wires of temperature sensor 162 and converts an analog electrical signal from second temperature sensor 162 to a digital signal for microprocessor 250. Together, first analog-to-digital converter 252 and second analog-to-digital converter 254 comprise measurement circuitry that couples the temperature sensors to microprocessor 250.

[0023] Memory 256 is a digital data storage device that is electrically coupled to microprocessor 250. Memory 256 contains data, as well as parameters such as thermal impedance information with respect to the pipe material and the stem portion. The thermal impedance of the stem portion will be determined during the manufacture of the system and thus can be entered during manufacture. The thermal impedance of the pipe material can be selected during commissioning of the system, or can otherwise be empirically determined during a calibration or other suitable process. Regardless, memory 256 contains parameters that allow microprocessor 250 to estimate process fluid temperature information from the signals obtained from temperature sensors 152 and 162.

[0024] Process vessel wall parameters, stored within memory 256, can include physical characteristics of the process vessel wall such as K_w of the process vessel wall as well as the process vessel wall thickness. Process vessel wall parameters may be stored in memory 256 when the temperature measurement assembly is manufactured. However, as set forth above, these parameters may be determined during configuration or commissioning of the assembly or during a calibration process.

[0025] According to Fourier's Conduction Law, heat flux through stem portion 110 should be the same as through the wall of process vessel 102. Under this condition, the temperature of the internal surface of the process vessel wall (and also the process fluid temperature) may be determined from the signal obtained from temperature sensor 152 and the signal obtained from terminal temperature sensor 162.

[0026] In the embodiment shown in FIG. 4, housing 108 may also include communication interface 258. Communication interface 258 provides communication between the temperature measurement assembly and control or monitoring system 262. So equipped, the temperature measurement system may also be referred to as a temperature measurement transmitter and may transmit the temperature of the process fluid to control or monitoring system 262. Communication between the temperature measurement system and control or monitoring system 262 can be through any suitable wireless or hard-wired connection. For example, communication may be represented by an analog current over a two-wire loop that ranges from 4-20mA. Alternatively, the communication may be transmitted in a digital form over a two-wire loop using the Highway Addressable Remote Transducer (HART[®]) digital protocol, or over a communication bus using a digital protocol such as FOUNDATION[™] Fieldbus. Communication interface 258 may optionally or alternatively include wireless communication circuitry 264 for communication by wireless transmission using a wireless process communication protocol such as WirelessHART in accordance with IEC 62591. Moreover, communication with control or monitoring system 262 can be direct or through a network of any number of intermediate devices, for example, a wireless mesh network (not shown).

[0027] Communication interface 258 can help manage and control communication to and from the temperature measurement system. For example, control or monitoring system 262 may provide for configuration of the temperature measurement system, including entering or selecting any suitable number of parameters relative to thermal impedance of the process vessel wall, etc.

[0028] The example shown in FIG. 4 may also include local operator interface 266. Local operator interface 266 can be provided to display the estimated temperature of the process fluid, as well as the measured temperature of the external surface provided directly by temperature sensor 152. Additionally, local operator interface may provide an

indication of the terminal temperature measured by temperature sensor 162. Further still, ambient temperature measurement can also be provided using an additional temperature sensor and such measurement can optionally be indicated by local operator interface 266. Local operator interface 266 may include any suitable number of buttons or keypad that allow a user to interact with the non-invasive temperature measurement system. Such interaction can include entering or selecting the material of the process fluid conduit as well as the thickness of the process fluid conduit wall.

[0029] FIG. 5 is a flow diagram of a method of inferring process fluid temperature in accordance with an embodiment of the present invention. Method 300 begins at block 302 where an external temperature of a process fluid conduit is measured. As set forth above, this external temperature is preferably measured using a temperature sensor positioned directly against the outside diameter or surface of the process fluid conduit. Next, at block 304, a terminal temperature within a housing of a non-invasive process fluid temperature calculation system is measured. While embodiments described herein generally refer to the measurement of the transmitter terminal temperature, embodiments of the present invention can be practiced by measuring the temperature of the housing itself, or any other suitable structure within the housing. Next, at block 306, the measured external conduit temperature and measured terminal temperatures are provided to a processing facility, such as a microprocessor 250 disposed within housing 108, such that the temperature of the process fluid can be inferred using a basic heat flux calculation, such as that set forth above. While embodiments described thus far have generally focused upon a processor, such as microprocessor 250, providing a calculation within housing 108, it is expressly contemplated that embodiments described herein can also be practiced by providing the raw temperature measurements from the external conduit temperature sensor and the terminal temperature sensor to a remote facility or processor that can estimate the process fluid temperature. Regardless, the basic heat flux calculation generally provides an estimate of the process fluid temperature using the values from external conduit temperature sensor and the terminal temperature sensor. As set forth above, dynamic weighting 308 can be applied in accordance with some embodiments of the present invention such that rapidly changing conditions can be dynamically adjusted. For example, in one embodiment, a fast changing process fluid temperature condition can be

further corrected by dynamically adjusting the thermal impedance of the sensor assembly parameters stored within memory 256 by the rate of change in the terminal temperature measurement versus the rate of change in the skin temperature measurement (provided by temperature sensor 152). If the skin temperature measurement is changing quickly, additionally correction may be applied during the time of quickly changing temperature in order to minimize error due to time constants. Similarly, if ambient temperature is changing quickly in relation to skin temperature, less correction may be applied.

[0030] Next, at block 310, the inferred process fluid temperature is provided as an output by the non-invasive process fluid temperature measurement system. This output can be provided as a local output via a local operator interface, as indicated at block 312, and/or the output can be provided to a remote device as indicated at block 314. Moreover, as indicated at block 316, the provision of the output to a remote device can be via a wired process communication coupling as indicated at block 316 and/or it may be provided wirelessly as indicated at block 318.

[0031] FIGS. 6A and 6B are charts illustrating results of non-invasive process fluid temperature estimation using heat flux calculations in accordance with embodiments of the present invention. As shown in FIG. 6A, the pipe skin temperature fluctuates to a relatively small extent during a time interval from approximately 12:40 PM to 2:45 PM. In that same time interval, the terminal temperature fluctuates between approximately 27 degrees Celsius and approximately 33 degrees Celsius. The process temperature is illustrated at reference numeral 400 and is tracked very closely by the corrected temperature output 402. The compensation error is directly indicated in FIG. 6B. As shown, embodiments of the present invention provide a non-invasive process fluid temperature calculation or estimation system that is able to accurately to reflect the temperature of the process fluid flowing within a process fluid conduit, such as a pipe, without requiring an intrusion into the process fluid conduit itself. Accordingly, process control may be improved using the heat flux-based temperature calculation techniques described herein.

[0032] Although the present invention has been described with reference to preferred embodiments, workers skilled in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention.

WHAT IS CLAIMED IS:

1. A process fluid temperature calculation system comprising:
a first temperature sensor disposed to measure an external temperature of a process fluid conduit;
a stem portion having a known thermal impedance;
a second temperature sensor spaced from the first temperature sensor by the stem portion;
measurement circuitry coupled the first and second temperature sensors; and
a microprocessor coupled to the measurement circuitry to receive temperature information from the measurement circuitry and to calculate a process fluid temperature output using a heat flux calculation.
2. The process fluid temperature calculation system of claim 1, and further comprising a clamp configured to attach to the process fluid conduit and maintain thermal contact between the process fluid conduit and the first temperature sensor.
3. The process fluid temperature calculation system of claim 1, and further comprising a housing attached to the stem portion, the housing containing the measurement circuitry, the second temperature sensor and the microprocessor.
4. The process fluid temperature calculation system of claim 3, and further comprising a terminal block disposed within the housing, the terminal block mounting the second temperature sensor.
5. The process fluid temperature calculation system of claim 3, and further comprising memory containing parameters for calculating heat flux.
6. The process fluid temperature calculation system of claim 5, wherein the parameters include physical characteristic of a wall of the process fluid conduit.
7. The process fluid temperature calculation system of claim 6, wherein the physical characteristic includes a material from which the process fluid conduit is constructed.

8. The process fluid temperature calculation system of claim 6, wherein the physical characteristic is process fluid conduit wall thickness.
9. The process fluid temperature calculation system of claim 1, and further comprising thermal insulation disposed about the process fluid conduit adjacent the first temperature sensor.
10. The process fluid temperature calculation system of claim 1, and further comprising thermal insulation disposed about the stem portion.
11. The process fluid temperature calculation system of claim 1, wherein the microprocessor is configured to dynamically compensate temperature output based on a rate of change of temperature measured by the first temperature sensor.
12. The process fluid temperature calculation system of claim 1, wherein the microprocessor is configured to dynamically compensate the temperature output based on a rate of change of temperature measured by the second temperature sensor.
13. The process fluid temperature calculation system of claim 1, wherein the microprocessor is configured to dynamically compensate the temperature output based on a rate of change of temperature measured by the first temperature sensor in comparison to a rate of change of temperature measured by the second temperature sensor.
14. The process fluid temperature calculation system of claim 1, and further comprising a communication interface configured to communicate the output to a remote device.
15. The process fluid temperature calculation system of claim 1, and further comprising a local operator interface coupled to the microprocessor.

16. The process fluid temperature calculation system of claim 1, wherein the measurement circuitry includes a plurality of analog-to-digital converters, a first analog-to-digital converter being coupled to the first temperature sensor and a second analog-to-digital converter being coupled to the second temperature sensor.

17. A method of calculating a temperature of process fluid within a process fluid conduit, the method comprising:

measuring a temperature of an external surface of the process fluid conduit;
measuring a temperature of a location spaced from the process fluid conduit by a stem portion having a known thermal impedance;
using a heat flux equation and the measured temperatures from the external surface of the process fluid conduit and the location spaced from the process fluid conduit by the stem portion to calculate heat flux; and
using the calculated heat flux in combination with a thermal impedance parameter of a wall of the process fluid conduit to calculate the temperature of process fluid within the process fluid conduit; and
providing the calculated temperature as an output.

18. The method of claim 17, and further comprising providing a process fluid having a known temperature in the process fluid conduit, and updating the known thermal impedance of the stem portion for calibration.

19. The method of claim 17, and further comprising dynamically compensating the estimation of process fluid temperature based on a rate of change of measurements of the external surface of the process fluid conduit.

20. A process fluid temperature calculation system comprising:
a pipe clamp;
a first temperature sensor coupled to the pipe clamp and configured to measure an external temperature of a process fluid conduit;
a stem portion coupled to the pipe clamp, the stem portion having a known thermal impedance;

a housing coupled to the stem portion, the housing containing a terminal block, measurement circuitry, and a microprocessor;

a second temperature sensor mounted to the terminal block within the housing;

wherein the measurement circuitry is coupled to the microprocessor and to the first and second temperature sensors; and

wherein the microprocessor is configured to provide a process fluid temperature output using a heat flux calculation and information from the measurement circuitry indicative of the external temperature of the process fluid conduit and the terminal block.

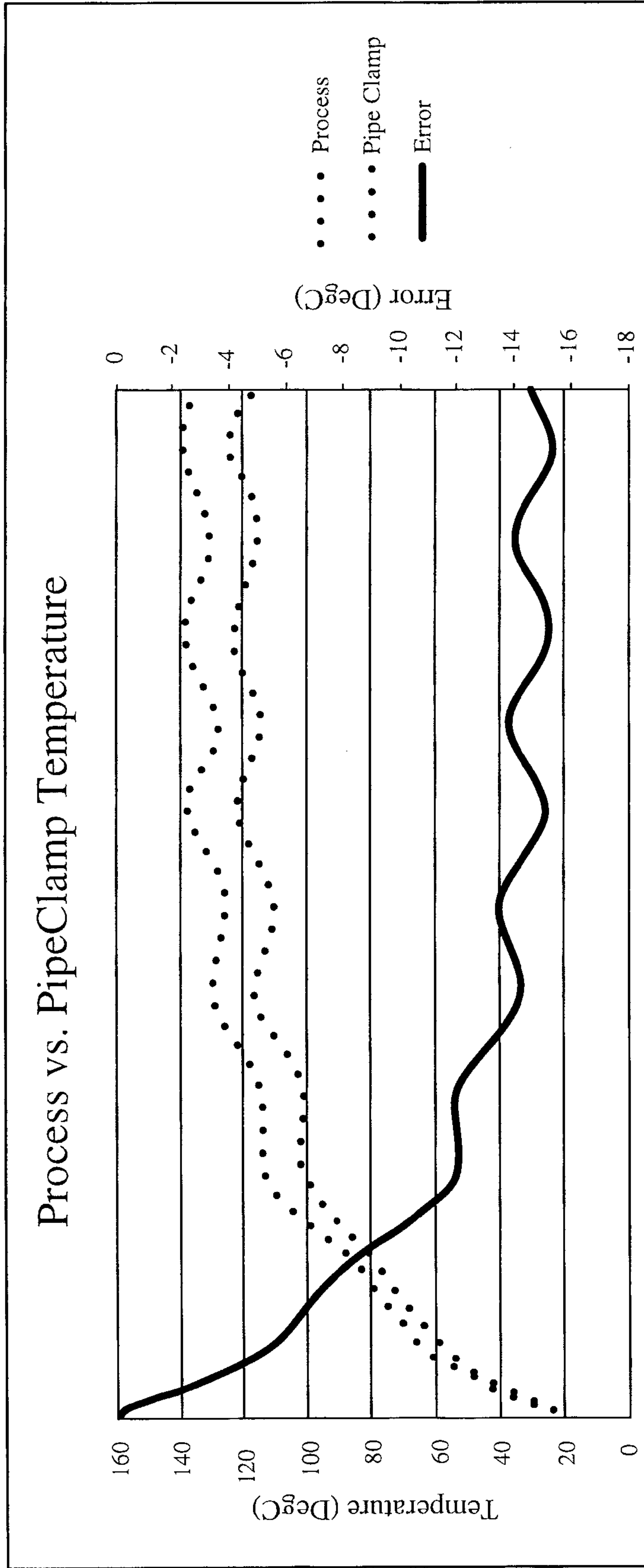


FIG. 1

2/6

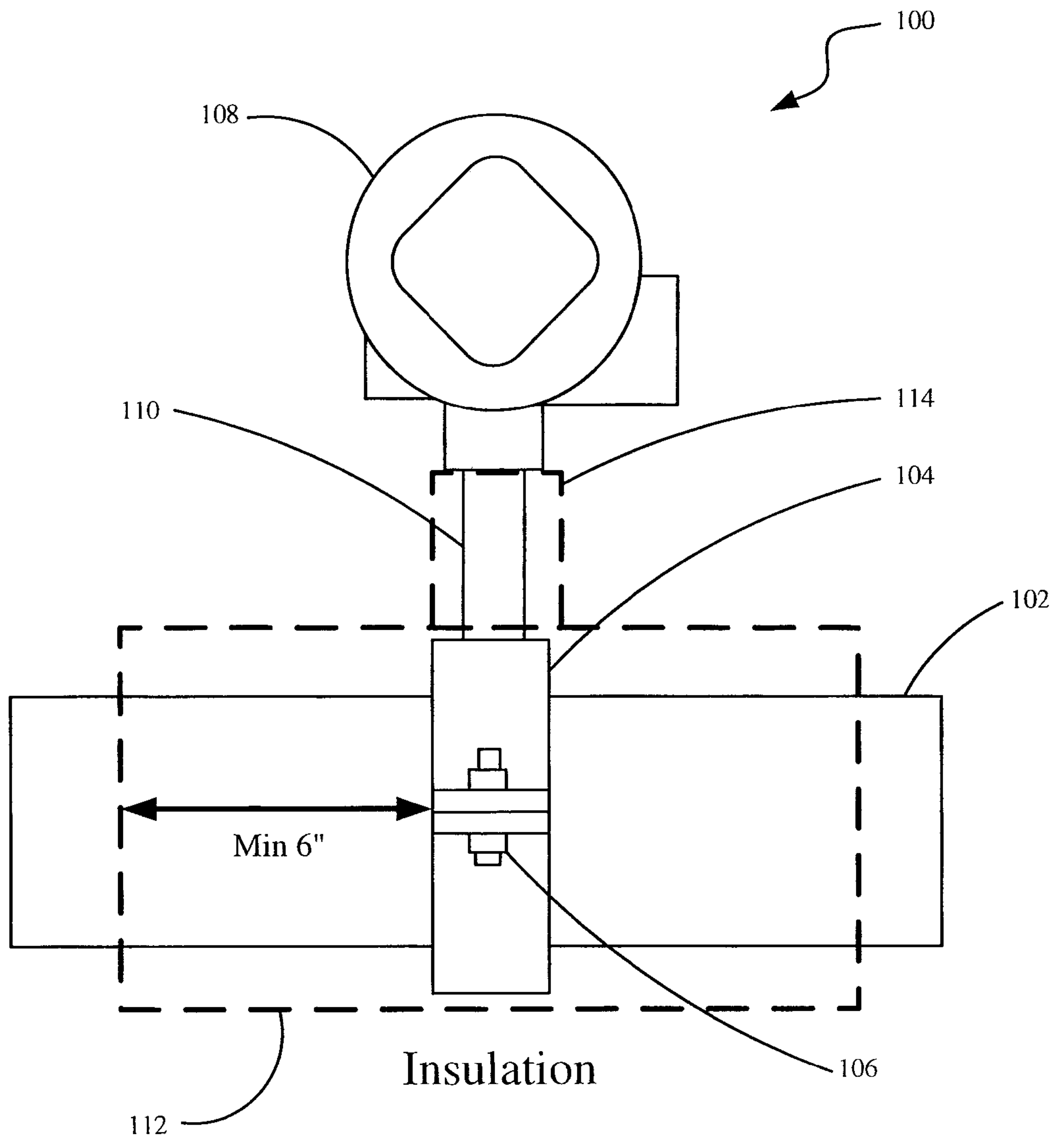


FIG. 2

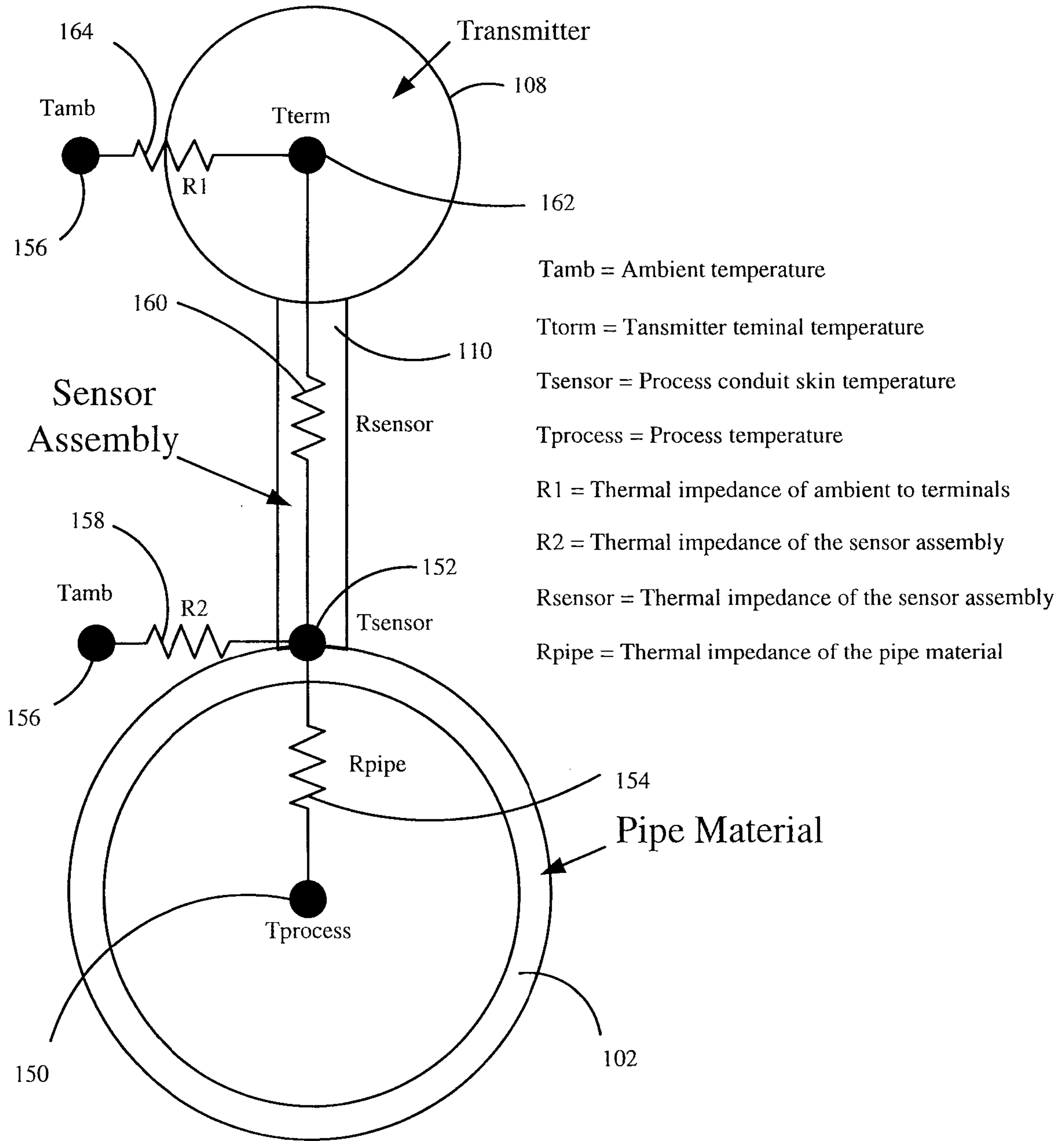


FIG. 3

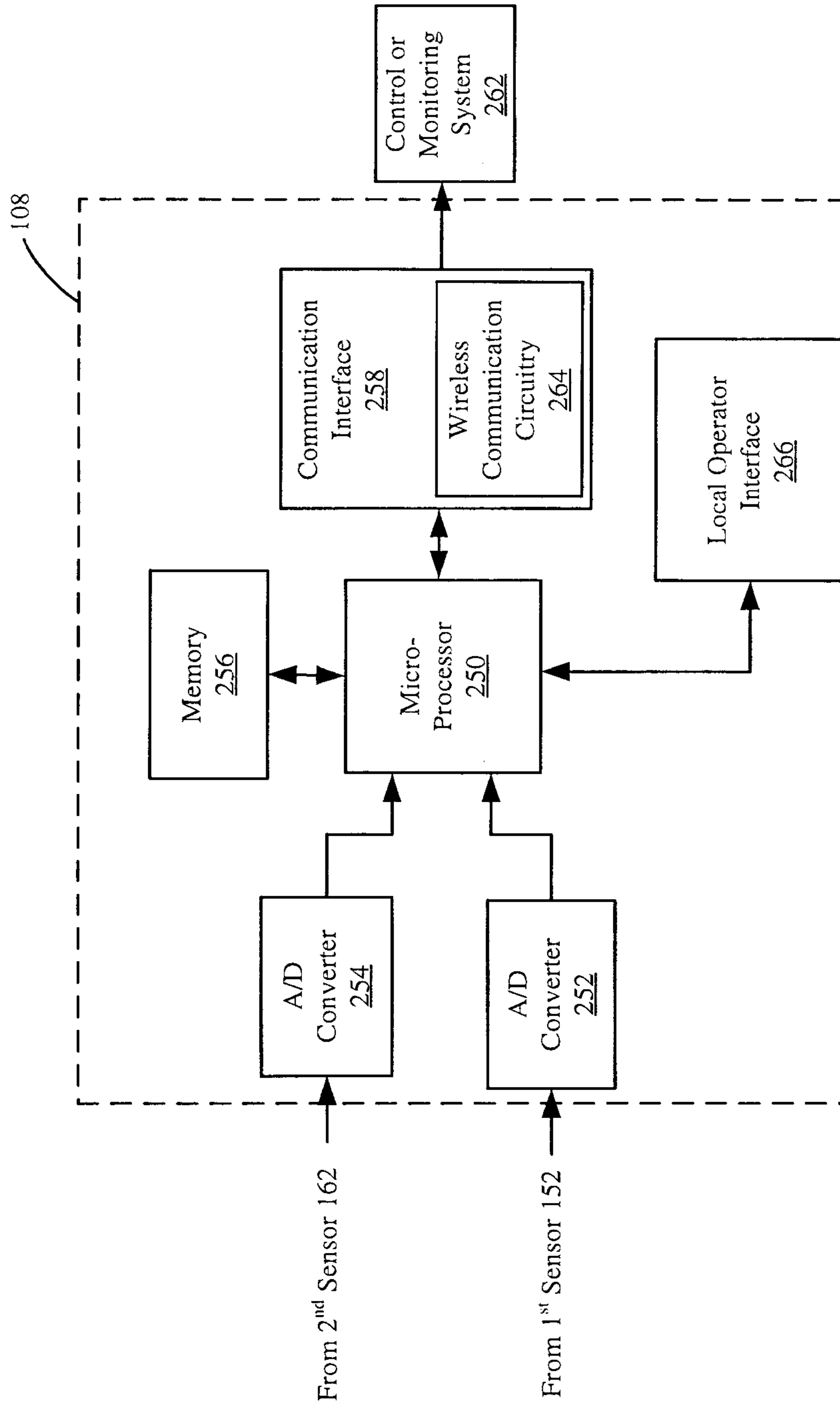


FIG. 4

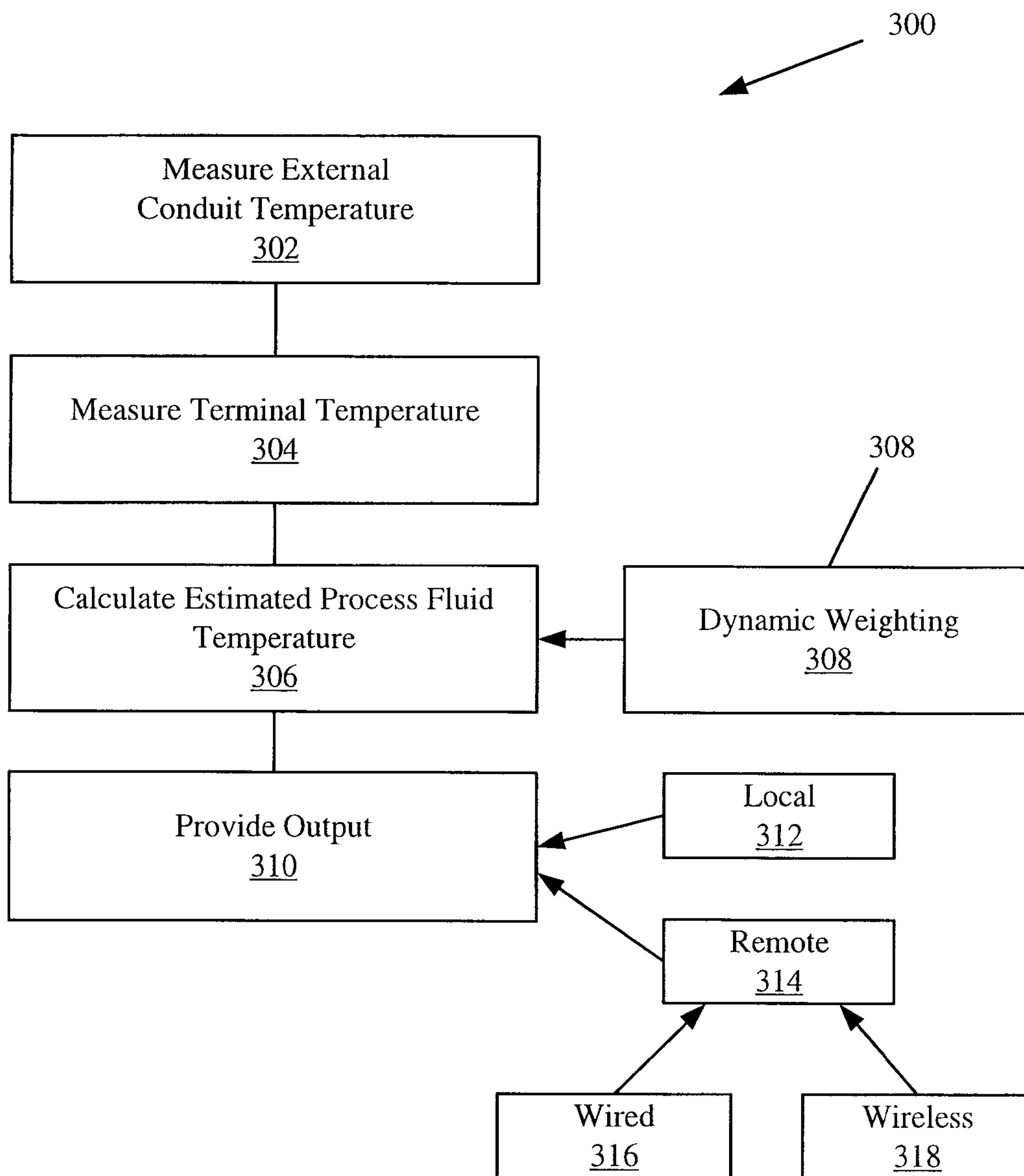


FIG. 5

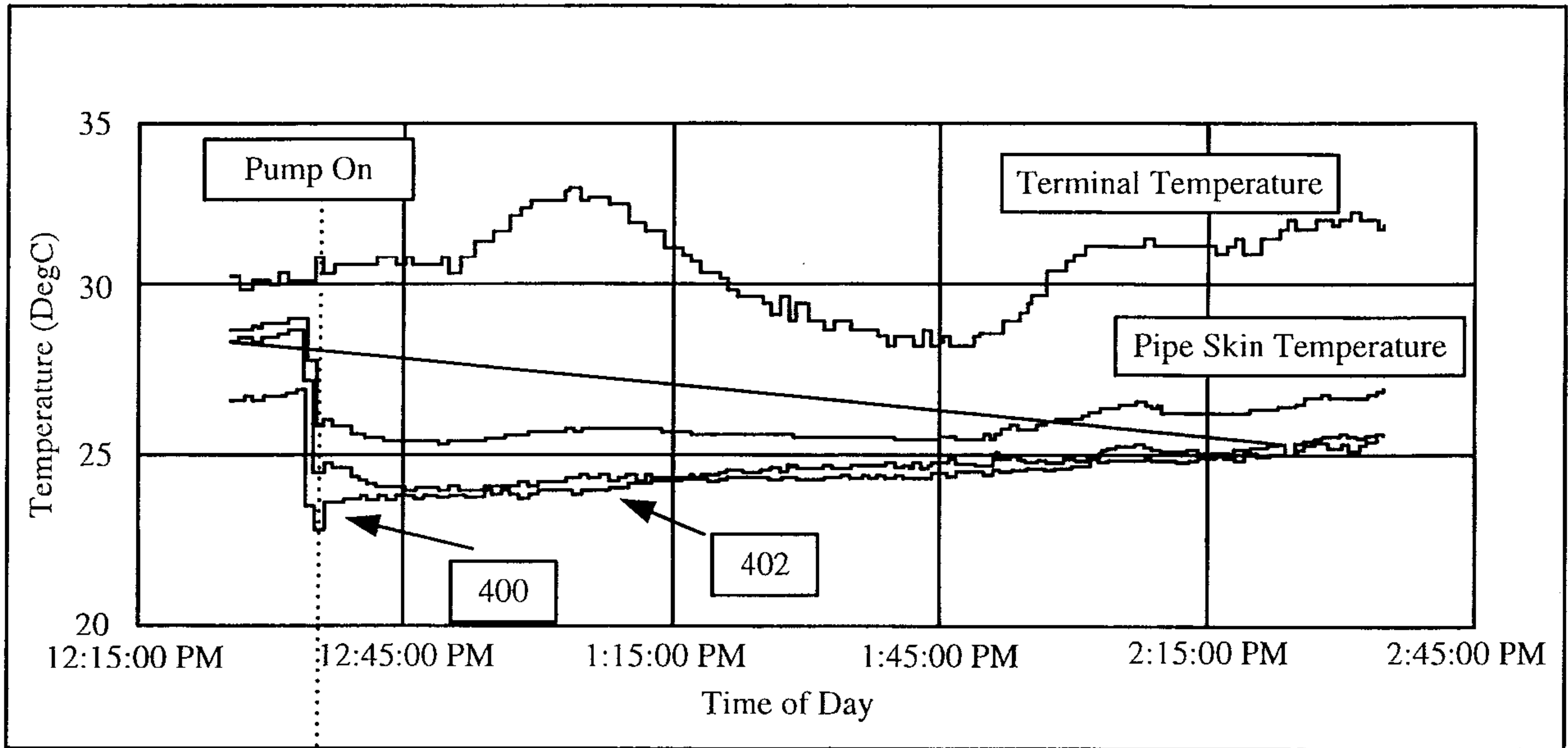


FIG. 6A

Compensation Error

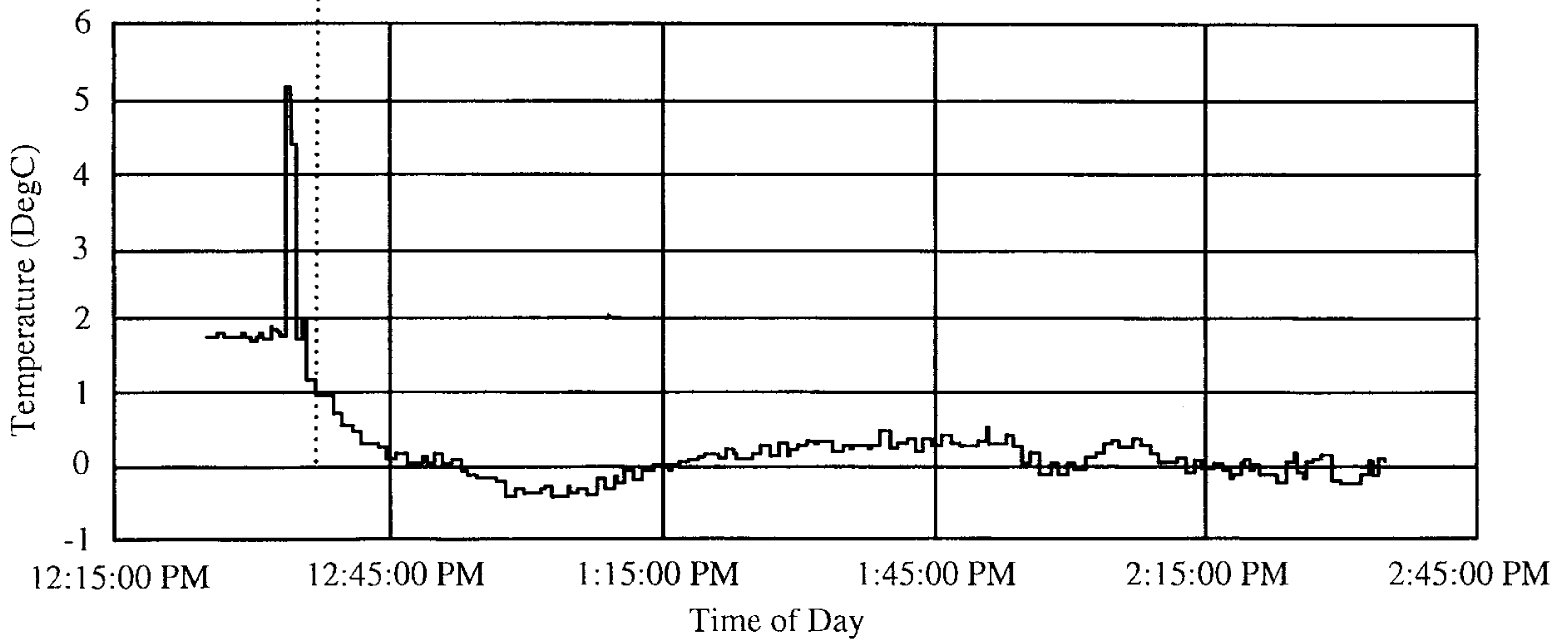


FIG. 6B