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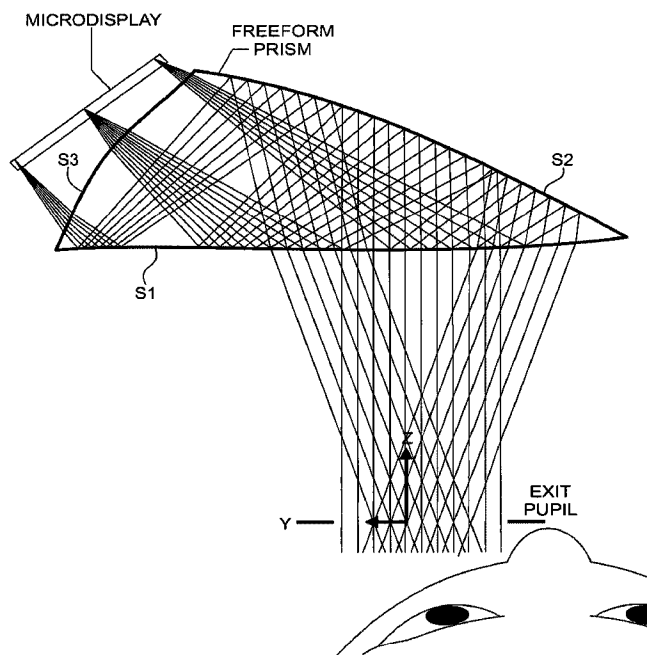
(72) Inventeurs/Inventors:
HUA, HONG, US;
KUHN, JASON W., US

(73) Propriétaire/Owner:
ARIZONA BOARD OF REGENTS ON BEHALF OF THE
UNIVERSITY OF ARIZONA, US

(74) Agent: BERESKIN & PARR LLP/S.E.N.C.R.L.,S.R.L.

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Near-to-eye systems and head-mounted displays and more particularly but not exclusively to an optimized freeform wedge-shaped prism design having free-form surfaces efficiently mathematically represented and configured to provide both high resolution and a large exit pupil heretofore unachieved.

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(71) Applicant: **ARIZONA BOARD OF REGENTS ON BEHALF OF THE UNIVERSITY OF ARIZONA** [US/US];
University of Arizona, Tech Transfer Arizona, 220 West
Sixth Street, 4th Floor, Tucson, AZ 85701 (US).

(72) Inventors: **HUA, Hong**; 1630 E. University Blvd, Tucson,
AZ 85721 (US). **KUHN, Jason, W.**; 1630 E. University
Blvd, Tucson, AZ 85721 (US).

(74) Agent: **HAUN, Niels** et al.; Dann Dorfman Herrell & Skillman, PC, 1601 Market Street, Suite 2400, Philadelphia, PA 19103 (US).

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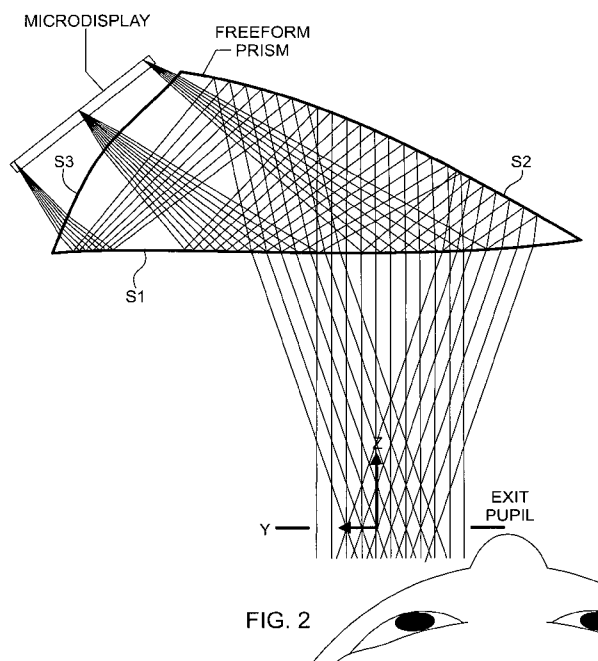


FIG. 2

(57) Abstract: Near-to-eye systems and head-mounted displays and more particularly but not exclusively to an optimized freeform wedge-shaped prism design having free-form surfaces efficiently mathematically represented and configured to provide both high resolution and a large exit pupil heretofore unachieved.

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HIGH-RESOLUTION FREEFORM EYEPiece DESIGN WITH A LARGE EXIT PUPIL

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FIELD OF THE INVENTION

The present invention relates to near-to-eye systems and head-mounted displays and more particularly but not exclusively to an optimized freeform wedge-shaped prism design having free-form surfaces efficiently mathematically represented and configured to provide both high resolution and a large exit pupil heretofore unachieved.

BACKGROUND

Head-mounted displays (HMD) have found myriads of applications from scientific visualization to engineering applications, from medical to defense industries, and from information display to entertainment. A key component to an HMD system is an eyepiece optics that collects the light emitted by a microdisplay and forms a magnified, distant image of the digital information presented through the microdisplay for the eye to view. On the other hand, designing a wide field of view (FOV), compact, low F-number and nonintrusive HMD with a large exit pupil has been a great challenge. The typical eyepiece structure using rotationally symmetric components has limitations in achieving low F-number, large eye relief, and wide FOV.

Many methods have been explored to achieve an HMD optical system which fulfils the above mentioned requirements. These methods include applying catadioptric techniques, introducing new elements such as aspherical surfaces, holographic and diffractive optical components, exploring new design principles such as using projection optics to replace an eyepiece or microscope type lens system in a conventional HMD design, and introducing tilt and decenter or even freeform surfaces. (Morishima et al., "The design of off-axial optical system consisting of aspherical mirrors without rotational symmetry," 20th Optical Symposium, Extended Abstracts, 21, pp.53-56, 1995. H. Hoshi, et al., "Off-axial HMD optical system consisting of aspherical surfaces without rotational symmetry," SPIE Vol. 2653, 234, 1996. S. Yamazaki, et al., "Thin wide-field-of-view HMD with freeform-surface prism and applications," Proc. SPIE, Vol. 3639, 453, 1999. Dewen Cheng et al, "Design of an

optical see-through head-mounted display with a low f-number and large field of view using a freeform prism,” *Applied Optics*, 2009. Dewen Cheng, et al. “Design of a wide-angle, lightweight head-mounted display using freeform optics tiling,” *Optics Letters*, 2011. H. Hua, X. Hu, and C. Gao, “A high-resolution optical see-through head-mounted display with eyetracking capability,” *Optics Express*, 2013.) Among the different methods mentioned above, freeform optical technology has demonstrated great promise in designing compact HMD systems. In particular, a wedge-shaped freeform prism takes advantage of total internal reflection (TIR), which helps minimize light loss and improve the brightness and contrast of the displayed images.

The concept of freeform HMD designs with a wedge-shaped prism was first presented by Morishima et al. in 1995, and the fabrication and evaluation method were explored by Inoguchi et al. (“Fabrication and evaluation of HMD optical system consisting of aspherical mirrors without rotation symmetry,” *Japan Optics '95, Extended Abstracts*, 20pB06, pp. 19-20, 1995). Following these pioneering efforts, many attempts have been made to design HMDs using freeform surfaces, particularly designs based on a wedge-shaped prism (U.S. Patent Nos. 5,699,194, 5,701,202, 5,706,136). For instance, Hoshi et al. presented a freeform prism design offering an FOV of 34° and a thickness of 15mm; Yamazaki et al. described a 51° optical see-through HMD (OST-HMD) design consisting of a freeform prism and an auxiliary lens attached to the prism; more recently Cheng et al demonstrated a 53° OST-HMD design with low F-number [US9,239,453 B2], and Hua et al presented the design of a high-resolution OST-HMD design integrated with eyetracking capability [Hua, Hu, and Gao, *Optics Express*, 21(25): 30993-30998, December 2013].

Figure 1 shows a schematic layout of a typical freeform prism eyepiece design consisting of three optical surfaces, labeled as S1, S2, and S3. The prism eyepiece serves as the near-to-eye viewing optics that magnifies the image displayed through a microdisplay. For the sake of convenience, the surface adjacent to the exit pupil was labeled as S1 in the refraction path and as S1' in the reflection path. The center of the exit pupil was set as the origin of the global coordinate system and the rest of the surfaces were specified with respect to this global reference. The inventors further adopted the convention of tracing the system backward, namely from the eye position to the microdisplay. The overall system was set to be symmetric about the YOZ plane, but not the XOZ plane. In Figure 1 the Z-axis is along the viewing direction, X-axis is parallel to the horizontal direction aligning with interpupillary direction, and the Y-axis is in the vertical direction aligning with the head orientation. A ray

emitted from a point on the microdisplay is first refracted by the surface S3 next to the microdisplay. After two consecutive reflections by the surfaces S1' and S2, the ray is transmitted through the surface S1 and reaches the exit pupil of the system. To enable optical see-through capability, an auxiliary lens may be cemented to the wedge-shaped prism-lens in order to minimize the ray shift and distortion introduced to the rays from a real-world scene when the auxiliary freeform lens is combined with the prism-lens.

Most of the existing wedge-prism-based eyepiece designs have several limitations. First of all, the exit pupil diameter (EPD) of most existing designs is typically from 4 to 8mm, which essentially results in a limited eyebox size. The eyebox defines a 3D volume in which the pupil of a viewer is placed to see the entire field of view of the display without losing imagery. A larger eyebox is preferred for HMD systems to facilitate ease of use and comfort.

Secondly, in most of the existing designs, the size of the microdisplays is relatively large, in the range of 0.8 to 1.3 inches, which affords a relatively large focal length or low optical power to achieve a typical 40-degree FOV. Even with an exit pupil of 8mm, the system F/# remains fairly high (greater than 3) and eases the optical design challenge. A large size microdisplay, however, offsets the advantage the compactness of using a freeform prism. In the more recent design by Cheng et al (AO 2009), smaller microdisplays, typically around 0.6", were adopted to achieve a 53-degree FOV, which requires a focal length of ~15mm. The substantially reduced focal length makes it very challenging to design a system with a large exit pupil and long eye clearance distance. As a result, the conventional design compromises the size of non-vignetted exit pupil diameter (about 6mm) by allowing a significant amount of vignetting for large field positions, which compromises the effective eyebox size to about 8mm at the designed eye clearance position.

Thirdly, the pixel size of the microdisplays used in most of the existing designs is typically at least 15 μ m or larger. As a result, relatively low optical power or long focal length is adequate for the eyepiece prism to achieve a moderate FOV. For instance, the pixel size of the microdisplay used in the design by Cheng et al is about 15 μ m, which helps to mitigate the challenge of designing a large FOV system. In the more recent designs by Hua et al (2013), microdisplays with pixel size of around 10 μ m, were adopted, which requires the freeform eyepiece to afford much higher optical resolution (e.g. 50 lps/mm for 10 μ m pixels) than designs with larger pixel sizes (e.g. 33 lps/mm for 15 μ m pixels). On the other hand, the microdisplays used in the design by Hua et al are about 0.8", which helps to mitigate the challenges of designing a high resolution system. In general, it is very challenging to design a

freeform prism eyepiece achieving low F-number and high optical resolution for a broad spectrum without adding additional elements for chromatic aberration correction.

Finally, the freeform prism typically is symmetric about the plane in which the surfaces are rotated and decentered and the optical path is folded. For instance, the prism schematic in

Figure 1 was set to be symmetric about the vertical YOZ plane. The optical surfaces are decentered along the vertical Y-axis and rotated about the horizontal X-axis so that the optical path is folded in the vertical YOZ plane to form a prism structure. With this type of

plane-symmetry structure, it is very challenging to achieve a wider field of view for the folding direction than the direction with symmetry. Therefore, most of the existing freeform

prism eyepiece designs, including the recent work by Cheng et al [AO 2009] and Hua et al [Optics Express 2013], choose to fold the optical path in the direction corresponding to the

direction of narrower FOV as shown in Figure 1, which makes it easier to achieve total internal reflection (TIR) in surface S1' and maintain a valid prism structure. As most display

applications typically prefer a landscape-type display, HMD systems typically align the wider

FOV direction horizontally and the narrower FOV direction vertically. As a result, most of the freeform prism-based HMDs typically mount the microdisplays above the eyebrow,

which leads to a front-heavy system and compromises the ergonomic design. Prism designs that fold the optical path along the wider FOV direction will allow mounting the microdisplays on the temple sides and mitigating the ergonomic challenge. In the prior art,

there are a few exceptions where the freeform prism designs were folded in the direction corresponding to the wider FOV. For instance, Hu and Hua presented the design of a high-

resolution freeform wedge prism which was folded in the wider FOV direction so that the prism was mounted horizontally [Hu and Hua, "High-resolution optical see-through multi-

focal plane head-mounted display using freeform wedge prism," Optics Express, May 2014.

Hu and Hua, "Design and tolerance of a freeform optical system for an optical see-through multi-focal plane display," Applied Optics, 2015.]. However, the microdisplay utilized in the

system has larger pixels (about 15 μm) and larger dimensions (about 0.7" diagonally) and the system has a relatively smaller exit pupil (about 6mm) than the present invention.

The existing body of work shows that it remains a great challenge to design a freeform eyepiece prism offering a wide field of view, high image resolution, large exit pupil for eye

placement, sufficient eye clearance, and elegant ergonomic design. Accordingly, it would be an advance in the field of head-mounted displays and near-to-eye systems to provide an eyepiece design which overcomes these limitations.

Other aspects and features of the present invention will become apparent to those ordinarily skilled in the art upon review of the following description of specific embodiments of the invention in conjunction with the accompanying figures.

SUMMARY OF THE DISCLOSURE

- 5 It is an object of the present invention to mitigate limitations within the prior art relating to free-form prism-lens optics design for near-to-eye and head-mounted display systems.
- In accordance with an embodiment of the invention there is provided a free-form prism-lens configured with a first free-form surface to receive light from a micro-display and transmit the received light into the body of the prism-lens; a second free-form surface configured to
- 10 receive the light transmitted into the body of the prism-lens from the first free-form surface and configured to reflect the received light at the second surface; and, a third free-form surface configured to receive the light reflected by the second free-form surface and to at least partially reflect the light back towards the second free-form surface and then out of the prism-lens, wherein the reflection at the second free-form surface and the at least partial
- 15 reflection at the third free-form surface occurs within a selected folding plane, and wherein the prism-lens has a field-of view in the folding plane greater than the field-of view in a plane perpendicular to the folding plane. The free-form prism-lens may have a centre-field effective F/# of less than 3.5 and an exit pupil diameter of at least 8mm. The prism-lens may optionally include an auxiliary lens disposed proximate to the third free-form surface such
- 20 that the auxiliary lens compensates for the shift and distortion of rays from a real-world scene by the second and third surfaces of the prism-lens.

BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the present invention will now be described, by way of example only, with reference to the attached Figures, wherein:

- 25 Figure 1 depicts a prior-art free-form prism-lens-based near-to-eye display in which the optical folding occurs along the shorter vertical dimension and the micro-display is located above the users eye proximate to the eyebrow, along with an auxiliary lens for corrected viewing of real-world scenes.
- Figure 2 depicts an embodiment of the invention of a free-form prism-lens absent any
- 30 auxiliary optical elements wherein the coordinate axes have been rotated such that the display

is located proximate to the user's temple, and the optical folding within the free-form prism-lens occurs in a selected plane along the wider horizontal field of view.

Figure 3 depicts a 3D CAD model of a prism-lens design according to an embodiment of the invention in perspective and plan views.

5 Figure 4 depicts the distortion grid of the prism-lens design according to the embodiment of the invention depicted in Figure 3.

Figure 5A depicts point-clouds of decreasing proximity to the centre-of-field shown in gradually from light to dark shades of gray, with red represented by the lightest shade and blue represented by the darkest shade, for the prism-lens according to the embodiment of the invention depicted in Figure 3.

10 Figure 5B depicts the modulation transfer function of the design for points shown in Figure 5A.

Figures 6A to 6E respectively depict the full-field plot of the polychromatic MTF values of the prism-lens according to an embodiment of the invention depicted in Figure 3 with a 3-mm exit pupil at the pupil positions of (0,0); (0, -2mm); (0, +2mm); (-2mm,0); and (2mm, 0) respectively.

15 Figures 7A to 7C respectively depict the MTF plots of the prism-lens according to an embodiment of the invention depicted in Figure 3 for three sampled wavelengths, 610nm, 560nm, and 475nm respectively, with a 3-mm centered pupil for the embodiment of the invention depicted in Figure 3.

Figure 8 depicts the full-field map of the image positions distorted by the prism-lens according to an embodiment of the invention depicted in Figure 3 corresponding to the three sampled wavelengths (610nm, 560nm, and 475nm) along with the paraxial image positions.

Other aspects and features of the present invention will become apparent to those ordinarily skilled in the art upon review of the following description of specific embodiments of the invention in conjunction with the accompanying figures.

25 DETAILED DESCRIPTION

The ensuing description provides representative embodiment(s) only, and is not intended to limit the scope, applicability or configuration of the disclosure. Rather, the ensuing description of the embodiment(s) will provide those skilled in the art with an enabling description for implementing an embodiment or embodiments of the invention, it being understood that various changes can be made in the function and arrangement of elements

without departing from the spirit and scope as set forth in the appended claims. Accordingly, an embodiment is an example or implementation of the inventions and not the sole implementation. Various appearances of “one embodiment,” “an embodiment” or “some embodiments” do not necessarily all refer to the same embodiments. Although various
5 features of the invention may be described in the context of a single embodiment, the features may also be provided separately or in any suitable combination. Conversely, although the invention may be described herein in the context of separate embodiments for clarity, the invention can also be implemented in a single embodiment or any combination of embodiments.

10 Reference in the specification to “one embodiment”, “an embodiment”, “some embodiments” or “other embodiments” means that a particular feature, structure, or characteristic described in connection with the embodiments is included in at least one embodiment, but not necessarily all embodiments, of the inventions. The phraseology and terminology employed herein is not to be construed as limiting but is for descriptive purpose only. It is to be
15 understood that where the claims or specification refer to “a” or “an” element, such reference is not to be construed as there being only one of that element. It is to be understood that where the specification states that a component feature, structure, or characteristic “may”, “might”, “can” or “could” be included, that particular component, feature, structure, or characteristic is not required to be included.

20 Reference to terms such as “left”, “right”, “top”, “bottom”, “front” and “back” are intended for use in respect to the orientation of the particular feature, structure, or element within the figures depicting embodiments of the invention. It would be evident that such directional terminology with respect to the actual use of a device has no specific meaning as the device can be employed in a multiplicity of orientations by the user or users. Reference to terms
25 “including”, “comprising”, “consisting” and grammatical variants thereof do not preclude the addition of one or more components, features, steps, integers or groups thereof and that the terms are not to be construed as specifying components, features, steps or integers. Likewise the phrase “consisting essentially of”, and grammatical variants thereof, when used herein is not to be construed as excluding additional components, steps, features integers or groups
30 thereof but rather that the additional features, integers, steps, components or groups thereof do not materially alter the basic and novel characteristics of the claimed composition, device or method. If the specification or claims refer to “an additional” element, that does not preclude there being more than one of the additional element.

In order to address and overcome the challenges described above in respect of prior art prism eyepiece designs the inventors have established a single-element freeform prism eyepiece design methodology. Within embodiments of the invention presented within this specification a single-element freeform prism eyepiece design is presented that not only achieves a high optical resolution of less than $10\mu\text{m}$, but also offers a diagonal FOV of about 40° , a large exit pupil of 12mm with low vignetting, and a large eye clearance distance greater than 21mm. The microdisplay utilized in our prototype is a 0.5" organic light emitting display (OLED) with a $10\mu\text{m}$ color pixel and pixel resolution of 1024x768. The eyepiece design itself, however, is able to support OLED panels of different dimensions or other type of microdisplays such as liquid crystal displays that have a pixel size greater than $8\mu\text{m}$.

Figures 2 and 3 show the 2D optical layout and 3D CAD model, respectively, of a free-form prism-lens according to an embodiment of the invention absent any auxiliary optical elements. A ray emitted from a point on the microdisplay is first refracted by the surface S3 next to the microdisplay. After two consecutive reflections by the surfaces S1' and S2, the ray is transmitted through the surface S1 and reaches the exit pupil of the system. The first surface (i.e., S1 and S1') of the prism is required to satisfy the condition of total internal reflection for rays reflected by this surface S1'. The rear surface S2 of the prism may be coated with a reflective coating for building an immersive HMD system which blocks the view of the real world scene. Alternatively, the surface S2 may be uncoated or coated with a partially reflective beamsplitting coating if optical see-through capability is desired using the auxiliary lens.

It should be noted that in the design disclosed according to an embodiment of the invention is presented with the global reference coordinate system centered with respect to the exit pupil, like most of the existing freeform prism designs. However, the reference axes are set differently from the existing designs presented within the prior art. Here the Z-axis is along the viewing direction, but the Y-axis is parallel to the horizontal direction aligning with interpupillary direction, and the X-axis is in the vertical direction aligning with the head orientation. In other words, the reference coordinate system is rotated 90-degrees around the Z-axis. As a result, the overall prism system is symmetric about the horizontal (YOZ) plane, rather than the typical left-right symmetry about the vertical plane. The optical surfaces (S1, S2, and S3) are decentered along the horizontal Y-axis and rotated about the vertical X-axis. As a result, the optical path is folded in a selected plane, i.e., the horizontal YOZ plane, corresponding to the direction of wider field of view, to form a prism structure. This

arrangement allows the microdisplay to be mounted on the temple side of the user's head, resulting in a much more balanced and ergonomic system packaging concept than a typical vertical-folding design with the microdisplay located above the eyebrow. It would be further evident that in the embodiments of the invention described within this specification that they differ from a typical vertical-folding design in which the FOV in the folding direction is narrower than the non-folding direction. Rather, embodiments of the invention has a FOV in the folding direction is much wider than the non-folding direction, *e.g.*, perpendicular to the selected plane, which makes a high-performance design very challenging.

The overall specifications of an exemplary optical system within which free-form prism-lenses according to embodiments of the invention may be exploited is summarized in Table 1. The inventor's goal is to achieve a very compact, lightweight, and wide FOV design using a wedge-shaped freeform prism with a large exit pupil and high optical resolution. Another requirement is to mount the microdisplays on the temple sides to avoid front-heaviness and improve ergonomic balance, which requires folding the optical path within the prism along the wider FOV direction. A small size microdisplay with high resolution was thus preferred. Based on the size, resolution, availability and cost, a 0.5-inch organic light emitting display (OLED) was selected, with a resolution of 1024×768 pixels and an about 10μm pixel size.

The inventors further targeted an HMD system with a diagonal full FOV of about 40°, which corresponds to a focal length around 18 mm. This combination offers a reasonable balance between FOV and angular resolution (1.8 arc minutes per pixel). In the design of visual instruments, especially HMDs, a large exit pupil is typically preferred to account for the swiveling of the eyes in their sockets without causing vignetting or loss of image. A large pupil offers better tolerance of the interpupillary distances (IPD) among different users without the need to mechanically adjust the eyepiece optics, and can allow moderate electronic IPD adjustment by laterally displacing the displayed pixels. A large pupil, however, often not only compromises the compactness and weight of the optical system, but also imposes limitations on the FOV due to the dramatically increased challenge of designing low F/# systems. Taking into account these factors, the inventors set the exit pupil diameter to be 12mm with no more than 40% vignetting at the maximum field positions, which leads to a system with an F/# of about 1.5 for the center fields. In designing HMD systems, a large eye clearance is desired to accommodate users wearing eyeglasses, but it affects the compactness of the viewing optics. A minimum of a 20mm eye clearance was set to accommodate users wearing low-eyeglasses.

Among the aberrations of an optical system, distortion causes the warping of the displayed image without reducing image sharpness, which allows computational or electronic correction. In designing conventional HMDs it is common to optimize the system to minimize the optical aberrations that reduce image quality which cannot be compensated electronically or computationally. In a freeform prism eyepiece, however, the distortion can be very large and irregular if it is left without any constraints. The inventors thus set a distortion limit of 10% at the maximum field angle and assume that the residual distortion is corrected using computational methods. In terms of other types of aberrations, the modulation transfer function (MTF) was selected to evaluate the overall image sharpness and was set to be no less than 10% across the entire visual field at a spatial frequency of 50lp/mm which corresponds to the Nyquist sampling frequency of the microdisplay.

Parameter	Specification
Microdisplay	
Size	0.5 inches (12.7mm) diagonally
Active display area	10.14mm×7.6mm
Resolution	1024×768 pixels
Pixel size	10μm
Eyepiece	
Type	folded freeform prism
Effective focal length	~18mm
Exit pupil diameter	12mm
Eye Clearance	>20mm
Eye relief	>23 mm
F/#	1.5
Number of freeform surfaces	3
Wavelength	650-465 nm
Field of view	>30° (H)×23°(V)
Vignetting	<40% for top and bottom fields
Distortion	<10% at the maximum field
Image quality	MTF>10% at 50 lp/mm
Optical path folding direction	Horizontal plane

Table 1. Specifications of one embodiment of the FFS Prism-lens HMD System

It is important to select a suitable method for a freeform surface representation. Different representation methods not only have different impacts on the ray tracing speed and the convergence of optimization, but also offer different degrees of design freedom. A suitable representation method should 1) provide adequate degrees of freedom; 2) require a reasonable amount of ray tracing time; 3) offer reliable convergence in the optimization process; and 4) be orthogonal.

Many types of orthogonal or non-orthogonal polynomial equations can be utilized to describe a freeform surface. For instance, a freeform surface could be represented by Equations (1A) and (1B).

$$z = \frac{c_x x^2 + c_y y^2}{1 + \sqrt{(1 - (1 + k)c_x x^2 - (1 + k)c_y y^2)}} + \sum_{j=1}^{37} C_j x^{2n} y^n \quad (1A)$$

$$2m + n \leq 10; \quad m = 0, 1, 2, \dots, 10; \quad n = 0, 1, 2, \dots, 10 \quad (1B)$$

where z is the sag along the local z -axis, x and y are the coordinates in the local coordinate system, k is the conic constant, c_x is radius of curvature of surface in sagittal direction, c_y is radius of curvature of surface in tangential direction, and C_j is the coefficient for $x^{2m}y^n$.

As an embodiment example, the inventors chose to use a user-defined surface representation, known as Yabe surfaces (A. Yabe, "Representation of freeform surface suitable for optimization," Applied Optics, 2012), after taking into account these factors listed above. A freeform surface shape symmetric to the X -axis is represented by an axially asymmetric quadratic and a set of orthogonal polynomials as give by Equation (2).

$$z(x, y) = \frac{c_{xx}x^2 + 2c_{xy}xy + c_{yy}y^2}{1 + \sqrt{1 - \gamma(c_{xx}x^2 + 2c_{xy}xy + c_{yy}y^2)}} + \sum_{n=0}^N \sum_{k=0}^n b_n^{n-2k} W_n^{n-2k}(x/r_0, y/r_0) \quad (2)$$

where z is the sag along the local z -axis, x and y are the coordinates in the local coordinate system, c_{xx} , c_{yy} , and c_{xy} are the curvature tensor at the origin, γ is a conic-like constant, and r_0 is the radius of the surface. The orthogonal polynomials on the unit circle are expressed by Equations (3) and (4) where $u = \rho \sin \theta$ and $v = \rho \cos \theta$.

$$W_n^m(u, v) = Q_n^m(\rho) \cos(m\theta) \quad (3)$$

$$W_n^{-m}(u, v) = Q_n^m(\rho) \sin(m\theta) \quad (4)$$

With this orthogonal surface representation, the paraxial properties, high-order surface shapes, and surface tilt are clearly separated. Most of the commercially available optical design software tools, such as CODE V® (Optical Research Associates, Pasadena, CA), provide the ability to model freeform surfaces in user-defined methods. Though the ray tracing speed of user-defined representations typically is much slower than the standard methods available in the software packages, the orthogonal surface representation could yield more efficient and compact surface representation than the more commonly used xy-polynomials and result in faster convergence during design optimization.

As an embodiment example, Tables 2 through 5 provide surface data for the design of the free-form prism-lens according to the embodiment of the invention depicted within Figure 2. Table 2 defines the surface references of each optical surfaces, S1 through S3 as well as the microdisplay in the global coordinate system. Tables 3 through 5 provide the optimized coefficients defining the optical surfaces S1 through S3.

	Origin of surface reference			Orientation of the surface
	X (mm)	Y (mm)	Z (mm)	Rotation about X-axis θ (°)
Surface S1	0	-0.2	21.3	3.1
Surface S2	0	3.3	31.8	-24.1
Surface S3	0	22.5	29.6	42.6
Microdisplay	0	-0.8	4.01	-5.6

Table 2. Definition of the local surface references in the global coordinate system.

Parameter	Value
Y Radius	91.762447
C1: Curvature tensor Cxx	0.0036021
C2: Cxy	0
C3: Gamma	-0.045698
C4: normalization radius	40
C5: highest radial order	10
C6: Q+3 -3	-3.8251964
C7: Q+3 -1	-7.8131066

C8: Q. +3. +1	0
C9: Q. +3. +3	0
C10: Q. +4. -4	0
C11: Q. +4. -2	0
C12: Q. +4. +0	-5.22786
C13: Q. +4. +2	-1.68526
C14: Q. +4. +4	0.185831

Table 3: Surface S1 (Yabe-Polynomial Freeform)

Parameter	Value
Y Radius	-105.41783
C1: Curvature tensor Cxx	-0.0172469
C2: Cxy	0
C3: Gamma	0.106071
C4: normalization radius	30
C5: highest radial order	10
C6: Q+3 -3	-0.7242956
C7: Q+3 -1	-3.7856926
C8: Q. +3. +1	0
C9: Q. +3. +3	0
C10: Q. +4. -4	0
C11: Q. +4. -2	0
C12: Q. +4. +0	2.56310988624996
C13: Q. +4. +2	-0.2917081
C14: Q. +4. +4	-0.0822885

Table 4: Surface-S2 (Yabe-Polynomial Freeform)

Parameter	Value
Y Radius	-29.999992
C1: Curvature tensor Cxx	-0.1751531
C2: Cxy	0
C3: Gamma	0.4759008
C4: normalization radius	20
C5: highest radial order	8
C6: Q+3 -3	-4.6906243
C7: Q+3 -1	-4.1547693
C8: Q. +3. +1	0
C9: Q. +3. +3	0
C10: Q. +4. -4	0
C11: Q. +4. -2	0
C12: Q. +4. +0	-2.6724760
C13: Q. +4. +2	6.31904234
C14: Q. +4. +4	3.32686085

Table 5: Surface-3 (Yabe-Polynomial Freeform):

During the design process, three representative wavelengths, 475nm, 560nm, and 610nm were selected in order to correspond with the peak emission spectra of the blue, green and red emitters within the selected microdisplay. The optical performance of the designed system was assessed at representative field angles for these three design wavelengths. Referring to Figures 4 through 6E respectively there are depicted the optical performance results for the free-form prism-lens according to the embodiment of the invention depicted within Figure 2. The distortion shown in Figure 4 implies the system distortion is well controlled, being less than 5% at the edge of the field of view. The polychromatic MTF curves for 25-sampled fields are shown in Figure 5, which were evaluated for a centered 3-mm pupil. The spatial frequency of 50 cycles/mm corresponds to the threshold spatial frequency of the microdisplay with a 10 μ m pixel size. The system achieved nearly 20% MTF value for the maximum field angle at the spatial frequency of 50 cycles/mm and an average MTF value of about 50% for the center 60% of the field of view. The average MTF is greater than 50% across the entire field of view at the frequency of 33 cycles/mm corresponding to a microdisplay pixel of 15 μ m. In other words, the optical resolution of this disclosed prism design is much higher

than the existing prism designs. Figures 6A to 6E respectively depict the full-field plot of the MTF distribution across the entire display field of view for the frequencies of 50 cycles/mm and 30 cycles/mm for a 3-mm pupil placed at five locations, namely centered (0,0), (0, -2), (0,2) (-2,0) and (2,0), respectively.

5 As a design constraint applied to the design of the free-form prism-lens according to an embodiment of the invention depicted in Figure 2 was that the prism design utilizes a single type of optical material, for instance Poly Methyl MethAcrylate (PMMA) or a Cyclo Olefin Polymer (COP), the full correction of chromatic aberrations due to optical dispersion is not feasible. This is often a limiting factor for designing a freeform prism with high optical
10 resolution for a broad optical spectrum. The embodiment of the invention presented within Figure 2 was designed for use in conjunction with an organic light emitting display (OLED) which has a larger color gamut than some of the other common commercial microdisplay technologies. Accordingly, the optical performance needs to be balanced for a broad visible spectrum.

15 In order to achieve high optical resolution, the inventors analysed the system response and adjusted the design by strategically adjusting the weights on three sampled wavelengths (475nm, 560nm, and 610nm) such that the performance of the optical system was corrected for each of the individual wavelengths whilst leaving chromatic aberration under-corrected. As a result, the image formed by each individual wavelength has achieved very high
20 resolution, while the display position of any given image point can be separated from those of other wavelengths originating from the same pixel position on the micro-display. Figures 7A to 7C respectively depict the MTF plots for these three sampled wavelengths, 610nm, 560nm, and 475nm, respectively, for a 3-mm centered pupil. These MTF plots demonstrate that the system forms superior image for each individual color image.

25 Such spatial displacements among different color elements, on the other hand, can be digitally corrected by applying a pre-warping operation to each individual color channel. Figure 8 plots the full-field map of the image positions corresponding to the three sampled wavelengths, 610nm, 560nm, and 475nm, respectively, along with the paraxial image positions. This full-field map provides data not only for image distortion correction, but also
30 to correct spatial displacements among different color elements for electronic pre-compensation of chromatic aberration before display.

The foregoing disclosure of the exemplary embodiments of the present invention has been presented for purposes of illustration and description. It is not intended to be exhaustive or to

limit the invention to the precise forms disclosed. Many variations and modifications of the embodiments described herein will be apparent to one of ordinary skill in the art in light of the above disclosure. The scope of the invention is to be defined only by the claims appended hereto, and by their equivalents.

- 5 Further, in describing representative embodiments of the present invention, the specification may have presented the method and/or process of the present invention as a particular sequence of steps. However, to the extent that the method or process does not rely on the particular order of steps set forth herein, the method or process should not be limited to the particular sequence of steps described. As one of ordinary skill in the art would appreciate,
- 10 other sequences of steps may be possible. Therefore, the particular order of the steps set forth in the specification should not be construed as limitations on the claims. In addition, the claims directed to the method and/or process of the present invention should not be limited to the performance of their steps in the order written, and one skilled in the art can readily appreciate that the sequences may be varied and still remain within the spirit and scope of the
- 15 present invention.

What is claimed is:

1. A free-form prism-lens constructed of a material with refractive index greater than 1 for use in a near-to-eye display system comprising:

a. a first free-form surface configured to receive light from a micro-display and transmit the received light into the body of the prism-lens;

b. a second free-form surface configured to receive the light transmitted into the body of the prism-lens from the first free-form surface and configured to reflect the received light at the second surface; and

c. a third free-form surface configured to receive the light reflected by the second free-form surface and to at least partially reflect the light back towards the second free-form surface and then out of the prism-lens,

wherein the reflection at the second free-form surface and the at least partial reflection at the third free-form surface occurs within a selected folding plane, and wherein the prism-lens has a field-of view in the folding plane greater than the field-of view in a plane perpendicular to the folding plane, and wherein the spatial distortion at maximum field angle is less than 10%.

2. The free-form prism-lens of claim 1, wherein said prism-lens has a center-field effective F/# of less than 3.5 and an exit pupil diameter of at least 8 mm.

3. The free-form prism-lens of claim 1, wherein at least one of the three free-form surfaces of the free-form prism-lens is described by an axially asymmetric quadratic and a set of orthogonal polynomials:

$$z(x, y) = \frac{c_{xx}x^2 + 2c_{xy}xy + c_{yy}y^2}{1 + \sqrt{1 - \gamma(c_{xx}x^2 + 2c_{xy}xy + c_{yy}y^2)}} + \sum_{n=0}^N \sum_{k=0}^n b_n^{n-2k} W_n^{n-2k}(x/r_0, y/r_0)$$

where z is a sag along the local z-axis, x and y are the coordinates in the local coordinate system, c_{xx} , c_{yy} , and c_{xy} are the curvature tensor at the origin, γ is a conic-like

constant, r_0 is the radius of the surface, and the orthogonal polynomials on a unit circle are expressed as:

$$W_n^m(u, v) = Q_n^m(\rho) \cos(m\theta) \quad \text{and} \quad W_n^{-m}(u, v) = Q_n^m(\rho) \sin(m\theta)$$

Where $u = \rho \sin \theta$ $v = \rho \cos \theta$.

4. The free-form prism-lens of claim 1, wherein the third free-form surface is coated with a reflective coating to reflect all light from the second free-form surface back towards the second free-form surface and then to exit the free-form prism-lens.

5. The free-form prism-lens of claim 1, wherein the third free-form surface, in addition to reflecting light from the second free-form surface back towards the second free-form surface and then to exit the free-form prism-lens also admits light from outside the free-form prism from real-world scenes to also be transmitted towards the second free-form surface and then to exit the free-form prism-lens.

6. The free-form prism-lens of claim 1, comprising an auxiliary lens disposed proximate to the third free-form surface, the auxiliary lens configured to minimize a shift and distortion of rays from a real-world scene by the second and third free-form surfaces.

7. The free-form prism-lens of claim 6 wherein the auxiliary lens has a surface with the same shape as the third free-form surface of the prism-lens and is disposed in optical contact with the third free-form surface of the prism-lens.

8. The free-form prism-lens of claim 1, wherein an eye-clearance is at least 18 mm.

9. The free-form prism-lens of claim 1, wherein the field-of view of the prism-lens in the folding plane is at least 28 degrees.

10. The free-form prism-lens of claim 1, wherein the field-of view of the prism-lens in the plane perpendicular to the folding plane is at least 21 degrees.
11. The free-form prism-lens of claim 1, wherein an effective focal length is less than 20 mm.
12. The free-form prism-lens of claim 1, wherein a vignetting at the maximum field positions is less than 40%.
13. The free-form prism-lens of claim 1, wherein the micro-display has a pixel pitch of 7.5 microns or larger.
14. The free-form prism-lens of claim 1, wherein a modulation transfer function across the entire field of view is greater than 30% at the spatial frequency of 33 line-pairs/mm and greater than 10% at the spatial frequency of 50 line-pairs/mm.
15. The free-form in prism lens of claim 1, wherein the prism-lens is formed through an injection-moulding process.
16. The free-form prism-lens of claim 1, wherein the prism-lens is composed of either poly methyl methacrylate or a cyclic olefin polymer.
17. The free-form prism-lens of claim 1, wherein a reflection of light by the second free-form surface towards the third free-form surface is achieved without application of any reflective coating to the second free-form surface.
18. The free-form prism-lens of claim 1, wherein the second free-form surface is configured to both perform reflection of light incident from the first free-form surface as well as perform refraction of light incident from the third free-form surface.

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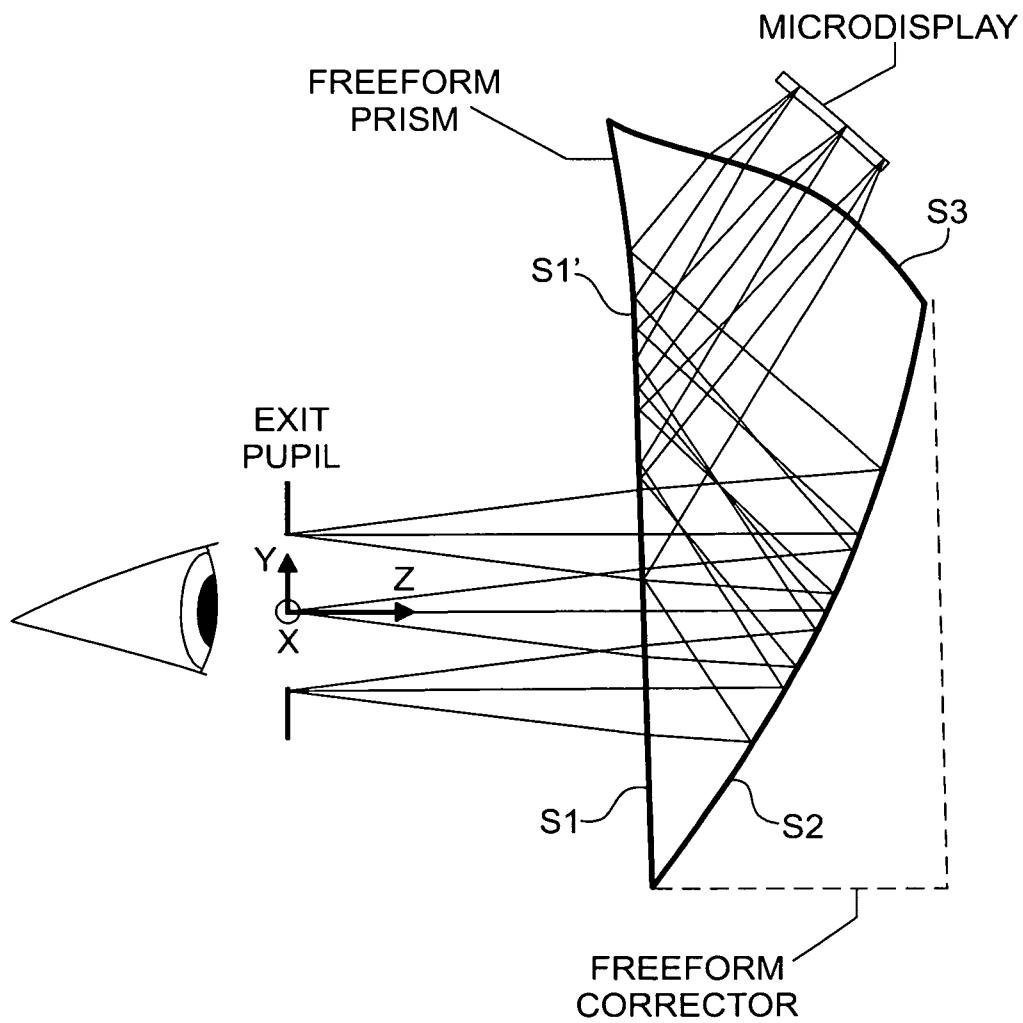
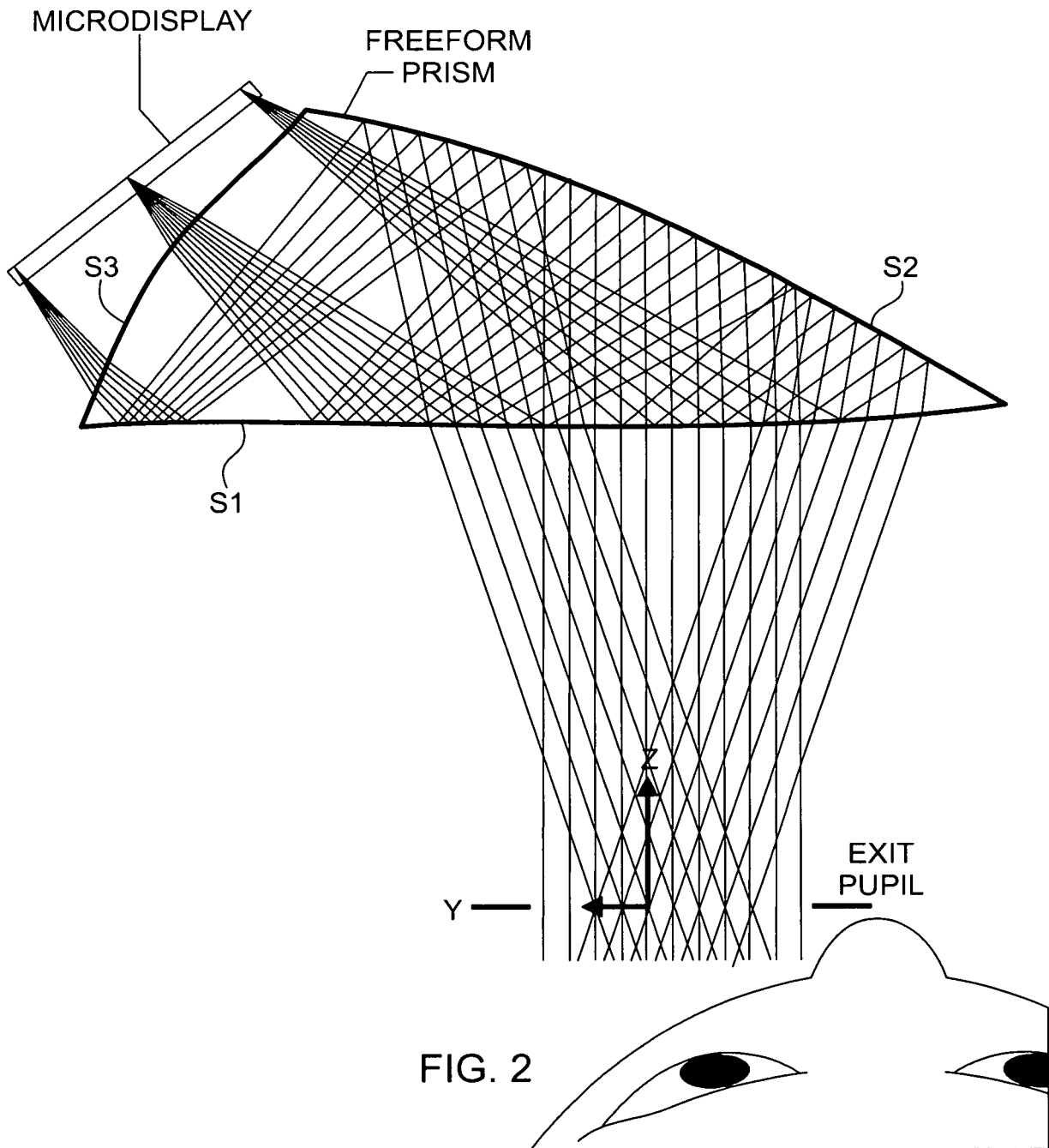


FIG. 1

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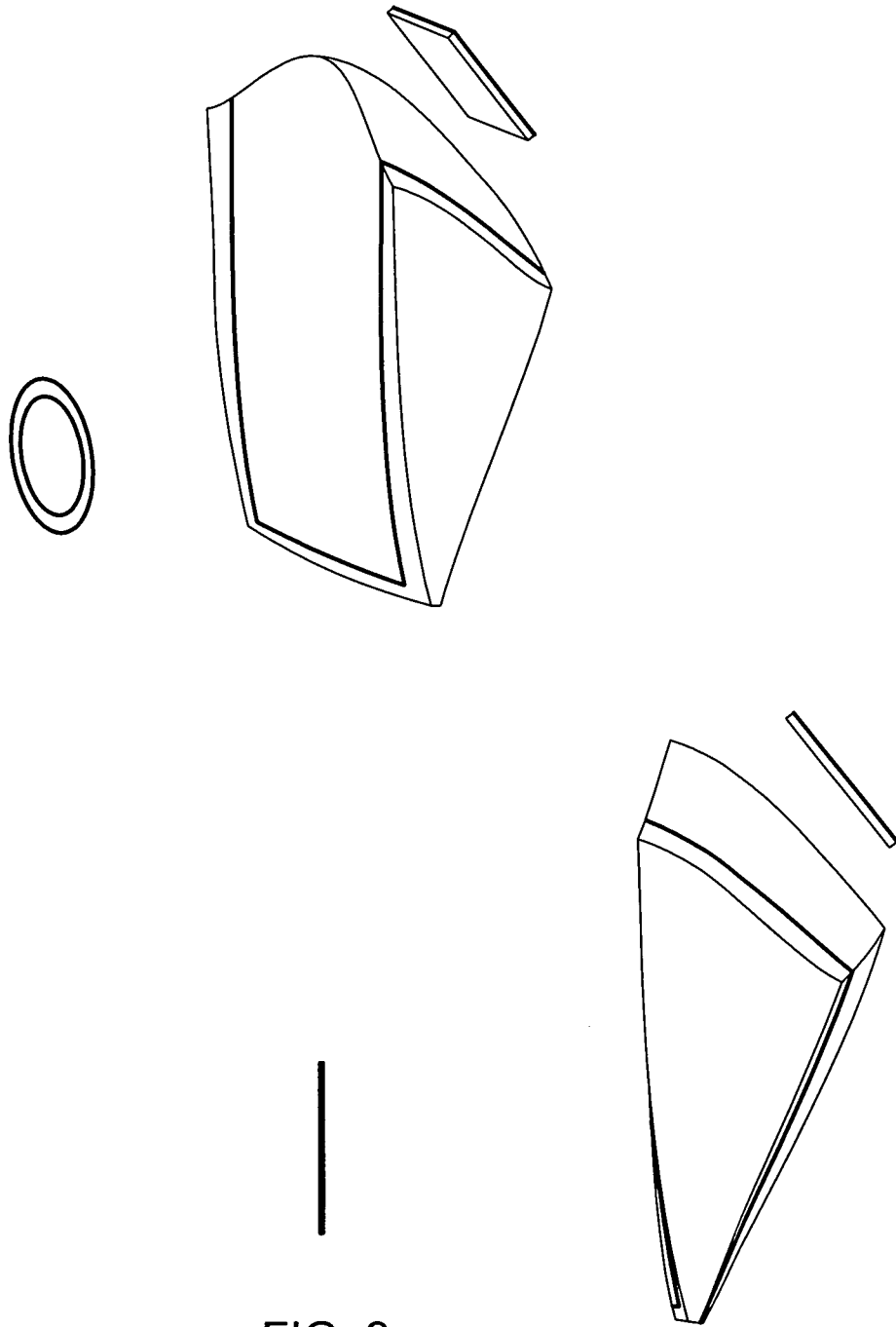


FIG. 3

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DISTORTION GRID (Z1) - eS FFS EYEPiece 30x23 EPD9

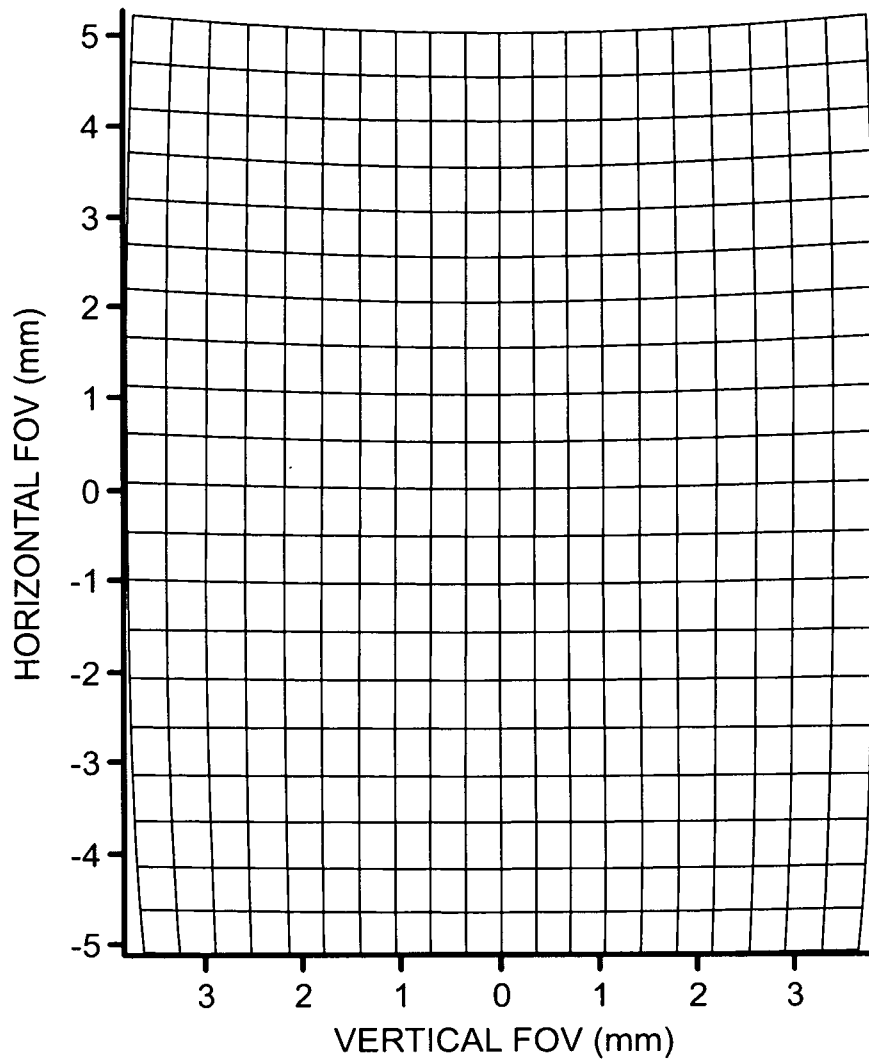


FIG. 4

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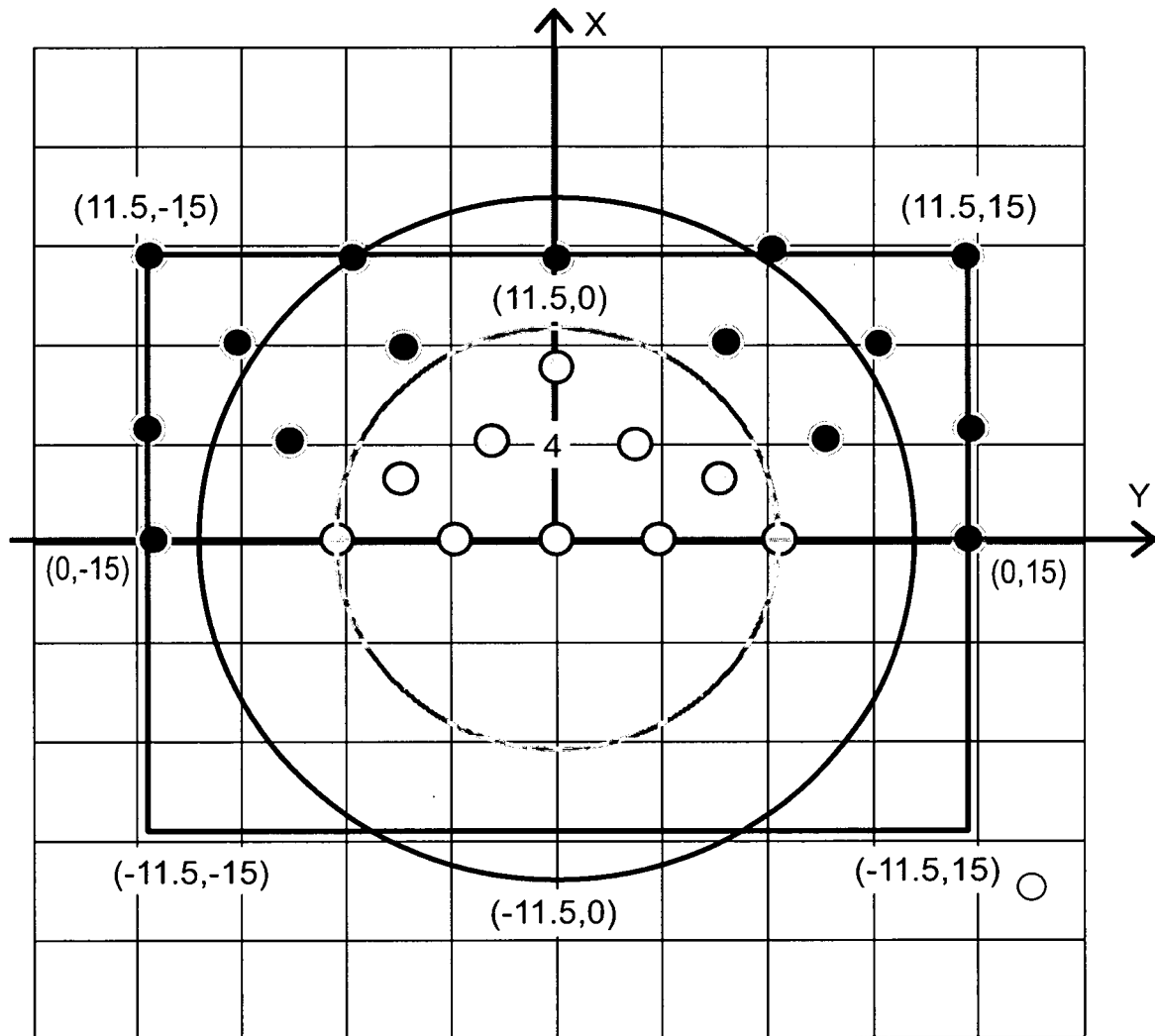


FIG. 5A

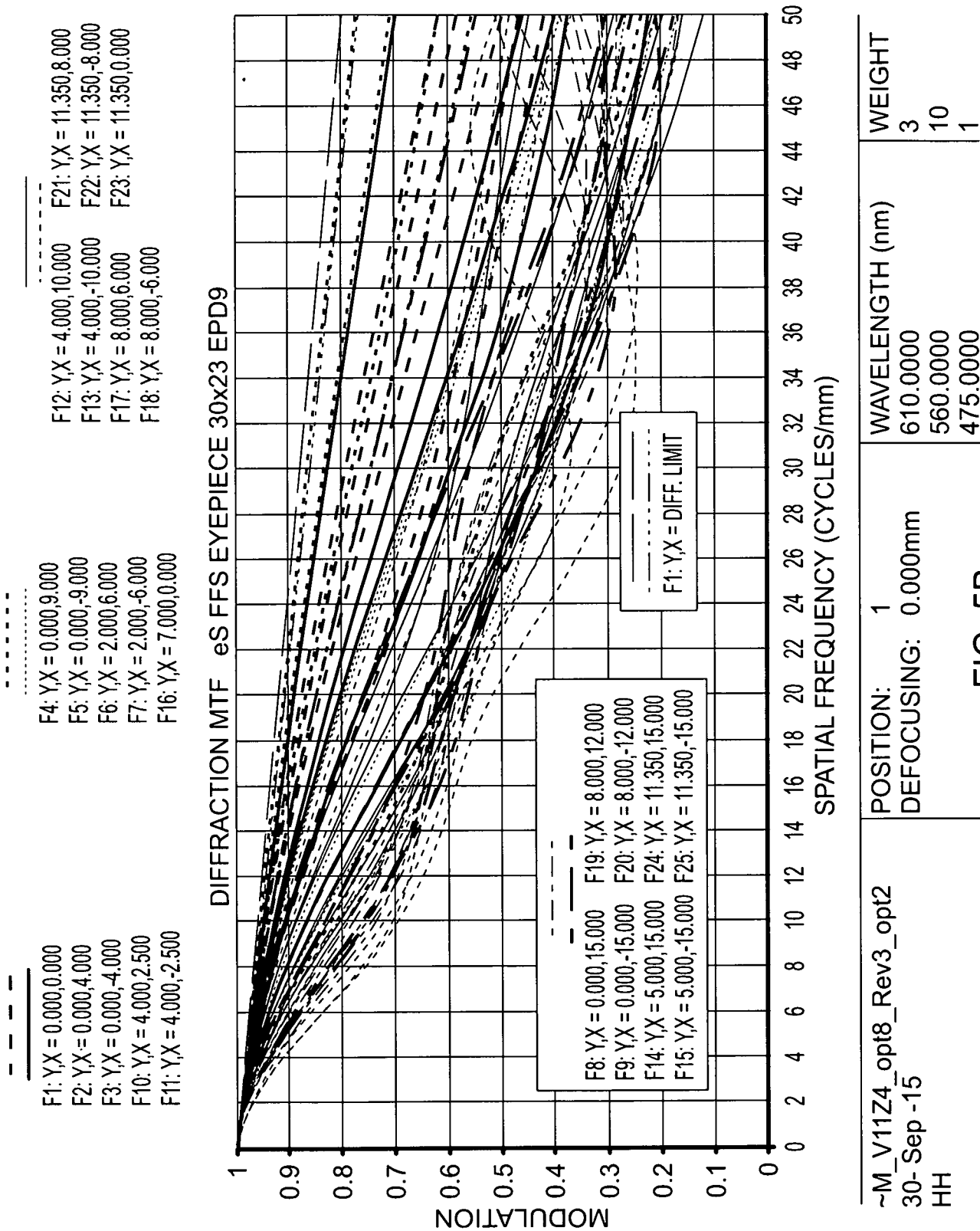


FIG. 5B

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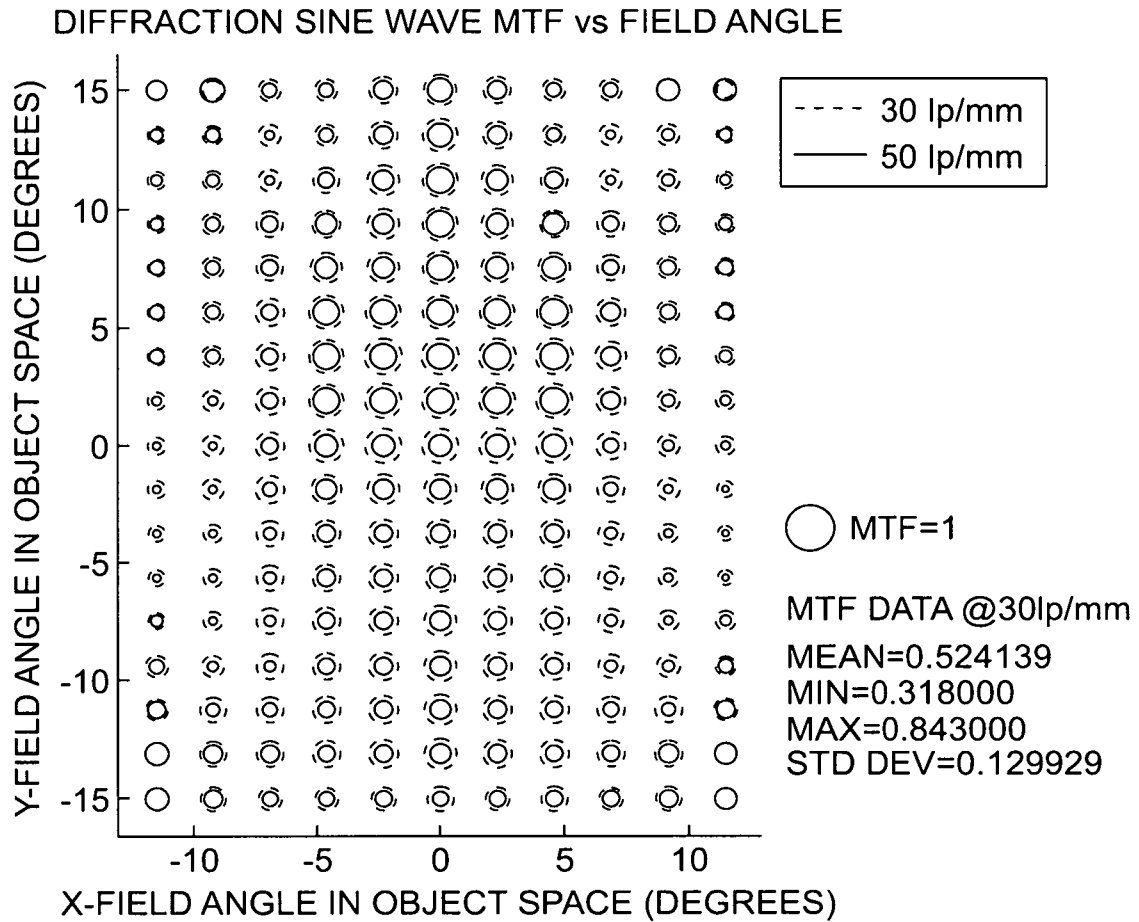


FIG. 6A

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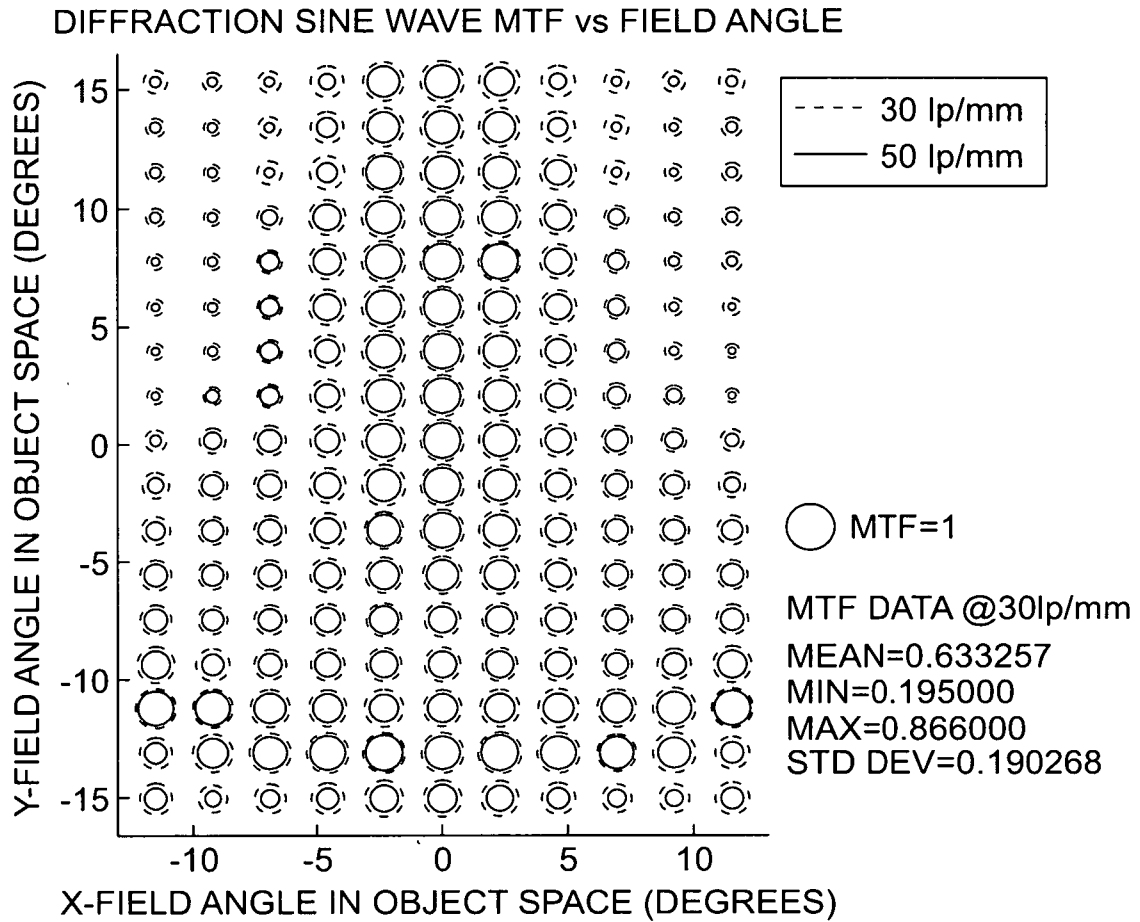


FIG. 6B

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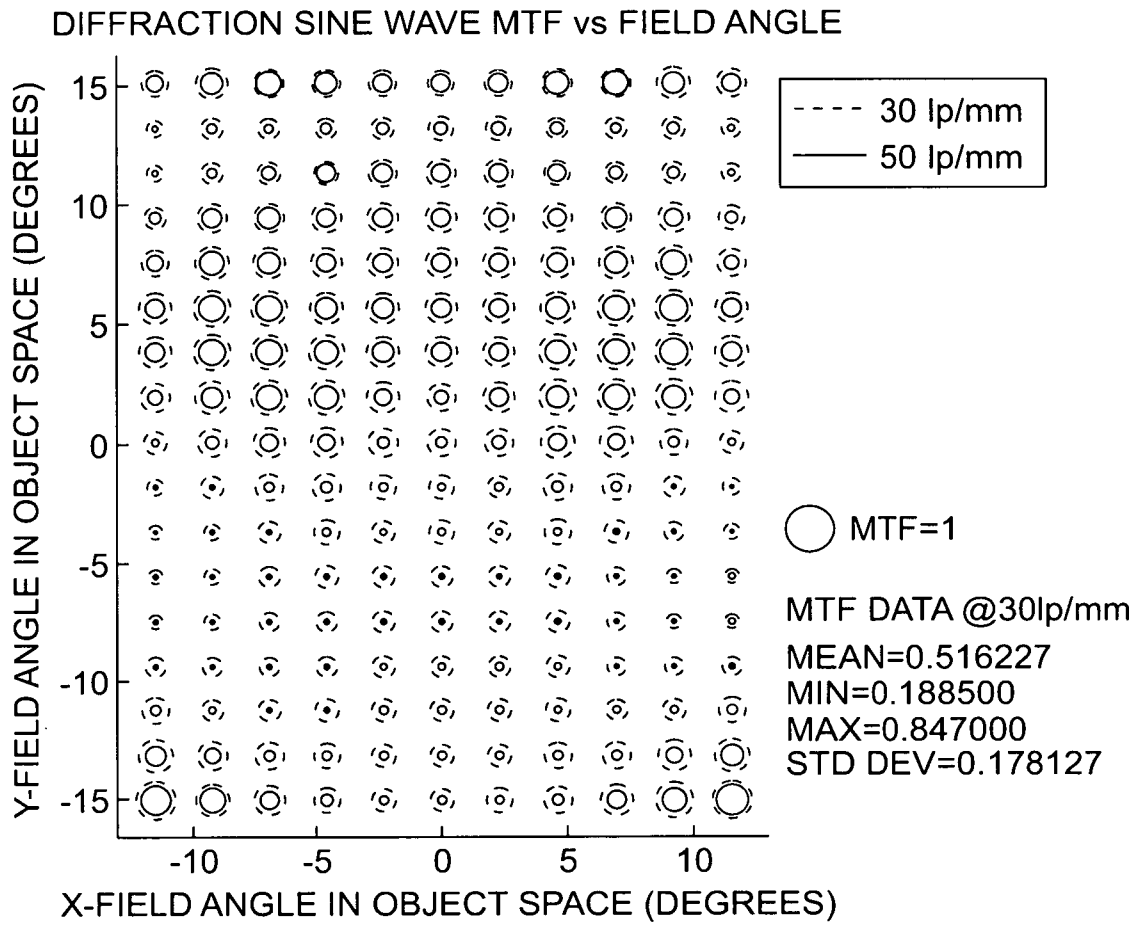


FIG. 6C

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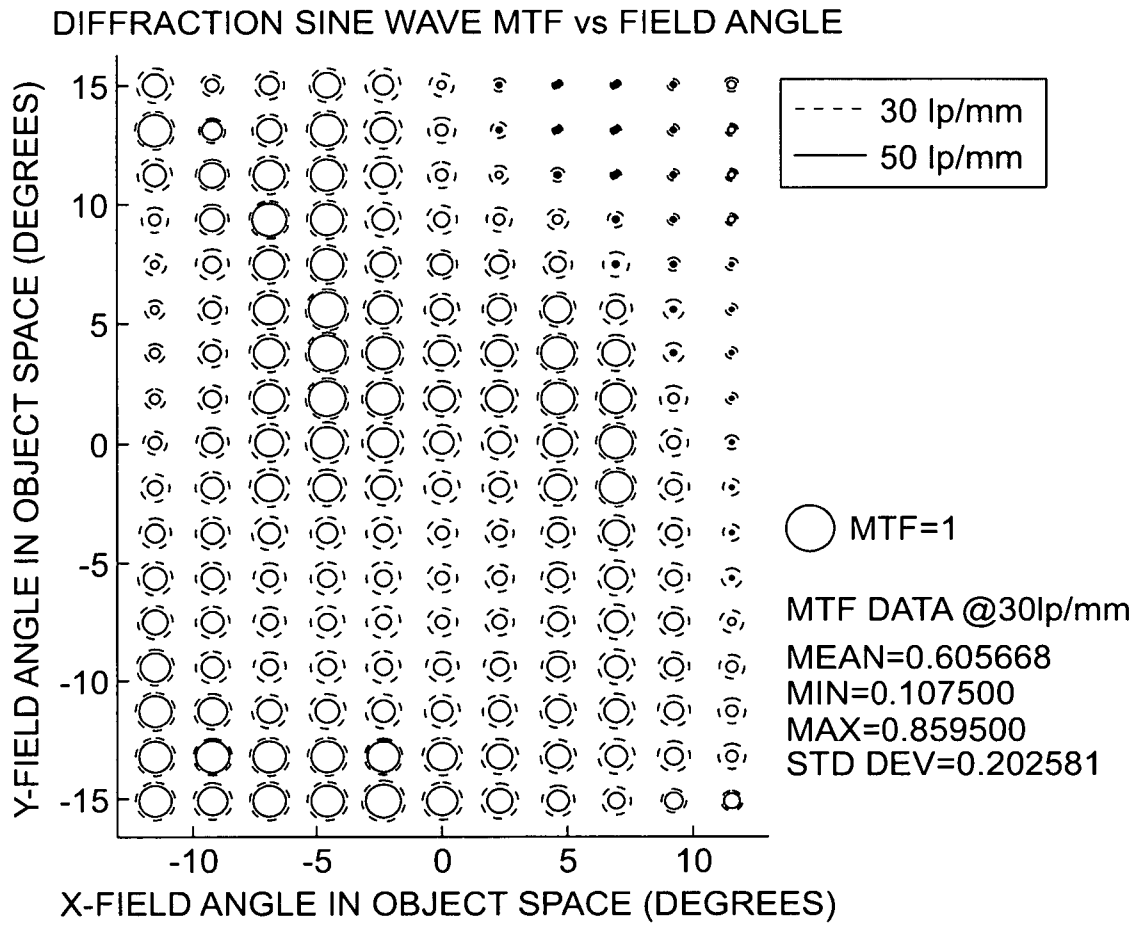


FIG. 6D

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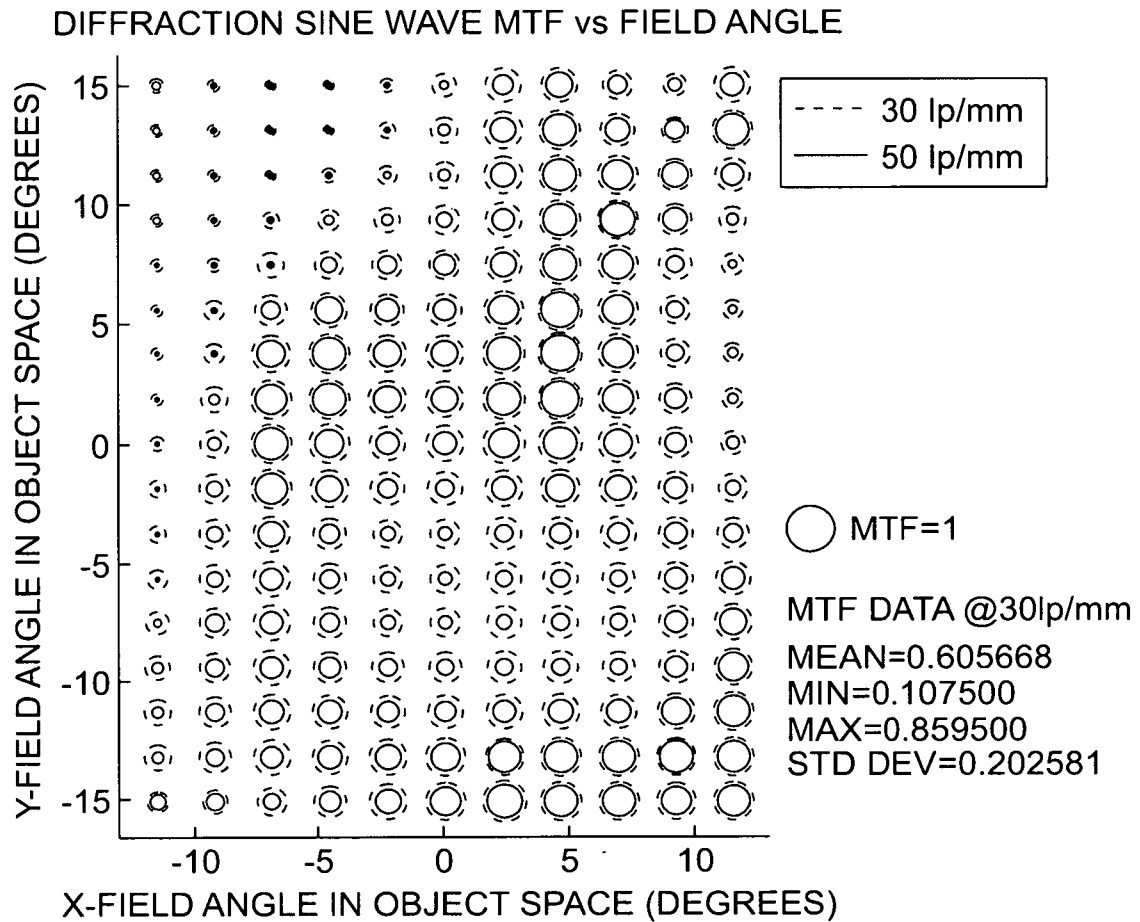
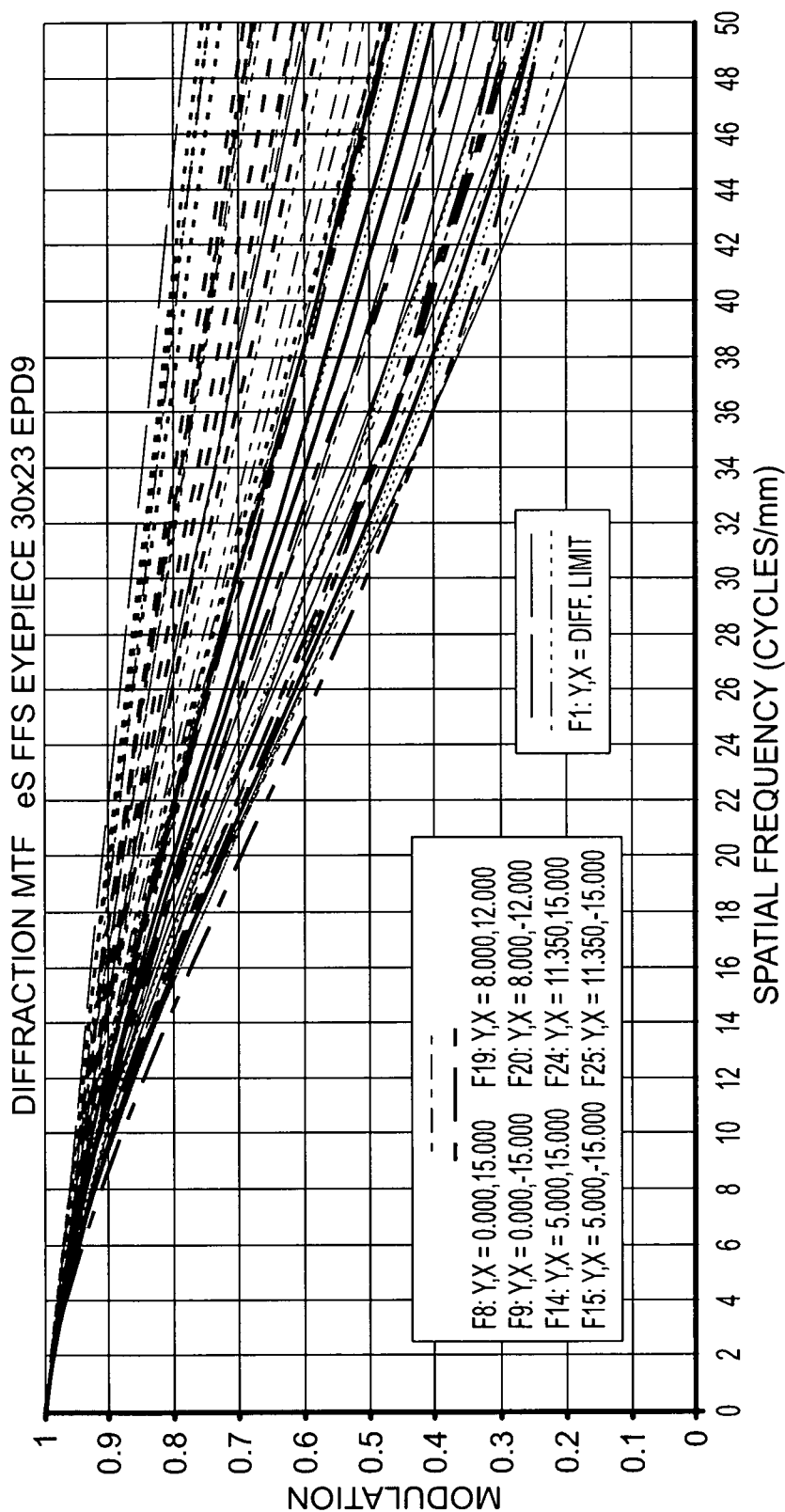
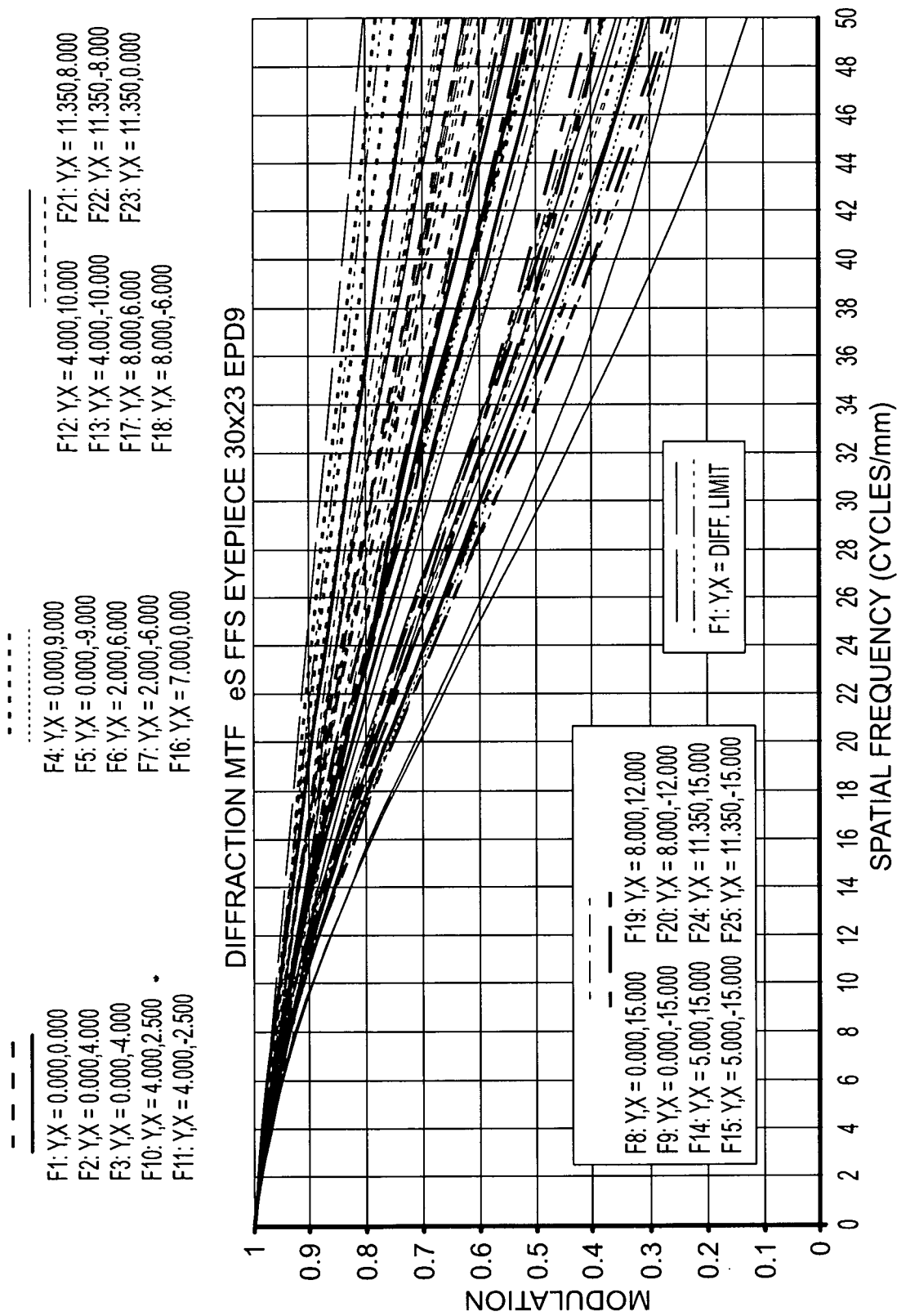


FIG. 6E



~opt8_Rev3_opt2_ap_temp 18- Mar -16 HH	POSITION: DEFOCUSING: 0.000mm	WAVELENGTH (nm) 610.0000 560.0000 475.0000

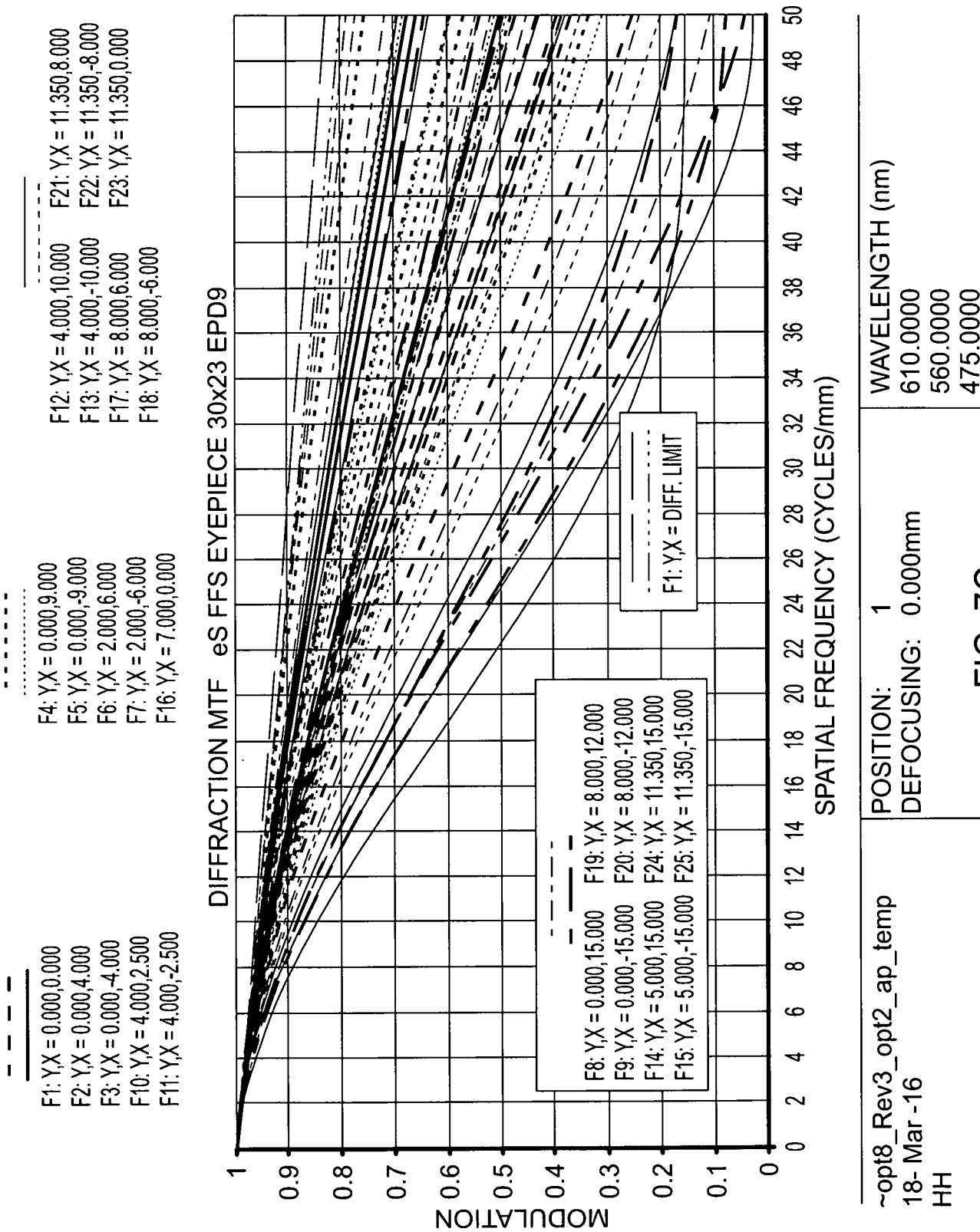
FIG. 7A



~opt8_Rev3_opt2_ap_temp	POSITION:	WAVELENGTH (nm)
18- Mar -16	1	
HH	DEFOCUSING: 0.000mm	610.0000
		560.0000
		475.0000

EIG 7B

FIG. 7B



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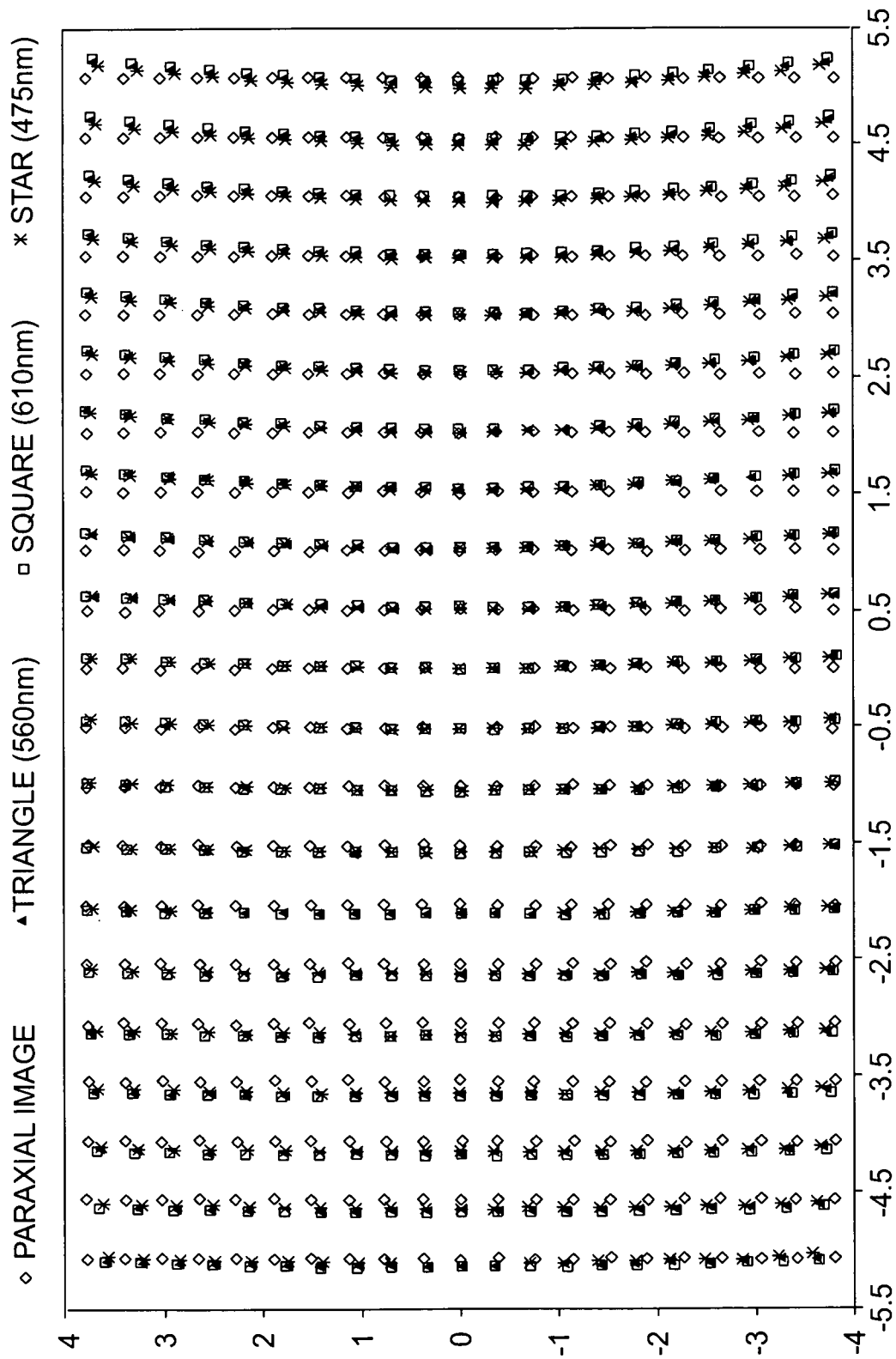


FIG. 8

