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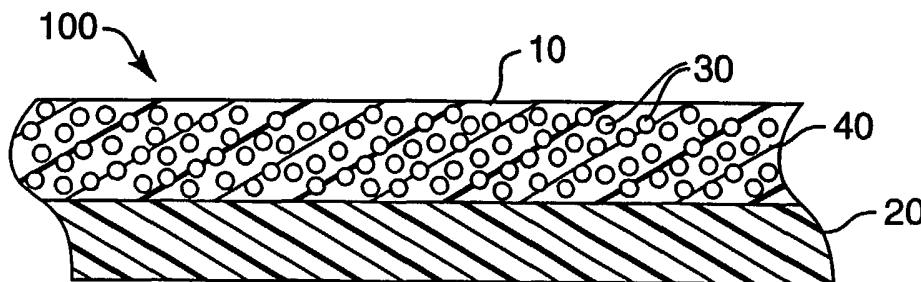
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(54) Title: NANOPARTICLES HAVING A RUTILE-LIKE CRYSTALLINE PHASE AND METHOD OF PREPARING THE SAME



(57) Abstract: Nanometer-sized particles comprise a mixed oxide of titanium and antimony and are characterized by rutile-like crystal phases. The particles are easily prepared by hydrothermal processing, and may be used as colloids, or in various compositions and articles.



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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

NANOPARTICLES HAVING A RUTILE-LIKE CRYSTALLINE PHASE AND METHOD OF PREPARING THE SAME

5 This invention relates to nanometer-sized particles comprising oxides of titanium and antimony, and in particular, to methods of making such particles, and compositions and articles containing same.

10 Nanocomposite materials, that is, materials having homogeneously dispersed inorganic nanoparticles in an organic binder, have been used as protective transparent coatings for various applications. Such materials may have improved abrasion resistance and/or optical properties (for example, refractive index) as compared to coatings of the corresponding organic binder not having inorganic nanoparticles dispersed therein.

15 Nanocomposite materials containing various inorganic nanoparticles, such as titania (that is, titanium dioxide) nanoparticles, have been described. Titania occurs in at least three crystal forms: anatase, brookite, and rutile. Of these, the rutile form has the greatest density, hardness, and refractive index.

20 Major problems with preparing titanium oxide sols, and particularly titanium oxide sols having the rutile crystalline phase may include: long process times, the need to use additional stabilizing counterions (for example, chloride, nitrate, etc.) that must be laboriously removed prior to use in applications such as organic protective films, extreme pH values, and/or limited stability.

25 It would be desirable to have quick and easy methods for preparing stable colloidal dispersions of inorganic particles containing titanium, wherein the particles have properties at least comparable to the rutile form of titania. It would also be desirable to homogeneously incorporate such particles into an organic binder to provide high index of refraction abrasion resistant coatings.

In one aspect, the invention provides a composition comprising a plurality of Ti/Sb mixed oxide nanoparticles in the form of an aqueous colloidal dispersion, wherein the Ti/Sb mixed oxide nanoparticles comprise a rutile-like crystalline phase.

30 In some embodiments the nanoparticles have at least one organic moiety bound to the nanoparticle surface.

In another aspect, the invention provides a method for preparing an aqueous colloidal dispersion of Ti/Sb mixed oxide nanoparticles comprising the steps of:

- a) providing an aqueous titania precursor;
- b) providing an aqueous antimony oxide precursor;
- c) combining with mixing both aqueous precursors; and
- d) hydrothermally processing the mixture;

5 wherein the weight ratio of titanium to antimony is in the range of from 0.14 to 11.3.

In some embodiments, the method further comprises the step of modifying the surface of the nanoparticles.

10 Colloidal dispersions prepared according to the invention typically are highly stable.

In another aspect, the invention provides a composition comprising agglomerated nanoparticles, wherein the agglomerated nanoparticles comprise Ti/Sb mixed oxide nanoparticles comprising a rutile-like crystalline phase.

15 In some embodiments, the agglomerated nanoparticles are redispersible into a liquid vehicle.

In another aspect, the invention provides a nanocomposite precursor comprising a plurality of nanoparticles homogeneously dispersed in an organic binder precursor, wherein the nanoparticles comprise Ti/Sb mixed oxide nanoparticles containing a rutile-like crystalline phase.

20 In another aspect, the invention provides a nanocomposite comprising a plurality of nanoparticles dispersed in an organic binder, wherein the nanoparticles comprise Ti/Sb mixed oxide nanoparticles containing a rutile-like crystalline phase.

In some embodiments, the nanoparticles have at least one organic moiety bound to the nanoparticle surface.

25 In some embodiments, nanocomposites according to the invention may be supported on a substrate.

Nanocomposites according to the invention are well suited for use as protective coatings, and may have a high refractive index.

As used herein, the following definitions apply:

30 "aqueous titania precursor" refers to an aqueous titanium containing composition that may be converted to titania by one or more of heating, evaporation, precipitation, pH adjustment, and combinations thereof;

“aqueous antimony oxide precursor” refers to an aqueous antimony containing composition that may be converted to antimony oxide by one or more of heating, evaporation, precipitation, pH adjustment, and combinations thereof;

5 “hydrothermal processing” means heating in aqueous media, in a closed vessel, to a temperature above the normal boiling point of water;

“nanoparticle” means a particle having a maximum particle diameter of less than 500 nanometers;

“rutile-like” means having a tetragonal crystal structure and a space group of $P4_2/mnm$ (#136);

10 “organic moiety” means an organic group, ion, or molecule; and

“mixed oxide” means an intimate mixture of titanium and antimony oxides.

FIG. 1 is a cross-sectional view of a composite article according to the invention.

15 **FIG. 2** is a schematic representation of a reaction system useful for preparing Ti/Sb mixed oxide nanoparticles according to the present invention.

FIG. 3 is a cross-sectional view of one embodiment of a pulse dampener useful in practice of the invention.

20 In its various aspects, the invention concerns nanoparticles comprising a mixed oxide of titanium and antimony (hereinafter abbreviated Ti/Sb mixed oxide), wherein at least a portion of the Ti/Sb mixed oxide has a rutile-like crystalline phase.

Nanoparticles of the invention comprise Ti/Sb mixed oxide. Typically, the weight ratio of titanium to antimony in the nanoparticles is in the range of 0.14 to 11.30, desirably in the range of from 0.22 to 5.02, and more desirably in the range of from 0.42 to 2.93.

25 Ti/Sb mixed oxide nanoparticles according to the invention desirably comprise a rutile-like crystalline phase. The rutile-like crystalline phase may co-exist with other crystalline phases within individual Ti/Sb mixed oxide nanoparticles. Individual nanoparticles may comprise up to 100 weight percent of the rutile-like crystalline phase. Ensembles of Ti/Sb mixed oxide nanoparticles (that is, all Ti/Sb mixed oxide
30 nanoparticles taken as a whole) will typically comprise nanoparticles having a variety of sizes, elemental compositions, and crystalline phases. The term “ensemble average” of a parameter, as used herein, refers to the average value of that parameter across the entire

ensemble being referred to. Thus, the term refers to a property of the bulk, not necessarily reflective of that property in each individual member of the ensemble.

Desirably, the ensemble average rutile-like crystalline phase content of Ti/Sb mixed oxide nanoparticles is at least 20 weight percent, more desirably at least 40 weight percent, more desirably at least 60 weight percent, and even more desirably at least 80 weight percent based on the total weight of Ti/Sb.

In some applications, it may be desirable that substantially all of the Ti/Sb mixed oxide nanoparticles contain a rutile-like crystalline phase.

Desirably, as measured by X-Ray Diffraction analysis (that is, XRD, as described hereinbelow), the ensemble average relative intensity of rutile-like crystalline phase as compared to anatase, for Ti/Sb mixed oxide nanoparticles of the invention, is greater than 1:10. Further, it may also be desirable that the relative intensity of any anatase or antimony oxide maxima observed by XRD have a relative intensity of less than 1 percent, more desirably less than 0.1 percent, where the relative intensity of the greatest diffraction maximum of the rutile-like phase is defined to be 100 percent.

Typically, the Ti/Sb mixed oxide nanoparticles are free of additional metallic elements, although for some particular applications it may be desirable to add additional elements (including silicon). If additional metallic elements are present, they are desirably in an amount of less than 0.1 moles per mole of titanium present in the ensemble average of Ti/Sb mixed oxide nanoparticles. Exemplary additional metallic elements include the rare earth elements.

Ti/Sb mixed oxide nanoparticles of the invention typically have an ensemble average particle size of less than 500 nanometers, more desirably less than 100 nanometers, and still more desirably less than 40 nanometers, especially when the nanoparticles are to be incorporated into a transparent coating.

In some embodiments, Ti/Sb mixed oxide nanoparticles may be combined with additional nanoparticles having a different elemental composition (for example, silica, zirconia, alumina, titania, antimony pentoxide). Desirably, such additional nanoparticles, if present, have an average particle size comparable to that of the Ti/Sb mixed oxide nanoparticles. Such nanoparticles may be commercially obtained, for example, from Nalco Chemical Co. (Naperville, IL) or Nyacol Nano Technologies, Inc. (Ashland, MA). Exemplary additional nanoparticles are also described in U.S. Pat. Nos. 5,037,579 and 6,261,700.

In some embodiments of the invention, the nanoparticles are selected such that colloids and nanocomposites are free from a degree of particle agglomeration or coagulation that would interfere with the desired properties of the composition. Desirably, individual, unassociated (that is, non-agglomerated and non-coagulated) particles are dispersed throughout the composition. In these embodiments, the particles desirably do not irreversibly associate (for example, by covalently bonding and/or hydrogen bonding) with each other.

In other embodiments, such as in the preparation of thin films, it may be desirable for the nanoparticles to irreversibly agglomerate, especially when employed without a dispersing medium (for example, liquid vehicle or binder).

Nanoparticles may be present in colloidal dispersions of the invention in an amount of up to 30 percent, or more. The amount may vary with density and surface characteristics of the nanoparticle. Desirably, nanoparticles are present in an amount of from 1 to 25 weight percent, more desirably from 10 to 20 weight percent, of the colloidal dispersion.

Depending on the application, the pH of colloidal dispersions of the invention may be any value, but typically range from 4 to 9, desirably from 5 to 8.

Colloidal dispersions of the invention are typically prepared as a dispersion of nanoparticles in an aqueous vehicle. The aqueous vehicle comprises water, typically as the predominant ingredient, and may contain organic solvents (especially solvents that may be present in the titania or antimony oxide precursors). Solvent may be added prior to, or more desirably following, hydrothermal processing. Exemplary organic solvents include alcohols, ethers, and/or ketones having from 4 to 12 carbon atoms. One such desirable solvent is 1-methoxy-2-propanol.

Solvents used in the present invention, if present, are chosen based on volatility and compatibility with the aqueous titania and antimony oxide precursors, binder precursor, and/or binder, depending on the point at which they may be added.

Nanoparticles according to the invention may be incorporated in a binder to form a nanocomposite. The nanoparticles may be either directly incorporated into the binder, or incorporated into a binder precursor that is subsequently cured to form a binder. Desirably, nanoparticles are present in the nanocomposite in an amount of at least 30 weight percent based on the total weight of the nanocomposite.

Compatibility of inorganic nanoparticles with organic binders is typically achieved by appropriate treatment of the inorganic particles with a coupling agent.

Prior to incorporation into either a binder or binder precursor, nanoparticles employed in practice of the present invention are typically surface-modified, which may be achieved by attaching surface-modifying agent(s) to the particle surface. Surface-modifying agent(s) attached to the surface of the particle can modify the surface characteristics of the particles to achieve a variety of properties including, for example, to increase the compatibility of the particles with the components of the composition, to facilitate dispersion of the particles in the composition (either from isolated or colloidal form), and to enhance optical clarity of the composition and combinations thereof. The particles can also be surface-modified to include surface groups capable of associating with other components of the composition. When the composition is polymerized, for example, the surface groups can associate with at least one component of the composition to become part of the polymer network. Preferably, the surface groups are capable of associating with the first monomer, the second monomer, or a combination thereof. Preferably, the particles are surface-modified to include a combination of surface groups capable of providing compositions having desired dispersion, clarity, adhesive, and rheological properties.

Schematically, surface-modifying agents can be represented by the formula A-B where the A group is capable of attaching to the surface of the particle, and where the B group is a compatibilizing group that may be reactive or non-reactive with the components of the composition. Compatibilizing groups B that impart polar character to the particles include, for example, polyethers. Compatibilizing groups B that impart non-polar character to the particles include, for example, hydrocarbons.

Exemplary suitable surface-modifying agents include, for example, carboxylic acids, sulfonic acids, phosphonic acids, silanes, phosphates, and combinations thereof. Useful carboxylic acids include, for example, long chain aliphatic acids including octanoic acid, oleic acid, and combinations thereof. Representative examples of polar modifying agents having carboxylic acid functionality include $\text{CH}_3\text{O}(\text{CH}_2\text{CH}_2\text{O})_2\text{CH}_2\text{CO}_2\text{H}$, 2-(2-methoxyethoxy)acetic acid, and mono(polyethylene glycol) succinate. Representative examples of nonpolar surface-modifying agents having carboxylic acid functionality include octanoic acid, dodecanoic acid, and oleic acid.

Exemplary useful silanes include organosilanes, for example, octyltrimethoxysilane, 3-methacryloyloxypropyltrimethoxysilane, 3-mercaptopropyltrimethoxysilane, n-octyltriethoxysilane, phenyltriethoxysilane, p-tolyltriethoxysilane, vinyltrimethoxysilane, and combinations thereof.

5 Exemplary useful non-silane surface-modifying agents capable of associating with organic components of the composition include acrylic acid, methacrylic acid, beta-carboxyethyl acrylate, mono-2-(methacryloxyethyl) succinate, and combinations thereof. A useful surface-modifying agent that imparts both polar character and reactivity to the particles is mono-(methacryloxypolyethyleneglycol) succinate.

10 Nanoparticles can be surface modified using a variety of methods including, for example, adding a surface-modifying agent to nanoparticles (for example, in the form of a powder or an aqueous sol) and allowing the surface-modifying agent to react with the nanoparticles. A co-solvent can be added to the composition to increase the compatibility (for example, solubility or miscibility) of the surface-modifying agent and/or surface
15 modified particles with the aqueous mixture.

The surface-modified nanoparticles may be intimately mixed with a curable binder precursor that may be subsequently processed prior to curing. The choice of binder precursor is not critical so long as it is not reactive under ambient conditions with the surface-modified nanoparticles. Exemplary binder precursors include, but are not limited
20 to, polymerizable materials such as free-radically polymerizable monomers and oligomers such as acrylates, methacrylates, allylic compounds, vinyl ethers, vinyl esters, and the like; epoxy resins; alkyd resins; phenolic resins; cyanate esters; melamine and melamine-formaldehyde resins; polyurethane resins, and mixtures thereof. Desirably, binder precursors comprise acrylates and/or methacrylates.

25 The binder precursor may include a catalyst or other curative in order to facilitate cure. Such catalysts and other curatives will depend on the nature of the binder precursor and may include those well known in the curing art, for example, thermal free radical initiators, such as peroxides and azo compounds, photoinitiators, photocatalysts, amine hardeners, mercaptans, etc.

30 The binder precursor may be cured to form a binder by application of energy such as heat or actinic radiation (for example, ultraviolet light and electron beam radiation), or through addition of a catalyst or curative. Desirably, in the case of free-radically

polymerizable binder precursors, a photoinitiator is present in the binder precursor and the mixture is irradiated with ultraviolet actinic radiation from a lamp, desirably in an inert atmosphere such as nitrogen. The use of actinic radiation to cure the binder precursor allows a high degree of flexibility in the choice of protecting groups.

5 When used, the amount of actinic radiation energy used for curing depends upon a number of factors, such as the amount and the type of reactants involved, the energy source, web speed, the distance from the energy source, and the thickness of the material to be cured. As general guidelines, actinic radiation typically involves a total energy exposure from 0.1 to 10 Joules per square centimeter, and electron beam radiation
10 typically involves a total energy exposure in the range from less than 1 megarad to 100 megarads or more, desirably 1 to 10 megarads. Exposure times may be from less than 1 second up to 10 minutes or more.

 Commercially available free-radical generating photoinitiators suitable for the invention include, but are not limited to, benzophenone, benzoin ether, and acylphosphine
15 photoinitiators such as those sold under the trade designations IRGACURE and DAROCUR from Ciba-Geigy Corp. (Ardsley, NY). The amount of photoinitiator(s) used typically varies between 0.1 and 15 weight percent, desirably between 0.5 and 7 weight percent, based on the total weight of the binder precursor.

 Co-initiators and amine synergists can be included in order to improve curing rate.
20 Examples of such include isopropylthioxanthone, ethyl 4-(dimethylamino)benzoate, 2-ethylhexyl dimethylaminobenzoate, and dimethylaminoethyl methacrylate.

 The volume ratio of surface-modified nanoparticles to binder precursor may range from 1:99 up to 70:30, desirably from 5:95 up to 55:45, and more desirably from 10:90 up to 40:60.

25 For applications in which transparency is important, nanoparticles present in the binder precursor and/or binder desirably have a small particle size (for example, < 40 nm) to minimize the effects of light scattering.

 Those skilled in the art will also appreciate that, depending on the application, the binder and its precursor can contain other optional adjuvants, such as surfactants, antistatic
30 agents (for example, conductive polymers), leveling agents, thermal initiators, photosensitizers, UV absorbers, stabilizers, antioxidants, fillers, lubricants, pigments, dyes, plasticizers, suspending agents, and the like.

As illustrated in **FIG. 1**, a composite article **100** may comprise a nanocomposite layer **10** containing Ti/Sb mixed oxide nanoparticles **30** dispersed in a binder **40**, and supported on a substrate **20**, wherein at least a portion of the Ti/Sb mixed oxide nanoparticles contain a rutile-like crystalline phase.

5 The substrate may be virtually any solid material. Non-limiting examples of such substrates include glass (including electronic displays), quartz, transparent or translucent ceramics, wood, metal, painted surfaces including painted metals, and thermoset and thermoplastic materials such as acrylic polymers (for example, polymethyl methacrylate), polycarbonates, polyurethanes, polystyrene, styrene copolymers, such as acrylonitrile-butadiene-styrene copolymer and acrylonitrile-styrene copolymer, cellulose esters (for
10 example, cellulose acetate, cellulose diacetate, cellulose triacetate, and cellulose acetate-butyrate copolymer), polyvinyl chloride, polyolefins (for example, polyethylene and polypropylene), polyamides, polyimides, phenolic resins, epoxy resins, polyphenylene oxide, and polyesters (for example, polyethylene terephthalate). Thermoplastic materials
15 may contain fillers and other adjuvants.

Desirably the substrate is glass or a thermoplastic polymer film. Substrates may be either opaque or transparent depending on the application.

Nanocomposite layer **10** may be prepared by coating a composition comprising nanoparticles **30** and a binder precursor onto substrate **20**, and curing the binder precursor.
20 Coating may be accomplished by virtually any known coating means that does not chemically or physically alter properties of the binder precursor. Exemplary coating methods include, for example, spin coating, knife coating, wire coating, flood coating, padding, spraying, exhaustion, dipping, roll coating, foam techniques, and the like.

The thickness of the mixture of binder precursor and nanoparticle layer that is
25 applied will depend on the particular primary substrate and application. For protective coatings, the thickness of the resultant cured nanocomposite layer is desirably in the range of from 1 nanometers up to 50 micrometers or even thicker, more desirably from 0.5 micrometers to 10 micrometers, and more desirably from 3 micrometers to 6 micrometers. Thicker nanocomposite layers may lead to crazing and other defects over time; however,
30 thinner layers often do not provide enough surface material to be scratch resistant.

When present as a coating on transparent or translucent substrates, the ingredients in the nanocomposite layer are desirably chosen so that it has a refractive index close to

that of the substrate. This can help reduce the likelihood of Moiré patterns or other visible interference fringes.

Ti/Sb mixed oxide nanoparticles are prepared by combining an aqueous titania precursor with an aqueous antimony oxide precursor.

5 As intimate mixing of titanium and antimony atoms in the crystal lattice is highly desirable, aqueous antimony oxide precursors are desirably molecular species (that is, species having a single antimony atom) or loosely associated species that dissociate under reaction conditions. Any titania or antimony oxide precursors meeting this requirement may be used.

10 Exemplary aqueous titania precursors include the reaction products of hydrogen peroxide with titanium alkoxides. Exemplary alkoxides include as 1-butoxide, 2-ethylhexoxide, 2-methoxy-1-ethoxide, linear and branched alkoxides (such as ethoxide, 1-propoxide, 2-propoxide, 2-butoxide, iso-butoxide, tert-butoxide, hexoxide, and the like). Two or more of the same or different organic ligands may be attached to the titanium.
15 Desirably, the aqueous titania precursor is a reaction product of a titanium alkoxide with hydrogen peroxide.

Exemplary aqueous antimony oxide precursors include the reaction products of antimony alkoxides with hydrogen peroxide and HSb(OH)_6 . Exemplary alkoxides include
20 as ethoxide, 1-propoxide, 2-propoxide, 2-butoxide, isobutoxide, tert-butoxide, hexoxide, and the like). Two or more of the same or different organic ligands may be attached to the antimony.

The aqueous titania and antimony oxide precursors are combined with mixing and simultaneously, or sequentially, are subjected to conditions whereby they form a mixed
25 oxide. The amount of each precursor employed is determined based on the stoichiometric quantity required to prepare Ti/Sb mixed oxide nanoparticles of the invention as described above. Additionally, aqueous metallic oxide precursors may be mixed with the aqueous titania and antimony oxide precursors, if desired.

30 After mixing the aqueous titania and antimony oxide precursors, the mixture is typically subjected to heat and pressure. In some embodiments, this may be accomplished by means of a pressure vessel such as a stirred or non-stirred pressure reactor, commercially available from Parr Instruments Co. (Moline, IL). The vessel should be

capable of withstanding pressure and capable of sealing. The vessel containing the mixture is sealed, and the solution is heated to a temperature satisfactory to drive the hydrolysis and condensation of the reactants. Typically, the vessel is heated at a rate of 5 °C/minute until the desired temperature is reached. Suitable pressures are governed by the temperature and the vessel used to heat the reaction mixture. Generally, the desired temperature is greater than 120 °C and less than 300 °C. Desirably, the temperature is between 150 °C and 200 °C. Heating the solution within the closed vessel creates pressure. The pressure within the vessel is typically between 18 atmospheres to 40 atmospheres. Typically, the solution is heated for up to 5 hours to ensure complete hydrolysis although shorter reaction times can be effective. The length of the heating time is determined by the time necessary to achieve the desired temperature of the bulk. Once this temperature is achieved, the reaction is typically over virtually instantaneously. Additional time at this temperature typically leads to increasing crystallite sizes, which usually trends with decreased colloidal stability of the nanoparticles. Desirably, the ensemble average rutile-like crystallite size of Ti/Sb mixed oxide nanoparticles is less than 20 nm, more desirably less than 15 nanometers.

After heating and subsequent cooling to room temperature, the mixed metal oxide particles are typically observed as a slurry of a solid precipitate (that is, agglomerated Ti/Sb mixed oxide nanoparticles) in the aqueous vehicle. The particles may be separated from the liquid by transferring the slurry into centrifuge bottles, centrifuging the slurry, and decanting the supernate. Other methods of separating the mixed metal oxide particles from the reaction mixture are possible such as filtration, sedimentation, or flushing.

Alternatively, any unwanted components of the reaction mixture may be removed by evaporation or by selective distillation. At this point, the metal oxide particles may, optionally, be dried.

Ti/Sb mixed oxide nanoparticles can also be prepared using a stirred tube reactor (that is, STR). Stirred tube reactors typically have a motor driven shaft that is coaxially positioned along the length of a heated tube. The shaft has multiple paddles mounted to it that provide mixing and heat transfer of the reaction mixture. Stirred tube reactors are well known in the art. One particular STR design is described in Example 15.

One embodiment of a process for preparing colloidal dispersions of Ti/Sb mixed oxide nanoparticles of the invention using an STR is outlined in **FIG. 2**. A reservoir **210**

contains an aqueous mixture of a titania precursor and an antimony oxide precursor having a solids content of 1 - 2 weight percent. Pump **220** feeds the aqueous mixture into STR **230** that is heated to around 180 °C to 220 °C in order to provide the heat necessary to set off the hydrothermal reaction that forms the nanoparticles. Desirably, pump **220** is
5 capable of maintaining a substantially even flow rate (for example, a diaphragm pump). Exemplary stirred tube reactors are described in U.S. Pat. Nos. 5,644,007 (Davidson et al.); 5,814,278 (Maistrovich et al.); 4,770,777 (Steadly); and PCT Application No. WO 01/5896, published August 16, 2001

In order to avoid pulsations due to the pump, which may lead to broadening of the
10 particle size distribution, and to assist in applying surface functionalizing agent to the nanoparticles, a pulse dampener **240** is desirably disposed between pump **220** and STR **230**. Hydraulic pulse dampeners are well known in the art. Exemplary pulse dampeners include closed-end pipes and are described in U. S. Pat. Nos. 5,816,291 and 2,504,424. Desirably the pulse dampener comprises a closed-end stand pipe.

One particularly useful embodiment of a pulse dampener is depicted in **FIG. 3**.
15 Pulse dampener **300** contains a pressurized fluid **315**, and consists of a length of pipe **310** having a cap **320** and an air cavity **325** at the uppermost end of the pipe, and a pressurized fluid inlet **330** at the lowermost end of the pipe. Transfer pipe **340** is perpendicularly joined to pipe **310**. Transfer pipe **340** is joined to back pressure valve **370**, which has an
20 outlet pipe **380**. Pipes **310**, **340** and **380** are connected such that fluid travels from the inlet pipe to the outlet pipe without loss of material. When used in practice of this embodiment of the invention, pressurized fluid emerges from outlet pipe **380** and enters the STR. Thus, a diaphragm pump may on its forward stroke push a liquid into pressurized fluid inlet **330** causing air cavity **325** to shrink in volume as the air
25 compresses. On the return stroke as the diaphragm pump refills for the next delivery, the compressed air acts as a mini-compression feed chamber and returns liquid to the fluid stream. The cycle repeats over and over as the pump operates, thereby smoothing pressure pulses of the fluid being pumped.

Typical residence times of the aqueous mixture in STR **230** are 10 - 20 minutes.
30 After leaving STR **230**, the heated mixture passes through a heat exchanger **250** to cool the mixture down before collection. Optionally, a second pump **260** may add a surface functionalizing agent in reservoir **290** to the heated mixture just prior to entering the heat

exchanger in order to treat the surface of the particles to prevent agglomeration. A back-pressure regulator valve 270 is positioned after the heat exchanger and controls the pressure of STR 230 to make sure that the water stays in a liquid state. Typical pressures in the STR are around 250 to 350 pounds per square inch (1.7 to 2.4 megaPascals). The STR provides internal mixing, which facilitates efficient heat transfer. In addition, the mixing action of the STR provides plug flow conditions inside the reactor.

After hydrothermal processing, the colloidal dispersion of Ti/Sb mixed oxide nanoparticles may contain outlier (that is, excessively large) particles. As a result, the aqueous colloidal dispersion coming out of the STR may not be optically transparent. These outlier particles may be removed by centrifugation thereby improving the clarity of the colloidal dispersion and narrowing the particle size distribution.

The colloidal dispersion may be used in that form or solvent (for example, water) may be replaced with an organic solvent or a solution containing an organic solvent and a dispersing aid to form slurry using methods well known in the art. Solvents used in the present invention may be chosen based on volatility and compatibility with any binder precursor that may be used in combination with the nanoparticles. Typical organic solvents include C₆-C₁₂ aliphatic compounds, aromatic compounds, alcohols, ethers, esters, and/or ketones. Exemplary aliphatic solvents include cyclohexane, heptane, toluene, xylene, 2-butanone, or 4-methyl-2-pentanone, 1-methoxy-2-propanol, and the like. 1-Methoxy-2-propanol is especially desirable.

Ti/Sb mixed oxide nanoparticles of the present invention may be advantageously combined with at least one dispersing aid that attaches an organic moiety, desirably through at least one covalent bond, to the surface of the metal oxide particles. Typical dispersing aids include alkoxysilanes such as alkyltrialkoxysilanes, organic acids such as carboxylic acids, alcohols, polyethylene glycols, mono- or di-esters of fatty acids, polyethylene oxide and polypropylene oxide, alkoxyated phosphonic acids and their esters, and combinations thereof.

Desirably, dispersing aids include alkoxysilanes, desirably octyltriethoxysilane, octadecyltrimethoxysilane, hexadecyltrimethoxysilane, carboxylic acids, and combinations thereof.

Other suitable dispersing agents include stearic acid, oleic acid, and KEN-REACT Coupling Agent KR TTS, commercially available from Kenrich Petrochemicals (Bayonne,

NJ). Dispersing aids that are coupling agents may be used. A coupling agent is a dispersing aid with two functional groups. Suitable coupling agents include methacrylic acid, glycine, glycolic acid, mercaptoacetic acid, methacryloyloxyethyl acetoacetate, allyl acetoacetate, 3-acryloxypropyltrimethoxysilane, 3-aminopropyltriethoxysilane, 3-
5 mercaptopropyltrimethoxysilane, 3-glycidoxypropyltrimethoxysilane, 7-octen-1-yltrimethoxysilane, and allyl triethoxysilane.

After the addition of the dispersing aid, the colloidal dispersion typically has a solids content in the range of from 1 to 2 weight percent, although higher and lower solids contents may also be employed. The colloidal dispersion is then stirred, preferably with
10 heating at temperatures greater than 60 °C and less than 95 °C, until the surface of the colloiddally-dispersed particles is substantially coated and/or reacted with the dispersing aid. The colloidal dispersion may be concentrated to give a colloidal dispersion having a solids content in the range of from 2 to 20 weight percent, desirably from 5 to 10 weight percent. The colloidal dispersion typically has a ratio of dispersing agent to metal oxide of
15 0.1 to 6.0 millimole/gram, desirably 0.2 to 2.0 millimole/gram.

An amount of water (neutral, acidic, or alkaline) may then be added in sufficient amount to remove any remaining hydrolyzable groups and further condense dispersing agents to the particle surface. For the purpose of the present invention, base hydrolysis was found to be particularly advantageous for hydrolysis of the alkoxyorganosilane and
20 condensation onto the particle surface.

An optional step involves the removal of high boiling point by-products from the stable colloidal dispersion, whereby the stable colloidal dispersion is concentrated to a syrup by heat or vacuum drying. If the stable colloidal dispersion comprises a polar liquid, the crystalline nanoparticles are weakly flocculated by the addition of a non-polar
25 liquid. If the stable colloidal dispersion comprises a non-polar liquid, the crystalline nanoparticles are weakly flocculated by the addition of a polar liquid. The flocculated nanoparticles are typically isolated by centrifugation and then washed by re-suspension in one of the flocculating liquids and separated by centrifugation. The precipitate may be dried to form a powder, or the precipitate may be dispersed in an organic liquid or solvent
30 to form a colloid.

Colloids of the present invention are stable dispersions as measured by centrifuging the colloid samples at 2500 rpm for 10 minutes. Colloids (or sols), if substantially free of sediment after centrifugation, are said to be stable dispersions.

The invention will now be described further by way of the following examples.

5

EXAMPLES

Materials employed in the examples that follow may be obtained from general commercial chemical vendors such as Aldrich Chemical Co. (Milwaukee, WI) unless otherwise indicated.

TEST METHODS USED IN THE EXAMPLES

10

Particle Size

Particle Size was determined by Photon Correlation Spectroscopic analysis using a Coulter N4 Submicron Particle Analyzer, commercially available from Coulter Corp. (Miami, FL).

Crystalline Phase

15

X-ray diffraction analysis (that is, XRD) was used to determine the crystalline phase. Data were collected using a Philips vertical diffractometer, commercially available from Philips Electronic Instruments Co. (Mahwah, NJ). The diffractometer was fitted with variable entrance slits, fixed 0.2 degree receiving slit, graphite diffracted beam monochromator, and proportional detector for registry of the scattered radiation. A sealed copper target X-ray source was used at generator settings of 45 kV and 35 mA. Each sample was prepared as an ethanol slurry on a glass substrate. Survey step scans were conducted from 5 to 80 degrees (2θ) using a 0.04 degree step interval and 4 second counting time. Identification of the crystalline phases present was achieved by comparison (as described by H. P. Klug and L. E. Alexander in "X-Ray Diffraction Procedures for Polycrystalline and Amorphous Materials", John Wiley & Sons, New York (1954)) of the observed diffraction maxima to the patterns present in the International Centre for Diffraction Data powder data file (International Centre for Diffraction Data, 12 Campus Boulevard, Newton Square, PA).

20

25

INTERMEDIATES USED IN THE EXAMPLES

30

Peroxy Titanic Acid

A 2-liter flask was charged with 848 g deionized water, 85 g of 30 weight percent hydrogen peroxide, commercially available from Fisher Scientific (Pittsburgh, PA) and 32

g of 0.33 M aqueous ammonium hydroxide. The stirred contents of the flask were cooled to 10 °C in a cold-water bath, and 35.6 g titanium tetraisopropoxide, commercially available from Gelest, Inc. (Tullytown, PA) was added slowly over 3 minutes resulting in an orange-yellow precipitate and the gentle evolution of gas. The slurry was allowed to slowly warm to room temperature over 6 hours over which time the precipitate was fully digested to give a yellow, pourable liquid composed of peroxy titanate acid in water (theoretical yield was 1 weight percent TiO₂).

Antimony Hydrogen Peroxide Solution

A 1-liter flask was charged with 469 g deionized water and 21 g of 30 weight percent hydrogen peroxide. The stirred contents were cooled to 5 °C in an ice bath, and 10.5 g antimony tri-n-butoxide was added slowly over 3 minutes resulting in a white precipitate. The slurry was allowed to slowly warm to room temperature over 6 hours during which time the precipitate was fully digested to give a clear colorless solution (theoretical yield was 1 weight percent Sb₂O₅).

Preparation Of Colloidal HSb(OH)₆

A 0.5-liter flask was charged with 297 g deionized water, 20 g AMBERLITE IR-120 (plus) ion-exchange resin, and 4.9 g potassium hexahydroxyantimonate. The resultant slurry was allowed to mix 14 hours and subsequently heated to 65 °C for 1 hour to form a stable white sol. The sol was cooled to room temperature and filtered on a C-grade glass frit to give an aqueous white colloid of HSb(OH)₆ with a measured pH of 3 (theoretical yield was 1 weight percent Sb₂O₅).

EXAMPLES 1 – 13 and COMPARATIVE EXAMPLES A – C

Examples 1 - 13 and Comparative Examples A - C were generated according to the following general procedure, with modifications to amounts of ingredients as indicated in Table 1, describes the preparation of an aqueous colloid containing Ti/Sb mixed oxide nanoparticles having a rutile-like crystalline phase.

A 2-liter pressure reactor, commercially available from Pressure Products Industries, Inc. (Warminster, PA) was charged with about 1200 g of a mixture of peroxy titanate acid and colloidal HSb(OH)₆ in a weight ratio as indicated in Table 1. The reactor was heated to 180 °C for 3 hours. The reactor was allowed to cool slowly to room

temperature over 12 hours. The resultant transparent colloid was filtered through a GF/B filter (glass fiber filter, 1.0 micrometer pore size), commercially available from Whatman, Inc. (Clifton, NJ).

5 The results show that nanoparticles having rutile-like phases were obtained for compositions of Ti/Sb mixed oxides having a theoretical Sb_2O_5 content greater than 10 weight percent, but less than 100 weight percent.

TABLE I

Example	Weight Percent Sb ₂ O ₅	Weight Ratio of Sb/Ti	Powder X-ray Diffraction			Powder X-ray Diffraction			Lattice Parameters				Dynamic Light Scattering ^a	
			Relative Intensities			Crystallite Sizes (nm)			Anatase		Rutile			Solution Particle size (nm)
			Anatase	Rutile	Sb ₂ O ₅ ·4H ₂ O	Anatase	Rutile	Sb ₂ O ₅ ·4H ₂ O	a	c	a	c		
Comparative Example A	0	0.00	100	2	0	19.5*	0.0	0.0	3.796	9.528	--	--	1000	
Comparative Example B	5	0.07	100	1	0	24.5	0.0	0.0	3.802	9.541	--	--	278	
1	10	0.14	100	14	0	19.0	14.0	0.0	3.800	9.522	4.610	2.974	233	
2	15	0.22	19	100	0	13.0	13.5	0.0	3.797	9.562	4.623	2.987	173	
3	20	0.31	3	100	0	<5	12*	0.0	--	--	4.628	2.990	42*	
4	25	0.42	0	100	0	0.0	10.5	0.0	--	--	4.633	2.997	51*	
5	30	0.54	0	100	0	0.0	10.0	0.0	--	--	4.639	2.998	6	
6	35	0.68	0	100	0	0.0	9.0	0.0	--	--	4.638	3.010	32	
7	40	0.84	0	100	0	0.0	9.8*	0.0	--	--	4.649	2.997	30	
8	45	1.03	0	100	0	0.0	10.0	0.0	--	--	4.657	3.012	3	
9	50	1.26	0	100	0	0.0	10.3*	0.0	--	--	4.657	3.001	28	
10	60	1.88	0	100	0	0.0	11.5	0.0	--	--	4.659	3.017	47	
11	70	2.93	0	100	0	0.0	12.5	0.0	--	--	4.664	3.006	166	
12	80	5.02	0	71	100	0.0	11.5	20.0	--	--	4.666	3.025	6	
13	90	11.30	0	12	100	0.0	12.0	17.5	--	--	4.658	3.018	105	
Comparative Example C	100	N/a	0	0	100	0.0	0.0	18.5	--	--	--	--	30	

In Table 1, “*” indicates the value is the numerical average of two separate measurements.

EXAMPLE 14

This example describes the preparation of an aqueous colloid of Ti/Sb mixed oxide nanoparticles having a rutile-like crystalline phase.

5 A 2-liter pressure reactor was charged with 1369 g of peroxy titanate acid and 342 g colloidal HSb(OH)₆ (weight ratio was 80 parts titanium dioxide to 20 parts antimony oxide). The reactor was heated to 180 °C for 2 hours. The pressure in the reactor reached 300 pounds per square inch (2.07 megaPascals). The reactor was cooled quickly to 75 °C by packing the outside of the reactor with dry ice. The reaction produced a transparent
10 colloid with a slight blue hue and a measured particle size of 31.9 nanometers with a standard deviation of 6.4 nanometers. A portion (that is, 5 mL) of the colloid was dried in a 100 °C oven and the resultant powder was analyzed by XRD which showed a rutile-like peak with 100 percent relative intensity having a 20.5 nanometers crystallite size and a 49 percent relative intensity anatase peak having a 15.0 nanometers crystallite size. There
15 was no evidence of a separate antimony oxide phase, instead the observed diffraction maxima for the rutile-like phase were slightly shifted from rutile itself, indicating the antimony atoms were distributed throughout the lattice structure.

EXAMPLE 15

This example shows the use of a stirred tubular reactor to prepare Ti/Sb according
20 to one embodiment of the invention.

Colloidal HSb(OH)₆ was added to peroxy titanate acid such that a calculated weight ratio of TiO₂ to Sb₂O₅ was 80/20 obtained. Sufficient concentrated ammonium hydroxide was added to the mixture in order to raise the pH to about 7, which made the precursor stable and prevented gelation. The mixture formed an intermediate peroxy
25 complex that was allowed to digest over 3 hours to form a clear orange solution of mixed metal peroxy complex (1 percent TiO₂/Sb₂O₅ by weight).

The mixture was injected in to a 316 stainless steel 2-liter stirred tube reactor operated at a heater temperature of 204 °C and a residence time of 11.1 minutes. The length of the STR was 60 inches and the inside diameter was 2 inches to give an L/D ratio
30 of 30. The throughput was 180 grams per minute, and the stirring motor speed was 120

revolutions per minute. The system pressure was 300 pounds per square inch (2.1 megaPascals). The temperature at the output of the reactor was 190 °C.

The mixture was pumped through the reactor using a diaphragm pump (Model No. EK-1) commercially available from American Lewa, Inc. (Holliston, MA) having a pulse dampener consisting of an air cavity made from an end-capped length of 10 inch 1/2" OD stainless steel pipe, and a back pressure valve arranged as depicted in **FIG. 3** contiguously situated between the pump and the inlet to the STR. The output mixture from the STR was immediately passed through a heat exchanger to rapidly cool the mixture to about 75-80°C. The particle size of the resultant colloidal dispersion was determined using a CHDF 2000 particle analyzer obtained from Matec Applied Sciences, Inc. (Northborough, MA). The weight average particle size was 123 nanometers.

This dispersion was centrifuged using a CARR POWERFUGE PILOT gravity centrifuge available from Kendro Laboratory Products (Franklin, MA) using a speed setting of 10 (corresponding to a G-Force of 20,308) resulting in a transparent colloidal dispersion of Ti/Sb mixed oxide nanoparticles, exhibiting a rutile-like crystalline phase, having a weight average particle size of 64 nanometers and a narrow size distribution.

EXAMPLE 16

This example shows the preparation of a composite article employing colloidal surface modified Ti/Sb mixed oxide nanoparticles having a rutile-like crystalline phase.

An 8-ounce (237 milliliters) glass jar was charged with 100 grams of antimony doped titanium oxide colloid (as prepared in Example 3) and 600 milligrams SILQUEST A1230 (a silane coupling agent commercially available from Witco Corp. of Endicott, NY). The transparent colloid was placed in an 80 °C oven for 16 hours, then cooled to room temperature. The colloid was transferred to a flask and reduced down to 3 grams utilizing a rotary evaporator. 1-Methoxy-2-propanol (18 grams, commercially available from Aldrich of Milwaukee, WI) was added to the colloid and the mixture was reduced to 7 grams utilizing a rotary evaporator. 1-Methoxy-2-propanol (12 grams) was added to the colloid and the mixture was reduced utilizing a rotary evaporator to give final colloid with 8.1 weight percent metal oxide.

This colloid was mixed with 1.85 grams of a mixture of 30 weight percent SR 295 (trade designation for pentaerythritol tetraacrylate), 30 weight percent SR 506 (trade designation for isobornyl acrylate), and 40 weight percent SR 238 (trade designation for

1,6-hexanediol diacrylate) all commercially available from Sartomer Company, Inc. (Exton, PA). Tris(N-nitroso-N-phenylhydroxyl-aminato)aluminum (2 milligrams) available from First Chemical Corp. (Pascagoula, MS) was added to the mixture, which was then reduced utilizing a rotary evaporator to 3.83 grams. Thermogravimetric analysis
5 of the resin indicated 22.65% inorganic solids in the resin.

2,4,6-Trimethylbenzoyl-diphenyl-phosphine oxide liquid photoinitiator commercially available from BASF Corp. (Mount Olive, NJ) under the trade designation LUCIRIN LR 8893, was added at 1 percent to the resin that was then bar coated at 0.5
10 mils thickness onto a 0.125inch polymethyl methacrylate sheeting.

The coated sample was cured by passing the coated sample through a Fusion UV
10 Systems UV processor (VPS-6 power supply, EPIQ 6000 irradiator obtained from Fusion UV Systems, Corp. (Rockville, MD) that was equipped with a "D"-bulb on full power (600W/in) and operating at a line speed of 40 feet per minute (12.2 meters per minute).

The resultant cured coated film had a measured refractive index of 1.569.

15

What is claimed is:

1. A composition comprising a plurality of Ti/Sb mixed oxide nanoparticles in the form of an aqueous colloidal dispersion, wherein the Ti/Sb mixed oxide nanoparticles comprise a rutile-like crystalline phase.

2. A composition comprising agglomerated nanoparticles, wherein the agglomerated nanoparticles comprise Ti/Sb mixed oxide nanoparticles comprising a rutile-like crystalline phase.

3. The composition of claim 2, wherein the agglomerated nanoparticles are redispersible into a liquid vehicle.

4. A nanocomposite precursor comprising a plurality of nanoparticles homogeneously dispersed in an organic binder precursor, wherein the nanoparticles comprise Ti/Sb mixed oxide nanoparticles containing a rutile-like crystalline phase.

5. The nanocomposite precursor of claim 4, wherein the binder precursor comprises a polymerizable material.

6. The nanocomposite precursor of claim 5, wherein the polymerizable material comprises an acrylate monomer or oligomer.

7. The nanocomposite precursor of claim 6, wherein the binder precursor further comprises a photoinitiator or photocatalyst.

8. A nanocomposite comprising a plurality of nanoparticles dispersed in an organic binder, wherein the nanoparticles comprise Ti/Sb mixed oxide nanoparticles containing a rutile-like crystalline phase.

9. The nanocomposite of claim 8, wherein the binder comprises a polymerized acrylate monomer.

10. The nanocomposite of claim 8, wherein the binder further comprises a photoinitiator or photocatalyst.
11. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average nanoparticle size is less than 100 nanometers.
12. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average nanoparticle size is less than 40 nanometers.
13. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the weight ratio of titanium to antimony in the nanoparticles is in the range of from 0.14 to 11.30.
14. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the weight ratio of titanium to antimony in the nanoparticles is in the range of from 0.22 to 5.02.
15. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the weight ratio of titanium to antimony in the nanoparticles is in the range of from 0.42 to 2.93.
16. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average rutile-like crystalline phase content of Ti/Sb mixed oxide nanoparticles is at least 20 weight percent.
17. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average

rutile-like crystalline phase content of Ti/Sb mixed oxide nanoparticles is at least 40 weight percent.

18. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average rutile-like crystalline phase content of Ti/Sb mixed oxide nanoparticles is at least 60 weight percent.

19. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average rutile-like crystalline phase content of Ti/Sb mixed oxide nanoparticles is at least 80 weight percent.

20. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average rutile-like crystallite size is less than 20 nanometers.

21. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the ensemble average rutile-like crystallite size is less than 15 nanometers.

22. The composition of claim 1, the composition of claim 2, the nanocomposite precursor of claim 4, or the nanocomposite of claim 8, wherein the nanoparticles have at least one organic moiety bound to the nanoparticle surface.

23. A method for preparing an aqueous colloidal dispersion of Ti/Sb mixed oxide nanoparticles comprising the steps of:

- a) providing an aqueous titania precursor;
- b) providing an aqueous antimony oxide precursor;
- c) combining with mixing both aqueous precursors; and
- d) hydrothermally processing the mixture;

wherein the weight ratio of titanium to antimony is in the range of from 0.14 to 11.3.

24. The method of claim 23, wherein the aqueous titania precursor is the reaction product of hydrogen peroxide with a titanium alkoxide.

25. The method of claim 24, wherein the titanium alkoxide is titanium tetraisopropoxide.

26. The method of claim 23, wherein the aqueous antimony oxide precursor is colloidal HSb(OH)_6 .

27. The method of claim 23, further comprising the step of modifying the surface of the nanoparticles.

28. The method of claim 23, wherein the pH of the mixture is between 5 and 8.

29. The method of claim 23, further comprising the step of centrifuging the hydrothermally processed mixture.

30. The method of claim 23, wherein hydrothermally processing comprises passing the mixture through a stirred tube reactor.

31. The method of claim 30, further comprising the step of centrifuging the hydrothermally processed mixture.

1/1

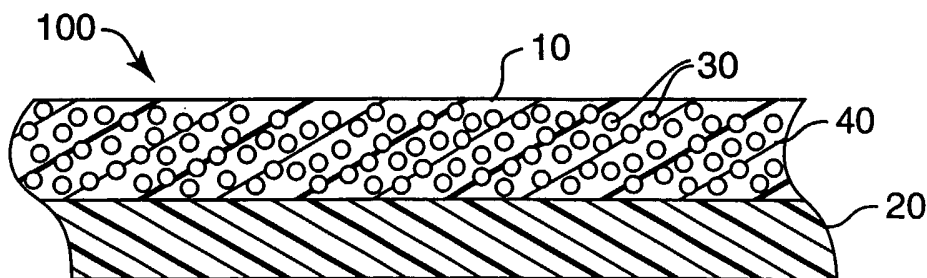


FIG. 1

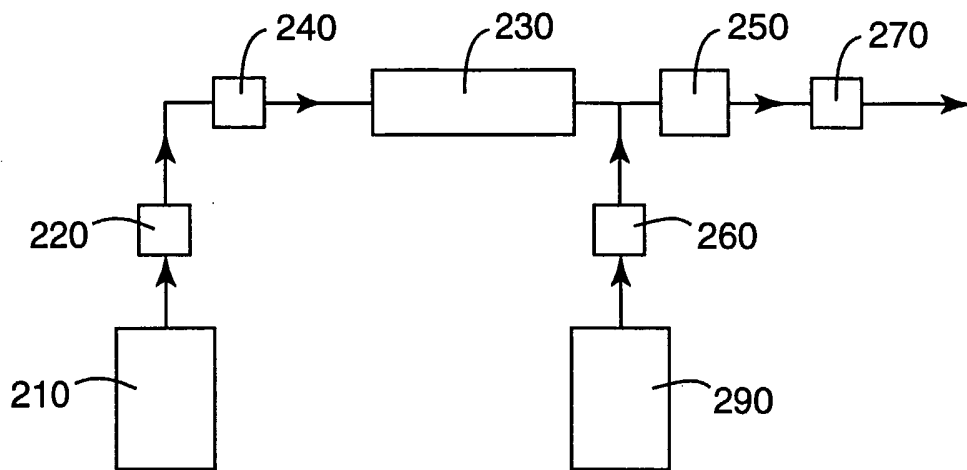


FIG. 2

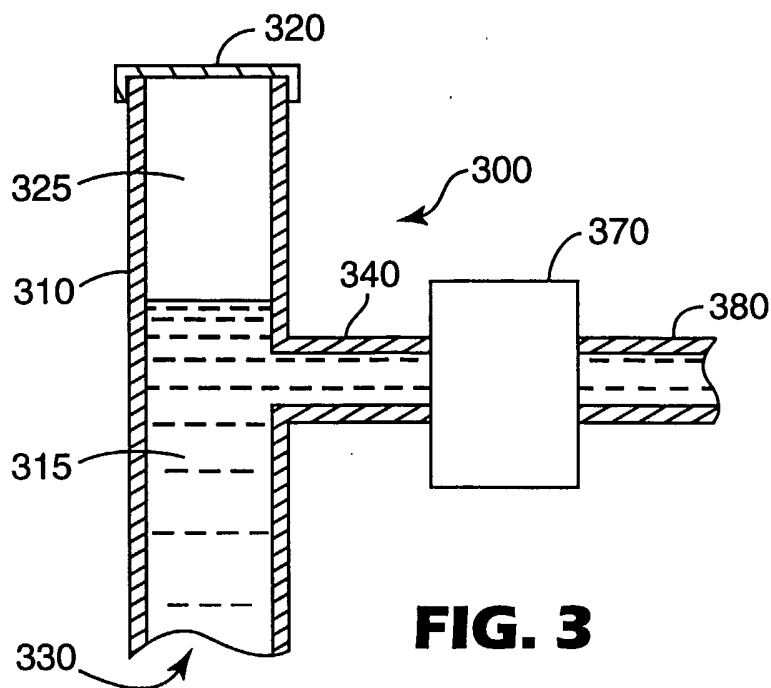


FIG. 3

INTERNATIONAL SEARCH REPORT

Intern: Application No

PCT/US 02/29392

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 7 C01G30/00 C08K3/22

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 C01G C08K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, INSPEC, COMPENDEX, PAJ, CHEM ABS Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 776 239 A (BRUNO SALVATORE ANTHONY) 7 July 1998 (1998-07-07) column 4, line 54 - line 62 column 5, line 39 -column 7, line 27 ---	1,2, 11-21,23
X	WO 00 44830 A (ALLIED SIGNAL INC) 3 August 2000 (2000-08-03) page 14, line 23 -page 17, line 14 page 21, line 11 -page 22, line 3 --- -/--	4-10

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

° Special categories of cited documents:

A document defining the general state of the art which is not considered to be of particular relevance

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L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

O document referring to an oral disclosure, use, exhibition or other means

P document published prior to the international filing date but later than the priority date claimed

T later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

X document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

Y document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

G document member of the same patent family

Date of the actual completion of the international search

13 December 2002

Date of mailing of the international search report

13/01/2003

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INTERNATIONAL SEARCH REPORT

Internat'l Application No

PCT/US 02/29392

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>DATABASE CA 'Online! CHEMICAL ABSTRACTS SERVICE, COLUMBUS, OHIO, US; VASILESCU, A. ET AL: "Sol-gel materials in TiO₂-Sb₂O₃ system" retrieved from STN Database accession no. 124:350104 XP002225004 abstract & ADVANCES IN SCIENCE AND TECHNOLOGY (FAENZA, ITALY) (1995), 3B(CERAMICS: CHARTING THE FUTURE), 717-724 ,</p>	1-3
A	<p>----- US 5 451 252 A (ELFENTHAL LOTHAR ET AL) 19 September 1995 (1995-09-19) the whole document -----</p>	1-3, 11-22

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 02/29392

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