A compression wave massage device for body parts is described, particularly for erogenous zones such as the clitoris, comprising a pressure field generation device (10), which shows at least one cavity (12) with a first end and a second end, located opposite the first end and distanced from said first end, with the first end being provided with at least one opening (8) for placement on a body part, and a drive device (20, 22), embodied to cause a change of the volume of at least one cavity (12) between a minimal volume and a maximal volume such that in at least one opening (8) a stimulating pressure field is generated. The particular feature of the invention is given in the fact that the cavity (12) is formed by a single chamber (14) and the ratio of the volume change to the minimal volume is not below 1/10, preferably not below 1/8.
Abstract

A compression wave massage device for body parts is described, particularly for erogenous zones such as the clitoris, comprising a pressure field generation device (10), which shows at least one cavity (12) with a first end and a second end, located opposite the first end and distanced from said first end, with the first end being provided with at least one opening (8) for placement on a body part, and a drive device (20, 22), embodied to cause a change of the volume of at least one cavity (12) between a minimal volume and a maximal volume such that in at least one opening (8) a stimulating pressure field is generated. The particular feature of the invention is given in the fact that the cavity (12) is formed by a single chamber (14) and the ratio of the volume change to the minimal volume is not below 1/10, preferably not below 1/8.
COMPRESSION WAVE MASSAGE DEVICE

The invention relates to a compression wave massage device for body parts, particularly erogenous zones such as the clitoris, comprising a device generating a pressure field, which shows at least one cavity with a first end and a second end, located opposite thereto and distanced from the first end, with the first end comprising at least one opening for placement on a body part and a drive device, which is embodied to generate a change of the volume of at least one cavity between a minimal volume and a maximal volume such that a stimulating pressure field is generated in at least one opening.

A device of the type mentioned at the outset is particularly known from DE 10 2013 110 501 A1. In this known device the cavity is formed by a first chamber and a second chamber. The second chamber shows an opening for placement on a body part or on an erogenous zone. The two chambers are connected to each other via a narrow connection channel. The drive device is embodied such that it only changes the volume of the first chamber, namely such that via the connection channel a stimulating pressure field is generated in the second chamber. This construction of prior art shows considerable disadvantages, though. The use with gliding gel or under water is impossible, since the lubricant or the water increases the throttle effect in the narrow connection channel to such an extent that the drive device is choked off. Additionally, the device of prior art fails to comply with the strict requirements of hygiene required here, since the connection channel due to its very narrow cross-section prevents any cleaning of the first chamber located at the inside so that contaminants and bacteria can accumulate there, which then cannot be removed.

The objective of the present invention is to provide a compression wave massage device of the type mentioned at the outset which shows a simple and simultaneously effective design, and additionally meets the strict requirements for hygiene.

This objective is attained in a pressure field generation device, which comprises at least one cavity with a first end and an opposite second end, located at a distance from the first end, with the first end comprising at least one opening for placement on a body part and a drive device, which is embodied to change the volume of at least one cavity between a minimal...
volume and a maximal volume such that a stimulating pressure field is generated in at least one opening, characterized in that the cavity is formed by a single chamber and the ratio of volume change to minimal volume is not below 1/10, preferably not below 1/8.

Accordingly, the invention is characterized in a single-chamber solution, which shows the advantages of a simpler construction, improved hygiene, particularly due to the ability of easier rinsing of the cavity according to the invention, formed by only a single chamber, and the easy handling with lubricant or under water.

Furthermore, according to the invention the ratio of the minimal volume to the volume change shall not exceed 10, particularly not exceed 8, since it was found that otherwise the suction effect becomes too low. Here, the volume change refers to the difference between the maximal volume and the minimal volume. The volume of the cavity is defined as the volume of a chamber which ends in the proximity of the opening in a virtually planar area, which virtually closes the opening.

Preferred embodiments and further developments of the invention are disclosed in the dependent claims.

Preferably the ratio of minimal volume to volume change should not be below 1, and preferably not below 2, since according to the invention it was found that otherwise the required power of the drive device becomes excessive and on the other hand the vacuum at the opening becomes too strong and perhaps even painful.

When using a flexible membrane, to be set into a reciprocal motion by the drive device, for the alternating generation of vacuum and pressure, here the minimal volume of the cavity is defined as the volume when the opening of the cavity is virtually closed with a planar area and the membrane is in an operating stage and/or a position with the shortest distance from the opening. On the other hand, the maximal volume of the cavity of the chamber is defined as the volume when the opening of the cavity is virtually closed with a planar area and the membrane is in an operating stage and/or a position showing the greatest distance from the opening. In order for the air flow to remain essentially unchanged over the entire length of the cavity of the chamber or to be at least almost consistent, preferably the cross-section of
the cavity of the chamber, defined perpendicular to the length between its two ends, should be unchanged or at least almost constant over the entire length between its two ends. The cross-section is preferably understood as defining the cross-sectional shape and/or the cross-sectional area.

The cavity of the chamber can preferably show essentially the form of a rotary body with a circular or elliptic cross-section.

Additionally, for generating a homogenous, unhindered and thus effective airflow it is advantageous when preferably the side wall of the chamber, limiting the cavity and connecting its two ends to each other, is free from discontinuous sections.

Beneficially the cavity of the chamber may show the form of a continuous tube.

Preferably the cross-section of the opening is essentially equivalent to the cross-section of the cavity of the chamber.

It has proven particularly advantageous to size the ratio of the width of the cavity of the chamber, defined perpendicular to its longitudinal extension, to the length of the cavity of the chamber, defined in the direction of its longitudinal extension, from 0.1 to 1.0, preferably from 0.2 to 0.6, particularly preferred from 0.38 to 0.4.

Preferably the cavity of the chamber is closed at its inner, second end with a flexible membrane which extends essentially over the entire cross-section of the cavity and is moved by the drive device alternating in the direction towards the opening and the direction opposite thereto. With such a construction the stimulating pressure field can be generated in a particularly simple and simultaneously effective fashion in the cavity of the single chamber provided according to the invention.

For reasons of hygiene, it is further advantageous if particularly the section of the chamber showing the opening is provided as an interchangeable socket, with its inner lateral wall forming a section of the lateral wall of the cavity leading towards the opening. Beneficially the socket should be made from a flexible material, preferably silicone.
In a further development of the preferred embodiment stated above the inner lateral wall of the socket should essentially be aligned to the other section of the lateral wall of the cavity such that any points of discontinuation between the socket and the inner section of the cavity of the chamber is avoided.

In an alternative further development of the above-stated preferred embodiment the inner lateral wall of the socket forms an essentially continuous lateral wall of the cavity, connecting the first end with the second end, and thus a lateral wall of the cavity connecting the opening of the socket with the membrane, and the socket together with the membrane form a one-piece component. Such a preferred further development offers, based on the one-piece connection of the socket and the membrane, a particularly easily produced design and additionally has advantages with regards to hygiene, because the entire component comprising membrane and socket can be exchanged, which is possible only with the one-chamber solution realized according to the invention.

Preferably the pressure field shall show a pattern of relative vacuum and pressure stages, which are modulated upon a reference pressure, preferably normal pressure. Beneficially the value of the overpressure in reference to normal pressure is lower than the value of the relative vacuum in reference to normal pressure, and measures preferably no more than 10% of the value of the relative vacuum. It has been found that under normal conditions of use, when the compression wave massage device, placed with its opening on the body part to be stimulated, is not impinged by excessive compression, potentially developing relative overpressure can largely dissipate so that already for this rather factual considerations, the focus must be given to a pressure field to be modulated primarily in the vacuum range. For this reason, it is alternatively also possible that the pressure field comprises a pattern of only relative vacuum stages, which are modulated on a reference pressure, for example normal pressure. In another preferred further development the pressure field is generated with an essentially sinusoidal periodic pressure progression, with the drive device here being required to cause a regular change of the volume of the cavity, for example with the help of an eccentric mechanism.
Preferably a control device may be provided, which controls the drive device and shows at least one control means by which the respective modulation of the pressure field can be adjusted.

Beneficially the device should be embodied as a manual device, preferably driven by a battery.

In the following, a preferred exemplary embodiment of the invention is explained in greater detail based on the attached drawings. Here it shows:

Fig. 1  a perspective side view of the compression wave massage device according to the invention in a preferred embodiment;

Fig. 2  a front view of the compression wave massage device of Fig. 1;

Fig. 3  a longitudinal section through the compression wave massage device of Fig. 1;

Fig. 4  an enlarged detail of the longitudinal section of Fig. 3 in the head section of the compression wave massage device of Fig. 1; and

Fig. 5  a compression wave progression preferably generated by the compression wave massage device of Fig. 1.

The preferred embodiment of the compression wave massage device 1 shown in the figures comprises an oblong housing 2 with a first end section 2a, an opposite second end section 2b, and a central section 2c located therebetween. Preferably the housing is made from plastic. As discernible from the figures 1 to 3, in the exemplary embodiment shown the two end sections 2a and 2b are rounded and taper slightly towards the central section 2c, which is embodied slightly narrower. At the first end section 2a of the housing 2 a projection 4 is formed, protruding perpendicular in reference to the longitudinal extension of the housing 2 and forming together with the first end section 2a of the housing 2 a head of the compression wave massage device 1, while the second end section 2b of the housing 2 preferably serving as the handle in order to hold the compression wave massage device 1 during application, described in greater detail in the following.
As further discernible from Fig. 1, in the direction of its longitudinal extension the housing 2 is composed of two half shells, with one of the half shells being provided with the above-mentioned projection 4. The two half shells of the housing 2, not marked in greater detail in the figures, are preferably glued to each other; alternatively it is also possible to connect the two half shells of the housing 2 in a different way, namely for example using screws or other fastening means arranged at the interior sides.

As particularly discernible from Figs. 1, 3, and 4, a socket 6 is located on the projection 4, which shows an opening discernible in Figs. 2 to 4 and marked with the reference character “8”. Preferably the socket 6 is made from a soft and/or flexible plastic material, such as silicone.

In the head of the compression wave massage device 1, formed by the first end section 2a of the housing 2 and the projection 4, a compression wave generation device 10 is located, by which a stimulating pressure field is generated with the help of the opening 8. As particularly discernible in detail from Fig. 4, the pressure field generation device 10 comprises a cavity 12 with an exterior first end 12a and an inner second end 12b, opposite the first end 12a and located distanced from the first end 12a, with the first end 12a simultaneously also forming the opening 8 in the socket 6. The cavity 12 is formed by a single continuous chamber 14 and is limited by an inner or lateral wall 12c connecting its two ends 12a, 12b to each other. As discernible from Figs. 3 and 4, the socket shows an exterior section 6a by which it can be detachably fastened to the projection 4, and an inner section 6b, with the exterior section 6a and the inner section 6b of the socket 6 being connected to each other in the proximity of the opening 8. The inner section 6b of the socket 6 is formed like a sheath and limits an exterior section of the cavity 12 leading to an exterior first end 12a. This way, the inner wall of the sheath-shaped inner section 6b of the socket 6 forms simultaneously an exterior section 12c1 of the inner or lateral wall 12c of the cavity 12, leading to the opening 8. Further, in the exemplary embodiment shown the cavity 12 is limited by an interior annular element 16, with its inner wall simultaneously forming the other inner section 12c2 of the lateral wall 12c of the cavity 12. Accordingly, in the
exemplary embodiment shown the continuous single chamber 14 is composed of the sheath-shaped inner section 6b of the socket 6 and the annular element 16.

Alternatively it is also possible, for example, that the annular element 16 is omitted and instead the sheath-shaped inner section 6b of the socket 6 is extended to the membrane 18 and is connected to the membrane 18 to a joint, one-piece component such that the inner wall of the sheath-shaped inner section 6b of the socket 6 would form in this case the entire lateral wall 12c of the cavity 12.

As further discernible in Figs 3 and 4, the arrangement of the socket 6 and the annular element 16 is rendered such that the first section 12c1 of the cavity 12 is aligned to the second section 12c2 of the cavity 12 such that the lateral wall 12c of the cavity 12 is free from any discontinuities. The cavity 12 of the chamber 14 essentially shows the form of a rotary body with a circular cross-section, with the cross-section of the cavity 12, defined perpendicular to its length L between the two ends 12a, 12b, in the exemplary embodiment shown essentially being almost constant over the entire length L between the two ends 12a, 12b and only expanding slightly towards the opening 8 such that the opening cross-section of the opening 8 is almost equivalent to the cross-section of the cavity 12. Alternatively it is also possible for example to provide the cavity 12 with an elliptic cross-section. Thus, the chamber 14 shows a continuous tube with a cross-section almost identical over its entire length, with in the exemplary embodiment shown the cavity being aligned in the direction of its length L approximately perpendicular to the longitudinal extension of the housing 2.

In the exemplary embodiment shown the ratio of the width of the cavity 12, defined perpendicular to its longitudinal extension, to the length L of the cavity 12, defined in the direction of its longitudinal extension, values to approximately 0.39. However, other values are also possible for the ratio of diameter or width to length of the cavity 12 of the chamber 14 from 0.1 to 1.0.

As further discernible from Figs. 3 and 4, the cavity 12 is closed at its inner second end 12b with a flexible membrane 18, preferably produced from silicone, which extends over the entire cross-section of the cavity 12 and is driven via the mechanism 20 by a drive engine.
22. Here the mechanism 20 is embodied such that the rotary motion of the output shaft 22a of the drive engine 22 is converted into a reciprocal longitudinal motion, causing the membrane 18 to be set in motion perpendicular to the level stretched, alternatively in the direction towards the opening 8 and opposite thereto. This way, the volume of the cavity 12 of the chamber 14 is altered depending on the rotation of the output shaft 22a of the drive engine 22. Preferably the mechanism 20 shows an eccentric or a con rod in order to convert the rotary motion of the output shaft 22a of the drive engine 22 into a reciprocal longitudinal motion for the reciprocal deflection of the membrane 18. In general, other forms of drives are also possible, which cause a deflection of the membrane 18 for changing the volume of the cavity 12. The reciprocal motion of the membrane 18 causes thereby a change of the volume of the cavity 12 between a minimal volume and a maximal volume such that a stimulating pressure field is generated in the opening 8. This can occur for example also in an electromagnetic, piezo-electric, pneumatic, or hydraulic fashion. However the arrangement must be made such that the ratio of the volume change to the minimal volume is not below 1/10 and preferably not below 1/8, so that the ratio of minimal volume to volume change is not exceeding 10, and preferably not exceeding 8, because otherwise during the motion of the membrane 18 in the direction away from the opening 8 the suction effect becomes too low. Further, preferably the arrangement should also be rendered such that the ratio of volume change to minimal volume is not greater than 1, and preferably not exceeding ½ so that the ratio of minimal volume to volume change is not below 1 and preferably not below 2, because otherwise on the one hand the power requirement of the drive engine 22 becomes excessive and on the other hand excessive vacuum develops during the motion of the membrane 18 in the direction away from the opening 8. This way, with the help of the flexible membrane 18 driven by the drive engine 22 alternating vacuum and overpressure stages are generated in the cavity 12 of the chamber 14.

The volume of the cavity 12 is defined as the volume of the chamber 14 which ends in the proximity of the opening 8 at a virtual planar area, which virtually closes the opening 8 when the membrane 18 is in its normal and/or middle position. The minimal volume of the cavity 12 is defined such that the opening 8 of the cavity 12 is virtually closed with a planar area and the membrane 18 is in a position with the shortest distance from the opening 8 and
thus in its maximally deflected state in the direction towards the opening 8. The maximal volume of the cavity 12 is defined here such that the opening 8 of the cavity 12 is virtually closed with a planar area and the membrane 18 is in a position with the greatest distance from the opening 8 and thus at a stage maximally deflected away from the opening 8.

As further discernible from Figs. 3 and 4, the drive engine 22, which in the described exemplary embodiment represents an electric motor, is connected via an electric cable 24 to an electric control circuit board 26, controlling the drive engine 22. As further discernible from Fig. 3, via an electric cable 28 a batter 30 is connected to the control circuit board 26, which provides the drive engine 22 and the control circuit board 26 with the required electric power. The battery 30 may optionally represent a battery that cannot be recharged or also a rechargeable accumulator. While in the exemplary embodiment shown the drive engine 22 is arranged in the connection area between the narrow central section 2c of the housing 2 and the first end section 2a of the housing 2 and thus adjacent to the head of the compression wave massage device 1 formed by the first end section 2a of the housing 2 and the projection 4, the battery 30 is arranged in the second end section 2b of the housing 2, resulting in the housing 2 being well balanced when the compression wave massage device 1 is held manually by the user.

As further discernible from Figs. 1 and 3, a power switch 32 is provided, with can be operated from the outside of the housing 2 to switch the compression wave massage device 1 on or off and is arranged in the narrow central section 2c of the housing 2. A sensor 34 is also arranged in the narrow, central section 2c of the housing 2, to be operated from the outside, by which the various operating conditions of the compression wave massage device 1 can be adjusted, and a control light 36 is arranged there, preferably embodied as a light diode visible from the outside. The power switch 32 and the sensor 34 are arranged directly on the control circuit board 26 fastened below the wall of the housing 2, while the control light 36 is connected via an electric cable, not shown in the figures, to the control circuit board 26.

In addition to the control of the drive engine 22, in the exemplary embodiment shown, the electric control circuit board 26 also assumes the charge management of the battery 30. For
this purpose, the control circuit board 26 is connected via an electric cable 38 to the charge contacts 40 arranged at the face of the second end section 2b of the housing 2 and accessible from the outside, as discernible from Figs. 1 to 3. An external charging device, not shown in the figures, can be connected to these connections 40 via a plug with magnetic plug-in contacts, which can be made to contact the connection contacts 40 to establish an electric connection based on magnetic forces.

The compression wave massage device 1 described is embodied as a hand-held device and for the application it is placed with the socket 6 onto a body part to be stimulated, not shown in the figures, such that in the proximity of the opening 8 of the socket 6 it is essentially surrounded. During operation of the compression wave massage device 1 then the body part to be stimulated is alternating subjected to different air pressures caused by the reciprocal motion of the membrane 18. Under normal application conditions, when no excessive pressures are applied after the placement of the compression wave massage device 1 with its socket 6 on the body part to be stimulated, relative pressures perhaps can largely dissipate which arise during the respective motion of the membrane 18 in the direction towards the opening 8 so that therefore essentially the pattern develops shown in Fig. 5 of a modulated relative vacuum in reference to the normal air pressure $P_0$. However, as discernible from the pressure progression of Fig. 5, here relative overpressures can occur in the maximum in reference to normal pressure $P_0$, which are considerably lower than the minima of the relative vacuum. Usually the value of the relative overpressure in reference to the normal pressure $P_0$ amounts to no more than 10% of the value of the relative vacuum in reference to the normal pressure $P_0$. Alternatively it is also possible that the pressure field only comprises a pattern of relative vacuum conditions, which are modulated on the normal pressure $P_0$ (quasi from the bottom). In particular when the mechanism 20 comprises an eccentric, the sinusoidal periodic pressure progression develops shown in Fig. 5.

Due to the fact that the cross-section of the cavity 12 of the chamber 14, as already described, is essentially almost constant over the entire length $L$, this results during operation in the air flow over the entire length $L$ of the cavity 12 essentially remaining constant as well. This way a particularly effective air flow can be generated for an effective
stimulation of the body part to be stimulated with relatively low energy consumption of the drive engine 22.

The control circuit board 26 preferably shows a memory, not shown in the figures, in which various modulation patterns are saved. By an appropriate operation of the sensor 34, here a desired modulation pattern can be selected in order to control the drive engine 22 accordingly.
Claims

1. A pressure wave massage device for the clitoris comprising:
   a pressure field generation device (10) and a drive device (20, 22),
   the pressure field generation device (10) comprising a cavity (12), the
   cavity (12) having a first end (12a) and a second end (12b), the first end
   (12a) being provided with an opening (8) for placement over the clitoris
   and the second end (12b) being located opposite the first end (12a) and
   distanced from the first end (12a),
   wherein
   the cavity (12) is limited by a lateral wall (12c) connecting the first
   end (12a) with the second end (12b) and is closed at the second end
   (12b) with a flexible membrane (18);
   the flexible membrane (18) essentially extends over the entire
   cross-section of the cavity (12);
   the drive device (20, 22) moves the flexible membrane (18) alternating
   in the direction towards the opening (8) and opposite thereto; and
   the drive device (20, 22) is embodied to generate a change of the
   volume of the cavity (12) between a minimal volume and a maximal vol-
   ume such that a stimulating pressure field is generated in the opening (8);
   the cavity (12) is formed by a single continuous chamber (14);
   the lateral wall (12c) of the chamber (14) limiting the cavity (12)
   and connecting its two ends (12a, 12b) to each other is free from discon-
   tinuations; and
   a ratio of the volume change of the cavity (12) to the minimal vol-
   ume of the cavity (12) is not below 1/10 and not greater than 1.

2. A device according to claim 1, characterized in that the flexible membrane
   (18) is made from silicone.

3. A device according to any one of claim 1 or 2, characterized in that a
   cross-section of the cavity (12) of the chamber (14) defined perpendicular
   to a length (L) between the two ends (12a, 12b) is essentially unchanged
   or at least almost consistent over the entire length (L) between the two
   ends (12a, 12b) such that air flow is essentially unchanged or at least al-
   most consistent over the entire length (L) of the cavity (12) of the chamber
   (14).
4. A device according to any one of claims 1 to 3, characterized in that the cavity (12) of the chamber (14) is essentially shaped as a rotary body with a circular or elliptic cross-section.

5. A device according to any one of claims 1 to 4, characterized in that the cavity (12) of the chamber (14) is shaped as a continuous tube.

6. A device according to any one of claims 1 to 5, characterized in that the opening cross-section of the opening is essentially equivalent to the cross-section of the cavity (12) of the chamber (14).

7. A device according to any one of claims 1 to 6, characterized in that a ratio of a width of the cavity (12) of the chamber (14), defined perpendicular to a longitudinal extension of the cavity (12) of the chamber (14) to a length (L) of the cavity (12) of the chamber (14), defined in the direction of its longitudinal extension, ranges from 0.1 to 1.0.

8. A device according to any one of claims 1 to 6, characterized in that a ratio of a width of the cavity (12) of the chamber (14), defined perpendicular to a longitudinal extension of the cavity (12) of the chamber (14), to a length (L) of the cavity (12) of the chamber (14), defined in the direction of its longitudinal extension, ranges from 0.2 to 0.6.

9. A device according to any one of claims 1 to 6, characterized in that a ratio of a width of the cavity (12) of the chamber (14), defined perpendicular to a longitudinal extension of the cavity (12) of the chamber (14), to a length (L) of the cavity (12) of the chamber (14), defined in the direction of its longitudinal extension, ranges from 0.38 to 0.4.

10. A device according to any one of claims 1 to 9, characterized in that the section of the chamber (14) comprising the opening (8) is provided as an exchangeable socket (6) with its inner lateral wall forming the section (12c1) of the lateral wall (12c) of the cavity (12) leading towards the opening (8).
11. A device according to claim 10, characterized in that the socket (6) is made from a flexible material.

12. A device according to claim 11, characterized in that the flexible material is silicone.

13. A device according to any one of claim 11 or 12, characterized in that the section (12c1) of the lateral wall (12c) of the cavity (12), formed by the inner lateral wall of the socket (6) and leading to the opening (8), is essentially aligned to the remaining section (12c2) of the lateral wall (12c) of the cavity (12).

14. A device according to any one of claims 10 to 12, characterized in that the inner lateral wall of the socket (6) essentially forms entirely the lateral wall (12c) of the cavity (12) connecting the first end (12a) to the second end (12b) of the cavity and thus the opening (8) to the membrane (18) and the socket (6) jointly with the membrane (18) being combined to a one-piece component.

15. A device according to any one of claims 1 to 14, characterized in that the stimulating pressure field shows a pattern of relative vacuum and over-pressure stages, which are modulated on a reference pressure.

16. A device according to claim 15, characterized in that the reference pressure is a normal pressure (P).

17. A device according to claim 16, characterized in that the value of the relative overpressure in reference to the normal pressure (P₀) is below the value of the relative vacuum in reference to the normal pressure (P₀).

18. A device according to claim 17, characterized in that the value of the relative overpressure in reference to the normal pressure (P₀) amounts to no more than 10% of the value of the relative vacuum in reference to the normal pressure (P₀).
19. A device according to any one of claims 1 to 14, characterized in that the stimulating pressure field shows a pattern of relative vacuum stages, which are modulated on a reference pressure.

20. A device according to claim 19, characterized in that the reference pressure is a normal pressure ($P_0$).

21. A device according to any one of claims 15 to 20, characterized in that the stimulating pressure field shows an essentially sinusoidal periodic pressure progression.

22. A device according to any one of claims 1 to 21, characterized in a control device (26, 32, 34) which controls the drive device (20, 22) and comprises at least one control means (32, 34) by which the respective modulation of the stimulating pressure field can be changed.

23. A device according to any one of claims 1 to 22, characterized in that the device is a handheld device.

24. A device according to claim 23, characterized in that the device is operated by a battery (30).

25. A device according to any one of claims 1 to 24, characterized in that the ratio of the volume change to the minimal volume is not below 1/8.

26. A device according to any one of claims 1 to 25, characterized in that the ratio of the volume change to the minimal volume is not greater than 1/2.