BIOCOMPATIBLE SOLID-PHASE MICROEXTRACTION COATINGS AND METHODS FOR THEIR PREPARATION

Abstract

A biocompatible coating, such as for a fiber, for solid phase microextraction (SPME) of a small molecule of interest from a matrix, with the coating having an extraction phase including SPME particles having pores dimensioned to absorb the small molecule of interest from the matrix and a biocompatible polymer being a polyacrylonitrile (PAN) or a co-polymer of polyacrylonitrile (PAN) that completely covers the SPME particles and homogeneously distributing the SPME particles therein and having reduced adsorption of proteins or macro-molecules onto the SPME particles and allowing the SPME particles to extract the small molecule of interest from the matrix.
Fig. 2

Comparative extraction time profile for verapamil
Calibration curve for loperamide in PBS and human plasma

Fig. 3
BIOCOMPATIBLE SOLID-PHASE MICROEXTRACTION COATINGS AND METHODS FOR THEIR PREPARATION

CROSS-REFERENCE TO RELATED APPLICATIONS


FIELD

[0002] The present disclosure relates to the extraction of small molecules of interest from a matrix, and in particular, to methods of preparation and use of biocompatible coatings and coated devices for sampling devices used for extracting components of interest in a biological matrix for further quantification or identification.

BACKGROUND

[0003] Presently, if one wants to accurately assess the concentrations of chemicals or drugs inside a living animal, a sample of the blood or tissue to be studied is removed from the animal and taken to an analytical laboratory to have the chemicals of interest extracted and quantified. Typically, a first step is a pre-treatment of the sample to convert it to a form more suitable for chemical extraction. In the case of blood, this may be by the removal of blood cells and/or some blood components by the preparation of serum or plasma. In the case of a tissue sample, this may be by many processes, including: freezing, grinding, homogenizing, enzyme treatment (e.g. protease or cellulase) or hydrolysis. Subsequently, compounds of interest are extracted and concentrated from the processed sample. For example serum samples may be subjected to liquid-liquid extraction, solid phase extraction or protein precipitation, followed by drying and reconstitution in an injection solvent. A portion of the injection solvent is introduced to an analytical instrument for chromatographic separation and quantification of the components. This method produces accurate results with high specificity for the compound of interest, but is time consuming and labor intensive. Also, because of the large number of steps in the process there is a significant chance of errors in sample preparation impacting the results. This method has good sensitivity and selectivity for the target compounds but is limited in that the chemical balance inside the animal is disrupted during sampling. In many cases, this disruption reduces the value of the results obtained, and in some cases makes this technique inappropriate for the analysis. Where the removed blood volume is a high proportion of the total blood volume of the animal, as is commonly the case when mice are used, the death of the animal results. This means that a different animal must be used for each data point and each repeat. By eliminating the need for a blood draw in this case, fewer animals would be required for testing and a significant improvement in inter-animal variation in the results would be achieved.

[0004] Alternatively, biosensors have been developed for some applications of analysis of chemical concentrations inside animals. In this case, a device consisting of a specific sensing element with an associated transducer is implanted. The device produces a signal collected by an electronic data logger that is proportional to the chemicals to which the sensor responds. The main limitations of this type of device are that they normally respond to a spectrum of chemicals rather than having specificity for only one chemical. Of the spectrum of chemicals to which the sensor responds, some produce a greater and some a lesser response. Sensors are also susceptible to interferences where another chemical present in a system interferes with the response produced by the target chemicals. It is for these reasons that biosensors are normally limited in terms of accuracy and precision. Additionally, biosensors are typically not as sensitive to low chemical concentrations as state-of-the-art, stand-alone, detectors. Such detectors, for example mass spectrometers, are used in the above mentioned conventional analysis techniques and in solid phase microextraction.

[0005] Microextraction is a significant departure from conventional "sampling" techniques, where a portion of the system under study is removed from its natural environment and the compounds of interest extracted and analyzed in a laboratory environment. As with any microextraction, compounds of interest are not exhaustively removed from the investigated system, and conditions can be devised where only a small proportion of the total amount of compound, and none of the matrix, are removed. This avoids disturbing the normal balance of chemical components. This could have a benefit in the non-destructive analysis of very small tissue sites or samples. Because extracted chemicals can be separated chromatographically and quantified by highly sensitive analytical instruments, high accuracy, sensitivity and selectivity are achieved.

[0006] With current commercially available solid phase microextraction (SPME) devices, a stationary extraction phase is coated onto a fused silica fiber. The coated portion of the fiber is typically about 1 cm long and coatings have various thicknesses. The fiber can be mounted into a stainless steel support tube and housed in a syringe-like device for ease of use. Extractions are performed by exposing the extraction phase to a sample for a pre-determined time to allow sample components to come into equilibrium with the extraction phase. After extraction, the fiber is removed to an analytical instrument (typically a gas or liquid chromatograph) where extracted components are desorbed and analysed. The amount of a component extracted is proportional to its concentration in the sample (J. Pawliszyn “Method and Device for Solid Phase Microextraction and Desorption”, U.S. Pat. 5,691,206.).

[0007] To date, commercial SPME devices have been used in some applications of direct analysis of living systems. For example they have been applied for the analysis of airborne pheromones and semiochemicals used in chemical communications by insects (Moneti, G.; Dani, F. R.; Pieraccini, G.T.S. Rapid Commun. Mass Spectrom. 1997, 11, 857-862),
(Frerot, B.; Malosse, C.; Cain, A. H. J. High Resolut. Chromatogr. 1997, 20, 340-342.) and frogs (Smith, B. P.; Zini, C. A.; Pawliszyn, J.; Tyler, M. J.; Hayasaka, Y.; Williams, B.; Caramao, E. B. Chemistry and Ecology 2000, 17, 215-225) respectively. In these cases, the living animals were non-invasively monitored over time by assessing the chemical concentrations in the air around the animal, providing a convenient means to study complicated dynamic processes without interference.

[0008] The current commercial devices do, however, have some limitations for in vivo and in vitro analysis of a biological matrix, such as blood or tissue. Firstly, the most difficult and undesirable problem is the adsorption of proteins and other macromolecules on the surface of SPME fibers. Macromolecules are understood to be biological components with a molecular mass greater than about 10,000 atomic mass units. These macromolecules constitute a diffusion barrier and decrease the extraction efficiency in subsequent experiments. In order to transfer all SPME advantages to the field of in vivo and in vitro analysis of biological samples, it is imperative to develop new biocompatible devices suitable for extracting compounds from biological matrices.


[0010] Polymers such as polypyrroles, derivatised cellulose, polysulfones, poly(acrylonitrile) (PAN), poly(ethylene glycol) and polyamides are currently used to prepare biocompatible membranes used for separation of sub-micron particles in biomedical applications. PAN has been widely used as membrane material in the fields of dialysis and ultrafiltration. It has been found that its properties can be fine-tuned by using specific co-monomers. The terms "polyacrylonitrile" and "PAN" are used herein to refer to homopolymers as well as copolymers of acrylonitrile containing at least about 85% by weight acrylonitrile and up to about 15% by weight of at least one other ethylenically unsaturated compound copolymerizable with acrylonitrile. For example, PAN can be tailored with a reactive group for enzyme immobilization. Furthermore, some co-monomers lead to improved mechanical strength, solvent resistance, high permeation flux, and biocompatibility. Accordingly, PAN-based membranes have great potential for the treatment of wastewater, the production of ultra-pure water, hemodialysis in artificial kidneys, and biocatalysis with separation. PAN is one of the most important polymers used in the biomedical area because of its exceptional qualities, such as good thermal, chemical, and mechanical stability as well as biocompatibility. Membranes made of PAN are widely used as dialyzers able to remove low to middle molecular weight proteins and for high-flux dialysis therapy. PAN is one of the best polymers in terms of biocompatibility.

[0011] However, good extractive materials are generally not biocompatible and PAN is not appropriate as an extractive material for SPME.

[0012] It is, therefore, desirable to provide a biocompatible composition able to extract small molecules from a matrix for use with solid phase microextraction devices, as well as a process for coating SPME fibers with said composition.

SUMMARY

[0013] The inventors of the present disclosure conceived of a method to obviate or mitigate at least one disadvantage of previous biocompatible compositions for solid phase microextraction devices.

[0014] According to one aspect, a process for coating a fiber with a biocompatible coating for use of the fiber in solid phase microextraction (SPME) of a small molecule of interest from a matrix. The process includes the step of coating the fiber with a coating of a biocompatible polymer and a solvent having solid phase microextraction (SPME) particles with pores dimensioned to absorb the small molecule of interest from the matrix suspended therein. The process also includes the steps of drying the coated fiber to remove the solvent and curing the dried coated fiber at an elevated temperature.

[0015] According to another aspect, a process for preparing a device for use in solid phase microextraction (SPME) of a small molecule of interest from a biological matrix. The process includes identifying the small molecule of interest to be extracted from the matrix and selecting extraction phase SPME particles having pores dimensioned to absorb the identified small molecule of interest from the matrix. The process also includes the process step of selecting a biocompatible polymer for suspending the SPME particles wherein the selection of the biocompatible polymer being responsive to the biocompatible polymers characteristic to reduce the adsorption of proteins and macromolecules onto the suspended SPME particles while allowing the SPME particles to extract the small molecule of interest from the matrix. The process further includes the steps of selecting a solvent for combining with the selected biocompatible polymer, dissolving the selected biocompatible polymer in the selected solvent and combining the selected SPME particles with the combination of the dissolved biocompatible polymer and the solvent to form a solid phase microextraction (SPME) coating solution.

[0016] Other aspects and features of the present disclosure will become apparent to those ordinarily skilled in the art upon review of the following description of specific embodiments in conjunction with the accompanying figures.

BRIEF DESCRIPTION OF THE DRAWINGS

[0017] Embodiments will now be described, by way of example only, with reference to the attached Figures, wherein:

[0018] FIG. 1A shows a scanning electron micrograph image, at 100x magnification, of a fiber coated with a coating of an exemplary embodiment.

[0019] FIG. 1B shows the scanning electron micrograph image at 1000x magnification.
FIG. 2 shows comparative extraction profiles over time for non-coated SPME fibers and SPME fibers that are coated with a biocompatible coating.

Fig. 3 shows calibration curves for extraction of loperamide, in two different matrices, using a coating of an exemplary embodiment.

DETAILED DESCRIPTION

One embodiment relates to coatings which can be used for direct microextraction of small molecules from a biological matrix, such as fluids or tissues. The biological fluids can be whole blood, serum, plasma, cerebrospinal fluid, peritoneal fluid, saliva or urine. The tissue could be, for example, isolated cells or organs. The small molecules can be drugs. The small molecules can be hydrophobic or hydrophilic and should generally weigh less than 10,000 atomic mass units. The small molecules can be drugs or biomarkers. A biomarker is a physiological substance that when present in abnormal amounts may indicate the presence of disease. The coatings can be prepared by covering flexible fibers with a suspension of various extractive particles (for example: C18-silica, RP-amide/silica, HS-F5/silica) in a polyacrylonitrile (PAN), polyethylene glycol, polypyrrole, derivatized cellulose, polysulfone, or polyamide solution. C18-silica particles would be understood by one of skill in the art to comprise silica particles derivatized with a hydrophobic phase, the hydrophobic bonded phase comprising octadecyl. For RP-amide/silica particles, the bonded phase comprises palmitamido-propyl. For HS-F5-silica particles, the bonded phase comprises pentadecafluorophenyl-propyl. The particles can be about 1.7 to about 50 μm particles. Preferably, the particles can be about 2 to about 20 μm particles. Preferably, the particles can be about 3 to about 10 μm particles. More preferably, the particles can be about 3 to about 7 μm particles. The particles can be spherical. The pore size diameter can be about 10 to about 200 Å. Preferably, the pore size can be about 100 to about 180 Å. The surface area can be about 200 m²/g to about 800 m²/g. Preferably, the surface area can be about 200 m²/g to about 300 m²/g.

It would be understood by a person of skill in the art that appropriate coatings can be formed with other extractive materials, and particularly with any extractive particles currently used in solid phase extraction or affinity chromatography (e.g. high pressure liquid chromatography), depending on the nature of the compound being extracted, in a similar manner than affinity chromatography relies on different particles for separating various compounds. For example, other particles could include such particles as: normal-phase silica, C1/silica, C4/silica, C6/silica, C8/silica, C30/silica, phenyl/silica, cyano/silica, diol/silica, ionic liquid/silica, molecular imprinted polymer particles, carbonbox 1006 or divinylbenzene. Mixtures of particles can also be used in the coatings. The particles can be inorganic (e.g. silica), organic (e.g. carbonbox or divinylbenzene) or inorganic/organic hybrid (e.g. silica and organic polymer). Furthermore, a person of skill in the art would understand that other bioactive polymeric materials could be used as glue or support. PAN can also be used for covering existing commercial extraction phases (for example: carbowax/templated resin) with a biocompatible layer.

It would be readily understood by one of skill in the art that the diameter of a fiber for SPME can be of millimeter to nanometer dimensions. Preferably, the diameter of a fiber can be between 0.1 millimeters and 0.6 millimeters. More preferably, the diameter of a fiber can be about 0.13 millimeters (0.005 inches). The wire can be formed of any acceptable material that would be amenable for use in a biological matrix. Such material may include silica, plastic, carbon or metal wire. Metal wires may be stainless steel, titanium, a nickel-titanium alloy, or any other metal wire known to a person of skill in the art. The flexible, inert, biocompatible nickel-titanium alloy can be Nitinol. A metal with shape memory properties that enable the wire to maintain straightness, even after it is coiled, is desirable.

Coated SPME wires can be used for in vitro analysis of drug concentrations as well as for in vivo analysis of intravenous drug concentrations in a living animal. Coated SPME probes for in vivo analysis can have any combination of extractive particles coated with an appropriate biocompatible coating, such as polyacrylonitrile (PAN), polyethylene glycol, polypyrrole, derivatized cellulose, polysulfone, or polyamide solution. Non-limiting examples of the coating include: a PAN/C-18 coating, a PAN/RP-amide coating, a polypyrrole glycol/HF-5 coating, a derivatized cellulose/C-18 coating, a polypyrrole/C-30 coating, a polysulfone/polyamide coating and polyamide/cyano coating.

Another embodiment relates to a continuous-coating process for producing SPME fibers coated with a biocompatible coating. Preferably, the biocompatible coating is PAN or Polyethylene glycol (PEG). In the continuous-coating process, a fiber can be wound on a spool and can be threaded through an applicator with a fixed opening that contains a suspension of extraction particles in a biocompatible coating solution. The extraction particles can be C18, RP-amide, HS-F5 silica particles or any other particle listed above. Mixtures of particles can be used. When the particles are silica particles and the biocompatible coating is PAN, the ratio of PAN/silica can be between 0.3 and 0.7 wt/wt. The preferred ratio of PAN/silica is 0.5 wt/wt. The ratio is based on the bare weight of silica and adjusted to the phase loading on the silica particles. The PAN/solvent solution can be between 5% and 15% PAN (w/w). Preferably, the PAN/solvent solution is between about 7.5% and about 12% PAN (w/w). More preferably, the PAN/solvent solution is about 10% PAN/solvent (w/w). The solvent can be any solvent known to one of skill in the art that dissolves PAN, for example: dimethylformamide (DMF), dimethyl sulfoxide, NaSCN, Ca(CNS), nitric acid, ethylene carbonate or mixtures thereof. More preferably, the solvent can be DMF. The suspension can be coated on a length of flexible metal fiber. The coated fiber can be passed through a heater at an elevated temperature and connected to another reel driven by a motor that can pull the fiber at a fixed speed. The elevated temperature can be between about 150°C and about 300°C. Preferably, the elevated temperature is between about 180°C and about 210°C. A person of skill in the art would readily understand that PAN is fully polymerized when it is dissolved in the solvent and as long as the solvent is fully evaporated, the fiber is properly coated. As such, any means known to a person of skill in the art to remove the solvent can be used to dry the coated fibers.

In the continuous-coating process, thin multiple layers of the suspension can be applied to the fiber until the desired coating thickness is obtained. The advantage is that each coating layer is bonded and the coating thickness is uniform throughout the length of the fiber. When the process parameters are controlled by automation, reproducibility between fibers can be greatly improved.
Another embodiment relates to a dip-coating process for producing SPME fibers coated with a biocompatible coating. Preferably, the biocompatible coating is PAN. A dip-coating process would be understood by a person of skill in the art to be a batch process. A length of fiber can be dipped into a suspension of extraction particles in a biocompatible coating solution. The extraction particles can be C-18, RP-amide, HS-F5 silica particles or any other particle listed above. Mixtures of particles can be used. When the particles are silica particles and the biocompatible coating is PAN, the ratio of PAN/silica can be between 0.3 and 0.7 wt/wt. The preferred ratio of PAN/silica is 0.5 wt/wt. The ratio is based on the bare weight of silica and adjusted to the phase loading on the silica particles. The PAN/solvent solution can be between about 5% and about 15% PAN (w/w). Preferably, the PAN/solvent solution can be between about 7.5% and 12% PAN (w/w). More preferably, the PAN/solvent solution can be about 10% PAN/solvent w/w. The solvent can be dimethylformamide (DMF), dimethyl sulfoxide, NaSCN, Ca(CNS)$_2$, nitric acid, ethylene carbonate or mixtures thereof. More preferably, the solvent can be DMF.

If desired, the coated fibers can be dried under flowing nitrogen and then cured for about 5 s to about 1.5 min at about 180°C to about 200°C in order to accelerate the removal of the solvent. A person of skill in the art would readily understand that PAN is fully polymerized when it is dissolved in the solvent and as long as the solvent is fully evaporated, the fiber is properly coated. As such, any means known to a person of skill in the art to remove the solvent can be used to dry the coated fibers.

The wires can be pre-processed before the coating process in order to clean and roughen the surface. Pre-processing can be accomplished by washing with acetone, etching for 1 min in concentrated hydrochloric acid, washing the wire with water and/or thoroughly cleaning the wire by sonication in water. Prior to use, the coated fibers can be conditioned in a water: methanol 50:50 wash for 30 min. Conditioning the C-18 based coatings with water or higher proportion of methanol can lead to worse reproducibility. Other coatings, however, can require only a very brief conditioning step (less than 5 min), or even none at all.

EXAMPLE 1

Dip Coating

Particles commonly used as HPLC stationary phases (0.47 g of C-18, RP-amide, or HS-F5 particles) were brought into suspension with 2 g of a solution made up of 10% w/w PAN in DMF. SPME coatings with a length of 1.5 cm were prepared by applying a uniform layer of slurry of PAN and different particles on the surface of stainless steel wires, allowing to dry under flowing nitrogen, and finally curing for about 1.5 min at 180°C. The SPME coating was applied by dipping the wires into the slurry and removing them slowly.

EXAMPLE 2

PAN as a Membrane

Existing fibers with conventional extraction phases (CWi/TPR—carboxylic/templated resin, from Supelco, Pa.) were coated with PAN by dipping them for 2 min in a solution of 10% PAN in DMF. Subsequently, the fibers were removed slowly from the solution, allowed to dry under flowing nitrogen, and finally cured by a short exposure (5 s) to a flow of nitrogen at 200°C.

EXAMPLE 3

Continuous Coating

Wire was coated on a first reel and threaded through an applicator filled with a coating suspension. The wire was then threaded through a heater and attached to a take-up reel. The wire was drawn through both the applicator and heater at a set speed. The thickness of the coating was measured and additional coatings were applied by switching the positions of the first reel and take-up reel, and repeating the previous coating, drying and switching steps until a desired thickness is achieved.

EXAMPLE 4

Analysis by Scanning Electron Microscopy

For SEM imaging, the fibers were cut into 7 mm long pieces, coated with gold (~10 nm) and analyzed using a LEO 1530 Emission Scanning Electron Microscope at the Waterloo Waterlab Facility. The SEM images of PAN/C-18 coatings (FIG. 1) demonstrate that the particles are completely covered with PAN and are homogeneously distributed within the coating.

SEM was also used to estimate the average thickness of each coating, which was found to be 60-62 μm. No swelling of the coating was observed during analysis time (extraction up to about 2 h and desorption for about 15 min).

EXAMPLE 5

Analysis by X-ray Photoelectron Spectroscopy

XPS (X-ray photoelectron spectroscopy) analyses were performed by using a multi-technique ultra-high vacuum Imaging XPS Microprobe system (Thermo VG Scientific ESCALab 250) equipped with a hemispherical analyzer with a mean radius of 150 mm and a monochromatic Al-Kα (1486.60 eV) X-ray source. The spot size for the XPS analysis used for the present work was approximately 0.5 mm by 1.0 mm. The samples were mounted on a stainless steel sample holder with double-sided carbon tapes. The sample was stored in vacuum (2×10⁻⁶ mbar) in the load-lock chamber of the Imaging XPS Microprobe system overnight to remove any remaining moisture before introduction into the analysis chamber maintained at 2×10⁻¹⁰ mbar. A combination of low energy electrons and ions was used for charge compensation on the non-conducting coating material during the analysis conducted at room temperature. Averages of five high resolution XPS scans were performed for each element of interest (C, N, O, S). Curve fitting was performed using CasaXPS VAMAS Processing Software and the binding energies of individual elements were identified with reference to the NIST X-Ray Photoelectron Spectroscopy Database.

All investigated fibers were exposed to undiluted human plasma at 37°C for 1 h (this is considered a rigorous biocompatibility test). They were then briefly washed with phosphate buffer and deionized water and dried in nitrogen before analysis. Survey scans and high resolution XPS scans
were used to determine the atomic percentages of the surfaces before and after exposure to plasma, as described in Example 8.

EXAMPLE 6

Analysis by LC/MS

[0038] Stock solutions of drugs (diazepam, verapamil, warfarin, nordiazepam, loperamider, and lorazepam as internal standard) with a concentration of 1 mM were prepared in a water:methanol 1:1 mixture and kept refrigerated at 4°C. (in 2 mL siliconized vials).

[0039] Human plasma (in 2 mL polypropylene vials with EDTA as anti-clotting agent) was stored at −20°C until analysis. For analysis, plasma was thawed at room temperature and aliquots of 1.5 mL plasma were transferred into clean vials. Appropriate amounts of stock drug solutions were added to obtain final concentrations of drug in the range 1 mM-50 μM, followed by vortex mixing for 1 minute. Samples and standards in PBS (phosphate buffer saline) were similarly prepared, to a final concentration in the range 0.1 mM-5 μM.

[0040] The time required for the drugs to reach equilibrium between the sample and the SPE fiber, for plasma and PBS samples at 2400 rpm vortex stirring and room temperature, was determined for all target compounds (diazepam, verapamil, and nordiazepam 5E-7M; warfarin 5E-6M; loperamide 5E-8M) by measuring the amount of compound extracted at different time points. Although the concentration of the sample analyzed by SPE was no impact on the extraction time profile and equilibrium time, the agitation conditions, coating thickness (especially for liquid coatings), distribution constant, and diffusion coefficient of the analyte play very important roles in determining an experimental equilibrium time. While the theoretical equilibrium time is infinite, the experimental equilibrium time can be considered to be the time required to extract at least 95% of the theoretical maximum.

[0041] To minimize the errors caused by different sampling times, the extraction time should be equal to or longer than the experimental equilibrium time. The experimentally determined equilibrium time was found to be between 4 and 55 min in most cases. No significant difference was observed when the equilibrium profile in PBS was compared to the equilibrium profile in plasma. When the target drugs were analyzed in mixtures, an extraction time corresponding to the maximum equilibrium time was used.

[0042] When existing commercial coatings were covered with a layer of PAN, the equilibrium time remained essentially unchanged. The mechanical stability of the fibers coated with PAN can be significantly improved: while original fibers can be used for 20 extractions before they break down, those coated with PAN can last for more than 50 extractions. In addition to improved biocompatibility and durability, the PAN coated fibers offer almost the same extraction capacity as the non-coated fibers (FIG. 2).

[0043] For extraction, samples were placed on a digital vortex platform and the extracting phase of the SPME fiber was immersed in the sample for a precise period of time, as determined above. Subsequently, the fiber was then briefly rinsed with water, and desorbed for analysis. The lowest carryover and the sharpest chromatographic peaks for the investigated drugs were obtained for a desorption time of 15 min, vortex stirring at 2400 rpm, and with a desorption solution prepared from acetonitrile:water:acetic acid (50:49:1). Unless otherwise specified, the sample volume was 1.5 mL and the fiber was desorbed for 15 minutes in an insert with 60 μL desorption solution containing lorazepam as internal standard (50 ng/mL).

[0044] Successful coupling of SPME with HPLC is dependent on the efficiency of the desorption step. Desorption can be effected on-line (manual introduction of the fiber into a desorption chamber) or off-line (in a vial or 96-well plate).

[0045] The carryover was found to be well below 3% (with three exceptions out of twenty determinations). For highly sensitive analyses, desorption is usually followed by solvent evaporation and reconstitution in a lower volume of solvent suitable for direct HPLC analysis. Nevertheless, desorption in 60 μL solvent was found to be entirely suitable. If required, the carryover can be further decreased by using larger volumes of desorption solution or longer desorption time.

[0046] All reproducibility, reusability, extraction efficiency, and calibration experiments were performed at equilibrium in similar conditions, following the general procedure for new SPE methods. Calibration curves were constructed by spiking PBS or human plasma with drug concentrations in the range of 0.5 nM-50 μM, which generally covers the therapeutic concentrations. All extractions and desorptions were performed manually.

[0047] LC-MS (liquid chromatography coupled with mass spectrometry) analyses were performed using an Agilent 1100 series liquid chromatograph (Agilent Technologies, Palo Alto, Calif.), equipped with a vacuum solvent degassing unit, a binary high pressure gradient pump, an autosampler, a column thermostat and a variable wavelength UV-VIS detector coupled on-line with an Agilent 1100 series MSD single quadrupole instrument with atmospheric pressure electro-spray ionization (ESI). High purity nitrogen used as nebulizing and drying gas was obtained from an in-house generator.

[0048] Chromatographic separations were carried out on a Discovery® C18 column (5 mmx2.1 mm, 5 μm particles, from Supelco), guarded by an on-line filter (0.2 μm). Data were collected and analyzed using the CHROMSTATION software from Agilent Technologies.

[0049] LC and ESI-MS conditions were as follows: column temperature 25°C, mobile phase acetonitrile: 20 mM ammonium acetate pH 7.0 with gradient programming (initial composition—10:90, ramped to 80:20 over 6 min and maintained until the end of the run), flow rate 0.25 mL min−1, nebulizer gas N2 (35 psi), drying gas N2 (13L min−1,300°C), capillary voltage 3500 V, fragmenter voltage 80 V, quadrupole temperature 100°C, positive ionization mode. Total run time was 9 min.

[0050] For optimization experiments, scan mode in the range 100-1500 amu was used; for quantification experiments, selected ion monitoring is used, with a scan time of 0.42 s/cycle and a dwell time of 65 ms. The following positive ions were monitored: diazepam, m/z 285.1; verapamil, m/z 455.3; warfarin, m/z 309.1; nordiazepam, m/z 271.1; loperamide, m/z 477.3; lorazepam, m/z 321.0. All other parameters of the mass-selective detector were automatically optimized using a calibration standard. Lorazepam was used as an internal standard for compensation of variations in the injection volume (20 μL).

EXAMPLE 7

Sterilization

[0051] Sterilization may be desired if the microextraction devices are to be used for in vivo experiments. Current ster-
ilization methods include heat, steam, chemical (ethylene oxide, alcohols, aldehydes), and radiation.

[0052] The new coatings were tested for extraction efficiency before and after chemical and steam sterilization. For chemical sterilization, the fibers were immersed in alcohol (methanol or ethanol) for 30 minutes and then allowed to dry. Sterilization by steam was performed in an autoclave at 121°C and 15 psi for 30 minutes.

[0053] No change in extraction efficiency was observed upon sterilization with alcohols, as this step is similar to the conditioning step (before extraction). In the case of sterilization in an autoclave, the proposed coatings showed no sign of deterioration (as determined from optical microscope images). This was expected since PAN coatings are known to withstand GC-injector temperatures (>250°C). Although no signs of breakdown were observed, the extraction capacity decreased by approximately 15% after sterilization, possibly because of the combined effect of heat and water vapors on the fused silica particles.

EXAMPLE 8

Biocompatibility

[0054] Many methods have been applied for the study of biocompatibility, ranging from the simple visual inspection to the most sensitive atomic force microscopes. Nevertheless, only a few methods are widely used and recognized: XPS, atomic force microscopy, surface plasmon resonance, and competitive ELISA (enzyme linked immunosorbent assay).

[0055] XPS or electron spectroscopy for chemical analysis (ESCA) is one of the most common types of spectroscopic methods for analysis of surfaces. The sampling depth for this method is approximately 1-30 nm (up to 100 nm mean-free pass), which encompasses a surface region highly relevant for bio-interactions.

[0056] The biocompatibility of various coatings was tested by XPS. A material is considered biocompatible if the amount of nitrogen and sulfur on the surface does not increase significantly after contact with a biological system. After exposure of PAN-based coatings to plasma, the amount of nitrogen and carbon on the surface generally decreases, accompanied by an increase in the amount of oxygen (Table 1). These observations suggest that most of the molecules adsorbed from human plasma contain a high percent of oxygen (usually because of non-specific adsorption), while their nitrogen content is lower than that of plasma proteins. Even more conclusive from a biocompatibility point of view is the amount of sulfur on the surface, since sulfur is naturally present in proteins but absent from the investigated SPME coatings. When compared to RAM and PPy, materials regarded as highly biocompatible, the new coatings based on PAN showed a much lower increase in sulfur.

<table>
<thead>
<tr>
<th>Protein/Coating</th>
<th>C % (RSD &lt; 5%)</th>
<th>N % (RSD &lt; 5%)</th>
<th>O % (RSD &lt; 10%)</th>
<th>S % (RSD &lt; 15%)</th>
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<tbody>
<tr>
<td>Human serum albumin</td>
<td>63.3</td>
<td>16.9</td>
<td>19.0</td>
<td>0.9</td>
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<td>Fibrinogen</td>
<td>62.8</td>
<td>18.0</td>
<td>18.8</td>
<td>0.5</td>
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<tr>
<td>PAN coating (bp*)</td>
<td>78.2</td>
<td>17.6</td>
<td>4.0</td>
<td>0.0</td>
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<tr>
<td>PAN coating (ap**)</td>
<td>73.5</td>
<td>15.1</td>
<td>11.3</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/HC-18 (bp*)</td>
<td>77.0</td>
<td>17.2</td>
<td>5.7</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/HC-18 (ap**)</td>
<td>73.6</td>
<td>13.9</td>
<td>12.5</td>
<td>0.0^3</td>
</tr>
<tr>
<td>PAN/RP-amine (bp*)</td>
<td>78.3</td>
<td>17.0</td>
<td>4.5</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/RP-amine (ap**)</td>
<td>68.6</td>
<td>15.5</td>
<td>15.8</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/HS-F5 (bp*)</td>
<td>79.3</td>
<td>20.1</td>
<td>0.4</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/HS-F5 (ap**)</td>
<td>70.9</td>
<td>15.2</td>
<td>13.7</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/RAM (bp*)</td>
<td>78.9</td>
<td>20.4</td>
<td>0.5</td>
<td>0.0</td>
</tr>
<tr>
<td>PAN/RAM (ap**)</td>
<td>72.6</td>
<td>16.3</td>
<td>10.4</td>
<td>0.5</td>
</tr>
<tr>
<td>PPy (bp*)</td>
<td>61.0</td>
<td>3.8</td>
<td>35.2</td>
<td>0.0</td>
</tr>
<tr>
<td>PPy (ap**)</td>
<td>69.7</td>
<td>12.4</td>
<td>17.6</td>
<td>0.3</td>
</tr>
</tbody>
</table>

*bp = before exposure to human plasma
**ap = after exposure to human plasma
^the experimental value was 0.04, below the limit of quantitation of 0.1%
The biocompatibility test based on XPS suggests that the most biocompatible PAN-based coatings are PAN/RP-amide and PAN/HS-F5, followed closely by PAN/C-18. Furthermore, the newly developed PAN-based coatings were inspected under the microscope after five minutes exposure to human plasma and whole mouse blood (without anti-clotting agents), and no clot adhesion to the coating was observed.

EXAMPLE 9

Drug—Plasma Protein Binding

Various SPME coatings were investigated by studying the extraction and separation of drugs from human plasma. As shown in FIG. 3, a very good linear relationship was obtained for a seven point calibration (n=3). FIG. 3 also indicates that drug binding to plasma proteins changes the amount of drug available for extraction and results in different calibration slopes for plasma and PBS.

The linear range covered more than three orders of magnitude for most drugs, with the exception of warfarin, where the linear range spanned over two orders of magnitude. The full details are shown in Table 2.

<table>
<thead>
<tr>
<th>Linear Range</th>
<th>PAN/C-18</th>
<th>PAN/RP-amide</th>
</tr>
</thead>
<tbody>
<tr>
<td>(mole/L)</td>
<td>PBS</td>
<td>Plasma</td>
</tr>
<tr>
<td></td>
<td>PBS</td>
<td>Plasma</td>
</tr>
<tr>
<td>Diazepam</td>
<td>1E-9-&gt;2E-6</td>
<td>1E-8-&gt;1E-5</td>
</tr>
<tr>
<td></td>
<td>3E-9-&gt;1E-6</td>
<td>5E-8-&gt;3E-5</td>
</tr>
<tr>
<td>Verapamil</td>
<td>1E-9-&gt;1E-6</td>
<td>5E-9-&gt;5E-6</td>
</tr>
<tr>
<td></td>
<td>2E-9-&gt;4E-7</td>
<td>2E-8-&gt;4E-6</td>
</tr>
<tr>
<td>Warfarin</td>
<td>2E-8-&gt;3E-6</td>
<td>2E-7-&gt;5E-5</td>
</tr>
<tr>
<td></td>
<td>2E-7-&gt;2E-6</td>
<td>2E-8-&gt;2E-5</td>
</tr>
<tr>
<td>Nifedipine</td>
<td>1E-6-&gt;2E-5</td>
<td>5E-9-&gt;2E-5</td>
</tr>
<tr>
<td></td>
<td>5E-7-&gt;2E-5</td>
<td>2E-7-&gt;3E-5</td>
</tr>
<tr>
<td>Loperamides</td>
<td>1E-6-&gt;2E-5</td>
<td>5E-9-&gt;2E-5</td>
</tr>
<tr>
<td></td>
<td>2E-7-&gt;3E-5</td>
<td>2E-8-&gt;2E-5</td>
</tr>
</tbody>
</table>

The determination of plasma protein binding by SPME is based on determining the free concentration of drug in the presence of plasma proteins. Briefly, the percentage of drug binding to plasma proteins (PPB) is calculated from the total and free concentration of drug:

\[
PPB \% = \frac{C_{\text{total plasma}} - C_{\text{free plasma}}}{C_{\text{total plasma}}} \times 100 = \left[ 1 - \frac{C_{\text{free plasma}}}{C_{\text{total plasma}}} \right] \times 100
\]  

where \( C_{\text{total plasma}} \) is the total concentration of drug in plasma and \( C_{\text{free plasma}} \) is the free concentration of drug in plasma.

Considering that the total drug concentration is directly proportional to the slope of the drug calibration curve in PBS and the free concentration is directly proportional to the slope of plasma calibration, Equation 1 becomes:

\[
PPB \% = 100 \left[ 1 - \frac{\text{slope calibration plasma}}{\text{slope calibration PBS}} \right]
\]  

Equation 2 was applied for the determination of drug plasma protein binding for the five test drugs, and the results are presented in Table 3. Only the most reproducible coatings were used, and the results correlate very well with previously published values.

What I claim is:

1. A biocompatible coating for solid phase microextraction (SPME) of a small molecule of interest from a matrix, the coating comprising:
   - an extraction phase including SPME particles having pores dimensioned to absorb the small molecule of interest from the matrix; and
   - a biocompatible polymer, which is selected from the group consisting of a polyacrylonitrile (PAN) and a co-polymer of polyacrylonitrile (PAN), completely covering the SPME particles and homogeneously distributing the SPME particles therein;
   - having reduced adsorption of proteins or macromolecules onto the SPME particles and allowing the SPME particles to extract the small molecule of interest from the matrix.

2. The biocompatible coating according to claim 1, wherein the SPME particles are selected from the group consisting of C-18/silica particles, RPamid/silica particles, HS-F5/silica particles, and mixtures thereof.

3. The biocompatible coating according to claim 1, wherein the SPME particles are about 5 μm particles.

4. The biocompatible coating according to claim 1, wherein the SPME particles have a pore size from about 120 Å to about 180 Å.

5. The biocompatible coating according to claim 1, wherein the SPME particles have a surface area of about 200 m²/g to about 300 m²/g.
6. The biocompatible coating according to claim 1, wherein the matrix is selected from the group consisting of biological fluid, tissues, organs and cells.

7. The biocompatible coating according to claim 1, wherein the matrix is a biological fluid which is selected from the group consisting of whole blood, plasma, serum, urine, cerebrospinal fluid, and peritoneal fluid.

8. The biocompatible coating according to claim 1, wherein the small molecule is a drug or a biomarker.

9. The biocompatible coating according to claim 1, wherein the small molecule is a drug selected from the group consisting of hydrophobic and hydrophilic molecule having a molecular mass less than about 10,000 atomic mass units.

10. The biocompatible coating of claim 1 wherein the SPME particles are distributed within the biocompatible polymer at a ratio (w/w) of about 0.47 g SPME to about 0.2 g biocompatible polymer.

11. A device for solid phase microextraction (SPME) of a small molecule of interest from a matrix, comprising:
a fiber; and

a biocompatible coating on the fiber, the coating including an extraction phase having SPME particles with pores dimensioned to absorb the small molecule of interest from the matrix; and

a biocompatible polymer completely covering the SPME particles and homogeneously distributing the SPME particles therein,

and having reduced adsorption of proteins or macromolecules onto the SPME particles and allowing the SPME particles to extract the small molecule of interest from the matrix.

12. The device of claim 11 wherein the SPME particles are about 5 μm particles.

13. The device of claim 11 wherein the SPME particles have a pore size from about 120 Å to about 180 Å.

14. The device of claim 11 wherein the SPME particles have a surface area of about 200 m²/g to about 300 m²/g.

15. The device of claim 11 wherein the biocompatible polymer is selected from the group consisting of polyacrylonitrile (PAN), a co-polymer of polyacrylonitrile (PAN), polyethylene glycol, and polyacrylate.

16. The device according to claim 11 wherein the matrix is selected from the group consisting of biological fluid, tissues, organs and cells.

17. The device according to claim 11 wherein the matrix is a biological fluid which is selected from the group consisting of whole blood, plasma, serum, urine, cerebrospinal fluid, and peritoneal fluid.

18. The device according to claim 11 wherein the small molecule is a drug or a biomarker.

19. The device of claim 11 wherein the small molecule is a drug selected from the group consisting of hydrophobic and hydrophilic molecule having a molecular mass less than about 10,000 atomic mass units.

20. The device of claim 11 wherein the SPME particles are distributed within the biocompatible polymer at a ratio (w/w) of about 0.47 g SPME to about 0.2 g biocompatible polymer.

21. The device of claim 11 wherein the SPME particles are selected from the group consisting of C18/silica particles, RP-amide/silica particles and HS-F5/silica particles.

* * * * *