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(71) Applicant (for all designated States except US): **ALMA MATER STUDIORUM - UNIVERSITA' DI BOLOGNA** [IT/IT]; Via Zamboni, 33, I-40126 Bologna (BO) (IT).

(72) Inventor; and

(75) Inventor/Applicant (for US only): **DARDARI, Davide** [IT/IT]; Via Carducci, 10, I-47039 Savignano sul Rubicone (FC) (IT).

(74) Agents: **CRUGNOLA, Pietro** et al.; Luppi Crugnola & Partners S.r.l., Viale Corassori 54, I-41100 Modena (IT).

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(54) Title: METHOD AND APPARATUS FOR COMMUNICATION IN ULTRA-WIDE BANDWIDTH RFID SYSTEMS

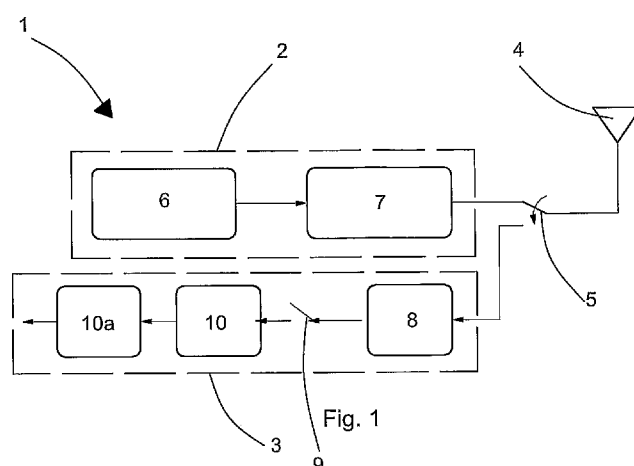


Fig. 1

(57) Abstract: A method for communication in ultra-wide bandwidth RFID systems comprising generating through a transceiver device an interrogation signal, composed of at least a sequence of equally time spaced pulses with period (T_3), transmitting said signal to at least one RFID identification device which generates a response signal and transmits it back to said transceiver device, said method further comprising coding said interrogation signal according to a numerical coding sequence, generating said response signal by varying, in each period (T_3) of said pulse sequence of the interrogation signal, the polarity of pulses using said numerical coding sequence. An apparatus for communication in ultra-wide bandwidth RFID systems comprising a transceiver device (1,101) and a RFID identification device (11), suitable for communicating each other, said RFID identification device (11) comprises a backscatter modulator (12) suitable for modulating a signal reflected by an antenna (18) of the identification device RFID.

**Method and apparatus for communication in ultra-wide
bandwidth RFID systems**

The present invention relates to a method and apparatus for
5 communication in ultra-wide bandwidth RFID systems, in
particular in those systems adopting passive or semi-passive
RFID identification devices.

The method and apparatus according to this invention are
utilizable on radiofrequency identification systems (Radio
10 Frequency IDentification RFID) adopting passive or semi-
passive RFID devices with electromagnetic coupling.

A RFID system consists of a transmitter-receiver device,
called reader, and one or more identification devices, called
tags, each of them is associated with an object, that to be
15 identified or localized. The reader generates an
interrogation signal which is received by tags. As response
to the received interrogation signal, tags send to the reader
a response signal containing specific information, such as,
the identifier of the object with which the tag is
20 associated.

Tags can be classified in three typologies depending on the
type of power supply they are equipped with:

- active tags: contain their own power source that
supplies the whole device which consist of a complete
25 radio transceiver;
- passive tags: do not have their own power source, they
derive the energy from the signal sent by the reader or,
in general, from the surrounding environment;
- semi-passive tags: contain their own power source
30 providing energy only for the information processing
circuits, but it is not able to supply a transceiver
radio device.

Passive and semi-passive tags are not equipped with a
transceiver and tag-reader information transmission is in
35 general based on an antenna modulator which controls the
antenna's load impedance. In this way passive and semi-

passive tags, to transmit their information, exploit the absorption or the reflection of the signal coming from the reader (usually a sinusoidal tone, hence a narrowband signal). In particular, the electromagnetic wave, incident to the tag's antenna, gives part of its energy to the antenna's load, while the remaining energy is reflected as backscattering. To transfer the information contained in its own memory, the tag modulates, through the control of the antenna's impedance (backscatter modulation), the reflected power (backscatter).

Passive tags are usually preferred in radiofrequency identification systems due to their better adaptability to requested applications, low cost, long lifetime, small size. The commercialized devices are mostly based on magnetic coupling (band at 13MHz). Recently passive devices based on narrow bandwidth electromagnetic coupling working in the 865 MHz and 2.4 GHz bands with operation range of about 3-4 meters have been introduced.

However, current RFID systems have several limitations: First of all, current RFID tags based on narrow bandwidth backscatter modulation are extremely limited in read/write operating range, typically less than 3-4 m. To achieve this operating range transmission power levels in the order of 2-4 W are required which preclude their use in specific environments such as in medical applications. The maximum number of tags contemporaneously addressable by the reader is strongly limited by the low transmission data rate and by the high probability of interference among tags present in the same area. One severe problem is represented by the reception of several echoes of the transmitted signal (multipath) due to signal reflections in the surrounding environment. Where the various signal echoes adding each other in destructive way thus creating shadowed zones within the coverage area and hence a less reliable system. Considering that signals are narrow bandwidth, the temporal resolution, and hence the spatial resolution is insufficient to achieve accurate

localization of tags at centimetre precision. That precludes the utilization of RFID tags in many applications where the localization capability is fundamental (for example, objects tracking).

5 Moreover, information transmission security problems are present. In fact, considering that these devices are passive, they cannot host ciphering devices, which would require a larger availability of energy: therefore data are easily detectable. Finally, current systems are not protected
10 against the presence of interference (for example, caused by other RFID systems working in the same area or by intentional interferers).

Recently, RFID systems adopting the impulse-radio Ultra Wide Band (UWB) technology, characterized by the transmission at
15 very low duty cycle, i.e. using pulses with duration less than one nanosecond, have been proposed.

UWB signals have a fractional bandwidth greater than 20% or an absolute bandwidth larger than 500 MHz: this offers several advantages both for communication and localization
20 applications. The ultra-wide bandwidth improves the reliability. In fact, as the signal contains a large number of spectral components, the probability that at least some of them can go through obstacles is increased. It offers extraordinary robustness to interference produced by other
25 systems and an extraordinary precision in distance estimation based on time-of-arrival measurement of the received signal.

The possibility to resolve various signal components reflected by the surrounding environment allows not only for reducing the shadowed zones within the coverage area but it
30 can be exploited advantageously by collecting the energy coming from different components using Rake receivers thus increasing the coverage area.

Summarizing, the UWB technology is a good candidate to overcome the limitations of the actual narrow bandwidth RFID
35 technology thanks to lower transmission power levels (<1 mW vs 2-4 W required by actual RFID systems), extremely accurate

localization (at centimetre level) even in indoor environments, robustness to interference and multipath propagation (better area coverage and reliability), possibility of large number of devices co-existing in the same area (multiple access).

UWB was recently proposed to realize radiofrequency tags (UWB-RFID), that is low cost and low energy consumption devices. So far, proposed tags are active and include a complete UWB transceiver powered by a battery.

US 7,154,396 describes a passive or semi-passive UWB-RFID system based on backscatter modulation, wherein a reader transmits a sequence of equal very short pulses which are reflected or not by the tag through the variation of the antenna loading conditions (matched load vs open circuit) according the information bit to be transmitted. However, no sufficient details are provided on the signal modulation and demodulation process.

Recent measurements on UWB antenna backscatter properties have shown that the signal reflected by the tag is composed of a backscatter component (named structural mode), dependent on the antenna physical structure whose intensity does not depend on antenna load and hence on the tag's information data, which results to be completely overlapped and dominant with respect to the backscatter component dependent on the antenna load (named antenna mode). This phenomena makes the solution proposed in US 7,154,396 not utilizable because the antenna reflects for each load condition, thus making extremely difficult, even impossible, to recognize the reflected pulses that are the code of the signal transmitted by the tag. This situation gets worse if, in addition to the signal reflected by the tag's antenna, other signal components reflected by the surrounding environment (clutter) or by other tags are present. Moreover, considering that the international spectrum regulatory constraints do not allow the emission of UWB signals with transmitted power level larger than about -2 dBm, associating one bit for each

reflected pulse, as proposed in US 7,154,396, does not guarantee a sufficient level of energy received by the reader for a reliable information detection at significant operating ranges.

5 One aspect of the present invention is directed to provide a method for the communication in ultra-wide bandwidth RFID devices able to overcome the above mentioned limitations.

Another aspect of the present invention is directed to provide an apparatus able to implement such a method.

10 According to the invention a method for the communication in ultra-wide bandwidth RFID systems is provided comprising generating through a transceiver device an interrogation ultra-wide bandwidth signal, said signal comprising at least a sequence of equally time spaced pulses with period (T_s),
15 transmitting said signal to at least one RFID identification device, processing said interrogation signal according to the information stored in said RFID device and transmitting it back to the transceiver device as response signal, receiving said response signal through said transceiver device and
20 further processing said response signal to detect said information included in said response signal, characterized in that it further comprises:

- coding said interrogation signal according to a numerical coding sequence that determines the polarity of each pulse of
25 said sequence of pulses;

- generating, in said RFID device, said response signal by varying, in each period (T_s) of said sequence of pulses of the interrogation signal, the polarity of the pulses using said numerical coding sequence through the variation of the
30 antenna load (backscatter modulation), so that all the pulses reflected by the tag in the same period (T_s) have the same polarity.

Owing to the invention it is possible to make the communication between the tag and the reader robust with
35 respect to signal reflections in the surrounding environment and to eliminate the effect of the tag's antenna structural

dependent component in the response signal.

Another aspect of this invention is directed to an apparatus for the communication in ultra-wide bandwidth RFID devices comprising a transceiver device and a RFID identification device configured to communicate each other, characterized in that said RFID device comprises a backscatter modulator configured to modulate a signal reflected by the RFID identification device's antenna, said backscatter modulator comprises a first switch S1, placed in parallel to the antenna, and a second switch, parallel to the antenna and in series to a load impedance.

The invention will be disclosed below, purely by way of non-limiting example, with reference to the attached drawings, in which:

Figure 1 shows the block diagram of a transceiver device of the present invention;

Figure 2 shows the block diagram of a RFID device of the present invention;

Figure 3 shows the electrical diagram of the RFID device of Figure 2;

Figure 4 shows the block diagram of a variation of the transceiver device of Fig. 1;

Figure 5 shows a table which illustrates the operating mode of the RFID device;

Figure 6 and 7 illustrate an example of signals transmitted and received by the transceiver device of Figure 1;

Figure 8 and 9 illustrate an example of signals transmitted and received by the transceiver device of Figure 4.

In Figure 1 the architecture of a transceiver device 1, named reader, of the present invention is reported. The transceiver device 1 is composed of a transmitting portion 2 and a receiving portion 3, both connected, alternatively, to a first UWB antenna 4, i.e., a ultra-wide bandwidth antenna, through a switch 5. The transmitting portion 2 includes a first numerical sequence, or code, generator 6, which can be binary $c_n \in \{-1, 1\}$, or ternary $c_n \in \{-1, 0, 1\}$.

The first numerical sequence generator 6 drives a pulse generator 7 which generates a signal composed of a series of sequences of pulses with period T_s , each one composed of N_s equally spaced pulses with time interval T_f , so that $T_s = T_f * N_s$.

5 Each pulse composing the sequence of pulses has typically a duration less than one nanosecond, whereas the pulse polarity depends on the corresponding number of the numerical sequence generated by the first numerical sequence generator 6.

To make the communication between the reader 1 and
10 identification RFID devices, named tags, associated therewith, "robust" with respect to the signal reflections in the surrounding environment, that is scarcely affected by such reflections, it is advantageously that the numerical sequence generated by first sequence generator 6 has zero
15 mean value, or quasi-zero mean value, that is the numerical sequence is composed of the same number of positive units "+1" and negative units "-1", or it is composed of a number of positive units "+1" slightly different from the number of negative units "-1", or vice versa. For example, denoting N^+
20 the number of positive units of the sequence and N^- the number of negative units, a numerical sequence suitable to make "robust" the communication between the tag and the reader could be, for example, a sequence wherein $N^+ = N^-$, or a sequence wherein $N^+ = N^- \pm 1$.

25 In Figure 6 there is shown an example of the structure of the signal transmitted by the reader 1, in which, in each period T_s pulse sequence, the pulses with positive polarity are greater by one unit than the pulses with negative polarity, i.e. $N^+ = N^- + 1$.

30 The code sequence is repeated continuously during the entire tag-reader communication. To avoid intersymbol interference due to multipath, in indoor environments the time interval T_f between one pulse and the successive one should be typically chosen in the order of 50-100 ns.

35 The signal generated by reader 1 is received by a tag 11, whose structure is illustrated in the block diagram of Figure

2. Tag 11 includes a backscatter modulator 12, i.e. a modulator of the signal reflected by tag 11, a second numerical sequence, or code, generator 13, similar to the first generator 6 of reader 1, the control unit 14, the synchronization unit 15 and eventually the power unit 16, a memory unit 17 and a second ultra-wide bandwidth antenna 18. The power unit 16 is present only in semi-passive tags to supply the digital section of tag 11, whereas it is not present in passive tags where the necessary energy to operate tag 11 is obtained directly from the electromagnetic field of the received signal or by exploiting other sources (solar, thermal, vibration, etc.).

In Figure 3 the electrical diagram of the backscatter modulator 12 is reported, which includes a first switch S1, parallel to the antenna 18, a second switch S4, parallel to the antenna 18 and in series to the load impedance Z matched to the antenna impedance, and a delay line 19 in series to antenna 18 including a third switch S2 and a fourth switch S3. The length of the delay line 19 determines a delay time τ in the reflection of the signal received by the tag 11. To avoid the dimensions of the delay lines, it is convenient to be chosen a delay time not higher than a few nanoseconds.

The response of tag 11 to the received signal sent by the reader depends on the configuration of switches S1-S4 of the backscatter modulator 12. With the switch S1, S2 and S4 open, independently on the switch S3 position, each pulse received by tag 11 is reflected back to reader 1 without polarity change and delay. When switch S1 is closed and switch S4 is open, independently of the state of switches S2 and S3, each pulse received by tag 11 is reflected back to reader 1 with polarity inversion and without delay.

With switch S2 close and the other switches open, each pulse received by tag 11 is reflected back to reader 1 without polarity inversion but with a delay equal to 2τ .

When switches S1 and S4 are open and switches S2 and S3 are closed, each pulse received by tag 11 is reflected back to

reader 1 with polarity inversion and delay 2τ .

Finally, with switch S4 close and switches S1 and S2 open, independently on position of switch S3, no received signal is reflected back by the tag.

5 In Figure 5 a table summarizing the different signal reflection configurations from tag 11 previously described is shown. The first column reports the status X, labeled from 0 to 4 of tag 11, the central column reports the configuration of switches from S1 to S4, where symbol 0 indicates an open
10 switch, symbol 1 indicates a closed switch, and symbol x indicates that the switch position can be open or closed indifferently. In the third column the signal reflected back by tag 11 is shown, where only the antenna mode component, that modulated by the tag, is reported, whereas the antenna
15 structural mode component is not affected by the tag.

The status X of tag 11 is changed at each time interval T_f according to the numerical sequence generated by the second numerical sequence generator 13, which is identical to the numerical sequence generated by the first numerical sequence
20 generator 6 of reader 1. In addition, the status of tag 11 is changed at each period T_s of the signal, depending on the information bit the tag intends to transmit to the reader, that is to each period T_s an information bit corresponding to a positive unit, or a negative unit, is associated. The
25 information bit sequence to be transmitted is contained in the memory unit 17 of tag 11. The control unit 14 retrieves this information bit sequence from the memory unit 17 and combines it with the numerical sequence generated by the second sequence generator 13 to determine the status of tag
30 11 at each time interval T_f and at each period T_s .

Using a backscatter modulator, as that illustrated in Figure. 3, different modes of modulation of the signal reflected by tag 11 are possible:

- a so called 2-PAM type modulation (binary pulse
35 amplitude modulation);
- a so called 2-PPM type modulation (binary pulse position

modulation);

- ON-OFF type modulation.

It has to be noted that 2-PAM and ON-OFF modulations can be realized using a backscatter modulator without the delay line 19, and hence a backscatter modulator wherein only switches S1 and S4 and the load impedance Z are present.

According to this invention, the modulation of the signal reflected by tag 11 is realized by inverting, within each period T_s of the sequence of pulses, the pulse polarity according to the same coding sequence of the reader so that all pulses within the same period T_s have the same polarity. This polarity inversion affects only the antenna mode component of the reflected signal, whereas it does not affect the structural mode component.

Based on the modulation scheme adopted by the tag, the polarity, position or presence of pulses in each period T_s depends on the information bit to be transmitted. As an example, when the specific case of a 2-PAM modulation scheme is considered, signal modulation consists of inverting the polarity of all pulses within each period T_s if the information bit to be transmitted is a negative unit, whereas the polarity of all pulses within each period T_s is kept unaltered if the information bit to be transmitted corresponds to a positive unit.

The signal received by the receiving portion 3 of the reader 1 is composed, in addition to the mentioned antenna mode and structural mode components of the signal reflected by tag 11, by all those components (clutter) reflected by the surrounding environment, not affected by such polarity inversions.

The receiving portion 3 of reader 1 includes a filter 8 matched to the received pulses, which function is to maximize the signal-to-noise ratio, a sampling device 9, an accumulation unit 10 and a threshold detector 10a. The accumulation unit 10 sums all received signal portions of duration T_f within a period T_s . Owing to the polarity

inversions generated by tag 11, pulses composing the antenna mode component of the reflected signal are summed together resulting in a signal having intensity N_s times larger than the intensity of the antenna mode component of a single pulse, while the structural mode and clutter components, even if dominant in each single pulse, are eliminated or drastically reduced owing to the zero mean or quasi-zero mean property of the code numerical sequence utilized.

In this way, the detector 10a is able to detect easily, with low probability of error, the coded signal reflected by tag 11, i.e. the antenna mode component of the signal, owing to the drastic reduction of the effects of the structural mode and clutter components in the received signal.

In Figure 6 and 7, an example of signal structure emitted by reader 1 and reflected by tag 11, as received by reader 1, are shown, respectively, where the antenna mode components are plotted with a continuous line, while the structural mode and clutter components are plotted with dashed lines. As can be noted, in each sequence of pulses in a period T_s of the signal received by reader 1 all antenna mode components have the same polarity, while the structural mode and clutter components have alternatively opposite polarity, in such a way the antenna mode components are summed by the detector 10a while the structural mode and clutter components give zero or quasi-zero sum.

In Figure 4 an alternative block diagram of a reader 101 including a transmitting portion 102, composed of only a pulse generator 107, and a receiving portion 103 composed of a filter 108 matched to the received pulses, which function is to maximize the signal-to-noise ratio, a sampling device 109, a first numerical binary $c_n \in \{-1, 1\}$, or ternary $c_n \in \{-1, 0, 1\}$ sequence generator 106, a multiplier 112 which multiplies the signal received by the reader by such a numerical sequence, an accumulation unit 110 and a threshold detector 111.

In addition, the reader 101 comprises a switch 105 to connect

alternatively the transmitting portion 102 and the receiving portion 103 to a ultra-wide bandwidth antenna 104. The functionality of reader 101 is equivalent to the functionality of reader 1 described previously. The first code sequence generator 106 is located in the receiving portion 103, instead of in the transmitting portion, whereas pulse generator 107 of the transmitting portion 102 is configured to send a sequence of pulses having the same polarity. The functionality of the tag remains unchanged.

According to this scheme, the interfering components of the signal due to the structural mode and clutter are received without polarity inversions while the useful component of the signal, that of antenna mode, carrying the information, is affected in tag 11 by polarity inversions according to the code sequence c_n . Such polarity inversions of the pulses reflected by tag 11 are compensated, in the receiving portion of the reader, through the multiplication, using the multiplier 112, of received signal samples by the code sequence c_n generated by the first numerical sequence generator 106, which is equal to the code sequence adopted by tag 11. After the multiplication the final result is the same as that obtained using the reader 1 version illustrated in the scheme in Figure 1.

In Figures 8 and 9, an example of signal structure emitted by reader 101 and reflected by tag 11, as received by reader 101, are shown, respectively, where the antenna mode components are plotted with a continuous line, while the structural mode and clutter components are plotted with dashed lines.

As can be noted, in each sequence of pulses in a period T_s of the signal received by reader 101 all antenna mode components have alternatively opposite polarities, while the structural mode and clutter components have the same polarity, in such a way that, after the multiplication, through the multiplier 112, of received signal samples by the code sequence c_n generated by the first numerical sequence generator 106, all

antenna mode components within each period T_s have the same polarity and are summed together by detector 111, while the structural mode and clutter components have alternatively opposite polarity giving zero or quasi-zero sum.

- 5 The present invention allows several advantages in tag-reader communication in a RFID system, such as high capability of the signal to penetrate through obstacles, low transmitted mean power, high immunity to interference caused by signal reflections in the surrounding environment and by the
- 10 presence of signals of other RFID systems; high transmission security because the signal can be decoded only if one knows the exact numerical sequence used in the reader and in the tag; high spatial and temporal resolution, possibility to manage at the same time a large number of tags, for example,
- 15 by assigning different numerical sequences to different tags; possibility of coexistence of several RFID systems in the same area by assigning different numerical sequences to the different systems.

CLAIMS

1. Method for the communication in ultra-wide bandwidth RFID systems comprising generating through a transceiver device (1) an interrogation ultra-wide bandwidth signal, said signal comprising at least a sequence of equally time spaced pulses with period (T_s), transmitting said signal to at least one RFID identification device (11), processing said interrogation signal according to the information stored in said RFID device (11) and transmitting it back to the transceiver device (1) as response signal, receiving said response signal through said transceiver device (1) and further processing said response signal to detect said information included in said response signal, characterized in that it further comprises:
- coding said interrogation signal according to a numerical coding sequence that determines the polarity of each pulse of said sequence of pulses;
 - generating, in said RFID identification device (11), said response signal by varying through the variation of the antenna load (backscatter modulation), in each period (T_s) of said sequence of pulses of the interrogation signal, the polarity of the pulses using said numerical coding sequence, so that all reflected pulses in the same period (T_s) have the same polarity.
2. Method for the communication in ultra-wide bandwidth RFID systems comprising generating through a transceiver device (101) an interrogation ultra-wide bandwidth signal, said signal comprising at least a sequence of equally time spaced pulses with period (T_s), transmitting said signal to at least one RFID identification device (11), processing said interrogation signal according to the information stored in said RFID device (11) and transmitting it back to the transceiver device (101) as response signal, receiving said response signal through said transceiver device

(101) and further processing said signal to detect said information included in said response signal, characterized in that it further comprises:

- generating said sequence of pulses so that all pulses of the sequence have the same polarity;

- generating, in said RFID identification device (11), said response signal by coding said interrogation signal according to a numerical coding sequence and to the information stored in said RFID device that determines the polarity of each pulse of said sequence of pulses by varying the antenna load conditions;

- decoding, in said transceiver device (101), said response signal by modifying, in each period (T_s) of said sequence of pulses of the response signal, the polarity of pulses using said numerical coding sequence, so that all pulses within the same period (T_s) have the same polarity.

3. Method according to claim 1, or claim 2, wherein said numerical sequence is a binary $c_n \in \{-1, 1\}$, or ternary $c_n \in \{-1, 0, 1\}$ numerical sequence.

4. Method according to claim 3, wherein said numerical sequence is a zero or quasi-zero sum numerical sequence.

5. Method according to claim 4, wherein in each period (T_s) of said numerical sequence the number of positive units (N^+) is equal to the number of negative units (N^-).

6. Method according to claim 4, wherein in each period (T_s) of said numerical sequence the number of positive units (N^+) differs from the number of negative units (N^-) in one unit.

7. Method according to claim 1, or any one of claims 3 to 6, as appended to claim 1, further comprising summing together the pulses in each period (T_s) of the response signal.

8. Method according to claim 2, or any one of claims 3 to 6, as appended to claim 2, further comprising summing together the pulses in each period (T_s) of the response

signal after said decoding.

9. Method according to any preceding claim, wherein the duration of each pulse in said sequence of pulses is less than one nanosecond.

5 10. Method according to any preceding claim, wherein a time interval (T_f) between two successive pulses of said sequence of pulses is not less than 50 nanoseconds.

11. Method according to any preceding claim, wherein the time interval (T_f) between two successive pulses of said
10 sequence of pulses is greater than 100 nanoseconds.

12. Apparatus for the communication in ultra-wide bandwidth RFID systems comprising a transceiver device (1; 101) and a RFID identification device (11) suitable for communicating each other, characterized in that said
15 RFID identification device (11) comprises a backscatter modulator (12) suitable for modulating a signal generated by said transceiver device (1; 101) and reflected back by an antenna (18) of the RFID identification device (11), said backscatter modulator
20 (12) comprising a first switch (S1) placed in parallel to the antenna (18) and a second switch (S4), parallel to the antenna (18) as well, and in series to a load impedance (Z).

13. Apparatus according to claim 12, wherein said
25 backscatter modulator (12) further comprises a delay line (19) placed in series to the antenna (18) and comprising a third switch (S2) and a fourth switch (S3).

14. Apparatus according to claim 12, or claim 13, wherein said transceiver device (1) comprises a transmitting
30 portion (2) and a receiving portion (3), said transmitting portion (2) comprising a first numerical sequence generator (6) operationally associated with a pulse generator (7).

15. Apparatus according to claim 12, or claim 13, wherein
35 said transceiver device (101) comprises a transmitting portion (102) and a receiving portion (103), said

transmitting portion (102) comprising a pulse generator (107) and said receiving portion (103) comprising a first numerical sequence generator (106) associated with a multiplier device suitable for multiplying the signal received by said receiving portion (103) by said numerical sequence.

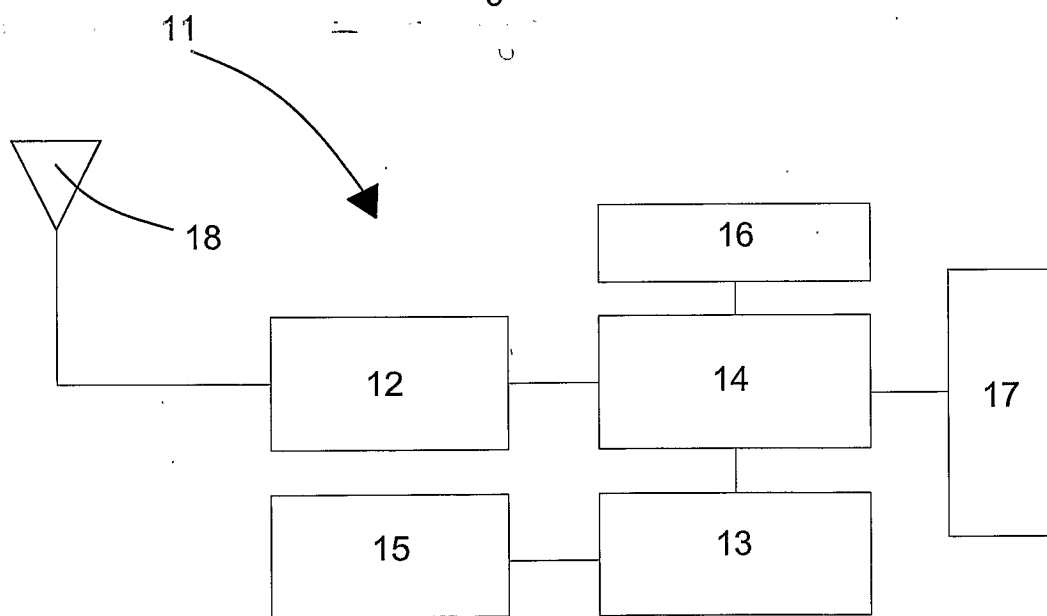
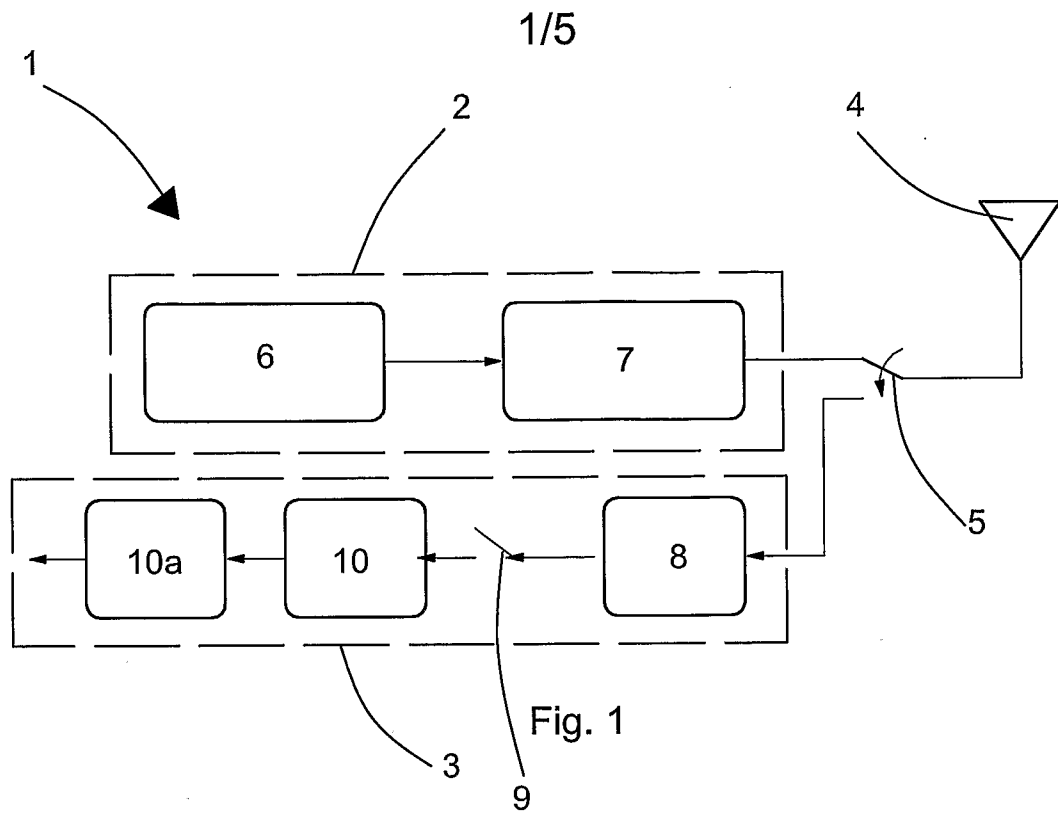
16. Apparatus according to claim 14, or claim 15, wherein said first numerical sequence generator (6; 106) generates a binary $c_n \in \{-1, 1\}$, or ternary $c_n \in \{-1, 0, 1\}$ numerical sequence.

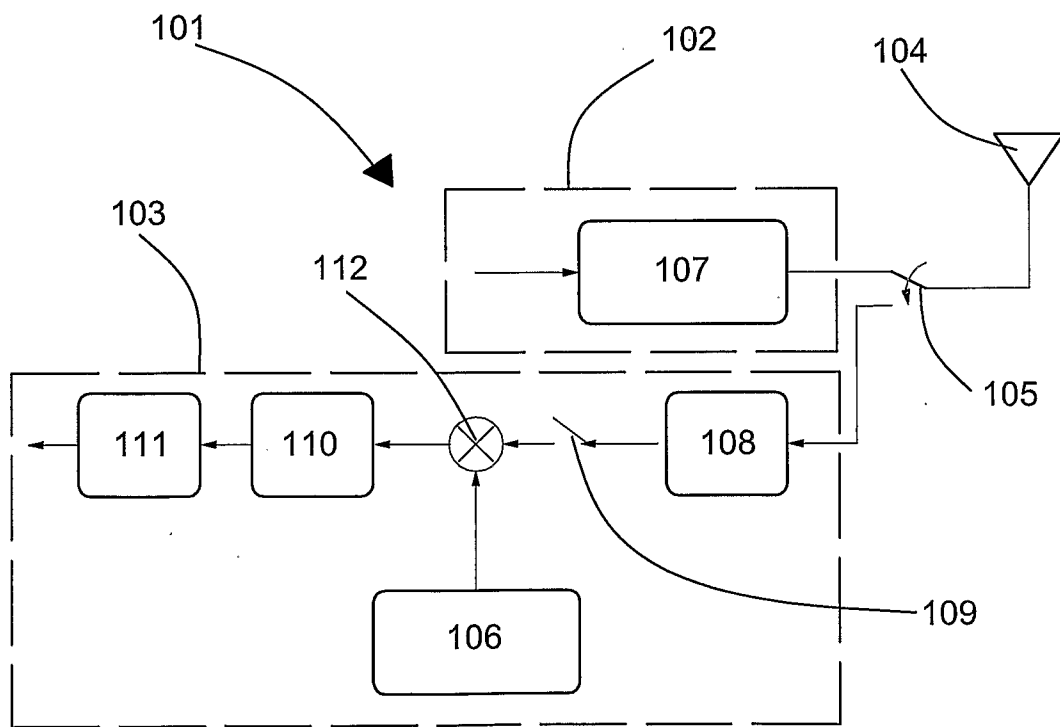
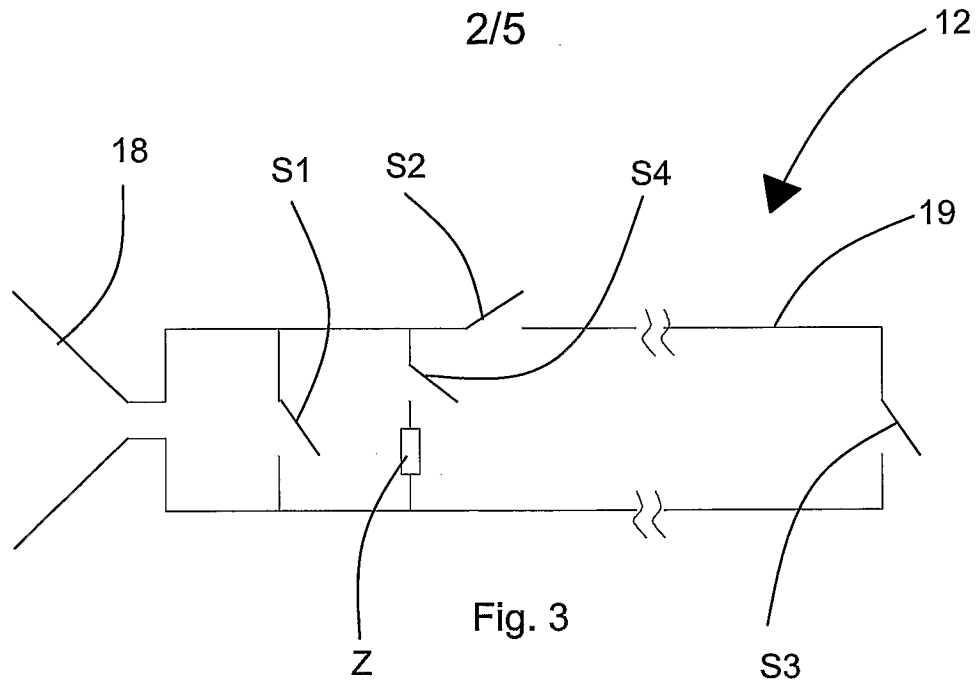
17. Apparatus according to any one of claim 14 to 16, wherein said receiving portion (3; 103) comprises a matched filter (8; 108), a sampler device (9; 109), an accumulation unit (10; 110), a threshold detector (10a; 111), an antenna (4; 104) and a switch (5; 105) to connect alternatively said antenna (4; 104) to said transmitting portion (2; 102) and said receiving portion (3; 103).

18. Apparatus according to any one of claim 12 to 17, wherein said RFID identification device comprises a second numerical sequence generator (13), a control unit (14), a synchronization unit (15), and a memory unit (17).

19. Apparatus according to claim 18, wherein said second numerical sequence generator (13) generates a numerical sequence identical to the numerical sequence generated by said first numerical sequence generator (6; 106).

20. Apparatus according to claim 18, or claim 19, wherein said RFID identification device further comprises a power unit (16).





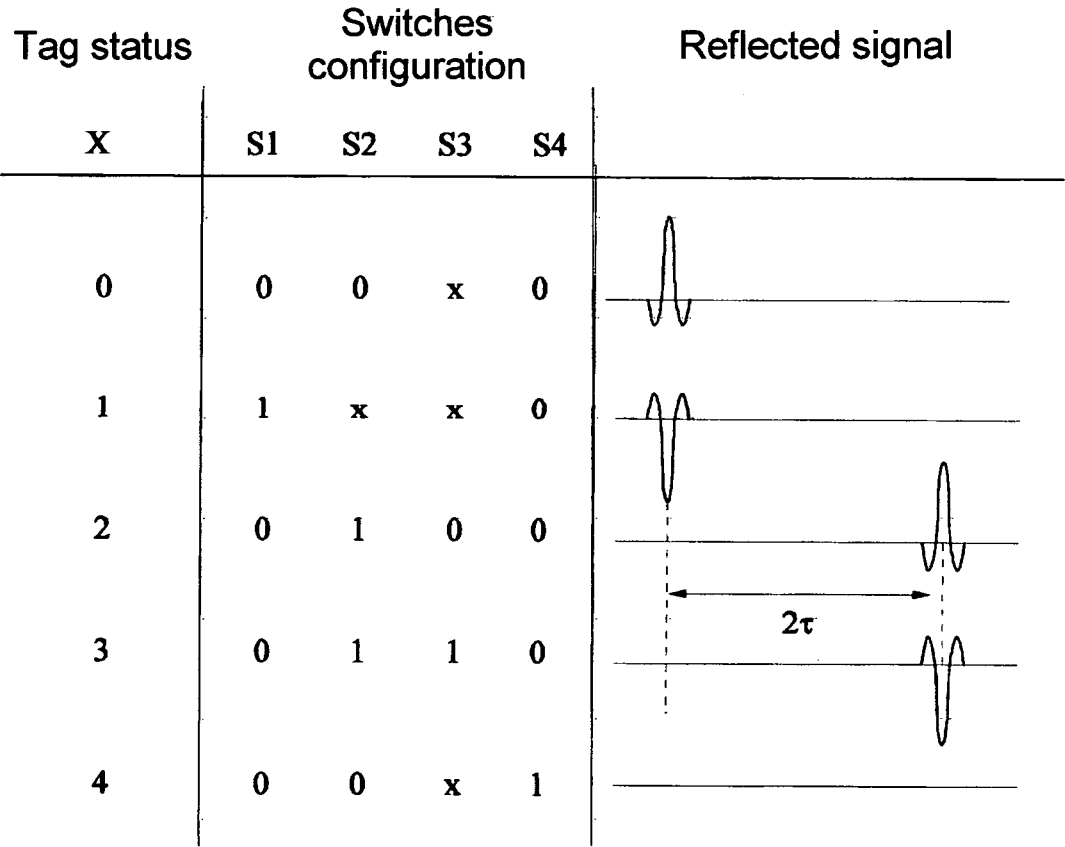


Fig. 5

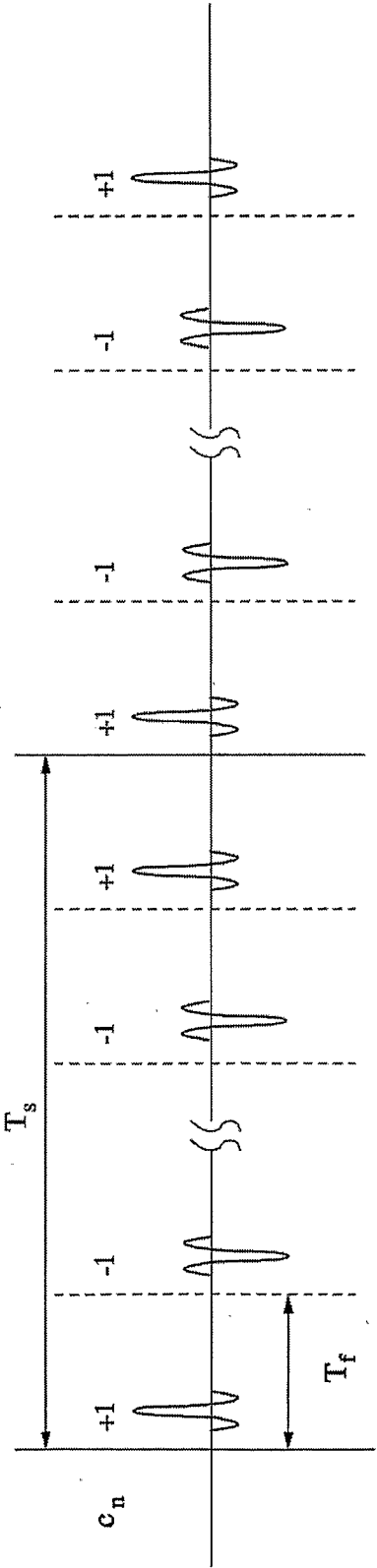


Fig. 6

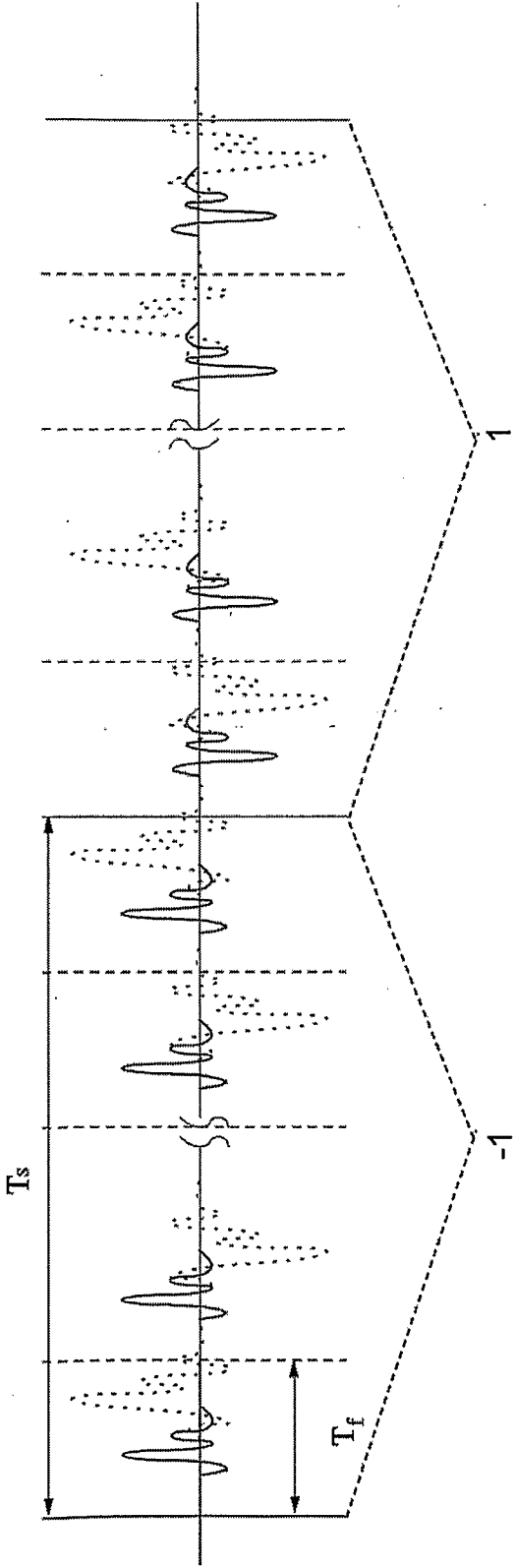


Fig. 7

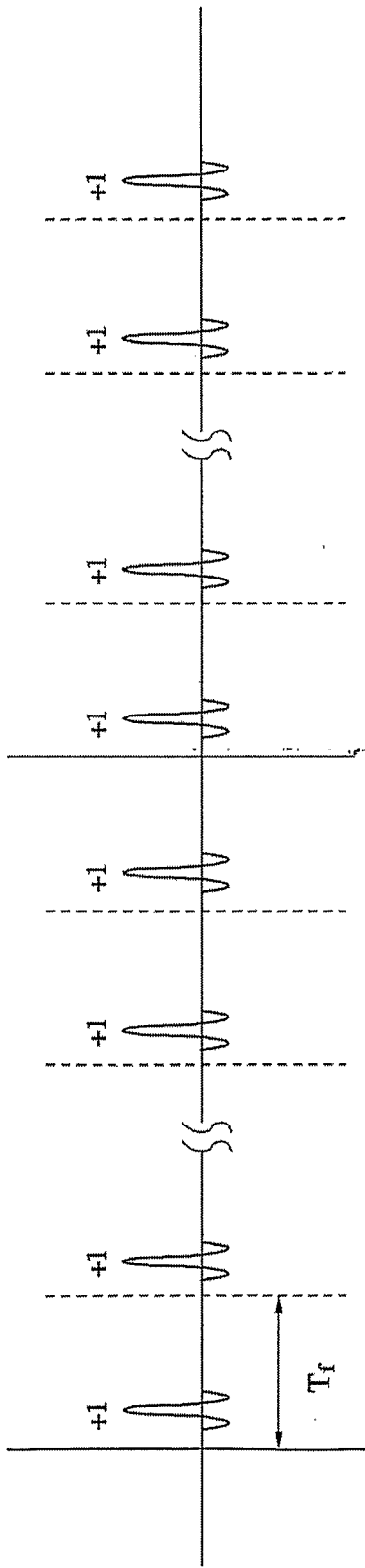


Fig. 8

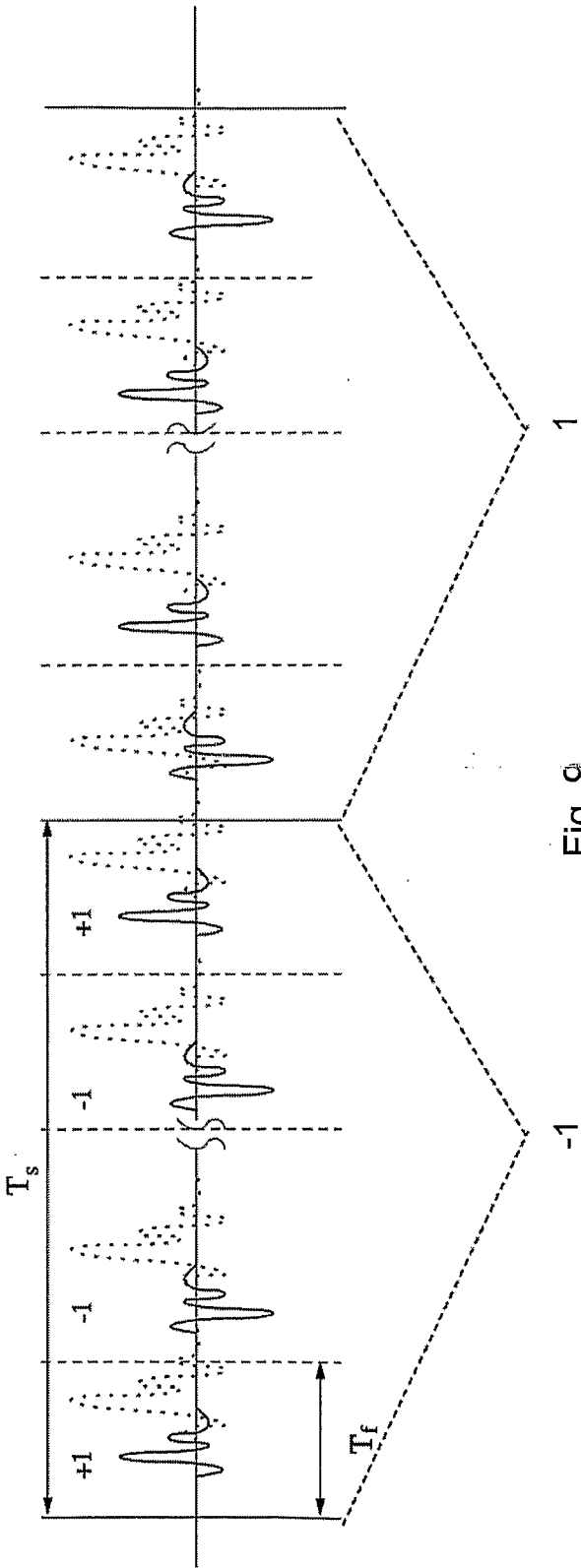


Fig. 9