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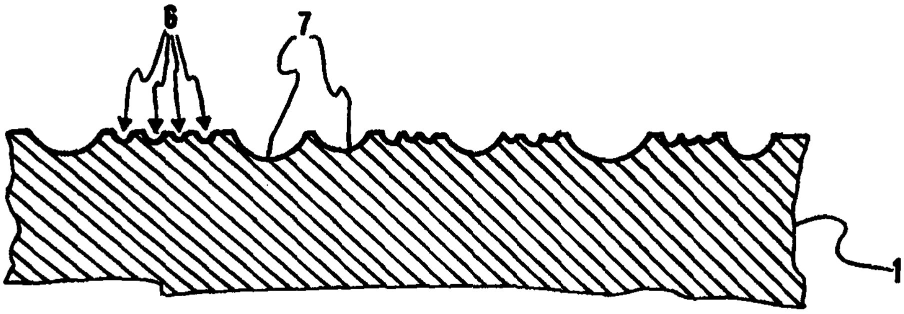
(54) Title: SURFACE OF A COOLING ROLL FOR CONTINUOUS CASTING MACHINES



(57) Abstract

A cooling roll having superficial wrinkles, for continuous casting machines with a pair of counterotating rolls in contact with the cast metal is characterized by the fact that it presents the surface that comes to contact with the cast metal provided with a first and a second dimensional order of cavities (6, 7) randomly spaced, and optionally, at least partially in contact between them; the strickle impressed on the roll surface (1) of each cavity (6, 7) of at least one of said first and second dimensional order being of poligonal or circular shape and, more preferably rhomboidal.

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SURFACE OF A COOLING ROLL FOR CONTINUOUS CASTING MASCHINES

DESCRIPTION

The present invention relates to an ingot mould roll for continuous casting machines and, more specifically, to the superficial conformation of the counterotating rolls of the ingot mold for the metal strip production.

Usually, strips are obtained by a conventional process that provides for the continuous casting of the flat bloom, followed by an eventual beveling, flat bloom heating and hot-rolling.

This process requires a great energy consumption for the flat blooms heating and for processing of the material. On the other hand, the continuous casting process of strips is a technique that enables to produce slim strips, directly as a cast product, thus eliminating the beveling and hot-rolling processes and maintaining the cold-rolling for the slimmer thicknesses only.

Therefore, in the case of a continuous casting of the strips the conditioning of their surfaces is clearly impossible, and it is therefore absolutely necessary that the strip be produced with the all but total absence of surface flaws. To obtain this result the solidification of the strip close to the ingot mold roll has to be piloted.

To solve this problem different solutions are available in art. One solution is based on the embodiment of predetermined gaps on the ingot mold surface. For instance, in the european patent application EP O 493 290 A1, a mobile wall for the metal solidification is described wherein a suitable wrinkledness is embodied on a copper chaplet, and whose cavities thereof are filled with a lower conductivity metal. Thus, a surface is created wherein an alternance is present between higher and lower thermal exchange zones.

Moreover, in the european patent EP O 309 247 B1 that result is obtained by making a series of cavities, of circular or oval shape, and with a regular disposition on the surface of each ingot mold roll.

In both cases a strip is produced with a wrinkled surface thereof. In the applications wherein the surface aspect is determinant this fact causes problems, as even the subsequent processes may be inadequate to restore the original wrinkledness. Moreover, the aforementioned solutions do not solve the problem on those roll surface zones that are left unaffected by the process, and therefore wherein very intense thermal exchanges occur.

Finally, in the first case the necessity of filling the cavities with a second metal and, in the second case, the necessity of emboding regularly spaced cavities on the roll surface, entails a great complexity and therefore a high cost of the embodiment and of the subsequent ingot mold maintainance.

Therefore, the present invention aims at solving the aforementioned drawbacks and at providing an ingot mold wherein the heat extraction and the metal solidification are functions of the ingot mold design, rather than of the inherent features of the material.

Therefore, the invention provides a cooling roll possessing surface wrinkles, for continuous casting machines with a pair of counterotating rolls in contact with the molten metal, characterized in that the surface wrinkles thereof consist in a multiplicity of cavities of a first and a second dimensional order, unevenly spaced on its surface, and optionally, being at least partially in contact among them.

According to the invention, the first order of cavities serves to the purpose of reducing the thermal flux between the solidifying metal and the roll. The depth of these cavities may vary between 2 and 10 μm, and their equivalent diameter is comprised between 10 and 50 μm.

Always according to the invention, the second order of cavities serves to the purpose of creating local gaps. Thus, the solidification is piloted by making it discrete rather than continuous, thereby breaking up and reducing the stresss caused by the shrinking that cause the strip flawing. By virtue of the presence of the first order of cavities that performs a first reduction of the thermal flux, this second order is constituted of cavities of different shapes and of dimensions contained in an equivalent diameter comprised between 0.2 and 1 mm, while the depth of each cavity thereof is comprised between 40 and 200 μm, with a consequent advantage for the surface aspect of the strip.

The fact that the cavities are randomly spaced on the roll's surface helps in the breaking and reducing of stresses due to the shrinkage, avoiding any preferential direction in which single stresses can combine locally, rising higher values able to cause micro-macro defects.

Moreover, the distance between each of the first order cavities is comprised from 0 to 60 μm, while the distance between each of the second order cavities is comprised from 0 to 1.5 mm.

Furthermore, the strickle impressed on the roll surface of each cavity of at least one of said first and second orders of cavities has a shape selected from the group comprising the polygonal and the circular shape and, more preferably, rhomboidal.

According to the invention, the surface of each roll that comes in contact with the cast metal is constituted of a material having a thermal conductivity comprised between 15 and 380 W/m·K. and is embodied in a material selected from the following group: steel, copper, nickel and chrome, and/or their alloys, selected in order to provide the constancy of cavities for the entire rolls life

Advantageously, according to the present invention, with an appropriate webbing of the ingot mold surface, the system is capable of producing flawless strips possessing a controlled wrinkledness such that it can be restored in the subsequent processes.

Specifically, according to the present invention, the webbing is obtained with a peening process of the surface of the rolls, in order to produce cavities on the same roll surface.

Advantageously, according to the present invention, cavities are closely distributed, randomly spaced, of shape that may vary according to the kind of shots employed and anyhow characterized in that it comprises the presence of two different orders of cavity. Thus, the solidification is piloted by making it happen in a discrete rather than continuous way, thereby breaking up and reducing the stresses due to the shrinking that cause the strip flawing.

An illustrative and comparative example will be disclosed hereinafter, given by way of explanation and not for limitative purposes, of the behaviour of a metal, initially liquid, when it is cooled in an ingot mold according to an embodiment of the present invention and according to an ingot mold of the state of the art, with reference to the annexed drawings wherein:

Figure 1 is a schematic sectional view showing the surface of a roll modified according to the present invention;

Figures 2a, 2b and 2c are schematic views showing the behaviour of a cast metal when it is solidified on a smooth surface;

Figures 3a and 3b are schematic views representing the behaviour of a cast metal when it is solidified on a surface according to the present invention; and

Figure 4 is a diagram reporting the values of the probability index of crack formation on steel strips depending on the strip temperature and on the smooth surface typology of a roll and for a surface modified according to the present invention.

Example

In this example the cast metal is austenitic inox steel AISI 304 as metal to be solidified with the shape of a strip with a 3 mm thickness. The sequence shown in figs. 2a, 2b and 2c reports the behaviour of that material when it is solidified on a smooth cooled copper chaplet.

With reference to fig.2a, in it the surface of a roll 1 as an element of an ingot mold is schematically represented. The surface is smooth and is in contact with a cast metal. It can be evidenced how the steel begins to solidify at the meniscus 3 of the ingot mold, forming a thin layer 2 of an all but uniform thickness of the order of 70-100 μm.

Then, according to figure 2b, the thin layer 2 detaches itself off the roll, and as it is a very thin and not very resistant structure, it is subject to great instability, therefore creating random waving with a variable pitch of around 30-80 mm. In this condition, the existence of waves causes the formation of an air space 4 of variable thickness between strip and roll, with maximum detachment values of the order of 20 μm. As a consequence, heat extraction from the strip becomes remarkably uneven and temperature differences of over 120 °C are generated on the strip surface, as the strip zones more detached from the roll remain very hot.

Then, as it can be noted in figure 2c, the solidified thickness 2 increases in an uneven way, with the forming of relevant thinnings 5 correspondingly to the zones that are more detached from the roll. When the ferrostatic pressure reaches a predetermined value equal to about 10 cm of depth off the meniscus, the same pressure brings again the strip in contact with the roll and the wavings gradually disappear. Nevertheless, even if temperature differences lessen, they persist until the exiting of the strip from under the rolls. However, correspondingly to zones 5 that present the most significant thinnings of the thickness, high values of tensile stress are generated, where the surface temperature is of the order of 1370 - 1390 °C and the

AISI 304 steel ductility is very low, thereby leading to the forming of cracks.

With reference now to figure 1 and to figures 3a and 3b, in them and in a schematic way the surface of a generic roll 1 is shown modified according to the present invention. Specifically, the thermal exchange mechanism changes drastically when in presence of a surface modified according to the present invention.

According to figure 3a, the intense initial thermal exchange is significantly curbed by the presence of a multiplicity of small cavities 6, and, moreover, as the steel 2 does not seep completely into a second multiplicity 7 of larger cavities , there is a slight delay in the solidification of the same correspondingly to the latter.

In the first instants of the solidification, near the meniscus 2 there is no forming of a thin layer of an all but uniform thickness (as is the case with the smooth surface roll), but instead the forming of completely solidified zones 8 interconnected by zones 9 still in a pasty state.

In this condition therefore, the detaching of the thin layer off the roll with the ensuing forming of waves does not take place. Thus, the strip surface reaches the complete solidification at an approximate depth of 10 cm off the meniscus when the ferrostatic pressure succeeds in keeping the strip adherent to the roll.

According to figure 3b, only from this moment onwards states of tensile stress are triggered in the strip, reaching the maximum values thereof on the surface of the colder zones near to the cavities 6 and 7. As it can be noted from the figure, there are zones 10 wherein stress states have an intensity that is much lower than those occurring on a strip cast with smooth surface rolls.

With reference now to figure 4, in it a diagram is shown, reporting the values of the probability index of crack forming on steel AISI 304 strips, depending on the latter temperature, and on the typology of a smooth roll surface and for a surface modified according to the present invention.

As it can be noted, the crackability index is significantly better for a roll with a surface peened according to the present invention, in an interval comprised between 1370 and 1390 °C, i.e. in the low ductility zone of the AISI 304 steel, in which the forming of cracks mainly occurs.

The present invention is not limited to the embodiment example described above, but comprises any embodiment variant whatsoever. To men skilled in the art further aims and advantages will be evident that the present invention possesses in other embodiment forms comprised in the scope of the appended claims.

CLAIMS

1. A cooling roll having wrinkles on its surface, for continuous casting machines with a pair of counterotating rolls in contact with the molten metal, characterized in that the wrinkles on its surface consist in a multiplicity of cavities having a first and a second dimensional order, unevenly spaced on its surface, and optionally, being at least partially in contact among them.

2. The cooling roll for continuous casting machines according to claim 1, wherein each cavity of said cavities of the first dimensional order has an equivalent diameter comprised between 10 and 50 μm and a depth comprised between 2 and 10 μm.

3. The cooling roll for continuous casting machines according to claim 1 or 2, wherein each cavity of said cavities of the second dimensional order has an equivalent diameter comprised between 0.2 and 1 mm and a depth comprised between 40 and 200 μm.

4. The cooling roll for continuous casting machines according to claims 1 to 3, wherein the distance between each of the cavities of the first dimensional order is comprised from 0 to 60 μm.

5. The cooling roll for continuous casting machines according to any one of the claims from 1 to 4, wherein the distance between each of the cavities of the second dimensional order is comprised from 0 to 1.5 mm.

6. The cooling roll for continuous casting machines according to any one of the preceeding claims, wherein the strickle of each cavity inpressed on the surface of the roll of at least one of said first and second dimensional order has a shape selected from the group comprising the polygonal and the circular shape.

7. The cooling roll for continuous casting machines according to the preceeding claim, wherein said polygonal shape of said cavity is substantially rhomboidal.

8. The cooling roll for continuous casting machines

according to any one of the preceeding claims, wherein the surface in contact with the cast metal is constituted of a material having a thermal conductivity comprised between 15 and 380 W/m·K.

9. The cooling roll for continuous casting machines according to any one of the preceeding claims, wherein said surface destined to come to contact with the cast metal is embodied in a material selected from the group:

- steel
- copper
- nickel
- chrome

and/or their alloys.

10. Ingot mold for machines for the continuous casting of metal strips characterized by the fact of comprising two counterotating rolls according to any one of the claims from 1 to 9.

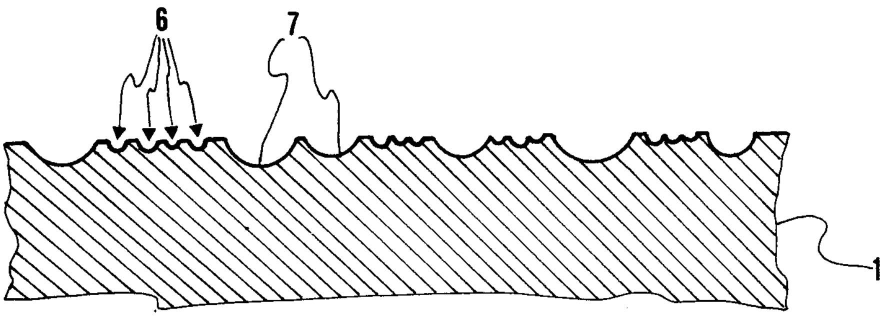

FIG 1

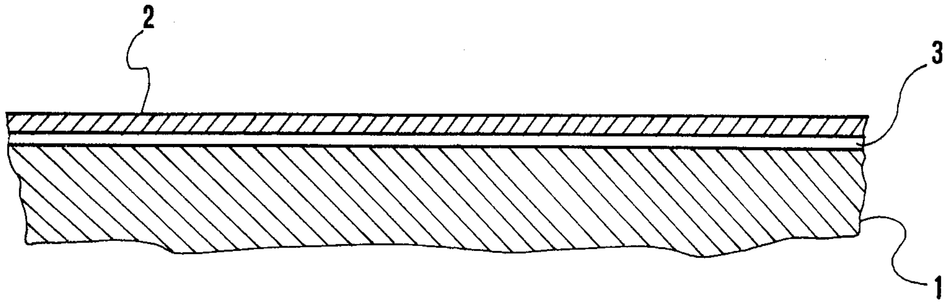

FIG 2A

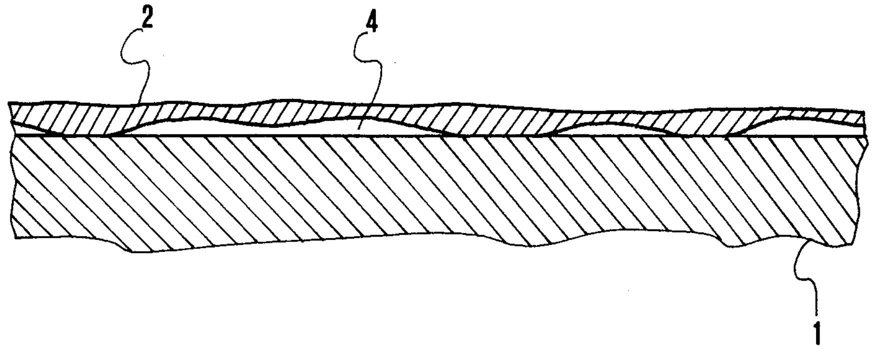

FIG 2B

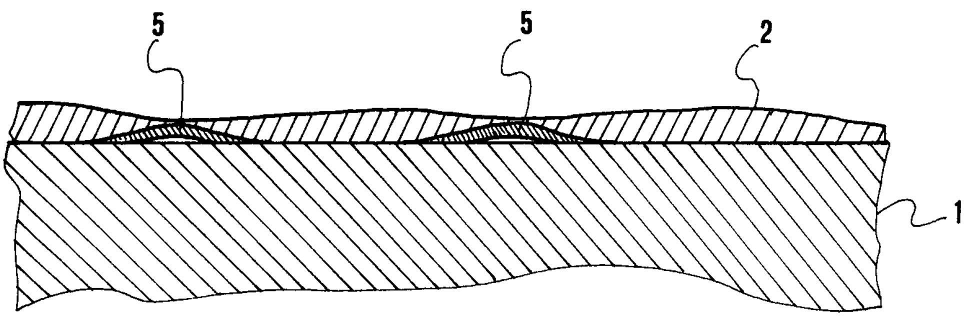

FIG 2C

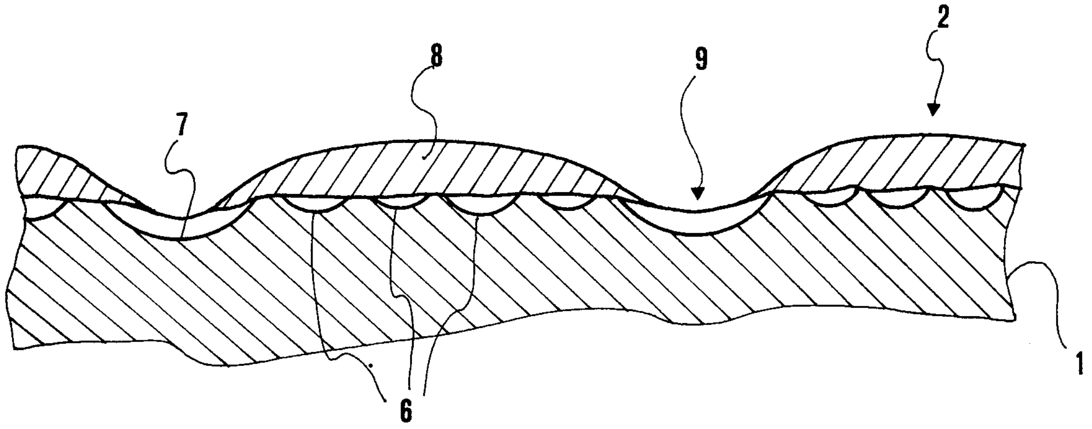

FIG 3A

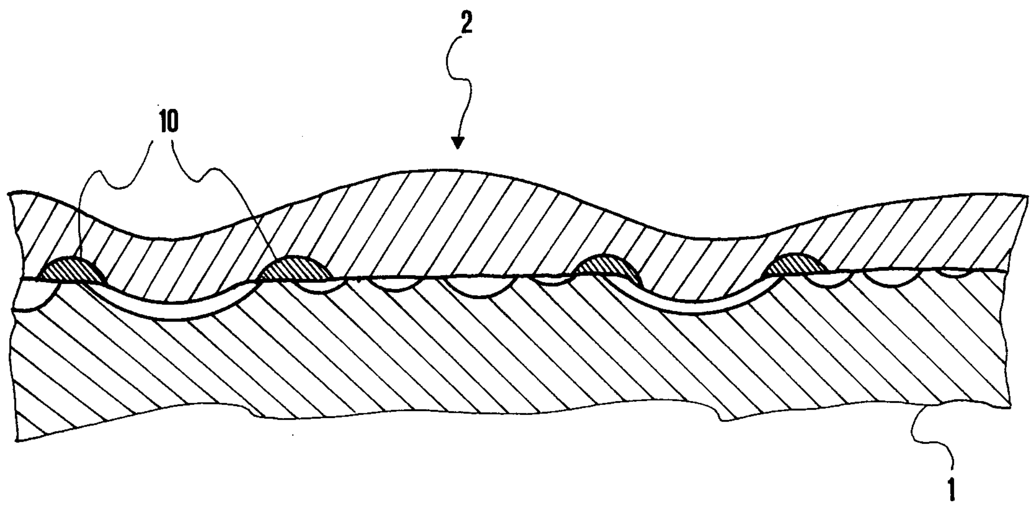

FIG 3B

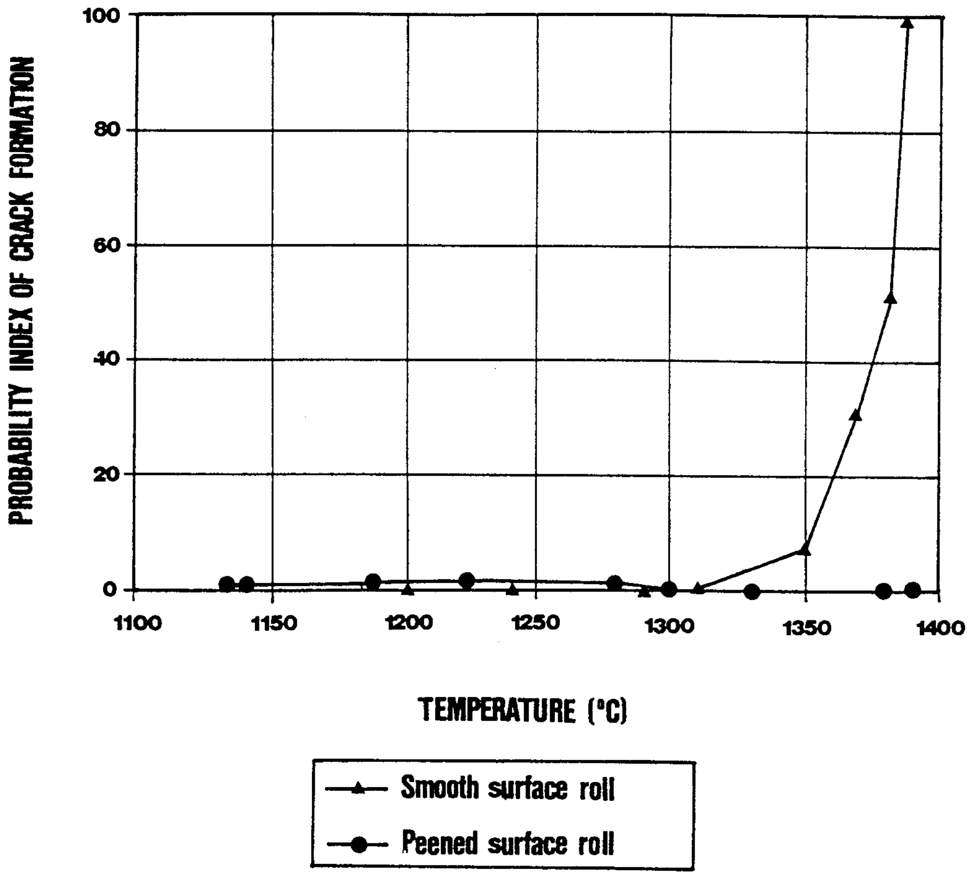
100
80
60
40
20
0
PROBABILITY INDEX OF CRACK FORMATION
1100
1150
1200
1250
1300
1350
1400
TEMPERATURE (°C)
Smooth surface roll
Peened surface roll

FIG. 4

INTERNATIONAL SEARCH REPORT

Inte onal Application No
PCT/IT 98/00319

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 B22D11/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 B22D B21B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0 309 247 A (NIPPON STEEL CORP ;MITSUBISHI HEAVY IND LTD (JP)) 29 March 1989 cited in the application	1-10
A	EP 0 463 177 A (NIPPON STEEL CORP) 2 January 1992 see claims; figure 3	1-10
A	US 4 027 716 A (THEOBALD REINER ET AL) 7 June 1977 see claim 4	9

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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