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DESCRIPTION

Cross-reference to Related Applications

[0001] This application claims the benefit of and priority to U.S. Application Serial No. 61/915,370, filed December 12, 2013, and U.S. Application Serial No. 62/011,410, filed June 12, 2014, and U.S. Application Serial No. 61/915,396, filed December 12, 2013.

Field of the Disclosure

[0002] The present disclosure is directed to urinary catheter products and, more particularly, to flushable catheters which include a surface treatment or coating that reduces friction to allow for easier and less traumatic insertion into and through the user's urethra.

Background

[0003] Flushable urinary catheter products are desirable. However, to date only oil-based coatings have proved feasible for use with flushable catheters because water-based coatings dissolve or degrade these water-soluble, flushable catheters. Flushable catheters with oil-based coatings have lubricity values that, while better than gel products, may not always be as high as the lubricity values for hydrophilically coated catheters. This could be a problem for customers who desire flushable catheters with hydrophilic type lubricity values. An example of a degradable urinary catheter can be found in EP-A-2301595.

Summary

[0004] The present disclosure provides flushable catheters that include hydrophilic outer coatings, as described in the claims. The catheters disclosed herein are catheters that structurally break down when contacted by water for convenient disposal down a toilet and through the sewer system. The catheters disclosed herein may be made from one or more materials that are affected by a fluid (for example, water, urine or fluids utilized in toilet and plumbing systems). Such materials may be water disintegratable or disintegratable materials. As used herein "water disintegratable" or "water disintegrable" materials refer to materials that are water soluble, water degradable, or water hydrolysable, and which dissolve, degrade, or otherwise break down when in contact with water over a selected period of time. In other examples, the material may be enzymatically hydrolysable. The water disintegratable and enzymatically hydrolysable materials are preferably flushable materials which are suitable for disposal in a toilet or sanitary system and, even more preferably, biodegradable flushable

materials which may be chemically broken down by living organisms or other biological means.

[0005] In one embodiment, the water disintegrable, flushable catheter has a catheter shaft that is made from a bi-layer tube that has a biodegradable outer layer (such as polylactic acid or polylactide, PLA) that will support the hydrophilic coating even when it's wetted with, for example, water or an aqueous solution. The outer layer bonds well to the water disintegrable inner layer but also allows a hydrophilic coating to be applied on top of the outer layer. The biodegradable outer layer also serves as a barrier that prevents or slows water from contacting the water disintegrable inner layer of the catheter shaft prior to and during use. The coating can be activated at point of use or just before it.

[0006] In another example, the water disintegrable flushable catheter includes a catheter shaft formed from a water disintegrable material wherein the hydrophilic coating is applied directly to the outer surface of the catheter shaft. The hydrophilic coating is active or wetted with a non-aqueous activation agent or a mixture of an activation agent and water. In this case the coating can be preactivated during manufacturing or packaging.

[0007] This is a water disintegrable, flushable catheter with a biodegradable outer layer that degrades via hydrolysis and/or dissolution and a purely water disintegrable inner layer, e.g., polyvinyl alcohol (PVOH). The outer layer breaks down at a slower rate than the inner layer and bonds well to the PVOH inner layer. The outer layer acts as a stable primer layer for hydrophilic style coatings. The outer layer acts as a temporary water barrier. This water barrier allows the hydrophilic coating to be hydrated but prevents water molecules attacking the PVOH substrate and causing the hydrophilic coating to fall off. The outer layer has been shown to be compatible with hydrophilic coatings. In one embodiment, the hydrophilic coating may be wetted just prior to use by the user.

[0008] In another aspect not being part of the invention, a flushable catheter includes a catheter shaft that is made from a water disintegrable material, such as PVOH, wherein the water disintegrable catheter is coated with a hydrophilic coating. The hydrophilic coating is wetted or activated with a non-aqueous wetting/activation agent, such as propylene glycol (PG), polyethylene glycol (PEG), tetra-ethylene glycol, glycerol and tri-ethylene glycol. In one alternative embodiment, the wetting agent includes a mixture of a non-water based composition, such as any of those mentioned above, and an amount of water. The water may be in an amount between about 0 wt% to about 20 wt%, between about 0 wt% to about 10 wt% or between about 0 wt% to about 5 wt%.

Brief Description of the Drawing

[0009] Fig. 1 is a longitudinal cross-section of a portion of a catheter having a bi-layer tube according to the present disclosure.

Detailed Description of the Embodiments

[0010] The present disclosure is directed to a water disintegrable flushable catheter that will dissolve, hydrolyze or biodegrade in water. It is coated with a hydrophilic coating and will achieve lubricity values typical of a hydrophilic catheter. In the past hydrophilic coatings have been problematic for water disintegrable catheters because they typically need water to hydrate the coating. While the coating will become lubricious on hydration, the substrate catheter will start to degrade and eventually become mechanically unstable. Thus, the water disintegrable catheter when in substantial contact with water in most instances will not support catheter functionality and will not support the hydrophilic coating. As the catheter breaks down the hydrophilic coating will become unstable and will not adhere to the catheter. Lab testing has confirmed this to be the case. It has also been shown that water-soluble outer layers such as polyvinylpyrrolidone (PVP) on top of PVOH will not overcome this problem even when cross-linked. In one embodiment, this disclosure provides a catheter that overcomes this problem by having a bi-layer catheter shaft tube that has a biodegradable outer layer (such as PLA) that will support the hydrophilic coating even when it's wetted. The outer layer bonds well to the water disintegrable inner layer but also allows a hydrophilic coating to be applied to the outer surface of the outer layer.

[0011] Fig. 1 illustrates portion of a catheter 10 according to the present disclosure. The catheter includes a catheter shaft that has a bi-layer tube 12 and a hydrophilic coating 14. In this embodiment, the tube 12 has a dual layer construction including a water disintegrable inner layer 16 and a biodegradable outer layer 18. The tube 12 may be made, for example, by coextrusion. A radial eyelet 20 extends through both layers 16, 18. A suitable tip (not shown) will be formed at the right end (as seen in Fig. 1) of the tube. Examples of suitable materials are PVOH for the inner layer 16 and PLA for the outer layer 18.

[0012] The biodegradable polymer outer layer 18 provides one or more of the following functionalities:

1. 1) It acts as a primer for the hydrophilic coating 14.
2. 2) It bonds well to the water disintegrable inner layer 16, which may be made of, for example, PVOH.
3. 3) Initially, the bi-tube outer layer 18 acts as a water barrier when the hydrophilic coating 14 is hydrated, i.e. outer layer 18 stops or slows the water molecules from contacting the inner PVOH layer 16 and thus prevents the inner PVOH layer 16 from dissolving too quickly and causing the catheter coating 14 to fall off or break up. This is due to the fact that the outer layer 18 degrades mainly via hydrolysis and not purely on the basis of its water solubility (if it's a blend). Outer layer 18 is a water disintegrable material that dissolves at a slower rate than the inner layer 16. This in turn means it will protect the inner layer 16 from the wetted hydrophilic coating 14 (or water molecules) because it will remain impervious to water for the required duration.
4. 4) The biodegradable outer layer 18 (e.g. PLA) is very thin. This means it will break down fast enough to meet flushability standards but will still protect the inner layer 16

long enough for full hydration of the hydrophilic coating 14 to occur and long enough for the patient to use the hydrophilically coated catheter 10. After the inner layer 16 dissolves first, a floppy outer skin will be left behind. It will flush easily and this skin is so thin (or is the correct blend of PLA/PVOH) so that it will break up into small enough pieces so that it will meet international standards for flushability. The PLA outer layer could be of low molecular weight so as to biodegrade very quickly and it could also have no cross linking so as to speed up the breakdown/dissolution of the outer layer once exposed to water. The PLA outer layer could also be blended with the likes of PVOH or PVP so as to facilitate a more rapid breakdown more suited to flushable products.

5. 5) The outer layer 18 can be any suitable biodegradable polymer (e.g. PLA) or co-polymer or blend. Polyesters, polyglycolide, polyglycolic acid, poly lactic-co-glycolic acid, polylactide may also be suitable materials. The outer skin can be a blend of a biodegradable polymer and a water-soluble polymer (e.g. PVOH) or it can be exclusively biodegradable and not necessarily water-soluble. For example, PVOH is known to accelerate the degradation of PLA by increasing the hydrophilicity of the blend film and by breaking the crystallinity of PLA. Therefore, the hydrophilicity and degradability of PLA/PVA blend film can be controlled in a certain range by adjusting the proportion of PLA and PVA. Reference Pub Med.gov, US national Library of Med Institutes of Health, Sheng Wu Yi Xue Za Zhi 2008 Feb;25(1):139-42.

[0013] Internal testing has shown that PLA tubes (with very rough surfaces) manufactured via laser printing techniques, with a hydrophilic coating, achieve lubricity values comparable to a hydrophilic product. Accordingly, tubes with an outer layer of PLA can be coated with hydrophilic type coatings and can achieve desirable lubricity levels.

[0014] Tests have also shown that PVOH tubing has poor solubility in ethanol and methanol and that PVOH tubes can be successfully coated with hydrophilic coatings from the above solvents. However, when the hydrophilic coated PVOH tubes are wetted (with 100% water) the coating falls off because the water molecules dissolve the surface of the water-soluble PVOH tubing. As confirmed by the testing in the preceding paragraph, this will not happen to a PLA (or equivalent) overcoat on top of a PVOH layer.

[0015] Other surface features can be included to optimize lubricity. For example, grooves could be formed on the PLA layers. These could further aid lubricity by protecting the hydrophilic coating that is in between the grooves from abrasion.

[0016] In an example, a water flushable catheter includes a shaft made from a water disintegrable polymer wherein the hydrophilic coating is applied directly to the water disintegrable material. In this example, the hydrophilic coating is wetted/activated with a non-aqueous composition or a mixture of a non-aqueous composition and an amount of water. Such non-aqueous compositions may include PG, PEG, tetra-ethylene glycol, glycerol or tri-ethylene glycol or mixtures thereof. In one example, the mixture includes the non-aqueous

composition and water wherein the amount of water is between about 0 wt% and about 20 wt% or between about 0 wt% and about 10 wt% or between about 0 wt% and about 5 wt% of the mixture. In one embodiment, the mixture includes PG and water. These non-aqueous compositions, alone or in a mixture with water, may also be used with a bi-layer tube as described above.

[0017] When non-aqueous compositions are used, alone or mixed with water, the catheter may be manufactured without the need for the customer to hydrate the coating immediately prior to use. That is, the hydrophilic coating may be activated during manufacturing or during packaging. This could be an advantage in terms of shelf life. It also retains the benefits of the product being "pre-hydrated" prior to the user opening the package and no manipulation would be required by the user to activate the coating. This may reduce the risk of spillage of the activation agent. Furthermore, packaged activated hydrophilic coating may be sterilized with ionizing radiation, such as gamma or e-beam radiation. For example, the packaged activated hydrophilic coating, which has been activated with a non-aqueous composition, may be sterilized with about 25kGy of gamma radiation.

[0018] The water disintegrable, flushable catheters disclosed herein provide the ability to utilize hydrophilic coatings on water disintegrable catheter shafts. Nobody would have expected one could have used such a coating on water disintegrable catheters because it would have been thought that the water used to activate the coating would have degraded the catheter to the point wherein the catheter could not be used. The water flushable catheters, however, provide a water disintegrable catheter that includes a hydrophilic or water based coating that achieves low CoF (coefficient of friction) values and can be flushed down the toilet for disposal thereof.

[0019] While the foregoing sets forth examples of suitable materials for making the flushable catheter of the present disclosure, it will be understood that other materials could be used. The catheter assembly may be made from one or more fluid (for example, water, urine or fluids utilized in toilet and plumbing systems) disintegrable materials. Such material may include, for example, water soluble, water hydrolysable or enzymatically hydrolysable materials, which dissolve or break down when in contact with water. The water disintegrable materials are preferably flushable materials which are suitable for disposal in a toilet or sanitary system and, even more preferably, biodegradable flushable materials which may be chemically broken down by water, living organisms or other biological means.

[0020] Such water disintegrable or enzymatically hydrolysable materials may include, for example, polyvinyl alcohol, including but not limited to an extrudable polyvinyl alcohol, polyacrylic acids, polylactic acid, polyesters, polyglycolide, polyglycolic acid, poly lactic-co-glycolic acid, polylactide, amines, polyacrylamides, poly(N-(2-Hydroxypropyl) methacrylamide), starch, modified starches or derivatives, amylopectin, pectin, xanthan, scleroglucan, dextrin, chitosans, chitins, agar, alginate, carrageenans, laminarin, saccharides, polysaccharides, sucrose, polyethylene oxide, polypropylene oxide, acrylics, polyacrylic acid blends, poly(methacrylic acid), polystyrene sulfonate, polyethylene sulfonate, lignin sulfonate, polymethacrylamides, copolymers of aminoalkyl-acrylamides and methacrylamides, melamine-

formaldehyde copolymers, vinyl alcohol copolymers, cellulose ethers, poly-ethers, polyethylene oxide, blends of polyethylene-polypropylene glycol, carboxymethyl cellulose, guar gum, locust bean gum, hydroxypropyl cellulose, vinylpyrrolidone polymers and copolymers, polyvinyl pyrrolidone-ethylene-vinyl acetate, polyvinyl pyrrolidone-carboxymethyl cellulose, carboxymethyl cellulose shellac, copolymers of vinylpyrrolidone with vinyl acetate, hydroxyethyl cellulose, gelatin, poly-caprolactone, poly(p-dioxanone), or combinations, blends or copolymers of any of the above materials. The water disintegrable or enzymatically hydrolysable materials may also be any of those that are included in certified flushable products that meet the National Sanitation Foundation standards for flushability or materials and products that meet INDA/EDANA Flushability Guidelines or the UK Water Industry Research, test protocols set forth in "Test Protocol to Determine the Flushability of Disposable Products, Review of the Manufactures 3rd Ed. Guidance Document," 2013, by Drinkwater et al. While catheters made from water disintegrable or enzymatically hydrolysable materials may be disposed of in a toilet, it is not necessary to dispose of such catheters in a toilet and such catheters may also be disposed in normal municipal waste systems or garbage collection systems.

Example I

[0021] CoFs of the coated and uncoated samples of PLA tubes, as an indicator of their lubricity, were measured using a Harland Friction Tester Model FTS5500. To determine the CoF of the tubes, a mandrel was inserted into 127 mm section of the coated or uncoated tube being tested. The tube was then clamped between two pieces of silicone rubber at 100g load wherein the silicone rubber had a Shore hardness of 60A. The tube with the mandrel inserted therein was pulled through the two pieces of silicone rubber at a speed of 10 mm/s. The force required to pull about 80 mm of the tube through the two pieces of silicone rubber was measured and recorded using a universal tensile tester equipped with a 200 N load cell. The CoF value was calculated from the ratio of recorded to applied loads (i.e., the recorded load divided by 2 times the applied load) when steady state was reached.

[0022] In a separate test, coated PLA tubes were abraded 25 times by passing the tubes through a hole which is just smaller than the outer diameter of the tubes. The hole was punched in a 1mm thick, silicone pad with Shore hardness of 60A. This test was designed to remove any portions of the coating that is not well adhered to the tubes. The CoFs of the abraded tubes were measured and an average CoF was calculated for each type of tube. Initial and abraded coefficient of friction (CoF) results, presented in the table below, are comparable to those for existing hydrophilic catheters.

Coefficient of Friction Values

Initial CoF	Abraded CoF (25 cycles)	Comment
0.0263	0.0263	These are very rough uneven and curved tubes. Results are very likely to improve with extruded bilayer tubing

Initial CoF	Abraded CoF (25 cycles)	Comment
0.0410	0.1204	These are very rough uneven and curved tubes. Results are very likely to improve with extruded bilayer tubing
Uncoated PLA control: 0.4248 (initial), 0.5478 (abraded)		

Example II

Tubes

[0023] A cross-head extrusion die was adapted to an injection moulding machine. Poly vinyl alcohol (PVOH) tubes were extruded at 195C. The extruded tubes were cooled with a pair of cooling inserts consisting of a split metal block mould with nominal diameter 5.2mm. The solid tubes were manually removed from the split mould after cooling.

Coating:

[0024] PVOH tubes were dipped coated in a Primer UV curable coating solution and cured for approximately 30s. Primed PVOH tubes were dipped in a Top Coat UV polyvinyl pyrrolidone UV curable coating and subsequently cured for approximately 10 minutes. Coated catheters were immersed in propylene glycol (PG) for 5 minutes to lubricate the coating (activated catheters). Activated catheters were left standing vertically for 5 minutes to remove the excess PG liquid by gravity. Thus, the initial CoF values shown in the table below correspond to CoF after 5 minutes of dipping the catheters into PG activation agent

Coefficient of friction (CoF):

[0025] CoF was measured using a Harland Friction Tester Model FTS5500. To determine the CoF of the tubes, a mandrel was inserted into 127 mm section of the coated or uncoated tube being tested. The tube was then clamped between two pieces of silicone rubber at 100g load wherein the silicone rubber had a Shore hardness of 60A. The tube with the mandrel inserted therein was pulled through the two pieces of silicone rubber at a speed of 10 mm/s. The force required to pull about 80 mm of the tube through the two pieces of silicone rubber was measured and recorded using a universal tensile tester equipped with a 200 N load cell. The CoF value was calculated from the ratio of recorded to applied loads (i.e., the recorded load divided by 2 times the applied load or 200g) when steady state was reached.

[0026] Coated tubes activated with PG were abraded 25 times by passing the tubes in air through a hoop 4.14mm in diameter (the relative diameters of the hoop and the tubes give an indication of the severity of the test). The hoop was punched in a 1mm thick, silicone pad with Shore hardness of 60A. This test was designed to remove any portions of the coating that is not well adhered to the tubes. The CoF of the abraded tubes were measured and an average CoF was calculated for each type of tube.

[0027] In a separate test, coated tubes activated with PG were left for an additional 10 minutes in the laboratory prior to testing the CoF. The table below shows a summary of 5 minutes, 15 minutes and abraded CoF (here 5 and 15 minutes is the time between the end of the dipping process in which PG is applied and the CoF test).

Sample no:	5 min CoF	Abraded CoF	15 min CoF
1	0.0512	0.0788	0.1117
2	0.1070	0.0959	0.1133
3	0.1035	0.0997	0.1026
4	0.1155	0.0930	0.0788
Average	0.0943	0.0918	0.1016

Example III

[0028] *Tubes:* PVOH tubes were manufactured by a traditional extrusion technique that used a water free cooling process..

[0029] *Coating:* PVOH tubes were dipped coated as in Example II. Coated catheters were immersed in 90% propylene glycol (PG) / 10% water for 5 minutes to activate the coating. Activated catheters were left standing vertically for 5 minutes to remove the excess PG/water by gravity. Thus, the initial CoF values shown in the table below correspond to CoF after 5 minutes of dipping the catheters into 90% PG/ 10% water activation agent

[0030] *Coefficient of friction (CoF):* CoF was measured using the same process as in Example II. Coated tubes activated with PG were abraded in air using the process of Example II. Then the tubes were abraded in water.

PVOH - Primer and Topcoat			
5mins Dwell in 90%PG / 10%Water			
Sample No.	Initial CoF	Abrasion In Air	Abrasion In Water
1	0.0461	0.1049	n/a
2	0.0475	0.0947	n/a
3	0.0441	0.1239	0.1425*

PVOH - Primer and Topcoat			
5mins Dwell in 90%PG / 10%Water			
Sample No.	Initial CoF	Abrasion In Air	Abrasion In Water
Average:	0.0459	0.1078	
SD:	0.0017	0.0148	

* Denotes that the sample had previously been abraded in air

Example IV

[0031] *Tubes:* PVOH tubes were prepared in the same manner as in Example III.

[0032] *Coating:* PVOH tubes were dipped coated as in Example II. Coated catheters were force hydrated in water for 30 seconds to activate the coating. Force hydrate in the context of Examples IV, V and VI means to soak or dip or completely immerse the sample in water for 30 seconds prior to CoF testing.

[0033] *Coefficient of friction (CoF):* CoF was measured using the same process as in Example II. Coated tubes activated with PG were abraded in air using the process of Example II. MO in this table means maxed out and the average value was recorded

PVOH - Primer and Topcoat		
30sec Force Hydrate in Water		
Sample No.	Initial CoF	Abrasion In Air
1	0.783	MO: 189.9
2	0.725	MO: 189.8
3	0.7002	MO: 170.9
Average:	0.7361	#N/A
SD:	0.0425	#N/A

Example V

[0034] *Tubes:* Tubes were prepared having a single layer of PLA. The PLA tubes in examples V and VI are PLA only, i.e., the tubes are made from a single layer/piece of PLA manufactured on a laser printer. The PLA tubes are then subsequently dipped into the Primer and or Topcoat and indicated by the Table heading.

[0035] *Coating:* PLA tubes were dipped coated as in Example II. Coated catheters were force

hydrated in water for 30 seconds to activate the coating.

[0036] *Coefficient of friction (CoF)*: CoF was measured using the same process as in Example II. Coated tubes activated with PG were abraded in air using the process of Example II.

PLA - Primer and Topcoat		
30sec Force Hydrate in Water		
Sample No.	Initial CoF	Abrasion In Water
1	0.0066	0.0065
2	0.0142	0.0141
3	0.0126	0.1189
4	0.0068	0.0296
Average:	0.0101	0.0423
SD:	0.0039	0.0520

Example VI

[0037] *Tubes*: Tubes were prepared having a single layer of PLA.

[0038] *Coating*: PLA tubes were dipped in a Top Coat UV polyvinyl pyrrolidone UV curable coating and subsequently cured for approximately 10 minutes. Coated catheters were force hydrated in water for 30 seconds to activate the coating.

[0039] *Coefficient of friction (CoF)*: CoF was measured using the same process as in Example II. Coated tubes activated with PG were abraded in air using the process of Example II.

PLA - Topcoat only		
30sec Force Hydrate in Water		
Sample No.	Initial CoF	Abrasion In Water
1	0.0232	0.0526
2	0.0136	0.0105
3	0.0625	0.1596
4	0.1451	0.074
Average:	0.0611	0.0742
SD:	0.0599	0.0628

It should be understood that various changes and modifications to the presently preferred embodiments described herein will be apparent to those skilled in the art. Such changes and modification can be made without departing from the scope of the invention disclosed herein.

REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

- [US61915370A \[0001\]](#)
- [US62011410A \[0001\]](#)
- [US61915396A \[0001\]](#)
- [EP2301595A \[0003\]](#)

Non-patent literature cited in the description

- **SHENG WU YI XUE ZA ZHI**Reference Pub Med.govUS national Library of Med Institutes of Health20080200vol. 25, 139-42 [\[0012\]](#)
- Test Protocol to Determine the Flushability of Disposable Products**DRINKWATER**Review of the Manufactures 3rd Ed. Guidance Document20130000 [\[0020\]](#)

Patentkrav

- 1.** Udskylleligt urinkateter, der omfatter:
et tolagsrør, som har et vandopløseligt inderlag og et biologisk nedbrydeligt yderlag, hvor yderlaget opløses ved en langsommere hastighed end inderlaget; og en hydrofil belægning på yderlaget.
- 2.** Udskylleligt urinkateter ifølge krav 1, hvor yderlaget er fremstillet af polymælkesyre.
- 3.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, hvor inderlaget er fremstillet af polyvinylalkohol.
- 4.** Udskylleligt urinkateter ifølge et hvilket som helst af kravene 1-3, hvor yderlaget er fremstillet af et materiale, der nedbrydes via hydrolyse.
- 5.** Udskylleligt urinkateter ifølge et hvilket som helst af kravene 1 og 3, hvor yderlaget er fremstillet af et materiale, der nedbrydes via opløsning.
- 6.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, hvor yderlaget binder godt til inderlaget.
- 7.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, hvor yderlaget fungerer som et stabilt primerlag for den hydrofile belægning.
- 8.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, hvor yderlaget fungerer som en midlertidig vandbarriere, der muliggør, at den hydrofile belægning kan hydratiseres, men forhindrer vandmolekyler i at angribe inderlaget.
- 9.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, der endvidere omfatter mindst én rille dannet på den ydre overflade af yderlaget.
- 10.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, hvor tolagsrøret omfatter et co-ekstruderet rør.
- 11.** Udskylleligt urinkateter ifølge et hvilket som helst af de foregående krav, hvor yderlaget omfatter en blanding af polymælkesyre og polyvinylalkohol.

DRAWINGS

