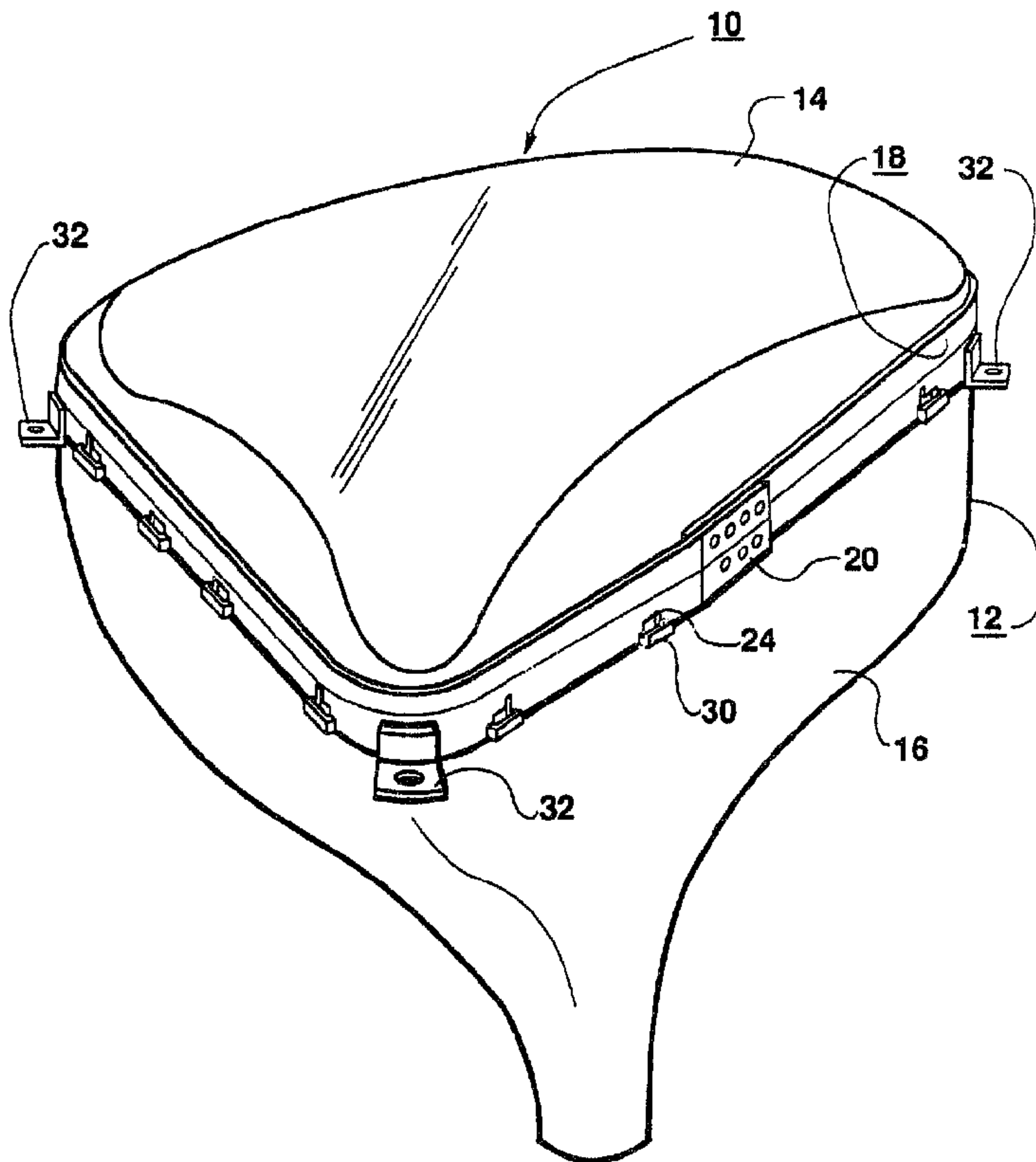




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(54) Titre : TUBE CATHODIQUE A BANDE ANTI-IMPLOSION THERMORETRACTABLE A DISPOSITIF LIMITEUR DE TENSION  
 (54) Title: CATHODE-RAY TUBE HAVING A SHRINKFIT IMPLOSION PROTECTION BAND WITH TENSION LIMITING MEANS



(57) Abrégé/Abstract:

A cathode-ray tube comprises an evacuated envelope which includes a faceplate panel joined to a funnel. A shrinkfit implosion protection band of at least one strip of metal, having oppositely disposed ends, is secured at a connective joint to form a loop with cold dimensions slightly smaller than the periphery of the panel prior to application of the band. The band has a given

**(57) Abrégé(suite)/Abstract(continued):**

sectional area with at least one opening formed therethrough. The band is fitted around the periphery of the panel to apply a compressive force thereto, as a result of the tension of the band. The band is improved by providing at least one slot within the band and in communication with the opening, to reduce the sectional area of the band sufficiently to lower the tension of the band below the minimum design limit of the connective joint.

ABSTRACT OF THE DISCLOSURE

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5 A cathode-ray tube comprises an evacuated envelope which includes a faceplate panel joined to a funnel. A shrinkfit implosion protection band of at least one strip of metal, having oppositely disposed ends, is secured at a connective joint to form a loop with cold dimensions slightly smaller than the periphery of the panel prior to application of the band. The band has a given sectional area with at least one opening formed therethrough. The band is fitted around the periphery of the panel to apply a compressive force thereto, as a result of the tension of the band. 10 The band is improved by providing at least one slot within the band and in communication with the opening, to reduce the sectional area of the band sufficiently to lower the tension of the band below the minimum design limit of the connective joint.

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CATHODE-RAY TUBE HAVING A SHRINKFIT IMPLOSION  
PROTECTION BAND WITH TENSION LIMITING MEANS

5 This invention relates generally to cathode-ray tubes (CRT's) having implosion protection bands and, more particularly, to such tubes having shrinkfit implosion protection bands with tension limiting means formed therein.

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15 A cathode-ray tube is evacuated to a very low internal pressure and accordingly is subject to the possibility of implosion due to the stresses produced by atmospheric pressure acting on all surfaces of the tube. This problem has been addressed in the art by providing the CRT with an implosion protection band. Such a band is used to apply a compressive force to the sidewall of a faceplate panel of the CRT to redistribute some of the forces. The redistribution of the forces decreases the probability of an implosion of the tube, by minimizing tension in the corners of the panel. An implosion protection band is also beneficial because it improves the impact resistance of the tube. Glass in compression is stronger than glass which is in tension, and the band causes compression in panel areas which otherwise would be in tension. Additionally, in the event of an implosion, the redistributed stresses cause the imploding glass to be directed toward the back of the cabinet in which the tube is mounted, thereby substantially reducing the probability of someone in the vicinity of the imploding tube being injured.

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35 An implosion protection band of the shrinkfit type typically is manufactured by forming a strip of steel into a loop having the same configuration as the faceplate panel to be protected, and joining the two ends of the strip on one side of the band. In some instances, the band is made by joining two identical

1 strips, on two sides, to form the loop. For both types of  
bands, the periphery of the loop is slightly smaller  
than the periphery of the faceplate panel. The loop is  
5 heated to approximately 300° to 500°C, and the  
coefficient of expansion of the material causes the loop  
to expand to dimensions permitting the loop to be  
slipped around the sides of the faceplate panel. As the  
band cools, it shrinks and tightly surrounds the panel,  
10 thereby applying the necessary implosion protection  
compression to the faceplate panel. The compressive  
force can be accurately controlled by exceeding the  
yield point of the metal in the band.

The ends of the strips are permanently joined by  
15 either welding or crimping. In either event, because  
the strip is used to apply substantial pressure to the  
sidewall of the tube, it is essential that the  
connective joint, formed where the two ends are coupled  
together, be sufficiently strong to withstand the  
20 tension applied to it by the band. Typically, the  
connective joint is designed to withstand a minimum  
tension of 5000 pounds (2268 kg). Because the tension  
of the band is directly proportional to the yield strength  
of the material and its sectional area, any increase in  
25 the yield strength of the band material that is in  
excess of its maximum limit will exert a tension on the  
connective joint in excess of its minimum design limit  
and may cause the joint to fail.

30 A cathode-ray tube according to the present  
invention comprises an evacuated envelope which includes a  
faceplate panel joined to a funnel. A shrinkfit implosion  
protection band of at least one strip of metal, having  
35 oppositely disposed ends, is secured at a connective joint  
to form a loop with cold dimensions slightly smaller than  
the periphery of the panel prior to application of the  
band. The band has a given sectional area with

1 at least one opening formed therethrough. The band is  
fitted around the periphery of the panel to apply a  
compressive force thereto, as a result of the tension of  
the band. The band is improved by providing means,  
5 within the band and in communication with the opening,  
for lowering the tension of the band below the minimum  
design limit of the connective joint.

In the drawings:

10 Fig. 1 is a perspective view of a CRT with a  
novel shrinkfit implosion protection band according to  
the present invention.

Fig. 2 is a front view of the tube and band of  
Fig. 1.

15 Fig. 3 is a typical elongation curve for a  
material from which the band can be made.

Fig. 4 is an enlarged view of a segment of the  
novel band, showing an opening and slot with a degaussing  
coil-retaining clip disposed within the opening.

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With respect to Figs. 1 and 2, a CRT 10 comprises  
an evacuated envelope 12 having a faceplate panel 14  
joined by a frit seal, not shown, to a funnel 16. An  
25 electron gun, also not shown, closes the opposite end of  
the funnel.

A shrinkfit implosion prevention band 18, in the  
form of a loop with cold dimensions slightly smaller  
than the periphery of the panel 14, is fitted around the  
30 panel by heating the band within the range of 300° to  
500°C, to cause it to expand, and then allowing it to  
cool. The tension of the cooled band 18 applies a  
compressive force to the panel. The band 18 is formed  
by joining together the opposite ends of at least one  
35 steel strip to form a connective joint 20. In the  
present embodiment, the strip has an overall unfolded  
width of about 3.0 inches (76.2mm) and a thickness

1 within the range of 0.042 to 0.045 inch (1.07 to  
 1.14mm). An inch (25.4mm) of one edge 22 of the strip  
 is folded over, to provide a double thickness of material  
 on the faceplate-side of the band and to create a band  
 5 18 with an operable width, W, of about 2 inches  
 (50.8mm). A plurality of openings 24 are formed by,  
 e.g., lancing the band 18 adjacent to the opposite  
 unfolded edge 26. Each of the openings 24 has a base 28  
 spaced a distance, D, of about 0.375 inch (9.5mm),  
 10 from the edge 26. A narrow strip of the band material  
 bridges the opening 24. The strip is formed out of the  
 plane of the band 18, to define a clip-receiving retainer  
 30. Typically, the retainer 30 has a width,  $w_1$ , of  
 about 0.184 inch (4.67mm) and an effective length, L,  
 15 of about 0.78 inch (19.81mm), which is slightly less  
 than the length of the base 28. A mounting lug 32 is  
 attached to the band 18 at each of the corners. As  
 described thus far, the band 18 is conventional.

20 A problem with the conventional band 18 is that  
 variations in the yield strength or the thickness of the  
 material, above the maximum allowable values, could  
 result in a tension on the connective joint 20 in excess  
 of its minimum design limit of 5000 pounds, resulting in  
 a failure of the joint. The minimum design limit is the  
 25 minimum tension at which the joint 20 will fail. The  
 steel band material has a specified yield strength, Y,  
 in the range of 37,000 to 42,000 psi (26.0 to 29.5 kg/mm<sup>2</sup>).  
 The maximum thickness, t, of the material is 0.045 inch  
 (1.14mm). The effective width W' of the band is defined  
 30 as the overall width, 3.00 inches (76.2mm), less the depth  
 of the opening 24, 0.375 inch (9.5mm), or 2.625 inches  
 (66.7mm). The maximum tension on the joint 20, for material  
 having a yield strength of 42,000 psi (29.5 kg/mm<sup>2</sup>), is

$$\begin{aligned}
 35 \quad T_{\max} &= Y \times W' \times t \\
 T_{\max} &= 42,000 \text{ psi} \times 2.625 \text{ in} \times 0.045 \text{ in} \\
 &\quad (29.5 \text{ kg/mm}^2 \times 66.7 \text{ mm} \times 1.14 \text{ mm}) \\
 T_{\max} &= 4,961.25 \text{ pounds (2243 kg)}.
 \end{aligned}$$

1 The tension on the joint 20 is below the minimum design  
limit, and the joint will hold. However, tests have shown  
that, after forming and working, the steel strip has a  
yield strength as high as 47,000 psi (33.0 kg/mm<sup>2</sup>). The  
5 resulting tension on the joint 20 for this material is

$$T_1 = 47,000 \text{ psi} \times 2.625 \text{ in} \times 0.045 \text{ in} \\ (33.0 \text{ kg/mm}^2 \times 66.7 \text{ mm} \times 1.14 \text{ mm})$$

$$T_1 = 5551.88 \text{ pounds (2509 kg)}.$$

This latter value of tension may cause the joint 20 to  
10 fail.

To prevent failure of the joint 20, while still  
providing sufficient compressive force on the panel 18,  
the two openings 24 adjacent to each of the lugs 32 at  
the corners of the band 18 are modified to include a  
15 slot 34 which communicates with the openings 24. Each  
of the slots 34 has a slot base 36 with a length, l, of  
about 0.25 inch (6.35mm), and a depth, d, of about 0.30 inch  
(7.62mm). The depth, d, of the slot 34, in combination with  
the depth, D, of the opening 24, increases the effective  
20 overall depth to about 0.675 inch (17.1mm), thereby  
reducing the effective folded band width to 2.325 in (59.1mm).  
The resulting force on the joint 20, for steel strip having  
a thickness of 0.45 inch (1.14mm) and a maximum yield  
strength of 47,000 psi (33.0 kg/mm<sup>2</sup>), is then

$$25 \quad T_2 = 47,000 \text{ psi} \times 2.325 \text{ in} \times 0.045 \text{ in} \\ (33.0 \text{ kg/mm}^2 \times 59.1 \text{ mm} \times 1.14 \text{ mm})$$

$$T_2 = 4917.38 \text{ pounds (2223 kg)}.$$

Thus, even in the worst case situation of a  
maximum material thickness of 0.045 inch (1.14mm) and a  
30 yield strength of 47,000 psi (33.0 kg/mm<sup>2</sup>), the tension on  
the joint 20 will not exceed the minimum design limit of  
5000 pounds (2268 kg).

Prior to fitting the band 18 on the tube 10, the  
band is stretched to slightly exceed the elastic limit  
35 of the metal, thereby causing the band to yield and to  
apply a known, predictable tension on the tube. This is  
evident from Fig. 3, which shows that the tension remains  
substantially constant after approximately a 5% elongation.  
The band 18 is stretched by the method described in

1 Canadian patent application No.2029538-4 , filed on  
November 08, 1990.

A segment of the novel band 18 is shown in Fig.  
4. A clip 38 is disposed within the opening 24 in the  
5 band 18. The clip 38 engages the clip-receiving  
retainer 30 and accurately locates a degaussing coil 40  
relative to the tube, not shown. The slot 34 does not  
interfere with either the location or retention of the  
clip 38. By incorporating the slot 34 and the opening  
10 24 in each of the eight corner-adjacent positions,  
economy is achieved by forming both the opening and the  
slot in a single operation. Additionally, since the  
tension on the band 18 is greater near the corners than  
elsewhere, the greatest protection for the joint 20 is  
15 achieved by locating the slots 34 within the eight  
corner-adjacent openings 24, so that the tension is  
substantially uniformly distributed to each of the four  
corners of the band.

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CLAIMS

1. A cathode-ray tube comprising an evacuated envelope having a faceplate panel joined to a funnel, and a shrinkfit implosion protection band of at least one strip of metal having  
5 opposite ends secured together at a connective joint, said joint having a minimum design limit which if exceeded will cause failure of said joint, said band being formed into a loop with cold dimensions slightly smaller than the periphery of said panel prior to application of said band, said band having a given sectional area  
10 with at least one opening formed therein, said opening having a base spaced from an edge of said band and being provided to accommodate a tube-related member, and said band being fitted around the periphery of said panel to apply a compressive force thereto as a result of the tension of said band; wherein said band  
15 includes a slot in communication with said opening for lowering the tension of said band below the minimum design limit of said connective joint, said slot having a base with a dimension smaller than a dimension of said base of said opening, said tube-related member being located and retained within said opening without  
20 interference from said slot.

2. The tube according to claim 1, wherein said band has at least eight said openings formed therein, two of said openings being adjacent to each of the corners of said band, and said band includes eight said slots each in communication with a  
25 different one of said openings.

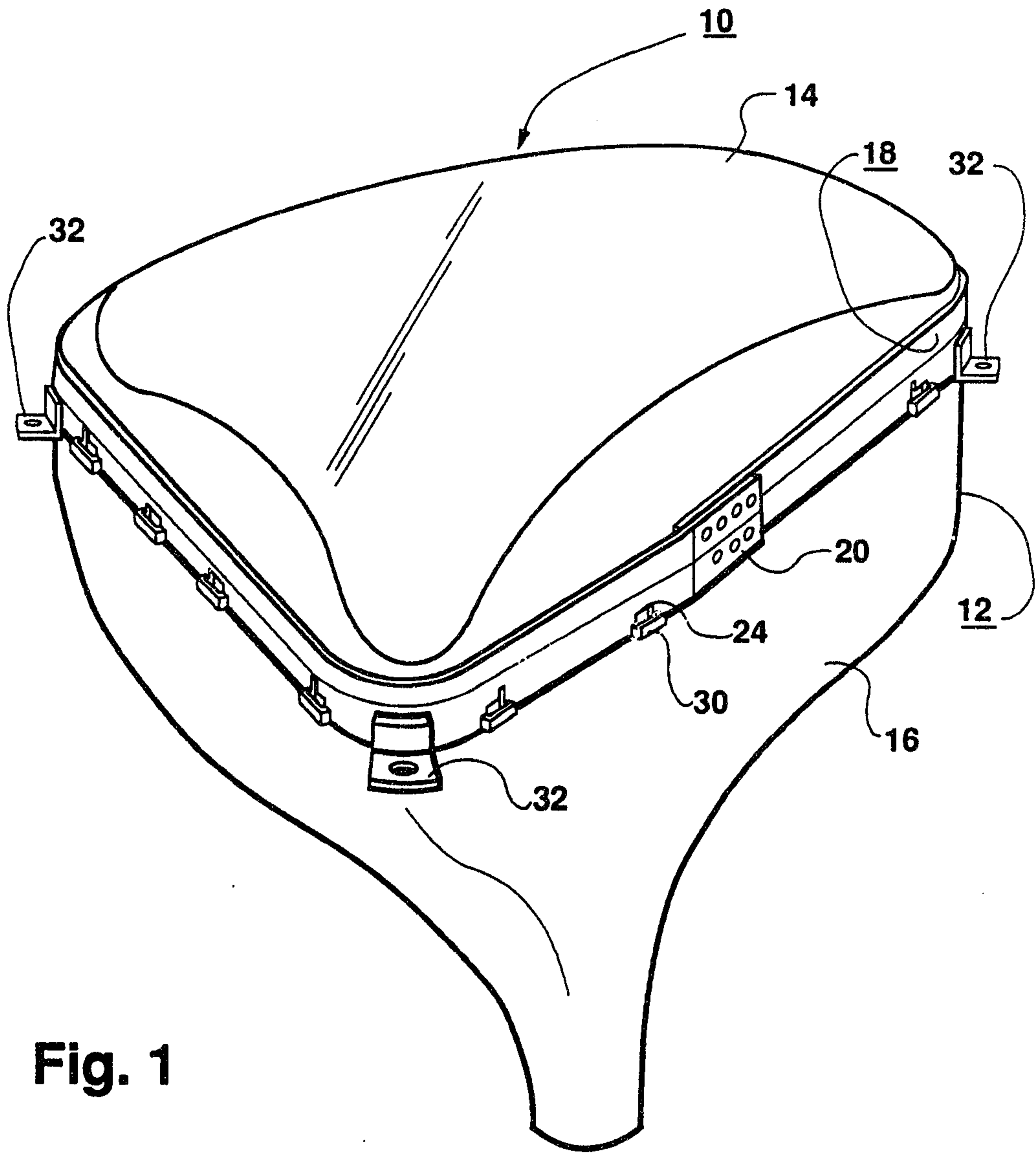


Fig. 1

Oltham and Weber

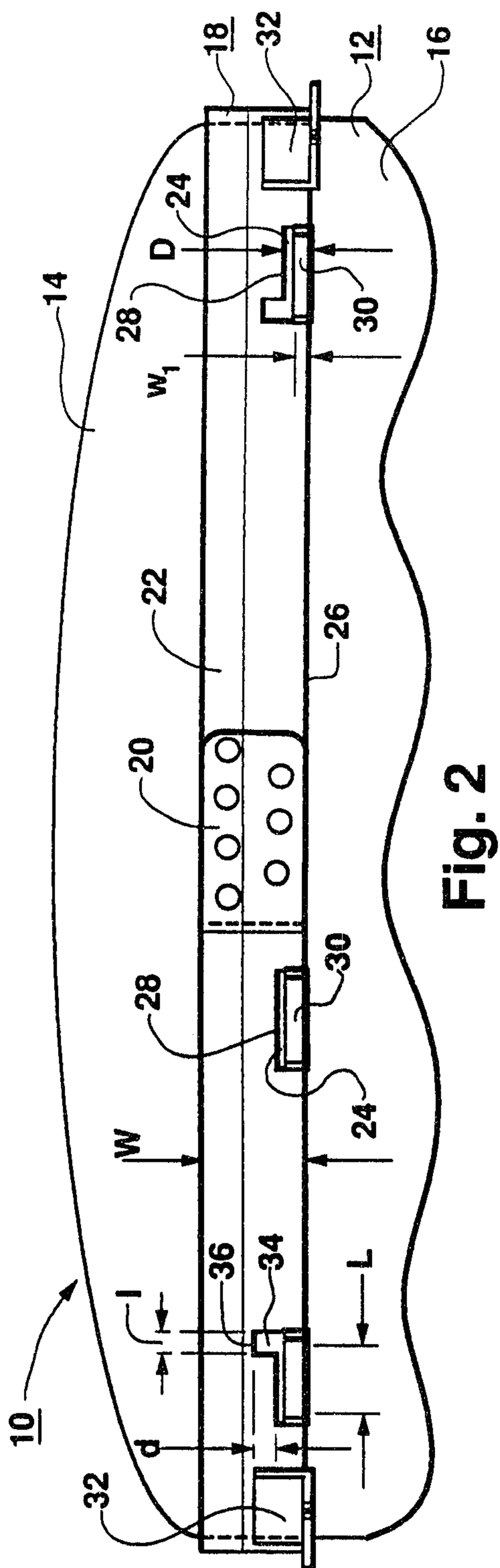


Fig. 2

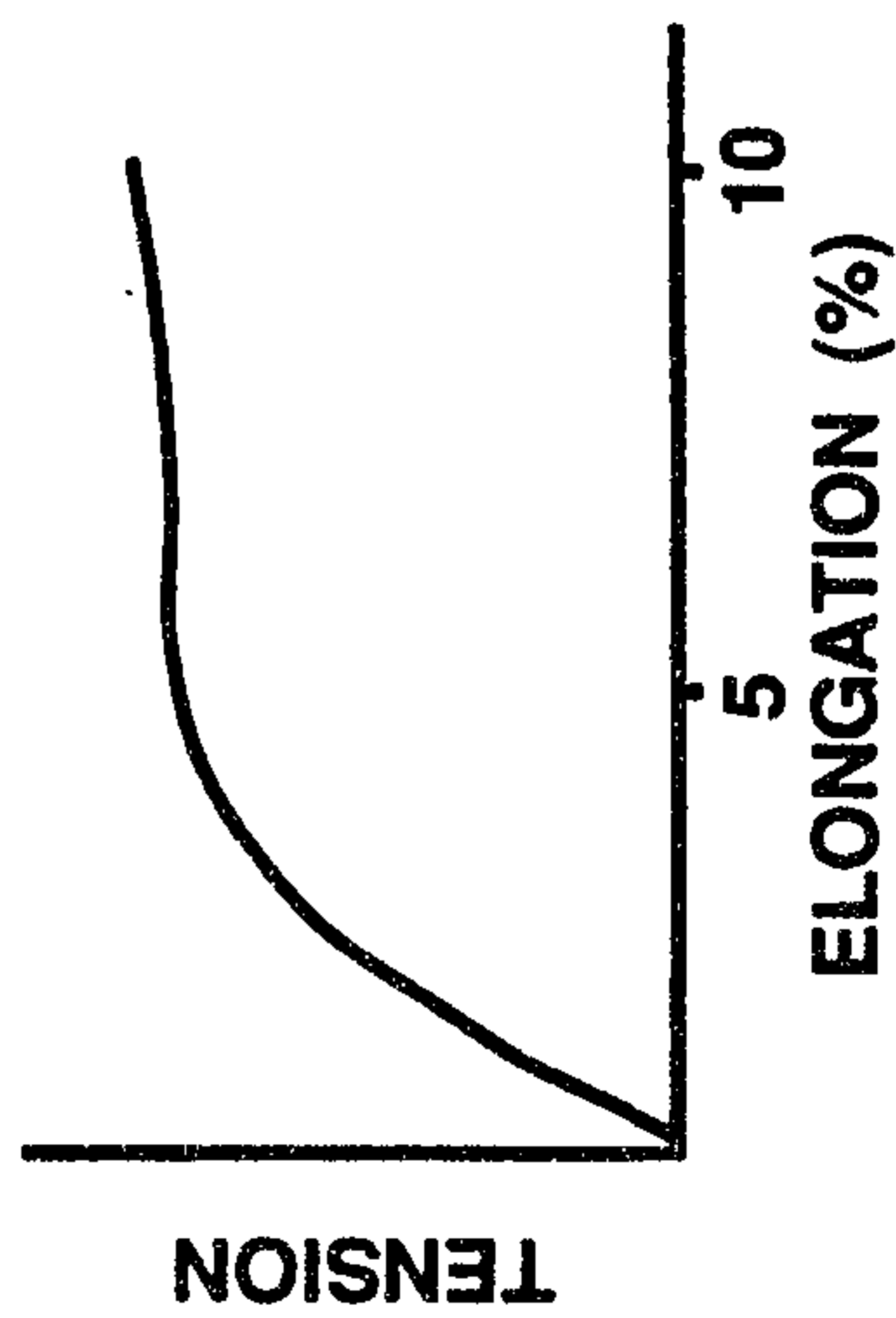
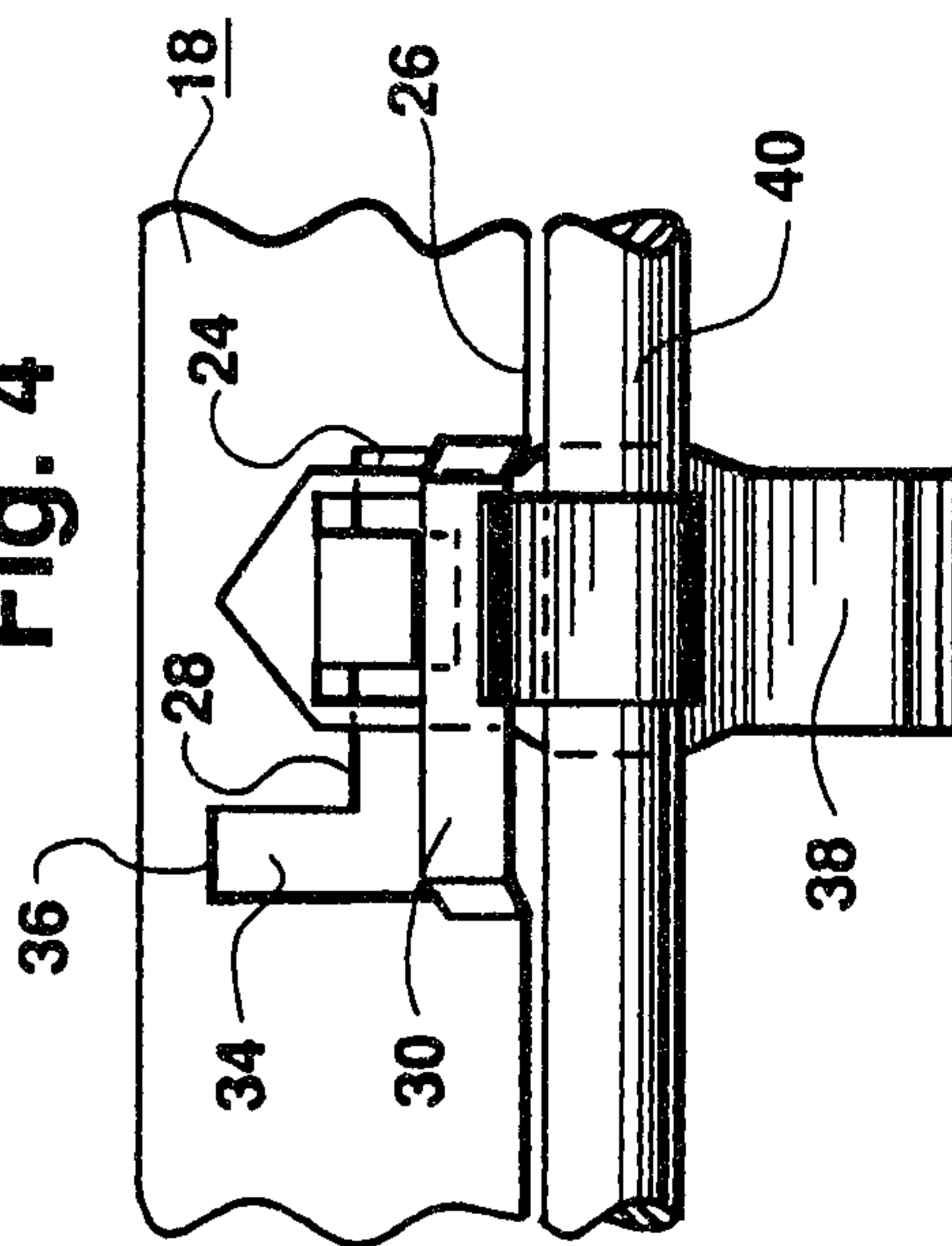


Fig. 4



Oldham and Wilde

