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(54) **HEAT EXCHANGER**

WÄRMETAUSCHER

ECHANGEUR DE CHALEUR

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- **MICROFILM OF THE SPECIFICATION AND DRAWINGS ANNEXED TO THE WRITTEN APPLICATION OF JAPANESE UTILITY MODEL, Application No. 153214/1987, (Laid-open No. 61566/1989) (TOYO RADIATOR CO., LTD.), 19-04-89.**

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Description

Technical Field

- 5 **[0001]** The present invention relates to a heat exchanging flowpassage comprising the features of the preamble of claim 1 and to a heat exchanging apparatus using a heat exchanging flow passage.

Background Art

- 10 **[0002]** In the past, nitrogen, oxygen, argon and other gases are stored in a superlow temperature storage tank in a liquefied state. When in use, the stored liquefied gas is fed to an evaporator where the gas is vaporized and gasified at an atmospheric temperature or in hot water.

- [0003]** However, in the past, cooling heat of the liquefied gas is not effectively utilized but is wasted. In order to effectively utilize the cooling heat to cool gases such as air, nitrogen, oxygen, argon, hydrogen, etc., or fluids such as a mixture of liquid and gas, etc., it is contemplated that a heat exchanger is intervened between a superlow temperature storage tank and an evaporator.

- [0004]** The conventional heat exchangers heretofore used have various configurations such as a coil type, a double tube type, a water injection type, a bushing type, a finned multitube type, etc.

- 20 **[0005]** The handbook H. Tietze, "Elemente des Apparatebaus", Springer-Verlag, Berlin, pages 216 and 217, published 1963, discloses a heat exchanger of the coil-type defining the preamble of claim 1 of the present invention.

- [0006]** However, the conventional heat exchangers as described above are poor in cooling effect because the fluid to be cooled flows through the tube regularly and is less affected by a temperature from wall surfaces of the tube. So, when being restricted as in an expansion valve at downstream in order to enhance the cooling effect, a large quantity of fluids cannot be cooled. Accordingly, there was a problem in that the conventional heat exchangers cannot be utilized in the case where a large quantity of fluids at a constant temperature need be secured.

- 25 **[0007]** The present invention is to overcome the problem as noted above with respect to prior art. It is an object of the present invention to provide a heat exchanging apparatus which can heat-exchange a large quantity of fluids efficiently without restricting the fluids, and accordingly, a large quantity of heat exchanging fluids at a constant pressure and at a constant temperature can be obtained and conveniently utilized, and in which the construction thereof can be simplified to thereby remove troubles and to lower the cost.

Disclosure of Invention

- 35 **[0008]** Technical means of the present invention for achieving the aforementioned object comprises a heat exchanging flow passage as defined in claim 1. The invention also relates to a heat exchanging apparatus as defined in claim 7. It is to be noted that the flowpassage termed herein means an article such as a tube through which fluid flows. The same is true for claims.

- [0009]** Preferably, in the aforementioned technical means, the heat exchanging flowpassage has tanks on the supply port side and on the discharge port side, and the supply path and the discharge path are communicated with the tanks.

- 40 **[0010]** According to the present invention constructed as described above, when the heat exchanging vessel is filled with the heat transfer medium and the fluid for heat exchange is supplied from the supply path to the heat exchanging flowpassage, the thus supplied fluid in the heat exchanging flowpassage flows into the plurality of the peripheral flowpassages arranged in parallel and the communicating flowpassages for communicating them. However, since the positions of the inlet and the outlet in the peripheral flowpassages are deviated in a peripheral direction, the fluid flows as a turbulence while repetitively impinging upon the wall surfaces of the heat exchanging flowpassages, during which the fluid can carry away heat of the heat transfer medium or heat of the fluid can be carried away by the heat transfer medium, and the fluid after heat exchange can be discharged outside the heat exchanging vessel from the discharge path. In this manner, the fluid is caused to flow in a turbulent state while repetitively impinging upon the wall surfaces of the heat exchanging flowpassages whereby the fluid is much affected by the temperature of the wall surfaces, and the fluids fed from the communicating flowpassages in the peripheral flowpassages are placed in the same condition and dispersed, thus enabling the effective heat exchange of a large quantity of fluids without restricting the fluids. Further, since the heat exchanging flowpassages can be configured by connection of flowpassages, the construction can be simplified.

- 55 **Brief Description of Drawings**

- [0011]** FIG. 1 is a perspective view of main parts showing a heat exchanging apparatus according to one embodiment of the present invention.

[0012] FIG. 2 is a schematic systematic view showing a using example in which the heat exchanging apparatus is incorporated between a superlow temperature storage tank for liquefied nitrogen and an evaporator.

[0013] FIG. 3 is a system constitutional view of an apparatus used for cooling experiments of dry air using the heat exchanging apparatus according to one embodiment of the present invention.

[0014] FIG. 4 is a graph showing the results of cooling experiments of dry air using a heat exchanging apparatus (a 2-stage ring type) according to one embodiment of the present invention (an axis of abscissa: passage time; an axis of ordinate: temperature of dry air to be discharged).

[0015] FIG. 5 is a graph showing the results of cooling experiments of dry air using a heat exchanging apparatus (a 5-stage ring type) according to one embodiment of the present invention (an axis of abscissa: passage time; an axis of ordinate: temperature of dry air to be discharged).

[0016] FIG. 6 is a table indicating the values every flow rate of dry air shown in the graph of FIG. 5.

[0017] The description of reference numerals used in the drawings is as follows:

2	Heat exchanging apparatus
3	Heat exchanging vessel
10	Heat exchanging flowpassage
11	Supply tube
12	Discharge tube
18	Annular tube (peripheral flowpassage)
19	Communicating tube
20	Tank on the supply port side
21	Tank on the discharge port side
100	Compressor
101	Flowmeter
102	Weight meter
103	Synflex tube (1/2 inch)
104	Liquid nitrogen (-196 °C)
105	Heat exchanger
106	Digital pressure gauge
107	Digital thermometer
108	Gas holder
109	Cooled dry air

Best Mode for Carrying Out the Invention

[0018] One embodiment of the present invention will be described hereinafter with reference to the drawings.

[0019] FIG. 1 is a perspective view of main parts showing a heat exchanging apparatus according to one embodiment of the present invention; and FIG. 2 is a schematic systematic view showing a using example in which the heat exchanging apparatus is incorporated between a superlow temperature storage tank for liquefied nitrogen and an evaporator.

[0020] As shown in FIG. 2, a superlow temperature storage tank 1 can store liquefied nitrogen at -196°C. The superlow temperature storage tank 1 has its bottom communicated with a bottom of a heat exchanging vessel 3 of a heat exchanging apparatus 2 according to the present invention by means of a tube 4, and a valve 5 is provided in the middle of the tube 4. An upper portion of the heat exchanging vessel 3 is communicated with an inlet of an evaporator 6 by means of a tube 8, and a supply tube 9 is communicated with an outlet of the evaporator 6. A heat exchanging flowpassage 10 is arranged within the heat exchanging vessel 3 of the heat exchanging apparatus 2 as will be described later, and a supply tube 11 and a discharge tube 12 for dry air inserted into the heat exchanging vessel 3 are communicated with the heat exchanging flowpassage 10. Valves 13 and 14 are provided in the middle of the supply tube 11 and the discharge tube 12, respectively, the discharge tube 12 being communicated with a tank 15. A plurality of supply tubes 16 are communicated with the tank 15, and a valve 17 is provided in the middle of each of the supply tubes 16.

[0021] The heat exchanging flowpassage 10 is composed of annular tubes 18 communicated in a circumferential direction which constitute peripheral flowpassages, communicating tubes 19 which constitute communicating passages, a tank 20 on the supply port side, a tank 21 on the discharge port side, and the like, as shown in FIG. 1. Plural rows (5 rows in the illustrated embodiment) of the annular tubes 18 are arranged in a parallel state so as to have a desired spacing in a vertical direction around a vertical axis. The annular tubes 18 adjacent to each other are communicated at plural locations by the communicating tubes 19 in a vertical direction. The communicating tubes 19 in each of upper and lower rows are arranged substantially at equal intervals while being alternately deviated in a peripheral direction to each other so that the positions of an inlet and an outlet at the annular tube 18 in each row are alternately

deviated in a peripheral direction, the inlet and the outlet being set so that the inlet and the outlet are not opposed on a straight line. The tank 20 on the supply port side and the tank 21 on the discharge port side are arranged on the lower inside and on the upper inside of the plural rows of the annular tubes 18. The tank 20 on the supply port side is communicated in its intermediate portion with the lowermost annular tube 18 by means of communicating tubes 22 arranged radially, and the tank 21 on the discharge port side is communicated in its upper end portion with the uppermost annular tube 18 by means of communicating tubes 23 arranged radially. The supply tube 11 is communicated with the bottom of the tank 20 on the supply port side, and the discharge tube 12 is communicated with the bottom of the tank 21 on the discharge port side.

[0022] The heat exchanging vessel 3, the annular tubes 18 constituting the said heat exchanging flowpassage 10, the communicating tubes 19, the tanks 20 and 21, the communicating tubes 22 and 23, the supply tube 11, and the discharge tube 12 are formed of materials which withstand a low temperature, for example, such as stainless steel and copper.

[0023] The operation of the aforementioned constitution will be explained hereinafter.

[0024] A liquefied nitrogen, which is a heat transfer medium, is supplied into and filled in the heat exchanging vessel 3 of the heat exchanging apparatus 2 by the tube 4 from the superlow temperature storage tank 1. The vessel 3 is applied with a heat insulating material 7 to prevent it from being frozen. In this state, dry air to be cooled by heat exchange is supplied to the tank 20 on the supply port side of the heat exchanging flowpassage 10 immersed with the liquefied nitrogen from the supply tube 11. The dry air supplied into the tank 20 flows into the lowermost annular tube 18 passing through the communicating tubes 22, and flows from the lowermost annular tube 18 into its upper annular tube 18 passing through the communicating tubes 19. Thereafter, the dry air sequentially flows into the upper level annular tube 18 passing through the communicating tubes 19, and flows from the uppermost annular tube 18 into the tank 21 on the discharge port side passing through the communicating tubes 23. In the tubes 18, 19, 22 and 23 and the tanks 20 and 21, cooling heat of the liquefied nitrogen, which is a refrigerant, is carried away from the wall surfaces thereof (that is, heat of dry air is carried away) to cool them while the dry air is flowing in a manner as described above. At this time, when the dry air flows into the lowermost annular tube 18 from the communicating tubes 22, it impinges upon the wall surface of the annular tube 18. Since the positions of the inlets in each row of annular tubes 18 are alternately deviated in a peripheral direction as described above and the inlet and the outlet are set so that they are not opposed, when the dry air flows into the annular tubes 18 from the communicating tubes 19, the dry air impinges upon the wall surfaces of the annular tubes 18 and is divided into left and right portions, and further impinges upon the dry air which likewise flows from the adjoining communicating tube 19 to impinge upon the wall surface of the annular tube 18, which dry air sequentially flows as a turbulence into the uppermost annular tube 18. In this way, the dry air repetitively impinges upon the wall surface and flows in a turbulent state which is much affected by the temperature of the wall surface, and dry air fed from the communicating tubes 19 on each line in the annular tubes 18 is placed in the same condition so that dry air does not flow only in a fixed line but is dispersed. Therefore, it is possible to efficiently carry away cooling heat of the liquefied nitrogen (that is, heat of dry air is carried away).

[0025] The same is true in the case where a part of the supply tube 11 is changed for that of the discharge tube 12 so that the supply tube 11 functions reversely to the discharge tube or the discharge tube 12 functions reversely to the supply tube.

[0026] The dry air cooled by the heat exchange as described above flows from the tank 21 into the tank 15 by the discharge tube 12, and can be distributed into using sites as desired by the plurality of the supply tubes 16. At each using site, the dry air can be mixed with air at normal temperature to adjust it to a suitable temperature for use. On the other hand, the liquefied nitrogen from which cooling heat was carried away by the heat exchange is introduced into the evaporator 6 by the tube 8 and vaporized at an atmospheric temperature or in hot water into nitrogen gas. The thus obtained nitrogen gas can be supplied to the using site as desired by the supply tube 9.

[0027] In the prior art, liquefied nitrogen is directly supplied to the evaporator 6. In the embodiment of the present invention, however, after being used for heat exchange by the heat exchanging apparatus 2, liquefied nitrogen is supplied to the evaporator 6, by which the temperature of liquefied nitrogen rises. Therefore, the evaporating efficiency obtained by the evaporator 6 can be improved.

[0028] The results of experiments on the cooling efficiency of dry air according to the embodiment of the present invention are given below. The experiments have been conducted under the following conditions.

Measured gas		
dry air	pressure dew point temperature	6.8 kg/cm ² less than -80 °C 9 °C

(continued)

Refrigerant gas		
liquid nitrogen	temperature	-196°C
	evaporation temperature	-188°C
	natural evaporation amount	0.05 kg/min

The system of the apparatus used for experiments is shown in FIG. 3.

[0029] The method of the present experiment may be summarized as follows:

1. Dry air for measurement was taken off through a 1/2 inch tube by a takeoff valve in the factory and supplied.
2. For obtaining the relationship between flow rate and pressure, a float type flowmeter was mounted at an inlet of a heat exchanger, and digital type pressure gauges were mounted at an inlet and an outlet.
3. All the heat exchanger were manufactured of SUS.
4. The heat exchanger was put into an SUS container applied with simple insulation and the container was internally filled with liquid nitrogen from an ELF. The container is of an open type with a lid merely placed.
5. For measuring the weight of the vaporized liquid nitrogen, the entire SUS container was placed on the weight meter to measure the weight from a change of graduations. The reduced value was measured every 30 seconds, and the mean value per minute of the same flow rate was obtained.
6. Dry air cooled by the heat exchanger was put into a gas holder by a 1/2 inch Synflex tube to measure a change of temperature by a digital type thermometer mounted on the holder.

[0030] The results of experiments are as shown in FIGS. 4 and 5.

[0031] FIG. 4 is a graph indicating temperatures of cooled dry air discharged from the heat exchanger with respect to the passage time from the start of supplying dry air in the case where a 2-stage ring type heat exchanger (in FIG. 1, two uppermost and lowermost annular tubes 18 are used, between which is connected the communicating tubes 19) was used.

[0032] The results of experiments may be summarized as follows:

1. The more flow rate of dry air, the heat exchanging efficiency for cooling is enhanced.
2. In the case where the flow rate of dry air is in the constant condition, an outlet pressure relative to an inlet pressure is substantially constant, and a variation of pressure rarely occurred.
3. A minimal temperature of dry air discharged reached to -162 °C, a cooling gas at a constant temperature relative to a constant flow rate was generated, and no variation of temperature occurred.
4. In the 2-stage ring, only cooling gas was discharged, and no liquefying phenomenon was found.
5. In 2 to 3 minutes after supply of dry air, a temperature reaches to approximately -160°C.

[0033] FIG. 5 is a graph indicating temperatures of cooled dry air discharged from the heat exchanger with respect to the passage time from the start of supplying dry air in the case where a 5-stage ring type heat exchanger was used.

[0034] As described above, according to the aforementioned embodiment, since a large quantity of dry air can be heat exchanged efficiently without restricting dry air, it is possible to obtain a large quantity of dry air cooled to a constant temperature. Further, since dry air is once stayed in the tank 20 on the supply port side from the supply tube 11, dry air can be supplied at constant pressure and at constant flow rate to the communicating tubes 19 in each line. Further, since dry air after cooled to a constant temperature from the communicating tubes 19 in each line is once stayed in the tank 21 on the discharge port side, it is possible to supply the dry air after cooled to the using site at constant pressure and at constant flow rate. It is possible to simply increase the quantity of dry air to be cooled by increasing a diameter, an area and a length of the annular tube 18, the communicating tube 19 or the like and a volume of the tanks 20 and 21.

[0035] While in the aforementioned embodiment, the tubes 18, 19, 11 and 12 having a circular section have been used for the peripheral flowpassage, the communicating flowpassage, the supply path, the discharge path or the like, it is to be noted that a square and an oval in section may be also used.

[0036] Further, the peripheral flowpassage is not limited to an annular shape but a square and an oval can be used. The communicating tubes 19 are not always arranged at equal intervals. The annular tubes may be different in diameter. The communicating tubes may not connect adjoining annular tubes, but for example, they may alternately connect annular tubes. Of course, as the heat transfer medium, there can be used, other than liquefied nitrogen, refrigerants such as liquefied oxygen, liquefied argon, LNG, etc. For the purpose of raising a temperature, a heating medium can be used. As a fluid subjected to heat exchange, there can be used, other than dry air, gases such as nitrogen, oxygen,

hydrogen, argon, natural gas, etc., and a mixture of liquid and gas. Further, alternatively, a plurality of rows of annular tubes 18 as peripheral flowpassages may be arranged in parallel in a lateral direction around a horizontal axis. Besides, the present invention can be variously changed in design within a scope not departing from the basic technical idea thereof.

[0037] As described above, according to the present invention, when the heat exchanging vessel is filled with the heat transfer medium and the fluid for heat exchange is supplied from the supply path to the heat exchanging flowpassage, the thus supplied fluid in the heat exchanging flowpassage flows into the plurality of the peripheral flowpassages arranged in parallel and the communicating flowpassages for communicating them. However, since the positions of the inlet and the outlet in the peripheral flowpassages are deviated in a peripheral direction, the fluid flows as a turbulence while repetitively impinging upon the wall surfaces of the heat exchanging flowpassages, during which the fluid can carry away heat of the heat transfer medium or heat of the fluid can be carried away by the heat transfer medium, and the fluid after heat exchange can be discharged outside the heat exchanging vessel from the discharge path. In this manner, the fluid is caused to flow in a turbulent state while repetitively impinging upon the wall surfaces of the heat exchanging flowpassages whereby the fluid is much affected by the temperature of the wall surfaces. Further, the temperature is lowered due to the turbulent expansion of the fluid, and the fluids fed from the communicating flowpassages in the peripheral flowpassages are placed in the same condition and dispersed without flowing in a specified communication flow passage, thus enabling the effective heatexchange of a large quantity of fluids without restricting the fluids. Accordingly, a large quantity of heat exchanging fluids at a constant temperature can be obtained and conveniently utilized. Further, since the heat exchanging flowpassages can be configured by connection of flowpassages, the construction can be simplified. Accordingly, troubles can be removed, and the cost can be lowered.

[0038] Moreover, the heat exchanging flowpassage has tanks on the supply port side and on the discharge port side, respectively, and the supply path and the discharge path are communicated with the respective tanks whereby the fluid is once stayed in the tank on the supply port side from the supply path and the fluid can be supplied to the communicating flowpassages in each line at constant pressure and at constant flow rate, and the fluid heat exchanged to a constant temperature is once stayed in the tank on the exhaust port side from the communicating flowpassages in each line and can be supplied to the using site at constant pressure and at constant flow rate, thus enabling further stable utilization.

Industrial Applicability

[0039] As described above, the heat exchanging apparatus according to the present invention is useful as a heat exchanging apparatus for air cooling and as a heat exchanging apparatus for air conditioning having a large capacity, and is suitable for use with a heat exchanging apparatus particularly for a freezing warehouse or the like which is large in scale and requires a low temperature.

Claims

1. A heat exchanging flowpassage (10) for a heat exchanging apparatus (2) comprising:

- a plurality of annular flowpassages (18) arranged substantially in parallel, and
- communicating flowpassages (19) communicating the annular flowpassages (18) at plural locations,

characterized in that

the communicating flowpassages (19) are alternately deviated in an annular direction to each other so that the positions of an inlet and an outlet at the each annular flowpassage (18) are alternately deviated in an annular direction.

2. A heat exchanging flowpassage (10) for a heat exchanging apparatus (2) according to claim 1,

characterized in that

the communicating flowpassages (19) between two annular flowpassages (18) are arranged substantially at equal intervals.

3. A heat exchanging flowpassage (10) for a heat exchanging apparatus (2) according to claim 1 or 2,

characterized in that

a supply port side tank (20) and a discharge port side tank (21) are provided.

4. A heat exchanging flowpassage (10) for a heat exchanging apparatus (2) according to claim 3,

characterized in that

the supply port side tank (20) is connected to one end of the annular flowpassages (18) and the discharge port side tank (21) is connected to the other end of the annular flowpassages (18).

- 5 5. A heat exchanging flowpassage (10) for a heat exchanging apparatus (2) according to claim 4,
characterized in that
one end of annular flowpassages (18) is connected to the supply port side tank (20) by communicating flowpassages (22).
- 10 6. A heat exchanging flowpassage (10) for a heat exchanging apparatus (2) according to claim 4 or 5,
characterized in that
the other end of annular flowpassages (18) is connected to the discharge port side tank (21) by communicating flowpassages (23).
- 15 7. A heat exchanging apparatus (2) comprising:
 - a heat exchanging vessel (3) to and from which a heat transfer medium is supplied and discharged,
 - a heat exchanging flowpassage (10) according to claim 1 to 6 provided within the heat exchanging vessel (3),
and
 - 20 - fluid supply path (11) and a fluid discharge path (12) communicated with the heat exchanging flowpassage (10).
8. A heat exchanging apparatus (2) according to claim 7,
characterized in that
the supply path (11) is connected to the supply port side tank (20) and the discharge path (12) is connected to the
25 discharge port side tank (21).

Patentansprüche

- 30 1. Wärmetauscher-Strömungskanal (10) für eine Wärmeaustauschvorrichtung (2), aufweisend:
 - mehrere ringförmige Strömungskanäle (18), die im wesentlichen parallel angeordnet sind, und
 - mehrere Verbindungs-Strömungskanäle (19), welche die ringförmigen Strömungskanäle (18) an mehreren
35 Stellen verbinden,

dadurch gekennzeichnet, dass
die Verbindungs-Strömungskanäle (19) in Umfangsrichtung zueinander versetzt abzweigen, so dass die Stellen einer Einlaßöffnung und einer Auslaßöffnung an jedem ringförmigen Strömungskanal (18) in Umfangsrichtung versetzt angeordnet sind.
- 40 2. Wärmetauscher-Strömungskanal (10) für eine Wärmeaustauschvorrichtung (2) nach Anspruch 1,
dadurch gekennzeichnet, dass
die Verbindungs-Strömungskanäle (19) zwischen zwei ringförmigen Strömungskanälen (18) im wesentlichen in gleichen Abständen angeordnet sind.
- 45 3. Wärmetauscher-Strömungskanal (10) für eine Wärmeaustauschvorrichtung (2) nach Anspruch 1 oder 2,
dadurch gekennzeichnet, dass
ein Tankbehälter (20) auf der Seite der Zuführöffnung und ein Tankbehälter (21) auf der Seite der Abführöffnung vorgesehen ist.
- 50 4. Wärmetauscher-Strömungskanal (10) für eine Wärmeaustauschvorrichtung (2) nach Anspruch 3,
dadurch gekennzeichnet, dass
der Tankbehälter (20) auf der Seite der Zuführöffnung an ein Ende der ringförmigen Strömungskanäle (18) angeschlossen ist und der Tankbehälter (21) auf der Seite der Abführöffnung an dem anderen Ende der ringförmigen
55 Strömungskanäle (18) angeschlossen ist.
5. Wärmetauscher-Strömungskanal (10) für eine Wärmeaustauschvorrichtung (2) nach Anspruch 4,
dadurch gekennzeichnet, dass

ein Ende der ringförmigen Strömungskanäle (18) durch Verbindungs-Strömungskanäle (22) an den Tankbehälter (20) auf der Seite der Zuführöffnung angeschlossen ist.

6. Wärmetauscher-Strömungskanal (10) für eine Wärmeaustauschvorrichtung (2) nach Anspruch 4 oder 5, **dadurch gekennzeichnet, dass** das andere Ende der ringförmigen Strömungskanäle (18) durch Verbindungs-Strömungskanäle (23) an den Tankbehälter (21) auf der Seite der Abführöffnung angeschlossen ist.

7. Wärmeaustauschvorrichtung (2), aufweisend:

- einen Wärmetauscher-Behälter (3), dem ein Wärmeübertragungsmedium zugeführt und entnommen wird,
- einen Wärmetauscher-Strömungskanal (10) nach den Ansprüchen 1 bis 6, der im Wärmetauscher-Behälter (3) vorgesehen ist, und
- einen Zuführkanal (11) und einen Abführkanal (12), welche an den Wärmetauscher-Strömungskanal (10) angeschlossen sind.

8. Wärmeaustauschvorrichtung (2) nach Anspruch 7, **dadurch gekennzeichnet, dass** der Zuführkanal (11) an den Tankbehälter (20) auf der Seite der Zuführöffnung angeschlossen ist und der Abführkanal (12) an den Tankbehälter (21) auf der Seite der Abführöffnung angeschlossen ist.

Revendications

1. Passage échangeur de chaleur (10) pour un appareil échangeur de chaleur (2), comprenant :

une pluralité de passages annulaires (18) agencés substantiellement en parallèle, et des passages de communication (19) faisant communiquer les passages annulaires (18) en une pluralité de positions,

caractérisé en ce que

les passages de communication (19) sont déviés alternativement suivant une direction annulaire les uns des autres de telle sorte que les positions d'une entrée et d'une sortie au niveau de chaque passage annulaire (18) soient déviées alternativement suivant une direction annulaire.

2. Passage échangeur de chaleur (10) pour un appareil échangeur de chaleur (2) selon la revendication 1,

caractérisé en ce que

les passages de communication (19) entre deux passages annulaires (18) sont agencés substantiellement à des intervalles égaux.

3. Passage échangeur de chaleur (10) pour un appareil échangeur de chaleur (2) selon la revendication 1 ou 2,

caractérisé en ce que

un réservoir de côté d'orifice d'alimentation (20) et un réservoir de côté d'orifice de refoulement (21) sont prévus.

4. Passage échangeur de chaleur (10) pour un appareil échangeur de chaleur (2) selon la revendication 3,

caractérisé en ce que

le réservoir de côté d'orifice d'alimentation (20) est connecté à une extrémité des passages annulaires (18) et le réservoir de côté d'orifice de refoulement (21) est connecté à l'autre extrémité des passages annulaires (18).

5. Passage échangeur de chaleur (10) pour un appareil échangeur de chaleur (2) selon la revendication 4,

caractérisé en ce que

une extrémité des passages annulaires (18) est connectée au réservoir de côté d'orifice d'alimentation (20) au moyen de passages de communication (22).

6. Passage échangeur de chaleur (10) pour un appareil échangeur de chaleur (2) selon la revendication 4 ou 5,

caractérisé en ce que

l'autre extrémité des passages annulaires (18) est connectée au réservoir de côté d'orifice de refoulement (21) au moyen de passages de communication (23).

7. Appareil échangeur de chaleur (2), comprenant :

- 5 une cuve échangeuse de chaleur à laquelle et depuis laquelle un milieu de transfert de chaleur est alimenté et refoulé,
un passage échangeur de chaleur (10) selon les revendications 1 à 6 prévu à l'intérieur de la cuve échangeuse de chaleur (3), et
10 une voie d'alimentation en fluide (11) et une voie de refoulement de fluide (12) en communication avec le passage échangeur de chaleur (10).

8. Appareil échangeur de chaleur (2) selon la revendication 7,

caractérisé en ce que

- 15 la voie d'alimentation (11) est connectée au réservoir de côté d'orifice d'alimentation (20) et la voie de refoulement (12) est connectée au réservoir de côté d'orifice de refoulement (21).

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FIG. 1

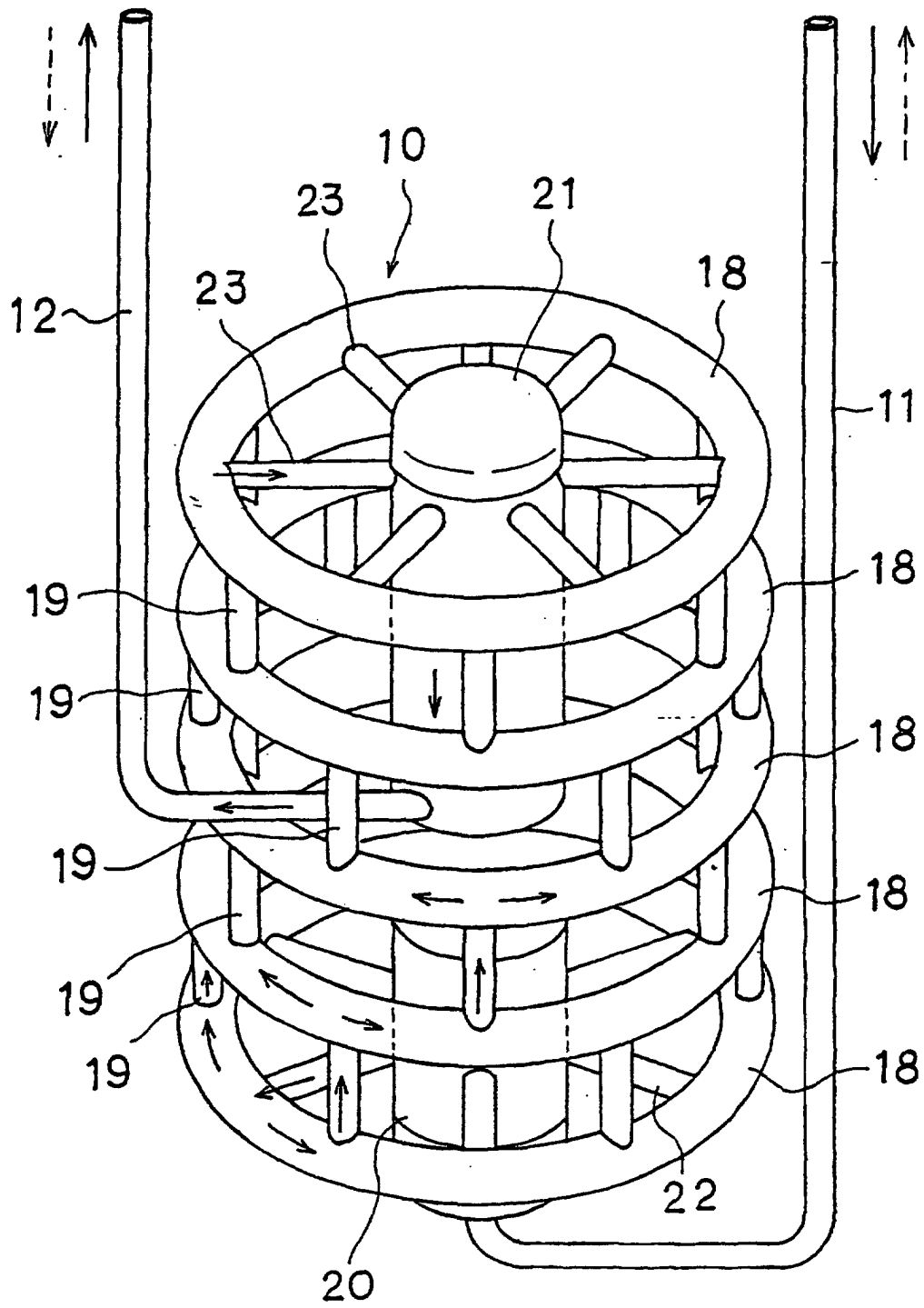


FIG. 2

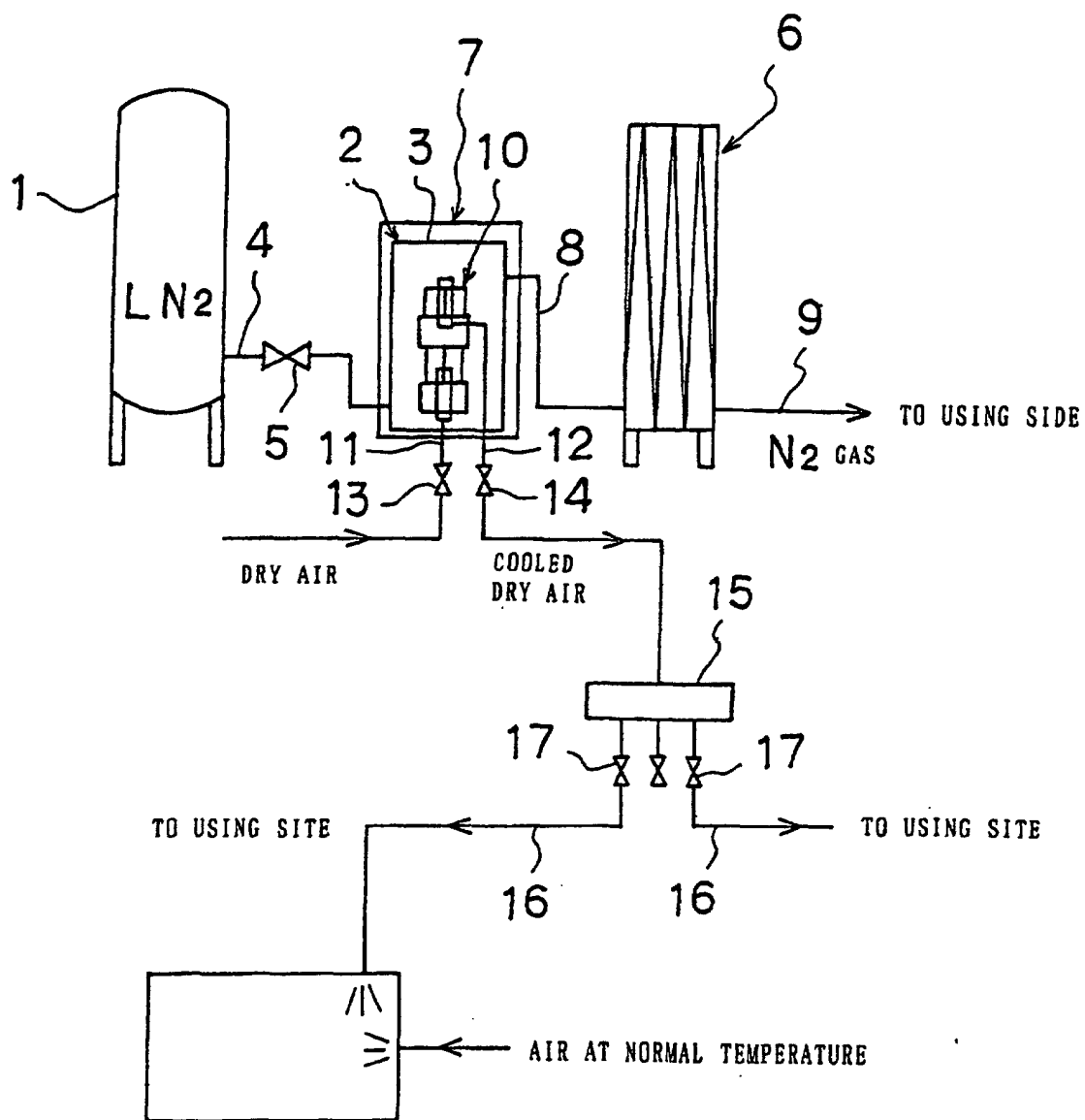


FIG. 3

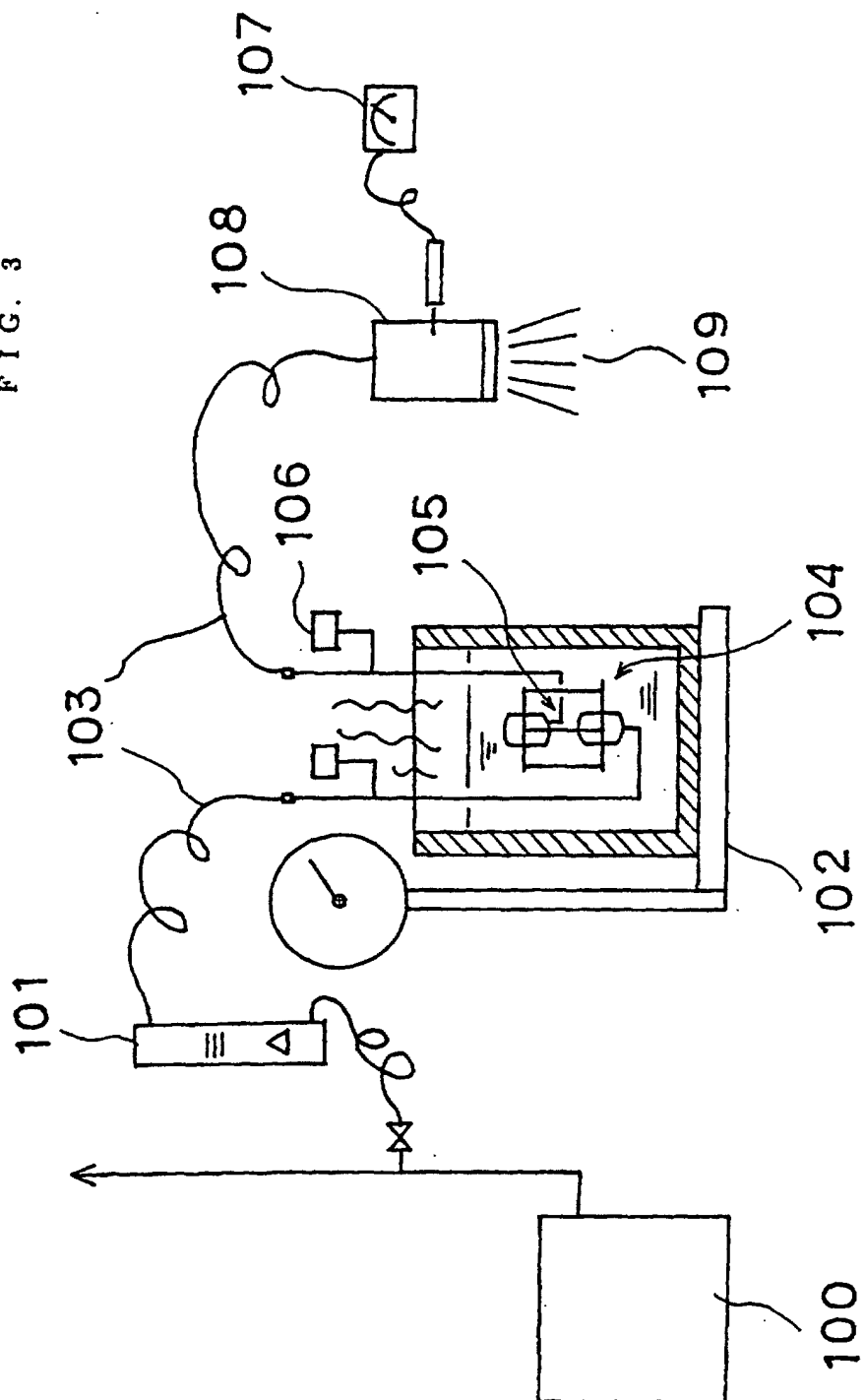


FIG. 4

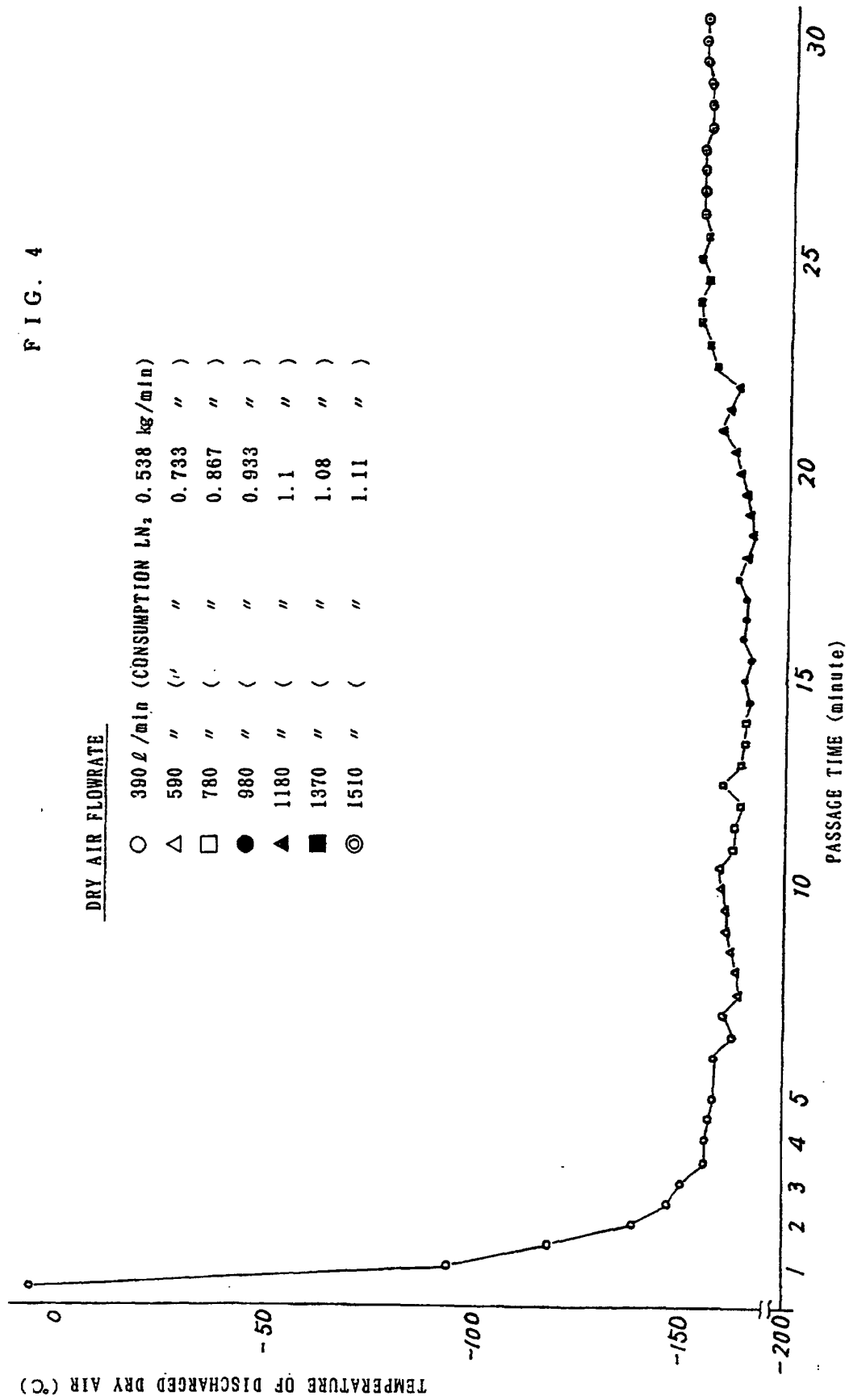


FIG. 5

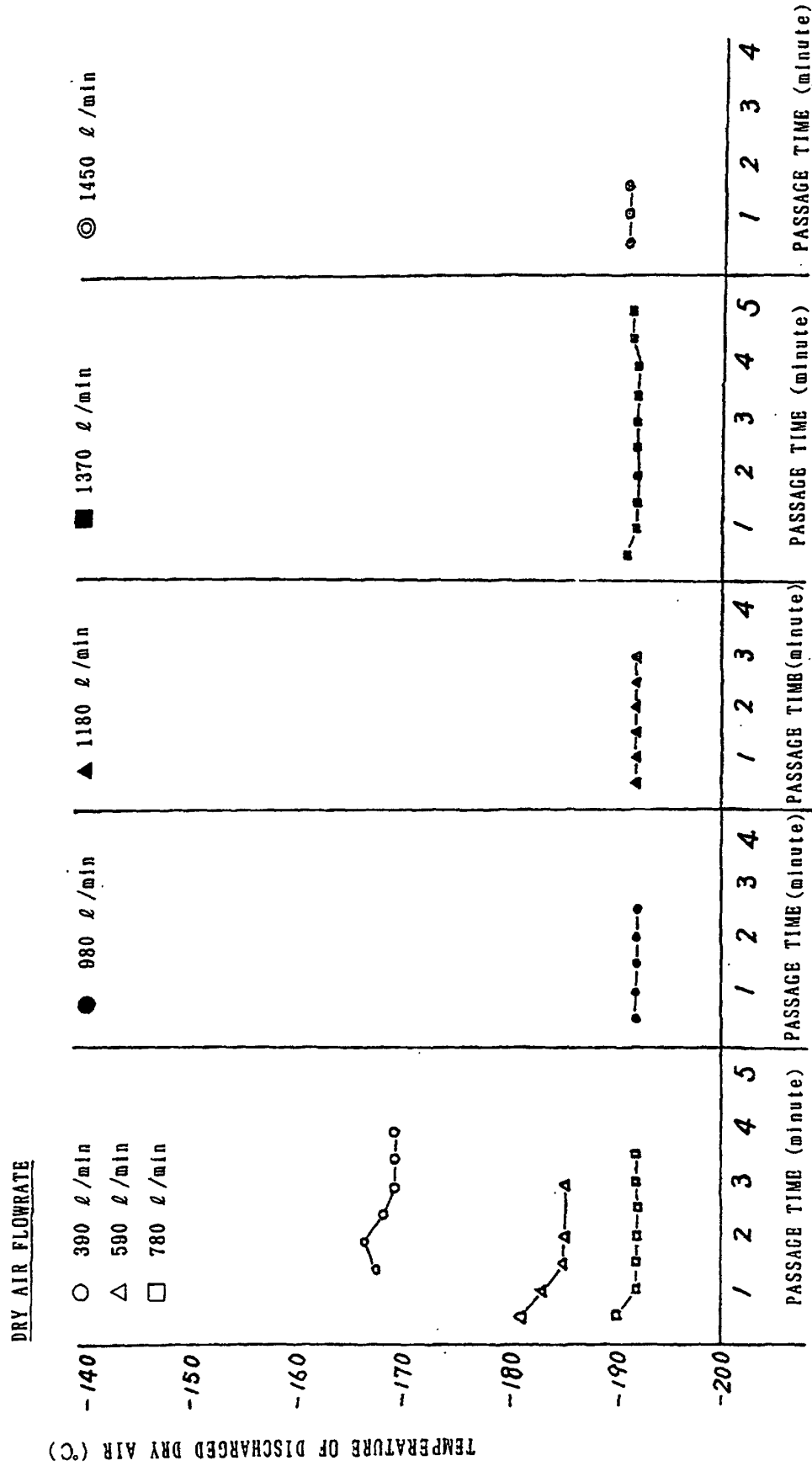


FIG. 6

MARKS IN THE GRAPH	DRY AIR FLOWRATE (ℓ /min)	MINIMUM TEMPERATURE OF RELEASE GAS ($^{\circ}\text{C}$)	INLET PRESSURE (kg/cm ²)	OUTLET PRESSURE (kg/cm ²)	CONSUMPTION LN ₂ (kg/min)	HEAT EXCHANGE EFFICIENCY	LIQUEFYING RATE (%)
○ ---- ○	390	-169	0.22-0.25	0.13-0.15	0.77	0.585	----
△ ---- △	590	-185	0.43-0.45	0.25-0.26	1.0	0.93	----
□ ---- □	780	-192	0.65-0.67	0.38	1.2	1.051	22.7
● ---- ●	980	-192	0.90-0.93	0.51-0.55	1.4	1.224	27.6
▲ ---- ▲	1180	-192	1.14-1.29	0.66-0.69	1.4	1.429	20.8
■ ---- ■	1370	-192	1.24-1.30	0.69-0.75	1.5	1.694	24.7