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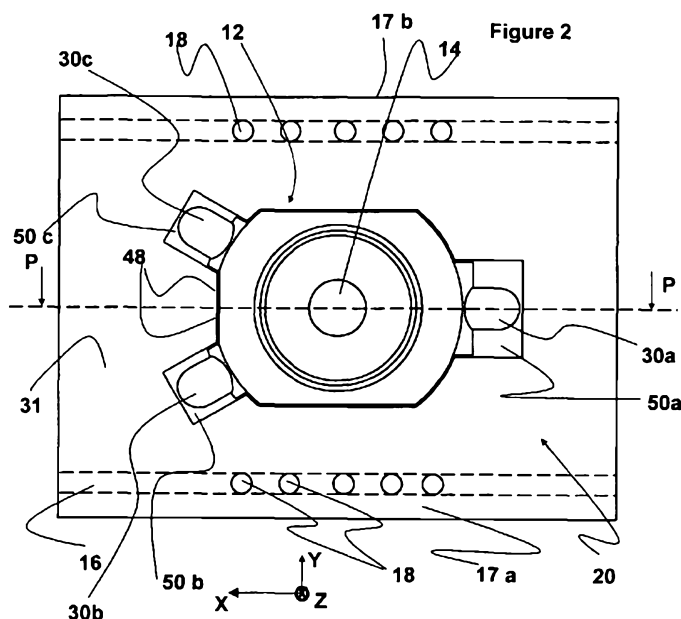
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[Continued on next page]

(54) Title: INNER NOZZLE FOR TRANSFERRING MOLTEN METAL CONTAINED IN A VESSEL, SYSTEM FOR CLAMPING SAID NOZZLE AND CASTING DEVICE



(57) Abstract: The invention relates to an inner nozzle (12) to be mounted onto a tube exchange device (10) for holding and replacing an exchangeable pouring nozzle for casting molten metal out of a vessel, said tube exchange device comprising a frame with a casting opening, said frame being suitable for being fixed to the lower side of a metal casting vessel and comprising a first, upper portion and a second, lower portion, joining at a middle section plane defining the plane where an inner nozzle (12) and an exchangeable pouring nozzle form a sliding contact, - the upper side portion of the frame comprising means for receiving and clamping (50a, 50b, 50c) in place at its pouring position a bearing surface of an inner nozzle (12) against a support portion of the upper side portion of the frame, such that the through bore of the inner nozzle (12) is in fluid communication with the casting opening, and - the lower portion comprising means for loading and moving along a first direction (X) into casting position an exchangeable pouring nozzle characterised in that at least two of the clamping means (50a, 50b, 50c) are arranged transverse to said first direction (X).

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Inner nozzle for transferring molten metal contained in a vessel, system for clamping said nozzle and casting device.

[0001] TECHNICAL FIELD

The present invention relates to the art of continuous molten metal casting. More specifically, it relates to the clamping of an inner nozzle in a continuous casting facility.

[0002] BACKGROUND OF THE INVENTION

5 In a casting facility, the molten metal is generally contained in a metallurgical vessel, for example a tundish, before being transferred to another container, for example into a casting mould. The metal is transferred from the vessel to the container via a nozzle system provided in the base of the metallurgical vessel, comprising an inner nozzle located at least partly in the metallurgical vessel and coming into tight contact with a sliding transfer plate (or casting plate) located below
10 and outside of the metallurgical vessel and brought into registry with the inner nozzle via a device for holding and replacing plates, mounted under the metallurgical vessel. This sliding plate may be a calibrated plate, a casting tube or a saggarr comprising two or more plates. Since all these types of plates are part of a nozzle comprising a plate connected to a tubular section of varying lengths depending on the applications and to distinguish them from valve gates used,
15 e.g., in a ladle, they will be referred to herein as "sliding nozzle", "pouring nozzle", "exchangeable pouring nozzle" or combinations thereof. The pouring nozzle can be used to transfer the molten metal in the form either of a free flow with a short tube, or of a guided flow with a longer, partly submerged casting tube.

[0003] An example of such casting facility is described in the document EP1289696. To provide
20 tight contact between the inner nozzle and the sliding pouring nozzle, the device for holding and replacing tubes comprises clamping means, intended to press against the inner nozzle, particularly downwards, and pushing means, intended to press on the sliding plate of the pouring nozzle, particularly upwards, so as to press the inner nozzle and the pouring nozzle against each other. These clamping and pressing means are generally arranged along the longitudinal edges
25 of the inner nozzle and the sliding plate, the longitudinal direction corresponding to the plate replacement direction.

[0004] One difficulty lies in the fact that the tightness of the inner nozzle / sliding plate interface must be as perfect as possible, lest the molten metal may flow is between the two parts, damaging the surfaces of the refractory elements when replacing the pouring nozzle with a new
30 one. Furthermore, the lack of tightness (contact between the two refractory elements) enables air to infiltrate, which is harmful both for the refractory elements and for the cast metal quality.

[0005] The present invention aims at enhancing the tightness of the contact surfaces between the inner nozzle plate and the sliding plate of the pouring nozzle. The present invention also aims at optimising the stress distribution in the refractory elements, for increasing their service
35 time.

[0006] SUMMARY OF THE INVENTION

The present invention is defined in the appended independent claims. Preferred embodiments are defined in the dependent claims. In particular, the present invention concerns a tube exchange device for holding and replacing an exchangeable pouring nozzle for casting molten metal out of a vessel, said tube exchange device comprising a frame with a casting opening, said frame being suitable for being fixed to the lower side of a metal casting vessel and comprising a first, upper portion and a second, lower portion, joining at a middle section plane defining the plane where an inner nozzle and an exchangeable pouring nozzle form a sliding contact, the upper side portion of the frame comprising:

- (a) means for receiving and clamping in place at its pouring position a bearing surface of an inner nozzle against a support portion of the upper side portion of the frame, such that the through bore of the inner nozzle is in fluid communication with the casting opening, and the lower side portion of the frame comprising,
 - (b) a passage extending along a first axis of first direction (X) between an inlet opening and an outlet opening suitable for receiving and moving an exchangeable pouring nozzle from said inlet to said outlet, passing by a casting position in registry with the casting opening of the frame,
 - (c) means for displacing and means for guiding said exchangeable pouring nozzle from a standby position to a casting position in registry with the casting opening of the frame, and optionally for guiding it to the outlet, said guiding means running substantially parallel to the first direction (X),
 - (d) means aligned with the guiding means and extending substantially parallel to the first direction (X) at the level of the pouring nozzle casting position for pressing up said exchangeable pouring nozzle at its casting position in the direction of the upper portion of the frame, characterised in that at least two of the clamping means are arranged transverse to said first direction (X).
- 25 **[0007]** In a preferred embodiment, the clamping means comprise at least a first clamping element (50a) intercepting and arranged substantially normal to said first direction (X).
- [0008]** In yet another embodiment, the clamping means comprise three clamping elements, wherein the respective centroids of the orthogonal projections onto the middle section plane of the clamping elements in their clamped position form the vertices of a triangle. As commonly
- 30 accepted by the person skilled in the art, the centroid of a plane figure is the point of intersection of all straight lines that divide said figure into two parts of equal moment about the line. In a triangle, the centroid is defined as the point of intersection of the medians. In particular, the triangle formed by the centroids of the clamping means projections is defined by one or any combination of any of the following geometries:
- (a) a first altitude of the triangle, referred to as X-altitude, passing through a first vertex, referred to as X-vertex, is substantially parallel to the first direction (X)
 - (b) A first median of the triangle referred to as X-median, passing through a first vertex, referred to as X-vertex, is substantially parallel to the first direction (X)
 - (c) a triangle according to (a) or (b) wherein the X-vertex points in the direction of the inlet

opening;

(d) a triangle according to (a) or (b) wherein the X-vertex points in the direction of the outlet opening;

(e) all the angles of the triangle are acute;

5 (f) the triangle is isosceles, preferably according to (a) and (b), more preferably according to (a), (b), such that the X-vertex is the meeting point of the two sides of equal length, more preferably according to (a), (b), and (e);

(g) a triangle according to (f) wherein the angle, 2α , formed by the centroid (46) of the casting opening and the two vertices of the triangle other than the X-vertex is comprised

10 between 60 and 90°;

(h) a triangle wherein the angle formed by the X-vertex is smaller than 60°.

[0009] It is preferred that a first clamping element corresponding to the X-vertex spans an angular sector, γ , comprised between 14 and 52°, and the other two clamping elements (50b, 50c) span an angular sector, β , between 10 and 20°, all angles measured with respect to the
15 centroid of the casting opening. It is also preferred that the inner ridge (i.e., adjacent the casting cavity) of the projection of said first clamping element intercept the first axis (X) with a tangent normal thereto. In yet a preferred embodiment, said first clamping element extending normal to the first direction (X) is movably mounted between an idle position and a clamping position, actuated from one position to the other by a crankshaft actuating means.

20 **[0010]** In a preferred embodiment, the tube exchange device of the present invention comprises at least one gas connection to a gas source, said connection being arranged between two of the three clamping elements, and pointing preferably substantially parallel to the first direction (X).

[0011] The present invention also concerns an inner nozzle made of a refractory core material
25 for casting molten metal from a metallurgical vessel, and suitable for being mounted on the upper portion of a pouring tube exchange device, said inner nozzle comprising:

(a) a substantially tubular portion with an axial through bore fluidly connecting an inlet opening to an outlet opening and

(b) a plate comprising a first, contact surface normal to the axial through bore and
30 comprising the outlet opening, and a second surface opposite to the first contact surface joining the wall of the tubular portion to the side edges defining the perimeter and thickness of the plate, characterized in that, the inner nozzle plate comprises three separate bearing elements jutting out of the side edges, each comprising a bearing ledge facing in the direction of the contact surface and distributed around the perimeter of the plate, wherein the centroids of the orthogonal
35 projections onto a plane parallel to the contact surface of the bearing ledges form the vertices of a triangle.

[0012] In a preferred embodiment, the triangle formed by the centroids of the projections of the three bearing ledges is defined by one or any combination of any of the following geometries:

(a) a first altitude of the triangle, referred to as X-altitude, passing through a first vertex,

referred to as X-vertex, is substantially parallel to a first axis (X)

(b) a first median of the triangle referred to as X-median, passing through the X vertex, is substantially parallel to said first axis (X)

(c) a triangle such that either the X-altitude or the X-median intercepts the central axis (Z) of the nozzle through bore at the through bore centre (46).

(d) all the angles of the triangle are acute;

(e) the triangle is isosceles, preferably according to (a) and (b), more preferably according to (a), (b), and (c) such that the X-vertex is the meeting point of the two sides of equal length, most preferably according to (a), (b), (c), and (d);

(f) a triangle according to (c) wherein the angle, 2α , formed by the through bore centre and the two vertices of the triangle other than the X-vertex is comprised between 60 and 90°;

(g) a triangle wherein the angle formed by the X-vertex is smaller than 60°.

[0013] All but the first, contact surface of the inner nozzle plate are preferably at least partially clad with a metal casing with the three bearing ledges being part of said metal casing. In a preferred embodiment, the inner nozzle comprises gas connection means in fluid communication with the casting through bore of the inner nozzle, so that the molten metal flowing through the inner nozzle can be covered by a blanket of an inert gas, such as Ar, He, Ne, and the like. The gas connection means can also be in fluid communication with a groove lying on the contact surface 26 of the inner nozzle, in order to protect the metal melt from oxidation in case of a leak at the interface between the inner nozzle contact surface and the pouring nozzle sliding surface. The gas connection means are preferably arranged between two bearing ledges.

[0014] The present invention also concerns an assembly of a tube exchange device as defined above and of an inner nozzle, wherein the inner nozzle comprises bearing elements mating the clamping means of the tube exchange device. Preferably the inner nozzle is also as defined above.

[0015] The present invention also concerns a metallic casing for cladding an inner nozzle as defined above, said metal casing comprising a main surface with an opening for accommodating the nozzle's tubular portion and side edges extending from the perimeter of the main surface, characterised in that said metallic casing comprises three separate bearing elements jutting out of said side edges, each bearing elements comprising a bearing ledge being oriented away from said main surface and being arranged around the periphery of the metal casing such that the centroids of each of said three bearing elements form the vertices of a triangle. The word centroid here means the geometric centre of the object's shape. The various geometries of the bearing ledges of the inner nozzle defined above apply mutatis mutandis to the present metal casing since the ledges are part of the metal casing.

[0016] BRIEF DESCRIPTION OF THE FIGURES

The invention will be understood more clearly on reading the following description, merely given as a non-limitative example of the scope of the invention, with reference to the figures, wherein:

- figure 1a is a perspective view of an inner nozzle according to one embodiment, in its

casting orientation;

- figure 1b is a perspective view of the nozzle of figure 1a when it is turned up side down in the vertical direction;

- figure 2 is a top view of the nozzle of figure 1 clamped in place in a tube exchange

5 device according to the present invention;

- figure 2a is a sectional view illustrating the structure of a clamping element of figure 2;

- figures 3 and 3a are top views of the nozzle of figure 1;

- figure 4 is a sectional view of a clamping element;

- figure 5 is a sectional side view of the inner nozzle of figure 1 standing in its casting
10 position on the tube exchange device prior to being clamped; and

- figures 5a to 5d are sectional views along a longitudinal plane illustrating the clamping steps of the clamping means in figure 4 for clamping one support ledge of an inner nozzle;

- figures 6a-c show the compressive stress distribution around the casting channel for various distributions of the inner nozzle clamping means.

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[0017] DETAILED DESCRIPTION OF THE INVENTION

The present invention relates to a tube exchange device for holding and replacing a sliding nozzle mounted under a metallurgical vessel for casting molten metal contained in the vessel, and for guiding the sliding nozzle to a casting position wherein it extends from a casting channel
20 of an inner nozzle provided on the metallurgical vessel. The plate replacement direction corresponding to a longitudinal direction of the device, and the directions non-parallel to said longitudinal direction corresponding to transverse directions of the device, with the direction perpendicular to the longitudinal direction being referred to as the normal direction. The sliding plate of the pouring nozzle and the inner nozzle each having two substantially longitudinal edges
25 and two transverse, generally normal edges.

[0018] The present invention proposes to apply the clamping force along the transverse edges of the inner nozzle, whilst the pressing force is applied onto the longitudinal edges of the pouring nozzle, such that the tightness at the transverse edges of the inner nozzle / sliding plate contact plane is improved. In other words, due to the clamping means and pushing means arranged in
30 this way, it is possible to apply a force setting the contact on substantially the entire circumference of the inner nozzle / sliding nozzle contact plane, hence superior tightness and thus a greater service life of the parts and improved cast metal quality. In particular, the inventors noted that it is more advantageous to apply the forces in this way than when the opposing thrust force and the clamping force are applied, as in the prior art, in that the high
35 pressure on the longitudinal edges of the inner nozzle and the sliding plate may bend and separate the respective transverse edges.

[0019] Moreover, the clamping means positioned in the transverse direction may further contribute to further referencing the inner nozzle in relation with to the frame of the tube exchange device along the longitudinal direction, which is particularly advantageous. Indeed, the

inner nozzle is subject to substantial shear forces in the longitudinal direction during plate the replacement of a pouring nozzle, and the clamping forces distributed in the transverse direction contribute to enhancing the stability of the inner nozzle in the longitudinal direction, and thus lock said nozzle in the longitudinal direction despite the shear stresses movements due to plate

5 replacements.

[0020] The term "clamping means" refers to means rotatably mounted on the frame of the tube exchange device for applying a clamping force onto a clamping surface of an inner nozzle, said force being transmitted to an opposite bearing surface against a matching support surface of the frame of the tube exchange device. Generally, the force applied by the clamping means onto the

10 inner nozzle is a downward force, applied onto a top surface of the inner nozzle, and the force applied by the pressing means onto the sliding nozzle plate is opposed to the former and generally oriented upwards, applied onto the bottom surface of the plate. The vertical direction is defined as the direction of flow of the molten metal at the metallurgical vessel outlet. The transverse direction is defined as any direction secant to the longitudinal direction, and the

15 normal direction is perpendicular to both longitudinal and vertical directions, such that the longitudinal, normal and vertical directions define an orthogonal referential. Furthermore, it should be noted that the forward direction is defined with reference to the nozzle replacement direction in the tube exchange device, the plate being moved from the rear to the front to adopt the following successive positions: standby position (when another nozzle is already in the

20 casting position), casting position (when the bore of the pouring nozzle is in registry with the inner nozzle through bore), sealing position (when a sealing surface provided on the plate of the pouring nozzle faces and seals the inner nozzle through bore outlet) and ejection position (when the plate sliding face is released from the tube exchange device). It should also be noted that several refractory surfaces of the plates of both the inner nozzle and the pouring nozzle are

25 generally clad with a metallic casing. The pouring nozzle generally comprises a tubular extension of varying lengths depending on the applications. The tubular extension may be extended sufficiently so that the end thereof is immersed in the downstream metallurgical vessel, for example in continuous casting moulds. The casting tube to be immersed is made of refractory element.

30 [0021] Hereinafter, the substantially vertical direction, corresponding to the casting direction, is referred to as the Z-direction, and the central axis of the through bore of the inner nozzle as the Z-axis, which is parallel to the Z-direction when the inner nozzle is mounted in its casting position on the tube exchange device. The longitudinal direction, corresponding to the plate replacement direction, is referred to as the X direction, which is substantially normal to the Z-direction; the X

35 axis is parallel to the X-direction and passes through the centroid of the casting opening of the tube exchange device.

[0022] The present invention is based on the observation that on traditional tube exchange devices, as disclosed e.g., in EP1289696, wherein the clamping means for holding the inner tube on the upper portion of the frame are positioned substantially parallel to the X-direction, and

substantially on top of the pressing means 18 pressing the pouring nozzle up against the contact surface of the inner nozzle 12 yielded problems of tightness. The inventor carried out a stress distribution analysis around the casting opening and realized that the level of compressive stress in the transverse portion of the plates was much lower than in the longitudinal sides, yielding the possible formation of a thin, albeit unacceptable gap that could lead to leakage of metal melt (cf. Figure 6a). The solution proposed in the present invention to solve this problem is to locate at least two, preferably three clamping elements 20 transverse to the X-direction along which the pressing means 18 are aligned. This apparently simple solution unexpectedly solves the problem of leakage risk of the prior art exchange tube systems, as will be seen in continuation.

5 [0023] In a continuous molten metal casting facility, such as for casting molten steel, a device 10 for holding and replacing sliding nozzles is used for transferring the metal contained in a metallurgical vessel, for example a tundish, to a container, such as one or a plurality of casting moulds. The device 10, partly represented in figure 2, is mounted under the metallurgical vessel, in registry with an opening in the floor thereof, such as to insert therethrough an inner nozzle 12, fixed to the frame of a tube exchange device 10 and attached to the base of the metallurgical vessel, for example with cement. A side view representation of a typical tube exchange device can be found in Figure 1 of EP1289696. The through bore 14 of the inner nozzle 12 defines a casting channel and the device 10 is arranged such that it can guide the sliding plate of a pouring nozzle to a casting position, such that the axial bore of the latter comes in fluid communication with the through bore 14 of the inner nozzle. For this purpose, the device 10 comprises means 16 for guiding the sliding nozzle through an inlet and from a standby position to a casting position. For example the guiding means can be in the form of guiding rails 16. The rails 16 are arranged along the longitudinal edges 17a, 17b of the channel of the device 10 leading from the device inlet, to the idle position and to the casting position. Moreover, at the pouring nozzle casting position, the device 10 comprises means 18 arranged parallel to the X-direction for pressing the plate of the pouring nozzle against the contact surface of the inner nozzle 12, for example compressed springs 18, said means being arranged to apply a force on a bottom surface of each of the two longitudinal edges of the sliding plate of the pouring nozzle, so as to press the plate in tight contact against the contact surface of the inner nozzle 12 and thus to create a fluid tight connection between the through bore 14 of the inner nozzle and the axial bore of the pouring nozzle. As can be seen in figure 2, the springs 18 are distributed along the longitudinal edges 17a, 17b of the device 10 substantially parallel to the X-direction. The device 10 further comprises means 20 for clamping the inner nozzle, described in more detail below, and arranged to apply a force on a top surface of two transverse edges of the inner nozzle 12, so as to keep the inner nozzle pressing against the device 10. The term transverse means in the present context, not parallel to, or secant with the X-direction.

[0024] The inner nozzle 12 comprises a metallic casing 22, cladding all but the first, contact surface (26) of the inner nozzle plate 24 made of a refractory material, as can be seen in Figure 1b. The metallic casing 22 reinforces the refractory element 24 and is preferably bonded to the

plate using a cement, The refractory plate is essential to support the high temperatures wherever the nozzle contacts metal melt, but its mechanical properties, in particular compression, shear, friction, and wear resistance are insufficient wherever there is concentration of stresses. For this reason, the refractory plate is clad with a metal casing wherever mechanical stresses are applied but away from any possible contact with molten metal. The thickness of the metal casing may vary from about 1 mm to greater than 6 mm, the thicker walls being generally when the metal casing is made of cast iron. The metallic casing lies clear from the contact surface 26 of the inner nozzle (cf. Figure 1b) as the latter is to be brought in intimate contact with the sliding surface of the plate of a pouring nozzle. Metal could not be used for cladding the contact surface because it would be damaged in case of any leak of metal melt with dramatic consequences. As mentioned supra, the contact surface 26 of the inner nozzle is intended to be brought into tight contact with the sliding surface of a pouring nozzle when said nozzle is pushed in place by the device 10 to the casting position, i.e. facing the inner nozzle 12. One end of the inner nozzle through bore 14 opens at the contact surface 26.

[0025] The inner nozzle 12 comprises three separate bearing elements 30a, 30b, 30c jutting out of the side edges and distributed around the perimeter of the plate. Each bearing element comprises a bearing ledge (34a, 34b, 34c) facing in the direction of the contact surface 26. The centroids of the orthogonal projection of the respective ledges onto a plane parallel to the contact surface 26 form the vertices of a triangle. The bearing elements and ledges thereof are actually part of the metallic casing cladding parts of the plate of the inner nozzle. This is advantageous because the clamping force is applied to a metal surface which does not crumble like refractory could possibly do when exposed to high compressive and shear stress concentrations. The surfaces of the three ledges define the bearing surface. They are preferably coplanar, but this is not essential to the present invention. They are preferably parallel to the contact surface 26 but this is not essential either, as a slight slope of the ledges can help to centre the inner nozzle on the tube exchange device 10. It is clear, however, that the bearing ledges of the inner nozzle must match the support portion and clamping means 20 of the tube exchange device 10. Opposite the bearing ledges (34a, 34b, 34c), the inner nozzle comprises clamping surfaces (32a, 32b, 32c) which are suitable for receiving the clamping means of the tube exchange device, such as to clamp into position the bearing ledges of the inner nozzle against matching support portions of the frame of the tube exchange device. The clamping surfaces are preferably metallic and may be part of the second surface of the plate, opposite the contact surface or they can be part of the bearing elements but separate from said second surface as illustrated in Figure 1.

[0026] The bearing elements 30a, 30b, 30c are separate and project from a peripheral surface 36 of the plate of the inner nozzle 12, said surface 36 extending from the bottom contact surface 26 of the plate, preferably but not necessarily, in a substantially vertical direction Z. In one embodiment, refractory material may extend between the bearing ledge and the clamping surface of a bearing element of the inner nozzle. In this embodiment, a portion of the refractory

is exposed to the compressive stresses of the clamping means 20, but any stress concentration is distributed by the metal layer separating the refractory from the clamping means and support surfaces of the tube exchange device. In a preferred embodiment, the bearing ledge and opposed clamping surfaces are separated by metal only. This ensures that the clamping force is not applied to the refractory at all, but to metal only. Like in the example illustrated in the figures, the three bearing elements 30a, 30b, 30c are entirely made of metal, i.e. there is only metal between the bearing ledges 34a, 34b, 34c and the clamping surfaces 32a, 32b, 32c.

[0027] As can be seen in figure 3, the inner nozzle 12 has two substantially longitudinal opposite edges 40a, 40b and two opposite edges: 42a, 42b, substantially normal to the longitudinal edges. Furthermore, a vertical central longitudinal plane P can be defined by the X-, and Z axes and the three bearing elements 30a, 30b, 30c may be arranged in a Y shape on the periphery 36 of the nozzle 12, the base 44a of the Y being arranged in the central longitudinal plane P coaxially with X-axis and the two arms 44b, 44c of the Y being arranged on either side of said plane P and all arms of the Y meeting at the centroid 46 of the inner nozzle through bore 14. More specifically, the second 30b and third 30c bearing elements have a second 34b and a third 34c bearing ledges, each of these second 34b and third 34c bearing ledges being arranged on either side of the longitudinal plane P. In the example described, the second and third bearing ledges are arranged symmetrically, but this is not necessarily the case. Furthermore, each of the orthogonal projections of the three bearing ledges 34b, 34c onto a plane parallel to the contact surface 26 have a centroid 34'b, 34'c positioned at an angle α (alpha) between 30 and 45° in relation to the longitudinal plane P, with reference to the centroid 46 of the inner nozzle 12, corresponding to the centre of the casting orifice 28. Furthermore, each of the second 34b and third 34c bearing ledges is included in an angular sector β (beta) between 10 and 20° with reference to the centre 46 of the inner nozzle 12. Moreover, the first bearing element 30a has a first bearing ledges 34a passing through the longitudinal plane P of the nozzle 12. More specifically, the bearing ledge 34a extends substantially symmetrically in relation to the plane P, the centroid 34'a of this surface being positioned in the plane P. The bearing ledge 34a may extend in a surface included in an angular sector γ (gamma) between 14 and 52° with the reference to the centre 46 of the inner nozzle. In the case represented in figure 3, the centroids 34'a, 34'b, 34'c of the projection of the bearing ledges corresponds to the centroids of the projection of the clamping surfaces 32'a, 32'b, 32'c.

[0028] The inner nozzle 12 may further comprise gas connection means 48, in fluid communication with the inner nozzle central bore 14 and/or with a groove lying on the contact surface 26. It is preferred that, said means 48 are arranged between the second 30b and third 30c bearing elements. In this instance, the means 48 comprises one or two channels opening onto a transverse vertical surface or transverse edge 49 belonging to the peripheral surface 36 and connecting the two bearing elements 30b, 30c. The injected gas is, for example, argon.

[0029] The clamping means 20 of the tube exchange device comprise two clamping elements arranged transverse to the X-axis. Preferably, three clamping elements 50a, 50b, 50c, are

arranged in a Y shape at the periphery of the inner nozzle 12 (cf. figure 2), i.e. a first clamping element 50a at the base of the Y, arranged on the rear portion of the central longitudinal plane P and a second 50b and a third 50c clamping elements, at the ends of both arms of the Y, arranged on either side of the front portion of said plane P. As can be seen, the clamping means are arranged to apply the force thereof on the transverse edges 42a, 42b of the inner nozzle. The clamping elements 50a, 50b, 50c have a complementary configuration of the bearing elements 30a, 30b, 30c. In this way, the first 50a, second 50b and third 50c clamping elements respectively apply a clamping force on the first 34a, second 34b and third 34c bearing ledges described above.

- 10 [0030] The second and third clamping elements 50b, 50c may be substantially identical. Only the structure of the element 50b will thus be described, with reference to figures 2 and 2a. The clamping element 50b is rotatably mounted on an axis 52b attached on the frame 31, extending substantially in a transverse direction. The element 50b has one free end bearing a so-called clamping surface 54b, intended to come into contact with the clamping surface 32b of the bearing element 30b, and apply a clamping force on said surface 32b by pressing thereon. For this purpose, the element 50b is actuated by a rotary device 56b (pivoting about a vertical axis) acting as a cam in contact with the element 50b. More specifically, when the cam 56 is rotated, it applies a horizontal force on the free end of the element 50b, according to the arrow illustrated in figure 2a, which pivots the free end downwards, and thus the surface 54b about the axis 52b.
- 15 20 The downward pivoting of the surface 54b thus generates a clamping force on the surface 32b which is transmitted to the opposite bearing ledge 34b which is clamped into position against the corresponding support portion of the frame. It should be noted that the clamping element 50b does not only apply a downward clamping force, but also a horizontal force, intended to lock the ledge 34b horizontally. Other clamping mechanisms known to the person skilled in the art can be used within the scope of the present invention, as it is the orientation rather than the clamping mechanism of the clamping means that define the gist of the present invention.

- 25 [0031] The structure of a first clamping element 50a will now be described, with reference to figures 4, 5 and 5a to 5d. The first clamping element 50a has a similar shape to that of the element 50b represented in figure 2a, except that it may extend over a larger surface than the element 50b. The element 50a is rotatably mounted on an axis 52a attached on the frame 31, extending in a direction transverse to the X-direction, and has a free end bearing a clamping surface 54a, intended to come into contact with the clamping surface 32a by pressing thereon. The element 50a can be actuated differently than the element 50b, particularly by means acting as a connecting rod. More specifically, it is actuated by a rotary device 56a pivotably mounted about an axis in the example normal to the X-axis and acting as a cam in contact with a cylinder 58. The cylinder 58 can move by translation in the X direction. It bears a rod 60 acting as a connecting rod, one end 62 of which is rotatably mounted about the free end of the clamping elements 58 and the opposite end 64 of which is rotatably mounted about the free end of the clamping element 50a, the element 50a acting as a connecting rod. Moreover, the cylinder 58
- 30 35

forms a housing for a rod 66 returned by return means 68 of the clamping element 50a in the idle position, e.g., a compressed spring.

[0032] The clamping element 50a is movably mounted between an idle position and a clamping position, actuated by the connecting rod system, as follows. The idle position is illustrated in figure 5a. To move to the clamping position, it is necessary to rotate the movable device 56a about the axis thereof, such that it moves the cylinder 58 in the horizontal direction illustrated by the arrow 70. As a result of this translation, the connecting rod 60 rotates the element 50a about the axis 52a thereof, as illustrated in figures 5b, 5c and 5d, such that the clamping surface 54a of the clamping element presses on the clamping surface 32a of the bearing element and the clamping element 50a adopts the clamping position thereof. Simultaneously with the translation of the cylinder 58, the rod 66 abuts against the vertical wall of the bearing element 30a, which compresses the spring 68 as illustrated in figure 5c and 5d. By means of the compression of this spring, the system can return to the idle position simply by rotating the device acting as a cam 56a. Indeed, in such crankshaft system, when the element 50a is in the clamping position, as illustrated in figure 5d, the rotation of the device 56a enables the cylinder 58 to move by translation in the direction indicated by the arrow 72 under the action of the spring 68 which is released, and thus enables the clamping element to return to the position illustrated in figure 5a.

[0033] The device 10 illustrated in the appended figures further comprises, between the two clamping elements 50b, 50c, two gas injection channels for the nozzle 12, opening on a vertical transverse surface 51 of the device 10. In this way, when the element 50a is in the clamping position, the injection channels of the device 10 extend from the channels 48 of the nozzle 12, and the clamping positions of the elements 50b, 50c provide a particularly tight junction of said channels.

[0034] The method for clamping the inner nozzle 12 in the device 10 will now be described on the basis of the embodiment illustrated in the figures. At the start of the clamping method, the inner nozzle 12 is simply placed onto the frame 31 of the tube exchange device 10. The clamping method comprises a first step of abutting the transverse vertical surface 49 of the nozzle 12, arranged between the bearing elements 30b, 30c, against the transverse vertical surface 51 of the frame 31 of the device 10, followed by actuation of the first clamping element 50a in the clamping position. The first element 50a thus moves by translation in accordance with the arrow 70 in figure 5a, abuts against the bearing element 30a, pressing the inner nozzle 12 against the front transverse edge 51 of the device 10, thus referencing same very precisely against said front edge. It is understood that the establishment of the clamping position by the clamping element 50a simultaneously gives rise to the compression of seals arranged in the gas injection channels 48. The seals may be positioned on the inner nozzle or on the device. They are preferably made of graphite. The translation along the arrow 70 enables controlled compression. Once the clamping element 50a is in the clamping position, the assembly method is followed by optionally simultaneous actuation of the two clamping elements 50b, 50c in the clamping position. The clamping of the first element 50a followed, in a second step, by the

clamping of the two other elements 50b, 50c, enables a particularly simple method, all the clamping elements 50a, 50b, 50c and the actuation means thereof forming a particularly advantageous clamping system.

[0035] Among the benefits of the inner nozzle 12 and the tube exchange device 10 described above, it should be noted that the clamping means apply the force thereof on the transverse edges 42a, 42b of the inner nozzle, whereas the pressing means 18 apply the force thereof onto the longitudinal edges of the plate of the sliding pouring nozzle against the longitudinal edges 17a, 17b of the device 10. As a result, a pressure is applied on substantially the entire circumference of the contact surface between the inner nozzle 12 and the sliding plate, hence superior tightness (cf. Figure 6(c)).

[0036] Another advantage of the present invention, is that, after use of the inner nozzle 12, the same metallic casing 22 can be used again to clad a new refractory element 24.

[0037] The present invention clearly enhances the fluid tightness of the interface between the contact surface 26 of an inner nozzle and the sliding surface of the plate of a pouring nozzle in a tube exchange device 10. Figure 6 shows the compressive stress distribution calculated as a result of the arrangement of the clamping means around the periphery of the casting opening: the darker the colouration, the higher the compressive stress. In Figure 6(a) is represented a prior art configuration as described, e.g., in EP1289696 with the clamping means 20 for clamping in place the inner nozzle arranged along the longitudinal edges, parallel to the X-axis and lying substantially on top of the pressing means 18 for pressing the sliding surface of the pouring nozzle against the contact surface 26 of the inner nozzle. It can be seen that the pressure is high only in the portion adjacent the longitudinal edges, with a low pressure along the transverse direction, yielding a high risk of leakage of molten metal upon casting and significant air aspiration. Figures 6(b) and (c) on the other hand are according to the present invention.

[0038] In Figure 6(b) there are two clamping elements 20 for clamping the inner nozzle, which are positioned substantially normal to the X-axis. It can be seen that the portion of the plate comprising the X-axis is exposed to a higher level of pressure than in the former geometry of Figure 6(a). In Figure 6(c), three clamps are arranged around the perimeter of the inner nozzle, wherein the centroids of the orthogonal projections of each clamping means 20 in their clamped positions on the plane of the contact surface of the inner nozzle form the vertices of a triangle, or the arms of a 'Y' joining at the centroid 46 of the through bore of the inner nozzle as discussed above. It can be seen in Figure 6(c) that the level of compression is very homogeneous with the whole perimeter of the plates being exposed to a high pressure, thus ensuring fluid tightness of the interface between the two surfaces of the inner nozzle and the pouring nozzle. Since the three clamp system seems to be so efficient, several embodiments of three clamp systems are discussed.

[0039] An altitude of a triangle is a straight line through a vertex and perpendicular to the opposite side. The intersection of the altitudes is the orthocentre. A median of a triangle is a straight line through a vertex and the midpoint of the opposite side, and divides the triangle into

two equal areas. The intersection point of the medians of a triangle is called the centroid.

[0040] In one embodiment, it is preferred that one median, referred to as the X-median and/or an altitude referred to as the X-altitude, both passing by the X-vertex of the projected triangle is coaxial with the X-axis, as represented in Figures 2(a) and 6(c). The other two clamping means
5 20 are disposed on either sides of the X-axis. Preferably, the triangle is isosceles with the two sides of equal length joining at the X-vertex, as is depicted in the foregoing Figures.

[0041] The X-vertex may point in the direction of the inlet opening. This configuration is advantageous in case of a gas connection located between the second and third vertices, other than the X-vertex, as the friction applied in the longitudinal direction by a pouring nozzle being
10 inserted into, respectively extracted from the lower portion of the tube exchange device would push the inner nozzle against said connection, thus ensuring a gas tight connection. Furthermore, the frictional forces cooperate with the crankshaft system installed on the first clamping means as explained supra. Alternatively, the X-vertex may be pointing towards the outlet opening.

15 [0042] It is preferred that all the angles of the triangle are acute to ensure an even distribution of the clamping means around the periphery of the nozzle. In particular it is preferred that the X-vertex be smaller than 60° . The angle, 2α , on the other hand, formed by the centroid (46) of the casting opening and the two vertices of the triangle other than the X-vertex is preferably comprised between 60 and 90° ;

20 [0043] As illustrated in the Figures, it is preferred that the triangle be isosceles, preferably with the X-median being coaxial with the X-axis. More preferably the X-vertex should be the intersecting point of the two sides of equal length (with this configuration, the X-median and the X-altitude are coaxial).

- 10. Tube exchange device;
- 12. inner nozzle;
- 14. Inner nozzle through bore;
- 16. guiding means;
- 17a, 17b longitudinal edges of device;
- 18. pressing means;
- 20. clamping means;
- 22. metallic casing;
- 24. refractory element;
- 26. contact surface;
- 28. casting opening;
- 30a, 30b, 30c Bearing elements;
- 31. frame;
- 32a, 32b, 32c Clamping surface of the bearing elements;
- 34a, 34b, 34c bearing ledge of the bearing elements;
- 36. peripheral surface;
- 40a, 40b longitudinal edges of nozzle;
- 42a, 42b transverse edges of nozzle;
- 44a Base of Y;
- 44b, 44c arms of Y;
- 46. centroid of the through bore opening of the inner nozzle;
- 48. gas injection means;
- 49. transverse surface of nozzle;
- 50a, 50b, 50c clamping elements;
- 51. transverse surface of device;
- 52a, 52b clamping element axis;
- 54b clamping surface of clamping element;
- 56a, 56b, 56c rotary device or cam;
- 58. cylinder;
- 60. rod acting as connecting rod;
- 66. Rod;
- 68. return means;
- 70. Horizontal direction;
- 72. Opposite direction of direction 70.

Claims

1. Tube exchange device for holding and replacing an exchangeable pouring nozzle for casting molten metal out of a vessel, said tube exchange device comprising a frame with a casting opening, said frame being suitable for being fixed to the lower side of a metal casting vessel and comprising a first, upper portion and a second, lower portion, joining at a middle section plane defining the plane where an inner nozzle and an exchangeable pouring nozzle form a sliding contact, the upper side portion of the frame comprising:
 - (a) means for receiving and clamping in place at its pouring position a bearing surface of an inner nozzle against a support portion of the upper side portion of the frame, such that the through bore of the inner nozzle is in fluid communication with the casting opening, and the lower side portion of the frame comprising,
 - (b) a passage extending along a first axis of first direction between an inlet opening and an outlet opening suitable for receiving and moving an exchangeable pouring nozzle from said inlet to said outlet, passing by a casting position in registry with the casting opening of the frame,
 - (c) means for displacing and means for guiding said exchangeable pouring nozzle from a standby position to a casting position in registry with the casting opening of the frame, and optionally for guiding it to the outlet, said guiding means running substantially parallel to the first direction,
 - (d) pressing means aligned with the guiding means and extending substantially parallel to the first direction at the level of the pouring nozzle casting position for pressing up said exchangeable pouring nozzle at its casting position in the direction of the upper portion of the frame,wherein the clamping means comprises three clamping elements, wherein the respective centroids of the orthogonal projections onto the middle section plane of the clamping elements in their clamped position form the vertices of a triangle, and wherein the clamping means are arranged transverse to said first direction.
2. Tube exchange device according to claim 1, wherein the clamping means comprises at least a first clamping element intercepting and arranged substantially normal to said first direction.
3. Tube exchange device according to any one of the preceding claims, wherein the triangle formed by the centroids of the three clamping elements is defined by one or any combination of any of the following geometries:
 - (a) a first altitude of the triangle, referred to as X-altitude, passing through a first vertex, referred to as X-vertex, is substantially parallel to the first direction;
 - (b) a first median of the triangle referred to as X-median, passing through a first vertex, referred to as X-vertex, is substantially parallel to the first direction;
 - (c) a triangle according to (a) or (b) wherein the X-vertex points in the direction of the inlet opening;
 - (d) a triangle according to (a) or (b) wherein the X-vertex points in the direction of the outlet opening;

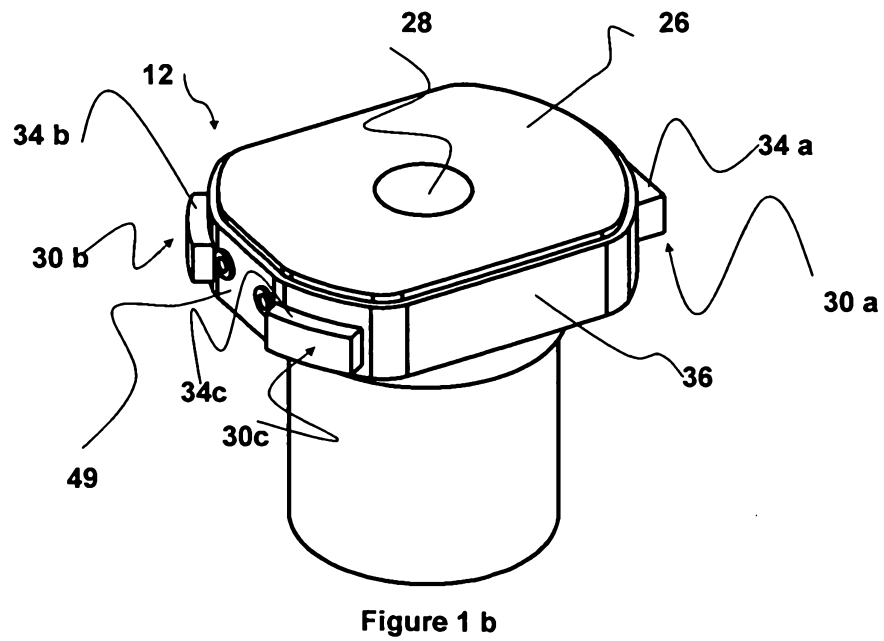
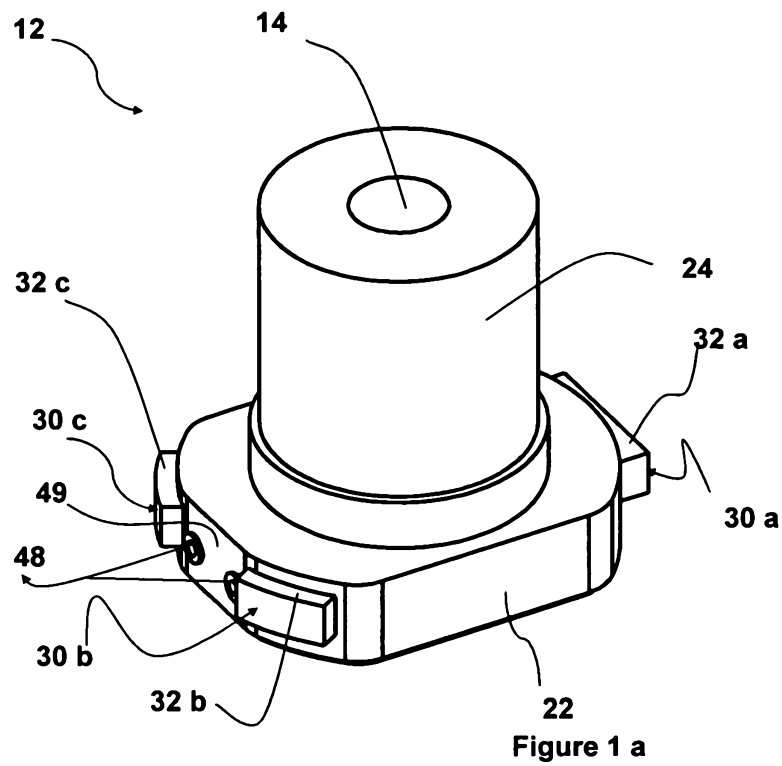
- (e) all the angles of the triangle are acute;
 - (f) the triangle is isosceles, preferably according to (a) and (b), more preferably according to (a), (b), such that the X-vertex is the meeting point of the two sides of equal length, more preferably according to (a), (b), and (e);
 - (g) a triangle according to (f) wherein the angle, 2α , formed by the centroid of the casting opening and the two vertices of the triangle other than the X-vertex is comprised between 60° and 90° ;
 - (h) a triangle wherein the angle formed by the X-vertex is smaller than 60° .
4. Tube exchange device according to claim 1 or 3, wherein a first clamping element corresponding to the X-vertex spans an angular sector, γ , comprised between 14° and 52° , and the other two clamping elements span an angular sector, β , between 10° and 20° , all angles measured with respect to the centroid of the casting opening.
 5. Tube exchange device according to claim 3(f), wherein the inner ridge of the projection of said first clamping element, corresponding to the X-vertex, intercept the first axis with a tangent normal thereto.
 6. Tube exchange device according to any one of claims 2 to 5, comprising at least one gas connection to a gas source, said connection being arranged between two of the three clamping elements, and pointing preferably substantially parallel to the first direction.
 7. Tube exchange device according to any one of claims 2 to 6, wherein the first clamping element extending normal to the first direction is movably mounted between an idle position and a clamping position, actuated from one position to the other by a crankshaft actuating means.
 8. Inner nozzle made of a refractory core material for casting molten metal from a metallurgical vessel, and suitable for being mounted on the upper portion of a pouring tube exchange device, said inner nozzle comprising:
 - (a) a substantially tubular portion with an axial through bore fluidly connecting an inlet opening to an outlet opening and
 - (b) a plate comprising a first, contact surface normal to the axial through bore and comprising the outlet opening, and a second surface opposite to the first contact surface joining the wall of the tubular portion to the side edges defining the perimeter and thickness of the plate,

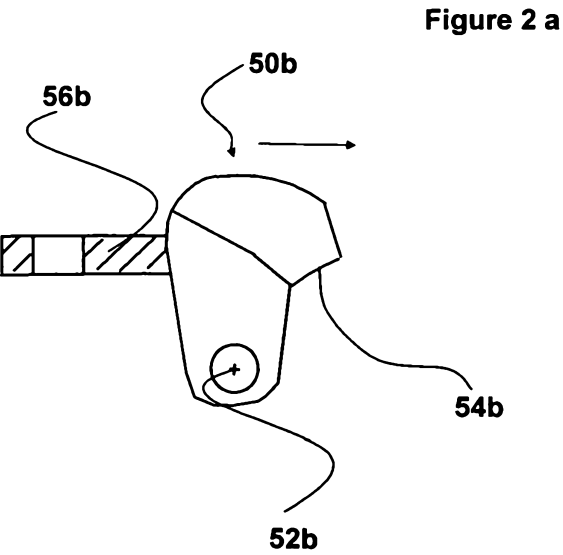
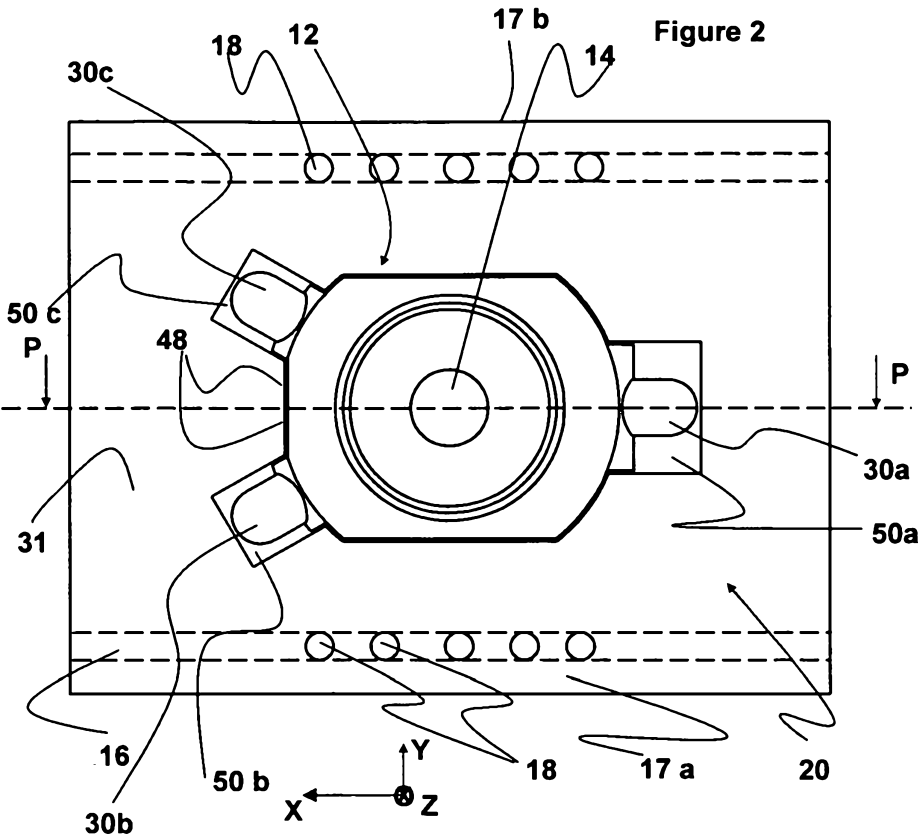
wherein, the inner nozzle plate comprises three separate bearing elements jutting out of the side edges, each bearing element comprising a bearing ledge facing in the direction of the contact surface and distributed around the perimeter of the plate, wherein the centroids of the orthogonal projections onto a plane parallel to the contact surface of the bearing ledges form the vertices of a triangle.
 9. Inner nozzle according to claim 8, wherein all but the first, contact surface of the inner nozzle plate are at least partially clad with a metal casing, and wherein the three bearing ledges are part of said metal casing.
 10. Inner nozzle according to claim 8 or 9, wherein the triangle formed by the centroids of the

projections of the three bearing ledges is defined by one or any combination of any of the following geometries:

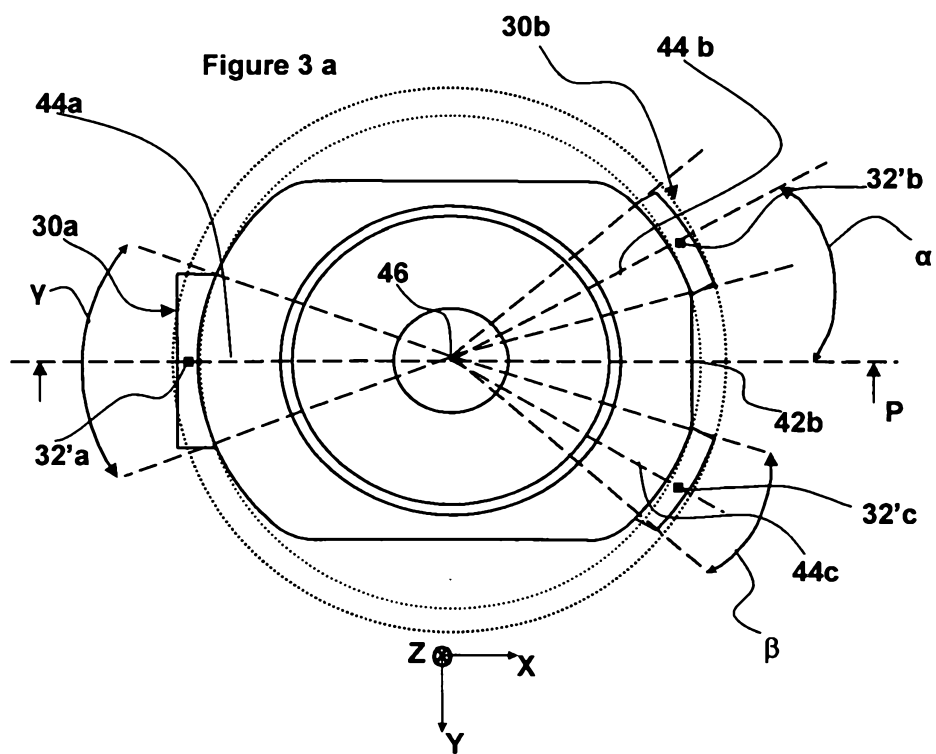
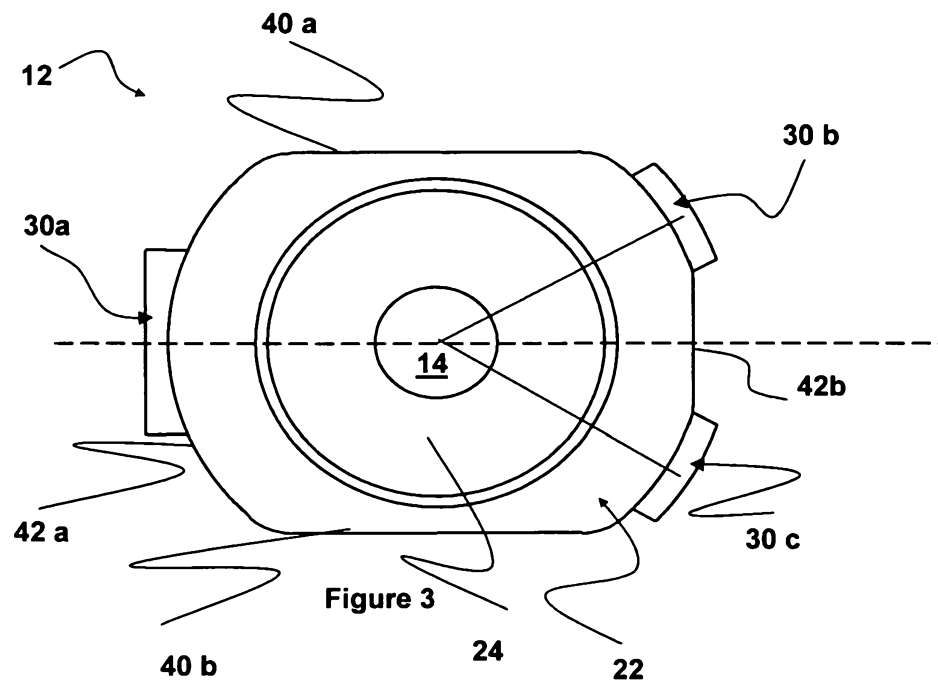
- (a) a first altitude of the triangle, referred to as X-altitude, passing through a first vertex, referred to as X-vertex, is substantially parallel to a first axis;
 - (b) a first median of the triangle referred to as X-median, passing through the X vertex, is substantially parallel to said first axis;
 - (c) a triangle such that either the X-altitude or the X-median intercepts the central axis of the nozzle through bore at the through bore centre;
 - (d) all the angles of the triangle are acute;
 - (e) the triangle is isosceles, preferably according to (a) and (b), more preferably according to (a), (b), and (c) such that the X-vertex is the meeting point of the two sides of equal length, most preferably according to (a), (b), (c), and (d);
 - (f) a triangle according to (c) wherein the angle, 2α , formed by the through bore centre and the two vertices of the triangle other than the X-vertex is comprised between 60° and 90° ;
 - (g) a triangle wherein the angle formed by the X-vertex is smaller than 60° .
11. Inner nozzle according to any one of claims 8 to 10, comprising gas connection means in fluid communication with the casting through bore and/or with a groove lying on the contact surface of the inner nozzle, said gas connection means being preferably arranged between two bearing ledges.
 12. Assembly of an inner nozzle and of a tube exchange device according to any one of claims 1 to 7, wherein the inner nozzle comprises bearing elements mating the clamping means of the tube exchange device.
 13. Assembly according to claim 12, wherein the inner nozzle is according to any one of claims 8 to 11.
 14. Metallic casing for cladding an inner nozzle according to any one of claims 9 to 11, when depending on claim 9, said metal casing comprising a main surface with an opening for accommodating the nozzle's tubular portion and side edges extending from the perimeter of the main surface, wherein said metallic casing comprises three separate bearing elements jutting out of said side edges, each bearing element comprising a bearing ledge being oriented away from said main surface, and being arranged around the periphery of the metal casing such that the centroids of each of said three bearing elements form the vertices of a triangle.
 15. Metallic casing according to claim 14, wherein the positions of the three bearing ledges is as defined in claim 10 when the metallic casing is clad onto an inner nozzle.

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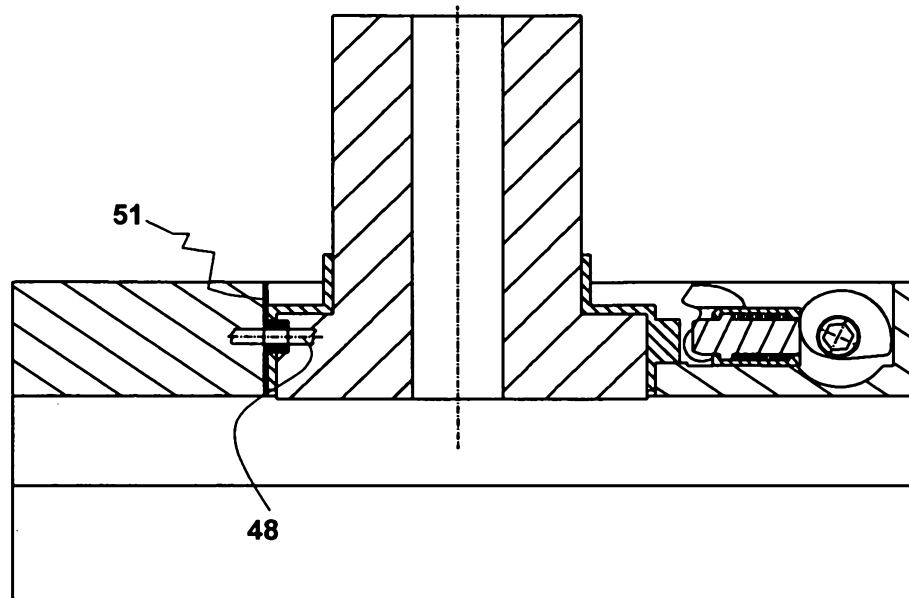


Figure 5

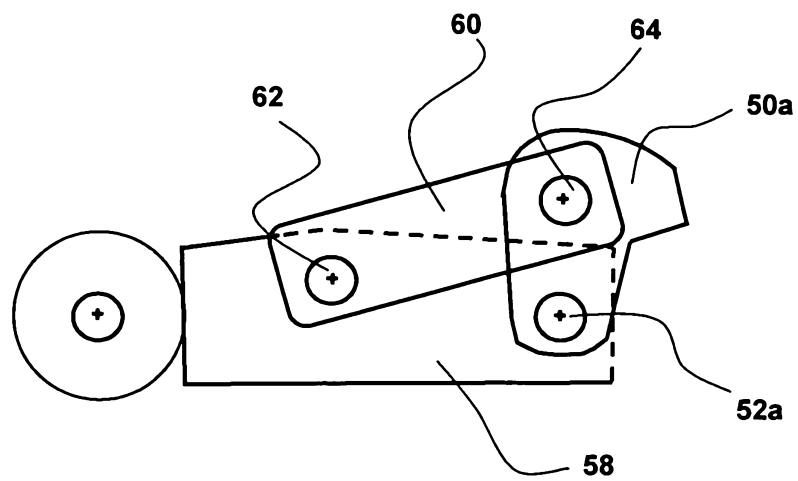
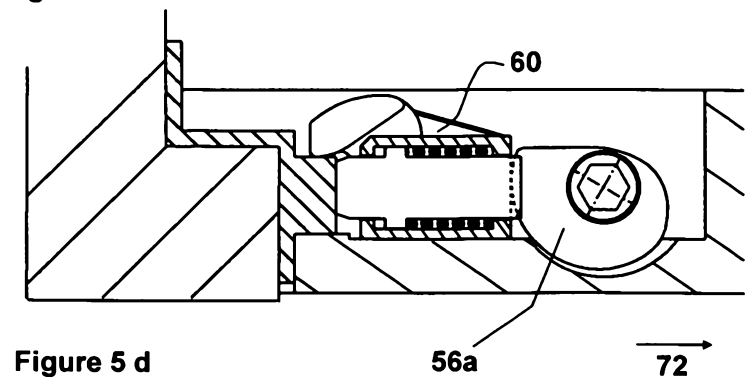
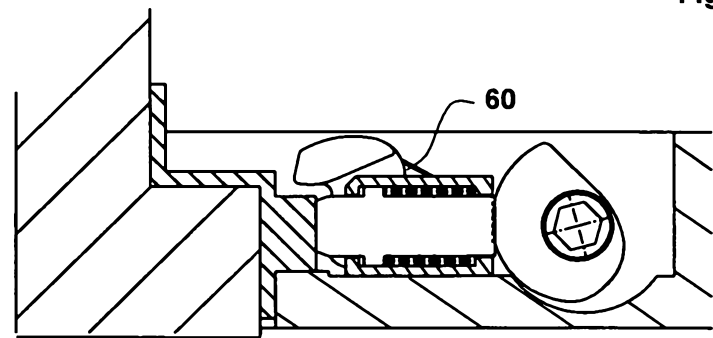
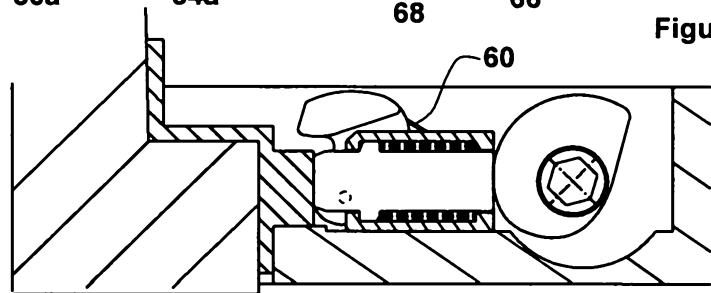
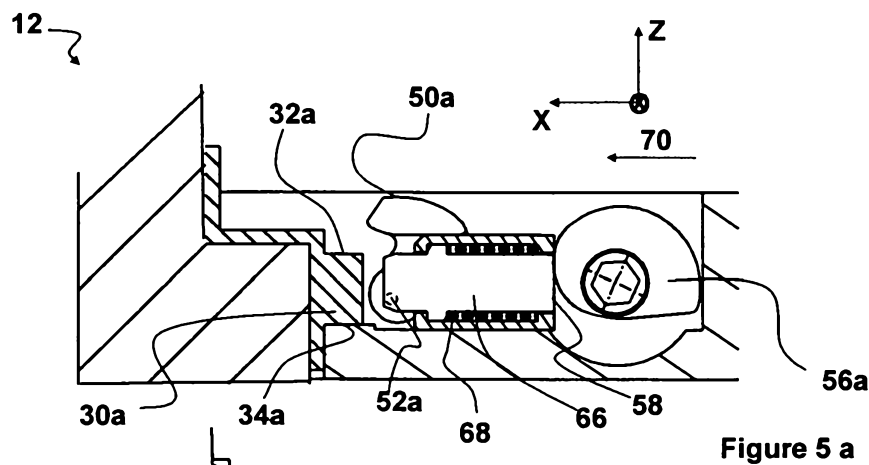


Figure 4



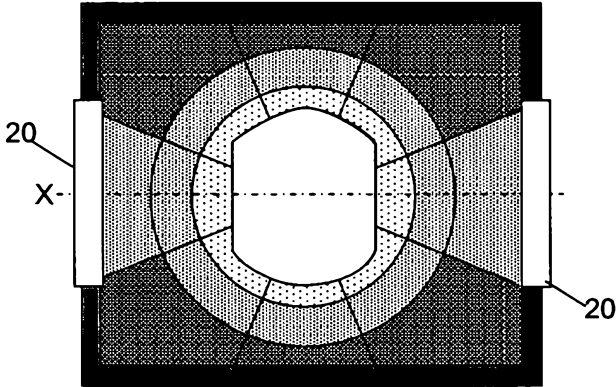
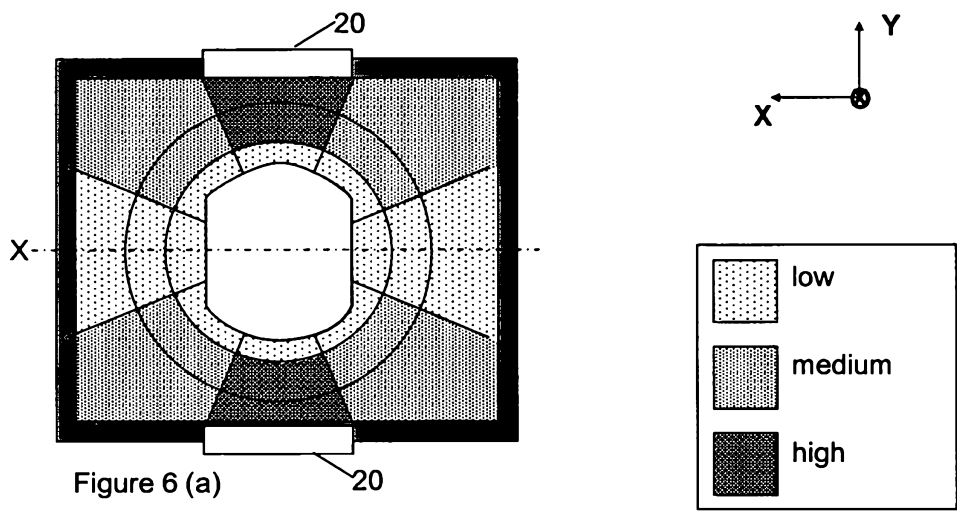


Figure 6 (b)

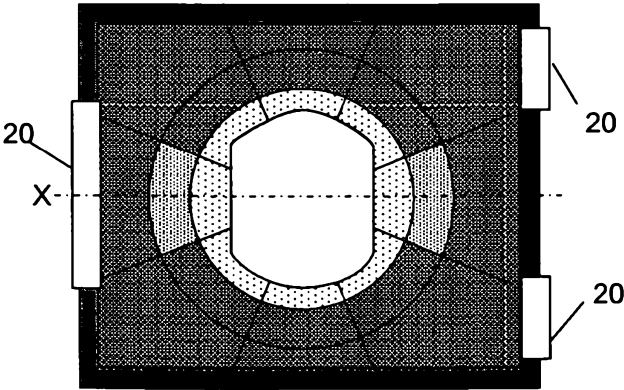


Figure 6 (c)

Figure 6