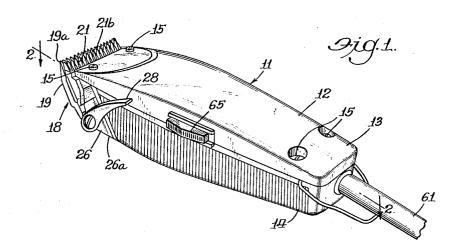
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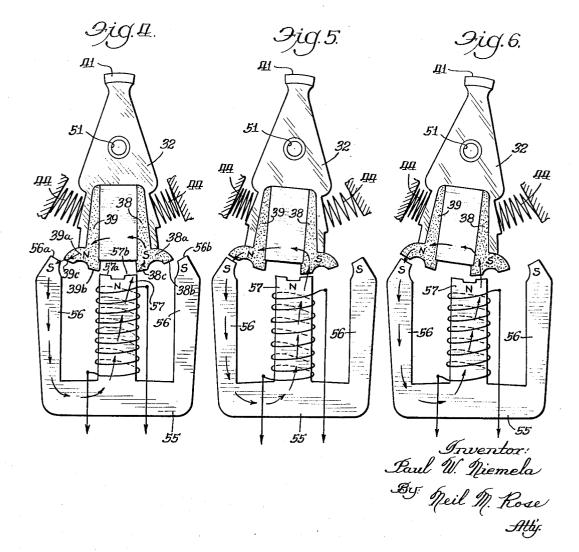
P. W. NIEMELA

HAIR CLIPPER HAVING OSCILLATING ARMATURE MOTOR

Filed July 5, 1968

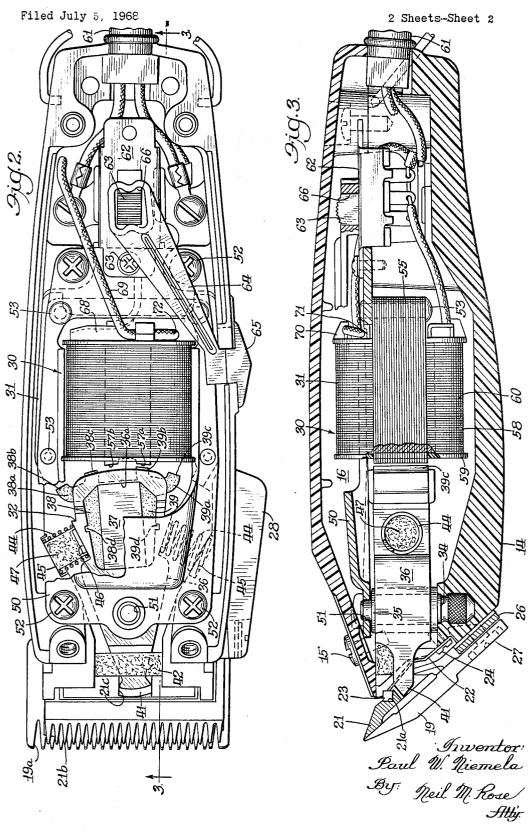
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HAIR CLIPPER HAVING OSCILLATING ARMATURE MOTOR



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3,493,793 HAIR CLIPPER HAVING OSCILLATING ARMATURE MOTOR Paul W. Niemela, Milwaukee, Wis., assignor to John Oster Manufacturing Company, Milwaukee, Wis., a 5 corporation of Wisconsin Filed July 5, 1968, Ser. No. 742,938 Int. Cl. H02k 33/06

U.S. Cl. 310-29

22 Claims

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ABSTRACT OF THE DISCLOSURE

A hair clipper having a vibratory motor mounted in a plastic housing by means of a post which pivotally supports the armature and locates the field supporting frame 15 which is secured to the plastic housing. The armature is provided with a permanent magnet to achieve a frequency of oscillation equal to the frequency of the alternating current source and having two pairs of armature poles cooperating with corresponding field poles to obtain a 20 that it is important that the motor output remain fairly performance characteristic particularly suited for an electric hair clipper.

BACKGROUND OF THE INVENTION

The invention relates to electric hair clippers and more specifically to an electric hair clipper being driven by an oscillating armature type electric motor. The use of vibratory or oscillating armature type motors has been relatively common in hair clippers for many years. In general, 30 these vibratory motor hair clippers have been lower in cost than the rotary armature motor hair clippers, and as a consequence, their use has been particularly important in the hair clipping sets sold for use in the home. In 35 general, the professional barber is interested in a hair clipper which will be as light as possible and give optimum performance. Accordingly, the barber has been willing to pay the additional cost demanded for the rotary armature motor type of hair clipper. 40

There have, however, been many attempts to satisfy the barber with a vibrator type hair clipper. The vibrator motors have in general been heavier than the rotary armature motors of similar power. This greater weight is particularly offensive to the barber who must use the 45 hair clipper relatively constantly during the day. Any small additional weight increases his fatigue considerably. Because of this weight problem which is inherent in the vibrator type motor, it is important that the power output per unit weight of such a motor be made as high as pos-50sible to permit minimizing the weight for a given power output.

Another problem which has made the vibrator motor hair clipper unpopular is the presence of excessive vibration of the clipper housing. The vibrator motor includes 55 an armature which reciprocates or oscillates to drive the blade of the hair clipper. All mass in the unit which is not a part of the armature vibrates at the same frequency as the armature but in the opposite direction. This vibration is in response to the forces driving the armature and 60 is exhibited as vibration transmitted through the housing to the hand of the user. The magnitude of the vibration, which the clipper housing transmits to the hand, is inversely proportional to the moment of inertia of the field and directly proportional to the moment of inertia of the 65armature. Accordingly, to produce a hair clipper which

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would utilize an oscillatory motor and be acceptable to professional barbers, it is important to minimize the mass of the armature and to provide a means for reversing its direction of movement with a minimum amount of noticeable housing vibration. While increasing the mass of the field would, of course, reduce housing vibrations, it is also necessary to maintain a light overall weight of the clipper since the barber may use it continuously for long periods.

An additional problem which adds to the unpopularity of the vibratory or magnetic clipper is the sensitivity of the motor to fluctuation in the supply voltage or changes in the load. In order to maintain a fairly constant blade stroke, the conventional vibrator motor powered hair clipper must be adjusted by the user whenever the load changes, such as when a blade set is lubricated or replaced, placed, and whenever the supply voltage fluctuates. Because of the vibrator motor's sensitivity the fluctuating input voltage or changes in the load and the fact constant over a range of loads and input voltages thereby eliminating the need for adjustment by the the user, it would be desirable to have a vibrator motor which would not be inherently load sensitive as are the prior art 25 devices.

The conventional construction of the typical hair clipper today involves the use of a split plastic housing which encloses the electric motor. In general, these motors are complete subassemblies which may be merely screwed or bolted to the plastic housing. Since the plastic housing itself must be made of fairly rigid material, it is desirable to utilize the plastic housing as at least a part of the motor supporting frame. In the past, many attempts to accomplish this objective have resulted in complex assembly procedures which have cost more than the savings associated with integrating the motor with the plastic housing.

SUMMARY OF THE INVENTION

The invention is directed to a vibratory electric motor which includes a novel field and armature structure. This structure increases the power output of the motor as compared to prior art motors of the same size, weight, and power input. The armature includes a permanent magnet which is associated with a pair of elongated pole pieces arranged to conduct the magnetic flux produced by the permanent magnet. From each of the pole pieces, a pair of salient pole faces project which cooperate with corresponding salient pole faces on the adjacent field member.

The field is an E-shaped laminated core having an energized coil mounted on the center leg. There is a salient pole formed on the ends of the outer legs and a salient pole having two pole faces formed on the end of the central pole of the field core. With the coil on the center leg energized, the two central field pole faces will always be magnetized at the same polarity and opposite the polarity of the two outer faces at a given point in time. Of the four pole faces on the armature and the four pole faces on the field, all are utilized in each half of the oscillating cycle. Two corresponding pole faces on the field and two on the armature will attract while the remaining two pole faces on the field and the two on the armature repel each other causing the armature to move in one direction. At the current in the coil winding

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diminishes sinusoidally, the force also decreases. Similarly, as the current changes polarity, the forces on the armature change direction forcing the armature motion to change direction. This arrangement in conjunction with the armature centering springs provides a smooth reversal of armature direction, provides a power stroke in each direction, and limits the motion of the armature to its most efficient range of operation.

Since with the oscillating armature motor it is difficult to maintain a uniform stroke under varying conditions of 10 load and input voltage, the action of the field on the armature at the reversal of direction is particularly important. This action limits the travel of the armature very effectively under light loads or no loads and high voltage conditions and eliminates the need for bumpers 15 or heavy no linear action restraining springs.

The armature is mounted within the plastic housing by means of an armature supporting pin which is molded into the plastic housing which serves as a motor supporting frame. The armature is pivotally supported on 20 this pin and is retained thereon by a metallic frame member which supports the motor field. By having the motor field accurately positioned on the frame member and by having the frame member accurately located through engagement with the end of the armature support pin, one 25 is assured of having the field accurately located with respect to the armature thus permitting a small air gap which is important in obtaining an efficiently operated motor. The field supporting frame is screwed to the plastic housing member which carries the armature support 30 pin but it is located entirely by the armature support pin.

An object of the present invention is to provide a low cost hair clipper which will be light in weight and have vibration.

A further object of the present invention is to provide an improved vibrator type motor which is high in efficiency and low in cost.

Another object of the present invention is to provide an 40improved vibrator type motor having a rate of oscillation equal to the frequency of the alternating current power supply.

Another object of the present invention is to provide by means of the four pairs of armature and field pole 45 faces, a hair clipper having a uniform stroke of oscillation of the armature at various blade loads and with line voltage fluctuations.

Still another object of the present invention is to provide an improved electric hair clipper having an armature 50 support pin molded integrally with one of the plastic housing halves and having this pin serve as a bearing for the armature and a locating means for the motor field.

Further objects and advantages of the present invention will become apparent as the following description 55 proceeds, and the features of novelty which characterize the invention will be pointed out with particularity in the claims annexed to and forming a part of this specification.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a perspective view of a hair clipper embodying my invention;

FIG. 2 is an enlarged section view taken substantially 65 along line 2-2 of FIG. 1;

FIG. 3 is a sectional view taken along line 3-3 of FIG. 2 assuming that FIG. 2 shows the complete hair clipper:

FIG. 4 is a schematic diagram illustrating the relationship between the armature and the field when the armature is in its rest position before energization of the field coil:

FIG. 5 is a schematic diagram similar to FIG. 4 but with the armature shown in its deflected position when 75 in FIG. 2 thereby locking the pole pieces 38 and 39

the field coil has magnetized the field to move the armature in one direction:

FIG. 6 is a schematic diagram similar to FIGS. 4 and 5 but shows the armature in its extreme position in which it has moved past the position shown in FIG. 5.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring to the drawings, there is shown in FIG. 1 a hair clipper designated generally by reference numeral 11. The hair clipper 11 includes a housing 12 which is made up of two housing members 13 and 14 which are secured together in abutting relation by screws 15 to form a motor enclosure 16.

Received on the front end of the elongated housing 12 is a blade set 18 which consists of a comb 19 and a cutter 21 which is pressed into shearing engagement with the comb 19 by means of a biasing spring 22. The biasing spring is a rectangular frame member having a plastic bearing portion 23 secured on its outer end for sliding engagement with a groove 21a formed in the cutter 21. At its inner edge, the biasing spring 22 is secured to the lower housing member 14 by means of screws 24.

The comb 19 and the cutter 21 are provided with teeth 19*a* and 21*b*, respectively, along their abutting outer edges as is best shown in FIGS. 1 and 2. The comb 19 is supported for movement relative to the lower housing member 14 by means of a blade support 26. The blade support 26 extends across the bottom of the housing member 14 as shown in FIG. 3 and has upwardly and inwardly turned ends 26a which are received in slots in the side wall of housing member 14 permitting the support 26 to slide in the plane of the blade set 18. The comb 19 is secured to the blade support 26 by means of screws 27. The a vibratory type motor which will produce little external 35 position of the blade support and the comb 19 is controlled by means of lever 28 which has on its inner face eccentric means to move the blade support 26 as the lever 28 is rotated. This type of control is old and well known in the art and serves to change the relative position of the comb 19 with respect to the cutter 21 so that the barber may cut hair very short when the blade set is positioned as shown in FIG. 3 or cut hair longer when the comb is displaced further outwardly with respect to the cutter 21.

> Mounted within the enclosure 16 is a motor 30 which includes a field or stator 31 and an oscillating armature 32. The armature 32 is supported for oscillating movement by means of a bearing pin 34 which is secured to the lower housing member 14 by having its low end molded into the plastic housing member 14. The armature itself includes an oil impregnated bearing bushing 35 which is secured to a nylon frame or carrier 36. The carrier 36 is formed with an internal pocket 36a in which is received a permanent magnet 37 and a pair of pole pieces 38 and 39. The pole pieces 38 and 39 are elongated members of magnetically permeable material such as soft iron and are formed at their outer ends with crescent shaped poles 38a and 39a which define a pair of salient pole faces 38band 38c and 39b and 39c respectively. Thus, each pole 60 piece has a pair of salient pole faces formed by the crescent shaped poles on the outer ends thereof. The permanent magnet 37 is polarized so that the pole pieces 38 and 39 are magnetized to the opposite polarity. As a consequence, the salient pole faces 38b and 38c formed on the pole 38a will be polarized to the opposite polarity from the other armature pole 39a having salient pole faces 39b and 39c.

> In order to assemble the pole pieces 38 and 39 to the nylon carrier 36, the pole pieces are first inserted through openings 40 until their elongated portions are positioned 70within the pocket 36a. They are then spread apart until suitable retaining ribs 38d and 39d engage corresponding notches in the nylon carrier 36. The permanent magnet 37 is then inserted downwardly into the pocket 36a as shown

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against removal or displacement outwardly through the openings 40. The frictional engagement between the permanent magnet 37 and the pole pieces 38 and 39 within the pocket 36a tends to prevent its removal from the pocket 36a. In addition, the strong magnetic force of the permanent magnet 37 tends to retain it within the pocket 36a.

The nylon carrier 36 of the armature 32 is formed with a driving lever 41 which extends radially from the bearing pin 34 in a direction opposite from the perma-10nent magnet 37 and the pole pieces 38 and 39. The cutter 21 is formed with a slot 21c which receives the end of the driving lever 41. As the armature 32 oscillates about the axis of the bearing pin 34, the cutter 21 is reciprocated in shearing engagement with the comb 19. As is 15 conventional in the hair clipper art, the area around the driving lever 41 where it extends outwardly from the motor enclosure 16 is surounded by a plastic foam 42 which prevents the entrance of hair clippings into the motor 16. 20

The armature 32 is biased to a central position by means of coil springs 44 which are compressed between the lower housing member 14 and the nylon carrier 36. The housing member 14 is formed with a pair of Ushaped recesses or spring seats 45 which receive the outer $_{25}$ ends of the springs 44. The inner ends of the springs 44 are received on locating bosses 46 which are formed integrally with the nylon carrier 36. To dampen vibration noises which otherwise might be associated with the springs 44, they are filled with foam plastic mate- 30 rial 47.

The motor field 31 is supported within the motor enclosure 16 by means of a sheet metal member 50 which is the field supporting frame. The member 50 serves not only to support the field 31 but also accurately 35 locates the field 31 with respect to the armature 32. This accurate location of the field is accomplished by locating the frame 50 from the bearing pin 34. An opening 51 in the frame 50 receives the upper end of the bearing pin 34 as shown in FIG. 3. The frame 50 is secured to 40 the lower housing member 14 by means of four screws 52 which extend through openings in the corners of the frame 50. The field 31 is riveted to the frame 50 by means of the rivets 53 which also retain the laminations in assembled relation.

The field 31 includes an E-shaped core 55 made of 45 minotions of 45laminations of magnetically permeable material which are retained together and secured to the frame 50 by means of the rivets 53 as explained above. The E-shaped core 55 has a pair of outer legs 56 and a central leg 57. $_{50}$ The central leg being substantially thicker than the outer legs and terminating in a pair of salient pole faces 57aand 57b. The outer legs of the core 55 terminate in salient poles 56a and 56b. Surrounding the central leg 57 of the core 55 is a coil 58 which includes a plastic bobbin 5559 and conventional insulated windings 60. When the coil 58 is energized by current flowing in either direction, it will induce magnetic flux which will cause the salient pole faces on the center leg 57 to be magnetized to one polarity while the salient poles 56a and 56b on the outer 60legs will be magnetized to the opposite polarity. It is evident from a review of the schematic diagrams in FIGS. 4-6 that the field will have two pairs of oppositely polarized pole faces. These pairs will be 56a and 57a and 57band 56b. The manner in which these poles cooperate with 65 corresponding armature poles will be explained more fully below.

The hair clipper 11 is provided with a power cord 61 which is connected to the end of the hair clipper opposite from the end on which the blade set 18 is mounted. $_{70}$ To control the supply of power to the motor 30, there is provided an on/off switch 62. The switch 62 is secured to one end of the field supporting frame 50 by means of a screw 63. Suitable leads are provided to interconnect the power cord 61, the switch 62, and the field coil 58. 75 load or high input voltage. If the motor was adjusted to

It should be noted that the assembly of the parts to the housing 12 is simplified considerably by having the switch 62 mounted integrally with the coil 31 and the supporting frame 50. The switch 62 is a slide switch having an operating button 63 which, of course, is located within the enclosure 16.

To permit operation of the switch 62 when the housing members 13 and 14 are assembled together, a switch control member 64 is provided. The switch control member 64 is formed with an outer operating portion 65 which is exposed for finger operation on the outer surfaces of the housing 12. At the other end of the switch control member, an opening 66 is formed which receives the operating button 63 of the on/off switch 62. The control member 64 is clamped between the housing members 13 and 14 with sufficient clearance provided for it to slide between its various operating positions. In so doing, the on/off switch 62 may be readily controlled. Thus, the control member 64 provides a simple and effective means of operating the switch 62 through the use of a single plastic part which is merely assembled between the housing members 13 and 14. The bobbin 59 of the coil 58 is formed with a simplified means for making the lead connections to the very fine coil wire 60. This means includes a plastic pocket 68 which is formed integrally with the end wall of the bobbin and receives the ends of the coil wire 60 and a connecting lead 69. An overhanging abutment 70 formed integrally with the ends wall of the bobbin and a lower wall 71 provides a space within which the lead wire 67 may be doubled back forming a loop 72. As the loop 72 is drawn up into more or less jamming engagement with the overhanging abutment 70 and the wall 71, a suitable strain relief is provided which prevents the application of any force on the connection between the lead wire 69 and the coil wire 60.

In analyzing the operation of the hair clipper 11, it should be understood that the device is intended to be energized by an alternating current power source such as the conventional 60 cycle 110 volt power supply. The coil 58 receives current flowing first in one direction and then in the other direction in each half cycle. This causes the polarity of the field poles to be reversed each half cycle. To understand the operation of the motor 30 and the manner in which the armature interacts with the field attention should be directed to the schematic diagrams of FIGS. 4, 5, and 6. It should be appreciated that the armature poles will, of course, always remain polarized in the same manner which has arbitrarily been shown in the figures as the pole piece 38 polarized south and the pole piece 39 polarized north. When the coil 58 receives current such that the central leg 57 is polarized north, the armature 32 tends to rotate clockwise as shown in FIGS. 4-6 by virtue of the attraction between the salient pole faces 39c and 56a and pole faces 38c and 57b and the repulsion between the salient pole faces 39b and 57a and pole faces 38b and 56b. The repelling an attracting forces would contribute equally to the output torque when averaged over each entire cycle. The armature 32 moves from the position shown in FIG. 4 to the position shown in FIG. 5 with the above described pole faces which were attracting each other ultimately becoming aligned as shown in FIG. 5. In FIG. 6, it is shown that there is some tendency from the armature 32 to override because of its inertia moving past the field poles. At this point, the attraction exerted by the poles retards the armature movement before the current flow changes and reverses the polarity. This action combined with the action of the springs 44 tends to provide a smooth reversal in the direction of the motion of the armature 32 with a minimum amount of vibration being produced.

The principal difficulties with prior art magnetic or oscillatory type hair clippers has involved the excessive armature vibrations which occur under conditions of no

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produce the proper stroke under normal voltage and load conditions, there would be a tendency for the armature to increase the stroke substantially when the load was lessened or removed. This would, of course, create significant problems with respect to changing the blade set and introducing varying loads to the motor.

By designing the instant hair clipper to have a normal stroke under load conditions equal to twice the width of the pole faces, I have obtained a hair clipper which provides essentially uniform stroke under varying conditions of load and voltage. When the load is lessened or eliminated, the armature pole faces tend to swing past the field pole faces to which they are attracted. Because the width of the field poles is equal to the width of the armature poles, an attracting force is exerted in a direction to prevent the armature poles from swinging past the field poles in the condition of light load or over voltage.

Many tests have been conducted under conditions of varying load and even with changes in the armature air gaps to represent normal manufacturing conditions. It 20 was found that variations of up to 100 percent in the load produced less than a 15 percent change in the stroke of the motor. In contrast, tests of conventional prior art clippers indicated variations of over 100 percent in the stroke under the same variations in load conditions. Accordingly, by a relatively simple modification in the configuration of the magnetic circuit, I have provided a practical, inexpensive magnetic hair clipper which is for practical purposes insensitive to load and voltage changes. By having the double pairs of pole faces on the armature 30and the field, I have been able to obtain controlled movement of the armature and thus concentrate the power in the desired range of operation. This vibrator motor is of reasonable physical configuration and has ideal performance characteristics for use in a hair clipper.

While it has been noted above that the armature pole faces are constructed of the same width as the field pole faces, the size and spacing of the magnetic poles should also be considered. The displacement or stroke for which the hair clipper is designed when operating under load may best be illustrated by considering FIG. 5 of the drawings. The motor operates most efficiently when the load is such that the armature displaces to the position shown in FIG. 5 and then oscillates to the corresponding position in the other position. In accomplishing such a 45 rotation, the armature moves through a stroke equal to approximately twice the width of each pole face. Another important design criteria is the dimensioning of each armature pole 38a and 39a with a width equal to approximately the distance between the outer pole face 50 56a or 56b and the adjacent center pole face 57a and 57b, respectively. This arrangement permits all of the field poles to exert maximum torque in either attracting or repelling the adjacent armature poles.

In this regard, by considering FIG. 4, one may see that armature pole faces are all adjacent to respective field pole faces but are not in overlapping relationship as when a pole face is positioned radially of another pole face. As the magnetic flux causes the armature to rotate from the position shown in FIG. 4 toward the position shown in FIG. 5, substantial torque is developed at the pole faces 39c and 38c as a consequence of the rapid rate of change of flux in the magnetic circuit. At the same time, there is a force produced at the pole faces 38b and 39bby virtue of the repelling force exerted by the field pole faces 56b and 57a. Since the torque reverses in direction as the armature moves toward the position shown in FIG. 6, the clipper is designed so that under full load the stroke will terminate with an outer armature pole face aligned with an outer field pole face. The action illustrated by FIG. 6 is operative only under conditions of light load or high impact voltage when the above described restraining action is necessary.

While there has been illustrated and described a par- 75

ticular embodiment of the present invention, it will be understood that changes and modifications may occur to those skilled in the art, and it is, therefore, contemplated by the appended claims to cover all such changes and modifications as fall within the true spirit and scope of the present invention.

What is claimed as new and desired to be secured by Letters Patent of the United States is:

1. A magnetic motor of the type having an oscillating armature comprising a field including an E-shaped laminated core and coil means for magnetizing the outer legs of said core to the opposite polarity from the center leg, an armature supported by a frame for pivotal movement about an axis spaced from said field, said legs being formed with pole faces having cylindrical curvatures the 15 axis of which is coincident with said armature axis, said armature including a permanent magnet and a pair of pole pieces connected to be magnetized to opposite polarities, each pole piece being formed with a pair of outwardly extending pole faces, said armature pole faces being of the same width as said field pole faces and positioned to move in closely spaced relation to said field pole faces, said armature and field pole faces being spaced so that one pole face of each pair of armature pole faces is 25attracted to a respective field pole face during each half cycle of alternating current energization of said field coil.

2. The combination of claim 1 wherein the center leg of said E-shaped core is formed with two pole faces, one of which is positioned to cooperate with one of said pole pieces and the other of which cooperates with the other pole piece.

The combination of claim 1 where in the rest position of the armature said outer field pole faces are displaced from but immediately adjacent to the outermost edges of said pole pieces so that energization of said coil by an alternating current causes said armature to oscillate through an angle in which the armature pole faces travel a distance equal to twice the width of a pole face.
The combination of the armature pole face.

4. The combination of claim 3 including springs which bias said armature to said rest position, said springs and the attraction between said armature and field pole faces preventing overtravel of said armature under conditions of light load and high imput power.

5. The combination of claim 1 wherein said armature pole faces in each pair are spaced apart a distance equal to the distance between an outer leg field pole face and its adjacent center leg field pole face less the combined width of the armature field poles of one pair.

6. An electric vibratory motor comprising an oscillating armature having two pairs of adjacent salient pole faces, a field having two pairs of salient pole faces, means for inducing magnetic flux in said armature whereby both pole faces in each said pair of armature pole faces will 55have the same polarity and one pair of armature pole faces will have the opposite polarity from the other pair, a field coil inducing magnetic flux in said field whereby each pole face in each said pair of field pole faces will have the opposite polarity from the other face in that 60 pair, a pole face in each of said pairs of field pole faces being closely spaced to each other and being magnetized with the same polarity, said armature oscillating between two positions in which a pole face of each pair of armature pole faces is aligned with a pole face in each pair of 65 field poles with a completely different set of pole faces being aligned in each of said two positions, said oscillating being produced by energizing said field coil with alternating current.

70 7. The vibratory motor of claim 6 wherein said armature includes a permenent magnet positioned to magnetize said pairs of armature pole faces to opposite polarities whereby said armature oscillates at the same frequency as the energizing current in the field coil.

8. The vibratory motor of claim 6 wherein said arma-

ture includes a pair of radially extending pole pieces formed with said armature pole faces, a permanent magnet positioned between said pole pieces to magnetize them to opposite polarities, each said pair of armature pole faces being formed by crescent shaped members at the ends of said pole pieces.

9. The vibratory motor of claim 6 wherein said field comprises an E-shaped core of magnetically permeable material with said coil on the center leg thereof, said field pole faces which are closely spaced and magnetized 10 to the same polarity are formed on the end of the center leg of said E-shaped field core.

10. The vibratory motor of claim 9 wherein said armature is formed with a pair of elongated pole pieces of magnetically permeable material, said pole pieces ex- $_{15}$ tendiing generally radially with respect to the axis of oscillation of said armature, a permanent magnet positioned between said pole pieces to magnetize said pole pieces to opposite polarities each of said pole pieces being formed at its outer end with one of said pairs of salient 20 pole faces.

11. An electric vibratory motor comprising a pivotally mounted armature including a permanent magnet supported by a non-magnetic carrier, said armature having two pairs of salient pole faces each peripherally spaced 25 and all situated equidistant from the axis of rotation of said armature, an E-shaped laminated field core of magnetically permeable material having a field coil wound on the central leg thereof, salient field pole faces formed on the free ends of the outer legs of said field, a pair of 30 salient field pole faces formed on the free end of said central leg, said field pole faces being spaced equidistant from said axis of rotation to provide a uniform air gap between said armature and field pole faces as the armature pivots about its axis, said pole faces being peripher-35 ally spaced so that the outermost pole face of one of said pair of armature pole faces is aligned with one of the outer field pole faces when the innermost pole face of the other pair of armature pole faces is aligned with the one of said pair of field pole faces on the central leg 40 which is most remote from said one pair of armature pole faces, said pairs of armature pole faces being symmetrical so that the outermost pole face of the other pair of armature pole faces are aligned with the other of said outer field pole faces when the innermost pole 45 face of said one pair of armature pole faces is aligned with the other of said pair of field pole faces on the central leg.

12. The combination of claim 11 wherein said carrier is formed with a side opening recess in which said magnet 50 means at one end for supporting said carrier for pivotal is received, a pair of pole pieces spaced apart and in engagement with opposite faces of said magnet so each pole piece is magnetized to the opposite polarity, one of said pairs of armature salient pole faces formed on each of said pole pieces. 55

13. The combination of claim 12 wherein each said pole piece comprises an elongated portion positioned in said recess in engagement with said magnet and a semicylindrical portion having the curved side thereof connected to said elongated portion and the outwardly extending walls of said semicylindrical portion defining one of said pairs of armature salient pole faces.

14. A vibratory motor comprising a stator having an energizing winding, an armature mounted for oscillatory motion in the magnetic field of said stator and includ- 65 ing a molded plastic carrier having an integrally formed drive arm at one end and a magnet supporting portion at the other end bearing means intermediate said drive arm and said magnet supporting portion, an enlarged recess in said magnet supporting portion, a pair of pole 70 pieces insertable into said recess with pole faces extending radially from the end of said magnet supporting portion, a permanent magnet supported in said recess and positioned to magnetize said pole pieces to opposite

through which said magnet is assembled, said magnet securing said pole pieces in assembled relation to said carrier.

15. The combination of claim 14 wherein said recess is wedge shaped, said pole pieces being positioned in part in passageways extending from said recess to the exterior of said carrier at the outer end of said magnet supporting portion.

16. The combination of claim 15 wherein said portions of said pole pieces within said recess are wedge shaped, said magnet having parallel outer walls which engage said pole pieces, interlocking means on said pole pieces and the walls of said carrier recess to secure said pole pieces against lengthwise displacement out of said recess.

17. The combination of claim 14 wherein said carrier includes passageways extending outwardly from said recess at the outer end of said magnet supporting portion, said pole pieces being positioned in said passageways with said pole faces exposed outside of said carrier and portions of said pole pieces positioned in said recess in engagement with said permanent magnet.

18. The combination of claim 17 wherein said magnet supporting portion of said carrier has a sidewardly facing opening adjacent said permanent magnet and through which said magnet is insertable into said recess, said recess being dimensioned to tightly receive said pole pieces and magnet whereby the parts are retained in assembled relation by virtue of their interfering engagement.

19. The vibratory motor of claim 14 wherein said stator includes an E-shaped laminated core having outer and inner salient pole faces, said pole pieces each being formed with two spaced salient pole faces, said salient pole faces on said core and said pole pieces being of equal width, said energizing winding magnetizing said outer salient pole faces to the opposite polarity from said inner salient pole face, said stator attracting one armature salient pole face of each pole piece during each half cycle of alternating current energization and said stator attracting the other armature salient pole face of each pole piece during alternate half cycles of current energization.

20. An oscillating armature type of magnetic motor comprising a stator having a plurality of salient pole faces, an energizing coil for magnetizing said pole faces to different polarities, said polarities being reversed as said coil is energized by alternating current, an armature having a plurality of salient pole faces and being positioned relative to said stator to be rotated in opposite directions during each half cycle of current, said armature including a carrier of non-magnetic material having pivot movement in a plane, a magnet supporting portion on said carrier having a side opening recess with said opening facing said plane of movement, end openings in said carrier communicative with said recess, L-shaped pole pieces having elongated portions within said recess and a pair of salient pole faces on the outer end of each pole piece positioned outside of said recess, said pole pieces extending through said end openings, a permanent magnet received in said recess in engagement with said pole 60 pieces, said magnet being dimensioned to be insertable through said side opening and said elongated portions of said pole pieces being dimensioned to be insertable into said recess through said end openings, said magnet and pole pieces fitting tightly into said recess to retain them therein when said armature is oscillated about said pivot means.

21. The combination of claim 20 wherein said pole pieces and the inside walls of said recess are formed with interengaging ribs and grooves which lock the elongated portions of said pole pieces against lengthwise movement in said recess.

22. The combination of claim 21 wherein said ribs and grooves are positioned so that said pole pieces may be pivoted about said pole faces after insertion of said elonpolarities, and an additional opening into said recess 75 gated portions into said recess to engage said ribs and

said grooves, said magnet being positioned to retain said pole pieces against pivotal movement.

References Cited

UNITED STATES PATENTS

2,238,390	4/1941	Кпорр 31029	D. 1. DOCCHII, Hogista
		Ruud 310—29	U.S
3,343,011	9/1967	Daniels et al 31029 X	10 30-43.92, 45; 310-37

FOREIGN PATENTS

3/1951 Great Britain.3/1951 Belgium. 651,083 499,614

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U.S. Cl. X.R.