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PIEZOELECTRIC COMPOSITES AND METHODS FOR MANUFACTURING SAME

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BACKGROUND OF THE INVENTION

Field of the Invention

10 This invention relates to piezoelectric composites, and more particularly to piezoelectric composites for high-frequency ultrasound applications and methods of manufacturing such composites.

Background Art

15 Typically, high quality medical imaging uses ultrasonic transducers or transducer arrays that posse the properties of good sensitivity and wide frequency bandwidth. Conventional transducers utilizing monolithic piezoelectric material such as, for example, lead ziconate titanate ("PZT"), typically exhibit a large acoustic impedance mismatch between the transducer and the medium under test, such as, for example, water, human tissue, and
20 the like. To overcome this problem, piezoelectric composites that are made of individual small piezoelectric elements surrounded and isolated by a polymer matrix, such as, for example, epoxy, have been proposed. These proposed small piezoelectric elements play an increasingly important role in the development of ultrasonic transducers for medical imaging. The most
25 commonly used structures of piezoelectric composite consist of small strips or posts of PZT that are embedded in a host matrix of polymer material. The height of the strips or posts is normally about one half wavelength at the operating frequency.

30 The conventional process for the fabrication of a piezoelectric composite, the "dice and fill" method, begins with a monolithic slab of piezoelectric material. Slots, or kerfs, are cut into the slab using a dicing saw.

The slots are then filled in with host material such as epoxy. A two-dimensional piezoelectric composite which consists of posts and host matrix is made by cutting the piezoelectric slab in two orthogonal directions.

5 The volume ratio, which is the ratio of ceramic volume over the whole composite and is usually equal to the ratio of ceramic width to pitch size in the cases of conventional 1-3 and 2-2 composites, affects characteristics of the piezoelectric composite such as coupling coefficient, velocity, acoustic impedance, and the like. Thus, changing the volume ratio allows for the customization of the particular piezoelectric composite for the desired
10 transducer application/design. Unfortunately, in the conventional "dice and fill" process, the slot/kerf size is determined by the thickness of the saw blade. It is difficult to make a specific volume ratio composite when the pitch size needs to be fixed. Normally, the volume ratio is changed by using blades of different thickness, but the volume ratio is still limited by the thickness of the
15 blades that can be chosen, particularly when the slots/kerfs to be cut are of fine dimensions.

SUMMARY

20 In one aspect, the present

Subsequently, in a shift-dicing step, each first interdigitated piezoelectric composite slab is cut using the same pitch and slot size as the cut that was made on the original piezoelectric base slab. The cutting position in this shift-dicing step is shifted in a width-wise dimension by a distance
5 equal to a portion of the ridge width. The remaining second ridges will consist of both piezoelectric material and polymeric fill material with a certain ratio which is determined by the shift distance of the cutting operation. Two such first interdigitated piezoelectric composite slabs are formed and then interdigitated by positioning them face to face and inserting the second ridges
10 of one first interdigitated piezoelectric composite slab into the second slots of the other first interdigitated piezoelectric composite slab. Because the width of each second ridge is less than the width of each second slot, a second gap is formed that may be filled with a polymeric material when the first interdigitated piezoelectric composite slabs are interdigitated. The uncut
15 portions on one or both sides of interdigitated slab may be removed by grinding or lapping. A uniform composite/array with any volume ratio can be made through above described process.

The invention disclosed herein presents a practical and easy way to produce such piezoelectric composite/array with arbitrary volume ratio for
20 both low and high frequency applications.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other features of the preferred embodiments of the
25 invention will become more apparent in the following detailed description in which reference is made to the appended drawings wherein:

Fig. 1A is a vertical section of one base piezoelectric slab diced in accordance with an embodiment of the present invention.

Fig. 1B is a vertical section of a pair of base piezoelectric slabs
30 disposed in overlying registration.

Fig. 1C is a vertical section of the pair of base piezoelectric slabs of Fig. 1B interdigitated in accordance with an embodiment of the present invention.

Fig. 1D is a vertical section of a first interdigitated piezoelectric composite slab with a portion of the piezoelectric base slab removed.

5 Fig. 2A is a vertical section of one first interdigitated piezoelectric composite slab of Fig. 1D showing portions of the slab to be removed, the portions to be removed shifted a predetermined distance in accordance with an embodiment of the present invention.

Fig. 2B is a vertical section of one first interdigitated piezoelectric composite slab of Fig. 2A diced in accordance with an embodiment of the present invention.

10 Fig. 2C is a vertical section of a pair of diced first interdigitated piezoelectric composite slabs disposed in overlying registration.

Fig. 2D is a vertical section of the pair of diced first interdigitated piezoelectric composite slabs of Fig. 2C interdigitated in accordance with an

to be removed are shifted a predetermined distance in accordance with an embodiment of the present invention.

Fig. 3G is a vertical section of one intermediate interdigitated composite slab of Fig. 3F diced in accordance with an embodiment of the present invention.

Fig. 3H is a vertical section of a pair of diced intermediate interdigitated piezoelectric composite slabs disposed in overlying registration.

Fig. 3I is a vertical section of the pair of diced intermediate interdigitated composite slabs of Fig. 3H interdigitated in accordance with an embodiment of the present invention.

Fig. 3J is a vertical section of a third interdigitated piezoelectric composite slab after grinding the top and bottom surfaces of the third interdigitated piezoelectric composite slab.

Fig. 4A is a vertical

Fig. 4G is a vertical section of one intermediate interdigitated composite slab of Fig. 4F diced in accordance with an embodiment of the present invention.

5 Fig. 4H is a vertical section of a pair of diced intermediate interdigitated composite slabs disposed in overlying registration.

Fig. 4I is a vertical section of the pair of diced intermediate interdigitated piezoelectric composite slabs of Fig. 4H interdigitated in accordance with an embodiment of the present invention.

10 Fig. 4J is a vertical section of a third interdigitated piezoelectric composite slab after grinding the top and bottom surfaces of the third interdigitated piezoelectric composite slab.

DETAILED DESCRIPTION OF THE INVENTION

15 The present invention is more particularly described in the following exemplary embodiments

invention allows for the production of two-dimensional composites, composite transducers, transducer arrays and the like of arbitrary and predetermined volume ratio and fine pitch.

Referring to Figures 1A-1D, a method for fabricating a first interdigitated piezoelectric composite slab 20 is shown. In one example, the fabrication process begins with a pair of conventional piezoelectric base slabs 10. Depending on the desired application, the base slab made is formed from any desired material having the appropriate electrical and acoustical properties. For example, the base slab may be formed from piezoelectric material, electrostrictive material, and the like. Each base slab is complementary to the other, and, as shown, is diced or cut to form first kerfs or first slots of a width K and a depth D . Each base slab 10 has a substantially planar upper surface 11 and has a longitudinal axis. As shown, a first cutting operation is preformed onto the upper surface of each base slab 10 so that a first plurality of longitudinally extending slots 12 of depth D and width K are defined in the planar upper surface of the base slab. Further, a first plurality of longitudinally extending ridges 14 having

The first gaps 16 (and the other gaps referenced herein) may be filled with a filling material. The filling material may comprise, for example, a polymeric material, such as, for example, epoxy, polymer micro-spheres, crystal bond, and the like, as is customary and standard practice in the manufacture of composite transducers, or they may be left, at least in part, unfilled. In one example, the diced slabs may be dry assembled and then the gap filling material may be introduced. In another example, at least one of the diced slabs is prewet and/or their slots filed with such gap filling material. Here, any excess amount of gap filling material can be forcibly displaced as the two diced slabs are brought together and the ridges of the first slab are interdigitated with the ridges of the second slab. In yet another example, at least one of the diced slabs is prewetted and the diced slabs are interdigitated and pulled together through capillary forces and/or atmospheric forces induced by a controlled withdrawal of excess gap filling material. One will appreciate that the gaps may not be completely filled or that they are only filled temporarily as some or the entire gap filling material is removed using conventional methods.

Next, the portion of the base slab 10 that extends above notional line 17 is ground, lapped away or otherwise removed to form

planar upper surface 21 and a longitudinal axis. Each first interdigitated piezoelectric composite slab is complementary to the other, and, as shown, is diced or cut in a shift-dicing step to form second kerfs or second slots of a width K and a depth D. In this aspect, a second cutting operation is
5 performed on the upper surface of each first interdigitated piezoelectric composite slab 20. The second cutting operation is spaced a distance S_1 that is a fraction of the pitch P from the original cutting, which, in this example, is $\frac{1}{4}$ the pitch P. The cutting position in this shift-dicing step is shifted in a width-wise dimension by a distance equal to a portion of the first ridge width. On
10 will appreciate that other fractions of the pitch P are contemplated for the shift distance S_1 of the second cutting.

After the second cutting, a second plurality of longitudinally extending slots 22 of depth D and width K are defined in the upper surface 21 of the first interdigitated piezoelectric composite slab 20. Further, a second plurality of
15 longitudinally extending ridges 24 having a width W and spaced by respective second slots 22 of the second plurality

gap 26 having a width K_2 is formed between each of the respective second ridges of the interdigitated diced first interdigitated piezoelectric composite slabs. The width of each second ridge is less than the width K between adjacent second ridges. In one example, the width K_2 of the second gap is substantially equal to the width K_1 of the first gap. One will appreciate that the second gaps may be filled with a polymeric material as described above.

Referring to Fig. 2E, a portion of the diced first interdigitated piezoelectric composite slabs that extends above notional line 27 is ground, lapped away, or otherwise removed to form a second interdigitated piezoelectric composite slab 30. In a further process, a portion of the diced first interdigitated piezoelectric composite slabs that extends below notional line 29 is ground, lapped away, or otherwise removed to form an alternative embodiment of the second interdigitated piezoelectric composite slab 30. As one will appreciate, the second interdigitated piezoelectric composite slab 30 has a pitch P_2 that is less than the pitch P_1 of the first interdigitated piez

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16. The method of claim 1, wherein the first gap is approximately the same size as the second gap.
17. The method of claim 1, wherein the shift distance S_2 is substantially equal to $1/4P$.

