

(12) **United States Patent**  
**Nagaoka et al.**

(10) **Patent No.:** **US 10,385,747 B2**  
(45) **Date of Patent:** **Aug. 20, 2019**

(54) **EXHAUST GAS PURIFICATION SYSTEM FOR INTERNAL COMBUSTION ENGINE, INTERNAL COMBUSTION ENGINE, AND EXHAUST GAS PURIFICATION METHOD FOR INTERNAL COMBUSTION ENGINE**

(71) Applicant: **ISUZU MOTORS LIMITED**, Tokyo (JP)

(72) Inventors: **Daiji Nagaoka**, Kamakura (JP); **Teruo Nakada**, Yokohama (JP); **Takayuki Sakamoto**, Fujisawa (JP)

(73) Assignee: **ISUZU MOTORS LIMITED**, Tokyo (JP)

(\* ) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 237 days.

(21) Appl. No.: **15/549,137**

(22) PCT Filed: **Feb. 1, 2016**

(86) PCT No.: **PCT/JP2016/052905**  
§ 371 (c)(1),  
(2) Date: **Aug. 4, 2017**

(87) PCT Pub. No.: **WO2016/125738**  
PCT Pub. Date: **Nov. 8, 2016**

(65) **Prior Publication Data**  
US 2018/0023435 A1 Jan. 25, 2018

(30) **Foreign Application Priority Data**  
Feb. 6, 2015 (JP) ..... 2015-022016

(51) **Int. Cl.**  
**F01N 3/08** (2006.01)  
**F01N 3/10** (2006.01)  
**F01N 9/00** (2006.01)  
**F01N 11/00** (2006.01)  
(Continued)

(52) **U.S. Cl.**  
CPC ..... **F01N 3/0814** (2013.01); **F01N 3/08** (2013.01); **F01N 3/0842** (2013.01);  
(Continued)

(58) **Field of Classification Search**  
CPC ..... F01N 3/0814; F01N 3/0842; F01N 3/106  
See application file for complete search history.

(56) **References Cited**  
U.S. PATENT DOCUMENTS

5,388,405 A 2/1995 Fujishita et al.  
5,560,201 A 10/1996 Fujishita et al.  
(Continued)

FOREIGN PATENT DOCUMENTS

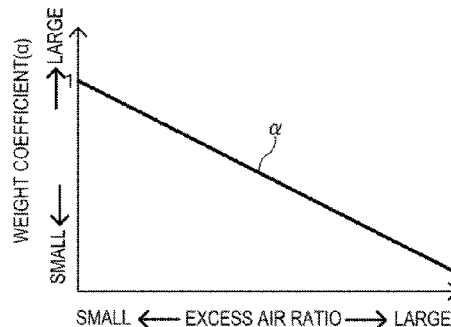
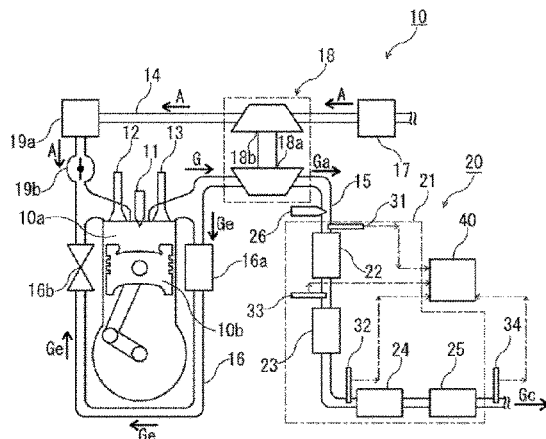
CN 102678240 A 9/2012  
DE 112008003421 T5 10/2010  
(Continued)

OTHER PUBLICATIONS

First Office Action for related CN App No. 201680008748.3 dated Nov. 6, 2018, 10 pages.  
(Continued)

*Primary Examiner* — Patrick D Maines  
(74) *Attorney, Agent, or Firm* — Procopio, Cory, Hargreaves & Savitch LLP

(57) **ABSTRACT**  
An exhaust gas purification system for an internal combustion engine includes an oxidation catalyst device on an upstream side in an exhaust passage of an internal combustion engine and a lean NOx trap catalyst device on a downstream side, a controller which controls the exhaust gas purification system is configured to, when a temperature-rising control of an exhaust gas in a regeneration control is performed to recover a purification ability of the exhaust gas purification system, perform a control that changes a measurement position of a control temperature which is a control amount of a feedback control in the temperature-rising control  
(Continued)



control, according to an excess air ratio or an oxygen concentration of the exhaust gas passing through the exhaust passage.

**5 Claims, 1 Drawing Sheet**

(51) **Int. Cl.**

**F01N 13/00** (2010.01)  
**F02D 41/02** (2006.01)  
**F02D 41/14** (2006.01)

(52) **U.S. Cl.**

CPC ..... **F01N 3/0871** (2013.01); **F01N 3/0885** (2013.01); **F01N 3/103** (2013.01); **F01N 3/106** (2013.01); **F01N 9/00** (2013.01); **F01N 11/00** (2013.01); **F01N 11/002** (2013.01); **F01N 13/009** (2014.06); **F01N 2260/04** (2013.01); **F01N 2560/025** (2013.01); **F01N 2560/06** (2013.01); **F01N 2560/14** (2013.01); **F01N 2900/1402** (2013.01); **F01N 2900/1404** (2013.01); **F01N 2900/1602** (2013.01); **F02D 41/024** (2013.01); **F02D 41/028** (2013.01); **F02D 41/029** (2013.01); **F02D 41/0275** (2013.01); **F02D 41/1441** (2013.01); **F02D 2200/0802** (2013.01); **Y02T 10/24** (2013.01); **Y02T 10/47** (2013.01)

(56)

**References Cited**

U.S. PATENT DOCUMENTS

5,722,236 A 3/1998 Cullen et al.  
 5,937,637 A 8/1999 Fujishita et al.

6,209,316 B1\* 4/2001 Duvinage ..... B01D 53/9495  
 60/274  
 2007/0125072 A1 6/2007 McCarthy, Jr. et al.  
 2007/0125073 A1 6/2007 Reuter  
 2007/0209351 A1 9/2007 Chimner et al.  
 2008/0028749 A1 2/2008 Haga et al.  
 2008/0039975 A1 2/2008 Haga et al.  
 2008/0092524 A1 4/2008 Yokoyama et al.  
 2009/0158714 A1\* 6/2009 Hermansson ..... F02D 41/0002  
 60/286  
 2009/0158715 A1 6/2009 Stroh et al.  
 2010/0132635 A1 6/2010 McCarthy, Jr. et al.  
 2012/0186226 A1 7/2012 Ren et al.  
 2015/0089925 A1\* 4/2015 Kita ..... F01N 3/023  
 60/274  
 2017/0362979 A1\* 12/2017 Nakada ..... B01D 53/9422

FOREIGN PATENT DOCUMENTS

EP 1930572 A2 6/2008  
 JP 2000-320324 A 11/2000  
 JP 2008-038812 A 2/2008  
 JP 2008-101562 A 5/2008  
 JP 2010-526233 A 7/2010  
 JP 2013-174203 A 9/2013  
 JP 2013174203 A \* 9/2013

OTHER PUBLICATIONS

Extended European Search Report for EP App No. 16746569.9 dated May 24, 2018, 6 pgs.  
 International Search Report and Written Opinion for PCT App No. PCT/JP2016/052905 dated Apr. 26, 2016, 8 pgs.

\* cited by examiner

FIG. 1

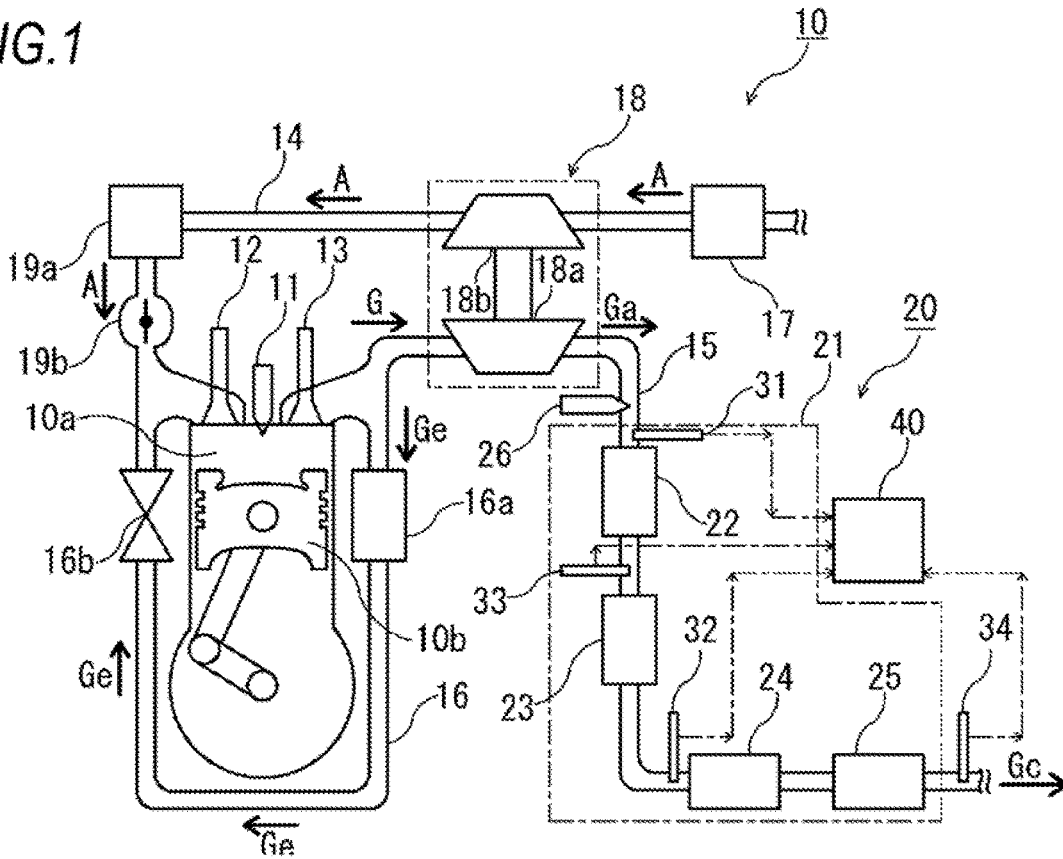
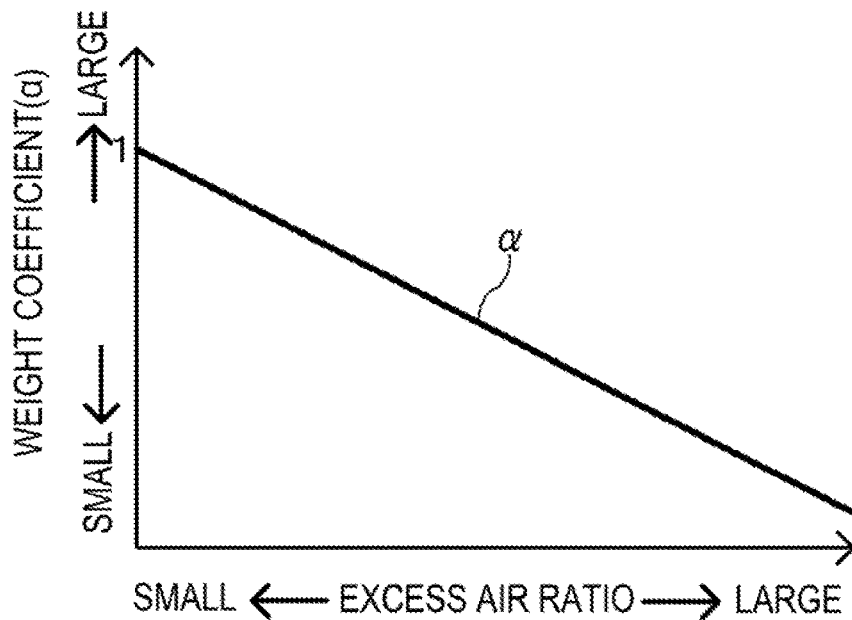


FIG. 2



**EXHAUST GAS PURIFICATION SYSTEM  
FOR INTERNAL COMBUSTION ENGINE,  
INTERNAL COMBUSTION ENGINE, AND  
EXHAUST GAS PURIFICATION METHOD  
FOR INTERNAL COMBUSTION ENGINE**

CROSS-REFERENCE TO RELATED  
APPLICATIONS

This application is a U.S. National Stage entry of PCT Application No. PCT/JP2016/052905, filed on Feb. 1, 2016, which claims priority to Japanese Patent Application No. 2015-022016, filed Feb. 6, 2015, the contents of which are incorporated herein by reference.

TECHNICAL FIELD

The present invention relates to an exhaust gas purification system for an internal combustion engine, an internal combustion engine, and an exhaust gas purification method for the internal combustion engine which can avoid a lack of temperature increment of each catalyst device, an overshooting at the time of increasing a temperature, heat degradation of a catalyst, erosion of the catalyst so as to perform the regeneration processing reliably when each catalyst device including an exhaust gas purification device of the internal combustion engine performs regeneration processing.

BACKGROUND ART

Generally, an exhaust gas purification system is used which includes an exhaust gas purification device which has catalyst devices such as an oxidation catalyst, a device (DOC), a particulate collection device (CSF, SCRF, and the like), a selective reduction catalyst (SCR) device, and a lean NOx trap catalyst device (LNT) to purify purification object components such as hydrocarbon (HC), carbon monoxide (CO), particulate substance (PM), and nitrogen oxide (NOx) included in exhaust gases of the internal combustion engine such as a diesel engine.

In the exhaust gas purification system, a temperature-rising control of the exhaust gas is regularly performed for the release and the reduction (NOx regeneration) of NOx stored in the lean NOx trap catalyst device, the combustion-removal (PM regeneration) of the particulate substance collected in the particulate collection device, the removal (sulfur purge) of the sulfur component accumulated in various catalyst devices such as an oxidation catalyst device or the lean NOx trap catalyst device, and the like.

In the related art, at the time of the temperature-rising control of the exhaust gas, a detection temperature of an exhaust gas temperature sensor provided in the vicinity of any one catalyst device in the catalyst devices, and the estimation temperature of any one catalyst device obtained by following methods are set as a control temperature which is a control value of a feedback control with respect to a target temperature of the exhaust gas in the temperature-rising control. In the case of some catalyst devices, normally, in view of responsiveness, the temperature relating to the catalyst device in which the heat generation amount by the combustion of unburned hydrocarbon (HC) supplied to increase a temperature is largest is used as the control temperature steadily.

With respect thereto, as described, for example, in Japanese Unexamined Patent Application Publication No. 2013-174203, an exhaust gas purification device is proposed which includes a selective reduction catalyst, a particulate

filter which is arranged on the exhaust gas upstream side from the selective reduction catalyst and in which an oxidation catalyst layer is formed to further collect the particulate in the exhaust gas, a liquid injection nozzle through which the hydrocarbon based liquid can be injected toward the particulate filter, and a liquid feeding unit which supplies the liquid to the liquid injection nozzle. In the exhaust gas purification device which purifies the exhaust gas of the engine, the temperature of the exhaust gas relating to the particulate filter is detected using a temperature sensor, and the liquid feeding unit is controlled on the basis of a detection output of the temperature sensor.

However, in a zone-coat and the like in which a plurality of catalyst devices or the catalyst layers are coated for each part in separate colors, a place (catalyst device) in which the heat generation amount is largest in the exhaust passage may be different according to an operating condition of the engine. For example, in the case of a system which is configured by the oxidation catalyst device, the lean NOx trap catalyst device, and the particulate collection device, when an excess air ratio  $\lambda$  in the exhaust gas is high, and the concentration of the oxygen is high, the most hydrocarbon is combusted by the oxidation catalyst device on the upstream side to generate heat. For this reason, in the lean NOx trap catalyst device or the particulate collection device on the downstream side, the temperature of each catalyst device is increased not by the generation of the combustion heat of the hydrocarbon, but by the heat transmission of the exhaust gas of which the temperature is increased by the oxidation catalyst device.

On the other hand, in a case where the excess air ratio of the exhaust gas is low and the concentration of the oxygen is low such as the sulfur purge (S purge: sulfur purge) control or rich combustion of NOx regeneration, the combustion of the hydrocarbon is caused using the oxygen adsorbed in the lean NOx trap catalyst device or the oxygen generated by NOx reduction, and thus the generation amount of the combustion heat of the hydrocarbon in the lean NOx trap catalyst device is larger than that in the oxidation catalyst device.

Similarly, in the case of the exhaust gas purification system configured by a plurality of catalyst devices in combination, a place in which the generation amount of the fuel heat is largest is changed according to the operating condition of the engine. Therefore, as in the related art, when the control temperature at the time of the temperature-rising control is fixed to a temperature relating to a specified catalyst device such as the catalyst device in which the heat generation amount due to the combustion of the hydrocarbon is largest, an insufficient temperature increment, an overshooting at the time of increasing a temperature, erosion, and the like may be occur according to the operating condition of the engine in another catalyst device other than the specified catalyst device.

CITATION LIST

Patent Literature

[Patent Literature 1]: Japanese Unexamined Patent Application Publication No. 2013-174203

SUMMARY OF THE INVENTION

Technical Problem

The present inventor found, through tests, such a relation between the change of the catalyst device in which a heat

generation amount is largest in an exhaust passage and an increased degree of temperature is high and the oxygen concentration of the exhaust gas when the operating condition of the engine is changed. For example, a phenomenon is found in which at the time of the PM regeneration processing or the high load of the engine in which the excess air ratio in the exhaust gas is high and the oxygen concentration is high, the heat generation amount of the oxidation catalyst device is large, and on the other hand, at the time of the sulfur purge control or the low load of the engine in which the excess air ratio in the exhaust gas is low, and the oxygen concentration is low, the heat generation amount of the lean NOx trap catalyst device is large.

From this point, it is acknowledged that in order to prevent that the insufficient temperature increment, the overshooting at the time of increasing a temperature, the erosion, and the like occur at the time of the temperature-rising control in the catalyst device, when the temperature-rising control is performed more optimally in response to the operating condition of the engine, preferably, a position of the control temperature in the feedback control, in other words, the catalyst device relating to the control temperature to be the target temperature is selected and changed in consideration of the oxygen concentration of the exhaust gas. That is, preferably, the catalyst device relating to the control temperature, in other words, a position where the control temperature is measured is changed on the basis of the oxygen concentration of the exhaust gas.

More specifically, following knowledge is obtained. When the excess air ratio or the oxygen concentration is high, the control temperature relating to the temperature of the former oxidation catalyst device may be adopted, and when the excess air ratio or the oxygen concentration is low, the control temperature relating to the temperature of the lean NOx trap catalyst device may be adopted. In addition, in order to avoid a drastic change of the control in association with the switch of the control temperature, preferably, the measurement temperature relating to the temperature of the former oxidation catalyst device and the measurement temperature relating to the temperature of the lean NOx trap catalyst device are weighted (target temperature ratio), the weight is gradually changed according to the excess air ratio or the oxygen concentration, the control temperature is calculated on the basis of a weighted average thereof, and the temperature-rising control is performed at the feedback control such that the control temperature becomes the target temperature.

The present invention has been made in consideration of the above situation, and an object thereof is to provide an exhaust gas purification system for an internal combustion engine, an internal combustion engine, and an exhaust gas purification method for the internal combustion engine in which during the temperature-rising control of the exhaust gas for recovering an exhaust gas purification ability of the catalyst device, a lack of temperature increment of catalyst devices, an overshooting at the time of increasing a temperature, heat degradation of a catalyst, and erosion of the catalyst can be avoided using the exhaust gas purification system for the internal combustion engine which includes an oxidation catalyst device on an upstream side and a lean NOx trap catalyst device on a downstream side in an exhaust passage of the internal combustion engine, thereby performing a regeneration processing reliably.

#### Solution to Problem

In an exhaust gas purification system for an internal combustion engine of the present invention to achieve the

above-described object, an exhaust gas purification system for an internal combustion engine includes an oxidation catalyst device on an upstream side in an exhaust passage of an internal combustion engine and a lean NOx trap catalyst device on a downstream side, and a controller which controls the exhaust gas purification system is configured to, when a temperature-rising control of an exhaust gas in a regeneration control is performed to recover a purification ability of the exhaust gas purification system, perform a control that changes a measurement position of a control temperature which is a control amount of a feedback control in the temperature-rising control, according to an excess air ratio or an oxygen concentration of the exhaust gas passing through the exhaust passage.

With this configuration, at the time of the temperature-rising control of the exhaust gas for performing regeneration processing on the catalyst devices included in the exhaust gas purification device, the measurement position of the control temperature which is the control amount of the feedback control in the temperature-rising control, that is, the control temperature to be a target temperature is changed and set in consideration of the oxygen concentration of the exhaust gas, and more specifically, the control temperature is set to the temperature relating to the catalyst device in which the heat generation amount is largest at that time in the exhaust gas purification system and the temperature is increased most, whereby the temperature-rising control of the exhaust gas can be optimized. Therefore, the lack of temperature increment of each of the catalyst devices, the overshooting at the time of increasing a temperature, the heat degradation of the catalyst, and the erosion of the catalyst can be avoided so that the regeneration processing can be performed reliably.

Further, the above-described exhaust gas purification system for the internal combustion engine further includes: a first temperature sensor which measures a first temperature relating to a temperature of the oxidation catalyst device; and a second temperature sensor which measures a second temperature relating to a temperature of the lean NOx trap catalyst device, and the controller is configured to, when the temperature-rising control of the exhaust gas in the regeneration control is performed to recover the purification ability of the exhaust gas purification system, perform a control such that the control temperature is set as the first temperature when the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage is higher than an upper limit threshold set in advance, and the control temperature is set as the second temperature when the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage is lower than a lower limit threshold set in advance, thereby obtaining following effect.

That is, when the heat generation amount of the oxidation catalyst device is larger than that of the lean NOx trap catalyst device, the excess air ratio and the oxygen concentration of the exhaust gas is higher than the upper limit threshold set in advance. Thus, the first temperature relating to the oxidation catalyst device is set as the control temperature, so that the temperature-rising control can be performed at the temperature of the oxidation catalyst device. In addition, when the heat generation amount of the lean NOx trap catalyst device is larger than that of the oxidation catalyst device, the excess air ratio and the oxygen concentration of the exhaust gas is lower than the lower limit threshold set in advance. Thus, the second temperature relating to the lean NOx trap catalyst device is set as the control temperature, so that the temperature-rising control

can be performed at the temperature of the lean NO<sub>x</sub> trap catalyst device. Therefore, the temperature-rising control of the exhaust gas can be optimized with the relatively simple control.

In the above-described exhaust gas purification system for the internal combustion engine, when the temperature-rising control of the exhaust gas in the regeneration control is performed to recover the purification ability of the exhaust gas purification system, when the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage is equal to or less than the upper limit threshold and equal to or more than the lower limit threshold, the controller performs a control to set the weight coefficient to be changed according to the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage, and to set the control temperature to a weighted average value of the first temperature and the second temperature using the weight coefficient. Therefore, the temperature-rising control can be performed while a drastic change due to the switch of the control temperature with respect to the change of the excess air ratio or the oxygen concentration is avoided.

The internal combustion engine of the present invention to achieve the above-described object includes the above-described exhaust gas purification system for the internal combustion engine, so as to make the same operational effect as that of the above-described exhaust gas purification system for the internal combustion engine.

In an exhaust gas purification method for the internal combustion engine of the present invention to achieve the above-described object, an exhaust gas purification method for an internal combustion engine having an exhaust gas purification system for the internal combustion engine, which includes an oxidation catalyst device on an upstream side and a lean NO<sub>x</sub> trap catalyst device on a downstream side in an exhaust passage of the internal combustion engine, the method includes: changing, when a temperature-rising control of an exhaust gas in a regeneration control is performed to recover a purification ability of the exhaust gas purification system, a measurement position of a control temperature which is a control amount of a feedback control in the temperature-rising control, according to an excess air ratio or an oxygen concentration of the exhaust gas passing through the exhaust passage, thereby it is possible to make the same operational effect as that of above-described the exhaust gas purification system for the internal combustion engine.

#### Advantageous Effects of the Invention

According to the exhaust gas purification system for the internal combustion engine, the internal combustion engine, and the exhaust gas purification method for the internal combustion engine in the present invention, at time of the temperature-rising control of the exhaust gas for performing the regeneration processing on the catalyst devices included in the exhaust gas purification device, the measurement position of the control temperature which is the control amount of the feedback control in the temperature-rising control, that is, the control temperature to be a target temperature is changed and set in consideration of the oxygen concentration of the exhaust gas, and more specifically, the control temperature is set to the temperature relating to the catalyst device in which the heat generation amount is largest at that time in the exhaust gas purification system and the temperature is increased most, thereby optimizing the temperature-rising control of the exhaust gas.

Therefore, it is possible to avoid a lack of temperature increment of each of the catalyst devices, an overshooting at the time of increasing a temperature, heat degradation of the catalyst, and erosion of the catalyst, and it is possible to perform the regeneration processing reliably.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a view schematically illustrating a configuration of an internal combustion engine which includes an exhaust gas purification system for an internal combustion engine of an embodiment according to the present invention.

FIG. 2 is a view schematically illustrating a relation between a weight coefficient which is a weight ratio of a first temperature to a second temperature and an excess air ratio of the exhaust gas.

#### DESCRIPTION OF EMBODIMENTS

Hereinafter, an exhaust gas purification system for an internal combustion engine, an internal combustion engine, and an exhaust gas purification method for the internal combustion engine in the embodiment according to the present invention will be described with reference to the drawings. Incidentally, the internal combustion engine of the embodiment according to the present invention includes an exhaust gas purification system for an internal combustion engine of the embodiment according to the present invention, so as to make the same operational effect as an operational effect made by the exhaust gas purification system for the internal combustion engine (to be described later).

First, an internal combustion engine (hereinafter, engine) 10 and an exhaust gas purification system 20 of the internal combustion engine of the embodiment according to the present invention will be described with reference to FIG. 1. The engine 10 are provided with a fuel injection device 11, an intake valve 12, and an exhaust valve 13 facing a cylinder 10a, and further with an intake passage 14 communicating with the intake valve 12, an exhaust passage 15 communicating with the exhaust valve 13, and an EGR passage 16.

The intake passage 14 is provided with an air cleaner 17, a compressor 18b of a turbocharger (turbo type supercharger) 18, an intercooler 19a, and an intake throttle valve 19b in order from the upstream side. Further, the exhaust passage 15 is provided with a turbine 18a of the turbocharger 18 and an exhaust gas purification device 21 in order from the upstream side. In addition, the EGR passage 16 is provided by connecting the intake passage 14 on the downstream from the compressor 18b with the exhaust passage 15 on the upstream from the turbine 18a. The EGR passage 16 is provided with an EGR cooler 16a, an EGR valve 16b in order from the upstream side.

As needed, new air A guided from the atmosphere is fed to the cylinder (cylinder) 10a through the intake valve 12 in association with the exhaust gas (EGR gas) Ge flowing in the intake passage 14 from the EGR passage 16. In addition, the exhaust gas G generated in the cylinder 10a flows out to the exhaust passage 15 through the exhaust valve 13. Some of the exhaust gas G flows to the EGR passage 16 as the EGR gas Ge. The remaining exhaust gas Ga (=G-Ge) flows in the exhaust gas purification device 21 through the turbine 18a, and after being purified, is released as the purified exhaust gas Gc into the atmosphere through a muffler (not illustrated) and a tail pipe (not illustrated).

In the configuration of FIG. 1, the exhaust gas purification device 21 of the exhaust gas purification system 20 includes

catalyst devices such as an oxidation catalyst (DOC) device **22**, a particulate collection device (CSF) **23**, a lean NOx trap catalyst device (LNT) **24**, and a subsequent-stage oxidation catalyst (DOC) device **25**. Incidentally, the catalyst devices may be provided in the exhaust gas purification device **20** in the reverse order to the arrangement order of the particulate collection device **23** and the lean NOx trap catalyst device **24**, that is, in order of the oxidation catalyst device **22**, the lean NOx trap catalyst device **24**, the particulate collection device **23**, and the subsequent-stage oxidation catalyst device **25**.

The fuel injection device **26** which injects the unburned fuel into the exhaust passage **15** is arranged in the exhaust passage **15** on the upstream side of the oxidation catalyst device **22**. The unburned fuel is injected into the exhaust passage **15** at the time of the temperature-rising control of the exhaust gas such as a NOx regeneration control on the lean NOx trap catalyst device **24**, a sulfur purge control on the oxidation catalyst device **22** and the lean NOx trap catalyst device **24**, and a PM regeneration control on the particulate collection device **23**. By the injection, the hydrocarbon which is an unburned fuel is oxidized by the oxidation catalyst device **22** and the like, and by oxidation heat, the temperature of the exhaust gas Ga is increased. When the temperature of the exhaust gas Ga is increased or the temperature of the hydrocarbon is increased by the combustion in the catalyst devices **22**, **23**, and **24**, the temperature of the lean NOx trap catalyst device **24** is increased to a temperature range of the release and the reduction of the occlusion NOx, the temperature of the particulate collection device **23** is increased such a temperature range that can realize the PM combustion, or the temperatures of the oxidation catalyst device **22** and the lean NOx trap catalyst device **24** are increased to such a temperature range that can realize desulfurization. In this manner, the exhaust gas purification ability of the catalyst devices **22**, **23**, and **24** are recovered.

The first temperature sensor **31** which detects the temperature TDOC of the exhaust gas Ga flowing in the oxidation catalyst device **22** is arranged in the exhaust passage **15** on the upstream side (inlet side) of the oxidation catalyst device **22**. In addition, the second temperature sensor **32** which detects a temperature TLNT of the exhaust gas Ga flowing in the lean NOx trap catalyst device **24** is arranged in the exhaust passage **15** on the upstream side of the lean NOx trap catalyst device **24**. In addition, the third temperature sensor **33** which detects the temperature TCSF of the exhaust gas Ga flowing out from the oxidation catalyst device **22** to flow in the particulate collection device **23** is arranged in the exhaust passage **15** between the oxidation catalyst device **22** and the particulate collection device **23**.

A  $\lambda$ -sensor **34** which measures the excess air ratio  $\lambda$  of the exhaust gas Ga or an oxygen concentration Co or an oxygen concentration sensor (not illustrated) is arranged on the downstream side of the exhaust gas purification device **20**. The  $\lambda$ -sensor or the oxygen concentration sensor may be arranged on the upstream side of the exhaust gas purification device **20**, or may be arranged in an exhaust manifold.

Herein, the temperature TDOC detected by the first temperature sensor **31** is set as a first temperature T1 relating to the oxidation catalyst device **22**. The temperature TLNT detected by the second temperature sensor **32** is set as a second temperature T2 relating to the lean NOx trap catalyst device **24**. The temperature TCSF detected by the third temperature sensor **33** is set as a third temperature T3 relating to the particulate collection device **23**.

Incidentally, the average value of the temperatures detected by the temperature sensors before and after the oxidation catalyst device **22** may be set as the first temperature T1. The average value of the temperatures detected by the temperature sensors before and after the lean NOx trap catalyst device **24** may be set as the second temperature T2. In addition, the average value of the temperatures detected by the temperature sensors before and after the particulate collection device **23** may be set as the third temperature. Further, instead of the exhaust gas temperatures on the upstream side of the catalyst devices **22**, **23**, and **24**, the exhaust gas temperatures on the respective downstream sides may be used.

A controller **40** is provided which controls the exhaust gas purification system **20** of the internal combustion engine of the present invention. Normally, the controller **40** is configured to be embedded in an engine control unit (ECU) which controls the whole operating condition of the engine **10**, but may be configured separately.

In the exhaust gas purification system **20** of the internal combustion engine of the embodiment according to the present invention, when the temperature-rising control of the exhaust gas Ga in the regeneration control is performed for recovering the purification ability of the exhaust gas purification system **20**, the controller **40** which controls the exhaust gas purification system **20** performs a control to change the measurement position of the control temperature Tc which is the control amount of the feedback control in the temperature-rising control, according to the excess air ratio  $\lambda$  or the oxygen concentration Co of the exhaust gas G passing through the exhaust passage **15**.

With the configuration, at the time of the temperature-rising control of the exhaust gas Ga for the regeneration processing to recover the purification ability of the catalyst devices **22** to **25** included in the exhaust gas purification device **20**, the amount of the unburned fuel (hydrocarbon) injected by the fuel injection device **26** is adjusted such that the control temperature Tc becomes a target temperature Tm set according to each regeneration processing. The measurement position of the control temperature Tc is changed according to the excess air ratio  $\lambda$  or the oxygen concentration Co of the exhaust gas Ga. More specifically, the measurement position is changed to the measurement temperature which reflects best the temperature (any one of T1, T2, and T3) of the catalyst device (any one of **22**, **23**, and **24**) in which the heat generation amount is largest at that time in the exhaust passage **15** and the temperature is increased most.

That is, when the temperature-rising control of the exhaust gas Ga in the regeneration control is performed for recovering the purification ability of the exhaust gas purification system **20**, the controller **40** performs a control such that the control temperature Tc is set as the first temperature T1 when the excess air ratio  $\lambda$  or the oxygen concentration Co of the exhaust gas Ga passing through the exhaust passage **15** is higher than an upper limit threshold A1 set in advance, and the control temperature Tc is set as the second temperature T2 when the excess air ratio  $\lambda$  or the oxygen concentration Co is lower than a lower limit threshold A2 set in advance. Incidentally, the upper limit threshold A1 and the lower limit threshold A2 are set in advance by the experiments and the like, and are stored in the controller **40**. In addition, when the control is simplified, the upper limit threshold A1 and the lower limit threshold A2 may be set the same as each other, and in this case, the first temperature T1 and the second temperature T2 preferably become the substantially same value.

In this manner, when the heat generation amount of the oxidation catalyst device **22** is larger than that of the lean NOx trap catalyst device **24**, the excess air ratio  $\lambda$  and the oxygen concentration  $Co$  of the exhaust gas  $Ga$  is larger than the upper limit threshold **A1**. Thus, the first temperature **T1** relating to the oxidation catalyst device **22** is set as the control temperature  $Tc$ , and the temperature-rising control can be performed at the first temperature **T1** of the oxidation catalyst device **22**. In addition, when the heat generation amount of the lean NOx trap catalyst device **24** is larger than that of the oxidation catalyst device **22**, the excess air ratio  $\lambda$  and the oxygen concentration  $Co$  of the exhaust gas  $Ga$  is lower than the lower limit threshold **A2** set in advance. Thus, the second temperature **T2** relating to the lean NOx trap catalyst device **24** is set as the control temperature  $Tc$ , and the temperature-rising control can be performed at the second temperature **T2** of the lean NOx trap catalyst device **24**. Therefore, the temperature-rising control of the exhaust gas  $Ga$  can be optimized with the relatively simple control.

When the temperature-rising control of the exhaust gas  $Ga$  in the regeneration control is performed to recover the purification ability of the exhaust gas purification system **20**, when the excess air ratio  $\lambda$  or the oxygen concentration  $Co$  of the exhaust gas  $Ga$  passing through the exhaust passage **15** is equal to or less than the upper limit threshold **A1** and equal to or more than the lower limit threshold **A2**, the controller **40** performs a control to set a weight coefficient  $\alpha$  to be changed according to the excess air ratio  $\lambda$  or the oxygen concentration  $Co$ , and to set the control temperature  $Tc$  to a weighted average value **T12** of the first temperature **T1** and the second temperature **T2** using the weight coefficient  $\alpha$ . In this manner, the temperature-rising control can be performed while a drastic change due to the switch of the control temperature  $Tc$  with respect to the change of the excess air ratio  $\lambda$  or the oxygen concentration  $Co$  is avoided.

The weight coefficient  $\alpha$  can be determined such that, for example,  $T12 = T1 \times \alpha + T2 \times (1 - \alpha)$ , or  $T12 = (T1 \times \alpha + T2) / (1 + \alpha)$ . The weight coefficient  $\alpha$  is set in advance by the experiments and the like with respect to the excess air ratio  $\lambda$ , and is stored in the controller **40**. In FIG. 2, the weight coefficient  $\alpha$  is set to be increased as the excess air ratio  $\lambda$  is smaller, and to be decreased as the excess air ratio  $\lambda$  is larger. Incidentally, in FIG. 2, a correlation between the excess air ratio  $\lambda$  and the weight coefficient  $\alpha$  is a linear relation falling downward to the right. However, the linear relation of FIG. 2 is illustrated as an example, and a curvilinear relation convex to a lower left side or a curvilinear relation convex to an upper right side may be adopted.

Incidentally, on the basis of the oxygen concentration  $\lambda$  of the exhaust gas  $Ga$ , in a case where the number of the temperatures of the catalyst device as a maximum heat generation amount is three or more, for example, in the case of TDOC, TLNT, and TCSF, the number of the weight coefficient is increased, and a temperature as the control temperature  $Tc$  is obtained as a weighted average. For example, the weight coefficients  $\alpha$  and  $\beta$  are set in advance with respect to the oxygen concentration  $\lambda$  of the exhaust gas  $Ga$ , and the control temperature  $Tc$  is set such that  $Tc = TDOC \times \alpha + TLNT \times \beta + TCSF \times (1 - \alpha - \beta)$ .

Next, the exhaust gas purification method for the internal combustion engine of the embodiment according to the present invention will be described. This method is an exhaust gas purification method for the internal combustion engine in the above-described exhaust gas purification system **20** of the internal combustion engine. In the method, when the temperature-rising control of the exhaust gas  $Ga$  in the regeneration control is performed to recover the purifi-

cation ability of the exhaust gas purification system **20**, the measurement position of the control temperature  $Tc$  which is the control amount of the feedback control in the temperature-rising control is changed according to the excess air ratio  $\lambda$  or the oxygen concentration  $Co$  of the exhaust gas  $Ga$  passing through the exhaust passage **15**.

According to the exhaust gas purification system **20** of the internal combustion engine, the internal combustion engine **10**, and the exhaust gas purification method for the internal combustion engine which are described above, at time of the temperature-rising control of the exhaust gas  $Ga$  for performing the regeneration processing on the catalyst devices **22**, **23**, and **24** included in the exhaust gas purification device **21**, the measurement position of the control temperature  $Tc$  which is the control amount of the feedback control in the temperature-rising control, that is, the control temperature  $Tc$  to be the target temperature  $Tm$  is changed and set in consideration of the excess air ratio  $\lambda$  or the oxygen concentration  $Co$  of the exhaust gas  $Ga$ , and more specifically, the control temperature  $Tc$  is set to the temperatures **T1**, **T2**, and **T3** relating to the catalyst devices **22**, **23**, and **24** in which the heat generation amount is largest at that time in the exhaust gas purification system **20** and the temperature is increased most, thereby optimizing the temperature-rising control of the exhaust gas  $Ga$ . Therefore, it is possible to avoid a lack of temperature increment of each of the catalyst devices **22**, **23**, and **24**, an overshooting at the time of increasing a temperature, heat degradation of the catalyst, and erosion of the catalyst, and it is possible to perform the regeneration processing reliably.

#### REFERENCE SIGNS LIST

**10** engine (internal combustion engine)  
**11** fuel injection device  
**15** exhaust passage  
**20** exhaust gas purification system  
**21** exhaust gas purification device  
**22** oxidation catalyst (DOC) device  
**23** particulate collection device  
**24** selective reduction catalyst (SCR) device  
**25** subsequent-stage oxidation catalyst (DOC) device  
**26** fuel injection device  
**31** first temperature sensor  
**32** second temperature sensor  
**33** third temperature sensor  
**34**  $\lambda$ -sensor  
**40** controller  
A new air  
G generated exhaust gas  
Ga exhaust gas passing through exhaust gas purification device  
Gc purified exhaust gas  
Ge EGR gas

The invention claimed is:

1. An exhaust gas purification system for an internal combustion engine, which includes an oxidation catalyst device on an upstream side in an exhaust passage of an internal combustion engine and a lean NOx trap catalyst device on a downstream side, comprising:

a controller which controls the exhaust gas purification system configured to, when a temperature-rising control of an exhaust gas in a regeneration control is performed to recover a purification ability of the exhaust gas purification system, perform a control that changes a measurement position of a control temperature which is a control amount of a feedback control in

11

the temperature-rising control, according to an excess air ratio or an oxygen concentration of the exhaust gas passing through the exhaust passage.

2. The exhaust gas purification system for the internal combustion engine according to claim 1, the exhaust gas purification system comprising:

- a first temperature sensor which measures a first temperature relating to a temperature of the oxidation catalyst device; and
- a second temperature sensor which measures a second temperature relating to a temperature of the lean NOx trap catalyst device,

wherein the controller is configured to, when the temperature-rising control of the exhaust gas in the regeneration control is performed to recover the purification ability of the exhaust gas purification system, perform a control such that the control temperature is set as the first temperature when the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage is higher than an upper limit threshold set in advance, and the control temperature is set as the second temperature when the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage is lower than a lower limit threshold set in advance.

3. The exhaust gas purification system for the internal combustion engine according to claim 2, wherein the controller is configured to, when the temperature-rising control of the exhaust gas in the regeneration control is performed to recover the purification ability

12

of the exhaust gas purification system, perform a control such that a weight coefficient is set to be changed according to the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage, and the control temperature is set to a weighted average value of the first temperature and the second temperature obtained using the weight coefficient, when the excess air ratio or the oxygen concentration of the exhaust gas passing through the exhaust passage is equal to or less than the upper limit threshold and equal to or more than the lower limit threshold.

4. An internal combustion engine comprising:  
the exhaust gas purification system for the internal combustion engine according to claim 1.

5. An exhaust gas purification method for an internal combustion engine having an exhaust gas purification system for the internal combustion engine, which includes an oxidation catalyst device on an upstream side and a lean NOx trap catalyst device on a downstream side in an exhaust passage of the internal combustion engine, the method comprising:  
changing, when a temperature-rising control of an exhaust gas in a regeneration control is performed to recover a purification ability of the exhaust gas purification system, a measurement position of a control temperature which is a control amount of a feedback control in the temperature-rising control, according to an excess air ratio or an oxygen concentration of the exhaust gas passing through the exhaust passage.

\* \* \* \* \*