

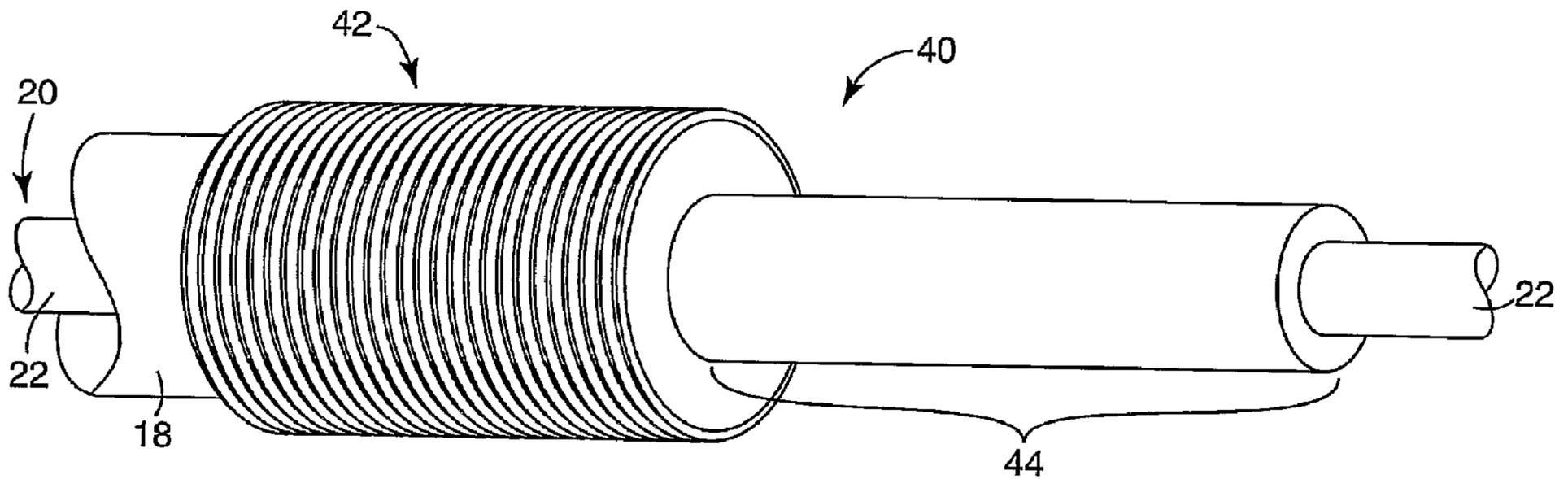


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(57) **Abrégé/Abstract:**

An elastomeric composition that includes a fluorelastomer and an epichlorohydrin. The elastomeric composition can be formed into cold-shrink articles that are resistant to tearing at elevated temperatures.

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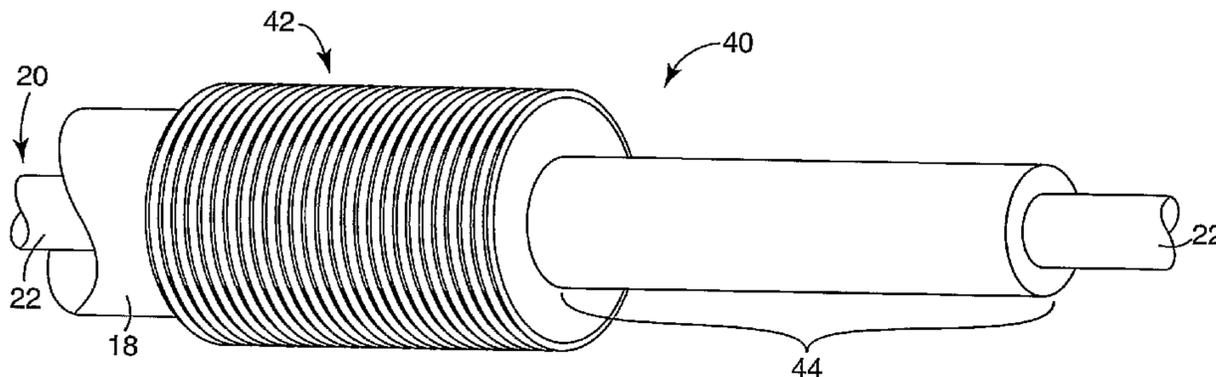
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(54) Title: COLD-SHRINK ARTICLE AND METHOD OF MAKING COLD-SHRINK ARTICLE



(57) Abstract: An elastomeric composition that includes a fluorelastomer and an epichlorohydrin. The elastomeric composition can be formed into cold-shrink articles that are resistant to tearing at elevated temperatures.

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COLD-SHRINK ARTICLE AND METHOD OF MAKING COLD-SHRINK ARTICLE

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FIELD

The present invention relates generally to cold-shrink articles for use in various applications. In particular, the present invention relates to cold-shrink articles formed from a composition including a fluorelastomer and an epichlorohydrin.

BACKGROUND

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Cold-shrink articles are used in a variety of different applications such as, for example, splicing together lengths of wire or cable and protecting, sealing, and/or insulating substrates from adverse environmental conditions. Examples of industries that use cold-shrink articles include the automobile, aerospace, power, telecommunication, chemical, and defense industries.

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A conventional cold-shrink article typically comprises a tubular member or other molded product that is capable of being expanded and mounted in an expanded state on a removable support core. The support core is typically hollow to allow the support core to be fed over a substrate. The support core is typically designed to collapse on demand and allow shrinkage of the cold-shrink article into contact with a substrate positioned inside
20 the support core. For a given application, a cold-shrink article is typically selected that, when released from the core in the absence of a substrate, will shrink from the expanded state on the core to a relaxed state having an inner diameter smaller than the outer diameter of the intended substrate. When deployed on the substrate, such sizing prevents the cold-shrink article from fully relaxing from the expanded state, which ensures a snug
25 engagement between the cold-shrink article and the substrate. Once the cold-shrink article is conveyed onto the substrate, the cold-shrink article remains in a partially expanded state over the life of its engagement with the substrate.

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It is known to form cold-shrink articles from elastomeric compositions that include an elastomer to facilitate expansion and contraction of the article without breakage or cracking. Examples of known elastomers employed in cold-shrink articles include EPDM rubber or silicone rubber.

BRIEF SUMMARY OF THE INVENTION

Although known cold-shrink articles generally perform satisfactorily at low temperatures such as, for example, room temperature, it is desirable to increase the

stability of cold-shrink articles at the elevated temperatures that may be in certain settings. In addition, it is desirable to increase the resistance of cold-shrink articles to degradation when exposed to acidic substances, caustic substances, or hydrocarbon fluids.

5 A need exists for cold-shrink articles that may stably be used in elevated temperature environments and/or environments where exposure to acidic chemicals, caustic chemicals, or hydrocarbon fluids may occur.

The present invention includes various elastomeric compositions that resist tearing at elevated temperatures. The elastomeric compositions include a fluoroelastomer and an epichlorohydrin. In some embodiments, the elastomeric compositions include a pigment,
10 an energy-beam absorbent, and/or a filler material.

The present invention further includes cold-shrink articles including an elastomeric member formed from the elastomeric compositions. In one embodiment, the elastomeric member does not tear while being held for seven days at a temperature of 150°C in a 200% radially expanded state. In one embodiment, the elastomeric member includes an energy-
15 beam induced identifier on an external surface of the elastomeric member.

The present invention further includes methods for forming cold-shrink articles from the elastomeric compositions. In one embodiment, the cold-shrink articles are cured in an oxygen-free and/or water-free atmosphere. In another embodiment, the cold-shrink articles are irradiated.

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BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a perspective view of a cold-shrink article of the present invention in a relaxed state, prior to expansion.

FIG. 2 is a perspective view of the cold-shrink article of FIG. 1 in an expanded state on a core.

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FIG. 3 is a perspective view of the cold-shrink article of FIG. 1 in an expanded state on the core of FIG. 2, with an associated substrate.

FIG. 4 is a perspective view of the cold-shrink article of FIG. 1 partially located on the core of FIG. 2 and partially deployed on the substrate of FIG. 3.

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FIG. 5 is a perspective view of the cold-shrink article of FIG. 1 including indicia and fully deployed on the substrate of FIG. 3.

FIG. 6 is a perspective view of a branched cold-shrink article of the present invention in a relaxed state prior to expansion.

FIG. 7 is a perspective view of the branched cold-shrink article of FIG. 6 in an expanded state on a plurality of cores.

FIG. 8 is a perspective view of a corrugated cold-shrink article of the present invention.

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DETAILED DESCRIPTION

The present invention includes elastomeric compositions that incorporate at least a fluorelastomer and an epichlorohydrin and includes cold-shrink articles formed from the elastomeric compositions. The term "epichloroydrin", as used herein, refers to any substance containing epichloroydrin, including any polymer containing epichlorohydrin monomers such as, for example, homopolymers, copolymer, terpolymers, and tetrapolymers that contain epichlorohydrin. The term "cold shrink", as used herein, is defined as the capability of an article (or a portion of an article) to shrink from an expanded state toward a relaxed, or a partially expanded, state at room temperature conditions (e.g., about 20°C - 25°C) and in the absence of heating. In some embodiments, cold-shrink articles of the present invention include an elastomeric member formed from an elastomeric composition that exhibits an improved chemical resistance and improved tear properties in expanded states at elevated temperatures.

Elastomers are included in the elastomeric compositions of cold-shrink articles to allow the cold-shrink articles to expand from a relaxed state to an expanded state, while also allowing the articles to cold-shrink back toward the relaxed state. A mixture of fluoroelastomer and epichlorohydrin is included in the elastomeric compositions of the present invention. Some embodiments of cold-shrink articles of the present invention may be exposed, in an expanded state, to temperatures of at least about 150°C for an extended period of time without exhibiting, upon unaided visual inspection by a human eye, any splitting, tearing, or breakage.

Unless otherwise stated, all concentrations herein are expressed in parts by weight per hundred parts by weight rubber (phr), with the rubber defined to be the total weight of both fluoroelastomer and epichlorohydrin. Thus, as used herein, the phr of a particular component represents the parts by weight of the component relative to 100 total parts by weight of fluoroelastomer and epichlorohydrin.

A wide range of concentrations of epichlorohydrin and fluoroelastomer may be included in the elastomeric compositions of the present invention. For example, in some

embodiments, the concentration of fluoroelastomer in the elastomeric compositions of the present invention may range from about 10 parts or greater by weight of fluoroelastomer to about 60 parts or less by weight of fluoroelastomer, per 100 total parts by weight of fluoroelastomer and epichlorohydrin, and the concentration of epichlorohydrin in the elastomeric compositions may range from about 40 parts or greater by weight of epichlorohydrin to about 90 parts or less by weight of epichlorohydrin, per 100 total parts by weight of fluoroelastomer and epichlorohydrin. As used herein, in the context of polymers containing epichlorohydrin (e.g., homopolymers, copolymers, terpolymers, and tetrapolymers that contain epichlorohydrin), parts by weight of epichlorohydrin refers to the total weight of the polymer containing the epichlorohydrin.

Some examples of suitable fluoroelastomers for use in the elastomeric compositions of the present invention include fluorinated elastomeric copolymers (i.e., polymers derived from two or more different monomers), fluorinated elastomeric terpolymers (i.e., polymers derived from three different monomers) and fluorinated elastomeric polymers including more than three different monomers. Some examples of suitable fluorinated elastomeric copolymers include copolymers of vinylidene fluoride, tetrafluoroethylene, and hexafluoropropylene (e.g., the DAI-EL G-801 product and the DAI-EL G-802 product, both commercially available from Daikin Industries of Osaka, Japan) and copolymers of vinylidene fluoride and tetrafluoroethane-perfluoro(methyl vinyl ether) (e.g., the VTR 8500 product or VTR 8650 product, both commercially available from Dupont-Dow Elastomer of Wilmington, DE). Examples of suitable fluorinated elastomeric terpolymers include terpolymers of tetrafluoroethylene, hexafluoropropylene and vinylidene fluoride. In some embodiments, the fluoroelastomer may be modified with iodine or another material to facilitate cross-linking of the fluoroelastomer.

Examples of suitable epichlorohydrins for use in the elastomeric compositions of the present invention include homopolymers of epichlorohydrin, copolymers containing epichlorohydrin, terpolymers containing epichlorohydrin, and elastomeric polymers derived from epichlorohydrin and three or more different monomers. Examples of particularly suitable copolymers of epichlorohydrin include copolymers of epichlorohydrin and ethylene oxide and copolymers of epichlorohydrin and allyl glycidyl ether. Examples of particularly suitable terpolymers of epichlorohydrin include

terpolymers of epichlorohydrin, ethylene oxide, and allyl glycidyl ether (e.g., the T3000L or HYDRIN[®] SC1000 product commercially available from Zeon Chemicals L.P. of Louisville, KY); and terpolymers of epichlorohydrin, propylene oxide, and allyl glycidyl ether.

5 Besides fluoroelastomer and epichlorohydrin, the elastomeric compositions of the present invention may also include additional optional materials such as reinforcing filler materials, fluoroplastics in addition to fluoroelastomers, pigments, energy-beam absorbents, antioxidants, stabilizing agents, fillers, oils, processing aids, neutralizers, rheology modifiers, silane coupling agents, cross-linking materials (e.g., cross-linking
10 agents, cross-linking co-agents, and cure accelerators), lubricants, flame retardants, flame retardant synergists, antimicrobials, any other additive known in the art, and any combination of these in any proportion. The concentration of these additional materials in the elastomeric composition of the present invention may be any concentration sufficient to provide a desired result.

15 Reinforcing filler material may optionally be included in the elastomeric composition of the present invention to enhance the split and tear properties of cold-shrink articles (formed from the elastomeric composition) at elevated temperatures. Examples of suitable filler materials include silica-based reinforcement filler, reinforcement-grade carbon black, fluoroplastics, clays, and any combination of any of these in any
20 proportions. In some embodiments, the concentration of the reinforcement filler in the elastomeric composition of the present invention may be, for example, as low as about 1.25 phr and as high as about 30 phr, on a weight basis. In other embodiments, the concentration of the reinforcement filler in the elastomeric composition may be as low as about 20 phr and as high as about 25 phr, on a weight basis.

25 As used herein, the term "silica-based reinforcement filler" is defined to include all compounds of the formula SiO₂ (e.g., pure silica); all compositions that include at least about ten weight percent of SiO₂ and/or an SiO₂ derivative, based upon the total weight of the composition; all silicates; and any combination of any of these in any proportion. Examples of suitable silica-based reinforcement fillers include silica (also referred to as
30 silicon dioxide); silane-treated silica; fumed silica (e.g., such as the CABOSIL[®] M-5 product commercially from Cabot Corporation of Billerica, MA); silane-treated fumed silica such as, for example, the AEROSIL[®] R972 product, the AEROSIL[®] R974 product,

and the AEROSIL[®] 200 product that are all commercially available from Degussa Company of Parsippany, NJ and the CABOSIL[®] line of silane-treated fumed silica products commercially from Cabot Corporation of Billerica, MA; silicates; and any combination of any of these in any proportion. Examples of suitable silicates include
5 calcium silicate, aluminum silicate, and mixtures of these.

In some embodiments, the average particle size of the silica-based reinforcement filler may be less than about 30 nanometers (nm). In other embodiments, the average particle size of the silica-based reinforcement filler may be as low as about 10 nm and as high as about 20 nm.

10 The phrase "reinforcement-grade carbon black", as used herein, includes any carbon black with an average particle size smaller than about 40 nm, which corresponds to an average surface area of about 65 m²/g. Some suitable average particle sizes for the reinforcement-grade carbon black are less than about 40 nm. Some particularly suitable average particle sizes for the reinforcement-grade carbon black range from greater than
15 about 10 nm, which corresponds to an average surface area of about 140 m²/g, to less than about 38 nm, which corresponds to an average surface area of about 46 m²/g. Some examples of suitable reinforcement-grade carbon black include N-100 series carbon black, N-200 series carbon black, N-300 series carbon black, and N550 carbon black, which are all commercially available from Cabot Corporation of Billerica, MA.

20 Examples of fluoroplastics that may suitably serve as the reinforcing filler material or as part of the reinforcing filler material include homopolymers of tetrafluoroethylene monomers, any copolymer that includes a tetrafluoroethylene monomer, any terpolymer that includes a tetrafluoroethylene monomer, any other polymer that includes a tetrafluoroethylene monomer and three or more different monomers, and any combination
25 of any of these in any proportion. Examples of suitable copolymers include copolymers of tetrafluoroethylene and hexafluoropropylene (e.g., the ZONYL[®] MP 1500 product commercially available from DuPont Fluoroproducts of Wilmington, DE). Some examples of suitable component concentrations of fluoroplastics in the elastomeric compositions of the present invention range from about 0 phr up to about 5 phr, on a
30 weight basis.

Examples of suitable clay fillers that may serve as (or as part of) the reinforcing filler material include silane-treated kaolin clay (aluminum silicate) fillers commercially

available from Engelhard Corporation of Iselin, New Jersey under the trade designations "Translink 37", "Translink 77", "Translink 445", "Translink 555", and "Translink HF-900". Examples of suitable component concentrations of clay filler in compositions of the present invention range from as low as about 10 phr to as high as about 40 phr, on a weight basis.

Examples of suitable energy beam absorbents for use in the elastomeric compositions of the present invention include PolyOne Material No. AD 3000051160 ("Stan-Tone MB-27838 Black"), PolyOne Material Product No. CC10041306WE, and "Stan-Tone MB-29293" (all available from PolyOne Corporation of Suwanee, Georgia); RTP Material No. RTP 0299 x 102892 SSL-801191, available from RTP Company of Winona, Minnesota; Clariant Material No. 00025275, available from Clariant Masterbatches Division of Albion, Michigan; Ticona Material No. 1000-2LM ND3650, available from Ticona of Summit, New Jersey; BASF Material No. NPP TN020327 ("Ultramid B3K LS Black 23189"), available from BASF Corporation Performance Polymers of Mt. Olive, New Jersey; and combinations thereof. These energy beam absorbent materials may include titanium dioxide, mica, and combinations thereof. Titanium dioxide may function as both a pigment and an energy beam absorbent, as discussed in Birmingham, Jr. et al., U.S. Patent No. 5,560,845.

The elastomeric compositions of the present invention may include a pigment or combination of pigments to affect a base color of cold-shrink articles formed from the elastomeric compositions of the present invention. Examples of suitable pigments include titanium dioxide; carbon black; zinc oxide; prussian blue; cadmium sulfide; iron oxide; chromates of lead, zinc, barium, and calcium; azo; thioindigo; anthraquinone; anthranthrene; triphenylenedioxazine; fat dye pigments; phthalocyanine pigments, such as copper phthalocyanine pigment and its derivatives; quinacridon pigment; pigments commercially available under the trade designations "Cinquasia", "Cromophtal", "Filamid", "Filester", "Filofin", "Hornachrome", "Horna Molybdate", "Hornatherm", "Irgacolor", "Irgalite", "Irgasperse", "Irgazin", "Micranyl", "Microlen", "Microlith", "Microsol", and "Unisperse", all from Ciba Specialty Chemicals of Tarrytown, NY; and any combination of any these in any proportion. In some embodiments, the color and concentration of pigment(s) incorporated within the elastomeric composition may depend upon how much energy beam absorbent is incorporated. As one example, a yellow-color

pigment may be used in combination with an energy beam absorbent to yield cold-shrink articles that, when exposed to a focused energy beam, exhibit high-contrast energy-beam induced indicia.

5 Examples of suitable antioxidants for use in the elastomeric compositions of the present invention include solutions of zinc 2-mercaptotoluimidazole in petroleum process oil (e.g., "Vanox ZMTI" and "Vanox MTP" commercially available from R.T. Vanderbilt Company, Inc. of Norwalk, Connecticut); mixtures of octylated diphenylamines (e.g. "Agerite Stalite" commercially available from R.T. Vanderbilt Company, Inc. of Norwalk, Connecticut); phenolic-based antioxidants (e.g., IRGANOX[®] 1010 commercially available
10 from Ciba Specialty Chemicals); aromatic amine type antioxidants (e.g., NAUGARD[®] 445 commercially available from Crompton Corporation of Middlebury, Connecticut); and combinations of these. Some examples of antioxidant concentrations in the elastomeric compositions of the present invention range from as low as about 0 phr to as high as about 3 phr, on a weight basis.

15 Examples oils that may suitably be included in elastomeric compositions of the present invention include hydrocarbon oils (e.g. poly(chlorotrifluorethylene) commercially available from Halocarbon Production Corporation of River Edge, NJ under the trade designation Halocarbon 95).

20 Examples of some suitable cross-linking agents for the elastomeric compositions include amines and peroxides, such as the following peroxides that are commercially available from R.T. Vanderbilt Company, Inc. of Norwalk, Connecticut: dicumyl peroxide (e.g., the VAROX[®] DCP product, the VAROX[®] DCP-40C product, the VAROX[®] DCP-40KE product, and the VAROX[®] DCP-40KE-HP product); benzoyl peroxide (e.g., the VAROX[®] ANS product); dibenzoyl peroxide (e.g., the VAROX[®] A 75
25 product); 2,5-dimethyl-2,5-di(t-butylperoxy) hexane (e.g., the VAROX[®] DBPH product, the VAROX[®] DBPH 40 MB product, the VAROX[®] DBPH-50 product, the VAROX[®] DBPH-50-HP product, the VAROX[®] DBPH-P20 product, and the VAROX[®] DCP-40KE product); t-butyl perbenzoate (e.g., the VAROX[®] TBPB product and the VAROX[®] TBPB-50 product); 2,5-dimethyl-2,5-di(t-butylperoxy) hexyne-3 (e.g., the VAROX[®] 130 product
30 and the VAROX[®] 130-XL product); alpha, alpha-bis(t-butylperoxy)diisopropylbenzene (e.g., the VAROX[®] VC-R product); di-(2-tert-butylperoxyisopropyl) benzene (e.g., the VAROX[®] 802-40C product, the VAROX[®] 802-40KE product, and the VAROX[®] 802-

40KE-HP product); di-(2-tert-butylperoxyisopropyl) benzene in EPR (e.g., the VAROX[®] 802-40MB product); derivatives of any of these; and any combination of these in any proportion. Examples of suitable cross-linking agent concentrations in the elastomeric compositions of the present invention range from as low as about 1 phr to as high as about 5 phr, on a weight basis.

Cross-linking co-agents may be incorporated in the elastomeric compositions of the present invention to enhance the cross-linking reaction. Examples of suitable cross-linking co-agents for incorporation in the elastomeric compositions include triallyl isocyanurates (e.g., the TAIC DLC-A product commercially available from Natrochem Inc. of Savannah, GA.) and acrylic co-agents. Examples of suitable acrylic co-agents include multi-functional monomers, such as difunctional and trifunctional monomers. Examples of suitable difunctional monomers include the following, which are commercially available from Sartomer Company, Inc., Exton, Pennsylvania: 1,3-butylene glycol diacrylate, 1,3-butylene glycol dimethacrylate, 1,4-butanediol diacrylate, 1,4-butanediol dimethacrylate, 1,6 hexanediol diacrylate, 1,6 hexanediol dimethacrylate, aliphatic dimethacrylate monomer, alkoxyated aliphatic diacrylate, alkoxyated cyclohexane dimethanol diacrylate, alkoxyated cyclohexane dimethanol diacrylate, alkoxyated cyclohexane dimethanol diacrylate, alkoxyated hexanediol diacrylate, alkoxyated hexanediol diacrylate, alkoxyated neopentyl glycol diacrylate, alkoxyated neopentyl glycol diacrylate, aromatic dimethacrylate monomer, caprolactone modified neopentylglycol hydroxypivalate diacrylate, caprolactone modified neopentylglycol hydroxypivalate diacrylate, cyclohexane dimethanol diacrylate, cyclohexane dimethanol dimethacrylate, diethylene glycol diacrylate, diethylene glycol dimethacrylate, dipropylene glycol diacrylate, ethoxylated (10) bisphenol alpha diacrylate, ethoxylated (2) bisphenol alpha dimethacrylate, ethoxylated (3) bisphenol alpha diacrylate, ethoxylated (30) bisphenol alpha diacrylate, ethoxylated (30) bisphenol alpha dimethacrylate, ethoxylated (4) bisphenol alpha diacrylate, ethoxylated (4) bisphenol alpha dimethacrylate, ethoxylated (8) bisphenol alpha dimethacrylate, ethoxylated bisphenol alpha dimethacrylate, ethoxylated bisphenol alpha dimethacrylate, ethoxylated(10) bisphenol dimethacrylate, ethoxylated(6) bisphenol alpha dimethacrylate, ethylene glycol dimethacrylate, hydroxypivalaldehyde modified trimethylolpropane diacrylate, neopentyl glycol diacrylate, neopentyl glycol

dimethacrylate, polyethylene glycol (200) diacrylate, polyethylene glycol (400) diacrylate, polyethylene glycol (400) dimethacrylate, polyethylene glycol (600) diacrylate, polyethylene glycol (600) dimethacrylate, polyethylene glycol dimethacrylate, polypropylene glycol (400) dimethacrylate, propoxylated (2) neopentyl glycol diacrylate, 5 tetraethylene glycol diacrylate, tetraethylene glycol dimethacrylate, tricyclodecane dimethanol diacrylate, triethylene glycol diacrylate, triethylene glycol dimethacrylate, tripropylene glycol diacrylate, tripropylene glycol diacrylate, and combinations thereof. Examples of suitable trifunctional monomers include trimethylolpropane trimethacrylate, trimethylolpropane triacrylate, and combinations thereof. Examples of suitable cross- 10 linking co-agent concentrations in the elastomeric compositions of the present invention range from as low as about 0.5 phr and as high as about 4.5 phr, on a weight basis.

The elastomeric composition of the present invention may be prepared by blending together the fluoroelastomer and the epichlorohydrin in an appropriate mixing apparatus. For example, the components of the elastomeric composition, including the 15 fluoroelastomer and the epichlorohydrin, may generally be combined in any order in an appropriate mixing apparatus at a component temperature of about 60°C.

Additional optional materials may also be included with the fluoroelastomer and the epichlorohydrin prior to mixing. If cross-linking agents or cross-linking co-agents are to be incorporated in the elastomeric composition, the components including the 20 fluorelastomer and the epichlorohydrin may be blended together in a first mixing step as described above. The cross-linking agents and/or cross-linking co-agents may then be blended into the elastomeric composition in a second mixing step at a lower temperature than the first mixing temperature, such as between about 50°C and about 100°C, to prevent premature cross-linking.

25 The elastomeric composition may then be formed into a cold-shrink article by any suitable process such as, for example, extrusion or molding. In some embodiments, the elastomeric composition of the cold-shrink article is cured, using a suitable curing process, to affect cross-linking of the elastomeric composition. Some examples of suitable curing processes include, for example, elevated temperature and pressure conditions (e.g., 30 autoclaving), irradiation, or any other suitable curing process known in the art.

In some embodiments, the cold-shrink article may be autoclaved in an oxygen-free and/or water-free atmosphere, with the oxygen-free and/or water-free atmosphere being

used in place of steam. As used herein, unless otherwise stated, the term “oxygen-free atmosphere” refers to an atmosphere of a set volume of gas that includes less than about one volume percent oxygen, based on the total volume of the gas in the atmosphere, and the term “water-free atmosphere” refers to an atmosphere of a set volume of gas that includes less than about 0.1 volume percent water vapor, based on the total volume of the gas in the atmosphere. Examples of oxygen free-atmospheres include atmospheres including greater than about 99% by volume of nitrogen gas, argon gas, helium gas, xenon gas, neon gas, any other suitable inert gas, and combinations of any of these in any proportion. For example, tubing of the present invention may be autoclave-cured in a mold. As used herein, the term “tubing” refers to a hollow cylinder open on both ends. In one embodiment, the tubing is first formed (e.g., by extrusion) and then placed inside spiral grooves of an aluminum mold. The mold is placed in a heated press and subjected to a temperature of about 185°C and a pressure ranging from about 5-14 megapascals (Mpa) (about 75-200 psi). One end of the tubing is connected to a pressurized nitrogen gas supply containing about 99.5% nitrogen gas by volume. The mold may be purged for about two minutes with the pressurized nitrogen gas supply at a flow rate of about 40 cubic ft of the pressurized nitrogen gas. Any other purge time and flow rate sufficient to reduce oxygen and/or moisture to acceptable levels may also be used. After the initial purging, the mold is sealed off, and the pressure inside the mold may be maintained at about 200 pounds per square inch (psi) for about 20 minutes. The mold is then released and the pressure in the mold is allowed to return to atmospheric pressure. The tubing may then be removed from the mold and cooled.

In another embodiment, the cold-shrink articles may be irradiated after being formed to cure the cold-shrink articles. Such curing may be accomplished, for example, by individually sealing the cold-shrink articles in polyethylene bags and subjecting the bags (and the contents of the bags) to an irradiation dosage of less than about 15 Mrads from a 4.5 MeV electron beam machine (commercially available from Radiation Dynamics Inc. of Edgewood, NY). In some embodiments, the elastomeric compositions employed in the cold-shrink articles to be irradiated may include an electron-beam sensitizer, such as triallyl isocyanurate (e.g., the TAIC DLC-A product commercially available from Nastrochem Inc. of Savannah, GA).

The elastomeric compositions of the present invention may be formed into cold-shrink articles of any shape or geometric configuration known in the art. Some non-exhaustive examples of cold-shrink articles include tubing, plaques, and multiple-branched structures (i.e., tube-like structures with multiple entrances and/or exits).

5 Cold-shrink articles of the present invention (formed from elastomeric compositions of the present invention) may exhibit various advantageous mechanical properties in various combinations under various environmental conditions (e.g., room temperature or 150°C). In some embodiments, cold-shrink articles of the present invention such as tubing and plaques may exhibit an elongation at break of at least about 450% at
10 room temperature and/or an elongation at break of at least about 250% at 150°C, when tested pursuant to the procedures of the Property Analysis and Characterization Procedure section of this document. Some embodiments of the cold-shrink articles of the present invention such as tubing and plaques may exhibit a percent permanent set of less than about 35% at 100°C, when tested pursuant to the procedures of the Property Analysis and
15 Characterization Procedure section. Furthermore, some embodiments of tubing and plaques formed from compositions of the present invention may exhibit a percent permanent set of less than about 25% at 100°C. In some embodiments, plaques formed from compositions of the present invention may exhibit a percent permanent set of less than about 20% at 100°C.

20 Various embodiments of the cold-shrink articles of the present invention resist tearing or splitting at elevated temperatures. For example, some embodiments of the cold-shrink articles of the present invention resist tearing when maintained in an expanded state for an extended period of time (e.g, seven days in a 200% radially-expanded state) at an elevated temperature of about 150°C.

25 Various embodiments of the cold-shrink articles of the present invention exhibit chemical resistance to substances such as, for example, diesel fuel and hydraulic fluid. Some embodiments of the cold-shrink articles of the present invention exhibit a percent weight increase of less than about 25% when immersed in diesel fuel at about 49°C for 24 hours and/or a percent weight increase of less than about 10% when immersed in
30 hydraulic fluid at about 71°C for 24 hours.

A tubular cold-shrink article 10 of the present invention is depicted in FIG. 1 in an initial relaxed state prior to any expansion. The cold-shrink article 10 includes a radial wall 11, an inner surface 14, and an outer surface 16.

When cold-shrink article 10 is in the initial relaxed state, the radial wall 11 has a longitudinal length A, an inner diameter B, an outer diameter C, and a layer thickness D. The longitudinal length A and the inner diameter B may vary based upon individual needs of a given application, such as for example, the dimensions of a substrate about which the cold-shrink article 10 will be placed. The outer diameter C is generally determined by the inner diameter B and the layer thickness D, where the layer thickness D is ordinarily substantially uniform both around a circumference E and along the length A of the cold-shrink article 10. The layer thickness D is desirably thin enough to allow the cold-shrink article 10 to readily expand from the initial relaxed state upon application of expansion forces.

Examples of suitable layer thickness D range from as low as about 0.060 inches to as high as about 0.25 inches. Examples of suitable inner diameter B range from as low as about 0.2 inches to as high as about 3 inches.

Various stages of a method for deploying the cold-shrink article 10 are depicted in FIGS. 2-5. The cold-shrink article 10 is depicted in an expanded state on the core 18 in FIG. 2. A substrate 20 is shown in FIG. 3 to be inserted into the core 18, which supports the expanded form of the cold-shrink article 10. The cold-shrink article 10 partially deployed from the core 18 onto the substrate 20 is depicted in FIG. 4. The cold-shrink article 10 fully deployed on the substrate 20 is depicted in FIG. 5. The cold-shrink article 10 may protect substrate 20 and/or may identify the substrate 20, which may, for example, comprise a wire, a cable, a fluid-carrying pipe, or a conduit.

To deploy the cold-shrink article 10 on the substrate 20, the cold-shrink article 10 is first cross-sectionally (or radially) expanded from the initial relaxed state to the expanded state and oriented on the core 18, as depicted in FIG. 2. As used herein, the terms "expanded", "expansion", "expanded state", and the like, refer to a cross-sectional expansion that increases inner diameter B and outer diameter C, as opposed to a longitudinal expansion that increases longitudinal length A, though such a longitudinal expansion is permissible. The cold-shrink article 10 may be expanded and placed onto the core 18 in any conventional manner. The core 18 may generally have any structure that is

suitable for retaining the cold-shrink article 10 in the expanded state. For example, the core 18 may be a rigid, hollow, plastic tube.

When the cold-shrink article 10 is in the expanded state, as best depicted in FIG. 2, the radial wall 11 has a longitudinal length A', an inner diameter B', an outer diameter C', and a wall thickness D'. Due to the expansion, the inner diameter B' and the outer diameter C' are larger than the inner diameter B and the outer diameter C, respectively. Suitable expansion of the cold-shrink article 10 may generally range from about 150% to about 400%, where the expansion is characterized in terms of the percent expansion of the inner diameter B relative to the inner diameter B'. Particularly suitable expansion of the cold-shrink article 10 may generally range from about 200% to about 300%.

The substrate 20 may be inserted within the core 18 holding the expanded form of the cold-shrink article 10, as depicted in FIG. 3. In some embodiments, the substrate 20 may be centered within the hollow portion of the core 18 using guide fingers (not shown) contained within the core 18. After the substrate 20 is inserted within the core 18, the cold-shrink article 10 is conveyed from the core 18 onto the substrate 20, as depicted in FIG. 4. The conveyance may be accomplished in a variety of manners, such as by sliding the cold-shrink article 10 from the core 18 onto the substrate 20, or by collapsing and removing the core 18 and thereby allowing the cold-shrink article 10 to encompass and come into engagement with the substrate 20.

When the cold-shrink article 10 is removed from the core 18, the cold-shrink article 10 cold shrinks from the expanded state toward (but not necessarily all the way to) the initial relaxed state. Whether or not the cold-shrink article 10 reaches the relaxed state depends on the diameter of the substrate 20. The substrate 20 may have a diameter that allows the cold-shrink article 10 to substantially return to the initial relaxed state and substantially regain the inner diameter B and the outer diameter C, as best depicted in FIG. 4. The inner diameter B of cold-shrink article 10 in the initial relaxed state may be slightly smaller than the exterior diameter of the substrate 20, which prevents the cold-shrink article 10 from fully shrinking back to the initial relaxed state, and thereby provides a snug and secure fit and engagement of the cold-shrink article 10 onto peripheral surfaces of the substrate 20. When the cold-shrink article 10 is fully deployed on the substrate 20, the inner surface 14 of the cold-shrink article 10 extends around, faces, and is typically in contact with the outer surface 22 of the substrate 20, as shown in FIG. 5.

In some embodiments, the outer surface 16 of the cold-shrink article 10 may include identifiers in the form of optional indicia 24, which may provide, for example, information relating to the cold-shrink article 10 and/or the substrate 20. The indicia 24 may be a single mark or a plurality of marks, and may include a variety of textual (i.e.,
5 alphanumeric) or graphical characters, symbols, and the like. The indicia 24 may also be or include machine-readable indicia, such as bar codes. Also, the indicia 24 may have a surface texture that is different from the texture of portions of the outer surface 16 other than the indicia 24.

The indicia 24 may be formed using any suitable process including, for example, ink application to the outer surface 16 and/or focused energy beam marking of the outer
10 surface 16. A focused energy beam refers to a directionally focused stimulated emission of radiation, such as a laser beam. The indicia 24, in the form of energy-beam induced indicia, may be formed, for example, by expanding the cold-shrink article 10 from the initial relaxed state, marking the outer surface 16 by application of energy from a focused
15 energy beam, and allowing the cold-shrink article 10 to cold shrink back toward the initial relaxed state.

To facilitate formation of energy-beam induced indicia, the elastomeric compositions of the present invention may include an energy beam absorbent. Such energy beam absorbents, upon heating by a focused energy beam, may be employed to
20 provide the indicia 24 with a different color than the color of the outer surface 16 other than the indicia. In this way, the color of the indicia 24 may contrast with the color of the outer surface 16 so the indicia are prominent and legible. If a high visual legibility of the indicia 24 is desired, both a pigment and an energy beam absorbent may be included in the elastomeric composition to provide a high contrast between the base color of the outer
25 surface 16 and the contrasting color of the indicia 24. For further discussion regarding energy-beam induced identifiers and methods for marking cold-shrink articles, see Application No. 10/806,811 filed on March 23, 2004 and entitled "Cold-Shrink Marker Sleeve."

In some embodiments, indicia 24 are legible to an unaided eye of an individual
30 with 20/20 vision located at least about 36 centimeters away from indicia 24 when the cold-shrink article 10 is in an expanded state or a relaxed state.

Information pertaining to the cold-shrink article 10 and/or the substrate 20 may also be conveyed to a user by a base color of the outer surface 16 of the cold-shrink article 10. For example, a blue base color of the outer surface 16 may convey different information to a user than a yellow or black base color. In some embodiments, the cold-shrink article 10 may include both the indicia 24 and an information-conveying base color of the outer surface 16.

Cold-shrink articles of the present invention may include a plurality of elastomeric members. A branched cold-shrink article 30 of the present invention, in a relaxed state prior to expansion, is depicted in FIG. 6. The cold-shrink article 30 may include a plurality of hollow elastomeric portions (or members) 32A, 32B, 32C, and 32D that each have the inner surface 14 and the outer surface 16. The respective inner surfaces 14 define elongate cavities (not shown) through each of the elastomeric portions 32A, 32B, 32C, and 32D that are in communication with each other.

When the hollow elastomeric portions 32A, 32B, 32C, and 32D are stretched to the expanded state, cores 18 may be inserted within the expanded portions 32A, 32B, 32C, and 32D, as depicted in FIG. 7, to maintain the portions 32A, 32B, 32C, and 32D in the expanded state. The cold-shrink article 30 (portions 32A, 32B, 32C, and 32D) may be deployed on one or more substrates 20 from the expanded states on the cores 18 pursuant to the methods described above in relation to deployment of the cold-shrink article 10.

Cold-shrink articles of the present invention may include corrugations that allow the cold-shrink articles to exhibit a longitudinal length in a non-corrugated relaxed state that is substantially longer than the longitudinal length of the cold-shrink articles when positioned on a removable core in an expanded, corrugated state. A cold-shrink article 40, which is partially deployed from the core 18 onto the outer surface 22 of the substrate 20, is depicted in FIG. 8. When in the expanded state on the core 18, the cold-shrink article 40 includes a multitude of corrugations 42. As illustrated by the cold-shrunk portion 44, after release from the core 18, unsupported corrugated portions of the cold-shrink article 40 extend longitudinally and the corrugations formerly present in the unsupported portions effectively disappear as the cold-shrunk portion 44 approaches the initial relaxed state.

PROPERTY ANALYSIS AND CHARACTERIZATION PROCEDURES

Various analytical techniques may be used to characterize the properties of cold-shrink articles of the present invention. Details about these analytical techniques follow.

As used herein, "ASTM D412" refers to ASTM D412 – 98a (Reapproved 2002) entitled "Standard Test Methods for Vulcanized Rubber and Thermoplastic Elastomers – Tension", which was published in January 2003 and is available from the American Society for Testing and Materials International of West Conshohocken, Pennsylvania.

5 I. Mechanical Property Tests

A. Elongation at Break and Stress at Break

Determinations of the stress at break and percent elongation at break for dumbbells formed from the elastomeric compositions of the present invention are performed pursuant to the procedures of Test Method A of ASTM D412 using a tensiTECH III tensile tester commercially available from Tech Pro of Cuyahoga Falls, Ohio.

A method described below similar to Test Method B of ASTM D412 may be used to determine the elongation at break for ring samples cut from tubing formed from elastomeric compositions of the present invention. According to the method employed herein, ring samples, having a longitudinal width of about 3/8 of an inch, are cut from the tubing, and the ring samples are placed in a tensile testing apparatus. Each end of each ring sample is secured to a jaw between two 0.124 inch-diameter pins attached to each jaw. The jaws of the tensile tester apparatus are then pulled in opposite directions at a rate of about 20 inches/minute and the strain and break loads are recorded. Unless otherwise stated herein, the elongation at break and stress at break tests are performed in a temperature-controlled box at a temperature of about 150°C, with the test samples conditioned for about 6 ± 2 minutes at 150°C before conducting the tests.

The stress at break for the ring samples is computed using the following equation:

$$\text{Actual Stress} = \frac{\text{Break Load}}{(2 \times \text{Width of Ring Sample} \times \text{Thickness of Ring Sample})}$$

The elongation at break for the ring samples is computed using the following equation:

$$\text{Actual Elongation of ID at break} = ((\text{Stretched circumference} - \text{Initial circumference}) / (\text{Initial circumference})) \times 100.$$

B. Percent Permanent Set

The percent permanent set test illustrates the amount of elastic recovery an article exhibits. The percent permanent set is calculated using the following equation:

$$\% \text{PermanentSet} = \frac{100 \times (\text{RelaxedLength} - \text{OriginalLength})}{(\text{TestLength} - \text{OriginalLength})}$$

To determine the percent permanent set for plaques, dumbbell test specimens are cut from plaques pursuant to the procedures of Test Method A of ASTM D-412. Parallel bench marks separated by a distance of an inch are placed at the approximate center of each dumbbell. The dumbbells are placed in a set fixture and stretched until the distance between the bench marks equals 2 inches, which correlates to 100% strain. The loaded set fixture is then placed in a 100°C oven for 3 hours. After 3 hours, the fixtures are removed from the oven and the stretched dumbbells are allowed to cool at room temperature (21°C ± 2°C) for 1 hour. The stretched dumbbells are removed from the set fixture and placed on a smooth wooden or cardboard surface. The distance between the parallel bench marks is measured after waiting 30±2 minutes. The percent permanent set is determined using the formula provided above with the original length equaling 1 inch, the test length equaling 2 inches, and the relaxed length equaling the final distance between the bench marks after cooling.

To determine the percent permanent set for tubing, ring samples having a length of 3/8 of an inch are cut from the tubing and the initial diameters of the ring samples are measured. The ring samples are then inserted over a steel mandrel having a diameter about twice the internal diameter of the tubing ring samples, which causes the ring samples to radially stretch about 100% in diameter. An end of the mandrel is equipped with a conical shape to facilitate inserting & removing the mandrel from the ring samples. While stretched on the mandrel, the ring samples are placed in a 100°C oven for 3 hours. After expiration of the 3-hour period, the mandrel and stretched ring samples are removed from the oven and allowed to cool at room temperature (21°C ± 2°C) for 1 hour. The ring samples are then removed from the mandrel and placed on a smooth wooden or cardboard surface. The internal diameters of the ring samples are measured after passage of 30±2 minutes, and the following formula is used to compute the percent permanent set of the ring samples:

$$\% \text{ Permanent Set} = \frac{100 (rd - od)}{md - od},$$

where *rd* is the relaxed diameter, *od* is the original diameter, and *md* is the mandrel diameter.

C. Tubing Split Test

Tubing split tests are conducted to illustrate the tear properties of the cold-shrink articles over time. The test is conducted using tubing samples prepared from elastomeric compositions of the present invention pursuant to the methods described above. Samples of tubing having a length of about 3 to 4 inches are cut and placed over steel mandrels, which have a diameter about three times the internal diameter of the tubing samples. As such, the tubing samples are expanded radially by about 200%. While retained in a state of about 200% radial expansion, the samples are placed in a 150°C oven for seven days. After expiration of the seven-day period, the elongated samples are visually inspected for signs of tearing. Tubing samples are deemed to have failed the split test if any tearing or splitting is visually observed by an unaided human eye.

II. Fluid Resistance Tests

The fluid resistance of cold-shrink articles of the present invention is determined by cutting dumbbell test specimens (pursuant to the methods of Test Method A of ASTM D412) from plaques formed from compositions of the present invention. The test specimens are weighed individually and then immersed in either hydraulic fluid or diesel fuel in wide test tubes. The test tubes containing the diesel fuel are placed in an oil bath maintained at a temperature of about 49°C for 24 hours and the test tubes containing the hydraulic fluid were placed in an oil bath maintained at a temperature of about 71°C for 24 hours. The test specimens are then removed from test tubes, padded dry with filter paper, and weighed individually. The respective percent absorptions of diesel fuel and hydraulic fluid for the test specimens are then computed using the initial weights and the final weights of the dumbbell test specimens.

III. Laser Marking Test

The visual legibility of the indicia is qualitatively determined for cold-shrink articles pursuant to the following procedure. Tubing without indicia, having a 1.0 mm outer diameter, is expanded onto a core with a 2.0 cm diameter. The expanded tubing is then laser marked to form indicia by a Nd:YAG laser system. The Nd:YAG laser system is commercially available under the trade name "Hi-Mark" No. 400 from GSI Lumonics, Inc. of Kanata, Ontario, Canada. The laser settings for the Nd:YAG laser system include a power setting of 64.8 watts, a rate of marking 5.1 cm/minute, and a frequency of 6 wave peaks per second. The set distance of the laser system head to the outer surface of the tubing is 18.3 cm (7.2 inches). The indicia is marked so the indicia, with the tubing in the

expanded state, exhibits a type-face height in a circumferential direction about the tubing of 2.0 mm.

After marking, the tubing is removed from the core and allowed to substantially cold shrink back toward the relaxed state. The indicia on the tubing substantially in the relaxed state is then visually observed by an unaided human eye. The marking is determined to be acceptable if the indicia (exhibiting a type-face height of 2.0 mm) on the tubing is visually legible by an unaided human eye (i.e., about 20/20 vision) from a distance of at least about 36 cm (about 14 inches).

EXAMPLES

The present invention is more particularly described in the following examples that are intended as illustrations only, since numerous modifications and variations within the scope of the present invention will be apparent to those skilled in the art. Unless otherwise noted, all parts, percentages, and ratios reported in the following examples are on a weight basis, and all reagents used in the examples were obtained, or are available, from general chemical suppliers such as the Sigma-Aldrich Chemical Company of Saint Louis, Missouri, or may be synthesized by conventional techniques. Also, unless otherwise stated, all performance data included herein for tubing is for tubing cured in an oxygen-free atmosphere. In addition, unless otherwise noted, all tests were performed pursuant to the property analysis and characterization procedures described above.

The following compositional abbreviations are used in the following Examples:

AEROSIL[®] R974: A silane-treated, fumed silica commercially available from Degussa Company of Parsippany, NJ.

ARMOSLIP CP: A slip agent commercially available from Lion Akzo Co., Ltd.

DAI-EL G-801: A fluoroelastomer copolymer of vinylidene fluoride and hexafluoropropylene commercially available from Daikin Industries of Osaka, Japan.

NAUGARD[®] 445: An aromatic, amine-type antioxidant commercially available from Crompton Corporation of Middlebury, Connecticut.

N-550 Black: A reinforcement-grade carbon black commercially available from Cabot Corporation, Billerica, MA.

- Stearic Acid: Stearic acid commercially available from Arizona Chemical of Florida.
- STAN-TONE[®] MB Black: An energy beam absorbent commercially available under the trade designation Stan-Tone[®] MB 29293 from PolyOne Corporation of Suwanee, Georgia.
- STAN-TONE[®] DB Yellow: A yellow pigment commercially available under the trade designation Stan-Tone[®] DB 29282 from PolyOne Corporation of Suwanee, Georgia.
- TAIC DLC-A: A cross-linking co-agent commercially available from Natrochem, Inc. of Savannah, GA.
- TiO₂: Titanium dioxide commercially available under the trade designation Ti-Pure[®] R-902 from DuPont.
- T3000L: An epichlorohydrin polymer commercially available from Zeon Chemicals of Louisville Kentucky.
- Translink 37: Silane treated kaolin clay (aluminum silicate) with a particle size of 1.4 micrometers, commercially available from Engelhard Corporation of Iselin, New Jersey.
- VAROX[®] DBPH-50-HP: A 2,5-dimethyl-2,5-di(t-butylperoxy)hexane cross-linking agent commercially available from R.T. Vanderbilt Company of Norwalk, CT.
- Zinc Omadine: A fungicide solution of 65% 2-pyridinethiol-1-oxide, zinc complex in a paraffinic oil (i.e., Zinc Omadine), commercially available from Arch Chemicals, Inc. of Cheshire, Connecticut.
- ZONYL[®] MP1500: A copolymer of tetrafluoroethylene and hexafluoropropylene commercially available from DuPont Fluoroproducts of Wilmington, DE.

Examples 1 - 3

Examples 1-3 concern cold-shrink articles of the present invention in the form of tubing and plaques. The component concentrations of the elastomeric compositions used to form the cold-shrink articles of Examples 1-3 are provided in Table 1. The elastomeric compositions of Examples 1-3 were prepared by combining the first fourteen components provided in Table 1 in a first mixing step, and then mixing these components in a

Banbury mixer at between about 20 and 40 revolution-per-minute for about 20 minutes at a temperature of about 60°C. The compositions were then further mixed in a 2-roll mixing mill heated to about 50°C for about 5 minutes. The TAIC DLC-A listed in Table 1 was then added to each composition in a second mixing step and the compositions were mixed
 5 for an additional 5 minutes. The compositions were then sheeted out in conventional fashion and cooled to the ambient temperature (22-24°C).

TABLE 1

Components (phr*)	Example 1	Example 2	Example 3
T3000L	80	60	40
DAI-EL G-801	20	40	60
ZONYL [®] MP1500	2	2	2
AEROSIL [®] R974	10	10	10
TiO ₂	9	9	9
Translink 37	20	20	20
Ca(OH) ₂	5	5	5
NAUGARD [®] 445	1	1	1
Stearic Acid	2	2	2
Armoslip-CP	1	1	1
Zinc Omadine Paste	0.75	0.75	0.75
STAN-TONE [®] DB Yellow:	0.45	0.45	0.45
STAN-TONE [®] MB Black	0.14	0.14	0.14
VAROX [®] DBPH-50-HP	3	5	5
TAIC DLC-A	2.5	4	4

*component concentrations are given in parts by weight per 100 total parts by weight of T3000L and DAI-EL G-801.

10 Physical Properties Tests for Examples 1-3

The elastomeric compositions of Examples 1-3 were extruded into tubing having an internal diameter of about 0.25 inches and a wall thickness of about 0.18 cm using a 3/4-inch extruder with a L/D ratio of 20. The extrusions were done at a barrel temperature of about 60°C and a die temperature between about 30°C and 60°C. The resulting tubing was
 15 cured in an oxygen-free atmosphere. The percent permanent set at 100°C, split resistance at 150°C for 7 days, stress at break at 150°C, and percent elongation at break at 150°C for the tubing of the compositions of Examples 1-3 were determined. The results of these tests are included in Table 2.

In addition, plaques were prepared by placing the compositions of Examples 1-3
 20 into molds and compression molding and curing the plaques at about 185°C under a pressure of about 5-10 Mpa for 15 minutes. This yielded plaques that were about 15 cm

long, about 10 cm long, and about 0.18 cm thick. The stress at break at room temperature, percent elongation at break at room temperature, and percent permanent set at 100°C test results for dumbbells cut from the plaques also are included in Table 2. The percent elongation and break and percent permanent set tests for the dumbbell samples were performed at room temperature.

TABLE 2

Composition	Example 1	Example 2	Example 3
ECO:FE Weight Ratio	80:20	60:40	40:60
Tubing Permanent Set (%)	21	24	28
Split Test Stretch (%)	207	208	210
Split Test Pass	6/6	6/6	4/6*
Tubing Stress at Break (psi)	227	261	292
Tubing Elongation at Break (%)	365	292	297
Plaque Permanent Set (%)	17	21	25
Plaque Stress at Break (psi)	1125	1256	1304
Plaque Elongation at Break (%)	632	561	515

* When tubing formed from the composition of Example 3 was tested at 175 % stretch, 3/3 samples passed the split test.

The data provided in Table 2 illustrates the expansion capabilities, durability, and tear performance at elevated temperatures of cold-shrink articles formed from the elastomeric compositions of Examples 1-3. The tubing samples of Examples 1-3 each exhibited a percent permanent set of less than 30%, with tubing samples of Examples 1 and 2 exhibiting percent permanent sets of less than 25%. In addition, all six tubing samples formed from each of the compositions of Examples 1 and 2 passed the extended split test provided in the Property Analysis and Characterization Procedures section of this document.

The dumbbell samples cut from plaques formed from the elastomeric samples of Examples 1-3 each exhibited a percent permanent set of less than 25% and a percent elongation at break at room temperature substantially greater than 250%.

In addition, the tubing samples of Examples 1-3 all marked well with a YAG laser and passed the laser marking test, when tested pursuant to the laser-marking procedures including in the Property Analysis and Characterization Procedures section of this document.

Example 4

The chemical resistance of dumbbell samples cut from plaques, formed from a composition similar to the composition of Example 1 and prepared by a procedure like that used for the composition of Example 1, was tested pursuant to the fluid resistance test procedures described above in Property Analysis and Characterization Procedures section of this document. The composition of Example 4 was generally the same as the composition of Example 1, except the Example 4 composition included 20 phr (weight basis) of AEROSIL[®] R974 based on the total weight of T3000L and DAI-EL G800 and did not include any Armoslip CP. The plaques were prepared pursuant to the method used to prepare the plaques of Example 1. After the dumbbell samples were subjected to the chemical resistance tests, the elongation at break and strain at break of the dumbbell samples was assessed at room temperature to determine the affects the chemicals had on the mechanical properties of the dumbbells. The results of these chemical resistance, stress at break, and elongation at break tests are included in Table 3.

TABLE 3

Test Fluid	Percent Weight Increase	Stress at Break (psi)	Elongation at Break (%)
Control (no fluid)	--	1520	787
Diesel Fuel	6.69	1253	665
Synthetic Hydraulic Fluid	1.31	1324	767

15

The data provided in Table 3 illustrates the chemical resistance of cold-shrink articles formed from the compositions of the present invention. As shown in Table 3, the dumbbell samples exhibited a percent weight increase in 49°C diesel fuel of 6.69% (substantially below the 25 % percent maximum threshold required by Military Spec, SC-X15111B, September 27, 1984) and a percent weight increase in 71°C hydraulic fluid of 1.31 % (substantially below the 10% weight increase maximum threshold required by Military Spec, SC-X15111B, September 27, 1984).

20

In addition, as shown in Table 3, the strain at break and the elongation at break for the dumbbell samples immersed in the diesel fuel and the hydraulic fluid did not change

substantially as compared to the control sample. The dumbbell samples immersed in diesel fuel and hydraulic fluid each exhibited an elongation at break at room temperature of greater than 450%.

Examples 5 & 6

5 Examples 5 and 6 concern cold-shrink articles formed from elastomeric compositions including carbon black. The component concentrations of the elastomeric composition used to form the cold-shrink articles of Examples 5 and 6 are provided in Table 4. The elastomeric composition of Examples 5 and 6 were prepared pursuant to the mixing procedures provided above for the compositions employed in Examples 1-3.

10

TABLE 4

Components (phr*)	Example 5	Example 6
T3000L	80	80
DAI-EL G-801	20	20
ZONYL [®] MP1500	2	2
AEROSIL [®] R974	20	20
N-550 Black	4	3
Ca(OH) ₂	5	5
NAUGARD [®] 445	1	1
Stearic Acid	2	2
Zinc Omadine Paste	0.75	0.75
TAIC DLC-A	2.5	2.5
VAROX [®] DBPH-50-HP	3	3.5

*component concentrations are given in parts per 100 total parts of T3000L and DAI-EL G-801.

Mechanical Properties and Chemical Resistance of Examples 5 and 6

15 Plaques and tubing were formed from the compositions of both Examples 5 and 6 pursuant to the procedures provided for the cold-shrink articles of Examples 1-3. Percent permanent set at 100°C, stress at break at 150°C, elongation at break at 150°C, extended split test at 150°C results for the tubing of Examples 5 and 6 are included in Table 5. In addition, the stress at break at room temperature, elongation at break at room temperature, diesel fuel absorption at 49°C, and hydraulic fluid absorption at 71°C test results for the
20 plaques of Examples 5 and 6 are included in Table 5.

TABLE 5

Test	Example 5	Example 6
Tubing Permanent Set (%)	26.6	21.4
Tubing Stress at Break (psi)	411	338
Tubing Elongation at Break (%)	552	399
Tubing Split Test at 200% stretch	Pass	Pass
Plaque Permanent Set (%)	15.9	16.2
Plaque Stress at Break (psi)	1771	1888
Plaque Elongation at Break (%)	686	625
Diesel Fuel Absorption at 49°C (weight basis increase)	5.30%	5.60%
Synthetic Hydraulic Fluid absorption at 71°C (weight basis increase)	4.00%	4.20%

The data provided in Table 5 further illustrates the expansion capabilities, durability, and tear performance of cold-shrink articles formed from the elastomeric compositions of Examples 1-3. The tubing samples of Examples 5-6 each passed the extended split test; each exhibited a percent elongation at break at 150°C greater than 250%; and each exhibited a percent permanent set of less than 30%, with the tubing samples of Example 6 exhibiting a percent permanent set of less than 25%. The dumbbell samples cut from plaques formed from the elastomeric compositions of Examples 5 and 6 each exhibited a percent permanent set substantially less than 25% and a percent elongation at break at room temperature substantially greater than 250%.

Although the present invention has been described with reference to preferred embodiments, workers skilled in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention.

CLAIMS:

1. A cold-shrink composition comprising:
a fluoroelastomer; and
5 an epichlorohydrin;
wherein the composition, when formed into a tubular elastomeric article, exhibits a
permanent set of less than about 35%.
2. The composition of claim 1, wherein the composition includes about 10 parts or
10 greater of fluoroelastomer and about 60 parts or less of fluoroelastomer, per 100 total parts
of fluoroelastomer and epichlorohydrin, and about 40 parts or greater of epichlorohydrin
and about 90 parts or less of epichlorohydrin, per 100 total parts of fluoroelastomer and
epichlorohydrin.
- 15 3. The composition of claim 1, and further comprising:
a filler material.
4. The composition of claim 1, wherein an article formed from the composition
exhibits less than about a 25% weight increase when immersed in diesel fuel for 24 hours
20 at a temperature of about 49°C or less.
5. The composition of claim 1, and further comprising: comprising:
an energy beam absorbent; wherein the composition is capable of being marked by
a focused energy beam.
25
6. A cold-shrink article comprising:
an elastomeric member in an expanded state, the elastomeric member comprising a
composition that comprises a fluoroelastomer and an epichlorohydrin; and
a removable core supporting the elastomeric member in the expanded state.
30

7. The cold-shrink article of claim 6, wherein the composition further comprises filler material selected from the group consisting of reinforcement-grade carbon blacks, silica-based fillers, clays, fluoroplastics, metal oxides, and combinations thereof.
- 5 8. The cold-shrink article of claim 6, wherein the elastomeric member exhibits a permanent set at 100°C of less than about 35%.
9. The cold-shrink article of claim 6, wherein the elastomeric member, when held at a temperature of 150°C, exhibits an elongation at break of at least about 200%.
- 10 10. The cold-shrink article of claim 6, wherein the cold-shrink article includes a plurality of elastomeric members having walls that define elongate cavities through each elastomeric member, the cavities in communication with each other.
- 15 11. The cold-shrink article of claim 6, and further comprising:
an energy-beam induced identifier on an external surface of the elastomeric member, wherein the composition further comprises an energy beam absorbent.
- 20 12. A method comprising:
blending components to form a composition, the components comprising a fluoroelastomer and an epichlorohydrin;
forming the composition into an elastomeric article;
expanding at least a portion of the elastomeric article; and
25 inserting a removable core into the expanded portion of the elastomeric article.

1/3

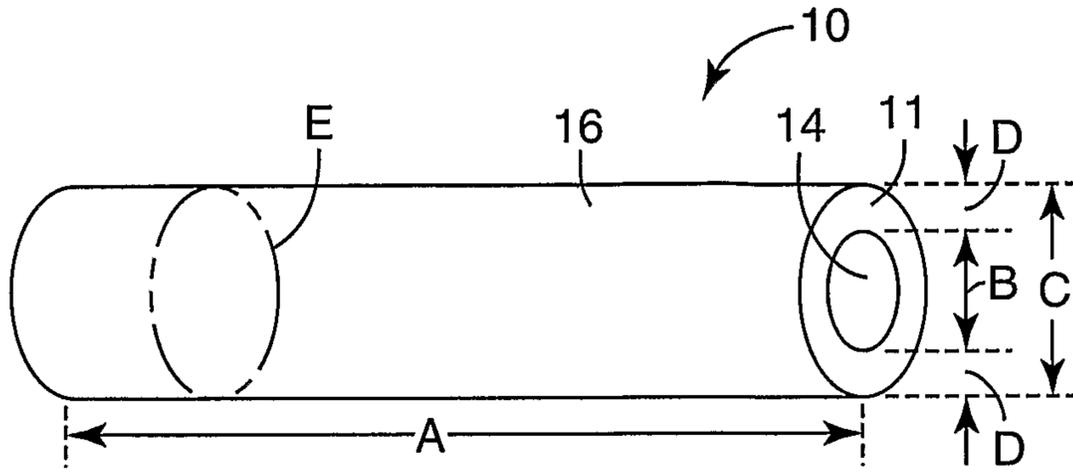


Fig. 1

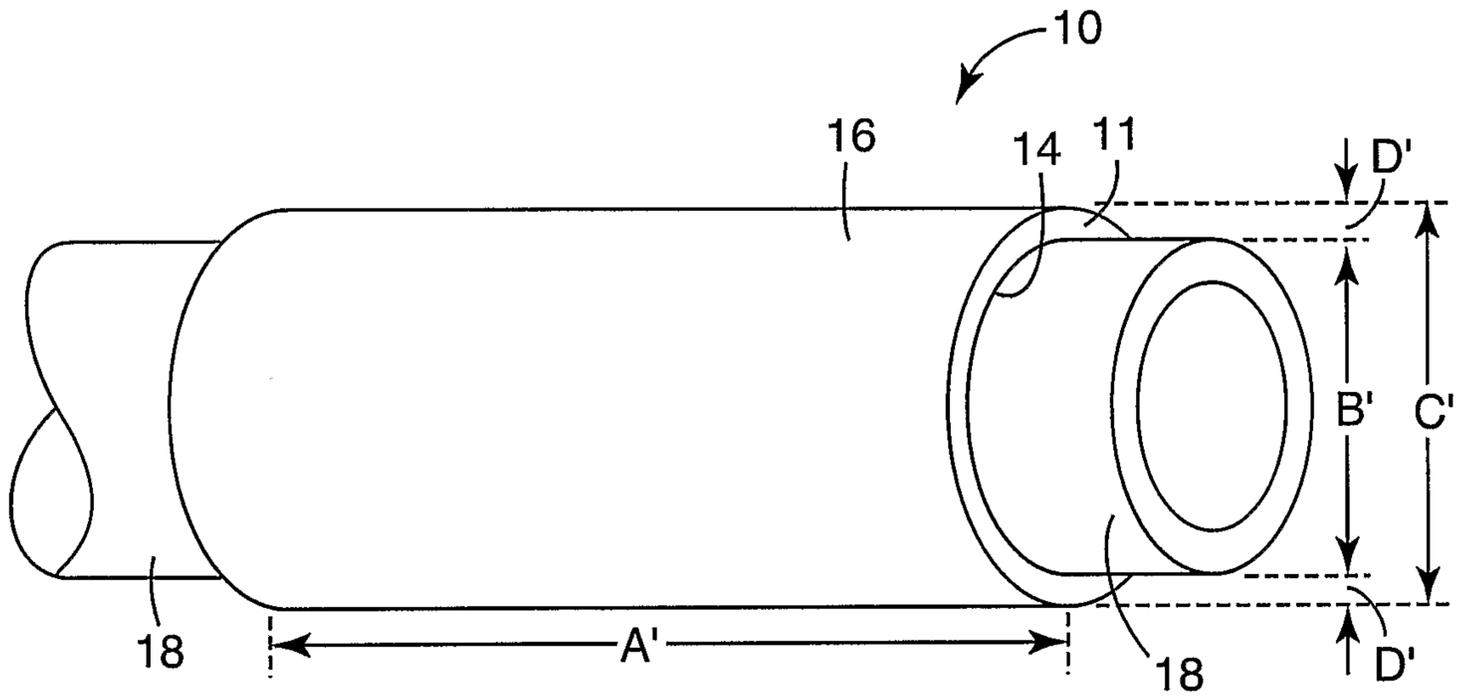


Fig. 2

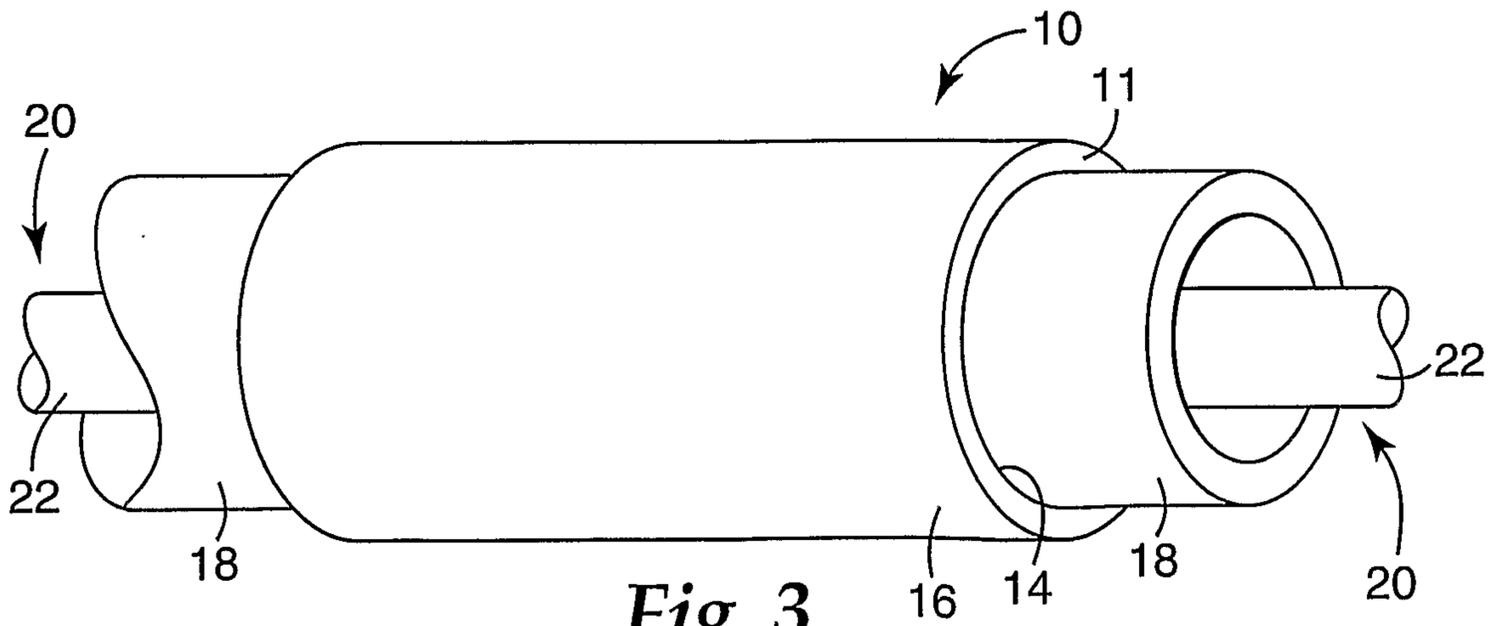


Fig. 3

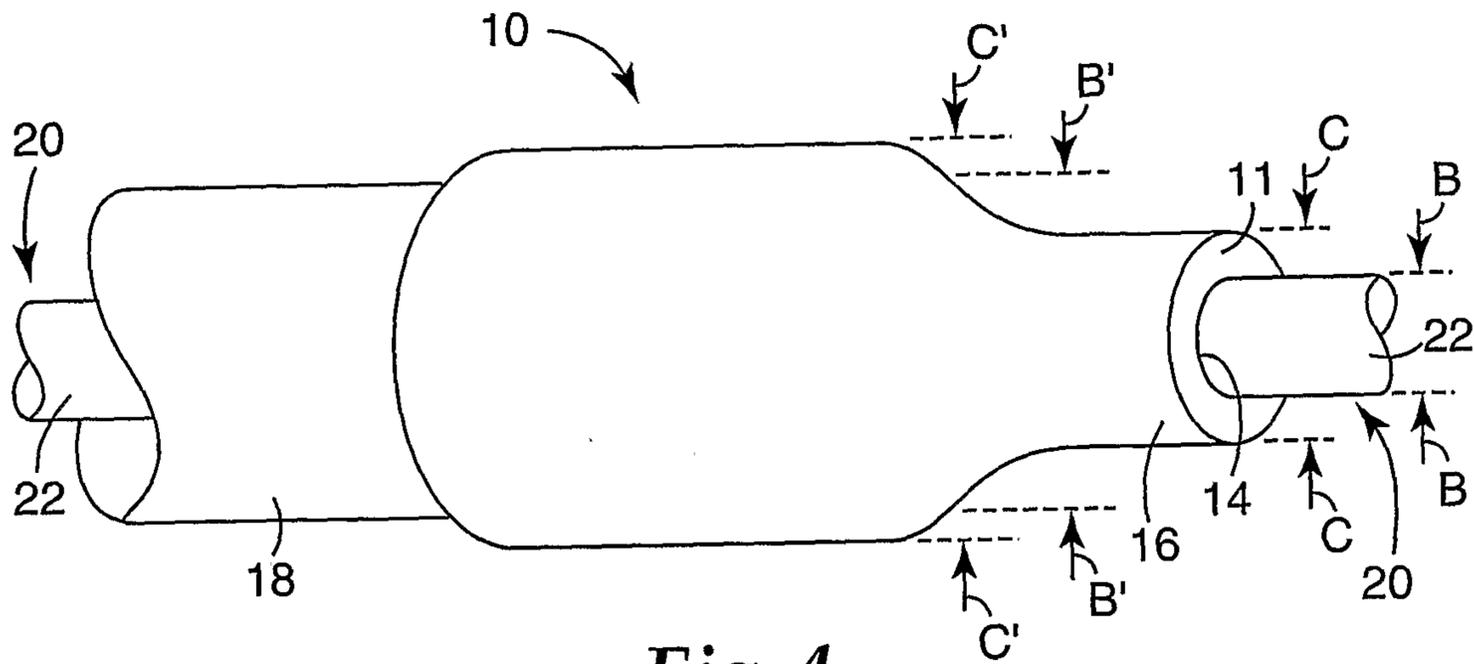


Fig. 4

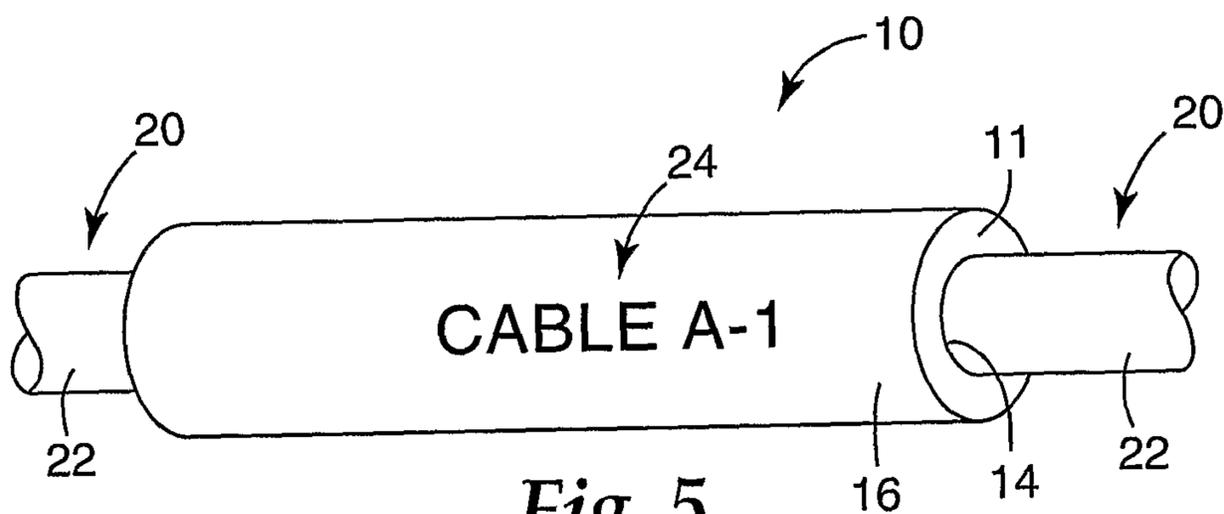


Fig. 5

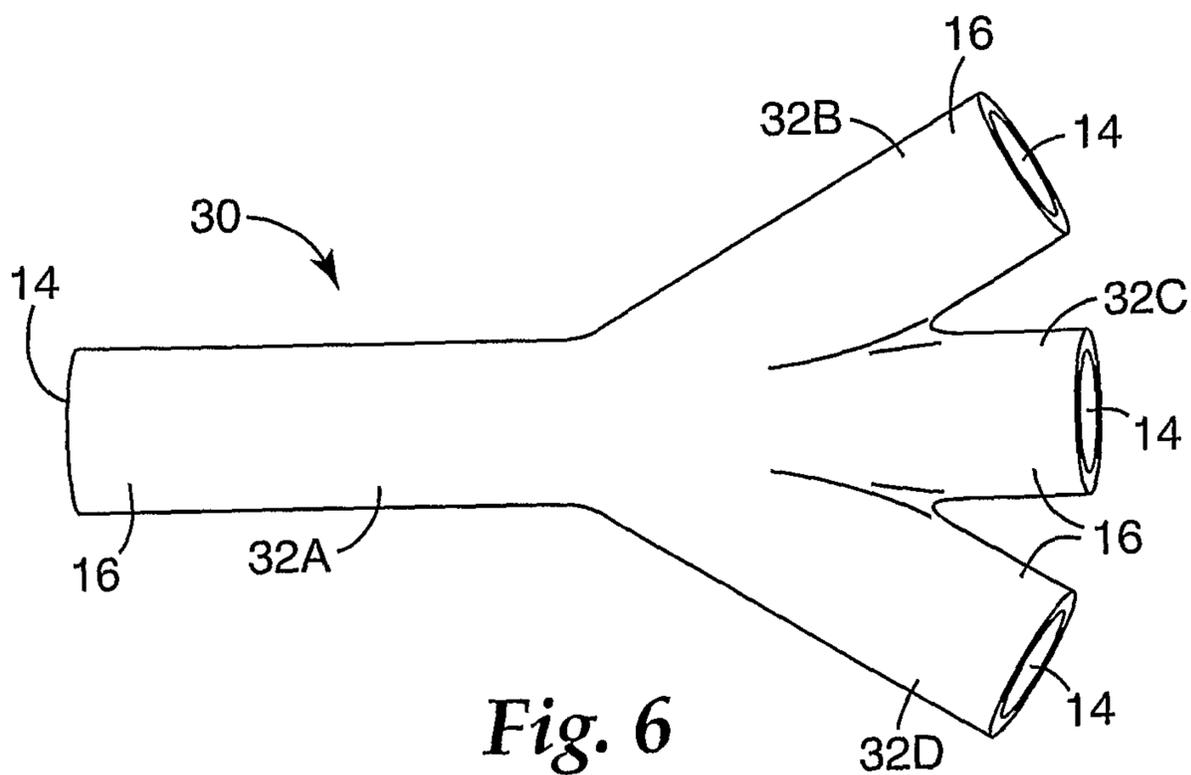


Fig. 6

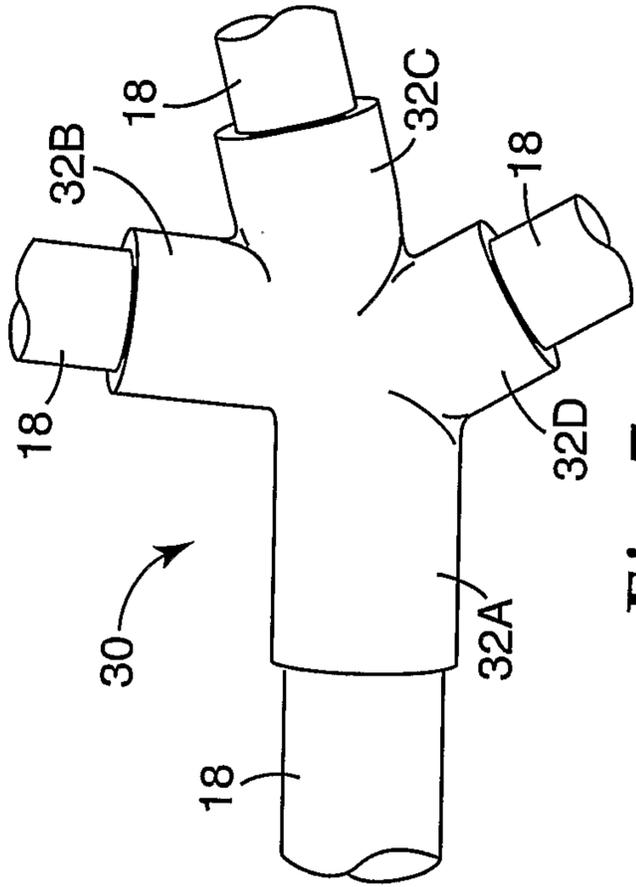


Fig. 7

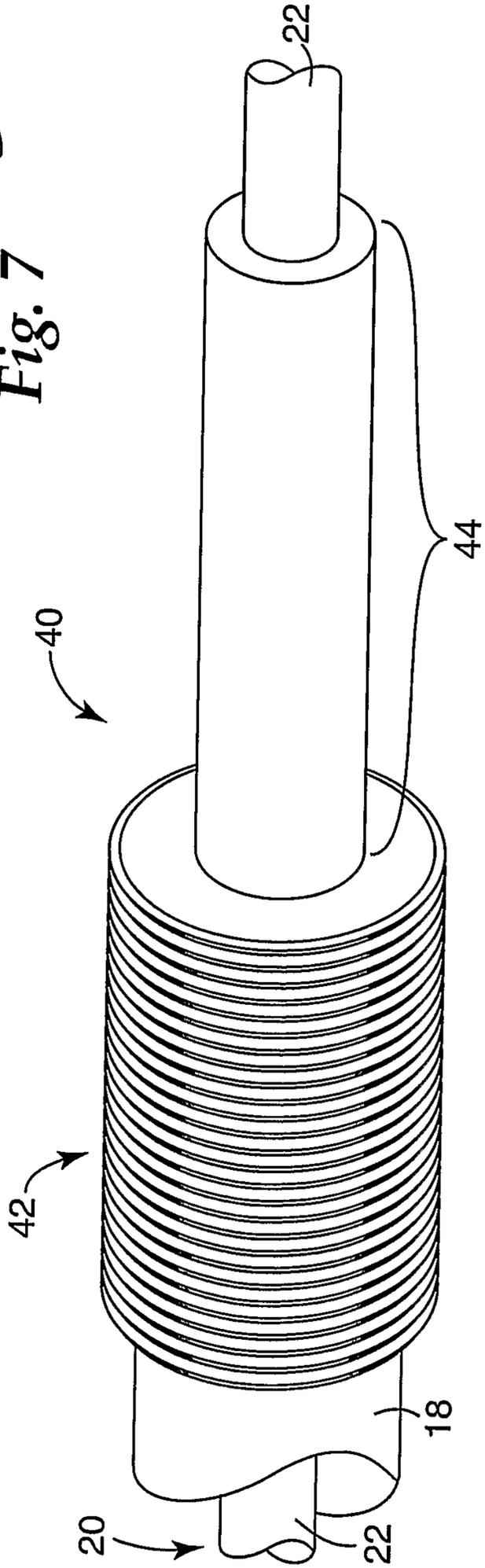


Fig. 8

