



(72) GROTH, RICHARD J., US

(72) ZHAO, YONGFU, US

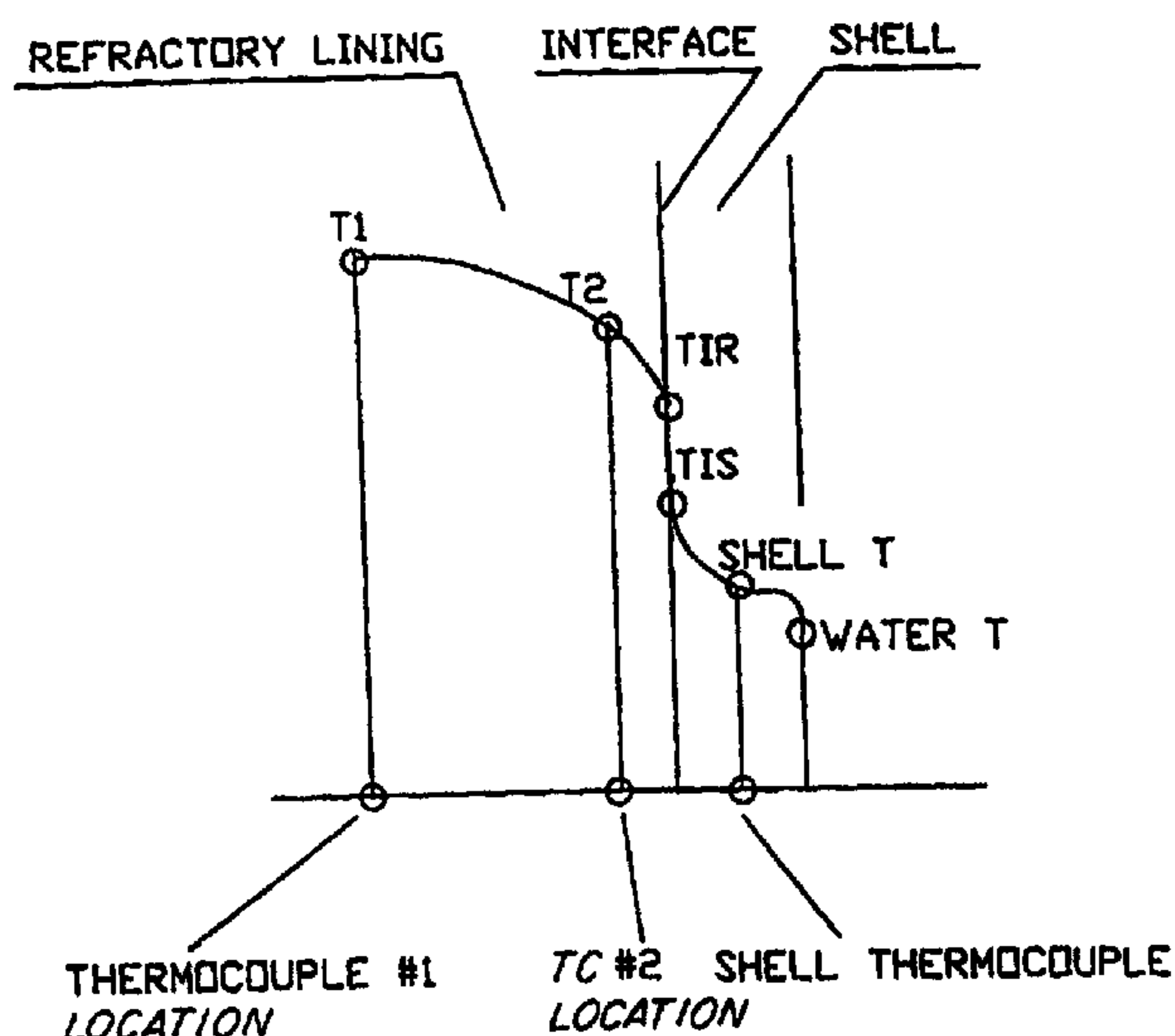
(71) USX ENGINEERS AND CONSULTANTS, INC., US

(51) Int.Cl.⁷ G01N 25/72, G01N 25/20, G01K 7/04, G01N 25/00

(30) 1997/09/26 (08/938,760) US

(54) **PROCEDE DE CONTROLE DE L'USURE ET D'ALLONGEMENT
DE LA DUREE DE VIE DU GARNISSAGE REFRACTAIRE
D'UN HAUT FOURNEAU**

(54) **METHOD FOR MONITORING THE WEAR AND EXTENDING
THE LIFE OF BLAST FURNACE REFRACTORY LINING**



(57) L'invention concerne un procédé de contrôle en direct de l'usure du garnissage réfractaire d'un haut fourneau. Ce procédé consiste à déterminer la ligne d'usure du garnissage à partir de signaux transmis par des sondes thermiques disposées par groupes, par exemple le groupe (10, 12, 14), le groupe (16, 18, 20), le groupe (22, 24, 26), logés de manière espacée sur toute l'épaisseur du garnissage réfractaire. D'autres procédés de l'invention comprennent: un procédé de détermination de l'épaisseur d'une couche protectrice d'un fond de poche en métal solidifié formé sur le foyer réfractaire, un procédé de détermination des conditions de transfert thermique entre un garnissage réfractaire et une carcasse métallique d'un haut fourneau, et entre la carcasse métallique et une eau de refroidissement appliquée à la carcasse, ainsi qu'un procédé d'allongement de la durée de vie du garnissage réfractaire.

(57) A method is provided for on-line monitoring of the wear of a refractory lining of a blast furnace. The method includes determining the wear line of the lining from signals provided by temperature probes located in groups, e.g., group (10, 12, 14), group (16, 18, 20), group (22, 24, 26), embedded at spaced locations across the thickness of the refractory lining. Other methods disclosed include: a method of determining the thickness of a protective layer of solidified metal skull formed on the refractory hearth, a method of determining the conditions of heat transfer between a refractory lining and a metal shell of a blast furnace and between the metal shell and cooling water applied to the shell, and a method of extending the life of refractory lining.



PCT

WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau

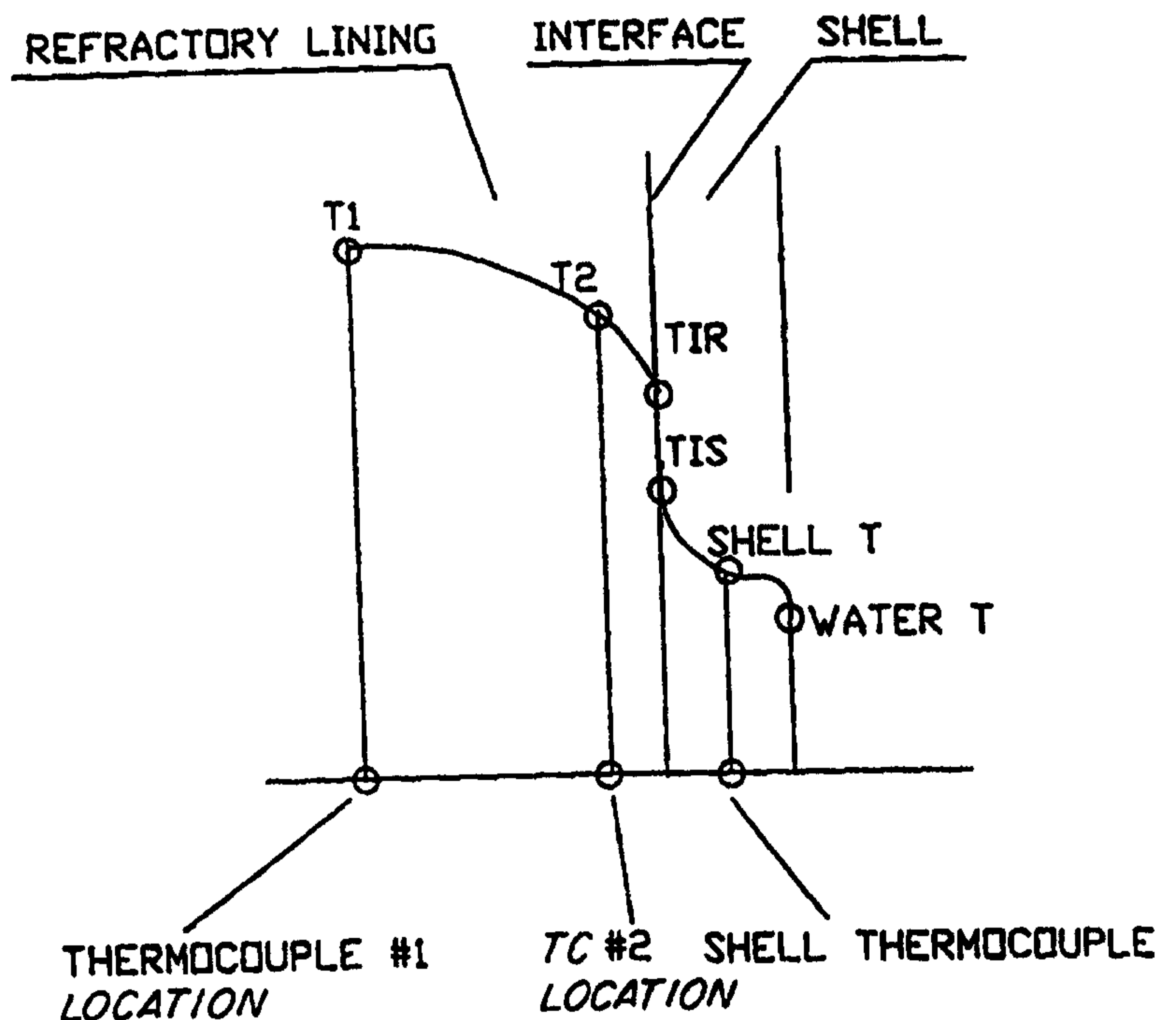
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶ : G01N 25/72, 25/00, 25/20, G01K 7/04	A1	(11) International Publication Number: WO 99/17106 (43) International Publication Date: 8 April 1999 (08.04.99)
<p>(21) International Application Number: PCT/US98/19582</p> <p>(22) International Filing Date: 17 September 1998 (17.09.98)</p> <p>(30) Priority Data: 08/938,760 26 September 1997 (26.09.97) US</p> <p>(71) Applicant: USX ENGINEERS AND CONSULTANTS, INC. [US/US]; 600 Grant Street, Pittsburgh, PA 15219 (US).</p> <p>(72) Inventors: GROTH, Richard, J.; 2315 McNary Boulevard, Pittsburgh, PA 15235 (US). ZHAO, Yongfu; 551 Deauville Drive #5, Monroeville, PA 15146 (US).</p> <p>(74) Agent: RIESMEYER, William, F., III; USX Corporation, Room 1500, 600 Grant Street, Pittsburgh, PA 15219 (US).</p>	<p>(81) Designated States: BR, CA, MX.</p> <p>Published <i>With international search report.</i></p>	

(54) Title: METHOD FOR MONITORING THE WEAR AND EXTENDING THE LIFE OF BLAST FURNACE REFRACTORY LINING

(57) Abstract

A method is provided for on-line monitoring of the wear of a refractory lining of a blast furnace. The method includes determining the wear line of the lining from signals provided by temperature probes located in groups, e.g., group (10, 12, 14), group (16, 18, 20), group (22, 24, 26), embedded at spaced locations across the thickness of the refractory lining. Other methods disclosed include: a method of determining the thickness of a protective layer of solidified metal skull formed on the refractory hearth, a method of determining the conditions of heat transfer between a refractory lining and a metal shell of a blast furnace and between the metal shell and cooling water applied to the shell, and a method of extending the life of refractory lining.



METHOD FOR MONITORING THE WEAR AND EXTENDING THE LIFE
OF BLAST FURNACE REFRACTORY LINING

Technical Field

The present invention is of a method for extending the life of a blast furnace refractory lining and, and particularly to a method which includes on-
5 line monitoring of campaign maximum and current average signals from a plurality of thermocouples embedded at spaced locations in the refractory lining and from a plurality of thermocouples embedded at spaced locations in a metal shell of the furnace, calculating from those
10 signals the wear line of the refractory lining and the thickness of a layer of solidified metal skull formed on an inner surface of the refractory, and then determining the conditions of heat transfer at the shell e.g. whether or not a gap has formed between the
15 refractory and the shell and whether or not water cooling of the shell is sufficient.

Background Art

The iron blast furnace typically is constructed of a metal shell with a refractory brick
20 lining. The life of the refractory brick lining determines the length of time that the furnace can be kept in operation before the furnace must be shut down for installation of new refractory. Longer refractory life decreases refractory cost and increases the
25 productivity achieved from the furnace. More expensive refractory brick have been used to extend the length of a furnace "campaign". Grouting or gunning of refractory material between the refractory brick and the metal shell has also been used as a repair measure
30 to close the gaps which sometimes form between the shell and the brick. Gaps between the brick and shell decrease heat transfer and cause increased wear of the refractory brick.

U. S. Patent 4,510793 discloses the use of a ceramic bar in a furnace wall which wears with the lining. The wear of the bar and the lining is detected ultrasonically by generating ultrasonic pulses in the bar and detecting the reflection of the pulses from the worn inner end of the bar.

Japanese Published Application 1-290709 discloses thermocouples embedded in the refractory on the bottom and bottom side wall part of a blast furnace. From the temperatures measured by the thermocouples, calculations are made to determine the state of packing of coke in the core of the furnace. When the packing of coke is inadequate for preferential flow of molten iron in the central part of the furnace, changes are made in the amount, grain size or hot characteristics of the coke charged to the furnace.

U. S. Patent 4,358,953, Horiuchi et al, discloses a method of monitoring the wear of refractory lining blast furnace walls by sensing temperatures at different points across the thickness of the refractory and analyzing the time delay between trigger signals representing internal phenomena of the furnace and the temperature probe output signals. This patent also describes a prior art method of determining the degree of wear from one dimensional heat transfer analysis. An apparatus for sensing temperature distribution in the refractory is also disclosed. A similar apparatus is disclosed in U. S. Patent 4,412,090, Kawate et al, and in U. S. Patent 4,442,706, Kawate, et al.

It is also known to use one-dimensional and two-dimensional heat transfer calculations to refractory temperature distributions and then later compare with measured temperatures to estimate remaining refractory and skull thickness. A method of

this type is disclosed in a literature paper entitled "Evaluation of Mathematical Model for Estimating Refractory Wear and Solidified Layer in the Blast Furnace Hearth", by Suh Young-Keun et al, ISIJ, 1994, Pages 223-228. However, no method previously existed for using measured temperatures to calculate the thickness of the brick and skull directly in a manner which considers interaction between measured temperatures at all locations in a vertical plane simultaneously. Also, no previous method existed that could be used on-line without human intervention to signal problems with gap formation, inefficient cooling on the shell, and to discern the irregular "elephant-shaped" erosion profiles and "bowl-shaped" erosion profiles, so as to enable corrective measures to be taken during furnace operation in order to extend the life of the refractory.

Other patents related to the measurement of wall thickness and/or temperature include U. S. 2,264,968; 2,987,685; 2,994,219; 3,018,663; 3,307,401; 3,512,413; 4,217,544; 4,248,809; and 4,539,846.

Disclosure of the Invention

This invention is of a method for extending the life of refractory lining the interior of a metal shell of a blast furnace. The method includes placing thermocouples in the refractory at a plurality of spaced locations and monitoring the signals produced by the thermocouples during furnace operation. An average of the temperature readings at each thermocouple location is determined periodically and recorded. The maximum temperature reading since the beginning of a campaign of the furnace is also determined and recorded. From the current average and campaign

maximum temperature readings from the thermocouple signals, a determination is made on-line, i.e. during furnace operation, as to whether a protective solidified layer of metal skull exists on the inner face of the refractory and the thickness of the skull. If no protective layer of solidified metal skull exists, or if it is of insufficient thickness, a determination is made as to whether a gap exists between the refractory and a metal shell of the furnace and the location of the gap or whether cooling of the metal shell is insufficient. Steps are then taken during furnace operation, based on the results of such calculations, to fill such gaps with refractory, to re-establish sufficient cooling of the shell or to form a protective solidified layer of sufficient thickness on the inner surface of the refractory. The method of this invention also includes performing a moving boundary calculation directly from measured temperatures at all thermocouple locations in a vertical plane simultaneously to discern irregular erosion profiles, e.g. "elephant-shaped" and "bowl-shaped" erosion of the refractory.

Brief Description of the Drawings

Figure 1 is a cross-section of one-half of a blast furnace hearth showing the arrangement of thermocouples in the refractory and metal shell of the hearth area of the furnace.

Figure 2 is a schematic side elevation view of the tap hole area of a blast furnace illustrating the placement of thermocouples in that area.

Figure 3 is a flow diagram of steps taken in accordance with the method of this invention.

Figure 4 is graphic representation of blast furnace hearth refractory lining wear and solidified metal skull formation determined according to the method of this invention.

5 Figure 5 is a schematic representation of two refractory-metal shell interface temperatures, TIR and TIS, determined by two different analyses, with TIR substantially greater than TIS, indicating the presence of a gap between the refractory and metal shell.

10 Figure 6 is a schematic representation of the two refractory-metal shell interface temperatures, TIR and TIS, with TIS substantially greater than TIR, indicating insufficient cooling of the metal shell.

15 Modes for Carrying Out the Invention

Referring to Figure 1, thermoprobes for measuring temperature, preferably thermocouples, are embedded in the refractory and the metal shell of a blast furnace in the hearth area. Thermocouples 10 and 20 12 are placed in the refractory sidewall of the hearth at two known positions across the thickness in a radial direction of the furnace. At least one thermocouple 14 is embedded at a known position in the metal shell in line with thermocouples 10 and 12 in the refractory. 25 This first group of thermocouples is preferably placed at the elevation of a tap hole of the furnace and in the vicinity of the tap hole. A second group of thermocouples 16, 18 and 20 is placed at substantially vertically aligned positions with the first group at an 30 elevation above the top surface 21 of the hearth pad. A third group of thermocouples 22, 24 and 26 is placed at substantially vertically aligned positions with respect to the first two groups at an elevation in the

corner of the hearth sidewall where the sidewall meets the hearth pad. Thermocouple groups are placed in the floor of the hearth i.e. in the heart pad, at two known elevations with their hot junctions vertically aligned. One pair of thermocouples 28 and 30 is placed in the centerline of the furnace. A second pair of thermocouples 32 and 34 is placed one-third of the way to the inside of the metal shell at the hearth sidewall. A third pair, 36 and 38 is placed two-thirds of the distance to that location. It is preferred that thermocouples in this arrangement be placed spaced locations around the periphery of the furnace, with thermocouple coverage concentrated in the areas of the potentially highest wear such as around the tap hole.

Referring to Figure 2, the placement of thermocouples around the tap hole area of the furnace is illustrated more specifically. Two groups of thermocouples 40 and 42 are located on either side of the tap hole at about the tap hole elevation. These thermocouples may be in-line in a horizontal direction normal to the plane of the drawing or spaced perhaps spaced about four inches (10 cm) from each other in the vertical direction as shown in Figure 2. At an intermediate elevation above the top surface of the hearth pad, five groups of thermocouples 44, 46, 48, 50 and 52 are located in the tap hole area. Another five groups of thermocouples 54, 56, 58, 60 and 62 are located at about the elevation of the corner of the sidewall and the top surface of the hearth pad. The thermocouples in the latter two groups may be spaced about two feet (0.6096 meters) apart in a horizontal direction in the plane of Figure 2.

As shown in Figure 3, the readings taken from the plurality of thermocouples embedded in the

refractory and shell are used as input in a computer program to carry out a sequence of heat transfer calculations. The current average and campaign maximum temperatures from these thermocouples are fed into a heat transfer model that translates these inputs into a heat flux. From this information, a one-dimensional heat transfer model calculates the location of the hot metal solidification isotherm, for example 2100°F for blast furnace iron. The solidification isotherm which results from this calculation is used as the initial boundary in a two-dimensional heat transfer model. The two-dimensional heat transfer program iterates until a final boundary of the solidification isotherm is determined by minimizing the difference between the measured and predicted temperatures at each measuring point. The two-dimensional heat transfer calculations are made on the basis of the following two equations:

$$J = \iint \left[\left(\frac{\partial T}{\partial x} \right)^2 + \left(\frac{\partial T}{\partial r} \right)^2 \right] dx dr$$

20

$$\frac{\partial J}{\partial T} = 0$$

where T is the temperature at the location where the radius co-ordinate from the centerline of the furnace is r, and the height co-ordinate is x. By using the average and the maximum temperatures, the sequence of heat transfer calculation provides two solidification isotherm interfaces, I_h and I_c, respectively, as shown in Figure 4. The interface I_h is closer to the hot side as compared with I_c. The isotherm interface I_c, which is closer to the cold side represents the wear profile of the refractory lining,

30

while I_c represents the skull formation between hot metal and the lining. The distance between I_h and I_c represents the thickness of the solidified skull. The presence of the skull prevents the lining from the direct attack by hot metal and enables extending the life of the blast furnace hearth. The beginning of an irregular erosion profile in the corner are is illustrated in Figure 4, where an "elephant-shaped" erosion is beginning to form as indicated by a greater erosion 62 in the corner than the erosion 64 in the adjacent sidewall. The method of this invention is able to determine "elephant-shaped" irregular erosion in an on-line calculation using a moving boundary calculation which considers interaction between measured temperatures at all locations in a vertical plane simultaneously.

The campaign maximum thermocouple readings represent the ultimate erosion profile of the refractory brick. Generally, the campaign maximum readings correspond to the highest heat flux and minimum calculated refractory thickness. These readings are then applicable to determine the critical isotherm corresponding to the actual erosion profile of the brick, I_c .

The average thermocouple readings represent the current condition within the hearth. The last hour's average temperatures recorded at each location is used to determine the current position of the critical isotherm and to calculate TIR and TIS, for purposes described hereinbelow, at all locations in the furnace hearth. The position of the current critical isotherm, I_h , relative to the isotherm corresponding to the maximum calculated refractory erosion profile, I_c , relates the presence and relative thickness of the

protective skull on the inside surface of the refractory at each location. In general, when the current average thermocouple readings approach the campaign maximum temperatures, $T_c \sim T_h$, this indicates
 5 that there is presently no protective skull layer on the inside surface of the brick.

After calculating the critical isotherms, at each location, calculated values of TIR and TIS are used to determine the presence of a gap between the
 10 shell and the hearth brickwork and the presence of a build-up on the furnace shell.

$$TIR = T_2 - \left[\frac{(L_1 - L_2)k_1(T)}{k_1(T)} \right] \left(\frac{T_1 - T_2}{L_2 - L_1} \right)$$

15

$$TIS = T_1 + \left[\frac{(L_2 - L_1)k_1(T)}{k_1(T)} \right] \left(\frac{T_1 - T_2}{L_2 - L_1} \right)$$

Where

TIR = Calculated shell interface temperature
 20 as calculated from hot side

TIS = Calculated shell interface temperature
 as calculated from water cooled side

T_1 = Measured temperature from location 1,
 see Figures 5 and 6

25 T_2 = Measured temperature from location 2,
 see Figures 5 and 6

T_s = Measured shell temperature

L_i = Relative position of shell interface
 as referenced from the coordinate system

L_1 = Relative position of thermocouple 1 as
 referenced from coordinate system
 L_2 = Relative position of thermocouple 2 as
 referenced from the coordinate system
 5 L_s = Relative position of shell
 thermocouple as referenced from the coordinate system
 $k_1(T)$ = Thermal conductivity as a function of
 temperature between locations 1 and 2
 $k_i(T)$ = Thermal conductivity between shell
 10 interface and location 2
 $k_s(T)$ = Thermal conductivity of the shell

Given these calculated values, the program
 then uses logical comparison statements to indicate
 15 potential warning conditions and directs appropriate
 action to alleviate any problems indicated.

As shown in Figure 5, TIR and TIS are
 calculated and then compared to determine if a gap has
 20 formed. TIR is calculated according to the formula
 above from temperatures T_1 and T_2 at thermocouple
 locations 1 and 2 in Figure 5 (which correspond, for
 example, to thermocouples 10 and 12 in Figure 1). TIS
 is calculated using the formula above from temperatures
 25 T_s , T_1 and T_2 temperatures (where T_s corresponds to
 thermocouple 14 in Figure 1). The following relation
 is used for that comparison:

If $(TIR - TIS) > \text{Preset limit (50}^\circ\text{F in one}$
 30 case) , then a gap has formed between the refractory and
 the metal shell. The preset limit typically may be
 selected from within a range of from 20 to 120°F.
 Corrective action may be taken to fill the gap e.g.

with a high conductivity grout material to re-establish contact with the cooled shell.

As shown in Figure 6, TIR and TIS are
5 calculated and then compared to determine if a build-up on the shell has occurred. The following relation is used for that comparison:

If $(TIS - TIR) > \text{Preset limit (50 F in one$
10 $\text{case})$, then the water cooling on the shell is insufficient. Again the preset limit typically may be selected from within a range of from 20 to 120°F. Action may be taken to check for a problem in the water system or to determine if a potential build-up has
15 formed on the outside surface of the shell which is interfering with proper heat transfer. After determining the cause of the problem, action may be taken to remove the build-up or to re-establish proper water flow in this area to improve heat removal
20 efficiency. Conventional measures may be taken to correct these problems, for example, the shell surface may be sand blasted to remove any build-up or other measures may be taken to correct insufficient water flow or high temperature water.

25 Where there is no gap formed between the refractory and the shell and where cooling of the shell is sufficient and yet there is no solidified metal skull formed on the refractory lining of the furnace, or the thickness of the skull is insufficient to serve
30 as protection for the refractory, measures may be taken to form a solidified metal skull of sufficient thickness to serve as protection for the refractory or to form additional refractory on the surface of the lining. Such measures may take the form of injecting

or charging titanium-bearing materials into the furnace to protect the inner surface of the hearth, or reducing production and adjusting tuyere velocity to form a solidified metal skull of sufficient thickness.

5 Industrial Applicability

The invention is applicable to blast furnaces for producing iron for the steel industry as well as in blast furnaces for producing non-ferrous metals.

1. A method of monitoring the wear of a refractory lining of a blast furnace wherein the refractory lining has temperature probes embedded therein, comprising the steps of:

a. measuring temperatures at different points across the thickness of the refractory lining by the temperature probes embedded therein;

b. estimating the location of a solidification isotherm of the hot metal in said furnace using a one dimensional heat transfer approximation;

c. using the one dimensional heat transfer approximation as the initial boundary to begin a moving boundary calculation from a two dimensional heat transfer model; and

d. continuing to iterate the two dimensional heat transfer model until a final boundary of said solidification isotherm is determined by minimizing the difference between the measured temperature and a temperature predicted by said two dimensional heat transfer model at each temperature measuring point; said final boundary of the solidification isotherm indicating the position of a wear surface of the refractory lining for purposes of monitoring the wear thereof.

2. A method of determining the thickness of a protective layer of solidified metal skull formed on the refractory hearth of a blast furnace wherein the refractory hearth has temperature probes embedded at spaced locations in radial directions from the center of the furnace and at various elevations across the thickness of the floor and walls thereof, comprising the steps of:

a. periodically measuring temperatures at said spaced locations in said radial directions and across the thickness of the furnace hearth floor and walls by the temperature probes embedded therein;

b. determining the maximum temperature recorded by each temperature probe since the beginning of a campaign of

AMENDED SHEET

the furnace and the average temperature recorded by each temperature probe during a current time period;

c. analyzing the relation of said campaign maximum and current average temperatures of said temperature probes embedded in the hearth walls correlated with the radial distance between the temperature probes and the center of the furnace and the relation of said campaign maximum and current average temperatures of said temperature probes embedded in the hearth floor correlated with the elevation distance between the location of the temperature probes in the hearth floor so as to predict the location of the wear line of the refractory hearth from the location of a solidification isotherm closest to a metal shell, and to predict the location of the inner surface of a solidified metal skull lining said refractory hearth from an isotherm closest to the hot side of the furnace remote from the metal shell, and

d. determining the thickness of the protective layer of solidified metal skull from the distance between the predicted wear line of the refractory hearth and the predicted inner surface of the metal skull.

3. A method according to claim 2 wherein said analysis is carried out by estimating the location of said solidification isotherms using a one dimensional heat transfer approximation, using this approximation as the initial boundary to begin a moving boundary calculation from a two dimensional heat transfer model, and continuing to iterate the two dimensional heat transfer model until a final boundary of each solidification isotherm is determined by minimizing the difference between the measured temperature at each temperature probe location and a predicted temperature at said location based on iterations of the two dimensional heat transfer model.

4. A method of determining the conditions of heat transfer between a refractory lining and a water cooled metal shell of a blast furnace wherein at least one group

AMENDED SHEET

of temperature probes are embedded at spaced locations in a radial direction of the furnace, said group of temperature probes including at least two temperature probes located in the refractory lining and at least one temperature probe in the water cooled metal shell of the furnace, comprising the steps of:

- a. from the temperature difference between temperature probes of said group aligned in a radial direction in the refractory lining, determining the temperature at the interface between the refractory lining and the metal shell, said interface temperature being designated TIR;
- b. from the summation of the temperature of the temperature probe embedded in the metal shell and the temperature difference between temperature probes aligned in a radial direction in the refractory lining, determining a second temperature at said interface, said interface temperature being designated TIS; and
- c. comparing the values of TIR and TIS to determine the difference there between.

5. A method according to claim 4 wherein a determination is made that a gap exists between the refractory lining and said metal shell when the temperature TIR is substantially greater than the temperature TIS.

6. A method according to claim 4 wherein a determination is made that cooling of the metal shell is insufficient when the temperature TIS is substantially greater than the temperature TIR.

7. A method of extending the life of a refractory lining of a blast furnace hearth, wherein the refractory lining of said hearth has temperature probes embedded at spaced locations in radial directions from the center of the furnace hearth and at various elevations across the thickness of the floor and walls of the furnace hearth, comprising the steps of:

AMENDED SHEET

a. periodically measuring temperatures at said spaced locations in said radial directions and across the thickness of the refractory lining of the hearth by the temperature probes embedded therein;

b. determining the maximum temperature recorded by each temperature probe since the beginning of a campaign of the furnace and the average temperature recorded by each temperature probe during a current time period;

c. analyzing the relation of said campaign maximum and current average temperatures of said temperature probes embedded in the hearth walls correlated with the radial distance between the temperature probes and the center of the furnace hearth and the relation of said campaign maximum and current average temperatures of said temperature probes embedded in the hearth floor correlated with the elevation distance between the temperature probes and the floor so as to predict the location of the wear line of the refractory lining from the location of a solidification isotherm closest to a metal shell, and to predict the location of the inner surface of a protective layer of solidified metal skull lining said refractory hearth from an isotherm closest to the hot side of the furnace remote from the metal shell,

d. determining the thickness of the solidified metal skull during actual furnace operation from the distance between the wear line of the refractory lining and the inner surface of the metal skull, and

e. maintaining sufficient thickness of said protective layer of solidified metal skull during operation of said furnace to extend the life of the refractory lining of said furnace hearth.

8. A method according to claim 7 wherein said analysis is carried out by estimating the location of said solidification isotherms using a one dimensional heat transfer approximation, using this approximation as the initial boundary to begin a moving boundary calculation

AMENDED SHEET

from a two dimensional heat transfer model, and continuing to iterate the two dimensional heat transfer model until a final boundary of each solidification isotherm is determined by minimizing the difference between the measured temperature at each temperature probe location and a predicted temperature at said location based on iterations of the two dimensional heat transfer model.

9. A method according to claim 7 further comprising temperature probes embedded in a water cooled metal shell of the furnace hearth aligned at the same elevation with the temperature probes in the furnace hearth walls, and wherein said step of maintaining a protective layer includes the step of maintaining adequate heat transfer from the refractory hearth walls to the metal shell of the furnace hearth and from the metal shell to cooling water applied to the metal shell; said step of maintaining adequate heat transfer including determining a first temperature at the interface between the refractory lining of the hearth and the metal shell from the temperature difference between at least two temperature probes aligned in a radial direction in the refractory hearth walls, said first interface temperature being designated TIR; determining a second temperature at said interface from the summation of the temperature of at least one of the temperature probes embedded in the metal shell and the temperature difference between said temperature probes aligned in the same radial direction as the temperature probe in said shell, said second interface temperature being designated TIS; comparing the values of TIR and TIS to determine the difference there between; and in the event of a substantial difference between TIR and TIS taking corrective action to minimize the difference .

10. A method for making on-line determinations of irregular erosion profiles of a refractory lining of a

AMENDED SHEET

blast furnace wherein the refractory lining has temperature probes embedded therein, comprising the steps of:

- a. measuring temperatures at different points across the thickness of the refractory lining at a plurality of elevations by the temperature probes embedded in the lining;
- b. initially estimating the location of a solidification isotherm of the hot metal in the furnace; and
- c. from the initial estimated isotherm location making a moving boundary calculation to determine the final boundary by minimizing the difference between the measured temperature and a temperature predicted by said moving boundary calculation at all temperature probe locations in a vertical plane simultaneously, in order to make on-line determinations of irregular erosion profiles of said refractory lining.

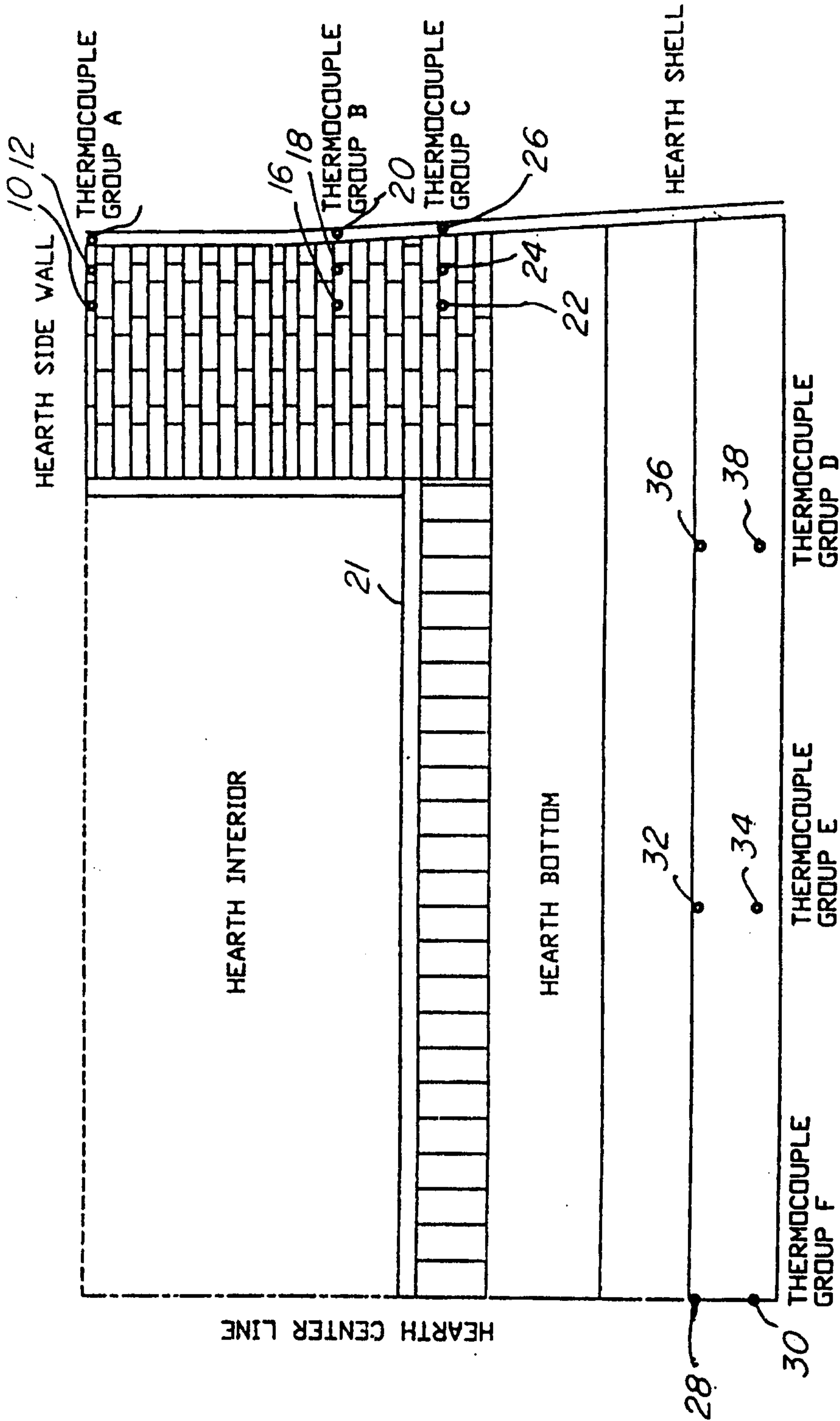
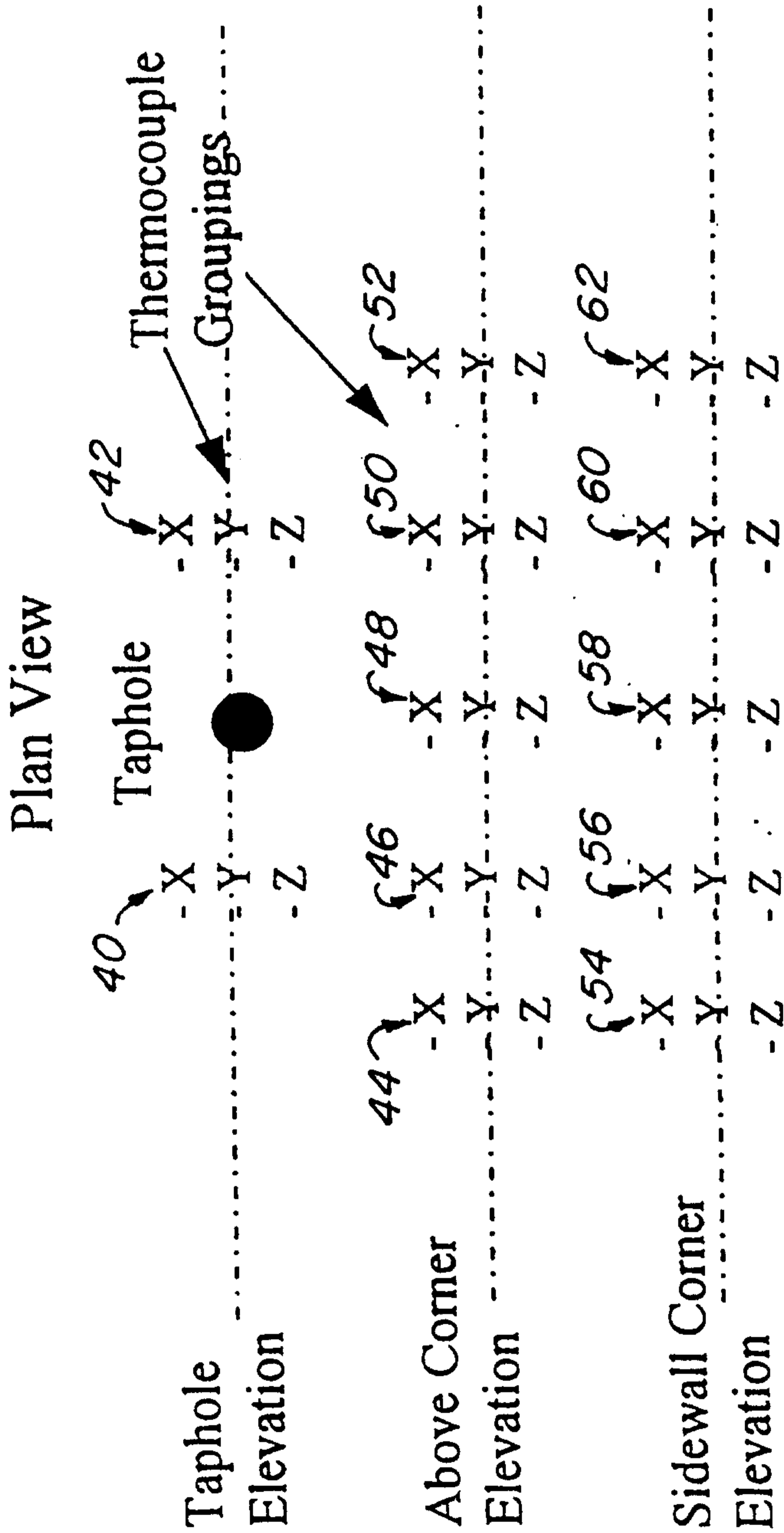


FIG. 1

Thermocouple Groupings Around Taphole



Legend	
- X	Deep Refractory TC
- Y	Shallow Refractory TC
- Z	Shell TC

FIG. 2

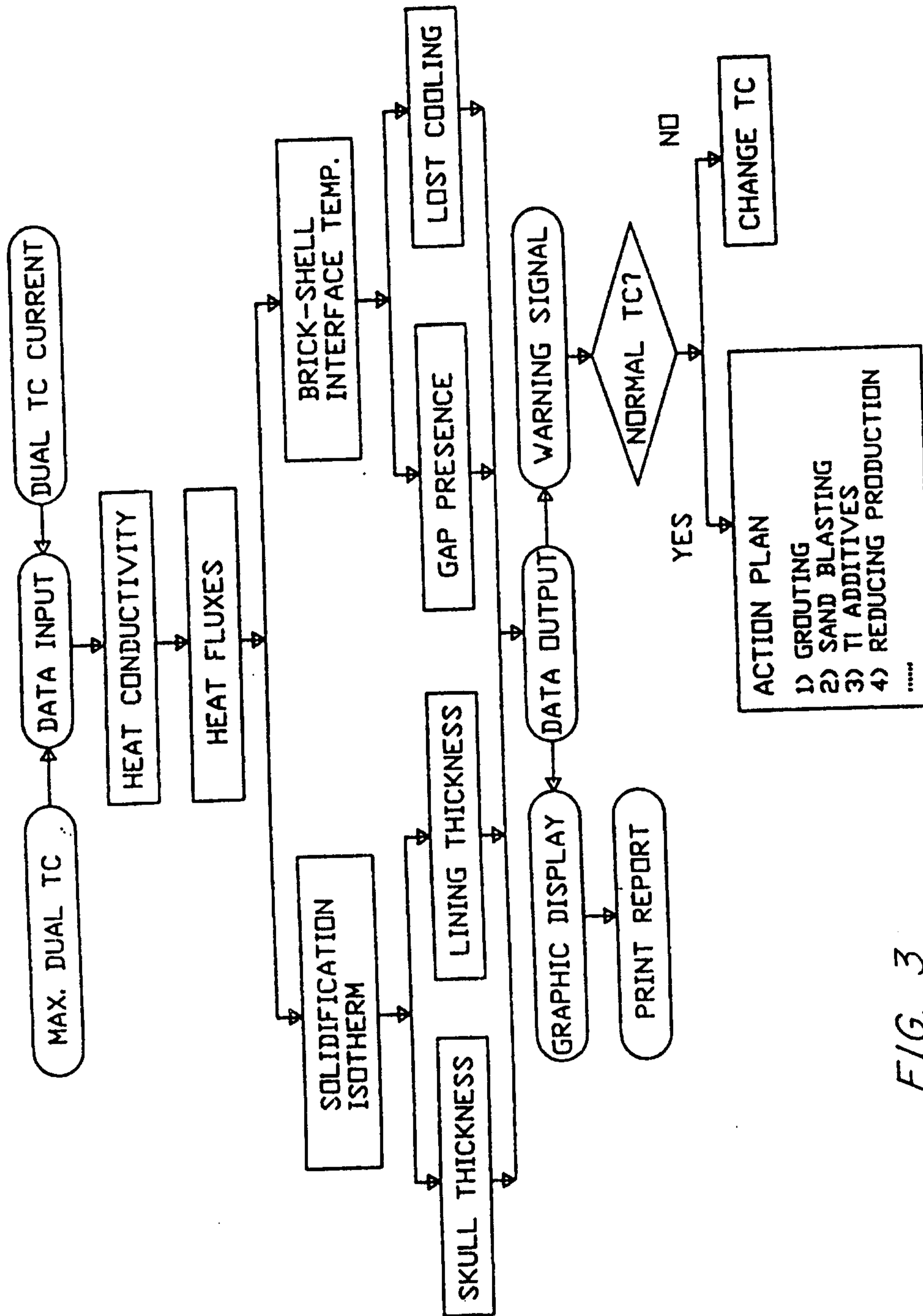


FIG. 3

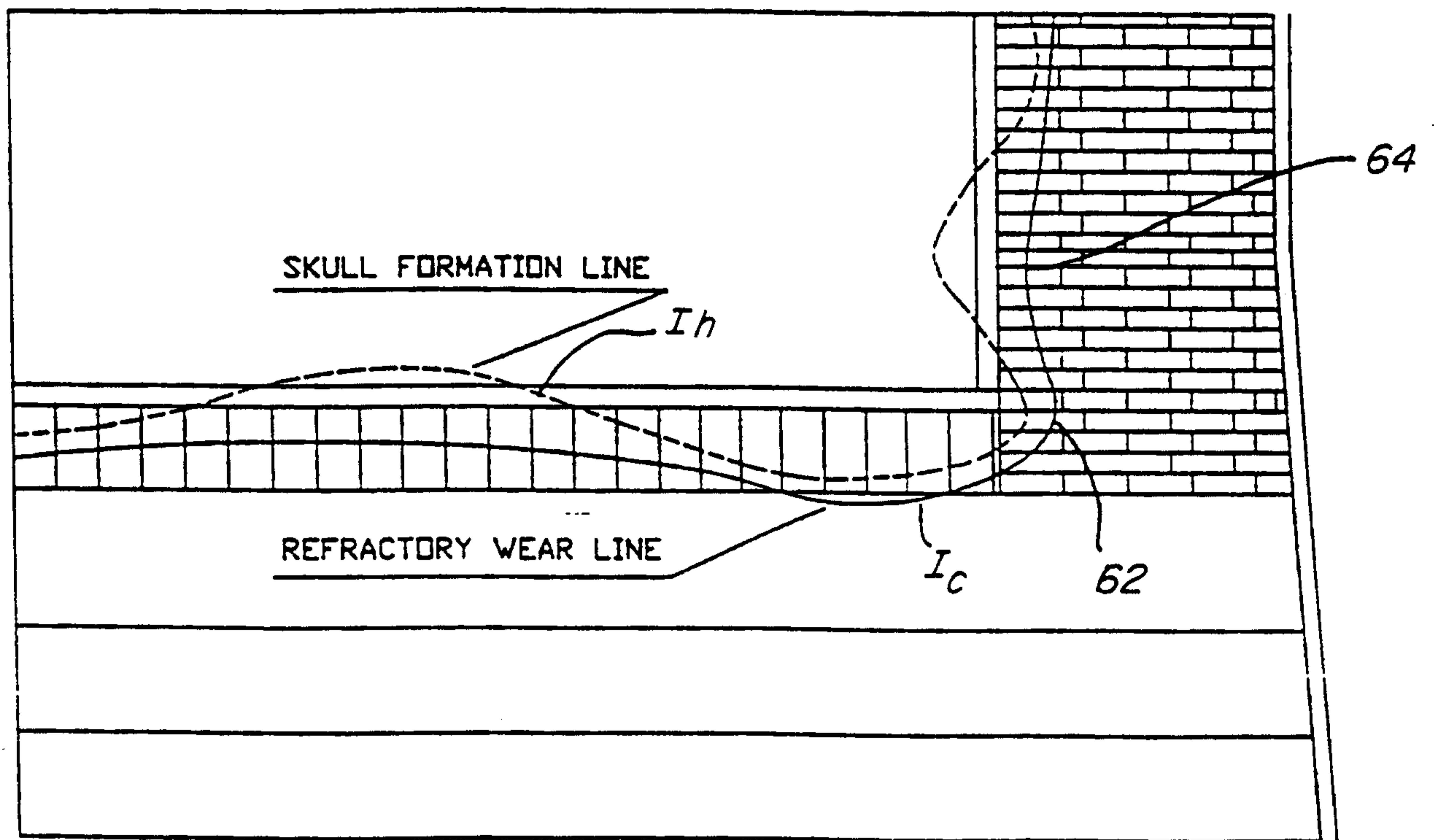


FIG. 4

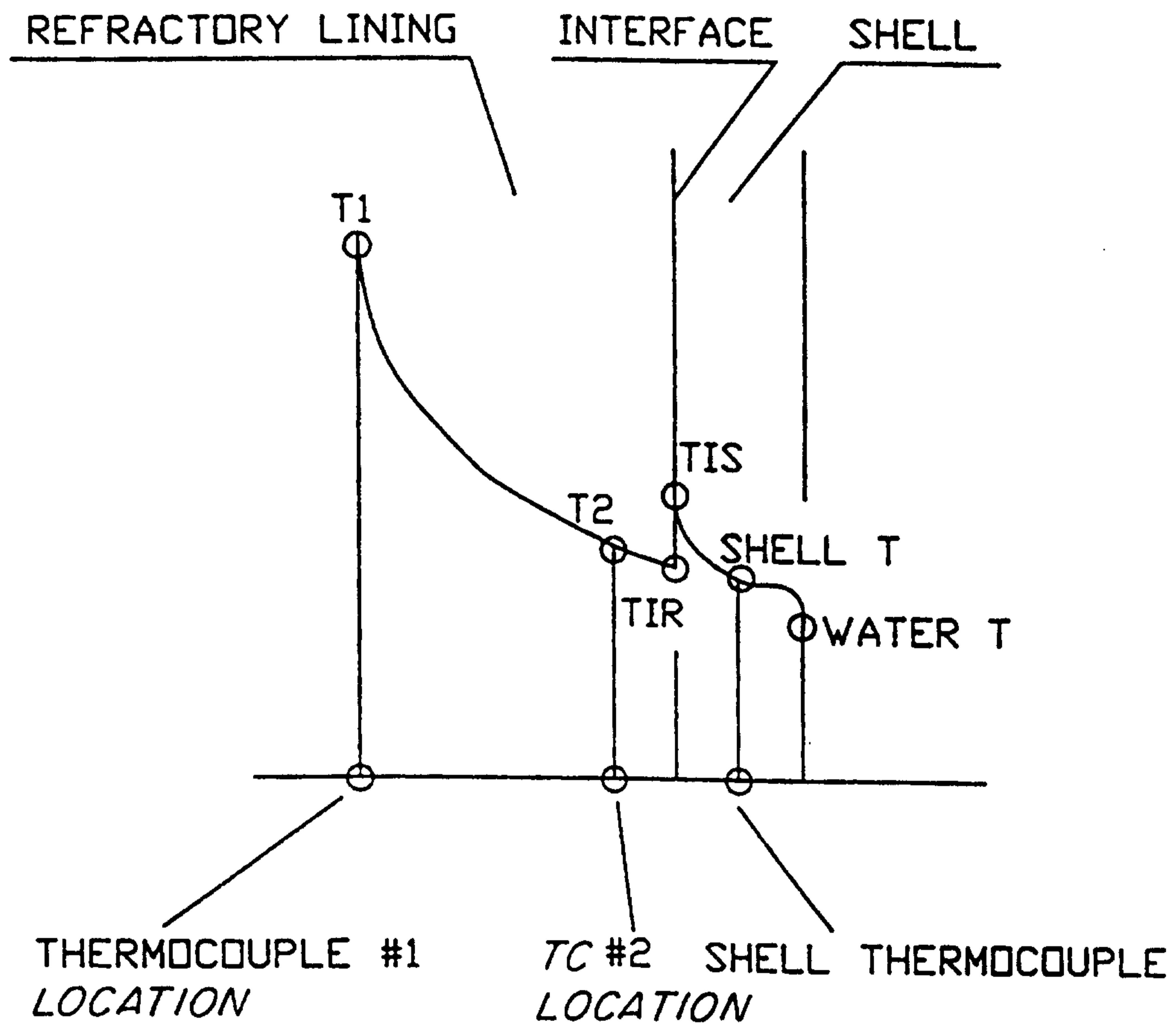


FIG. 5

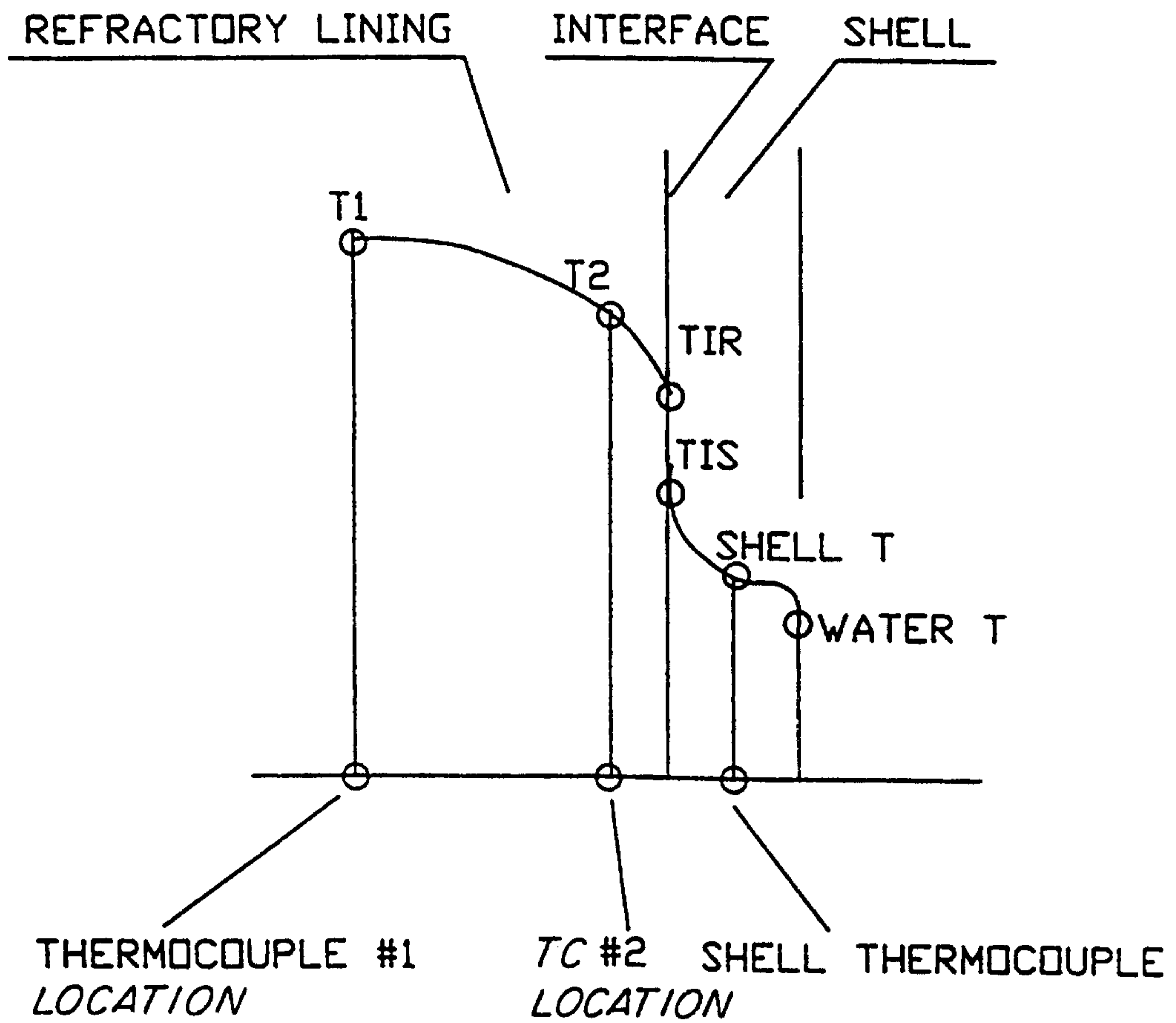


FIG. 6