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(54) **SYSTEMS AND METHODS FOR DETECTION OF LABELED MATERIALS**

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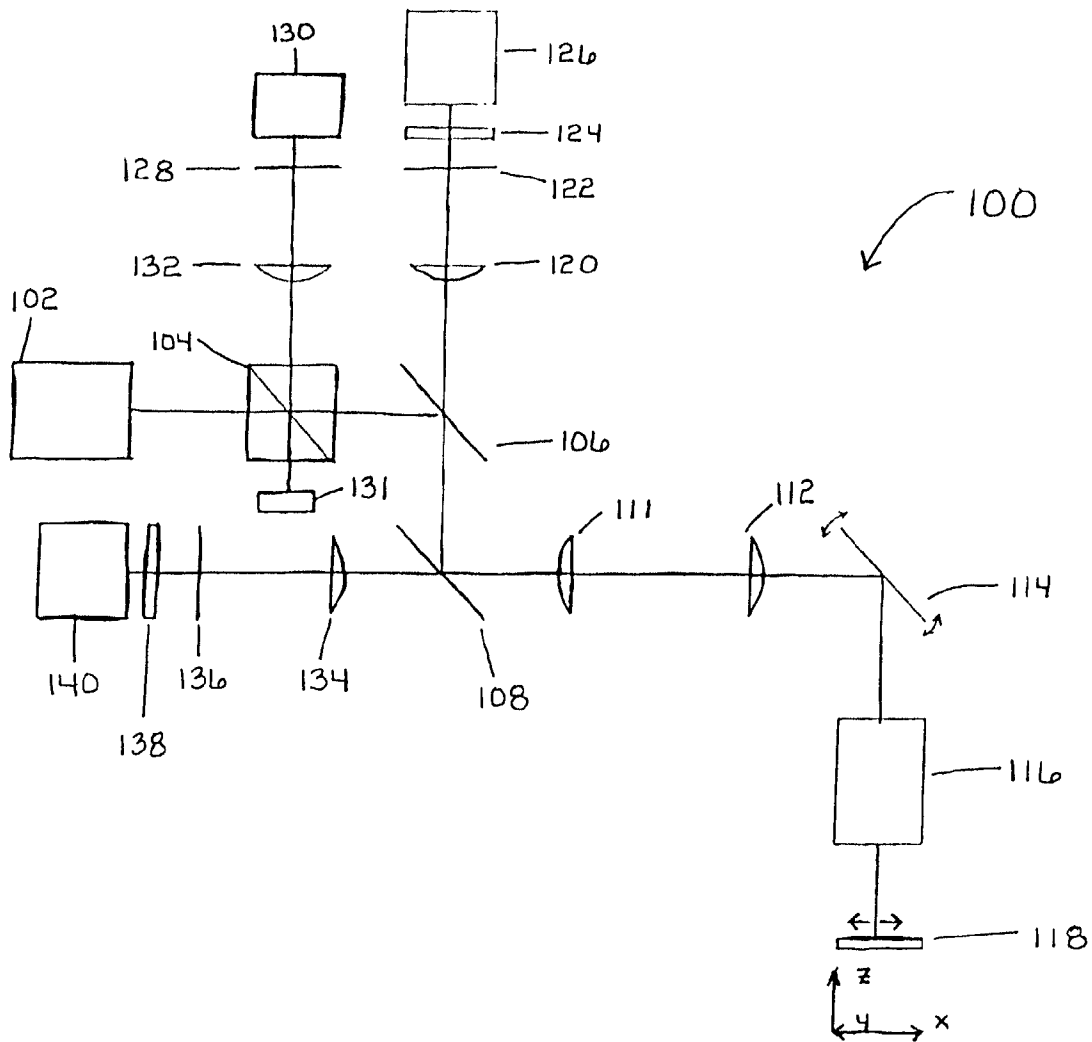
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(57) **ABSTRACT**

Labeled targets on a support synthesized with polymer sequences at known locations according to the methods disclosed in U.S. Pat. No. 5,143,854 and PCT WO 92/10092 or others, can be detected by exposing marked regions of sample to radiation from a source and detecting the emission therefrom, and repeating the steps of exposition and detection until the sample is completely examined.

Related U.S. Application Data

(63) Continuation of application No. 09/295,214, filed on Apr. 21, 1999, now Pat. No. 6,207,960, which is a



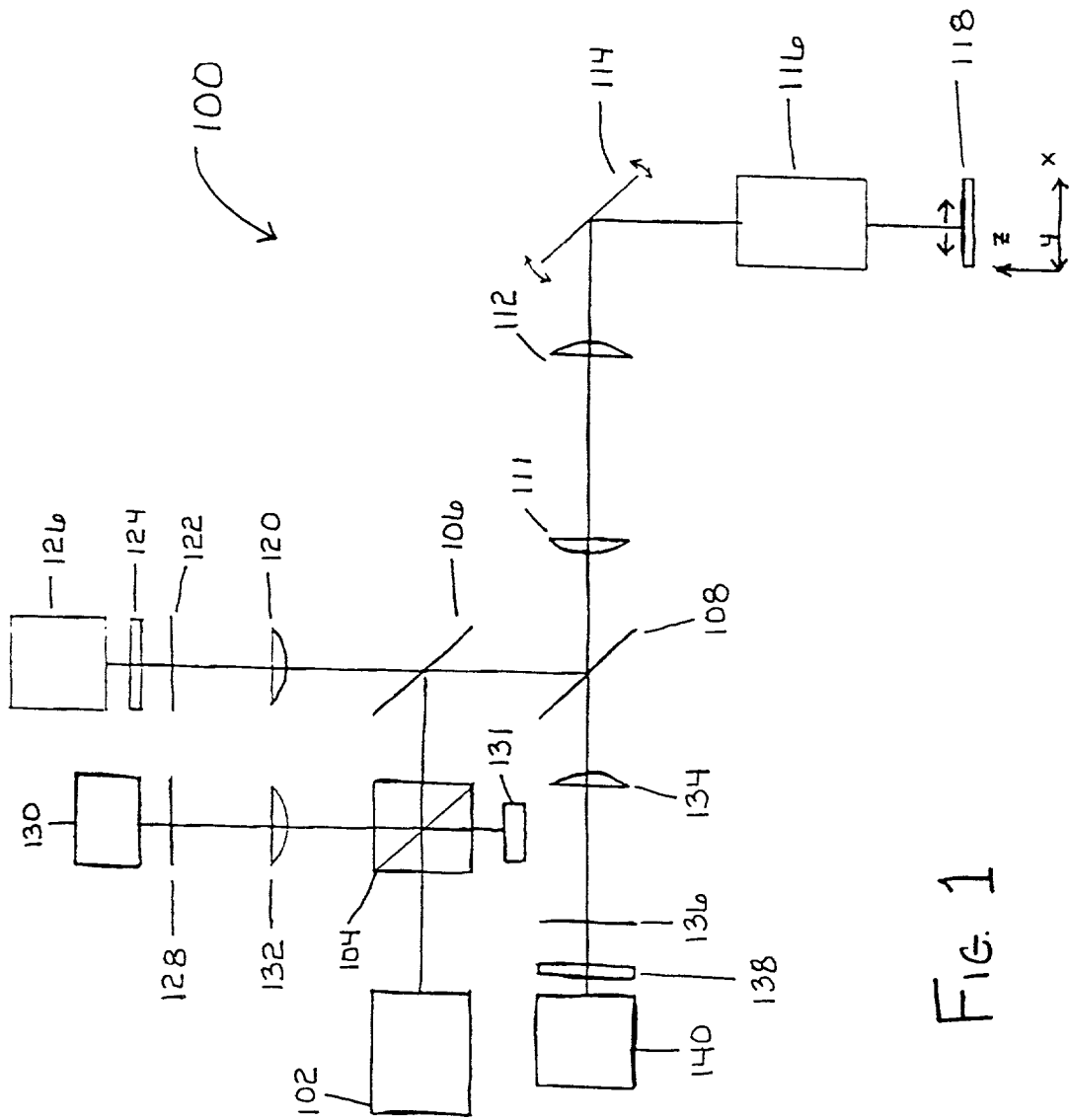


FIG. 1

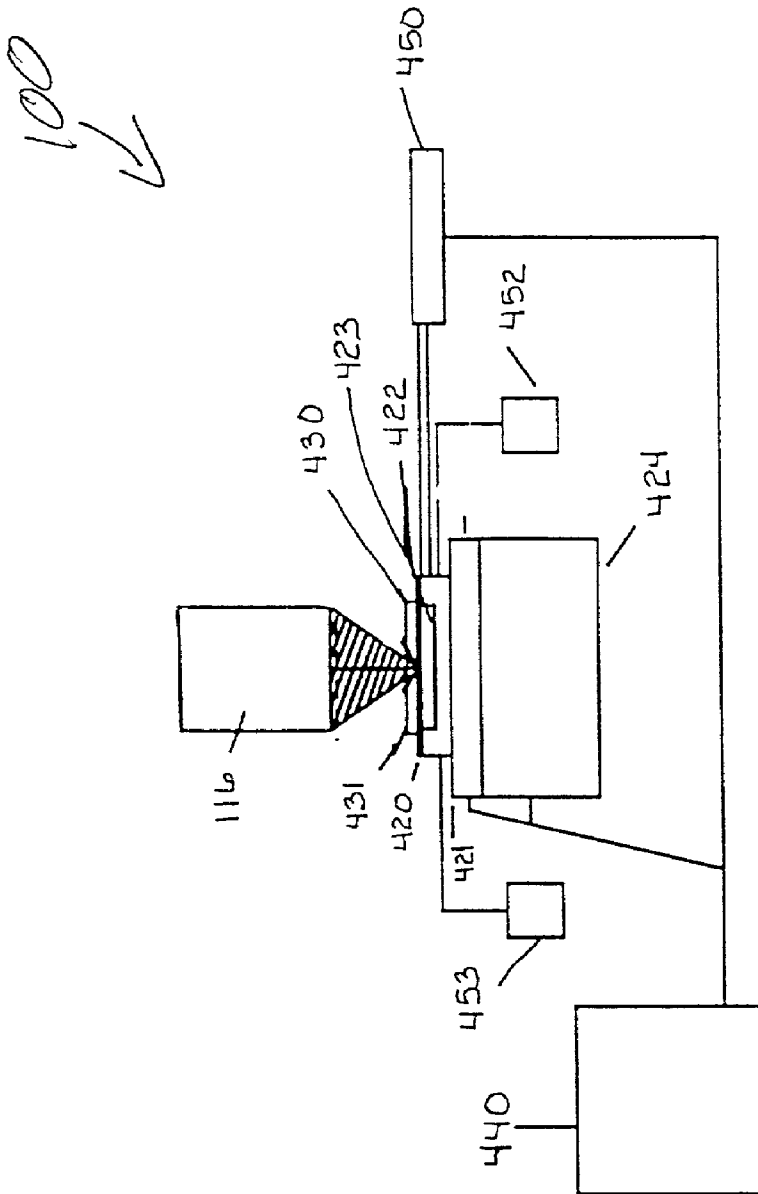


FIG. 2

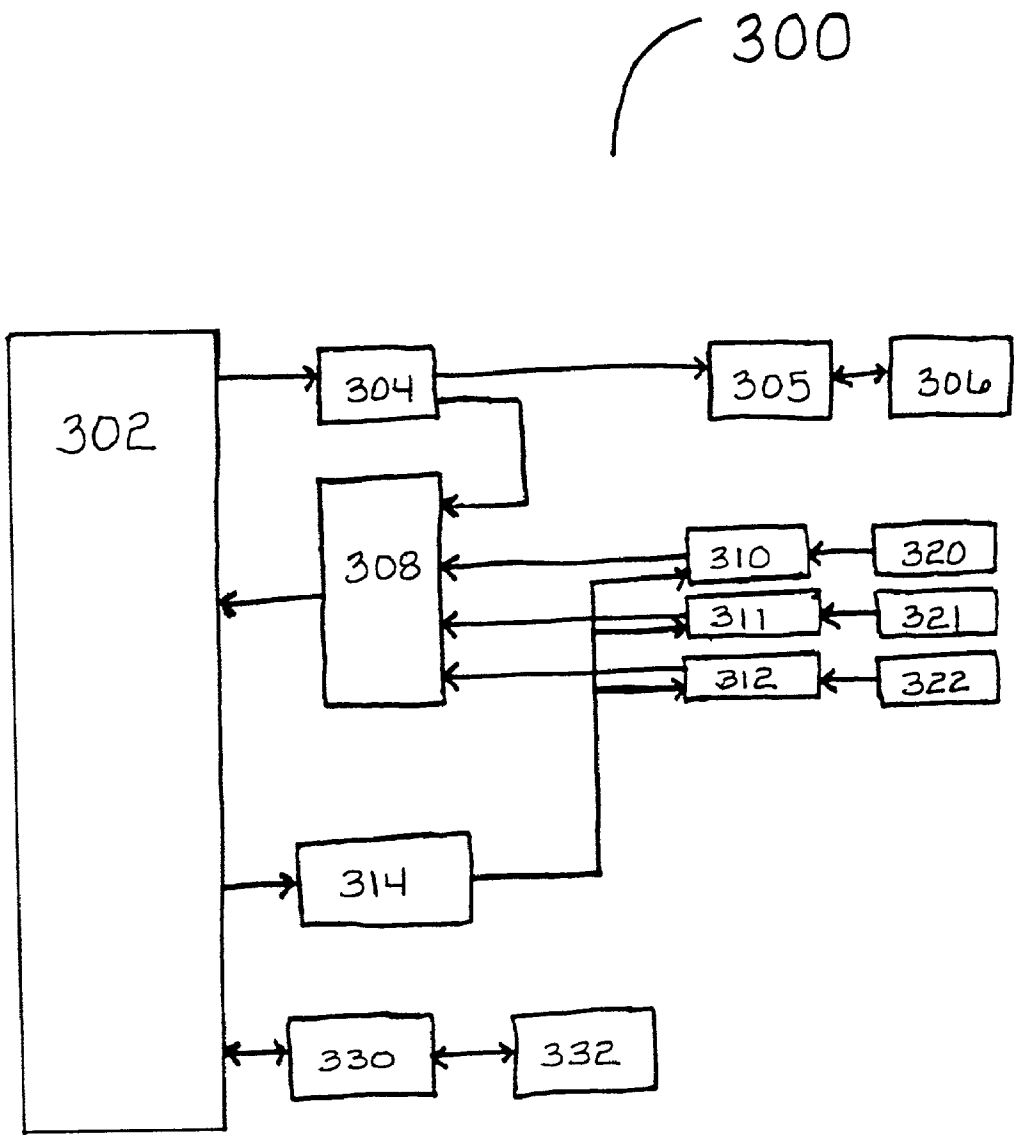


FIG. 3

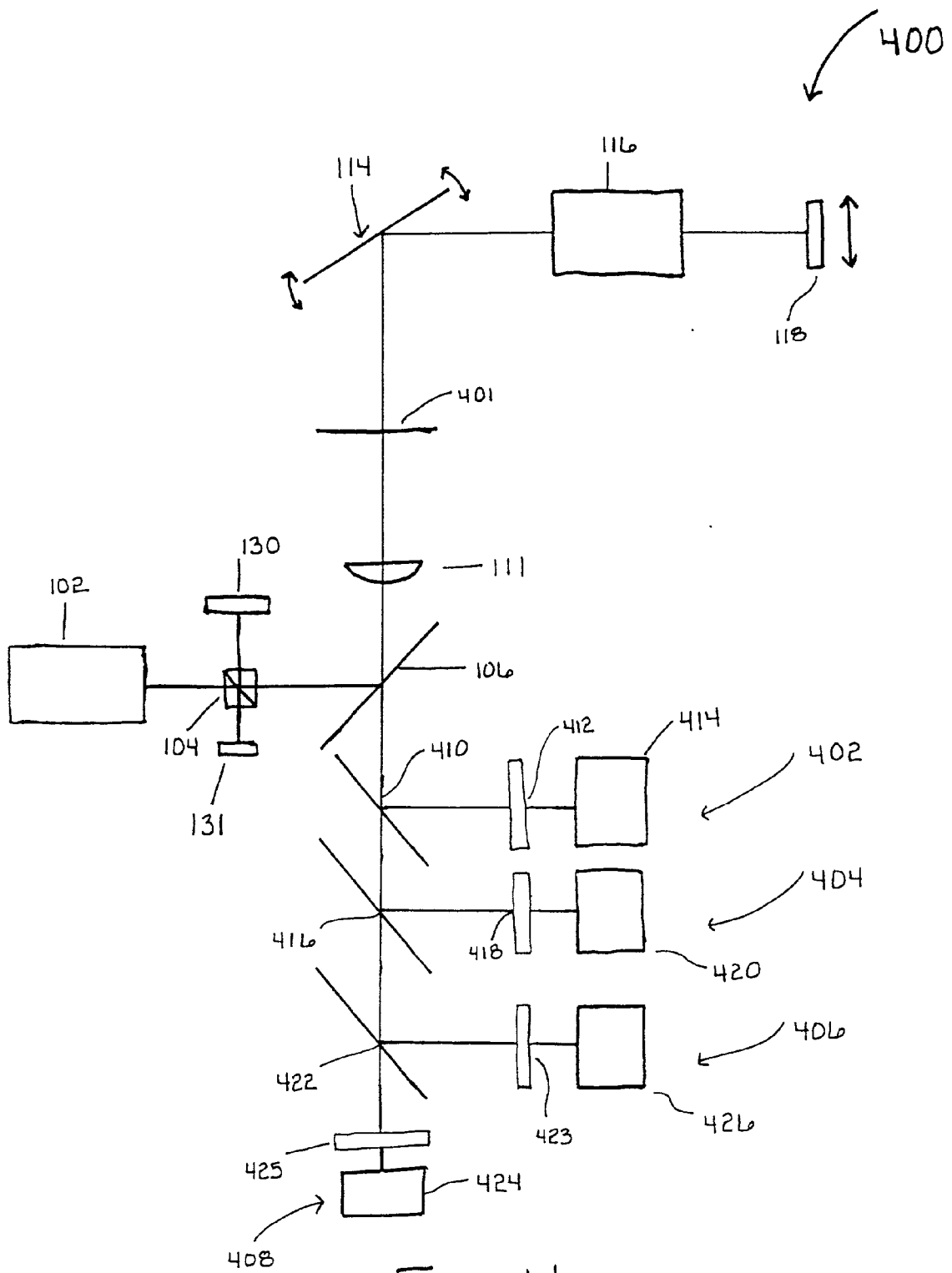


FIG. 4

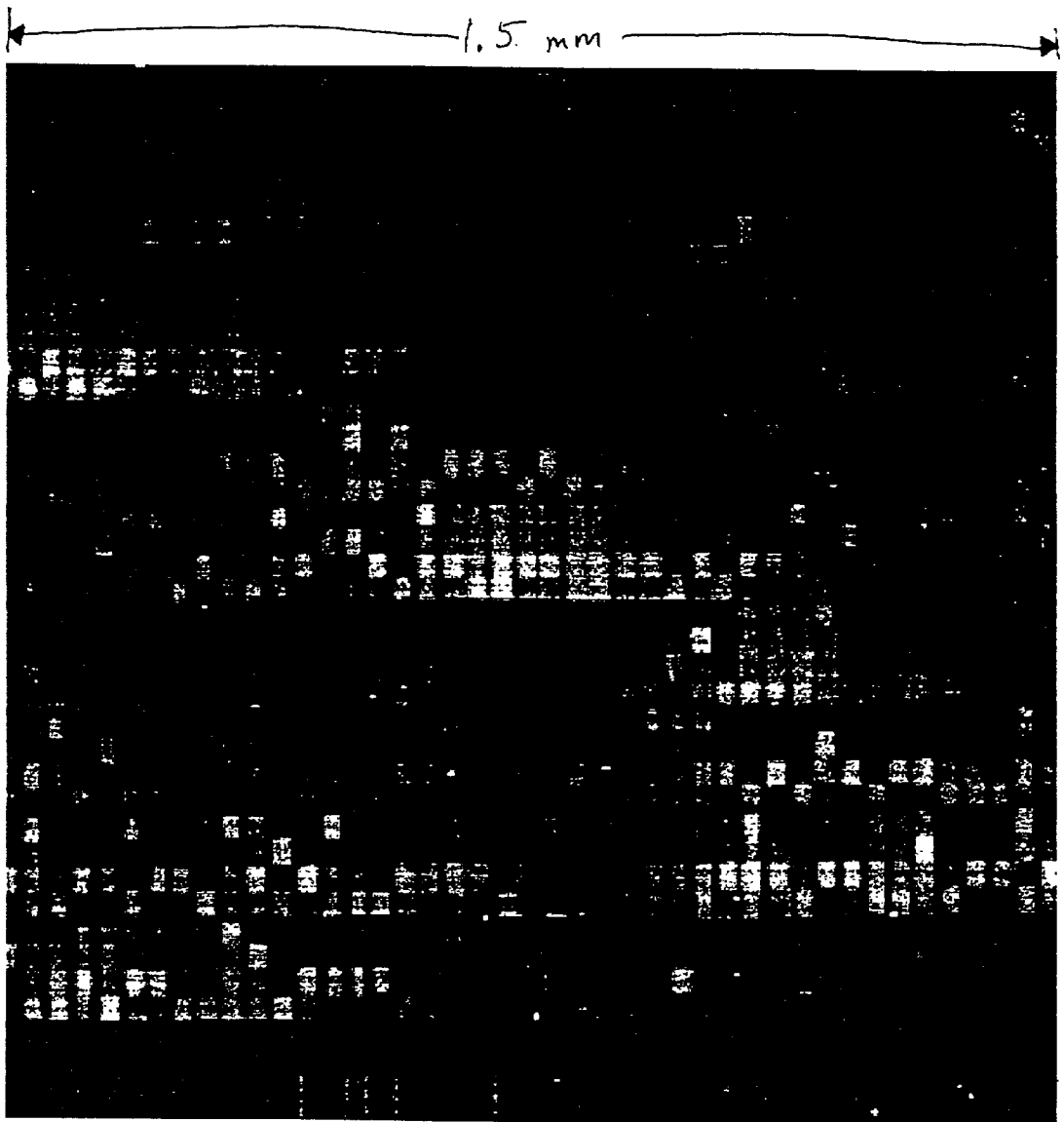


FIG. 5

SYSTEMS AND METHODS FOR DETECTION OF LABELED MATERIALS

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] The present application is a regular application of provisional U.S. Patent Application Serial No. 60/017,203, filed May 16, 1996 (Attorney Docket No. 16528X-018900), the complete disclosure of which is hereby incorporated herein by reference for all purposes. This application is also related to commonly assigned, U.S. patent application Ser. No. 08/301,051, filed Sep. 9, 1994, now U.S. Pat. No. 5,578,832, and U.S. patent application Ser. No. 08/195,889, filed Feb. 10, 1994 (Attorney Docket Nos. 16528X-003800 and 16528X-006000, respectively) the complete disclosures of which are incorporated herein by reference for all purposes.

BACKGROUND OF THE INVENTION

[0002] The present invention generally relates to the field of imaging. In particular, the present invention provides scanning systems and methods for high speed imaging of a sample containing labeled materials, and particularly for scanning arrays of polymer sequences, e.g., oligonucleotide arrays.

[0003] Methods and systems for imaging samples containing labeled markers such as confocal microscopes are commercially available. Confocal microscopes generally employ a pinhole that is confocal with the illuminated spot on the specimen to reject light that is not reflected or emitted from objects in the focal plane. This rejection of out-of-focus light enables the microscope to collect and combine a series of optical slices at different focus positions to generate a two or three dimensional representation of the specimen.

[0004] Some scanning microscopes employ radiation direction systems, such as galvanometers that include servo-mounted mirrors, to rapidly scan a laser spot across a substrate. Although these microscopes have relatively high scan rates (e.g., on the order of about 30 lines/second or greater), they generally do not achieve both the resolution and field of view that is necessary for some applications, such as imaging an array of sequenced materials on a substrate. In fact, a galvanometer-based confocal microscope's field of view is generally proportional to its resolution. For example, a typical 40 \times microscope objective, which has a 0.25 μm resolution, has a field size of only about 500 μm . Thus, conventional galvanometer-based confocal microscopes are inadequate for applications requiring both high resolution and a large field of view.

[0005] Scanning confocal microscope systems, such as those discussed in U.S. Pat. No. 5,143,854 (Pirring et al.), PCT WO 92/10092, and U.S. patent application Ser. No. 08/195,889 (Attorney Docket Number 16528X-006000), incorporated herein by reference for all purposes, are also known. These scanning systems include an optical train which directs a monochromatic or polychromatic light source to about a 5 micron (μm) diameter spot at its focal plane. In some cases, a photon counter detects the emission from the device in response to the light. The data collected by the photon counter represents one pixel or data point of the image. Thereafter, the light scans another pixel as a translation stage moves the device to a subsequent position.

[0006] As disclosed, these scanning confocal microscope systems provide high resolution by using an appropriate objective lens and large field of view by using appropriate translation stages. These translation stage-based confocal microscopes, however, obtain high resolution and field of view by sacrificing system throughput. As an example, an array of sequenced material using the pioneering fabrication techniques, such as those disclosed in U.S. Pat. No. 5,143,854 (Pirring et al.) and U.S. patent application Ser. No. 08/143,312, incorporated herein by reference for all purposes, may have a density of about 10^5 sequences. Assuming that 36 pixels are required for each sequence, the image can take over at least 10 minutes to acquire.

[0007] From the above, it is apparent that improved methods and systems for imaging a sample are desired.

SUMMARY OF THE INVENTION

[0008] The present invention provides systems, methods and apparatus for detecting marked regions on substrate surfaces. In particular, the present invention provides methods and apparatus for scanning a substrate to obtain an image with high sensitivity and resolution at a high speed. The confocal scanning microscopes of the present invention combine the high scan rate of galvanometer based scanning microscopes with a sufficiently high resolution, sensitivity and a large enough field of view for imaging high density arrays of materials, such as those found in the fields of combinatorial chemistry and genetic analysis.

[0009] In one aspect, the present invention provides a system for detecting marked regions on a surface of a substrate, which comprises an excitation radiation source, and focusing optics for focusing the excitation radiation to regions on the surface of the substrate. A radiation direction system is also included for linearly scanning the focused excitation radiation across the surface of the substrate. A detector is positioned for detecting an emission from the substrate surface in response to the excitation radiation, and a data acquisition system records the amount of detected emission as a function of a position on the surface of the substrate from which the emission was detected.

[0010] In one embodiment, the focusing optics comprises an objective lens having a ratio of scanning field diameter to focused spot diameter of greater than 2000, preferably greater than 3000 and more preferably greater than 4000. Thus, the microscope is, for example, capable of focusing a laser beam to a spot having a diameter of about 3 microns at any point within a flat field having a length of about 14 mm. In addition, the objective lens has at least a 0.2 numerical aperture, preferably a 0.25 numerical aperture, which provides sufficient sensitivity to detect fluorescently marked regions on the substrate.

[0011] The radiation direction system preferably comprises a galvanometer mirror that scans the excitation radiation across the surface of the substrate. The objective lens has an external entrance pupil preferably located at or near the galvanometer mirror's pivot location. The mirror usually oscillates at a frequency of at least 7.5 Hz, preferably at least 20 Hz and more preferably at least 30 Hz. In this manner, the laser spot can usually be scanned across the substrate at velocities of about 5 image lines/second, preferably at least 10 image lines/second, and more preferably at least about 30 image lines/second. This allows the microscope to rap-

idly scan high density substrates, such as the polymer array substrates disclosed by Pirrung. It should be noted that the mirror may scan unidirectionally (e.g., with a sawtooth wave) or bidirectionally (e.g., with a symmetric triangle wave). In the latter case, the galvanometer frequency would generally be about half of the data acquisition speed in image lines/second. Accordingly, the frequency of the galvanometer in the latter case may be lower than 7.5 Hz in order to scan 5 image lines/second.

[0012] In another embodiment, the present invention also provides a system for detecting fluorescent regions on a surface of a substrate, which comprises an excitation radiation source, and first focusing optics for focusing the excitation radiation on the surface of the substrate in a focused spot having a diameter no greater than 10 μm , preferably less than 5 μm and more preferably about 3 μm . An oscillating or reciprocating radiation direction system scans the spot linearly across the surface of the substrate, with a focused travel distance of at least 10 mm and preferably about 14 mm. In one embodiment, an optical train separates fluorescence emitted from the surface of the substrate from the excitation radiation reflected from the surface. An autofocus system may also be included for automatically placing the surface of the substrate in a focal plane of the focusing optics.

[0013] The present invention also provides methods of scanning substrates using the above systems. For example, in one aspect, the invention provides a method of scanning a polymer array having a plurality of different polymer sequences, each of the different polymer sequences being immobilized on a surface of a substrate in a different known location, to identify which polymer sequence on the array is bound by a fluorescent target molecule. The method comprises focusing an excitation radiation source upon the surface of the substrate, and scanning the excitation radiation across the surface of the substrate at a speed of at least 5 image lines/second. Fluorescent emissions are collected from the surface of the substrate in response to the excitation radiation. These fluorescent emissions are recorded as a function of a position on the surface of the substrate. The position on the surface indicates the polymer sequence on the array that is bound by the fluorescent target molecule.

[0014] A further understanding of the nature and advantages of the inventions herein may be realized by reference to the remaining portions of the specification and the attached drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0015] FIG. 1 is a schematic illustration of one embodiment of a scanning system according to the present invention.

[0016] FIG. 2 illustrates one embodiment of a scanning system that includes a flow cell on which a substrate is mounted.

[0017] FIG. 3 is a schematic illustration of a computer based system for controlling and recording data from a scanning system according to the present invention.

[0018] FIG. 4 is a schematic illustration of an alternate embodiment of a scanning system according to the present invention.

[0019] FIG. 5 is an enlarged view of a scanned image generated using a scanning system of the present invention.

DESCRIPTION OF THE PREFERRED EMBODIMENT

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[0027] IV. Detailed Description of a Second Embodiment of the Imaging System

[0028] I. Definitions

[0029] The following terms are intended to have the following general meanings as they are used herein:

[0030] 1. Complementary: Refers to the topological compatibility or matching together of interacting surfaces of a probe molecule and its target. Thus, the target and its probe can be described as complementary, and furthermore, the contact surface characteristics are complementary to each other.

[0031] 2. Probe: A probe is a surface-immobilized molecule that is recognized by a particular target. Examples of probes that can be investigated by this invention include, but are not restricted to, agonists and antagonists for cell membrane receptors, toxins and venoms, viral epitopes, hormones (e.g., opioid peptides, steroids, etc.), hormone receptors, peptides, enzymes, enzyme substrates, cofactors, drugs, lectins, sugars, oligonucleotides, nucleic acids, oligosaccharides, proteins, and monoclonal antibodies.

[0032] 3. Target: A molecule that has an affinity for a given probe. Targets may be naturally-occurring or manmade molecules. Also, they can be employed in their unaltered state or as aggregates with other species. Targets may be attached, covalently or non-covalently, to a binding member, either directly or via a specific binding substance. Examples of targets which can be employed by this invention include, but are not restricted to, antibodies, cell membrane receptors, monoclonal antibodies and antisera reactive with specific antigenic determinants (such as on viruses, cells or other materials), drugs, polynucleotides, nucleic acids, peptides, cofactors, lectins, sugars, polysaccharides, cells, cellular membranes, and organelles. Targets are sometimes referred to in the art as anti-probes. As the term targets is used herein, no difference in meaning is intended. A "Probe Target Pair" is formed when two macromolecules have combined through molecular recognition to form a complex.

[0033] II. General**[0034]** A. Introduction

[0035] The present invention provides methods and apparatus for scanning a substrate to obtain a highly sensitive and resolved image at a high speed. The invention will have a wide range of uses, particularly, those requiring quantitative study of a microscopic region from within a larger region, such as 2 or 3 μm^2 over 100 mm^2 . For example, the invention may find application in the field of histology (for studying histochemical stained and immunological fluorescent stained images), or fluorescence in situ hybridization. In one application, the invention herein is used to image an array of probe sequences fabricated on a support.

[0036] High resolution scanning systems and methods, whether microscopic or macroscopic, have routinely been used in the electronics industries, e.g., in the semiconductor and microfabrication industries, to scan microfabricated electronics, e.g., microprocessors, microcircuitry, and the like. However, such scanning also has great utility in the field of combinatorial chemistry and genetic analysis. Specifically, high resolution scanning methods and devices can be used in the application of polymer arrays. These polymer arrays are generally made up of a large number of different polymer sequences that are coupled to the surface of a typically planar substrate.

[0037] The substrate on which the polymer sequences are formed may be composed from a wide range of material, either biological, nonbiological, organic, inorganic, or a combination of any of these, existing as particles, strands, precipitates, gels, sheets, tubing, spheres, containers, capillaries, pads, slices, films, plates, slides, etc. The substrate may have any convenient shape, such as a disc, square, sphere, circle, etc. The substrate is preferably flat but may take on a variety of alternative surface configurations. For example, the substrate may contain raised or depressed regions on which a sample is located. The substrate and its surface preferably form a rigid support on which the sample can be formed. The substrate and its surface are also chosen to provide appropriate light-absorbing characteristics. For instance, the substrate may be a polymerized Langmuir Blodgett film, functionalized glass, Si, Ge, GaAs, GaP, SiO_2 , SiN_4 , modified silicon, or any one of a wide variety of gels or polymers such as (poly)tetrafluoroethylene, (poly)vinylidenedifluoride, polystyrene, polycarbonate, or combinations thereof. Other substrate materials will be readily apparent to those of skill in the art upon review of this disclosure. In a preferred embodiment, the substrate is flat glass or silica.

[0038] According to some embodiments, the surface of the substrate is etched using well known techniques to provide for desired surface features. For example, by way of the formation of trenches, v-grooves, mesa structures, or the like, the synthesis regions may be more closely placed within the focus point of impinging light. The surface may also be provided with reflective "mirror" structures for maximization of emission collected therefrom.

[0039] Surfaces on the solid substrate will usually, though not always, be composed of the same material as the substrate. Thus, the surface may be composed of any of a wide variety of materials, for example, polymers, plastics, resins, polysaccharides, silica or silica-based materials, car-

bon, metals, inorganic glasses, membranes, or any of the above-listed substrate materials. In one embodiment, the surface will be optically transparent and will have surface Si—OH functionalities, such as those found on silica surfaces.

[0040] These arrays are typically prepared in a manner that allows groups of each different polymer sequence to be coupled in a different known location on the substrate surface. The pioneering methods for synthesizing these arrays have been previously described. For example, methods of synthesizing arrays of polymers using light directed synthesis methods are described in U.S. Pat. No. 5,143,854 to Pirrung et al., and U.S. Pat. No. 5,405,783 to Fodor et al., the complete disclosures of which are incorporated herein by reference. Additionally, mechanical methods for synthesizing these arrays are described in, e.g., U.S. Pat. No. 5,384,261 to Winkler et al., the complete disclosure of which is incorporated herein by reference. Using these pioneering methods, the combination of photolithographic and fabrication techniques may, for example, enable each probe sequence ("feature") to occupy a very small area ("site") on the support. In some embodiments, this feature site may be as small as a few microns or even a single molecule. For example, about 10^5 to 10^6 features may be fabricated in an area of only 12.8 mm^2 . Such probe arrays may be of the type known as Very Large Scale Immobilized Polymer Synthesis (VLSIPSTM). For ease of discussion, the arrays for use with the present invention are described in terms of arrays of different oligonucleotide sequences. However, it should be readily understood that a variety of different polymer array types are equally applicable to the devices of the invention. Furthermore, the scanners of the present invention may also be used in the reflectance mode to scan non-fluorescent surfaces.

[0041] In those applications using polymer arrays, such arrays may be prepared having all nucleotide sequences of a given length, composed of the basis set of monomers. For example, an array of oligonucleotides containing all possible sequences of length n which is made up of the basis set of four nucleotides contains up to 4^n oligonucleotides on its surface. For an array of 8mer or 10mer oligonucleotides, such arrays may include upwards of about 65,536 and 1,048,576 different oligonucleotides, respectively. Generally, where it is desired to produce arrays having all possible polymers of length n , a simple binary masking strategy can be used, as described in U.S. Pat. No. 5,143,854 to Pirrung.

[0042] Alternate masking strategies can produce arrays of probes which contain a subset of polymer sequences, i.e., polymers having a given subsequence of monomers, but are systematically substituted at each position with each member of the basis set of monomers. In the context of oligonucleotide probes, these alternate synthesis strategies may be used to lay down or "tile" a range of probes that are complementary to, and span the length of a given known nucleic acid segment. The tiling strategy will also include substitution of one or more individual positions within the sequence of each of the probe groups with each member of the basis set of nucleotides. These positions are termed "interrogation positions." By reading the hybridization pattern of the target nucleic acid, one can determine if and where any mutations lie in the sequence, and also determine what the specific mutation is by identifying which base is contained within the interrogation position. Tiling methods

and strategies are discussed in substantial detail in Published PCT Application No. 95/11995, the complete disclosure of which is incorporated herein by reference in its entirety for all purposes.

[0043] Tiled arrays may be used for a variety of applications, such as identifying mutations within a known oligonucleotide sequence or "target". Specifically, the probes on the array will have a sub-sequence which is complementary to a known nucleic acid sequence, but wherein at least one position in that sequence has been systematically substituted with the other three nucleotides. See, e.g., U.S. Pat. No. 5,527,681, the complete disclosure of which is incorporated herein by reference.

[0044] Generally, the sample nucleic acid for which sequence information is desired is contacted with the array. This "target" sequence is typically labeled with a detectable group such as a fluorescent moiety, i.e., fluorescein or rhodamine. Following hybridization of the target to the array, one can detect the position on the array to which the target sequence binds by scanning the surface of the array for fluorescence.

[0045] The surface is typically scanned by directing excitation radiation at the surface to activate the fluorescent labeling group in the target, which in turn emits a fluorescent response radiation. The fluorescent response radiation is detected and assigned to the region from which it originated. By knowing the position from which the fluorescence originates, one can identify the sequence to which the target binds.

[0046] Although generally used herein to define separate regions containing differing polymer sequences, the term "feature" generally refers to any element, e.g., region, structure or the like, on the surface of a substrate. Typically, substrates to be scanned using the scanning systems described herein, will have small feature sizes, and consequently, high feature densities on substrate surfaces. For example, individual features will typically have at least one of a length or width dimension that is no greater than 100 μm , and preferably, no greater than 50 μm , and more preferably greater than about 20 μm . Thus, for embodiments employing substrates having a plurality of polymer sequences on their surfaces, each different polymer sequence will typically be substantially contained within a single feature.

[0047] The probe arrays will have a wide range of applications. For example, the probe arrays may be designed specifically to detect genetic diseases, either from acquired or inherited mutations in an individual DNA. These include genetic diseases such as cystic fibrosis, diabetes, and muscular dystrophy, as well as acquired diseases such as cancer (P53 gene relevant to some cancers), as disclosed in U.S. patent application Ser. No. 08/143,312, already incorporated by reference.

[0048] Genetic mutations may be detected by a method known as sequencing by hybridization. In sequencing by hybridization, a solution containing one or more targets to be sequenced (i.e., samples from patients) contacts the probe array. The targets will bind or hybridize with complementary probe sequences. Generally, the targets are labeled with a fluorescent marker, radioactive isotopes, enzymes, or other types of markers. Accordingly, locations at which targets

hybridize with complimentary probes can be identified by locating the markers. Based on the locations where hybridization occur, information regarding the target sequences can be extracted. The existence of a mutation may be determined by comparing the target sequence with the wild type.

[0049] The interaction between targets and probes can be characterized in terms of kinetics and thermodynamics. As such, it may be necessary to interrogate the array while in contact with a solution of labeled targets. Consequently, the detection system must be extremely selective, with the capacity to discriminate between surface-bound and solution-born targets. Also, in order to perform a quantitative analysis, the high-density volume of the probe sequences requires the system to have the capacity to distinguish between each feature site.

[0050] B. Overview of the Imaging System

[0051] The devices of the present invention generally employ a scanning device which rapidly sweeps an activation radiation beam or spot across the surface of the substrate. The devices also include focusing optics for focusing the excitation radiation onto the surface of the substrate in a sufficiently small area to provide high resolution of features on the substrate, while simultaneously providing a wide scanning field. An image is obtained by detecting the electromagnetic radiation emitted by the labels on the sample when the labels are illuminated. In one embodiment, fluorescent emissions are gathered by the focusing optics and detected to generate an image of the fluorescence on the substrate surface. In preferred aspects, the devices of the invention further employ confocal detection systems to reduce or eliminate unwanted signals from structures above and below the plane of focus of the excitation radiation, as well as autofocus systems to focus both the activation radiation on the substrate surface and the emitted radiation from the surface. Generally, the excitation radiation and response emission have different wavelengths. Filters having high transmission in the label's emission band and low transmission in the excitation wavelength may be utilized to inhibit the detection of undesirable emission. These generally include emission from out-of-focus planes or scattered excitation illumination as potential sources of background noise.

[0052] In operation, the devices of the present invention include one or more sources of excitation radiation. Typically, these source(s) are immobilized or stationary point light sources, e.g., lasers such as argon, helium-neon, diode, dye, titanium sapphire, frequency-doubled diode pumped Nd:YAG and krypton. Typically, the excitation source illuminates the sample with an excitation wavelength that is within the visible spectrum, but other wavelengths (i.e., near ultraviolet or near infrared spectrum) may be used depending on the application (i.e., type of markers and/or sample). In some embodiments, the sample is excited with electromagnetic radiation having a wavelength at or near the absorption maximum of the species of label used. Exciting the label at such a wavelength produces the maximum number of photons emitted. For example, if fluorescein (absorption maximum of 488 nm) is used as a label, an excitation radiation having a wavelength of about 488 nm would induce the strongest emission from the labels.

[0053] In instances where a multi-labeling scheme is utilized, a wavelength which approximates the mean of the

various candidate labels' absorption maxima may be used. Alternatively, multiple excitations may be performed, each using a wavelength corresponding to the absorption maximum of a specific label. Table I lists examples of various types of fluorophores and their corresponding absorption maxima.

TABLE 1

Candidate Fluorophores	Absorption Maxima
Fluorescein	488 nm
Dichloro-fluorescein	525 nm
Hexachloro-fluorescein	529 nm
Tetramethylrhodamine	550 nm
Rodamine X	575 nm
Cy3™	550 nm
Cy5™	650 nm
Cy7™	750 nm
IRD40	785 nm

[0054] The excitation radiation from the point source is directed at a movable radiation direction system which rapidly scans the excitation radiation beam back and forth across the surface of the substrate. A variety of devices may be employed to generate the sweeping motion of the excitation radiation. For example, resonant scanner or rotating polygons, may be employed to direct the excitation radiation in this sweeping fashion. Generally, however, galvanometer devices are preferred as the scanning system. As used herein, the term "galvanometer" refers to devices that employ a servo motor to oscillate or rotate a mirror over a restricted, predefined range, which is typically less than 90°. This generates a rapidly sweeping or rastering beam reflecting from the galvanometer mirror, which is then directed at and swept across the surface of a substrate that is to be scanned. Typically, an optical train may be employed between the activation source and the galvanometer mirror to assist in directing, focusing or filtering the radiation directed at and reflected from the galvanometer mirror.

[0055] The galvanometers employed in the devices and systems of the present invention typically sweep a scanning spot across the substrate surface at an oscillating frequency that is typically greater than about 7.5 Hz, preferably greater than about 20 Hz and more preferably, greater than about 30 Hz. With this frequency, the spot can typically be scanned across the substrate at a velocity of at least about 20 lines/second, preferably in about 5 image lines/second, preferably at least 10 images lines/second, and more preferably at least about 30 image lines/second. It should be noted that the mirror may scan unidirectionally (e.g., with a sawtooth wave) or bidirectionally (e.g., with a symmetric triangle wave). In the latter case, the galvanometer frequency would generally be about half of the data acquisition speed in image lines/second. Accordingly, the frequency of the galvanometer in the latter case may be lower than 7.5 Hz in order to scan 5 image lines/second. The activation radiation is then directed through focusing optics to focus the sweeping beam at the surface of the array which is used to interrogate the target sequence. These same focusing optics also collect emitted fluorescence from the substrate surface for subsequent detection.

[0056] The objective lens is preferably selected to provide high resolution, as determined by the focused spot size, while still allowing a wide scanning field. "Focused spot

size" is defined by the diameter of the focused activation spot on the surface of the substrate at $1/e^2$ intensity points. "Scanning field" is defined as the length of travel of the focused activation beam or "spot," in one dimension parallel to the direction of travel of the sweeping beam. The confocal system of the present invention generally provides a focused spot size having a diameter no greater than about 10 μm , preferably no greater than about 5 μm , and more preferably about 3 μm . In addition, these systems have a scanning field with a dimension parallel to the direction of the sweep of the activation beam that is usually greater than about 10 mm and more preferably about 14 mm.

[0057] For ease of discussion, the combined measurement of resolution and effective scanning field are provided as a ratio of the size of the effective field of view of the objective to the size of the focused spot from the scanner. For example, a scanner having a scanning field of 2 mm and a focused spot size of 10 μm would have a ratio of 200 (2 mm/0.010 mm). While a scanner having an effective scanning field of 14 mm with a focused spot size of 3 μm would have a ratio of 4666. In general, the scanning system of the present invention usually has a ratio of size of effective field of view to size of focused spot of at least about 2000, preferably greater than about 3000, and more preferably greater than about 4000. It should be noted that "scanning field" generally refers to the direction in which the galvanometer mirror scans the laser spot across the substrate. The translation stage moves the substrate in the direction orthogonal to the scanned direction, and this direction may be larger than 14 mm.

[0058] In one embodiment of the present invention, high fluorescence collection efficiency is achieved by providing an objective lens having a numerical aperture that is at least about 0.2. In particularly preferred aspects, the numerical aperture is at least about 0.25. This translates to an F/number of about F/2.5 to F/2.

[0059] In addition to providing smaller spot size while not sacrificing scanning field size, the focusing optics of the scanning system may include a telecentric objective lens. This allows the activation beam to strike the scanning surface at an angle that is substantially normal to that surface, across the entire scanning surface, i.e., regardless of where the input beam is propagating through the lens relative to the lens axis. By "substantially normal" is meant an angle of incidence of approximately 0°, e.g., between 0° and 5°, and preferably from 0° to 2°.

[0060] As the activation radiation spot is swept across the surface of the substrate, it activates any fluorescent groups that remain upon the surface, e.g., those that are bound to the surface. The activated groups emit a response radiation or emission which is then collected by the objective lens and directed back through the optical train via the servo mounted mirror. In order to avoid the detrimental effects of reflected excitation radiation upon the detection of the fluorescence, dichroic mirrors or beam splitters may be included in the optical train. These dichroic beam splitters or mirrors are reflective to radiation in the wavelength of the excitation radiation while transmissive to radiation in the wavelength of the response radiation. For example, where an Argon laser is used as the point energy source, it will typically generate activation radiation having a wavelength of about 488 nm. Fluorescence emitted from an activated fluorescein moiety

on the other hand will typically have a wavelength between about 515 and 545 nm. As such, dichroic mirrors may be included which transmit light having a wavelength greater than 515 nm while reflecting light of shorter wavelengths. This effectively separates the excitation radiation reflected from the surface of the substrate from the response radiation emitted from the surface of the substrate. Similarly, additional dichroic mirrors may be used to separate signals from label groups having different response radiation wavelengths, thereby allowing simultaneous detection of multiple fluorescent indicators, and thus, simultaneous interrogation of a single array with multiple target sequences. Specifically, a first target sequence may be labeled with a shorter wavelength fluorescent label, e.g., fluorescein, while a second target sequence is labeled with a longer wavelength fluorescent label, e.g., carbocyanin dyes such as CY3 which emit response radiation in the range of 550 to 600 nm. The response radiation from each of these targets may be separated and individually detected through the inclusion of additional dichroic beam splitters and detectors.

[0061] Following separation of the response radiation from the reflected excitation radiation, the response radiation or fluorescence is then directed at a detector, e.g., a photomultiplier tube, to measure the level of response radiation and record that level as a function of the position on the substrate from which that radiation originated. Typically, the response radiation is focused upon the detector through a spatial filter such as a confocal pinhole. Such spatial filters reduce or eliminate unwanted signals from structures above and below the plane of focus of the excitation radiation. Additionally, the device may incorporate a bandpass filter between the dichroic mirror and the detector to further restrict the wavelength of radiation that is delivered to the detector.

[0062] As noted above, the reflected excitation radiation may generally be used in an autofocusing system in the devices described herein. In particular, the reflected excitation radiation may also be directed at a detector, e.g., a photodiode, that is preferably located behind another spatial filter, i.e., a confocal pinhole.

[0063] The substrate surface may be moved closer to and further from the objective lens using, e.g., a translation stage upon which the substrate is mounted. As the substrate is moved out of focus, the amount of reflected excitation radiation contacting the photodiode will be reduced. As the substrate is brought back into focus, this amount will increase, reaching a maximal value when the substrate is in focus. Control for the autofocus system is generally supplied by an appropriately programmed computer, which moves the translation stage in response to the input from the photodiode, until a maximum is reached. Generally, this computer is the same computer which receives, compiles and stores the input from the fluorescence detector or photomultiplier tube, to produce an output of fluorescence as a function of position on the array, typically in the form of a numerical representation or a scan image. Examples of autofocus confocal systems for use in fluorescent scanning devices are generally described in commonly assigned, co-pending U.S. patent application Ser. No. 08/195,889, filed Feb. 10, 1994, the complete disclosure of which is incorporated herein by reference for all purposes. These autofocus systems generally permit the focusing of light reflected from a weakly reflecting surface, e.g., the wet side

of a glass substrate, even in the vicinity of a strongly reflecting surface, e.g., the dry side of a glass substrate, as well as being capable of focusing on a featureless surface, e.g., smooth glass.

[0064] III. Detailed Description of One Embodiment of the Imaging System.

[0065] A. Detection Device

[0066] FIG. 1 is an optical block diagram illustrating the imaging system 100 according to the present invention. Typically, imaging system 100 is used to obtain images of oligonucleotide probe arrays to which fluorescently labelled DNA or RNA is bound. It might also be used for other applications, such as wafer or mask inspection, or for imaging of polypeptide or other polymer arrays, electrophoresis gels, or biological specimens. As shown in FIG. 1, a beam of excitation radiation, e.g., 488-nm light, from a laser 102 is partially reflected and partially transmitted by a beamsplitter 104. The reflected portion of the beam impinges upon a photodetector 131 (optional), which is typically a photodiode used as a laser power monitor. The portion of the beam that is transmitted through beamsplitter 104 is reflected by dichroic beamsplitters 106 and 108 and transmitted through lenses 111 and 112, which provide a telescope to expand the beam emitted by laser 102 and to demagnify the collimated fluorescence obtained from the surface of the substrate. In an exemplary embodiment, lens 111 has a focal length of 20 mm and lens 112 has a focal length of 80 mm. Other focal lengths and focal length ratios can be used, but system performance (confocality, resolution, etc.) may be affected. The expanded laser beam is reflected by mirror 114 and focused by lens 116, which is described in more detail below.

[0067] Mirror 114, which typically is an 18 mm×28 mm octagon or ellipse, is a galvanometer mirror that oscillates (i.e., scans) at a rate of typically several Hertz or several tens of Hertz. In preferred aspects, the galvanometer mirror oscillates at frequencies greater than 7.5 Hz, preferably about 20 Hz and more preferably about 30 Hz. A resonant scanner or rotating polygonal mirror could be used instead of a galvanometer. Typically, imaging system 100 obtains an image of a 2-dimensional area by scanning the laser beam in one dimension while moving the sample in an orthogonal direction.

[0068] Optimally, sample 118 is positioned such that the plane of interest (e.g. the surface to which labelled target molecules are bound) is located in the plane where the laser light is focused. Light remitted by sample 118 is collected by lens 116, reflected by mirror 114, and transmitted through lenses 112 and 111. Remitted light may consist of fluorescence, phosphorescence, specular reflection, diffuse reflection, Raman scattering, etc. Remitted light having a wavelength greater than 555 nm passes through dichroic beamsplitter 108 and is focused by lens 134 onto pinhole 136. Remitted light having a wavelength between 515 and 555 nm is reflected by beamsplitter 108, passes through dichroic beamsplitter 106, and is focused by a lens 120 onto a pinhole 122. The light that is transmitted through pinholes 136 and 122 impinges upon filters 138 and 124, respectively; the light that passes through these filters impinges upon photodetectors 140 and 126, respectively. Filter 138 transmits light having wavelengths between 555 and 607 nm, and filter 124 transmits light having wavelengths between 515

and 545 nm. Remitted light having wavelengths less than 515 nm is reflected by beamsplitters **108** and **106** and partially reflected by beamsplitter **104**; the light reflected by beamsplitter **104** is focused by a lens **132** onto a pinhole **128**. The light that is transmitted through pinhole **128** impinges upon a photodetector **130**.

[0069] Pinholes **136**, **122**, and **128** are typically confocal pinholes. Specifically, remitted light that originates from the location on sample **118** where the laser beam is focused is maximally transmitted through the pinholes, while light that originates from other locations is not. Lenses **134**, **120**, and **132** preferably have focal lengths of 50 mm. Pinholes **136** and **122** preferably have diameters of 100 microns; pinhole **128** preferably has a diameter of 50 microns. Other lens focal lengths and pinhole diameters can be used, but system performance (confocality, sensitivity to misalignment, etc.) may be affected.

[0070] If lens **116** is not fully corrected for lateral color, the remitted light that is focused onto pinholes **136** and **122** might move laterally (across the plane of the pinhole) as mirror **114** is scanned. In this case it might be advantageous to use pinholes that are elliptical or rectangular rather than round, or to use slits instead of pinholes. For example, lens **116** in the present scanner has about 3 microns of lateral color at the edges of the scan field; consequently, the remitted light can move laterally by about 40 microns across the pinholes. Reasonable sizes for pinholes **136** and **122** in this case might be approximately 75 microns by 125 microns.

[0071] Photodetectors **140** and **126** are typically photomultipliers and are typically intended for the detection of relatively weak signals such as fluorescence. Various light detectors may be used, including photodiodes, avalanche photodiodes, phototransistors, vacuum photodiodes, photomultiplier tubes, and other light detectors.

[0072] Typically, photodetector **130** is used to aid in focusing the sample prior to scanning or while it is being scanned. The amount of reflected laser light reaching photodetector **130** is a maximum when the laser beam is focused onto the surface of sample **118**. Focusing can be done either manually, or by a motorized translation stage under computer control. Frequently, sample **118** is a glass slide mounted in a liquid-filled flow cell (see FIG. 2) and the surface of interest is the second surface of the glass, i.e. the glass-liquid interface. Typically the reflection from this surface is much weaker than the reflection from the first surface of the glass, i.e. the glass-air interface, but the system is sufficiently confocal that the reflection peaks from the 2 surfaces are well separated.

[0073] The system described above is particularly useful in the detection of fluorescence from targets that are labelled with dyes such as fluorescein and phycoerythrin. Other dyes (rhodamines, carbocyanines, etc.) can be used, but laser **102**, beamsplitters **108** and **106**, and filters **138** and **124** may need to be altered depending on the dyes' absorption and emission spectra.

[0074] In some cases, target molecules may be labeled with particles or very large molecules that scatter laser light but do not fluoresce. In these cases, it may be desirable to detect diffusely scattered light but not specularly reflected laser light. An annular aperture can be placed between

beamsplitter **104** and lens **132**. If the inner diameter of the annulus is selected properly, this aperture will block specularly reflected laser light while transmitting diffusely scattered laser light, which can then be detected by photodetector **130**.

[0075] Objective lens **116** was designed to meet a number of specifications, and may be obtained from, e.g., Special Optics, Part No. 55-S30-15 (Wharton, N.J.). The objective lens is usable with a galvanometer (or resonant scanner, rotating polygon, etc.), i.e. with an entrance pupil that is external to the lens and is located at or near the galvanometer mirror's pivot location. The lens is also capable of focusing a TEM₀₀-mode laser beam having a wavelength of 488 nm to a spot having a diameter no greater than 3 microns at the 1/e² intensity points, and should be capable of doing this at any point within a flat field having a diameter no less than 14 mm.

[0076] Objective lens **116** is within 2 degrees of telecentric, i.e. the transmitted laser beam should be parallel to the optical axis of the lens to within 2 degrees. (If the lens is not telecentric or nearly so, specularly reflected light from near the edges of the field might miss the lens and therefore not be detected.) In addition, lens **116** was designed so that the F/number would be no greater than f/2, i.e. numerical aperture no less than 0.25, with no vignetting even at the edges of the field. (F/number is a measure of the lens's light-gathering ability and is important if the lens is to be used for the detection of weak signals). Objective lens **116** is capable of focusing a polychromatic beam, having wavelengths between 488 and 600 nm and filling the entrance pupil, to a spot having a diameter no greater than 10 microns, and is capable of doing this at any point within a flat field having a diameter no less than 14 mm.

[0077] Objective lens **116** preferably has a focal length of about 30 mm. A lens having a different focal length, but still meeting the above specifications could be readily designed and would be acceptable for the purposes described herein. Lens **116** can focus a 488 nm laser beam to a diffraction-limited spot when the ratio of input beam diameter to lens focal length is less than approximately 0.21, e.g. it can focus a 6.2 mm diameter beam to a 3 micron diameter spot. If a larger focal spot is desired, the input beam diameter can be made smaller, e.g. by changing the ratio of the focal lengths of lenses **111** and **112** or by demagnifying the beam between laser **102** and beamsplitter **104**.

[0078] Lens **116** was designed to be able to image a 14 mm field with 3 micron resolution and 0.25 numerical aperture; however, the design can easily be scaled up, e.g. to image a 28 mm field with 6 micron resolution and 0.25 numerical aperture (or potentially, to image a 280 mm field with 60 micron resolution and 0.25 numerical aperture, although the lens would be extremely large and costly). This scale-up involves merely multiplying the thicknesses, diameters, and radii of curvature of all of the elements of lens **116** by a constant. Similarly, the entire scanner can be scaled up for imaging of larger areas by multiplying all of the lens diameters and focal lengths, pinhole diameters, and mirror diameters by the same factor.

[0079] B. Data Acquisition

[0080] As shown in FIG. 3, imaging system **300** includes a galvanometer **306** (to which a mirror **114** is attached) and

a galvanometer driver board **305**, which can be obtained from General Scanning Inc. (Watertown, Mass.). Galvanometer **306** is a model M2T. Other suitable galvanometers and driver boards are available, e.g. from Cambridge Technology Inc. (Watertown, Mass.). The input to driver board **305** is a voltage waveform from arbitrary waveform generator **304** (Keithley Metrabyte model PCIP-AWFG, Taunton, Mass.), which is installed in an ISA slot in computer **302**. Circuitry on board **305** attempts at every instant to force galvanometer **306** to whatever angular position is commanded by waveform generator **304** (the desired angular position is linearly related to the waveform voltage). Waveform generator **304**, after being programmed, can generate a waveform indefinitely without further intervention by computer **302**. The waveform used is typically a sawtooth wave: e.g. if the waveform period is 33.3 msec, the voltage ramps up linearly for 25 msec, during which time data are acquired as the laser beam sweeps across the field; during the next 8.3 msec the voltage returns to its initial value and the laser beam retraces. Other waveforms such as sine waves or symmetric triangle waves could be used. Various methods of waveform generation that do not require the PCIP-AWFG waveform generator are known.

[**0081**] Currents from photomultipliers **320** and **321** and from photodiode **322** are converted to voltages by either transimpedance amplifiers or load resistors, optionally followed by voltage amplifiers. Simple op-amp circuits for this purpose are well known. The voltages are then low-pass filtered by filters **310**, **311**, and **312**, e.g., programmable 4-pole Bessel filters (Frequency Devices model 824L8L-6, Haverhill, Mass.). Filter cutoff frequencies are digitally programmable in 400-Hz steps from 400 Hz to 102.4 kHz and are set by digital input-output board **314** (Computer Boards Inc. model CIO-DIO24, Mansfield, Mass.) installed in computer **302**. Similar digital I/O boards are available from several other manufacturers. Filter cutoff frequencies are set by software so that each filter's output rise time in response to a step input is approximately equal to the time between A/D conversions. For example, if A/D conversions are 6 microseconds apart, the cutoff frequencies are set to 66 kHz. A variety of other types of filters (filters with more or fewer poles of different transfer functions (e.g. Butterworth), fixed-frequency filters, or simple RC filters) could be used instead.

[**0082**] Filter outputs are digitized by a 12-bit, 330-kHz analog-to-digital converter on data acquisition board **308** (Computer Boards Inc. model CIO-DAS16/330). Similar data acquisition boards are available from several other manufacturers. Digitized data are displayed by computer **302**, typically in the form of a gray-scale image, and are written to the computer's hard disk for subsequent data analysis. If the internal clock on data acquisition board **308** is used to trigger A/D conversions, the images obtained may be slightly distorted. A/D conversions that are equally far apart in time are not equally far apart in space, i.e., the velocity of the laser beam across sample **118** is not exactly constant, partly because lens **116** is not an ideal f-theta lens, and partly because of non-ideal behavior by driver board **305** and galvanometer **306**. Therefore, A/D conversions are preferably triggered by waveform generator **304**, which has digital output channels in addition to its analog output channel. When waveform generator **304** is appropriately programmed and its digital output pulses are appropriately spaced, image distortion can be eliminated.

[**0083**] Typically 4096 A/D conversions are performed per scan line, and if the user wants fewer than 4096 pixels/line the A/D conversions are binned by software in groups of 2 or more. For example, if the length of a scan line is 14 mm, the laser beam moves 3.4 microns between one A/D conversion and the next; and if, for example, the user chooses a pixel size of 13.6 microns, software adds the numbers from 4 A/D conversions for each pixel. One version of the software allows 8192 A/D conversions per scan line. The utility of doing more A/D conversions per line diminishes as the pixel size becomes less than the laser spot size.

[**0084**] Translation stages **332** (typically a 2-axis or 3-axis set of stages) are controlled by indexer **330**. Two axes of translation are usually used: a scan axis (parallel to the plane of the sample and perpendicular to the direction of motion of the laser spot), and a focus axis (parallel to the optical axis of lens **116**). A third axis orthogonal to the other two may also be desirable. Computer **302** sends commands to indexer **330**, and receives information about translation-stage status from indexer **330**, e.g., using an RS-232 interface. An indexer that communicates with computer **302** using another interface, such as a GPIB or ISA interface, could be used instead. Translation stage speed is set such that the distance that sample **118** moves per scan line is equal to the desired pixel size.

[**0085**] Software allows the user to control various scan parameters, including the size of the area to be scanned, the pixel size, the scan speed, and which output or outputs to digitize (either of the photomultiplier outputs, or the photodiode output, or a combination thereof). Default parameters are 14 mm×14 mm scan area, 10.2 micron pixel size, and scan speed of 30 lines/second. With these parameters, an image contains 1365×1365 pixels and can be acquired in about 45 seconds. These parameters are usually suitable for users who need to image 12.8 mm×12.8 mm oligonucleotide arrays having features that are approximately 100 μm×100 μm. Other scan parameters are suitable in other circumstances. The source code for this software is enclosed in Appendix A, of which is hereby incorporated herein by reference for all purposes.

[**0086**] For example, if the features are 400 μm×400 μm the user might choose a pixel size of 27.2 microns. In this case an image of a 14 mm×14 mm area contains 512×512 pixels and can be obtained in about 17 seconds. On the other hand, if the features are 30 μm×30 μm, the user might choose a pixel size of 3.4 microns. In this case an image of a 14 mm×14 mm area contains 4096×4096 pixels and can be acquired in about 2 minutes and 16 seconds. If an image with adequate signal-to-noise ratio is not obtained at a scan speed of 30 lines/second, the user might choose to reduce the scan speed, for example to 7.5 lines/second (quadrupling the scan time approximately quadruples the number of photons detected per pixel, and therefore in many cases approximately doubles the signal-to-noise ratio).

[**0087**] Scanned areas can vary from the 14 mm×14 mm dimensions described above, and need not be square. For example, software options can allow the user to reduce the length of a scan line, e.g., to as little as 4 mm or smaller if a user so desired, with a pixel size as small as 1 micron, and to set the number of lines per scan independently of the other scan parameters. In the galvanometer-scanned direction, a single scan can not cover a region that is larger than the field

of view of lens 116, e.g., 14 mm. However, the system may cover a region that is several inches wide in the orthogonal direction (limited only by the length of travel of the translation stage). Other software options allow users automatically to scan a chip several times, with any desired time interval between scans (useful for certain kinetics experiments), and automatically to scan several different chips on a wafer (useful for wafer inspection prior to dicing and packaging). Another option allows users to choose between 2 different output file formats: one format which saves "raw" data, with 2 bytes per pixel; and a space-saving format which saves "scaled" data, with one byte per pixel. A scaled data value is directly proportional to the square root of the raw data value. A lookup table for converting from scaled data back to raw data is stored in the file's header.

[0088] Referring to FIG. 2, a system and method for holding sample 118 within a flow cell will now be described. It should be clearly understood that the present invention is not limited to a flow cell. For example, the sample 118 may be part of a packaged chip, such as a diced chip glued into a disposable plastic package. A more complete description of a packaged chip can be found in commonly assigned, co-pending applications Ser. No. 08/485,452, filed Jun. 7, 1995 (Attorney Docket No. 16528X-006910), the complete disclosures of which are incorporated herein by reference for all purposes.

[0089] As shown, imaging system 100 further includes a body 422 for holding a support 430 containing the sample on a surface 431. In some embodiments, the support may be a microscope slide or any surface which is adequate to hold the sample. The body 422, depending on the application, may be a flow cell having a cavity 423. The flow cell, for example, may be employed to detect reactions between targets and probes. In some embodiments, the bottom of the cavity may comprise a light absorptive material so as to minimize the scattering of incident light.

[0090] In embodiments utilizing the flow cell, surface 431 is mated to body 422 and serves to seal cavity 423. The flow cell and the substrate may be mated for sealing with one or more gaskets. In one embodiment, the substrate is mated to the body by vacuum pressure generated by a pump 452. Optionally, the flow cell is provided with two concentric gaskets and the intervening space is held at a vacuum to ensure mating of the substrate to the gaskets. Alternatively, the substrate may be attached by using screws, clips, or other mounting techniques.

[0091] When mated to the flow cell, the cavity encompasses the sample. The cavity includes an inlet port 421 and an outlet port 420. A fluid, which in some embodiments contains fluorescently labeled targets, is introduced into the cavity through inlet port 421. A pump 453, which may be a model no. B-120-S made by Eldex Laboratories, circulates fluids into the cavity via inlet 421 port and out through outlet port 420 for recirculation or disposal. Alternatively, a syringe, gas pressure, or other fluid transfer device may be used to flow fluids into and through the cavity.

[0092] Optionally, pump 453 may be replaced by an agitation system that agitates and circulates fluids through the cavity. Agitating the fluids shortens the incubation period between the probes and targets. This can be best explained in terms of kinetics. A thin layer, known as the depletion layer, is located above the probe sample. Since targets

migrate to the surface and bind with the probe sequences, this layer is essentially devoid of targets. However, additional targets are inhibited from flowing into the depletion layer due to finite diffusion coefficients. As a result, incubation period is significantly increased. By using the agitation system to dissolve the depletion layer, additional targets are presented at the surface for binding. Ultrasonic radiation and/or heat, shaking the holder, magnetic beads, or other agitating technique may also be employed.

[0093] In some embodiments, the flow cell is provided with a temperature controller 450 for maintaining the flow cell at a desired temperature. Since probe/target interaction is sensitive to temperature, the ability to control it within the flow cell permits hybridization to be conducted under optimal temperature. The temperature controller 450 may include a circulating bath, a refrigerated air circulating device, resistance heater, peltier device (thermoelectric cooler), or other temperature controller may be implemented.

[0094] As previously mentioned, the flow cell is oriented to maintain the substrate perpendicular to the optical axis of the collection optics. According to one embodiment, flow cell 422 may be mounted to a translation stage 424 for moving the flow cell in an orthogonal direction relative to the optical path. The flow cell may be mated to the translation stage by vacuum pressure generated by pump 452. Alternatively, screws, clips or other mounting techniques may be employed to mate the flow cell to the translation stage.

[0095] IV. Detailed Description of an Alternative Embodiment of the Imaging System.

[0096] An optical block diagram of a second embodiment of imaging system 400 is shown in FIG. 4. As depicted, imaging system 400 comprises components which are common to the system described in FIG. 1. In this scanner, lens 116 is intended for use at a finite rather than an infinite conjugate ratio, and therefore lens 112 is omitted. This scanner uses only a single pinhole 401, and all of the remitted light passes through this pinhole 401 before being separated by the various dichroic beamsplitters. This scanner has 2 additional dichroic beamsplitters, spectral filters, and photomultipliers, and therefore can be used for 4-channel rather than merely 2-channel fluorescent scanning.

[0097] As discussed above in the previous embodiment, a beam of excitation radiation, e.g., 488-nm light, from a laser 102 is partially reflected and partially transmitted by a beamsplitter 104. The reflected portion of the beam impinges upon a photodetector 131 (optional), which is typically a photodiode used as a laser power monitor. The portion of the beam that is transmitted through beamsplitter 104 is reflected by dichroic beamsplitter 106 and transmitted through lens 111, focused onto pinhole 401, and expanded to the desired diameter at the entrance pupil lens 116.

[0098] The beam of excitation radiation is focused by lens 116 and scanned across the sample 118 by galvanometer mirror 114, as discussed above. Light remitted by sample 118 is collected by lens 116, reflected by mirror 114, and focused onto confocal pinhole 401. Light that is transmitted through pinhole 401 is collimated by lens 111. Remitted light having wavelengths less than 515 nm is reflected by beamsplitter 106 and partially reflected by beamsplitter 104; the light reflected by beamsplitter 104 impinges upon a

photodetector **130**. Remitted light having a wavelength above 515 passes through beamsplitter **106** and is sent to one of the four channels **402**, **404**, **406**, **408** depending on its wavelength. For example, imaging system **300** may be constructed such that remitted light having a wavelength between 515 and 545 is reflected by dichroic beamsplitter **410**, and passes through a filter **412** onto photodetector **414**. Remitted light having a wavelength between 545 and 570 nm, for example, may be reflected by dichroic beamsplitter **416**, where it passes through filter **418** and onto photodetector **420**. Similarly, beamsplitter **422** is constructed to reflect remitted light having wavelengths between 570 and 595 nm through filter **423** onto photodetector **426**. Remitted light having wavelengths greater than 595 nm are transmitted through beamsplitter **422**, to pass through filter **425** onto photodetector **424**.

[**0099**] The present invention is further illustrated by the following example. This example is merely to illustrate aspects of the present invention and is not intended as limitations of this invention.

EXAMPLE

[**0100**] A tiling array was designed for the entire human mitochondrial genome. See M. Chee et al., "Accessing genetic information with high-density DNA arrays", *Science*

vol. 274, pgs. 610-614 (1996). The array contained 134,688 different probe sequences, each occupying a separate 35 μm feature. The overall array dimensions were 1.28 cm \times 1.28 cm. Using long range PCR and RNA polymerase promoter tagged primers, a 16.3 kb fragment of mtDNA was amplified directly from genomic DNA samples. Labeled 16.3 kb RNA targets were prepared by in vitro transcription from the PCR amplicons and hybridized to the array.

[**0101**] A scanning system as described above was used to scan the array and a 4096 \times 4096 pixel image was obtained, each pixel representing 3.4 μm . The entire array was scanned in under three minutes. A close-up view of a scanned image of this array is shown in **FIG. 5**. The scanned image shown covers a 1.5 mm \times 1.5 mm segment of 14 mm \times 14 mm image of a 12.8 mm \times 12.8 mm array.

[**0102**] While the foregoing invention has been described in some detail for purposes of clarity and understanding, it will be clear to one skilled in the art from a reading of this disclosure that various changes in form and detail can be made without departing from the true scope of the invention. All publications and patent documents cited in this application are incorporated by reference in their entirety for all purposes to the same extent as if each individual publication or patent document were so individually denoted.


```

'automatically scans 1 to 4 chips
'includes code to set DIO24
'for 0.2 inch leadscrew instead of 5 mm leadscrew
'high resolution - 4096 pixels/line
'super VGA version - requires cbqbli.qlb

'$INCLUDE: '\galvo\CB.BI4'
DIM volt(1 TO 250), encoder(1 TO 250)
DIM dat%(1 TO 4096), dat2%(1 TO 4096)

DIM slide$(1 TO 4), seqfile$(1 TO 4), projseqstrand$(1 TO 4), targettype$(1
TO 4)
DIM targetconc$(1 TO 4), hybtimetemp$(1 TO 4), flowcellsoln$(1 TO 4),
temperature$(1 TO 4)
DIM opname$(1 TO 4), other$(1 TO 4)
DIM dye$(0 TO 1)

TYPE regtype
  ax AS INTEGER
  bx AS INTEGER
  cx AS INTEGER
  dx AS INTEGER
  bp AS INTEGER
  si AS INTEGER
  di AS INTEGER
  flags AS INTEGER
END TYPE
DIM inregs AS regtype, outregs AS regtype

'set default scan parameters
nscans% = 1
minutes = 2
pixelsize = 10.2
pixelsize% = 10
rows% = 1365
cols% = 1365
distance = 68535 '69632*.984252
surface$ = "2"
subdir$ = "generic"
datadir$ = "c:\galvo\data\generic"
filename$ = "test01"
nfilename$ = "test01.dat"
leftfilename$ = "test"
rightfilename$ = "01"
blank$ = " "
hoffset = 0
voffset = 0
focusoffset = 0
glassthickness% = 700
'4096 data points are acquired per line
'if pixel size > 3.4 then 2 or more data points are added for each pixel
'if pixel size < 13.6 then image is displayed at 1/2 or 1/4 resolution
screenres% = 2
col% = 341
binning% = 3
binning1% = 2
dye% = 1
speed$ = "30 "
dye$(0) = "555-607 nm (phycoerythrin)"
dye$(1) = "515-545 nm (fluorescein) "
focusxt$ = "c:\galvo\focus.txt"

'draw logo
SCREEN 12
LINE (219, 289)-(219, 189), 2
LINE -STEP(100, 0), 2
LINE -STEP(-100, 100), 2
PAINT (244, 239), 2
LINE (319, 189)-(419, 289), 8

```

```

LINE -STEP(0, -100), 8
LINE -STEP(-100, 100), 8
PAINT (394, 239), 8
SLEEP 1

GOSUB setfilters

CHDIR datadir$

start:
CLOSE #2
CLOSE #4
CLOSE #8
OPEN "com1:9600,n,8,1,cs0,ds0" FOR RANDOM AS #8
ON ERROR GOTO errorhandler
SCREEN 0, 0, 0
SCREEN 0, 1, 1

video$ = "normal"
COLOR 7
PRINT "number of chips to scan: "; nscans%
LOCATE 1, 41
PRINT "glass thickness (microns): "; CHR$(247); LTRIM$(STR$(glassthickness%))
LOCATE 9, 1
PRINT "bandpass filter: ";
IF dye% = 0 THEN COLOR 14 ELSE COLOR 10
PRINT dye$(dye%)
COLOR 7
PRINT "speed (lines per second): "; speed$
PRINT
PRINT "pixel size (microns):"; pixelsize
PRINT "number of scan lines: "; rows%
PRINT "surface to focus on: "; surface$
LOCATE 14, 43
PRINT "focus offset (microns):"; focusoffset
PRINT "horizontal offset (microns):          vertical offset (microns):";
voffset
LOCATE 15, 29
PRINT hoffset
PRINT "subdirectory for data file: "; subdir$
PRINT "file name: "; filename$
LOCATE 17, 43
PRINT "view or edit comments"
LOCATE 20, 1
PRINT "start scan"
LOCATE 20, 41
PRINT "exit to DOS temporarily"
PRINT "quit"
COLOR 6
LOCATE 1, 1
PRINT "r"
LOCATE 1, 41
PRINT "g"
LOCATE 3, 1
LOCATE 9, 2
PRINT "a"
LOCATE 10, 2
PRINT "d"
LOCATE 12, 3
PRINT "x"
LOCATE 13, 8
PRINT "o"
LOCATE 14, 3
PRINT "r"
LOCATE 14, 41
PRINT "z"
LOCATE 15, 1
PRINT "h"
LOCATE 15, 41

```

```

PRINT "v"
LOCATE 16, 3
PRINT "b"
PRINT "f"
LOCATE 17, 41
PRINT "j"
PRINT
PRINT
PRINT "s"
LOCATE 20, 63
PRINT "y"
PRINT "q"
COLOR 7

GOSUB setscanspeed

OPEN "c:\galvo\setup" FOR INPUT AS #5
'focusfactor=1 for 1-micron encoder, focusfactor=2 for 0.5-micron encoder
INPUT #5, focusmove, horizmove, vertmove, powerfactor, focusfactor,
granularity%
CLOSE #5

DO: LOOP UNTIL INKEY$ = ""
maininputloop:
DO
DO
a$ = LCASE$(INKEYS)
LOOP WHILE a$ = ""
SELECT CASE a$
CASE "n"
VIEW PRINT 23 TO 23
INPUT "number of chips to scan (1 min, 4 max)"; nscans1%
VIEW PRINT
IF nscans1% > 0 AND nscans1% < 5 THEN
nscans% = nscans1%
LOCATE 1, 25
PRINT nscans%
ELSE BEEP
END IF
CASE "g"
VIEW PRINT 23 TO 23
INPUT "approximate glass thickness in microns (100 min, 9999 max)";
glassthickness1%
VIEW PRINT
IF glassthickness1% > 99 AND glassthickness1% < 10000 THEN
glassthickness% = glassthickness1%
LOCATE 1, 69
PRINT " "
LOCATE 1, 69
PRINT LTRIM$(STR$(glassthickness%))
ELSE BEEP
END IF
CASE "a"
IF dye% = 1 THEN dye% = 0 ELSE dye% = 1
LOCATE 9, 18
IF dye% = 0 THEN COLOR 14 ELSE COLOR 10
PRINT dye$(dye%)
COLOR 7
CASE "p"
IF speed$ = "30 " THEN speed$ = "7.5" ELSE speed$ = "30 "
LOCATE 10, 27
PRINT speed$
GOSUB setscanspeed
GOSUB setfilters
CASE "x"
VIEW PRINT 23 TO 23
INPUT "pixel size in microns"; pixelsize
VIEW PRINT
pixelsize = INT(pixelsize / 3.4 + .5) * 3.4

```

```

IF pixelsize < 3.4 THEN pixelsize = 3.4
IF pixelsize > 27.2 THEN pixelsize = 27.2
LOCATE 12, 22
PRINT blank$
LOCATE 12, 22
PRINT pixelsize
pixelsize% = INT(pixelsize)
rows1% = INT(13926.4 / pixelsize + .1)
IF rows1% > 4092 THEN rows1% = 4092
VIEW PRINT 23 TO 23
DO
  PRINT "change number of scan lines to"; rows1%;
  INPUT a$
  a$ = LCASE$(a$)
  IF a$ <> "y" AND a$ <> "n" THEN BEEP
  LOOP UNTIL a$ = "y" OR a$ = "n"
  VIEW PRINT
  IF a$ = "y" THEN
    rows% = rows1%
    LOCATE 13, 22
    PRINT blank$
    LOCATE 13, 22
    PRINT rows%
    distance = INT(69632 * .984252 * rows% / 4096 * pixelsize / 3.4 + .5)
  END IF
  GOSUB setscanspeed
  cols% = INT(13926.4 / pixelsize + .1)
  screenres% = 1
  IF cols% > 1024 THEN
    screenres% = 2
    col% = 512
  END IF
  IF cols% = 1365 THEN col% = 341
  IF cols% = 4096 THEN
    screenres% = 4
    col% = 256
  END IF
  binning% = 4096 \ cols%
  binning1% = binning% - 1
CASE "o"
  VIEW PRINT 23 TO 23
  INPUT "number of scan lines"; rows%
  VIEW PRINT
  distance = INT(69632 * .984252 * rows% / 4096 * pixelsize / 3.4 + .5)
  IF rows% < 2 THEN rows% = 2
  IF rows% > 4092 THEN rows% = 4092
  LOCATE 13, 22
  PRINT blank$
  LOCATE 13, 22
  PRINT rows%
CASE "r"
  IF surface$ = "1" THEN surface$ = "2" ELSE surface$ = "1"
  LOCATE 14, 22
  PRINT surface$
CASE "z"
  VIEW PRINT 23 TO 23
  INPUT "focus offset (microns)"; focusoffset
  VIEW PRINT
  LOCATE 14, 66
  PRINT blank$
  LOCATE 14, 66
  PRINT focusoffset
CASE "h"
  VIEW PRINT 23 TO 23
  INPUT "horizontal offset (microns)"; hoffset
  VIEW PRINT
  LOCATE 15, 29
  PRINT blank$
  LOCATE 15, 29

```

```

PRINT hoffset
CASE "v"
VIEW PRINT 23 TO 23
INPUT "vertical offset (microns)"; voffset
VIEW PRINT
LOCATE 15, 67
PRINT blank$
LOCATE 15, 67
PRINT voffset
CASE "b"
SCREEN 0, 2, 2
CLS
PRINT "The following subdirectories exist:"
OPEN "c:\galvo\subdir.lst" FOR INPUT AS #1
DO UNTIL EOF(1)
    INPUT #1, a$
    PRINT a$; " ";
LOOP
CLOSE #1
PRINT
asksubdir:
INPUT "subdirectory for data file"; subdir$
subdir$ = LTRIM$(RTRIM$(subdir$))
datadir$ = "c:\galvo\data\" + subdir$
CHDIR datadir$
SCREEN 0, 1, 1
LOCATE 16, 29
PRINT blank$
LOCATE 16, 29
PRINT subdir$
SCREEN 0, 2, 2
FOR ch% = 1 TO 4
    slide$(ch%) = ""
    seqfile$(ch%) = ""
    projseqstrand$(ch%) = ""
    targettype$(ch%) = ""
    targetconc$(ch%) = ""
    flowcellsoln$(ch%) = ""
    temperature$(ch%) = ""
    opname$(ch%) = ""
    other$(ch%) = ""
    comment$(ch%) = ""
NEXT
ch% = 1
GOTO listfiles
CASE "f"
SCREEN 0, 2, 2
CLS
listfiles:
PRINT "Subdirectory " + subdir$ + " contains the following files:"
FILES "*.dat"
askfilename:
DO
IF nscans% > 1 THEN
PRINT "Last 2 characters in filename must be a number less than ";
num$ = LTRIM$(STR$(101 - nscans%))
IF 101 - nscans% < 10 THEN num$ = "0" + num$
PRINT num$
PRINT "and will be incremented by 1 for each scan."
END IF
DO
INPUT "filename (8 characters maximum)"; filename$
filename$ = LTRIM$(RTRIM$(filename$))
length% = LEN(filename$)
IF length% > 8 OR (length% < 3 AND nscans% > 1) OR length% < 1 THEN
PRINT "Too many or too few characters. Try again."
ELSEIF nscans% > 1 OR LEN(filename$) > 2 THEN
rightfilename$ = RIGHT$(filename$, 2)
leftfilename$ = LEFT$(filename$, length% - 2)

```

```

        nonnumeric% = 0
        IF nscans% > 1 THEN
            IF ASC(LEFT$(rightfilename$, 1)) < 48 OR ASC(LEFT$(rightfilename$, 1))
> 57 OR ASC(RIGHT$(rightfilename$, 1)) < 48 OR ASC(RIGHT$(rightfilename$, 1))
> 57 THEN
                PRINT "Last 2 characters must be numbers. Try again"
                nonnumeric% = 1
            ELSEIF VAL(rightfilename%) > 100 - nscans% THEN PRINT "Last 2
characters must be a number less than"; num$
            END IF
        END IF
    END IF
    LOOP UNTIL length% > 0 AND length% < 9 AND (nscans% = 1 OR (nonnumeric% =
0 AND VAL(rightfilename%) < 101 - nscans% AND length% > 2))
    nfilename$ = filename$ + ".dat"
    OPEN nfilename$ FOR BINARY AS #2
    IF LOF(2) = 0 THEN
        CLOSE #2
        EXIT DO
    END IF
    DO
        INPUT "file already exists - overwrite (y or n)"; a$
        a$ = LCASE$(a$)
        IF a$ <> "y" AND a$ <> "n" THEN PRINT "type a single character, either
y for yes or n for no"
        LOOP UNTIL a$ = "y" OR a$ = "n"
        CLOSE #2
        IF a$ = "y" THEN
            KILL nfilename$
            EXIT DO
        END IF
    LOOP
    SCREEN 0, 1, 1
    LOCATE 17, 12
    PRINT blank$
    LOCATE 17, 12
    PRINT filename$
CASE "j"
    SCREEN 0, 2, 2
structuredcomments:
    CLS
    IF ch% = 0 THEN ch% = 1
    COLOR 7
    PRINT "chip position: "; ch%
    COLOR 8
    PRINT "file name: ";
    IF ch% = 1 THEN
        PRINT filename$
    ELSEIF nscans% >= ch% THEN
        PRINT leftfilename$;
        a$ = LTRIM$(STR$(VAL(rightfilename%) + ch% - 1))
        IF VAL(a$) < 10 THEN a$ = "0" + a$
        PRINT a$
    ELSE PRINT
    END IF
    PRINT
    COLOR 7
    PRINT "slide number: "; slide$(ch%)
    PRINT "sequence file name: "; seqfile$(ch%)
    PRINT "project/sequence/strand: "; projseqstrand$(ch%)
    PRINT "target type: "; targettype$(ch%)
    PRINT "target concentration: "; targetconc$(ch%)
    PRINT "hybridization time and temperature: "; hybtimetemp$(ch%)
    PRINT "flow cell solution: "; flowcellsoln$(ch%)
    PRINT "scan temperature: "; temperature$(ch%)
    PRINT "operator name: "; opname$(ch%)
    PRINT "other comments: "; other$(ch%)
    PRINT
    PRINT "comment: "; LEFT$(comment$(ch%), 71)

```

```

PRINT MID$(comment$(ch%), 72, 80)
PRINT
PRINT
IF ch% > 1 THEN PRINT "copy comments from chip 1 to chip"; ch% ELSE PRINT
PRINT "erase all comments for chip"; ch%
PRINT "return to main menu"
COLOR 6
LOCATE 1, 3
PRINT "i"
LOCATE 4, 1
PRINT "s"
LOCATE 5, 3
PRINT "q"
PRINT "p"
LOCATE 7, 8
PRINT "t"
LOCATE 8, 8
PRINT "c"
PRINT "h"
PRINT "f"
LOCATE 11, 12
PRINT "a"
LOCATE 12, 10
PRINT "n"
PRINT "o"
LOCATE 15, 3
PRINT "m"
LOCATE 19, 4
IF ch% > 1 THEN PRINT "y" ELSE PRINT
PRINT "e"
PRINT "r"
COLOR 7
DO
  'GOSUB powermeasure
  'LOCATE 17, 13
  'PRINT power%; " "
  GOSUB shortdelay
  a$ = LCASE$(INKEY$)
  LOOP WHILE a$ = ""
  SELECT CASE a$
  CASE "i"
    VIEW PRINT 23 TO 23
    INPUT "chip position"; chl%
    VIEW PRINT
    IF chl% > 0 AND chl% < 5 THEN
      ch% = chl%
      GOTO structuredcomments
    ELSE BEEP
    END IF
  CASE "s"
    VIEW PRINT 23 TO 23
    INPUT "slide number"; slide$(ch%)
    IF LEN(slide$(ch%)) > 20 THEN slide$(ch%) = LEFT$(slide$(ch%), 20)
    VIEW PRINT
    LOCATE 4, 15
    PRINT blank$
    LOCATE 4, 15
    PRINT slide$(ch%)
  CASE "q"
    VIEW PRINT 23 TO 23
    INPUT "sequence file name"; seqfile$(ch%)
    IF LEN(seqfile$(ch%)) > 20 THEN seqfile$(ch%) = LEFT$(seqfile$(ch%), 20)
    VIEW PRINT
    LOCATE 5, 21
    PRINT blank$
    LOCATE 5, 21
    PRINT seqfile$(ch%)
  CASE "p"

```

```

VIEW PRINT 23 TO 23
LINE INPUT "project/sequence/strand? "; projseqstrand$(ch%)
projseqstrand$(ch%) = LTRIM$(RTRIM$(projseqstrand$(ch%)))
IF LEN(projseqstrand$(ch%)) > 20 THEN projseqstrand$(ch%) =
LEFT$(projseqstrand$(ch%), 20)
VIEW PRINT
LOCATE 6, 26
PRINT blank$; blank$
LOCATE 6, 26
PRINT projseqstrand$(ch%)
CASE "t"
VIEW PRINT 23 TO 23
LINE INPUT "target type? "; targettype$(ch%)
targettype$(ch%) = LTRIM$(RTRIM$(targettype$(ch%)))
IF LEN(targettype$(ch%)) > 20 THEN targettype$(ch%) =
LEFT$(targettype$(ch%), 20)
VIEW PRINT
LOCATE 7, 14
PRINT blank$; blank$
LOCATE 7, 14
PRINT targettype$(ch%)
CASE "c"
VIEW PRINT 23 TO 23
LINE INPUT "target concentration? "; targetconc$(ch%)
targetconc$(ch%) = LTRIM$(RTRIM$(targetconc$(ch%)))
IF LEN(targetconc$(ch%)) > 20 THEN targetconc$(ch%) =
LEFT$(targetconc$(ch%), 20)
VIEW PRINT
LOCATE 8, 23
PRINT blank$; blank$
LOCATE 8, 23
PRINT targetconc$(ch%)
CASE "h"
VIEW PRINT 23 TO 23
LINE INPUT "hybridization time and temperature? "; hybtimtemp$(ch%)
hybtimtemp$(ch%) = LTRIM$(RTRIM$(hybtimtemp$(ch%)))
IF LEN(hybtimtemp$(ch%)) > 20 THEN hybtimtemp$(ch%) =
LEFT$(hybtimtemp$(ch%), 20)
VIEW PRINT
LOCATE 9, 37
PRINT blank$; blank$
LOCATE 9, 37
PRINT hybtimtemp$(ch%)
CASE "f"
VIEW PRINT 23 TO 23
LINE INPUT "flow cell solution? "; flowcellsoln$(ch%)
flowcellsoln$(ch%) = LTRIM$(RTRIM$(flowcellsoln$(ch%)))
IF LEN(flowcellsoln$(ch%)) > 20 THEN flowcellsoln$(ch%) =
LEFT$(flowcellsoln$(ch%), 20)
VIEW PRINT
LOCATE 10, 21
PRINT blank$; blank$
LOCATE 10, 21
PRINT flowcellsoln$(ch%)
CASE "a"
VIEW PRINT 23 TO 23
LINE INPUT "scan temperature? "; temperature$(ch%)
temperature$(ch%) = LTRIM$(RTRIM$(temperature$(ch%)))
IF LEN(temperature$(ch%)) > 20 THEN temperature$(ch%) =
LEFT$(temperature$(ch%), 20)
VIEW PRINT
LOCATE 11, 19
PRINT blank$
LOCATE 11, 19
PRINT temperature$(ch%)
CASE "n"
VIEW PRINT 23 TO 23
LINE INPUT "operator name? "; opname$(ch%)
IF LEN(opname$(ch%)) > 20 THEN opname$(ch%) = LEFT$(opname$(ch%), 20)

```



```

VIEW PRINT
LOCATE 12, 16
PRINT blank$
LOCATE 12, 16
PRINT opname$(ch%)
CASE "o"
VIEW PRINT 23 TO 23
LINE INPUT "other comments? "; other$(ch%)
other$(ch%) = LTRIM$(RTRIM$(other$(ch%)))
IF LEN(other$(ch%)) > 40 THEN other$(ch%) = LEFT$(other$(ch%), 40)
VIEW PRINT
LOCATE 13, 17
PRINT blank$; blank$; blank$; blank$
LOCATE 13, 17
PRINT other$(ch%)
CASE "m"
VIEW PRINT 23 TO 25
LINE INPUT "comment (up to 151 characters)? "; comment$(ch%)
comment$(ch%) = LTRIM$(RTRIM$(comment$(ch%)))
comment$(ch%) = LEFT$(comment$(ch%), 151)
CLS 2
VIEW PRINT
LOCATE 15, 10
PRINT SPACE$(71)
PRINT SPACE$(80)
LOCATE 15, 10
PRINT LEFT$(comment$(ch%), 71)
PRINT MID$(comment$(ch%), 72, 80)
CASE "y"
IF ch% > 1 THEN
already$ = "n"
IF slide$(ch%) <> "" OR seqfile$(ch%) <> "" OR projseqstrand$(ch%) <>
"" OR targettype$(ch%) <> "" OR targetconc$(ch%) <> "" OR hybtimetemp$(ch%)
<> "" OR flowcellsoln$(ch%) <> "" OR temperature$(ch%) <> "" OR opname$(ch%)
<> "" OR other$(ch%)
<> "" OR comment$(ch%) <> "" THEN
already$ = "y"
VIEW PRINT 23 TO 23
INPUT "Do you really want to overwrite the comments that are already
here (y or n)"; a$
VIEW PRINT
IF LCASE$(a$) = "y" THEN already$ = "n"
END IF
IF already$ = "n" THEN
slide$(ch%) = slide$(1)
seqfile$(ch%) = seqfile$(1)
projseqstrand$(ch%) = projseqstrand$(1)
targettype$(ch%) = targettype$(1)
targetconc$(ch%) = targetconc$(1)
hybtimetemp$(ch%) = hybtimetemp$(1)
flowcellsoln$(ch%) = flowcellsoln$(1)
temperature$(ch%) = temperature$(1)
opname$(ch%) = opname$(1)
other$(ch%) = other$(1)
comment$(ch%) = comment$(1)
GOTO structuredcomments
END IF
ELSE BEEP
END IF
CASE "e"
VIEW PRINT 23 TO 23
INPUT "Do you really want to erase all comments for this chip (y or n)";
a$
VIEW PRINT
IF LCASE$(a$) = "y" THEN
slide$(ch%) = ""
seqfile$(ch%) = ""
projseqstrand$(ch%) = ""
targettype$(ch%) = ""

```

```

        targetconc$(ch%) = ""
        hybtimetemp$(ch%) = ""
        flowcellsoin$(ch%) = ""
        temperature$(ch%) = ""
        opname$(ch%) = ""
        other$(ch%) = ""
        comment$(ch%) = ""
        GOTO structuredcomments
    END IF
CASE "r"
    SCREEN 0, 1, 1
    GOTO maininputloop
CASE ELSE
    BEEP
END SELECT
LOOP
CASE "s"
    EXIT DO
CASE "y"
    SCREEN 0, 2, 2
    CLS
    DO
        SHELL "cd"
        LINE INPUT "enter a DOS command (or enter 'done')>"; dosstring$
        dosstring$ = LTRIM$(RTRIM$(LCASE$(dosstring$)))
        IF dosstring$ = "done" THEN EXIT DO
        IF dosstring$ = "scan" THEN
            BEEP
        ELSE IF dosstring$ <> "" THEN SHELL dosstring$
        END IF
        PRINT
    LOOP
    SHELL "c:"
    SHELL "\logout.bat"
    CHDIR datadir$
    SCREEN 0, 1, 1
CASE "q"
    a% = cbDDBitOut(1, AUXPORT, 0, 1)
    DO
        a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
        LOOP UNTIL bitval% = 1
    DO
        a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
        LOOP UNTIL bitval% = 0
        a% = cbDDBitOut(1, AUXPORT, 0, 0)
    SYSTEM
CASE ELSE
    BEEP
END SELECT
COLOR 7
LOOP
SCREEN 0, 2, 2
CLS

IF nscans% > 1 AND (LEN(filename$) < 3 OR ASC(LEFT$(rightfilename$, 1)) < 48
OR ASC(LEFT$(rightfilename$, 1)) > 57 OR ASC(RIGHT$(rightfilename$, 1)) < 48
OR ASC(RIGHT$(rightfilename$, 1)) > 57 OR VAL(rightfilename$) > 100 -
nscans%) THEN
    DO: LOOP UNTIL INKEY$ = ""
    PRINT "If you want to do"; nscans%; "scans, you must choose another file
name."
    PRINT "Press any key to return to menu."
    DO: LOOP WHILE INKEY$ = ""
    GOTO start
END IF
OPEN nfilename$ FOR BINARY AS #2
IF LOF(2) > 0 THEN
    DO
        PRINT "file " + filename$ + " already exists - overwrite (y or n)";

```

```

        INPUT a$
        a$ = LCASE$(a$)
        IF a$ <> "y" AND a$ <> "n" THEN PRINT "type a single character, either
y for yes or n for no"
        LOOP UNTIL a$ = "y" OR a$ = "n"
        CLOSE #2
        IF a$ = "y" THEN
            KILL nfilename$
        ELSE
            CLOSE #8
            GOTO start
        END IF
    END IF
END IF
CLOSE #2

dataline$ = SPACE$(cols% * 2)

'call interrupt 21H service 36H (get free disk space)
inregs.dx = 3 'drive a=1, b=2, c=3, etc.
inregs.ax = &H3600
CALL interrupt(&H21, inregs, outregs)
IF outregs.bx < 0 THEN outregs.bx = 65536 + outregs.bx ELSE outregs.bx =
outregs.bx
bytesfree& = outregs.bx& * outregs.ax * outregs.cx
bytesneeded& = (512& + 2& * rows% * cols%) * nscans%
IF bytesfree& < bytesneeded& THEN
    DO: LOOP UNTIL INKEY$ = ""
    BEEP
    PRINT
    PRINT "There is not enough space on the disk for your file";
    IF nscans% > 1 THEN PRINT "s." ELSE PRINT "."
    PRINT "You need"; bytesneeded&; "bytes but there are only"; bytesfree&;
"bytes available."
    PRINT
    PRINT "Press any key to return to menu."
    CLOSE #2
    CLOSE #4
    CLOSE #8
    DO: LOOP WHILE INKEY$ = ""
    GOTO start
END IF
IF bytesfree& < 10000000 THEN
    BEEP
    PRINT
    PRINT "There are only"; bytesfree&; "bytes free on the hard disk."
    PRINT "Delete some files soon."
    BEEP
    SLEEP 1
END IF

ON ERROR GOTO 0

PRINT
PRINT "scanspeed$="; scanspeed$

PRINT
PRINT "Stages are moving to their home positions. Please wait.":
PRINT "Press the F1 key for emergency stop."
KEY(1) ON
ON KEY(1) GOSUB emergencystop
PRINT #8, "mn j0 fsa0 fsb1 fsc0 a80 3gh-4 "
INPUT #8, echo$
'wait for stages to run into limit switches
DO
    SLEEP 1
    PRINT #8, "3r "
    GOSUB shortdelay
    GOSUB readr
LOOP UNTIL INSTR(r$, "3r *R") > 0

```

```

PRINT #8, "1gh-4 "
INPUT #8, echo$

'this stage has fixed limits, 2 home positions, therefore do this
PRINT #8, "2v4 2d100000 2g "
INPUT #8, echo$
DO
  SLEEP 1
  PRINT #8, "2r "
  GOSUB shortdelay
  GOSUB readr
LOOP UNTIL INSTR(r$, "2r *S") > 0 OR INSTR(r$, "2r *R") > 0

PRINT #8, "2gh4 "
INPUT #8, echo$
DO
  SLEEP 1
  PRINT #8, "1r "
  GOSUB shortdelay
  GOSUB readr
LOOP UNTIL INSTR(r$, "1r *R") > 0
DO
  PRINT #8, "2r "
  SLEEP 1
  GOSUB shortdelay
  GOSUB readr
LOOP UNTIL INSTR(r$, "2r *R") > 0

'GOSUB powermeasure
PRINT
'PRINT "power="; power%; "uW"
'PRINT USING "noise= ### mV"; noise * 1000
'GOSUB shortdelay
'PRINT
DO: LOOP UNTIL INKEY$ = ""
PRINT "Load sample. Press any key when done."
'cursorline% = CSRLIN
'cursorline% = cursorline% - 4
DO
  ' GOSUB powermeasure
  ' LOCATE cursorline%, 7
  ' PRINT power%; "uW "
  ' LOCATE cursorline% + 1, 7
  ' PRINT USING "### mV"; noise * 1000
LOOP WHILE INKEY$ = ""
'LOCATE CSRLIN + 2, 1
PRINT "Stages are moving. Please wait."
horizmove = INT(horizmove - voffset)
vertmove = INT(vertmove + hoffset)
a$ = LTRIM$(STR$(focusmove + (700 - glassthickness%) * focusfactor))
PRINT #8, "v6 1d" + a$ + " 1g 2d" + LTRIM$(STR$(horizmove)) + " 2g "
INPUT #8, echo$
GOSUB waitloop1
GOSUB waitloop2
PRINT #8, "3d" + LTRIM$(STR$(vertmove)) + " 3g fsb0 "
INPUT #8, echo$
GOSUB waitloop3
PRINT #8, "2a80 2v10 2d" + LTRIM$(STR$(INT(69632 * (1 - rows% / 4096 *
pixelsize / 3.4) + .5))) + " 2g "
INPUT #8, echo$
GOSUB waitloop2

OPEN focustxt$ FOR OUTPUT AS #7
PRINT #7, "chip relative focus positions (microns)"
PRINT #7, "-----"
CLOSE #7

FOR ch% = 1 TO nscans%

```

```

IF ch% > 1 THEN
PRINT #8, "2v10 2a80 2d-250000 2g "
INPUT #8, echo$
IF surface$ = "1" THEN
PRINT #8, "1v10 1d-2000 1g "
ELSE
PRINT #8, "1v10 1d-4000 1g "
END IF
INPUT #8, echo$
GOSUB waitloop1
GOSUB waitloop2
SLEEP 1
END IF

IF ch% > 1 THEN
rightfilename$ = LTRIM$(STR$(VAL(rightfilename$) + 1))
IF VAL(rightfilename$) < 10 THEN rightfilename$ = "0" + rightfilename$
filename$ = leftfilename$ + rightfilename$
nfilename$ = filename$ + ".dat"
END IF

a% = cbDDBitOut(1, AUXPORT, 0, 1)

'IF ch% = 1 OR bath$ = "y" THEN
DO
a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 1
DO
a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 0
a% = cbDDBitOut(1, AUXPORT, 0, 0)
focusmax = 0
focusmin = 199999
misfocusthreshold = 50
'find focus at 2 sides of area to be scanned
IF ch% = 1 THEN
PRINT
PRINT "Finding focus. Please wait.";
END IF
logfile$ = "c:\galvo\galvo.log"
OPEN logfile$ FOR APPEND AS #3
PRINT #3, " "
PRINT #3, subdir$, nfilename$, DATE$, TIME$
CLOSE #3
GOSUB findfocus
secondfocus = focus
OPEN logfile$ FOR APPEND AS #3
PRINT #3, "focus x0 ";
PRINT #3, USING "##### ###.# "; focus / focusfactor; x0;
CLOSE #3
IF surface$ = "1" THEN
PRINT #8, "1v10 1d-1000 1g "
ELSE
steps$ = "3000"
IF glassthickness% > 700 THEN steps$ = LTRIM$(STR$(3000 +
(glassthickness% - 700) * 5 / 1.5))
PRINT #8, "1v10 1d-" + steps$ + " 1g "
END IF
INPUT #8, echo$
PRINT #8, "2a80 2v10 2d" + LTRIM$(STR$(distance)) + " 2g " '70550
INPUT #8, echo$
GOSUB waitloop2
GOSUB findfocus
firstfocus = focus
OPEN logfile$ FOR APPEND AS #3
PRINT #3, USING "##### ###.# "; focus / focusfactor; x0
CLOSE #3
IF ch% = 1 THEN
PRINT

```

```

PRINT "focus positions vary by"; focusrange / focusfactor; "microns";
PRINT
focuszero = secondfocus
END IF
OPEN focustxt$ FOR APPEND AS #7
PRINT #7, USING "### #####"; ch%; (secondfocus -
focuszero) / focusfactor; (firstfocus - focuszero) / focusfactor
CLOSE #7
a% = cbDBitOut(1, AUXPORT, 0, 1)
scantime = 136.5333 * rows% / 4096
IF speed$ = "7.5" THEN scantime = scantime * 4
focussteps = INT(5 * (secondfocus - firstfocus) / focusfactor)
focussteps$ = LTRIM$(STR$(focussteps))
focusspeed = ABS(focussteps / scantime / 25000) + .000005
focusspeed$ = ". "
FOR i% = 1 TO 5
IF focusspeed < 10 ^ (i% - 6) THEN EXIT FOR
focusspeed = focusspeed * 10
MID$(focusspeed$, i% + 1, 1) = LTRIM$(STR$(INT(focusspeed)))
focusspeed = focusspeed - INT(focusspeed)
NEXT i%
focusspeed$ = RTRIM$(focusspeed$)
'because focusspeed is in multiples of .00001, time needed to move
'focussteps can be much greater than scantime in some cases
IF VAL(focusspeed$) > 0 THEN
actualtime = ABS((focussteps / 25000) / VAL(focusspeed$))
IF actualtime > scantime + 5 THEN
focussteps = INT(focussteps * scantime / actualtime)
focussteps$ = LTRIM$(STR$(focussteps))
END IF
END IF
IF ch% = 1 THEN PRINT "focussteps$="; focussteps$, "focusspeed$=";
focusspeed$;
'ELSE
PRINT #8, "2a80 2v10 2d" + LTRIM$(STR$(distance)) + " 2g " '70550
INPUT #8, echo$
GOSUB waitloop2
'END IF

'move focus stage to starting position
IF firstfocus < secondfocus THEN
PRINT #8, "1a10 1v1 1d-4000 lg "
INPUT #8, echo$
GOSUB waitloop1
PRINT #8, "1d3000 lg "
INPUT #8, echo$
GOSUB waitloop1
GOSUB read1
PRINT #8, "1d" + LTRIM$(STR$(5 * (firstfocus - VAL(a$)) / focusfactor -
100)) + " lg "
INPUT #8, echo$
ELSE
PRINT #8, "1a10 1v1 1d4000 lg "
INPUT #8, echo$
GOSUB waitloop1
PRINT #8, "1d-3000 lg "
INPUT #8, echo$
GOSUB waitloop1
GOSUB read1
PRINT #8, "1d" + LTRIM$(STR$(5 * (firstfocus - VAL(a$)) / focusfactor +
100)) + " lg "
INPUT #8, echo$
END IF
GOSUB read1
PRINT #8, "1d" + LTRIM$(STR$(5 * (firstfocus - VAL(a$)) / focusfactor)) + "
lg "
INPUT #8, echo$
GOSUB waitloop1

```

```

PRINT #8, "ld" + focussteps$ + " lv" + focusspeed$ + " 2a2 2d-" +
LTRIM$(STR$(distance)) + " 2v" + scanspeed$ + " "
INPUT #8, echo$

SHELL "if exist e:tempfile.dat del e:tempfile.dat>c:\junk\junk"
OPEN "e:tempfile.dat" FOR BINARY AS #2
a$ = " "
FOR i% = 1 TO 100
  PUT #2, i%, a$
NEXT
a$ = STRING$(1, 0)
FOR i% = 101 TO 512
  PUT #2, i%, a$
NEXT
a$ = CHR$(252)
PUT #2, 1, a$
PUT #2, , cols%
PUT #2, , rows%
totalpoints% = 1& * rows% * cols%
PUT #2, , totalpoints%
OPEN logfile$ FOR APPEND AS #3
b$ = "CLS=" + LTRIM$(STR$(cols%))
PUT #2, 34, b$
PRINT #3, b$ + " ";
b$ = "RWS=" + LTRIM$(STR$(rows%))
PUT #2, 43, b$
PRINT #3, b$ + " ";
b$ = "SIZ=" + LTRIM$(STR$(pixelsize%))
PUT #2, 52, b$
PRINT #3, b$ + " ";
b$ = "VE=" + scanspeed2$
PUT #2, 59, b$
PRINT #3, b$ + " ";
'b$ = LTRIM$(STR$(power%))
'PUT #2, 79, b$
PRINT #3, ' "power=" + b$
CLOSE #3
b$ = MID$(DATE$, 1, 6) + MID$(DATE$, 9, 2)
PUT #2, 83, b$
b$ = TIME$
PUT #2, 92, b$

delim$ = " " + CHR$(20) + " "
IF comment$(ch%) = "" THEN comment$(ch%) = " "
PUT #2, 101, comment$(ch%)
IF slide$(ch%) <> "" OR seqfile$(ch%) <> "" OR projseqstrand$(ch%) <> "" OR
targettype$(ch%) <> "" OR targetconc$(ch%) <> "" OR hybtimetemp$(ch%) <> ""
OR flowcellsoln$(ch%) <> "" OR opname$(ch%) <> "" OR other$(ch%) <> "" OR
temperature$(ch%) <> "" -
THEN
  PUT #2, , delim$
  PUT #2, , slide$(ch%)
  PUT #2, , delim$
  PUT #2, , seqfile$(ch%)
  PUT #2, , delim$
  PUT #2, , projseqstrand$(ch%)
  PUT #2, , delim$
  PUT #2, , targettype$(ch%)
  PUT #2, , delim$
  PUT #2, , targetconc$(ch%)
  PUT #2, , delim$
  PUT #2, , hybtimetemp$(ch%)
  PUT #2, , delim$
  PUT #2, , flowcellsoln$(ch%)
  PUT #2, , delim$
  PUT #2, , temperature$(ch%)
  PUT #2, , delim$
  PUT #2, , opname$(ch%)
  PUT #2, , delim$

```

```

    PUT #2, , other$(ch%)
    PUT #2, , delim$
END IF
CLOSE #2

IF ch% = 1 THEN
'change video mode to 1024 x 768
inregs.ax = &H4F02
inregs.bx = &H105
CALL interrupt(&H10, inregs, outregs)
'set up gray scale
inregs.ax = &H1010
FOR i% = 0 TO 15
    inregs.bx = i%
    inregs.cx = 1028 * i%
    inregs.dx = 1024 * i%
    CALL interrupt(&H10, inregs, outregs)
NEXT
video$ = "svga"
END IF

a$ = "line          max          min          line ave          scan ave
chip"
a$ = a$ + STR$(ch%)
inregs.dx = 12032
GOSUB svgaprint

GOSUB takedata
inregs.dx = 12032
a$ = SPACE$(80)
GOSUB svgaprint
a$ = LTRIM$(STR$(highclip&)) + " pixels clipped high," + STR$(lowclip&) + "
pixels clipped low"
IF ch% = nscans% THEN a$ = a$ + ".    Copying data to disk.  Please wait."
GOSUB svgaprint
SHELL "move e:tempfile.dat " + datadir$ + "\" + nfilename$ + " >c:\junk\junk"
NEXT ch%
ch% = 1
DO: LOOP UNTIL INKEY$ = ""
a$ = LTRIM$(STR$(highclip&)) + " pixels clipped high," + STR$(lowclip&) + "
pixels clipped low"
CLOSE #4
PRINT #8, "3v6 3d-700000 3g "
INPUT #8, echo$
DO
    a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 1
DO
    a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 0
a% = cbDDBitOut(1, AUXPORT, 0, 0)
a$ = a$ + ".    Done with scan.  Press any key to continue."
GOSUB svgaprint
DO: LOOP WHILE INKEY$ = ""
a$ = SPACE$(120)
GOSUB svgaprint
a$ = "quit (y or n)?"
GOSUB svgaprint
GOSUB shortdelay
DO: LOOP UNTIL INKEY$ = ""
DO
    y$ = LCASE$(INKEY$)
    LOOP WHILE y$ = ""
    IF y$ <> "y" AND y$ <> "n" THEN BEEP
LOOP UNTIL y$ = "y" OR y$ = "n"
CLOSE #8
IF nscans% > 1 THEN
    SCREEN 0, 0, 0

```



```

SHELL "type " + focustxt$
PRINT
PRINT
PRINT "Press any key to continue."
DO: LOOP UNTIL INKEY$ = ""
DO: LOOP WHILE INKEY$ = ""
END IF
IF y$ = "n" THEN GOTO start
SCREEN 0, 0, 0
a% = cbDBitOut(1, AUXPORT, 0, 1)
DO
  a% = cbDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 1
DO
  a% = cbDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 0
a% = cbDBitOut(1, AUXPORT, 0, 0)
SYSTEM

coarsefocus:
'scan through peak
delaytime = .2
GOSUB delay
vmax = -1
PRINT #8, "1fsa0 1fsb0 1fsc0 1v.2 1d25 "
INPUT #8, echo$
DO
  PRINT #8, "1g "
  INPUT #8, echo$
  GOSUB waitloop1
  sum = 0
  FOR i% = 1 TO 100
    a% = cbAIn(1, 2, BIPPT625VOLTS, voltage%)
    sum = sum + voltage%
  NEXT
  IF sum > vmax THEN vmax = sum
LOOP WHILE sum + 500 > vmax
PRINT #8, "1g "
INPUT #8, echo$
GOSUB waitloop1
RETURN

findfocus:
'find surface 1
GOSUB coarsefocus
'find surface 2 if necessary
IF surface$ = "2" THEN
  PRINT #8, "1d" + LTRIM$(STR$(INT(glassthickness% * 2.14))) + " 1g "
  INPUT #8, echo$
  GOSUB waitloop1
  GOSUB coarsefocus
END IF
GOSUB delay
SLEEP 1
'scan back through focus in 1 micron steps
PRINT #8, "1d-5 "
INPUT #8, echo$
vmax = -1
nstep = 0
DO
  PRINT #8, "1g "
  INPUT #8, echo$
  GOSUB waitloop1
  nstep = nstep + 1
  voltsum = 0
  FOR k% = 1 TO 100
    a% = cbAIn(1, 2, BIPPT625VOLTS, voltage%)
    voltsum = voltsum + voltage%
  NEXT k%

```

```

IF voltsum > vmax THEN
  vmax = voltsum
  npeak = nstep
END IF
volt(nstep) = voltsum
GOSUB read1
encoder(nstep) = VAL(a$)
LOOP WHILE voltsum + 500 > vmax
GOSUB read1
posnow = VAL(a$)
GOSUB fitparabola
RETURN

fitparabola:
xsum# = 0
ysum# = 0
xysum# = 0
x2sum# = 0
x2ysum# = 0
x3sum# = 0
x4sum# = 0
numpoints = 2 * (nstep - npeak) + 1
IF ch% = 1 THEN PRINT
FOR n = nstep - numpoints + 1 TO nstep
  y = volt(n)
  IF ch% = 1 THEN PRINT n, y
  xsum# = xsum# + n
  ysum# = ysum# + y
  xysum# = xysum# + n * y
  x2sum# = x2sum# + n * n
  x2ysum# = x2ysum# + n * n * y
  x3sum# = x3sum# + n * n * n
  x4sum# = x4sum# + n * n * n * n
NEXT
factor# = x3sum# - x2sum# * xsum# / numpoints
denom# = x2sum# - xsum# * xsum# / numpoints
quotient# = (xysum# - xsum# * ysum# / numpoints) / denom#
quotient2# = factor# / denom#
anum# = x2ysum# - x3sum# * quotient# - x2sum# / numpoints * (ysum# - xsum#
* quotient#)
adenom# = x4sum# - x3sum# * quotient2# + x2sum# / numpoints * (xsum# *
quotient2# - x2sum#)
a# = anum# / adenom#
b# = (xysum# - a# * factor# - xsum# * ysum# / numpoints) / denom#
x0 = -b# / 2 / a#
focus = encoder(INT(x0 + .5)) + focusoffset * focusfactor
IF ch% = 1 THEN PRINT "x0="; x0, "focus="; focus / focusfactor;
IF ch% = 1 THEN
  IF x0 < 10 THEN
    PRINT
    PRINT
    PRINT "Autofocus error: x0 < 10."
    PRINT "c = continue anyway, t = try again, s = stop."
    DO: LOOP UNTIL INKEY$ = ""
    DO
      INPUT "c, t, or s"; a$
      a$ = LCASE$(a$)
      IF a$ <> "c" AND a$ <> "t" AND a$ <> "s" THEN PRINT "Enter a single
character, either c or t or s."
      LOOP UNTIL a$ = "c" OR a$ = "t" OR a$ = "s"
      IF a$ = "s" THEN
        CLOSE #2
        CLOSE #4
        CLOSE #8
        GOTO start
      ELSEIF a$ = "t" THEN
        IF surface$ = "1" THEN
          PRINT #8, "1v10 1d-1000 1g "
          INPUT #8, echo$

```

```

        ELSE
        PRINT #8, "1v10 1d-3000 1g "
        INPUT #8, echo$
        END IF
        SLEEP 1
        GOTO findfocus
    END IF
END IF
IF focus > focusmax THEN focusmax = focus
IF focus < focusmin THEN focusmin = focus
focusrange = focusmax - focusmin
IF focusrange / focusfactor > misfocusthreshold THEN
PRINT
PRINT
IF focusrange < 100 THEN PRINT "Possible a"; ELSE PRINT "A";
PRINT "utofocus error. Focus positions vary by"; focusrange /
focusfactor; "microns."
DO: LOOP UNTIL INKEY$ = ""
DO
    INPUT "Continue anyway (y or n)"; a$
    a$ = LCASE$(a$)
    IF a$ <> "y" AND a$ <> "n" THEN PRINT "Enter a single character, either
y for yes or n for no."
    LOOP UNTIL a$ = "y" OR a$ = "n"
    IF a$ = "y" THEN
        misfocusthreshold = focusrange / focusfactor
    ELSE
        CLOSE #2
        CLOSE #4
        CLOSE #8
        GOTO start
    END IF
END IF
END IF
RETURN

waitloop1:
'wait for stage to stop moving
DO
    r$ = SPACE$(10)
    PRINT #8, "1r "
    GOSUB readr
    LOOP UNTIL INSTR(r$, "1r *R") > 0
    RETURN

waitloop3:
DO
    r$ = SPACE$(10)
    PRINT #8, "3r "
    GOSUB readr
    LOOP UNTIL INSTR(r$, "3r *R") > 0
    RETURN

waitloop2:
DO
    r$ = SPACE$(10)
    PRINT #8, "2r "
    GOSUB readr
    LOOP UNTIL INSTR(r$, "2r *R") > 0
    RETURN

readr:
INPUT #8, r$, junk$
RETURN

read1:
PRINT #8, "1x4 "
INPUT #8, echo$, a$
RETURN

```

```

read3:
b$ = SPACE$(20)
PRINT #8, "3x4 "
INPUT #8, echo$, b$
RETURN

errorhandler:
IF ERR = 76 THEN
DO
INPUT "subdirectory does not exist - create it (y or n)"; a$
a$ = LCASE$(a$)
IF a$ <> "y" AND a$ <> "n" THEN PRINT "enter a single character, either
y for yes or n for no"
LOOP UNTIL a$ = "y" OR a$ = "n"
IF a$ = "y" THEN
MKDIR datadir$
CHDIR datadir$
OPEN "c:\galvo\subdir.lst" FOR APPEND AS #1
PRINT #1, subdir$
CLOSE #1
RESUME NEXT
ELSE RESUME asksubdir
END IF
ELSEIF ERR = 53 THEN
PRINT "none"
RESUME NEXT
ELSE ON ERROR GOTO 0
END IF

shortdelay:
time = TIMER
DO
IF TIMER < time THEN time = time - 86400
LOOP UNTIL TIMER > time + .1
RETURN

delay:
time = TIMER
DO
IF TIMER < time THEN time = time - 86400
LOOP UNTIL TIMER > time + delaytime
RETURN

emergencystop:
PRINT #8, "s "
INPUT #8, echo$
a% = cbStopBackground(1)
KEY(1) OFF
CLOSE #2
SHELL "if exist e:tempfile.dat move e:tempfile.dat " + datadir$ + "\" +
nfilename$ + " >c:\junk\junk"
IF logfile$ = "c:\galvo\galvo.log" THEN
OPEN logfile$ FOR APPEND AS #3
PRINT #3, "scan interrupted by user at "; TIME$
CLOSE #3
END IF
CLOSE #4
CLOSE #7
CLOSE #8
DO: LOOP UNTIL INKEY$ = ""
IF video$ = "normal" THEN
PRINT
PRINT "Scan interrupted by user. Press any key to return to menu.";
ELSE
inregs.dx = 12032
a$ = SPACE$(120)
GOSUB svgaprint
a$ = "Scan interrupted by user. Press any key to return to menu."
GOSUB svgaprint

```

```

END IF
DO: LOOP WHILE INKEY$ = ""
RETURN start

powermeasure:
'find laser power
'sum = 0
'FOR i% = 1 TO 100
'  'status = AI.VRead(1, 0, 20, voltage#)
'  sum = sum + voltage#
'NEXT
'power% = INT(sum * 10 * powerfactor + .5)
'Gain% = 100
'IF power% > 15 THEN Gain% = 50
'IF power% > 30 THEN Gain% = 20
'FOR i% = 1 TO 100
'  'status = AI.VRead(1, 1, gain%, voltage#)
'NEXT i%

'find noise
'max = -1
'min = 1
'FOR i% = 1 TO 100
'  'status = AI.VRead(1, 1, gain%, voltage#)
'  IF voltage# > max THEN max = voltage#
'  IF voltage# < min THEN min = voltage#
'NEXT i%
'noise = max - min
'IF noise < .0001 THEN noise = .0001
'RETURN

takedata:
'skip scan if focus positions vary by >100 microns
'IF ch% > 1 AND ABS((firstfocus - secondfocus) / focusfactor) > 100 THEN
  PRINT #8, "2a80 2v10 2d-" + LTRIM$(STR$(distance)) + " 2g "
  OPEN focustxt$ FOR APPEND AS #7
  PRINT #7, "probable autofocus error - did not scan chip"; ch%
  CLOSE #7
  OPEN logfile$ FOR APPEND AS #3
  PRINT #3, "probable autofocus error - did not scan chip"
  CLOSE #3
  GOTO skippedscan
END IF
OPEN "e:tempfile.dat" FOR BINARY AS #2
a$ = " "
PUT #2, 512, a$

ave% = 1000
sum = 0
TotalCount& = 4096
Gain% = UNI2PT5VOLTS
Options% = BACKGROUND + EXTCLOCK + CONVERTDATA
BitNum% = 0

lowclip& = 0
highclip& = 0
OPEN logfile$ FOR APPEND AS #3
scanstarttime = TIMER
PRINT #3, "starting scan at "; TIMER'$
CLOSE #3
DO
  a% = cbDBitIn(1, AUXPORT, 1, bitval%)
  LOOP UNTIL bitval% = 0
DO
  a% = cbDBitIn(1, AUXPORT, 1, bitval%)
  LOOP UNTIL bitval% = 1
  PRINT #8, "2g 1g "
DO

```

```

    a% = cbDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 1

DO
    a% = cbDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 0

UDStat% = cbAInScan(1, dye%, dye%, TotalCount%, 10000%, Gain%, dat%(1),
Options%)
IF UDStat% <> 0 THEN
    PRINT
    PRINT "error"; UDStat%;
    DO: LOOP UNTIL INKEY$ = ""
    PRINT ". Press any key to continue.";
    CLOSE #2
    DO: LOOP WHILE INKEY$ = ""
    PRINT
    GOTO start
END IF
DO
    UDStat% = cbGetStatus(1, Status%, CurCount%, CurIndex%)
LOOP UNTIL Status% = IDLE

DO
    a% = cbDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 0

UDStat% = cbAInScan(1, dye%, dye%, TotalCount%, 10000%, Gain%, dat2%(1),
Options%)
IF UDStat% <> 0 THEN
    PRINT
    PRINT "error"; UDStat%;
    DO: LOOP UNTIL INKEY$ = ""
    PRINT ". Press any key to continue.";
    CLOSE #2
    DO: LOOP WHILE INKEY$ = ""
    PRINT
    GOTO start
END IF

FOR j% = 1 TO rows%
    max% = 0
    min% = 32767
    jj% = j% \ screenres% MOD 752
    linesum% = 0
    DEF SEG = VARSEG(dataline$)
    address% = SADD(dataline$)
    IF j% MOD 2 = 0 THEN
        FOR i% = binning% TO cols% * binning% STEP binning%
            SELECT CASE binning%
            CASE 1
                a% = dat2%(i%)
                IF a% = 4095 THEN highclip% = highclip% + 1
                IF a% = 0 THEN lowclip% = lowclip% + 1
            CASE 2
                c% = dat2%(i%)
                b% = dat2%(i% - 1)
                IF b% = 4095 OR c% = 4095 THEN highclip% = highclip% + 1
                IF b% = 0 OR c% = 0 THEN lowclip% = lowclip% + 1
                a% = b% + c%
                dat2%(i% \ 2) = a%
            CASE 3
                d% = dat2%(i%)
                c% = dat2%(i% - 1)
                b% = dat2%(i% - 2)
                IF b% = 4095 OR c% = 4095 OR d% = 4095 THEN highclip% = highclip% + 1
                IF b% = 0 OR c% = 0 OR d% = 0 THEN lowclip% = lowclip% + 1
                a% = b% + c% + d%
                dat2%(i% \ 3) = a%
            END SELECT
        NEXT i%
    END IF
NEXT j%

```

```

CASE ELSE
a% = 0
lowclip% = 0
highclip% = 0
FOR k% = 0 TO binning1%
  b% = dat2%(i% - k%)
  a% = a% + b%
  IF b% = 4095 THEN highclip% = 1
  IF b% = 0 THEN lowclip% = 1
NEXT
IF highclip% = 1 THEN highclip& = highclip& + 1
IF lowclip% = 1 THEN lowclip& = lowclip& + 1
dat2%(i% \ binning%) = a%
END SELECT
IF a% > max% THEN max% = a%
IF a% < min% THEN min% = a%
linesum& = linesum& + a%
POKE address%, PEEK(VARPTR(a%))
address% = address% + 1
POKE address%, PEEK(VARPTR(a%) + 1)
address% = address% + 1
NEXT i%
ELSE
FOR i% = binning% TO cols% * binning% STEP binning%
SELECT CASE binning%
CASE 1
a% = dat%(i%)
IF a% = 4095 THEN highclip& = highclip& + 1
IF a% = 0 THEN lowclip& = lowclip& + 1
CASE 2
c% = dat%(i%)
b% = dat%(i% - 1)
IF b% = 4095 OR c% = 4095 THEN highclip& = highclip& + 1
IF b% = 0 OR c% = 0 THEN lowclip& = lowclip& + 1
a% = b% + c%
dat%(i% \ 2) = a%
CASE 3
d% = dat%(i%)
c% = dat%(i% - 1)
b% = dat%(i% - 2)
IF b% = 4095 OR c% = 4095 OR d% = 4095 THEN highclip& = highclip& + 1
IF b% = 0 OR c% = 0 OR d% = 0 THEN lowclip& = lowclip& + 1
a% = b% + c% + d%
dat%(i% \ 3) = a%
CASE ELSE
a% = 0
lowclip% = 0
highclip% = 0
FOR k% = 0 TO binning1%
  b% = dat%(i% - k%)
  a% = a% + b%
  IF b% = 4095 THEN highclip% = 1
  IF b% = 0 THEN lowclip% = 1
NEXT
IF highclip% = 1 THEN highclip& = highclip& + 1
IF lowclip% = 1 THEN lowclip& = lowclip& + 1
dat%(i% \ binning%) = a%
END SELECT
IF a% > max% THEN max% = a%
IF a% < min% THEN min% = a%
linesum& = linesum& + a%
POKE address%, PEEK(VARPTR(a%))
address% = address% + 1
POKE address%, PEEK(VARPTR(a%) + 1)
address% = address% + 1
NEXT i%
END IF
DEF SEG = &HA000
row% = jj% MOD 64

```

```

inregs.dx = inregsdx
IF row% = 0 OR j% = 1 THEN
  inregs.dx = jj% \ granularity%
  inregsdx = inregs.dx
END IF
inregs.ax = &H4F05
inregs.bx = 0
CALL interrupt(&H10, inregs, outregs)
SELECT CASE screenres%
CASE 1
  address% = 1024& * row%
  SELECT CASE j% MOD 2
  CASE 0
    FOR i% = 1 TO cols%
      color1% = 1& * dat2%(i%) * 7 \ ave%'7 was 5
      IF color1% > 15 THEN color1% = 15
      POKE address%, color1%
      address% = address% + 1
    NEXT
  CASE 1
    FOR i% = 1 TO cols%
      color1% = 1& * dat%(i%) * 7 \ ave% '7 was 5
      IF color1% > 15 THEN color1% = 15
      POKE address%, color1%
      address% = address% + 1
    NEXT
  END SELECT
CASE 2
  SELECT CASE j% MOD 2
  CASE 0
    address% = 1024& * row%
    FOR i% = 2 TO cols% \ 2 STEP 2
      color1% = 1& * dat2%(i%) * 7 \ ave%'7 was 5
      IF color1% > 15 THEN color1% = 15
      POKE address%, color1%
      address% = address% + 1
    NEXT
  CASE 1
    address% = 1024& * row% + col%
    FOR i% = cols% \ 2 + 2 TO cols% STEP 2
      color1% = 1& * dat%(i%) * 7 \ ave% '7 was 5
      IF color1% > 15 THEN color1% = 15
      POKE address%, color1%
      address% = address% + 1
    NEXT
  END SELECT
CASE 4
  SELECT CASE j% MOD 4
  CASE 0
    address% = 1024& * row%
    FOR i% = 4 TO cols% \ 4 STEP 4
      color1% = dat2%(i%) * 7 \ ave%'7 was 5
      IF color1% > 15 THEN color1% = 15
      POKE address%, color1%
      address% = address% + 1
    NEXT
  CASE 1
    address% = 1024& * row% + col%
    FOR i% = cols% \ 4 + 4 TO cols% \ 2 STEP 4
      color1% = dat%(i%) * 7 \ ave% '7 was 5
      IF color1% > 15 THEN color1% = 15
      POKE address%, color1%
      address% = address% + 1
    NEXT
  CASE 2
    address% = 1024& * row% + 512
    FOR i% = cols% \ 2 + 4 TO 3 * cols% \ 4 STEP 4
      color1% = dat2%(i%) * 7 \ ave%'7 was 5
      IF color1% > 15 THEN color1% = 15

```



```

        POKE address&, color1%
        address& = address& + 1
    NEXT
CASE 3
    address& = 1024& * row% + 768
    FOR i% = 3 * cols% \ 4 + 4 TO cols% STEP 4
        color1% = dat%(i%) * 7 \ ave% '7 was 5
        IF color1% > 15 THEN color1% = 15
        POKE address&, color1%
        address& = address& + 1
    NEXT
END SELECT
END SELECT
sum = sum + linesum&
lineave% = linesum& \ cols%
ave% = (sum / cols%) \ j% + 1
a$ = " "
SELECT CASE j% MOD 5
CASE 0
    inregs.dx = 12037 '12032=47*256+5
    a$ = LTRIM$(STR$(j%))
    GOSUB svgaprint
CASE 1
    inregs.dx = 12049
    GOSUB svgaprint
    a$ = LTRIM$(STR$(max%))
    GOSUB svgaprint
CASE 2
    inregs.dx = 12061
    GOSUB svgaprint
    a$ = LTRIM$(STR$(min%))
    GOSUB svgaprint
CASE 3
    inregs.dx = 12078
    GOSUB svgaprint
    a$ = LTRIM$(STR$(lineave%))
    GOSUB svgaprint
CASE 4
    inregs.dx = 12095
    GOSUB svgaprint
    a$ = LTRIM$(STR$(ave%))
    GOSUB svgaprint
END SELECT
PUT #2, , dataline$

DO
    UDStat% = cbGetStatus%(1, Status%, CurCount&, CurIndex&)
LOOP UNTIL Status% = IDLE

IF UDStat% <> 0 THEN
    PRINT
    PRINT "error"; UDStat%;
    DO: LOOP UNTIL INKEY$ = ""
    PRINT ". Press any key to continue.";
    CLOSE #2
    DO: LOOP WHILE INKEY$ = ""
    PRINT
    GOTO start
END IF

DO
    a% = cbDDBitIn(1, AUXPORT, 1, bitval%)
LOOP UNTIL bitval% = 0

IF j% \ 2 = j% / 2 THEN
    UDStat% = cbAInScan(1, dye%, dye%, TotalCount&, 10000&, Gain%, dat2%(1),
Options%)
ELSE

```

```

        UDStat% = cbAInScan(1, dye%, dye%, TotalCount%, 10000%, Gain%, dat%(1),
Options%)
    END IF

NEXT j%
skippedscan:
CLOSE #2
a% = cbStopBackground(1)
INPUT #8, echo$
IF ch% = 1 OR ABS((firstfocus - secondfocus) / focusfactor) < 101 THEN
    OPEN logfile$ FOR APPEND AS #3
    PRINT #3, "done with scan at "; TIMER'S
    PRINT #3, highclip% & "pixels clipped high,"; lowclip% & "pixels clipped low"
    CLOSE #3
ELSE GOSUB waitloop2
END IF
RETURN

setscanspeed:
scanspeed = .02075 * pixelsize / 3.4 * .984252
IF speed$ = "7.5" THEN scanspeed = scanspeed / 4
scanspeed2 = scanspeed * 5 'mm/sec
scanspeed$ = ". "
FOR i% = 1 TO 5
    IF scanspeed < 10 ^ (i% - 6) THEN EXIT FOR
    scanspeed = scanspeed * 10
    MID$(scanspeed$, i% + 1, 1) = LTRIM$(STR$(INT(scanspeed)))
    scanspeed = scanspeed - INT(scanspeed)
NEXT i%
scanspeed$ = RTRIM$(scanspeed$)
IF scanspeed2 < 1 THEN
    scanspeed2$ = ". "
    FOR i% = 1 TO 5
        IF scanspeed2 < 10 ^ (i% - 6) THEN EXIT FOR
        scanspeed2 = scanspeed2 * 10
        MID$(scanspeed2$, i% + 1, 1) = LTRIM$(STR$(INT(scanspeed2)))
        scanspeed2 = scanspeed2 - INT(scanspeed2)
    NEXT i%
    scanspeed2$ = RTRIM$(scanspeed2$)
ELSE
    scanspeed2$ = LEFT$(LTRIM$(STR$(scanspeed2)), 6)
END IF
RETURN

svgaprint:
'call interrupt 10H service 2 (set cursor position)
inregs.ax = 512
inregs.bx = 0
CALL interrupt(&H10, inregs, outregs)
'call interrupt 10H service E (teletype write to active page)
inregs.bx = 12
FOR k% = 1 TO LEN(a$)
    inregs.ax = 3584 + ASC(MID$(a$, k%, 1)) '3584=14*256
    CALL interrupt(&H10, inregs, outregs)
NEXT k%
RETURN

setfilters:
'set filters to 66 kHz (or 14 kHz) by writing to CIO-DIO24 digital I/O board
at port &h2e0
'66 / 102.4 * 256 - 1 = 164, 14 / 102.4 * 256 - 1 = 34
IF speed$ = "30 " THEN freq% = 164 ELSE freq% = 34
OUT &H2E0, freq%
time = TIMER
DO
    IF TIMER < time THEN time = time - 86400
LOOP UNTIL TIMER > time + .1
IF INP(&H2E0) <> freq% THEN
    SCREEN 0, 0, 0

```

```
PRINT "Problem with digital I/O board (CIO-DIO24)."  
SYSTEM  
END IF  
RETURN
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What is claimed is:

1. A system for detecting marked regions on a surface of a substrate, the system comprising:

- an excitation radiation source;
 - a focusing system for focusing radiation from said excitation radiation source onto a selected region of said surface of said substrate, said focusing system including an objective lens having a ratio of scanning field diameter to focused spot diameter of greater than about 2000, and a numerical aperture greater than about 0.2;
 - a radiation direction system for scanning said focused excitation radiation across said surface of said substrate at a rate of at least 5 image lines/second;
 - a detector for detecting an emission from said surface of said substrate in response to said excitation radiation, wherein said objective lens receives said emission and transmits the emission to the detector; and
 - a data acquisition system for recording an amount of said emission detected as a function of a position on said surface of said substrate from which said emission was emitted.
2. The system of claim 1, wherein said focusing system has a ratio of scanning field diameter to focused spot diameter of greater than 3000.
3. The system of claim 1, wherein said focusing system has a ratio of scanning field diameter to focused spot diameter of greater than 4000.
4. The system of claim 1, wherein said focusing system focuses said excitation radiation in a spot having a diameter of less than about 10 μm .
5. The system of claim 1, wherein said focusing system focuses said excitation radiation on said surface of said substrate in a spot having a diameter of less than about 5 μm .
6. The system of claim 1 wherein said focusing system focuses said excitation radiation on said surface of said substrate in a spot having a diameter of about 3 μm .
7. The system of claim 1, wherein said scanning field diameter is greater than about 10 mm.
8. The system of claim 1, wherein said scanning field diameter is about 14 mm.
9. The system of claim 1, wherein said numerical aperture is greater than about 0.25.
10. The system of claim 1, wherein said focusing system is achromatic.
11. The system of claim 1, wherein said radiation direction system is capable of scanning a spot across the substrate at a rate of at least 10 image lines/second.
12. The system of claim 1, wherein said radiation direction system is capable of scanning a spot across the substrate at a rate of at least 30 image lines/second.
13. The system of claim 1, wherein said radiation direction system comprises an angularly oscillating mirror or a rotating polyhedral mirror.
14. The system of claim 1, further comprising a translation stage upon which said substrate is mounted, said translation stage being moveable in at least one dimension perpendicular to an optical axis of said objective lens.
15. The system of claim 1, further comprising an auto-focus system for placing said surface of said substrate in a focal plane of said focusing system.
16. The system of claim 1, further comprising a translation stage upon which said substrate is mounted, said

translation stage being moveable in at least one dimension parallel to an optical axis of said focusing system and at least one dimension perpendicular to said optical axis of said focusing system.

17. The system of claim 1 further comprising a collection system comprising:

- collection optics for collecting fluorescence emitted from said surface of said substrate and for collecting an excitation radiation reflected from said surface of said substrate;
 - separation optics for separating said emitted fluorescence from an excitation radiation reflected from said surface of said substrate and focusing said fluorescence through a confocal pinhole; and
 - a recorder responsive to said fluorescence, for recording an amount of said fluorescence focused through said confocal pinhole.
18. The system of claim 1, wherein said surface of said substrate comprises a plurality of distinct polymer sequences in different known locations on said surface.
19. The system of claim 18, wherein each of said different polymer sequences is contained in a feature having at least one of a width or length dimension of less than about 50 μm .
20. The system of claim 1 further comprising a processor for processing and storing said signal so as to generate a 2-dimensional image of said sample.
21. The system of claim 1 further comprising a body for immobilizing said substrate, the substrate having at least a first surface with a sample thereon, the body comprising:

- a mounting surface;
 - a cavity in said mounting surface, said first surface mated to said mounting surface for sealing said cavity, said sample being in fluid communication with said cavity, said cavity having a bottom surface comprising a light absorptive material;
 - an inlet and an outlet being in communication with said cavity such that fluid flowing into said cavity for contacting said sample flows through said inlet and fluid flowing out of said cavity flows through said outlet; and
 - a temperature controller for controlling the temperature in said cavity.
22. The system of claim 21 wherein said temperature controller comprises a thermoelectric cooler.
23. A system for detecting marked regions on a surface of a substrate, the system comprising:
- an excitation radiation source;
 - first focusing optics for focusing said excitation radiation on said surface of said substrate in a spot having a diameter no greater than 5 μm , said focusing optics including an objective lens;
 - a reciprocating radiation direction system for scanning said spot linearly across said surface of said substrate, said spot having a travel distance of at least 10 mm;
 - an optical train for separating emissions from said surface of said substrate from excitation radiation reflected from said surface of said substrate, said optical train including said objective lens; and

an autofocus system for automatically placing said surface of said substrate in a focal plane of said first focusing optics.

24. The system of claim 23, wherein said optical train includes a dichroic beam splitter for separating fluorescence emitted from said surface of said substrate from excitation radiation reflected from said surface of said substrate.

25. The system of claim 23, wherein said autofocus system comprises:

second focusing optics for focusing said excitation radiation reflected from said surface of said substrate through a confocal pinhole onto a photodiode; and

a translation stage upon which a substrate is mounted, said stage being capable of moving in a direction parallel with an optical axis of said first focusing optics for moving said substrate into a focal plane of said first focusing optics.

26. The system of claim 23 further comprising a detector for detecting an emission from said surface of said substrate in response to said excitation radiation, and a data acquisition system for recording an amount of said emission detected as a function of a position on said surface of said substrate from which said emission was emitted.

27. A method of scanning a polymer array having a plurality of different polymer sequences, each of said different polymer sequences being immobilized on a surface of a substrate in a different known location, to identify which polymer sequence on said array is bound by a target molecule, the method comprising:

focusing an excitation radiation source upon said surface of said substrate with an objective lens;

scanning said excitation radiation across said surface of said substrate at a speed of at least about 5 image lines/second;

collecting emissions from said surface of said substrate in response to said excitation radiation with said objection lens;

recording said emissions as a function of a position on said surface of said substrate, said position indicating the polymer sequence on said array is bound by a target molecule.

28. The method of claim 27, wherein said polymer array comprises a plurality of different oligonucleotide sequences immobilized on said surface of said substrate in different known locations.

29. The method of claim 27 further comprising focusing the excitation radiation source to a spot having a diameter of about 3 μm and scanning the spot in linear direction across the substrate for at least 14 mm.

30. The method of claim 27 further comprising the steps of:

immobilizing said substrate on a body;

exciting said sample on said substrate with an excitation radiation having a first wavelength from an electromagnetic radiation source, said excitation radiation

detecting a response radiation having a second wavelength in response to said excitation radiation, said response radiation representing an image of said plurality of regions;

exciting a subsequent plurality of regions on said sample;

processing and storing said response radiation to generate a 2-dimensional image of said sample; and

auto-focusing said sample in a focal plane of said excitation radiation.

31. The method as recited in claim 30 wherein said body comprises a mounting surface having a cavity thereon, said substrate being immobilized on said mounting surface such that said sample is in fluid communication with said reaction chamber, said reaction chamber comprising an inlet and an outlet for flowing fluids into and through said reaction chamber.

32. The method as recited in claim 31 wherein said body further comprises a temperature controller for controlling the temperature in said cavity.

33. The method as recited in claim 27 wherein said excitation radiation is scanned across said surface of said substrate at a speed of at least about 10 image lines/second.

34. The method as recited in claim 27 wherein said excitation radiation is scanned across said surface of said substrate at a speed of at least about 30 image lines/second.

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