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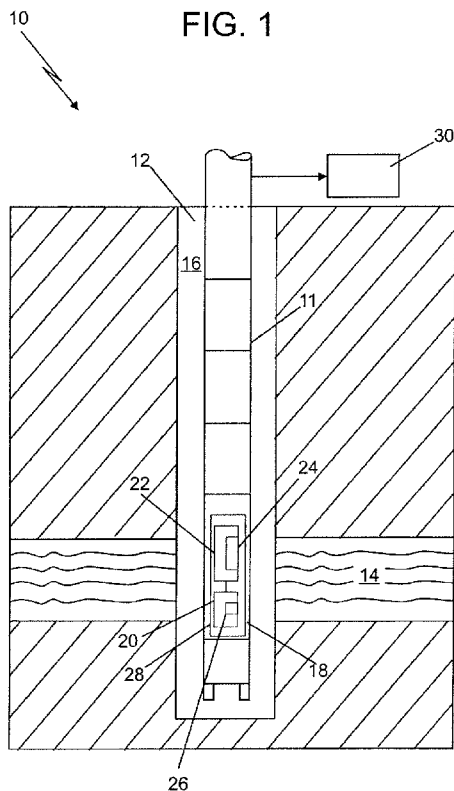
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(54) Title: APPARATUS AND SYSTEM FOR GEOSTEERING AND FORMATION EVALUATION UTILIZING IMPROVED ANTENNAS



(57) Abstract: An apparatus for measuring one or more earth formation properties during applications including formation evaluation and geosteering applications is provided. The apparatus includes: an elongated body; at least one recessed portion on a periphery of the elongated body; an electrically conductive coil forming a closed loop, at least a portion of the coil extending through the at least one recessed portion; and a u-shaped magnetically permeable and non-conductive material disposed between the coil and the at least one recessed portion, the u-shaped material partially surrounding the coil in the at least one recessed portion. A system for measuring one or more properties of an earth formation is also provided.

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**APPARATUS AND SYSTEM FOR GEOSTEERING AND FORMATION  
EVALUATION UTILIZING IMPROVED ANTENNAS**

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**BACKGROUND**

[0001] Various formation evaluation (FE) tools are used in hydrocarbon exploration and production to measure properties of geologic formations during or shortly after the excavation of a borehole. The properties are measured by formation evaluation tools and other suitable devices, which are typically integrated into a bottom hole assembly (BHA).  
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[0002] Some FE tools include antennas that are used during FE operations, such as logging-while-drilling (LWD) and geosteering operations. Examples of such antennas include so-called "slot" design antennas, such as "Z-type" antennas ("Z-antennas") typically used in multi-frequency and multi-spacing propagation resistivity ("MPR") tools and "X-type" antennas ("X-antennas") typically used in azimuth propagation resistivity ("APR") tools.  
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[0003] Current LWD antennas require a minimum slot length in order to generate a sufficiently strong signal, and thus impact space requirements and sizes of associated downhole tools. Furthermore, the lengths of such antennas make it infeasible to incorporate differing types of tools, such as MPR and APR tools, together to improve LWD operations such as geosteering operations.  
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**SUMMARY**

[0004] Disclosed herein is an apparatus for measuring one or more earth formation properties during applications including formation evaluation and geosteering applications. The apparatus includes: an elongated body; at least one recessed portion on a periphery of the elongated body; an electrically conductive coil forming a closed loop, at least a portion of the coil extending through the at least one recessed portion; and a u-shaped magnetically permeable and non-conductive material disposed between the coil and the at least one recessed portion, the u-shaped material partially surrounding the coil in the at least one recessed portion.  
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[0005] Also disclosed herein is a system for measuring one or more properties of an earth formation. The system includes: a drillstring configured to support a drilling device; and a measurement tool disposed on the drillstring and including at least one antenna. The antenna includes: an elongated body; at least one recessed portion on a periphery of the elongated body; an electrically conductive coil forming a closed loop, at least a portion of the coil extending through the at least one recessed portion; and a u-shaped magnetically permeable and non-conductive material disposed between the coil and the at least one recessed portion, the u-shaped material partially surrounding the coil in the at least one recessed portion.

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### **BRIEF DESCRIPTION OF THE DRAWINGS**

[0006] The following descriptions should not be considered limiting in any way. With reference to the accompanying drawings, like elements are numbered alike:

**FIG. 1** depicts an exemplary embodiment of a logging system;

**FIG. 2** depicts an exemplary embodiment of a measurement tool of **FIG. 1**;

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**FIG. 3** depicts a side view of an exemplary embodiment of an antenna;

**FIG. 4** depicts a top view of another exemplary embodiment of an antenna;

**FIGS. 5a** and **5b** depict additional exemplary embodiments of an antenna;

**FIG. 6** depicts comparative signal strength measurements for a prior art antenna and the antennas of **FIGS. 5a** and **5b**;

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**FIGS. 7a** and **7b** depict further exemplary embodiments of an antenna;

**FIG. 8** depicts comparative signal strength measurements for a prior art antenna and the antennas of **FIGS. 7a** and **7b**;

**FIGS. 9a** and **9b** depict exemplary embodiments of an assembly including multiple co-located antennas;

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**FIGS. 10a** and **10b** depict additional exemplary embodiments of an assembly including multiple co-located antennas;

**FIG. 11** depicts comparative signal strength measurements showing effects of slot lengths on signal strength;

**FIG. 12** depicts comparative signal strength measurements showing effects of increases in effective cross area on signal strength;

5 **FIG. 13** depicts comparative signal strength measurements showing effects of magnetic permeability of filled material on signal strength;

**FIG. 14** depicts comparative signal strength measurements showing effects of shape and position of filled material on signal strength;

**FIG. 15** depicts a diagram of an antenna tuning circuit;

10 **FIG. 16** depicts comparative signal strength measurements showing effects of the number of turns of the coil on signal strength;

### **DETAILED DESCRIPTION**

[0007] A detailed description of one or more embodiments of the disclosed system and method are presented herein by way of exemplification and not limitation with  
15 reference to the Figures.

[0008] Referring to **FIG. 1**, an exemplary embodiment of a well logging system **10** includes a drillstring **11** that is shown disposed in a borehole **12** that penetrates at least one earth formation **14** for making measurements of properties of the formation **14** and/or the borehole **12** downhole. Drilling fluid, or drilling mud **16** may be pumped  
20 through the borehole **12**. As described herein, “formations” refer to the various features and materials that may be encountered in a subsurface environment. Accordingly, it should be considered that while the term “formation” generally refers to geologic formations of interest, that the term “formations,” as used herein, may, in some instances, include any geologic points or volumes of interest (such as a survey  
25 area).

[0009] As described herein, “logging” refers to the taking of formation property measurements. Examples of logging processes include measurement-while-drilling (MWD) and logging-while-drilling (LWD) processes, during which measurements of

properties of the formations and/or the borehole are taken downhole during or shortly after drilling. The data retrieved during these processes may be transmitted to the surface, and may also be stored with the downhole tool for later retrieval. Other examples include logging measurements after drilling, wireline logging, and drop shot logging. As referred to herein, “downhole” or “down a borehole” refers to a location in a borehole away from a surface location at which the borehole begins.

[0010] A formation evaluation (FE) downhole measurement tool **18** may be disposed in the well logging system **10** at or near the downhole portion of the drillstring **11**, and includes one or more of various types of sensors or receivers **20** to measure various properties of the formation **14** as the tool **18** is lowered down the borehole **12**. Such sensors **20** include, for example, nuclear magnetic resonance (NMR) sensors, resistivity sensors, porosity sensors, gamma ray sensors, seismic receivers and others.

[0011] In one embodiment, the tool **18** may be inserted in the drillstring **11**, and allowed to fall by gravity to a downhole position, or be pumped to the downhole position via the mud **16**. In other embodiments, the tool **18** may be lowered by a wireline, inserted during a MWD or LWD process, or inserted downhole by any other suitable processes. In one embodiment, the tool **18** includes a communications assembly **22** for transmitting data and communication signals between the tool **18** and a remote processor. The communications assembly **22** may be part of any selected telemetry system, such as a wireline or wired pipe communication system or a wireless communication system including mud pulse telemetry and/or RF communication. In one embodiment, the communications assembly **22** includes at least one communication antenna **24** connected to the sensor **20**.

[0012] In one embodiment, the tool **18** includes an electronics unit **26** for receiving data from and/or control of the tool **18**. The electronics unit **26** may also control the communications assembly **22** for communicating with a remote processor. The sensor **20**, the communications assembly **22** and/or the electronics unit **26** may be included in a common housing **28**. With respect to the teachings herein, the housing **28** may represent any structure used to support at least one of the sensor **20**, the communications assembly **22**, and the electronics unit **26**.

[0013] The tool **18** may be operably connected to a surface processing unit **30**, which may act to control the sensor **20**, and may also collect and process data generated by the sensor **20** during a logging process. In one embodiment, the surface processing unit **30**, includes any number of transmitting and/or receiving antennas (not shown) to receive signals from, and/or send signals to, the communications assembly **22**.

[0014] The surface processing unit **30** may also include components as necessary to provide for processing of data from the tool **18**. Exemplary components include, without limitation, at least one processor, storage, memory, input devices, output devices and the like. As these components are known to those skilled in the art, these are not depicted in any detail herein.

[0015] Although the present embodiment provides the surface processing unit **30** to receive and process the frequency data, any number or types of processors, circuits or devices for controlling operation of the tool **18**, processing data and/or communicating with the communications assembly **22** may be provided downhole. Such devices may include any suitable components, such as storage, memory, input devices, output devices and others.

[0016] Referring to **FIG. 2**, there is provided an exemplary embodiment of the measurement tool **18**. The measurement tool **18** includes transmitting antennas **32** and receiving antennas **34**. In one embodiment, the transmitting antennas **32** are used to inject electromagnetic signals into the borehole and the surrounding formation **14**, and the receiving antennas **34** are used to receive the signals that return from the formation **14**. These signals may be utilized to determine, for example, the amplitude attenuation or phase shift of the interrogating electromagnetic wave. Each antenna **32, 34** includes a respective electronics unit **36** to perform functions such as tuning. The antennas **32, 34** may be configured to operate at any desired frequency, such as 400 kHz and 2 MHz. The number and type of antennas shown in **FIG. 2** is merely exemplary. Any suitable number and combination of antennas, including for example, transmitting antennas, receiving antennas, Z-antennas and X-antennas, may be incorporated in the tool **18**.

[0017] Referring to **FIG. 3**, an exemplary embodiment of an antenna **40** is shown. In this embodiment, the antenna **40** is a Z-antenna. The antenna **40** includes an

elongated body **42** that includes one or more recesses or slots **44** disposed on a periphery of the elongated body **42**. In these embodiments, each slot **44** extends along axial and circumferential directions relative to the elongated body **42**. One or more coils **46** extends in a circumferential direction through each slot **44**, and each slot has a “u-shaped” magnetically permeable material **48**, such as a ferrite material, disposed between the coil **46** and an inner surface of the slot **44**. In one embodiment, a protective cover **49**, made of non-electrically conductive material, is disposed over the slot **44** to protect the slots **44** from fluid and to prevent fatigue. In one example, the non-conductive cover **49** is at least 1/8 inch thick. The cover **49** can be optionally designed as a separate piece for an easier replacement if it is worn away during the drilling process.

[0018] As used herein, the “axial” direction refers to a direction generally parallel to the longest axis of the elongated body. For Z-antennas, the axial direction is perpendicular to a plane formed by the coil, and for X-antennas, the axial direction is parallel to the plane formed by the coil. For Z-antennas, the axial direction is parallel to the direction of the magnetic flux relative to a point on the periphery of the elongated body, and for X-antennas, the axial direction is perpendicular to the direction of the magnetic flux. The “radial” direction refers to a direction perpendicular to the axial direction and extending from the periphery to the center of the elongated body. The “azimuthal” direction refers to a direction corresponding to a straight line that is perpendicular to the axial direction and perpendicular to the radial direction. It should be noted that, although embodiments presented herein describe a cylindrical elongated body, any elongated body having any suitable shape may be utilized. In other embodiments, the plane formed by the coil in the Z-antenna is at any selected angle relative to the longest axis of the elongated body.

[0019] The number of slots **44** is not limited, and may be as few as a single circumferential slot **44** or a plurality of slots **44**. In one embodiment, the slot **44** is a single slot extending in a circumferential direction completely around the periphery, as shown in FIG. 4. As shown in FIG. 3, the coil **46** includes two turns around the circumference of the elongated body **42**, but may constitute a single turn or any desired number of turns. As used herein, “u-shaped” refers to a configuration that partially surrounds the coil **46**, and has a first portion disposed on an interior surface

of the slot, and two side portions on opposite ends of the first portion that extend in a radial direction toward the periphery of the elongated body **42**. The signal strength increases when the u-shaped magnetic material **48** is filled into the slots **44** to guide the magnetic flux to flow either inward or outward.

5 **[0020]** In one embodiment, each slot **44** is a slim-cut or slim slot **44**. As used herein, “slim” refers to a length of the slot **44** in the axial direction that is less than the axial length of prior art slots, which typically is about five inches. The slim slots **44** are less than five inches. In one embodiment, the axial length of each slot **44** is less than or equal to about one inch, for example, 0.4 inch or 0.6 inch as shown in **FIG. 3**. In  
10 one embodiment, the axial length is from 0.4 inch to one inch, which provides a sufficiently strong signal while the relatively short length of the resulting antenna **40** lends mechanical strength. In another embodiment, the u-shaped permeable material **48** extends in a radial direction so that the distance between the outermost surface of the u-shaped material **48** and the periphery of the elongated body **42** is about 1/8 inch  
15 or 0.125 inch.

**[0021]** Referring to **FIGS. 5a** and **5b**, additional embodiments of a Z-antenna **50** are shown. Antenna **50** includes an elongated body **52** having a plurality of slots **54**. In one embodiment, the slots **54** are slim length slots. One or more coils **56** extend in a circumferential direction through each slot **54**, and each slot **54** has a u-shaped  
20 magnetically permeable material **58**, such as a ferrite material, disposed between the coil **56** and an inner surface of the slot **54**. In one embodiment, a protective cover **59**, made of non-conductive materials, is disposed over the slot **54**.

**[0022]** As shown in **FIGS. 5a** and **5b**, the coil **56** includes two turns around the circumference of the elongated body **52**, but may constitute a single turn or any  
25 desired number of turns. In one embodiment, the antenna **50** has four slots **54**, although any suitable number of slots **54** may be utilized, such as two slots **54** or a single circumferential slot **54**. In the embodiment shown in **FIG. 5a**, the axial length of the slot **54** is approximately two inches, and the azimuthal length of the slot **54** is approximately 0.5 inch. In the embodiment shown in **FIG. 5b**, the axial length of the  
30 slot **54** is approximately three inches, and the azimuthal length of the slot **54** is approximately 0.2 inch. As shown in these embodiments, the axial length of the slots is reduced, and the total width of the slot is varied based on the axial length to

preserve signal strength. In one embodiment, the depth of each slot in the radial direction is about 0.425 inch.

[0023] FIG. 6 shows a comparison of the signal strength for the embodiments of FIG. 5a and 5b verses a prior art Z-antenna having sixteen slots, each of which is 5 0.125 inch in width (in the azimuth direction), five inches in length (in the axial direction of the antenna pipe), and 0.5512 inches in depth (along a radial direction of the pipe). The prior art Z-antenna is labeled “existing” in FIG. 6. As is evident from FIG. 6, the u-shaped configuration described herein provides comparable signal strength even with reduced numbers and axial lengths of the slots.

10 [0024] Referring to FIGS. 7a and 7b, an exemplary embodiment of an antenna 60 is shown. In this embodiment, the antenna 60 is in an X-antenna configuration. The antenna 60 includes an elongated body 62 that includes one or more recesses or slots 64 disposed on a periphery of the elongated body. In these embodiments, each slot 64 extends along axial and azimuthal directions relative to the elongated body 62. One 15 or more coils 66 forms a closed path defining a plane parallel to the axis of the elongated body 62 and extends through each slot 64, and each slot has a u-shaped permeable material 68 disposed between the coil 66 and an inner surface of the slot 64. The number of slots 64 is not limited, and may be any desired number. In the embodiments shown in FIG. 7a and 7b, the antenna includes two slots 64, but may 20 include any number of slots 64. As shown in FIGS. 7a and 7b, the coil 66 includes two turns around the closed path, but may constitute a single turn or any desired number of turns. The antenna 60, in one embodiment, includes an optional protective non-conductive cover 69.

[0025] In one embodiment, each slot 64 has an axial length of approximately five 25 inches or less, and has an azimuth length of one inch or less. For example, FIG. 7a illustrates an embodiment with each slot 64 having a five inch axial length and a 0.8 inch azimuth length, and FIG. 7b illustrates an embodiment with each slot 64 having a 3.5 inch axial length and a one inch azimuth length. Other embodiments include slots 64 having an azimuth length of one inch or less, such as 0.6 inch.

30 [0026] Referring to FIG. 8, exemplary dimensions are described and evaluated as compared to a prior art Z-antenna, which is labeled “existing”, and such evaluation is

used to determine preferred axial lengths of the X-antenna slots 64 based on various azimuthal lengths. The graph shown in **FIG. 8** illustrates calculations of signal strength versus slot spacing, for the prior art Z-antenna, and embodiments of the Z-antenna described herein having axial slot lengths of 0.6 inch, 0.8 inch and one inch, respectively. Signal strengths are measured for 400 kHz and 2 MHz frequencies. To estimate the axial length of a slot 64 for an X-antenna, the relationship between the prior art Z-antenna and signal measurements from embodiments of the Z-antennas 40 and/or 50 of different axial lengths is used.

[0027] In this example, the radius of the elongated body (a tool pipe in this example) is 3.375 inch. Since three turns are generally used in prior art X-antennas, a factor of three should be considered. In one embodiment, in order to minimize the length, a factor of 4 can be achieved by a pre-amplifier. In the 0.6 inch measurement, the total length of the slot for the Z-antenna is the perimeter of the antenna, which is  $2*\pi*(3.375 \text{ inches}) = 21.2 \text{ inches}$ . For a X-antenna, two oppositely located slots are cut into the elongated body. Thus, for the 0.6 inch azimuthal cut X-antenna, the axial length will be  $[(21.2 \text{ inches})/2]*3/4 = 8 \text{ inches}$ . For a 0.8 inch azimuthal cut X-antenna, the signal is about 2.5 times of the prior art signal. Thus, the length can be calculated as  $[(21.2 \text{ inches})/2]/\text{sqrt}(2.5)*3/4 = 5 \text{ inches}$ . The same operation can be applied to a one-inch azimuthal cut X-antenna, for which the signal is about 5 times that of the reference signal. The length thus will be  $[(21.2 \text{ inches})/2]/\text{sqrt}(5)*3/4 = 3.5 \text{ inches}$ . In this example, the square root (sqrt) is used because of the use of both transmitter and receiver antennas in the simulations.

[0028] Referring to **FIGS. 9** and **10**, embodiments of an antenna are shown that extend the single antenna designs to a two- or three-component collocated antenna. During a LWD process, the tool 18 is continually rotating. Thus, a two-component collocated antenna as shown in **FIG. 9** is possible for obtaining all components out of full tensor measurements except the XY component. **Figure 10** shows two design options for a three-component collocated antenna when the XY component is needed. Although these embodiments are described as having specific numbers of slots and coils, and specific dimensions, such numbers and dimensions are merely exemplary and may be adjusted as desired.

[0029] Referring to **FIGS. 9a** and **9b**, an antenna assembly **70** is shown that includes an elongated body **72** having a pair of slots **74** disposed on a periphery of the elongated body **72**. In these embodiments, each slot **74** extends along axial and azimuthal directions relative to the elongated body **72**. One or more coils **76** forms a closed path defining a plane parallel to the axis of the elongated body **72** and extends through each slot **74**, and each slot has a u-shaped permeable material **78** disposed between the coil **76** and an inner surface of the slot **74**. The antenna assembly **70** also includes additional coils **75** that extend around the periphery of the elongated body **72** in a circumferential direction. In the embodiment shown in **FIG. 9a**, each slot has an axial length of about five inches and an azimuth length of about 0.8 inch. In the embodiment shown in **FIG. 9b**, each slot **74** has an axial length of about 3.5 inches and an azimuth length of about one inch.

[0030] Referring to **FIG. 10a** and **10b**, in this embodiment the antenna assembly **70** includes an additional pair of slots **73**, each including additional u-shaped permeable material **77**, and additional coils **79**, which also form a loop in a plane parallel to the axis of the elongated body **72**. In the embodiment shown in **FIG. 10a**, each slot **73**, **74** has an axial length of about five inches and an azimuth length of about 0.8 inch. In the embodiment shown in **FIG. 10b**, each slot **73**, **74** has an axial length of about 3.5 inches and an azimuth length of about one inch.

[0031] In the above examples shown in **FIGS. 9** and **10**, the slots **74** are configured according to an X-antenna configuration. In other embodiments, the slots **74** are configured in a Z-antenna configuration.

[0032] In order to evaluate the efficiency of different antenna designs, the signal strength from one transmitter to two receivers for a prior art Z-antenna is measured for comparison with antennas having various modifications. The impact on signal strength of various characteristics of different embodiments of the antennas described herein is shown, compared to a prior art Z-antenna. Such characteristics include the reduced length of an antenna, the effective cross area, the magnetic permeability of filled material, the shape of the material, the depth of cutting, and the number of turns of coil. These impacts are shown to demonstrate how various characteristics can be modified to compensate for the reduced length of the antennas described herein relative to prior art antennas.

[0033] Referring to **FIGS. 11-16**, the prior art Z-antenna described includes slots having an azimuthal length of 0.125 inch in width, an axial length of five inches, and a radial depth of 0.5512 inch. The prior art Z-antenna is labeled “existing” in the graphs of **FIGS. 11-16**.

5 [0034] Referring to **FIG. 11**, the effects of shortening slot lengths for an antenna is shown. **FIG. 11** shows signal strength relative to slot spacing for the prior art antenna having five inch axial slots, an antenna having three-inch slots, and an antenna having two-inch slots. As demonstrated in **FIG. 11**, absence of other factors, a reduction in the slot’s axial length corresponds to a reduction in signal strength. Furthermore, the  
10 signal strength is not linearly proportional to the permeability when the length of path along the magnetic flux direction is not long enough. The effective permeability becomes smaller when the path is cut shorter.

[0035] Various characteristics of the antenna described herein counteract the relationship between slot length and signal strength to provide for a signal strength  
15 that is comparable to or greater than prior art antenna signal strengths. Various combinations of the characteristics described below may be used to increase signal strength.

[0036] Referring to **FIG. 12**, the effects of an increase in the effective cross area is shown. The cross area is the non-metallic area in the plane defined by the coil,  
20 defined by the slots, that is perpendicular to the magnetic flux. The effective cross area provides an open path for the magnetic flux to flow. The larger the effective cross area, the stronger the signal will be. **FIG. 12** shows the variation of signal strength with the number of slots used in receiver antennas while keeping the cross area of each slot unchanged. As is evident from **FIG. 12**, the signal strength is  
25 linearly proportional to the effective cross area.

[0037] Referring to **FIG. 13**, the effects of the magnetic permeability of filled material are shown. Usually, high magnetically permeable materials are used to attract the magnetic flux so that the efficiency of the antenna is improved. **FIG. 13** shows the variation of the signal strength with the relative permeability of filled  
30 material, i.e., the ratio of the permeability of the filled material to the permeability of free space, for the circumferential antennas of two different cut lengths (0.4 inch and

one inch). As shown in **FIG. 13**, the signal strength increases with the increase in magnetic permeability and saturates after a certain value. For a ferrite material with a relative-magnetic-permeability ( $\mu_r$ ) of 125, the signal is saturated. In other words, there is no need to use a higher magnetic permeability material. **FIG. 13** demonstrates a saturation of the signal when  $\mu_r$  is greater than or equal to approximately 100.

**[0038]** Referring to **FIG. 14**, the effects of the shape and position of the filled magnetically permeable material is shown. **FIG. 14** shows the signal strength for the prior art “existing” antenna, as well as for antennas having a u-shaped magnetically permeable material. **FIG. 14** shows signal strengths for design options including a slot having a radial depth similar to prior art slots (labeled “Deeper cut”), a slot having a shallow cut so that the u-shaped magnetically permeable material is close to the periphery, such as 1/8 inch (labeled “0.6 inch cut (Strip)”), and a slot having the shallow cut, u-shaped material and two coil turns (labeled “0.6 inch cut (2 turn)”). As shown herein, to counteract the reduction in signal strength, the u-shaped material and multiple turns increases the signal strength. The use of u-shape magnetically permeable material makes it feasible to design a slim cut (in the magnetic flux direction) antenna. The signal strength becomes stronger when the filled magnetic material and the coil(s) are closer to the collar surface.

**[0039]** Referring to **FIGS. 14** and **15**, the effects of the number of turns on the antenna is shown. In general, for a fixed voltage input, increasing the number of turns without any special treatment would not increase the magnetic moment and associated magnetic field, since the impedance is proportionally increased. Accordingly, in one embodiment, a tuning circuit **80** is coupled to the coil to allow the voltage in the coil to increase when multiple turns are utilized. The tuning circuit can thus be used to tune the antenna to yield a maximum current in the antenna loop.

**[0040]** The tuning circuit **80** includes a transformer **82** used to match the impedance of the tuning circuit **80** to the coil to reduce voltage reflection for high frequency measurements. When a resonance condition is reached between the tuning circuit **80** and the coil, the pure resistance comes from both coil resistance and tuning circuit residual resistance including the transformer **82**. However, the larger part of the resistance is from the tuning circuit **80**. Accordingly, the resonance current in the

antenna loop is almost unchanged in response to the number of turns, allowing the tuning circuit to provide an increased current. In the example shown in **FIG. 14**, resistance **84** is the total pure resistance “R” whereas the resistance for the antenna loop is about 0.05 Ohm. Exemplary components of the tuning circuit **80** include the coil loop inductance **86**, as well as an additional inductor **88** and capacitors **90**. The values described in this example are not limiting.

**[0041]** Referring to **FIG. 16**, the signal strength versus the number of turns is shown. As is evident from **FIG. 16**, adding turns to an antenna significantly increases the signal strength. In this example, the signal strength for a two-turn antenna (labeled “0.6 inch cut (2 turn)”) is almost four times that of a single turn antenna (“0.6 inch cut (1 turn)”).

**[0042]** The systems and methods described herein provide various advantages over existing processing methods and devices. The antennas described herein exhibit a reduction in size and manufacturing cost, and thereby save space for easier arrangement of multiple antennas, while keeping a similar or better antenna performance comparing to prior art antennas, such as the existing "slots" design as in MPR (Z-antenna) and APR (X-antenna) type tools. Shortening an antenna can also provide more flexibility in combining different antennas.

**[0043]** Another benefit of shortening the antennas is the possible reduction of the manufacturing costs. For example, a single circumferential cut, or a reduced number of slots can be manufactured more quickly and easily than prior art antennas that typically include sixteen slots.

**[0044]** For X-antenna configurations, for example, the antenna described herein can be designed to be significantly shorter than prior art X-antennas. Prior art antennas typically include sixteen slots of 0.125” width deployed along the pipe on opposite sides, and are generally about one foot long. Embodiments of the X-antennas described herein are significantly shorter, as they include fewer slots and shorter axial lengths. Furthermore, use of the antennas described herein, particularly the X-antennas described herein, makes it possible to design a collocated multi-component antenna. Any workable X-antenna can be modified according to the embodiments described herein to add a Z-component by circumferentially wiring additional coil(s).

[0045] In support of the teachings herein, various analyses and/or analytical components may be used, including digital and/or analog systems. The system may have components such as a processor, storage media, memory, input, output, communications link (wired, wireless, pulsed mud, optical or other), user interfaces, software programs, signal processors (digital or analog) and other such components (such as resistors, capacitors, inductors and others) to provide for operation and analyses of the apparatus and methods disclosed herein in any of several manners well-appreciated in the art. It is considered that these teachings may be, but need not be, implemented in conjunction with a set of computer executable instructions stored on a computer readable medium, including memory (ROMs, RAMs), optical (CD-ROMs), or magnetic (disks, hard drives), or any other type that when executed causes a computer to implement the method of the present invention. These instructions may provide for equipment operation, control, data collection and analysis and other functions deemed relevant by a system designer, owner, user or other such personnel, in addition to the functions described in this disclosure.

[0046] Further, various other components may be included and called upon for providing aspects of the teachings herein. For example, a sample line, sample storage, sample chamber, sample exhaust, pump, piston, power supply (e.g., at least one of a generator, a remote supply and a battery), vacuum supply, pressure supply, refrigeration (i.e., cooling) unit or supply, heating component, motive force (such as a translational force, propulsional force or a rotational force), magnet, electromagnet, sensor, electrode, transmitter, receiver, transceiver, controller, optical unit, electrical unit or electromechanical unit may be included in support of the various aspects discussed herein or in support of other functions beyond this disclosure.

[0047] One skilled in the art will recognize that the various components or technologies may provide certain necessary or beneficial functionality or features. Accordingly, these functions and features as may be needed in support of the appended claims and variations thereof, are recognized as being inherently included as a part of the teachings herein and a part of the invention disclosed.

[0048] While the invention has been described with reference to exemplary embodiments, it will be understood by those skilled in the art that various changes may be made and equivalents may be substituted for elements thereof without

departing from the scope of the invention. In addition, many modifications will be appreciated by those skilled in the art to adapt a particular instrument, situation or material to the teachings of the invention without departing from the essential scope thereof. Therefore, it is intended that the invention not be limited to the particular  
5 embodiment disclosed as the best mode contemplated for carrying out this invention, but that the invention will include all embodiments falling within the scope of the appended claims.

CLAIMS

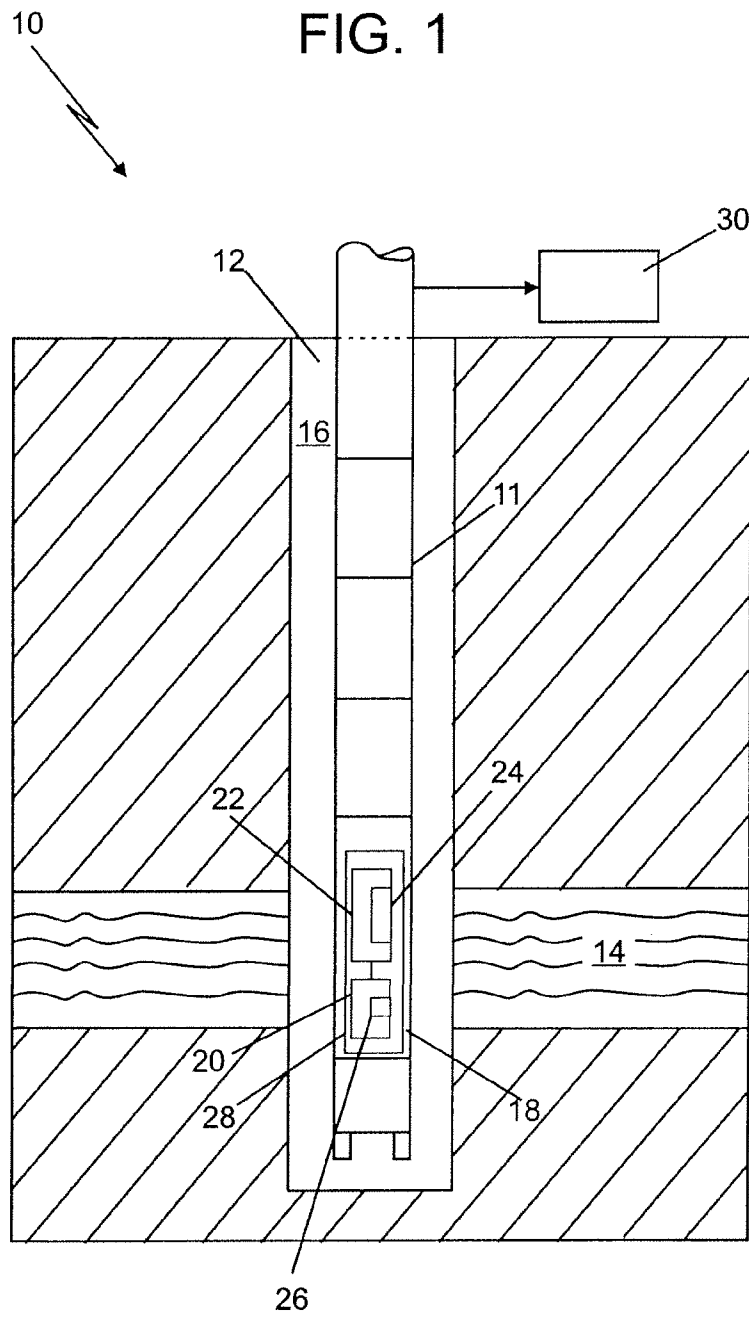
What is claimed is:

- 1 1. An apparatus for measuring one or more earth formation properties during  
2 applications including formation evaluation and geosteering, the apparatus  
3 comprising:
  - 4 (a) an elongated body;
  - 5 (b) at least one recessed portion on a periphery of the elongated body;
  - 6 (c) an electrically conductive coil forming a closed loop, at least a portion  
7 of the coil extending through the at least one recessed portion; and
  - 8 (d) a u-shaped magnetically permeable and non-conductive material  
9 disposed between the coil and the at least one recessed portion, the u-  
10 shaped material partially surrounding the coil in the at least one  
11 recessed portion.
- 1 2. The apparatus of claim 1, wherein the recessed portion has a length in a  
2 direction parallel to a magnetic flux direction of less than five inches.
- 1 3. The apparatus of claim 2, wherein the recessed portion has a length in the  
2 direction parallel to the magnetic flux direction of less than or equal to  
3 approximately one inch.
- 1 4. The apparatus of claim 1, wherein the coil includes a plurality of turns.
- 1 5. The apparatus of claim 1, wherein the magnetically permeable material has a  
2 relative permeability of at least 100.
- 1 6. The apparatus of claim 1, wherein the coil forms a plane at a selected angle  
2 relative to a longest axis of the elongated body, and the at least one recessed  
3 portion is at least one slot extending in a circumferential direction relative to a  
4 periphery of the elongated body.
- 1 7. The apparatus of claim 6, wherein the plane is perpendicular to the longest  
2 axis.
- 1 8. The apparatus of claim 6, wherein the recessed portion is a single slot  
2 extending around the entirety of the periphery.

- 1 9. The apparatus of claim 1, wherein the coil forms a plane parallel to a longest  
2 axis of the elongated body, the at least one recessed portion is at least one slot  
3 extending along an azimuthal direction, the azimuthal direction corresponding  
4 to a straight line perpendicular to the longest axis and perpendicular to a radial  
5 direction of the elongated body.
- 1 10. The apparatus of claim 9, wherein the at least one recessed portion is one or  
2 more pairs of recessed portions, each pair located on an opposite side of the  
3 elongated body relative to the longest axis.
- 1 11. The apparatus of claim 10, further comprising an additional coil that forms a  
2 plane perpendicular to the longest axis of the elongated body.
- 1 12. The apparatus of claim 1, wherein the magnetically permeable material is a  
2 ferrite material.
- 1 13. The apparatus of claim 1, further comprising a non-conductive cover disposed  
2 on an exterior of the elongated body and surrounding the at least one recess.
- 1 14. A system for measuring one or more properties of an earth formation, the  
2 system comprising;  
3 (a) a drillstring configured to support a drilling device; and  
4 (b) a measurement tool disposed on the drillstring and including at least  
5 one antenna, the antenna including:  
6 (c) an elongated body;  
7 (d) at least one recessed portion on a periphery of the elongated body;  
8 (e) an electrically conductive coil forming a closed loop, at least a portion  
9 of the coil extending through the at least one recessed portion; and  
10 (f) a u-shaped magnetically permeable and non-conductive material  
11 disposed between the coil and the at least one recessed portion, the u-  
12 shaped material partially surrounding the coil in the at least one  
13 recessed portion.
- 1 15. The system of claim 14, wherein the recessed portion has a length in a  
2 direction parallel to a magnetic flux direction of less than five inches.

- 1 16. The system of claim 14, wherein the coil includes a plurality of turns.
- 1 17. The system of claim 14, wherein the magnetically permeable material has a  
2 relative permeability of at least 100.
- 1 18. The system of claim 14, wherein the antenna is selected from at least one of a  
2 Z-type antenna and an X-type antenna.
- 1 19. The system of claim 14, wherein the at least one antenna is selected from at  
2 least one of: a transmitter for injecting an electromagnetic signal into the earth  
3 formation, and a receiver for receiving a signal return from the earth  
4 formation.
- 1 20. The system of claim 14, wherein the system is a logging-while-drilling  
2 measurement system.

FIG. 1



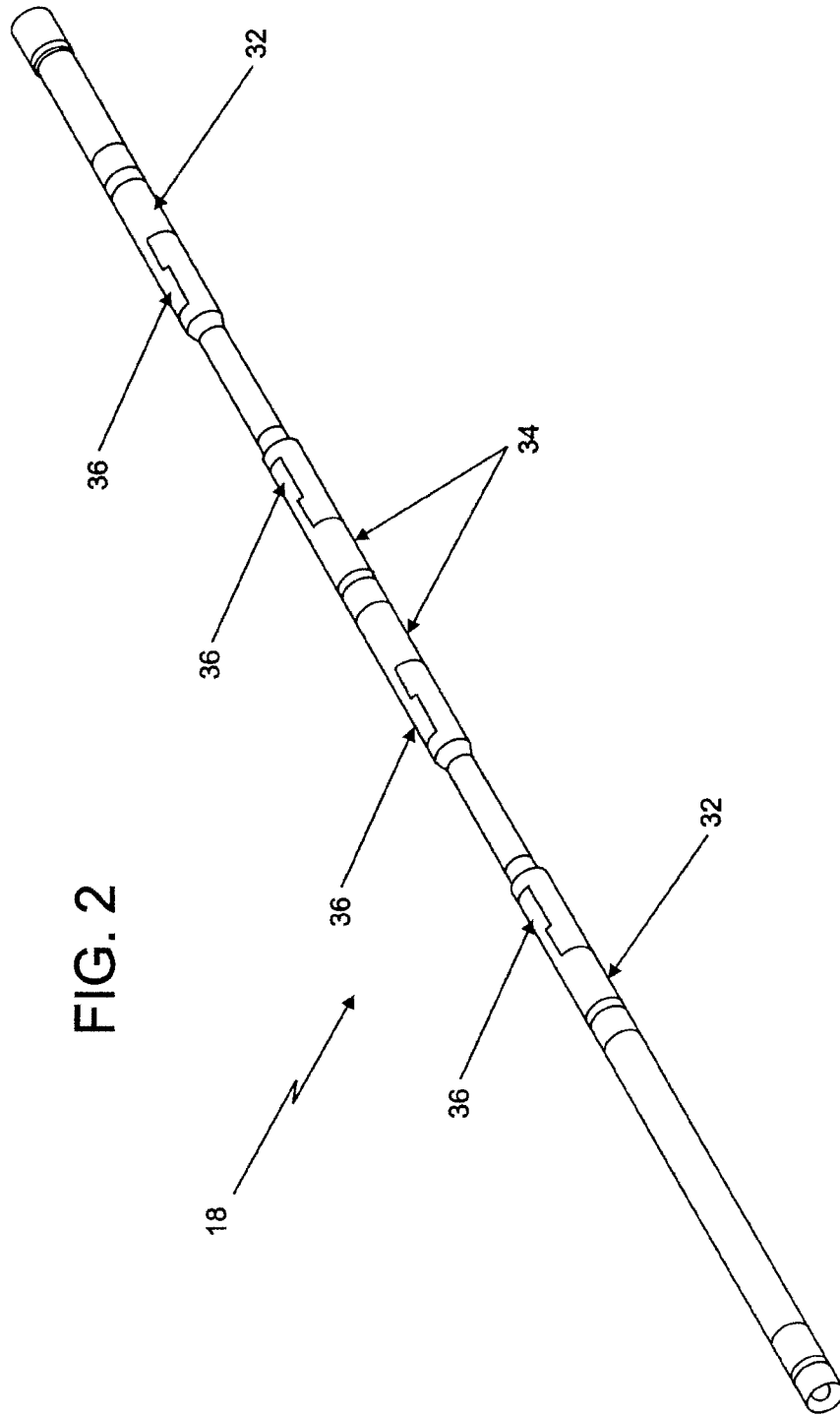


FIG. 3

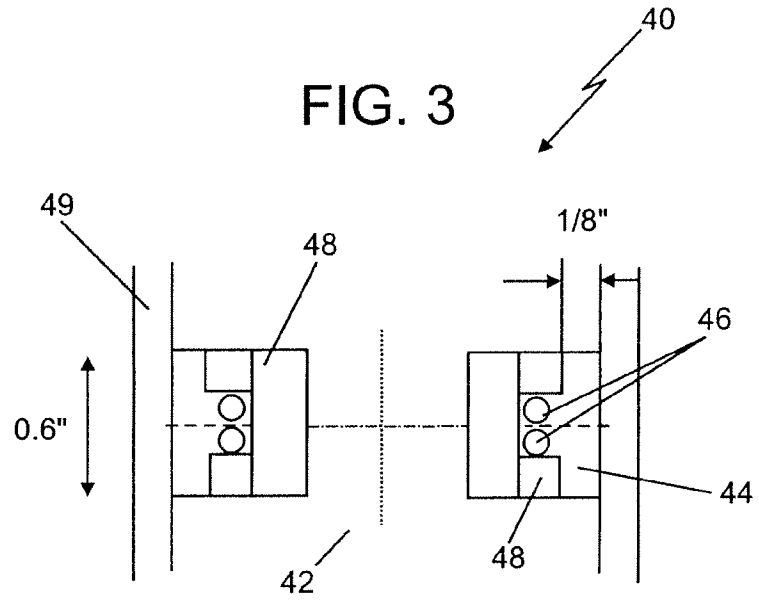


FIG. 4

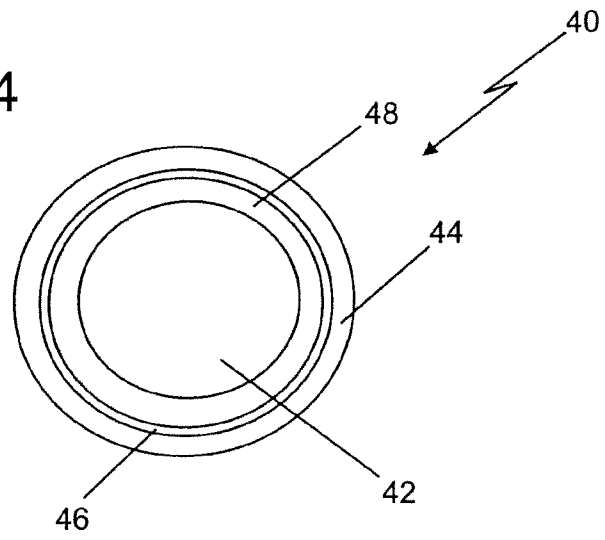


FIG. 5a

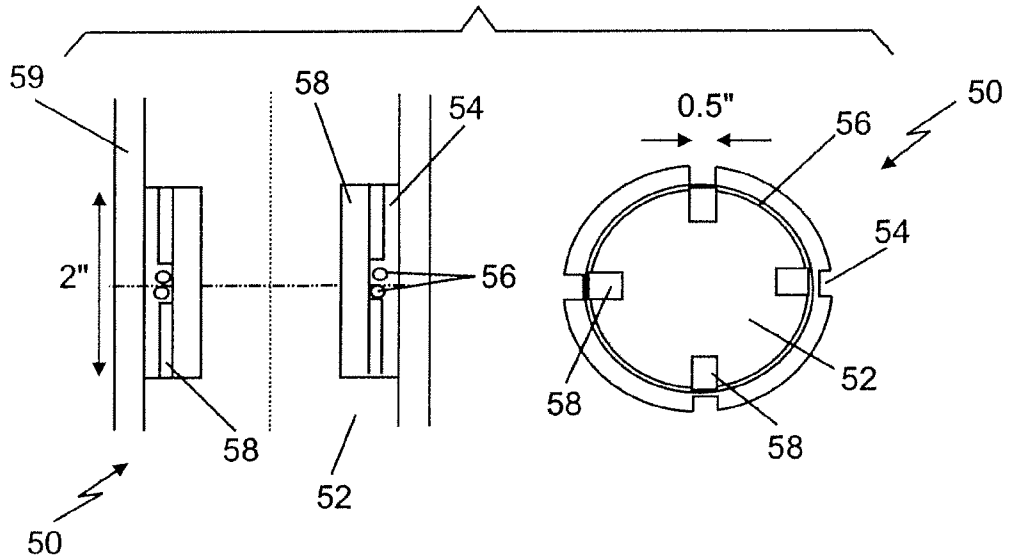


FIG. 5b

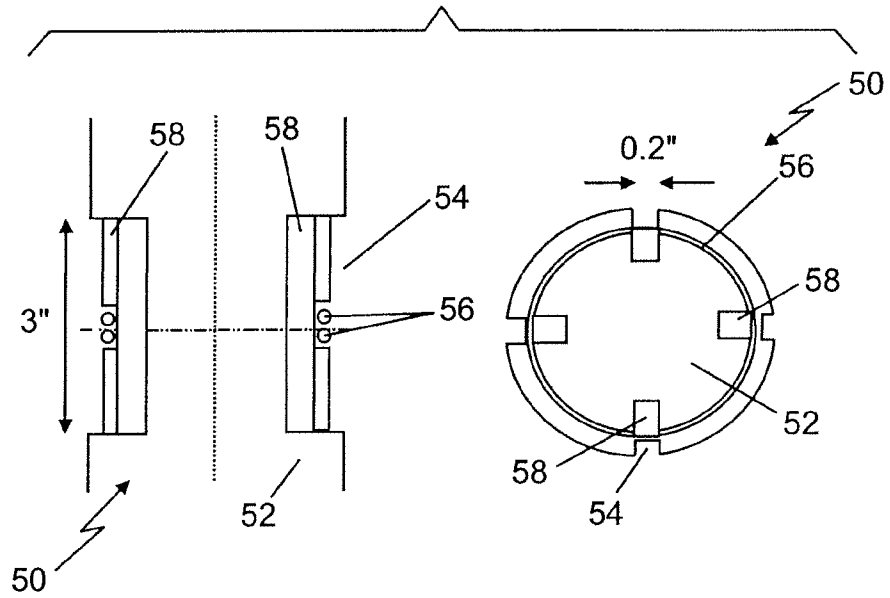


FIG. 6b

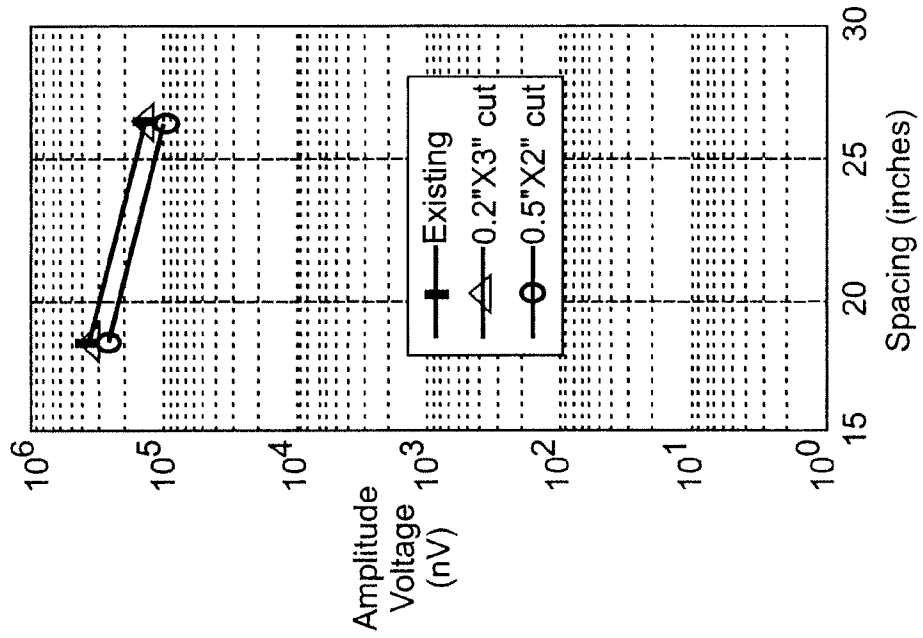
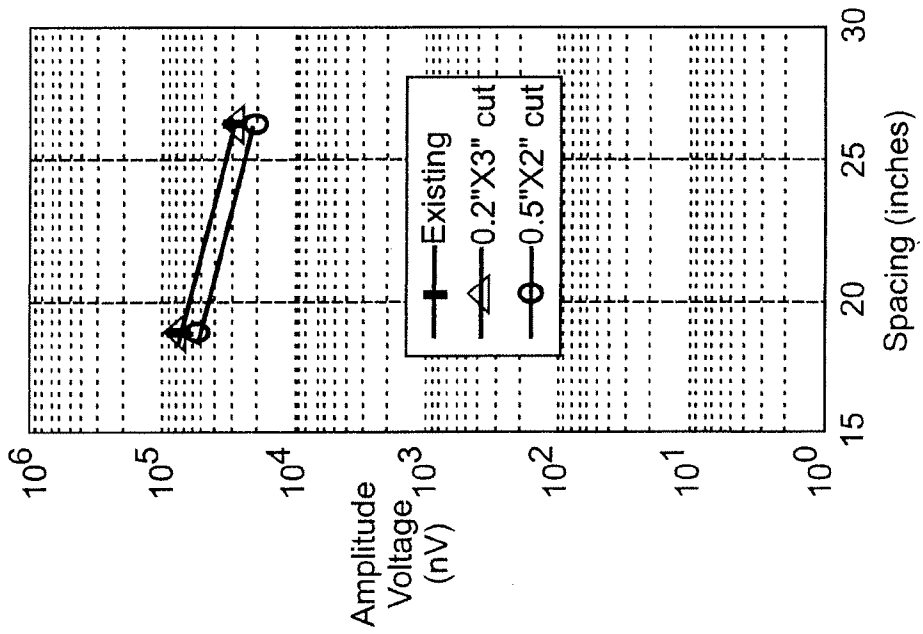
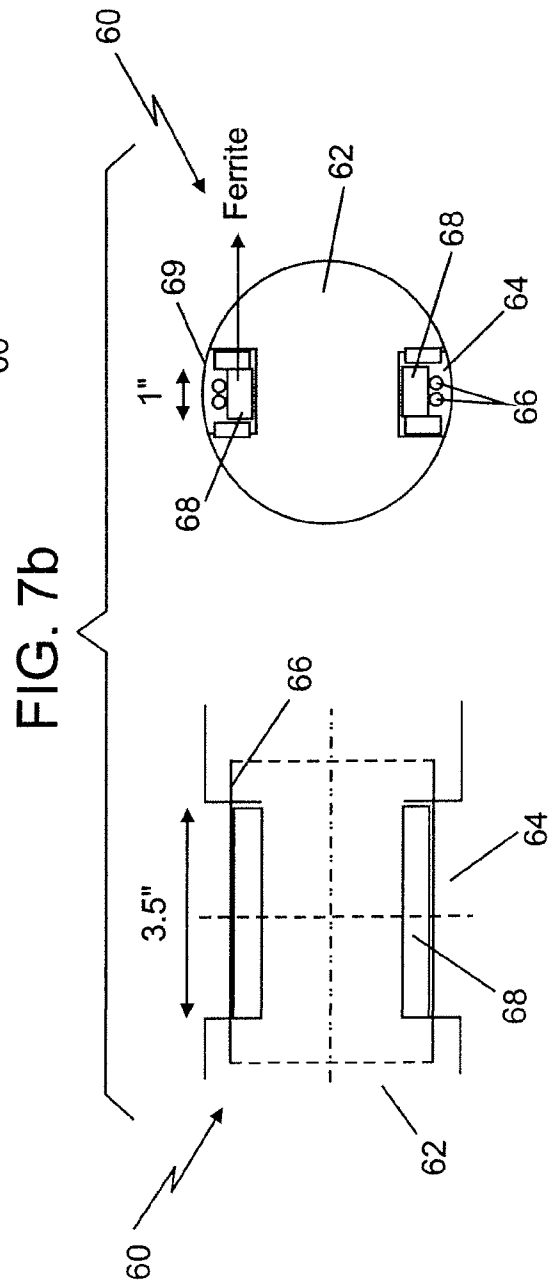
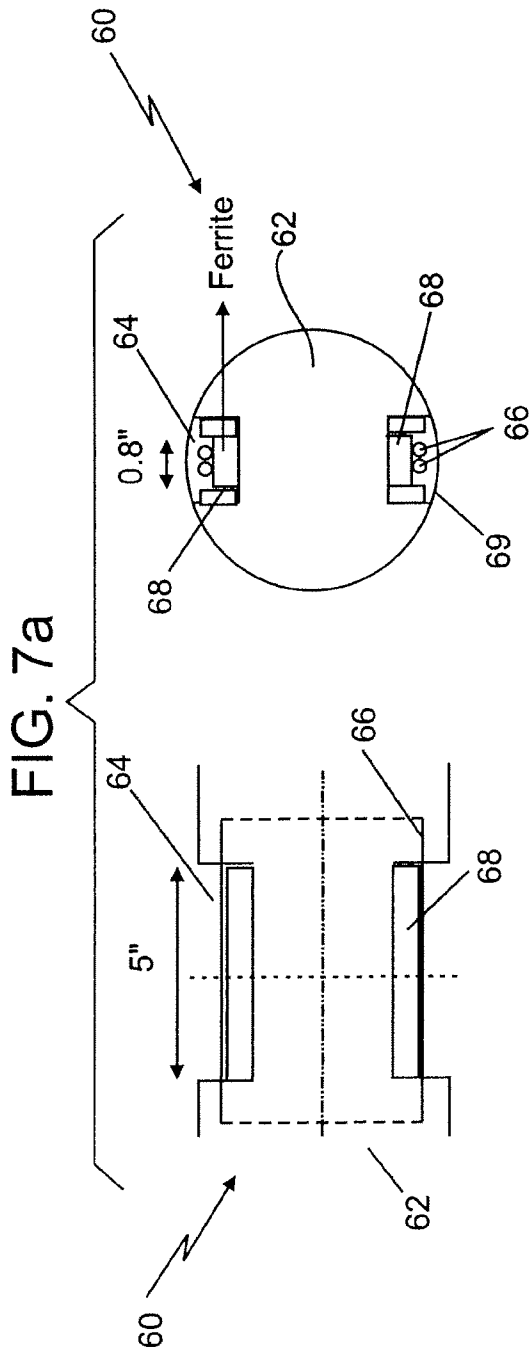
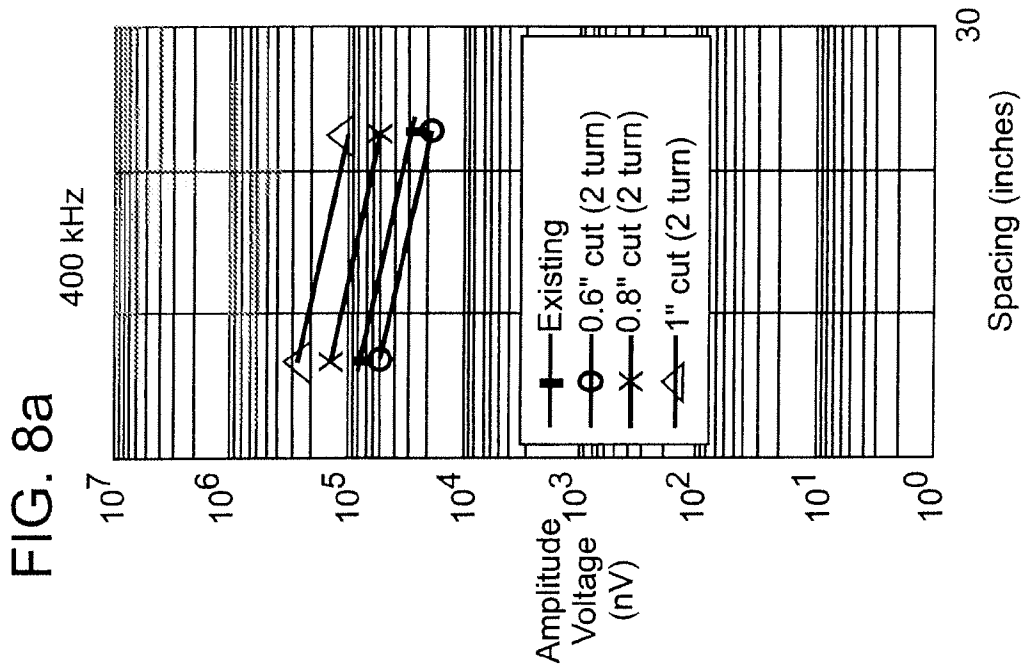
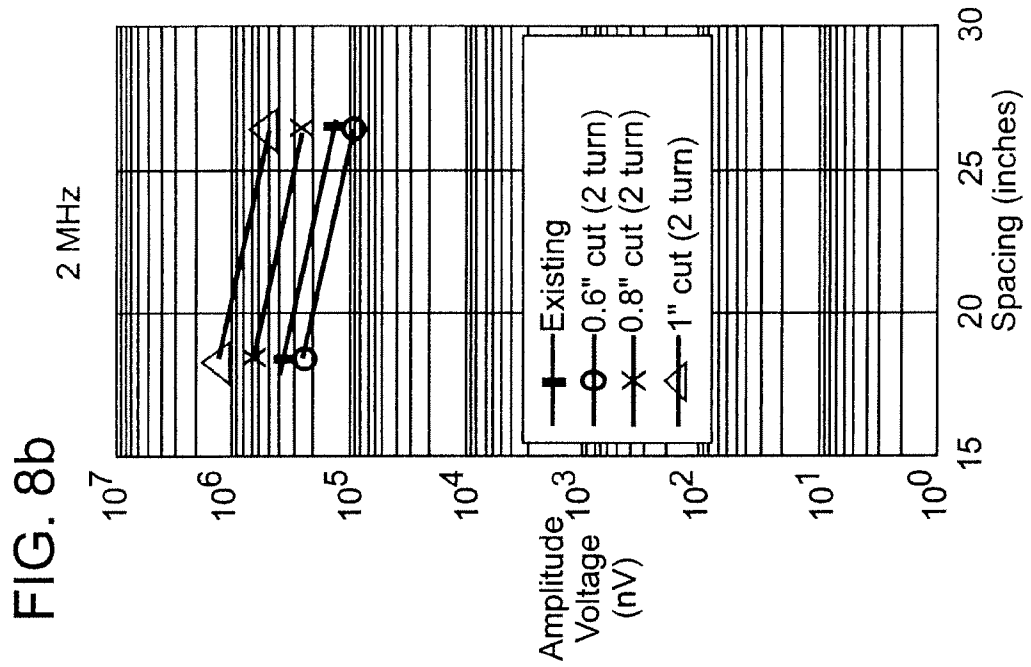
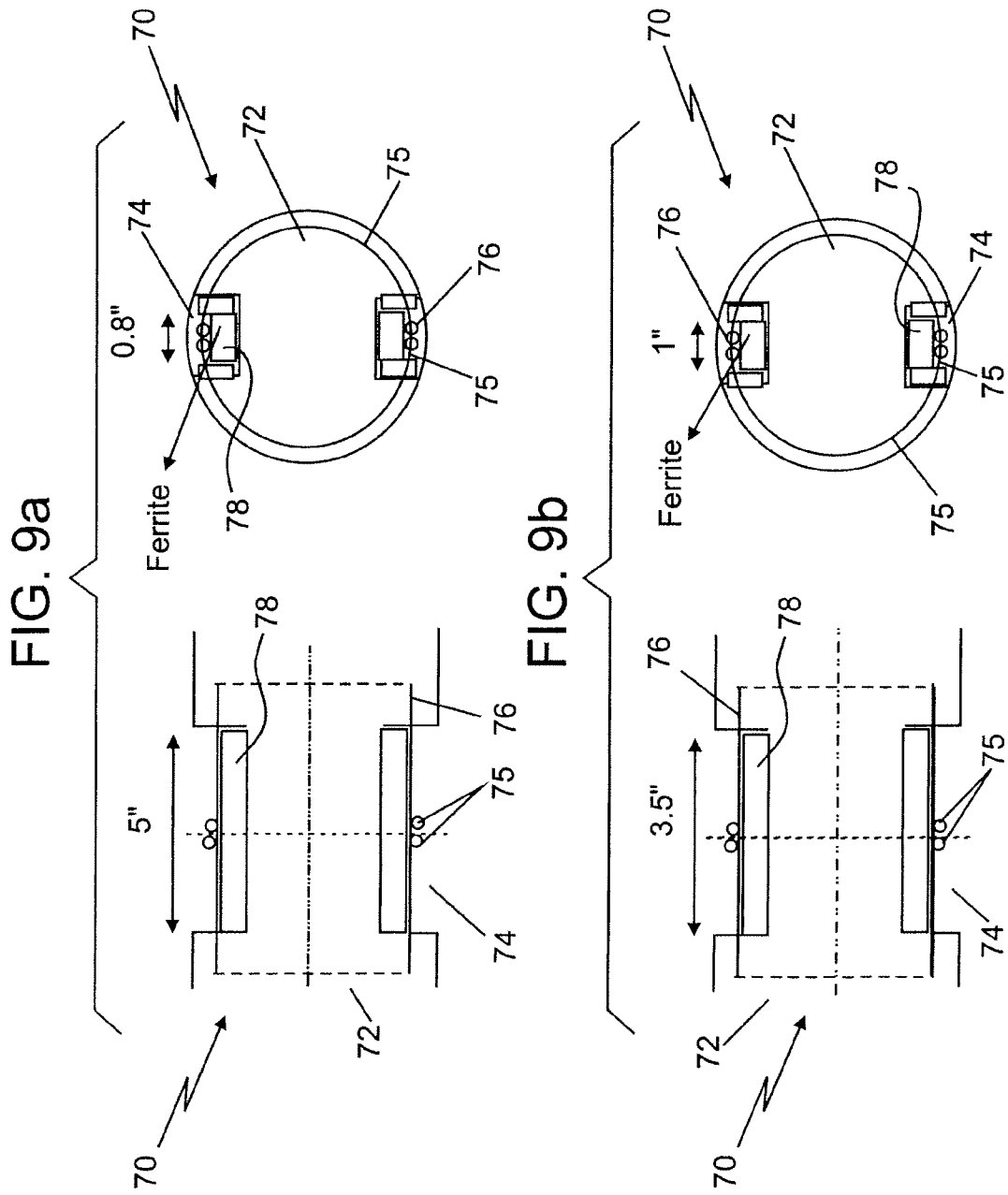


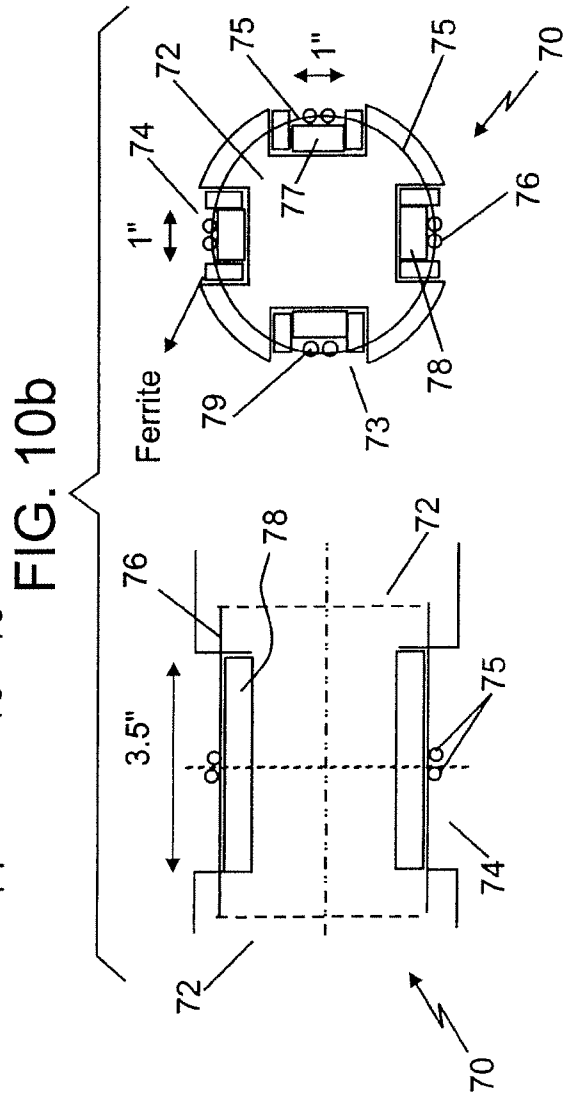
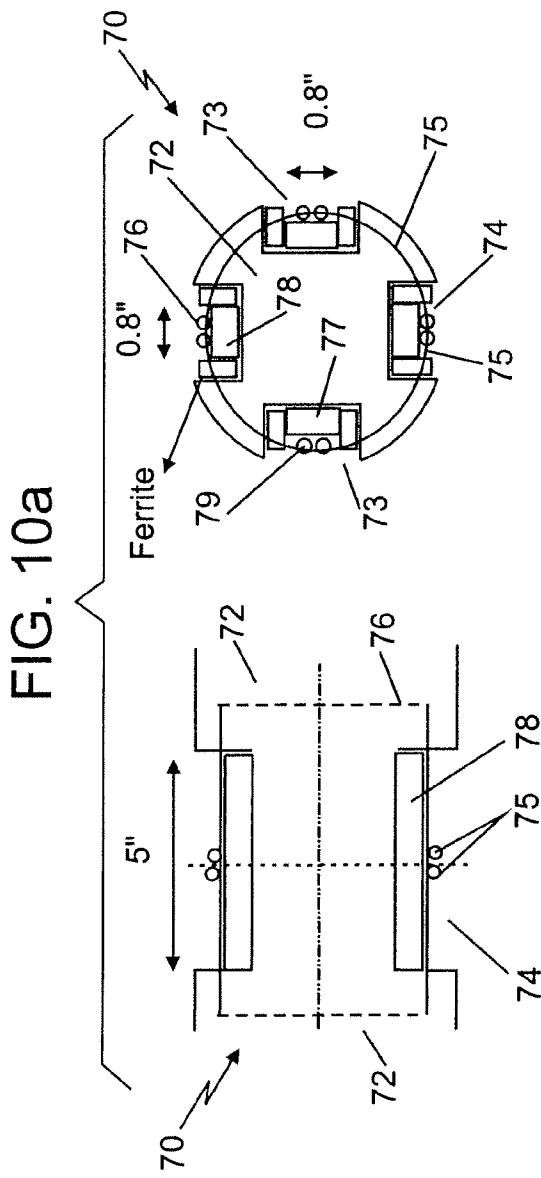
FIG. 6a











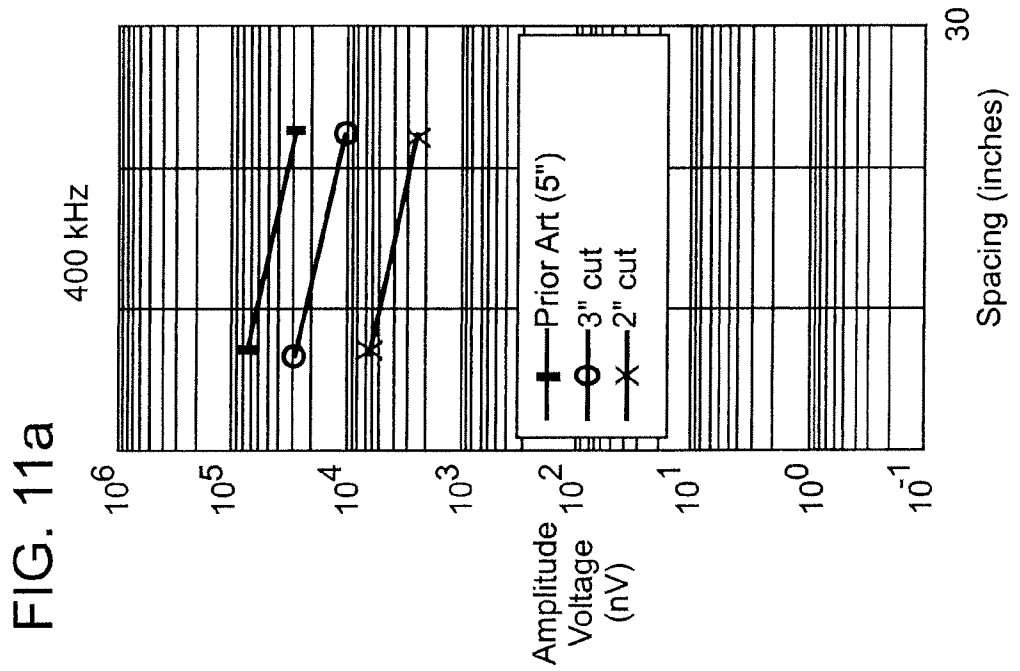
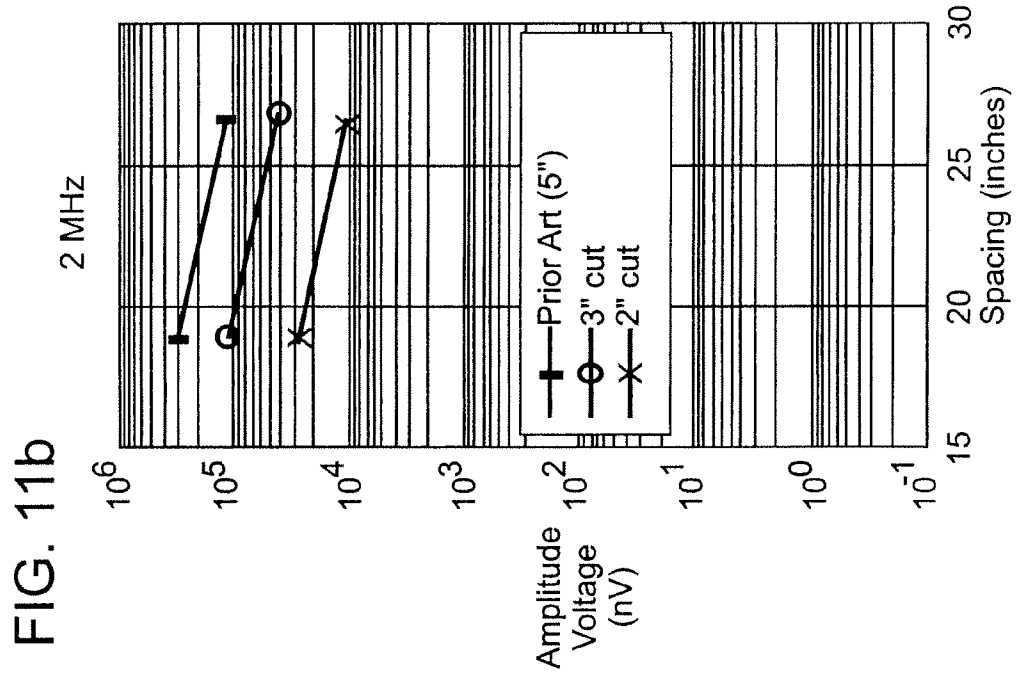


FIG. 12a

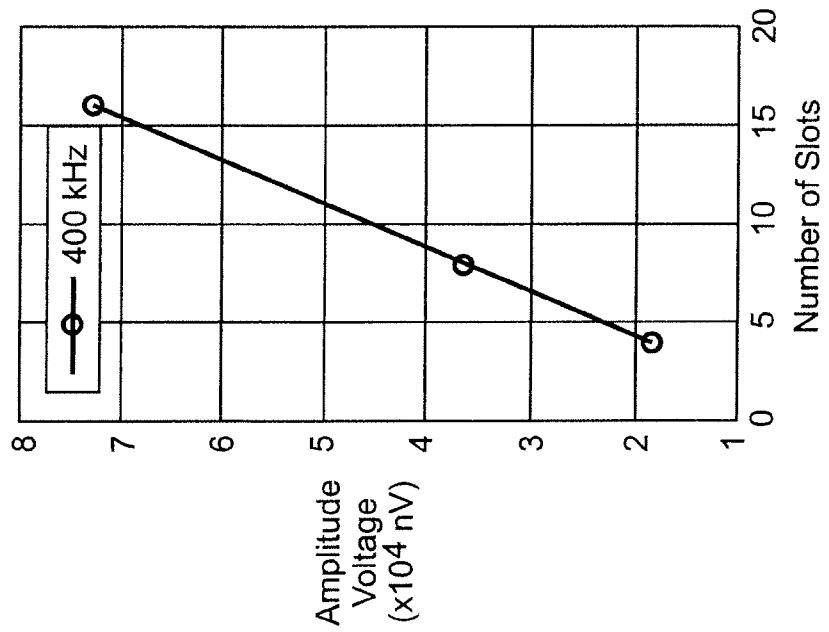


FIG. 12b

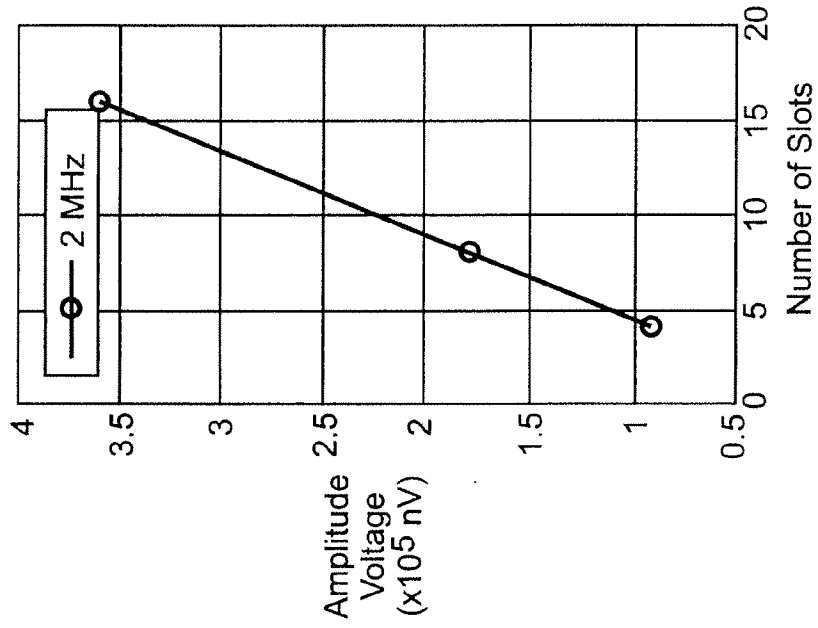


FIG. 13b

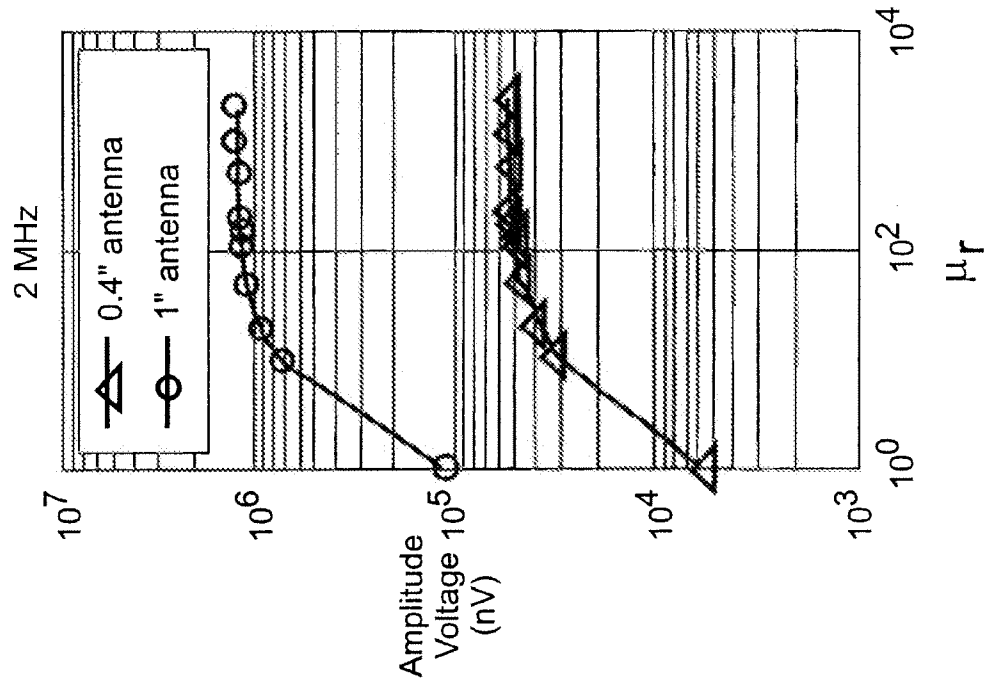


FIG. 13a

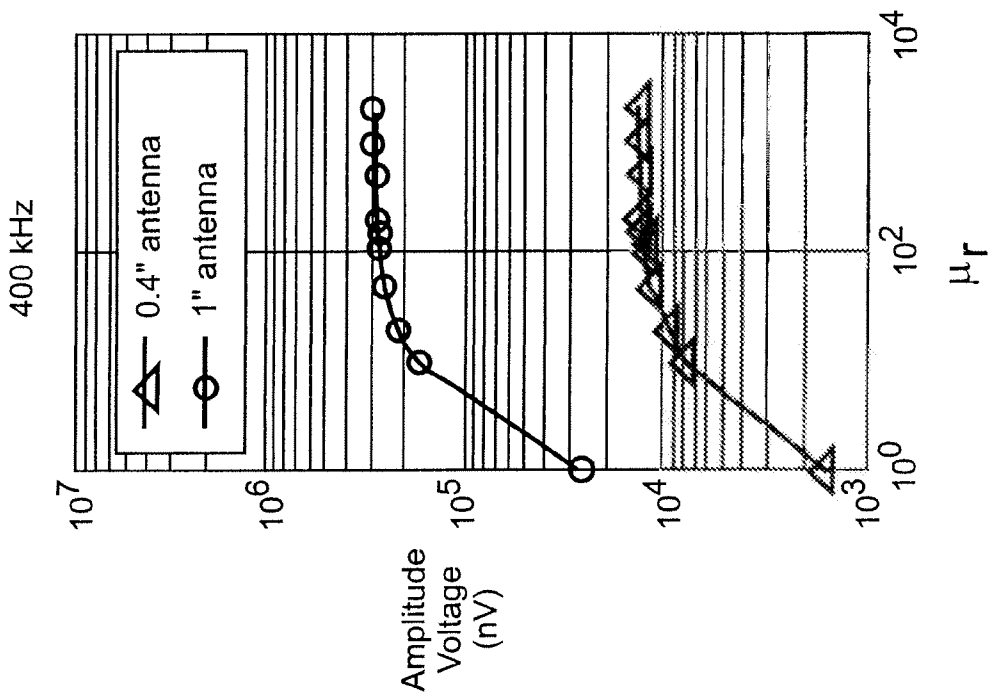


FIG. 14a

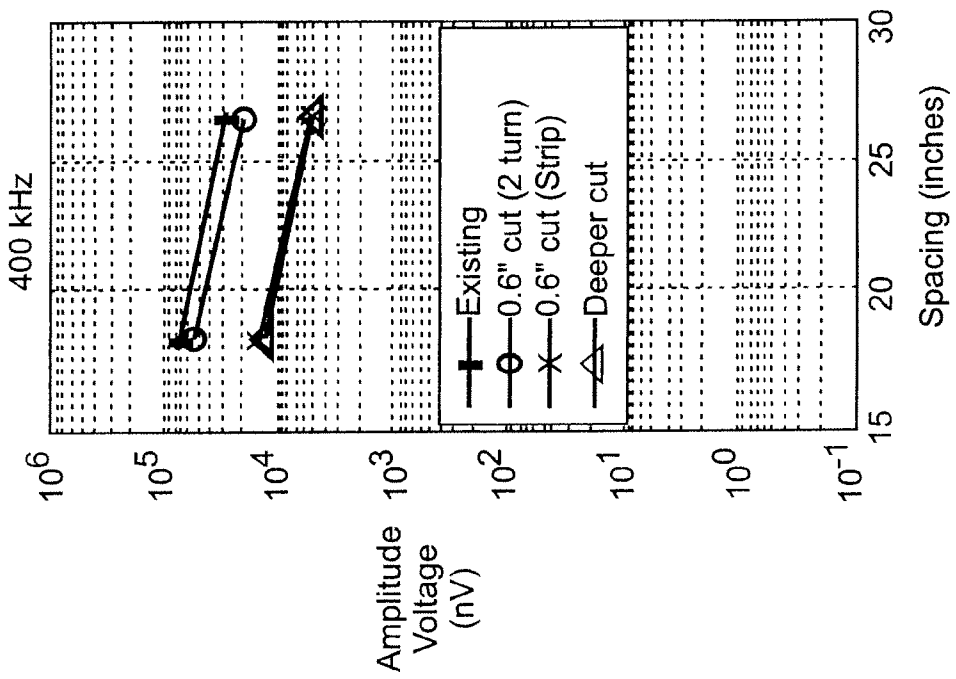
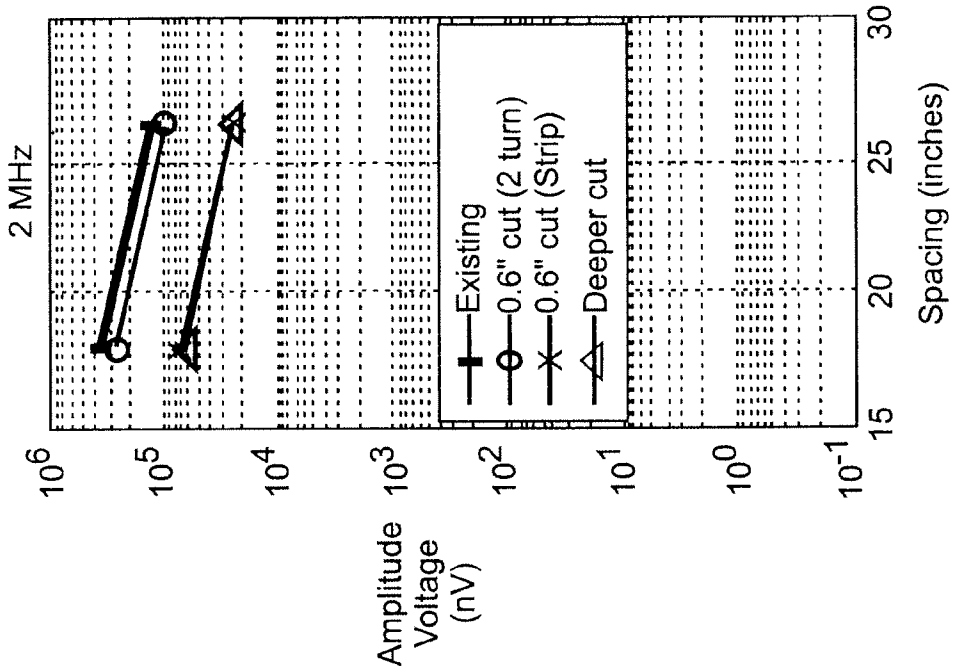


FIG. 14b



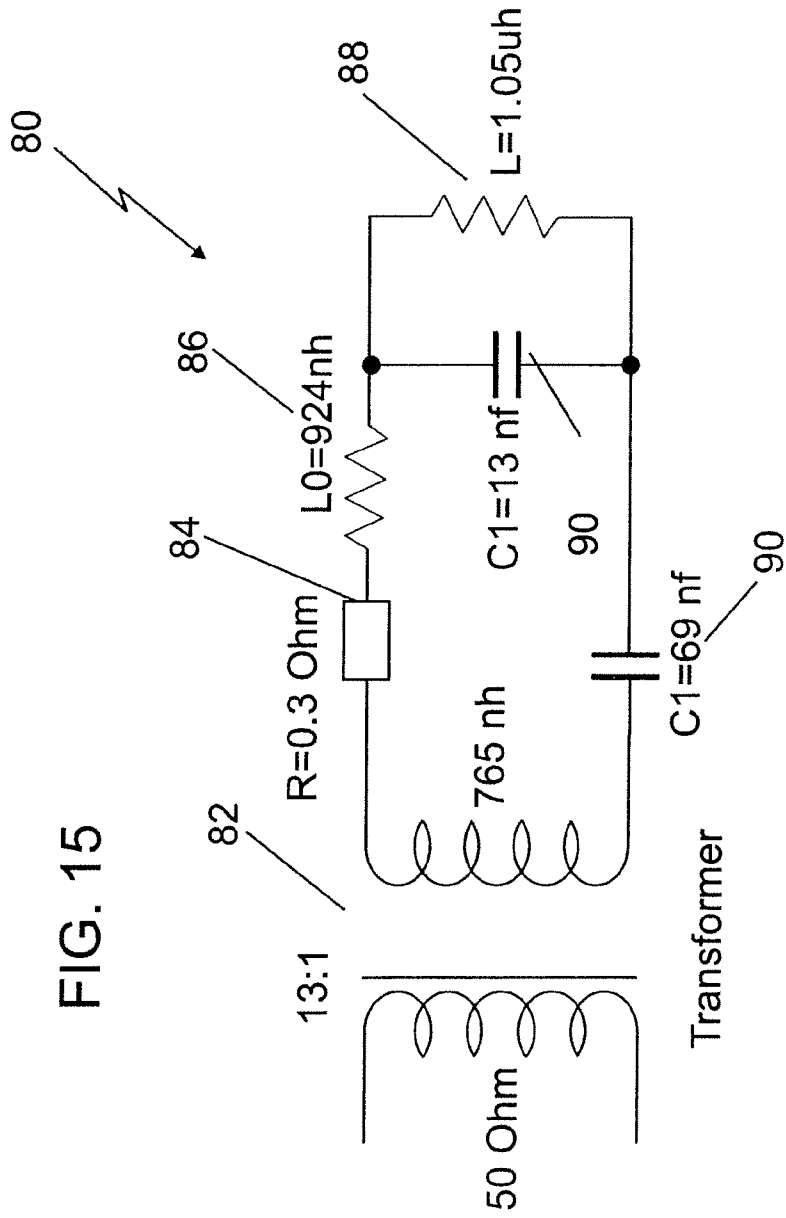


FIG. 16a

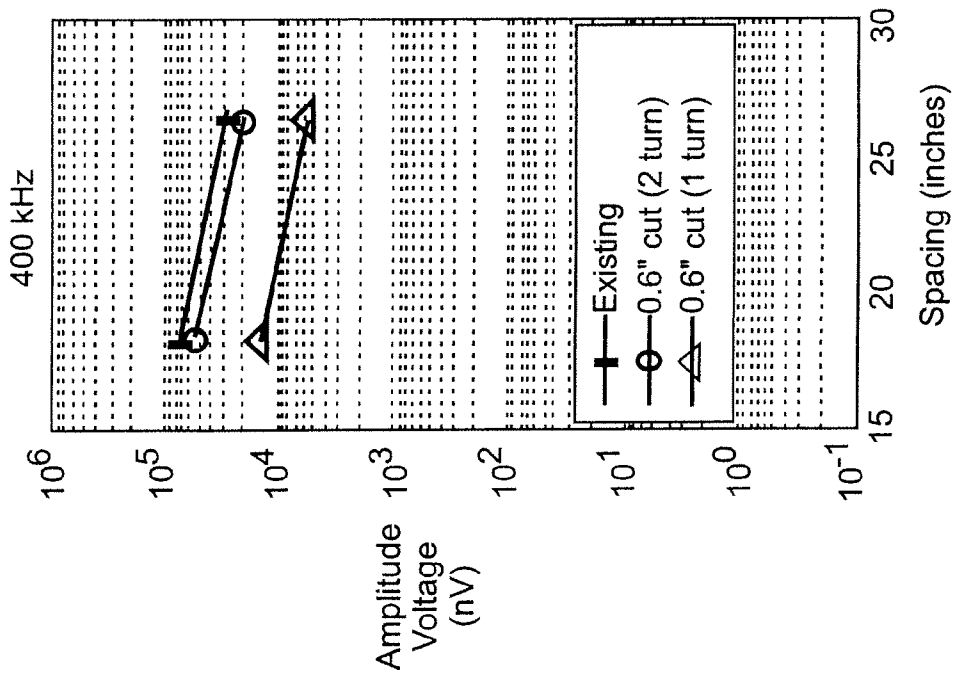


FIG. 16b

