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(57) Abrégé/Abstract:

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ABSTRACT

We form a weather-resistive barrier on a building by applying a compressible latex foam on the joints between adjacent sheets of construction sheathing, with the sheets having been coated with an aqueous coating composition.

WEATHER-RESISTIVE BARRIER FOR BUILDINGS

This invention relates to a method for making a weather-resistive barrier for buildings.

Many buildings are constructed with exterior wood, cement or gypsum-based sheets that are overlaid with decorative facades or claddings (e.g., wood, aluminum or vinyl sidings). When such a building is under construction, in many cases, a flexible sheeting material (e.g., Tyvek from DuPont, felt or tar paper) is nailed or stapled to the construction sheathing before the cladding is mounted. Such sheeting material provides some protection while the building is under construction, as well as after the cladding is mounted. Such protection includes a resistance against wind and liquid water penetration.

Such flexible sheeting, however, is labor intensive to apply because the sheeting material must be unrolled and stretched over the area to be covered by hand, then nailed or stapled into place. And it is not a very good wind or water barrier. As the sheeting material involves placing sheets side by side with some overlap of the sheets, adjacent sheets are not typically sealed together, allowing for wind to enter between the overlaps. Water can also enter the overlaps, and even can enter behind the flexible sheeting through nail or staple holes.

Some (e.g., U.S. Patent Publication No. 20050005567) have suggested using liquid coatings on the sheathing, and using tapes on the joints between adjacent sheets in order to bridge the gaps between adjacent sheets. Such tapes often require a separate coating that must be applied with a trowel or scraper that dries to form a hard sealant over the tape. This taping and coating process is quite labor intensive.

Others (e.g., U.S. Patent Publication No. 20050229524) have suggested applying liquid coatings on sheathing before installation on buildings, and employing tapes or calks to cover the joints between adjacent sheets of sheathing.

Latex foams have been used as sealants and caulks around windows in houses under construction. Typically, such foams are dispensed from cans and expand upon application. Also, foams are designed to fit in tight slots and not over joints with open space on one side. As such, these foams tend not to adhere well to wood or gypsum

sheathing, leaving joints unevenly covered. When such foams dry, however, they are difficult to compress such that they are typically not used to seal joints between sheathing sheets since the expanded foam does not compress when cladding is applied, causing cladding to buckle or ripple outwardly from the building.

This invention is a method of making a weather-resistive barrier on a building that employs adjacent sheets of wood, cement or gypsum exterior sheathing on a structural frame with joints between the sheets, comprising:

(a) applying polymeric coating composition on a plurality of sheathing sheets before installation on the building wherein the polymeric coating has a density when dried of greater than 0.7 g/ml;

(b) installing a plurality of the coated sheathing sheets on the building so that sheets are adjacent one another with joints between adjacent sheets; and

(c) applying a foamed aqueous emulsion polymer composition to at least some of the joints wherein the composition comprises an aqueous emulsion polymer with a T_g less than 25°C, a surfactant, and a blowing agent, and wherein the foamed aqueous emulsion polymer composition has a compressibility factor of not more than 3.

Preferably, the polymeric coating (a) is an aqueous-based coating composition.

As an optional step, after the foamed aqueous composition is applied to the joints, the foamed composition is coated with an aqueous coating composition. When this overcoating is performed, the additional coating can also be applied to at least part of the coated sheets as well. That part is preferably the part adjacent the joints coated with the foamed composition.

The method of this invention further comprises installing a decorative cladding over the coated sheathing.

Preferably, the foamed composition (c) has the ability when dried to be compressed to a thickness of not more than 3 mm under a stress of no more than 0.0035 MPa. In one embodiment, the foamed composition (c) has the ability to self-compress to not more than 3 mm under no externally applied stress

Optionally, should the foamed aqueous composition not flatten or self compress on its own when dried, one can mechanically flatten the foamed composition, say, with a rubber or wooden roller or spatula.

By "joints" we refer to abutting edges of adjacent sheets of sheathing and/or to the gaps that are left between adjacent sheets. Sheathing can have for example, tongue and groove joints, or two adjacent sheets can each have two flat edges that abut one another or are a close distance apart (leaving gaps), as is commonly observed during building construction.

Preferably, at least one of the compositions (a) or (c) comprises a polyfunctional amine or a polyethyleneimine to facilitate skinning of the compositions so as to resist water while the composition(s) is drying, or to allow further coatings to be more quickly applied over those compositions.

In particular, for either the foam component (c) or the coating component (a) or both, it may be desired to cause faster setting or skinning than would otherwise occur by drying. This may be advantageous in preventing a recently applied but incompletely dried weather resistive foam (c) from being washed off by a sudden rainstorm. Also, if sheathing sheets are coated with coating composition (a), the sheets can be stacked together without sticking if the composition (a) dries quickly. Accelerated setting or skinning can be achieved by including in the formulation a polyfunctional amine as disclosed in U.S. Patent No. 5,804,627 (Rohm and Haas) or a polyethyleneimine as disclosed U.S. Patent No. 6,376,574 (Dow). RhoplexTM EC-1791 QS from the Rohm and Haas Company, Philadelphia, PA is a suitable fast setting, waterborne polymer.

The coating composition (a) should be selected so as to allow for an appropriate water vapor transmission for the building. Depending on the climate, the capacity of a building's heating, ventilation and air conditioning (HVAC) system, the material of construction of the entire building and other factors known to building scientists, the coating component (a) should be chosen to give a finished weather resistive barrier with an appropriate water vapor transmission rate to reduce any moisture condensation in the walls of the building. This vapor transmission rate is most often measured according to ASTM E-96 and expressed in units of perms, where higher perms correlate with a greater rate of water vapor transmission. OSB, a common sheathing material, has approx 3-6 perms. For a home, in which interior moisture from cooking and bathing is generated, a weather resistive barrier (a) with > 10 perms may be desired, so that any moisture which

reaches the OSB is not unduly inhibited from diffusing through the barrier (a) to the exterior.

By contrast, commercial buildings usually have higher capacity HVACs, that can remove sufficient moisture from the interior so that water does not condense in the walls. Thus, a low perm weather resistive barrier may be preferred. One skilled in the art of coating formulation can make coatings with a desired perm value, measuring candidate coating compositions (b) according to ASTM E-96. Furthermore, commercially available coatings are sometimes provided with a perm data, which can aid in the selection of a coating properly matched to the building science teachings.

Some suitable composition for the coating component (a) include:

- Rhoplex™ EC-2540 (a flexible, acrylic polymer emulsion) without any further additives.
- A blend of 90 parts Rhoplex™ EC-2540 / 10 parts Ropaque™ Ultra E (a non film forming polymer which provides coating opacity).
- Sto Gold Coat (a yellow coating based on styrene-acrylic copolymer, with 5.7 Perms) from Sto Corp of Atlanta, GA.
- Henry Airbloc 33 (a black coating based on acrylic copolymer, with 11.6 Perms) from Henry Inc. of Huntington Park, Ca.
- Henry Airbloc 06WB (a black coating based on asphalt emulsion, with 0.02 Perms) from Henry Inc. of Huntington Park, Ca.

A suitable composition (a) is given in Example 16 below.

Coating composition (a) can be applied by spray equipment, brush or roller. Preferably coating composition (a) is factory applied, in which case, in addition to the application methods above, one can apply the coating composition (a) on the sheathing by curtain coating, dipping, flood coating. Typically, wood sheathing (e.g., oriented strand board) is made by compressing wood chips impregnated with polymer (e.g., urea or phenol formaldehyde) in a high temperature operation. It would be advantageous to utilize the heat in the sheathing to dry the aqueous coating composition. Thus, one could apply the aqueous coating to the sheathing before the heat curing of the sheathing, or after the heat curing while the sheathing is still at an elevated temperature in the sheeting factory.

Aqueous polymers and copolymers suitable for both the foam aqueous component (c) and for the coating component (a) used in this invention can be acrylic class or vinyl acetate-acrylic class of polymers, as shown in the examples. Other classes of polymers are also suitable, such as styrene-acrylics (e.g. RhoplexTM 2019R from Rohm and Haas or Acronal S-400 from BASF); ethylene-vinyl acetates, styrene-butadienes, and polyurethane dispersions, examples of which are described in U.S. Patent No. 7,179,845 (Fomo Products Inc.). Useful acrylic emulsion polymers include RhoplexTM EC-2540, RhoplexTM EC-1791 QS, RhoplexTM MC-1834, RhoplexTM AC-630. RovaceTM 9100 is an acrylic-vinyl acetate copolymer. The Rhoplex and Rovace polymers are available from Rohm and Haas Co. of Philadelphia, PA.

"Glass transition temperature" or "Tg" means the mid-point glass transition temperature of a polymer as determined by differential scanning calorimetry (DSCTM), in accordance with ASTM E-1356-91 where samples are run on a TA Instruments Q-1000 DSC at a ramp rate of between 10° to 20°C/min., in a nitrogen atmosphere, from -90°C to 150°C (twice). The midpoint inflection was taken from the second heating. When we say that a polymer has a Tg of greater than a stated value, we mean that the midpoint of the single inflection point in the DSC curve is above that value. Should the DSC curve have multiple inflection points, then the midpoint of at least one of the inflection points is above that value.

As explained above, the foam component (c) contains a surfactant. Many surfactants and combinations thereof can be suitable for generation and stabilization of aqueous foams (c) used in this invention. Among these are nonionic surfactants, anionic surfactants and cationic surfactants. Suitable non-ionic surfactants include those based on ethoxylated octylphenol (TRITONTM X series), ethoxylated nonylphenol (TERGITOLTM NP series), ethoxylated secondary alkyl alcohols (TERGITOLTM TMN and 15-S series), all available from Dow Chemical, and linear alcohol ethoxylates in the Brij series from ICI Americas.

Suitable anionic surfactants include anionic sulfates, sulfonates, phosphates or phosphonates such as sodium lauryl sulfate (e.g. Stanfax-234 from Para-Chem), sodium salts of sulfated fatty alcohol ethoxylates (e.g. Disponil FES-32 from Cognis Corp.),

sodium dodecylbenzene sulfonate (e.g. Rhodacal DS-4 from Rhodia Corp.), sodium dioctyl sulfosuccinate (e.g. Aerosol OT-70 from Cytec Industries), ammonium salt of alkyl ethoxylate phosphate (e.g. Rhodacal RS-610 from Rhodia Corp.) and anionic carboxylate salts such as ammonium stearate and potassium oleate (e.g. Stanfax-320 and Stanfax-1 respectively, from Para-Chem). Preferred anionic surfactants are salts of stearic acid, particularly ammonium and potassium salts.

Suitable cationic surfactants include those disclosed in U.S. Patent No. 7,179,845 (Fomo Products Inc.) and in U.S. Patent No. 5,696,174 (Allied Foam Tech Corp)

Suitable blowing agents to make the foam component (c) include air, carbon dioxide, nitrogen, low boiling hydrocarbons (e.g., propane, butane, isobutane) and low boiling halocarbons, and lower alkyl ethers (e.g., dimethyl ether). Air or carbon dioxide are preferred. A mixture of such blowing agents can be used as well.

It is known that carbon dioxide as a blowing agent can make an aqueous foamable composition more acidic by forming carbonic acid (H_2CO_3). Those skilled in the art know well the effect of pH on the stability of certain latex polymers and of foam, and can take suitable measures to ensure the stability of the foamable composition. These measures can include adjusting the pH or buffer content of the foamable composition, adding alternative or additional surfactants, or other means.

In addition to adding gaseous carbon dioxide to foam the composition, it is also well known to generate this gas in situ. This can be accomplished, for example, by including carbonate salts such as sodium carbonate in the aqueous foamable composition (c), then acidifying the composition before or during its application.

Optional ingredients in both the (a) and (c) compositions include biocides (e.g. mildewcides, fungicides and/or bactericides), insecticides, insect repellants, rheology modifiers, extenders (fillers), opacifying pigments (mineral and organic (e.g. opaque polymer)), fly ash, dispersants, defoamers, UV stabilizers, colorants, fire retardants, pH adjusters or buffers, coalescents, cosolvents, glass fibers, carbon fibers, microbeads and anti-freeze agents. It is particularly advantageous to employ an opacifying pigment to at least composition (a) as it allows the coating to be seen on the sheathing material to alert one to any spots that might be missed, and to give the consumer and the installer an assurance that enough coating has been applied.

The polymers used in compositions (a) and (c) may optionally contain an adhesion promoter. Preferably the polymer used in (a) and (c) is acrylic (co)polymer that contains hydroxyl groups and other adhesion promoting groups, such as carboxyl groups, groups from primary, secondary, or tertiary amines, oxazoline ester groups, and the like. Other such adhesion-promoting monomers are disclosed in U.S. Patent No. 6,649,691 and the references cited therein.

The polymers used in compositions (a) and (c) may optional employ technology to improve their resistance to becoming dirty. Such technology could be an additive such as benzophenone as disclosed in US 3,320,198 (Du Pont), or could be a copolymerized monomer as disclosed in US 5,248,805 (Rhone Poulenc) and in US 5,248,805 (BASF).

An optional component of foam (c) is a water-repellant composition. Such compositions can slow any water penetration after the foam dries. Such water-repellant compositions include waxes and silicones.

Optionally the coating composition (a) comprises an infrared-reflective material such as Arctic® infrared reflective pigments from Shepherd Color Company of Cincinnati. Other suitable IR-reflective pigments are aluminum flake reflective pigment, such as those from Eckart America Corp of Louisville, KY. Other examples of suitable infrared-reflective pigments include those described in Lotsch, U.S. Patent No. 4,311,527.

The advantage of infrared-reflective materials in the coating composition (a) is that heat is reflected in the direction where heat originates: (1) out of the building in summer; and (2) into the heated building in winter. This can achieve year-round energy efficiency.

Compositions (a) and/or (c) can optionally contain fire retardant or fire protective extenders and/or chemical flame retardants. Such extenders include alumina trihydroxide or magnesium hydroxide (both from Huber Engineered Materials of Atlanta, GA) and vermiculite. Chemical flame retardants include compounds that are brominated as well as organo-phosphorus or boron-based. Such materials are available from Albemarle Corp. of Baton Rouge, LA.

Compositions (a) and (c) preferably contain materials that impart freeze-thaw stability. Such materials include propylene glycol and ethylene glycol. One can also

use surfactants like Triton X-405 to impart in-can freeze-thaw resistance to the coating or foam compositions (a) and (c).

While the examples below employ either a simple batch mixer or an aerosol can to make foam (c), the foam can be made and applied to buildings using various known methods and equipment, for example, the continuous foamer model no. 2M*172 from E.T. Oakes Corp., Hauppauge, N.Y. Other foam generator/applicator equipment include static mixers, as disclosed in U.S. Patents Nos. 5,492,655 (Schuller International Inc.), 4,986,667 (3M), and 6,422,734 (National Gypsum LLC). Still other foam generators include venturi or air eductors to draw and mix air into a fluid stream, such as disclosed in U.S. Patents Nos. 6,010,083 (BetzDearborn Inc.), 6,042,089, and 6,561,438 (Fountainhead Group).

The aqueous foam component (c) can also be dispensed from a pressurized aerosol container, as disclosed in U.S. Patent No. 7,029,609 (Rathor) and references contained therein.

In addition to the materials described above, other materials used in the Examples below are as follows. Foamaster NXZ (defoamer) is available from Cognis Corp. Snowwhite 12 (calcium carbonate) is supplied by Omya Inc. Colortrend "F" 888-1045 (colorant) is supplied Degussa Corp. Tamol™ 850 (dispersant) is available from Rohm and Haas Co. Acrysol™ TT-615 (rheology modifier) is available from Rohm and Haas Co. Imsil A-150 is ground silica from Unimin Specialty Minerals Inc. of Elco, IL.

"Comparative example, DAP" is DAP Tex Plus available from DAP Inc. of Baltimore, MD. It is a water-borne foam delivered from an aerosol can, propelled with a mixture of propane, butane and methyl ether.

Examples 1-8. Foam generation and evaluation.

To 80g of polymer emulsion Rhoplex™ EC-2540 (Tg -10 °C), surfactants were added with gentle mixing. This liquid mixture was placed in the 5L mixing bowl of a Hobart bakery mixer, then whipped on high speed (#3) with the wire whisk attachment for 5 minutes. Density of the resultant foams was measured by scooping foam into a 135 mL paper cup and striking level, then weighing.

By “compressibility factor” we employ the following test. We apply a wet 12 mm thick and 50 mm wide bead of the foamed composition to a flat surface, and allow it to dry. When dried if it can be compressed to a thickness of not more than 3 mm under a stress of no more than 0.035 MPa, it has a compressibility factor of not more than 3 using the following test with the 2.2 kg weight described below. “MPa” is mega pascals.

Foams prepared as above were troweled in a band 50 mm wide and 12 mm thick (2x0.5 inches) onto a flat board. After drying 24 hours, the thickness of the band was measured, and entered into Table 1 as “H24h.”

A stiff aluminum plate 75 mm long x 25 mm wide x 3.3 mm thick was laid across the dried foam band, to span the width of the band completely and have a contact area between the plate and foam of 25 mm x 50mm (1x2 inches). Weights were placed onto the plate to give a total weight of 225g, (approx 0.5 lb) creating a pressure of about 0.0035 MPa, and the height of the foam under the plate was measured after 1 minute, and entered into Table 1 as “H225 g.” If this value was >2mm, weight was increased to 2.2kg (approx 5lbs) creating a pressure of about 0.035 MPa, the height was measured after 1 minute and entered in Table 1 as “H2.2kg.” This “H2.2.kg” value is the “Compressibility factor” described above and in our claims.

Table 1. Height of foam bands, after drying and compression with weights.

Example	Stanfax-320	2 nd Surfactant	g/mL	H24h	H225g	H2.2kg	Observations
1	4.0g	0	0.09	5mm	2mm		Fine, white foam.
2	0	4.0g Triton X-405	0.11	6	1.5		Some foam cells visible by eye.
3	0	3.0g Tergitol NP-10	0.09	4	1.3		Like #2
4	0	4.0g Stanfax-234	0.05	<2	<1.0		faster to foam vs.1, partial collapse.
5	2.0	1.6g Stanfax-234	0.07	3	1.2		
6	1.0	0.8g Stanfax-234	0.08	4	1.5		
7	0.4	0.8g Stanfax-234	0.09	3	1.0		
8	0.4	1.6 g Stanfax-234	0.06	2	0.9		White, textured
DAP*		comparative example	0.12	22	16	5mm	Expanded in first 24h. When 2.2kg removed, rebounds to 9mm.

Examples 9-12. Alternative latexes

Foams were generated from other latexes in the same manner as examples 1-8.

Their characteristics are reported in Table 2.

Table 2. Foams from alternative emulsion polymers. All used 80g of emulsion, 0.8g of Stanfax-234 and 0.8g of Stanfax-320

Ex	Emulsion	Tg	g/mL	H24h	H225g	H2.2kg	Observations
9	Rhoplex™ EC-1791 QS	-40 °C	0.15	5mm	1.8mm		Flexible skin on top.
10	Rhoplex™ MC-1834	+8 °C	0.07	7	4	1.1mm	
11	Rhoplex™ AC-630	+25 °C	0.05	9	6	1.8	Least flexible.
12	Rovace™ 9100	+18 °C	0.05	1	<1.0		

Example 13. Foam with lower fraction of polymer.

A mixture of 50g of Rhoplex™ EC-2540, 10g of water, 40g of Stanfax-234 and 10g of Stanfax-320 was whipped to a foam as in examples 1-8.

Example 14. Foam and coating made with same coating composition.

As explained above, we can make a foam composition (c) from the same basic coating composition that is used for coating (a). The advantage of this approach is that one can simply add suitable materials to composition (a) to create a foam (c). In this fashion, one can then make a coating (a) that can be also be used to make a foam (c) with the addition of a few additional ingredients.

An example of this is to make (a) with a mixture of 50 g (wet) of Rhoplex™ EC-2540, 10g of water and 50g of Imsil-150 which we blended at low speed for 30 seconds for coating component (b). To make foam (c) from this coating (a), we added a combination of 1g of Stanfax-234 and 10g of Stanfax-320, and the mixture was whipped to a foam with air as in examples 1-8.

Table 3. Characteristics of foams from Examples 13 and 14.

Ex.	Description	g/mL	H24h	H225g	H2.2kg
13	High surfactant	0.13	1.6mm	1.6mm	
14	Inorganic extender	0.13	10	6	1.8mm

Example 15. Foam Properties

15a. Flexibility: The foam from example 6, and the comparative DAP foam were cast 6 mm thick in 200x200 mm sheets over a glass fiber mesh on release paper. After drying at least one day, foam strips with mesh were wrapped around cylindrical metal mandrels of various diameters: 100, 50, 25 and 6 mm. Foam of example 6 did not crack on any mandrel; DAP foam cracked on the all the mandrels.

15b. Tensile Strength and Elongation: The foam from example 6, and the comparative DAP foam were cast 6mm thick in 200x200 mm sheets on release paper, without any mesh. Samples were cured for 4 days. Using a template, dog bone samples were cut, width of neck region 0.25in (6.35mm) width of grasp points 0.75in (19.05mm). Samples were tested in tension until fracture, at a position rate of 2.0in/min (50.8mm/min). Fracture is defined by formation of two independent pieces of material, that are in no way connected to one another. For Example 6, the maximum tensile strength of 0.045 MPa at 2750% elongation. For DAP, the maximum strength of 0.02 MPa occurred at 100% elongation.

Tensile Strength & Elongation	Example 6 Foam	DAP Comp.
Yield Strength (MPa)	0.01	0.015
% Elongation @ Yield	180	50
Max Strength (MPa)	0.045	0.02
% Elongation @ Max Strength	2750	400
Break Strength (MPa)	0.04	0.00
% Elongation @ Break	3000	175

15c. Creep resistance in compression: Sheets of foam were cast on release paper. to an initial thickness of 12mm (and 50mm wide and 200 mm long), and dried at least one day. A stiff aluminum plate weighing 2.5 grams (40mm x 40 mm x 0.66mm thick) was placed on each sheet. Weights were applied on the aluminum plate to compress its thickness, and the decrease in thickness was measured over time. To experience a similar compressive creep as the comparative example, the inventive foam Example 6 required less than one tenth as much weight.

	Foam Ex. 6	Foam Ex. 6	DAP	DAP
Initial Height $t=t_0$ (MM)	10.58	8.44	12.94	12.8
Weight applied (g)	7g	20g	400g	800g
% Compression over time				
t=30min	18%	33%	18%	31%
60min	24%	29%	25%	38%
90min	24%	28%	31%	39%
120min	29%	28%	32%	40%
45h	40%	43%	41%	52%

The significant of this compressibility is that decorative cladding can easily be applied over foams used in this invention without the cladding being distorted by not being able to compress the foam that might be protruding from the exterior sheathing joints.

Example 16. A liquid sheathing coating:

Material	Part by Weight
Water	9.5
Propylene Glycol	0.67
Tamol™ 850	0.26
Triton x-405	3.4
Foamaster NXZ	0.15
Rhoplex™ EC 2540	37.14
Begin Grind	
Snowwhite 12	47.91
Foamaster NXZ	0.15
Colortrend "F" 888-1045	
Red Iron Oxide	0.12
Aqueous Ammonia (28%)	0.17
Acrysol™ TT-615	0.53
Total	100

The above recipe was made on a 5000 g scale. During the initial weigh out, materials were added in order one at a time to a grind pot. Following each addition, the contents of the pot were briefly agitated by swirling. After the addition of Rhoplex™ EC-2540 the grind pot was transferred from the bench top and placed on the Cowles™ high speed disperser to mix and grind ingredients. Snowwhite 12 was slowly added to ensure good dispersion. Agitator speed was initially set to 1000 rpm and was increased with addition of the Snowwhite 12 to approximately 1300 rpm. Foamaster NXZ was added immediately following the Snowwhite 12 addition, and the grind was held for 5 minutes for full incorporation. Following the addition of the Acrysol™ TT-615, the grind was held for 20 minutes. During this time the agitator speed was increased to between 2000-3000 rpm depending on conditions. Grind was filtered with 100mesh and de-aired using a vacuum canister and agitator.

Example 17. Impact resistance of foam.

Foam from example 6, and the comparative DAP foam were cast in 14 mm thick 127x127 mm square Teflon™ molds on top of release paper. After 4 days of cure the samples were removed from the molds but remained affixed to the release paper, and were then subjected to a falling dart impact tester. The dart (908g (2lb)) weight and 12mm ((0.5inch) spherical tip) was dropped onto a fresh area of foam which rested on a hard flat board, from progressively higher heights until the coating was visibly torn. The foam of Example 6 passed at 1372 mm (54 inches) the highest height the impact tester will allow. Comparative example DAP failed at the lowest height of 12mm (0.5 inches).

Example 18 – Preparation of sheathing test joint

Two 150x75 mm rectangular sheets of oriented strand board (“OSB”) are laid onto a flat surface and coated by spray over the entire exterior surface with the coating of example 16 and then dried overnight, to a final coating thickness of approximately 15 dry mils (0.38 mm). These sheets are then clamped to a rigid backing such that the 150mm sides are parallel to each other but 6mm apart, forming an open, 6 mm-wide gap between the adjacent rectangles. Such a gap simulates those found between sheets of exterior sheathing in residential and commercial buildings under construction.

A band of foam of example 6 is applied 50mm wide and 12 mm thick when wet over and across the gap and dried overnight to form a foam bridge approx 3 mm thick. The clamps are removed to free the sheets from the supporting backing, to provide a test joint spanned by foam.

Optionally, before removing the clamps, the coating of example 16 is applied across the foam which bridges the joint and onto approximately 6 to 12mm of the coated OSB adjacent to the foam-bridged joint, such that no uncoated foam is seen. This coating is conveniently applied by brush in 2 coats with 2 hours of drying between coats then dried overnight, to a final coating thickness of approximately 15 dry mils (0.38 mm). The clamps are removed to free the sheets from the supporting backing, to provide a test joint spanned by foam and entirely covered by the coating. Multiple samples of these joints are used in the following water tightness test.

Example 19 Foam from aerosol can. A mixture of 95g of Rhoplex™ EC-2540, 4g of Stanfax-320 and 1g of Stanfax-234 was placed into a an aluminum can (200 mL are available from McKernan Packaging Clearinghouse of Reno, NV) which was closed with a bottle closure (Body Orifice #062 , Stem Orifice #018 and a Spout # S20L7, all available from Seaquist Perfect Dispensing of Cary, IL). The can was then charged with 2.0g of propane and 4.0g of n-butane. The can was shaken for 30 sec, inverted and the trigger depressed, to dispense a foam of similar properties as in example #1 above. Optionally, a flexible hose was affixed to the can spout before dispensing to allow the stream of foam to be directed into and over a joint between OSB boards. As a further option, a flattened funnel (opening 42mm wide x 4mm thick) was affixed to the end of the flexible hose, allowing a band of foam to be applied over the gap in a rapid single pass.

Examples 20-21. Dimensional stability of aqueous foam from an aerosol can.

Aerosol cans as in Example 20 were filled with the following recipes, then were kept on a shelf for 3 months to monitor their storage stability.

	Ex 21	Ex 22
Rhoplex™ EC-2540	100g	-
Rhoplex™ 1791 QS	-	100g

Stanfax-320	7.25	6.75
Propane	10	5.7
Butane	0	2.0

After storage, foams were discharged and troweled into a band 50 mm wide and 12 mm thick on a flat board and the thickness of the band was measured periodically for 24 hours, after which no further thickness changes were seen. All foams expanded in size for approximately 2 hours after the time of application. Overnight, the foams which are suitable as a component of the invention reduced to 25% of their as-applied thickness or less. The comparative DAP example continued to expand beyond the 2 hour mark, and its ultimate thickness was about double its as-applied thickness.

Time after discharge	Ex. 21	Ex. 22	DAP Comp.
30 min	15.4mm	15.9mm	17.4mm
45	15.7	15.8	18.5
60	15.6	15.5	19.3
90	15.6	15.6	20.4
120	15.3	15.2	21.2
24 hours	3.0	2.0	24.3

The method of this invention has several interesting characteristics. First, as compared to sheet material such as Tyvek, the method of this invention may increase the durability of the building structure by allowing less wind-driven water to get to the sheathing material, which can be important when oriented strand board is used as the underlying sheathing material. The method may also improve the acoustics of the building under construction by (1) sealing the joints between adjacent sheets of sheathing to retard sound transmission between the joints; and/or (2) the coating composition on the sheathing material may dampen vibration.

WE CLAIM

1. A method of making a weather-resistive barrier on a building that employs adjacent sheets of wood, cement or gypsum exterior sheathing on a structural frame with joints between the sheets, comprising:

(a) applying a polymeric coating composition on a plurality of sheathing sheets before installation on the building wherein the polymeric coating has a density when dried of greater than 0.7 g/ml;

(b) installing a plurality of the coated sheathing sheets on the building so that sheets are adjacent one another with joints between adjacent sheets; and

(c) applying a foamed aqueous emulsion polymer composition to at least some of the joints wherein the composition comprises an aqueous emulsion polymer with a T_g less than 25°C, a surfactant, and a blowing agent, and wherein the foamed aqueous emulsion polymer composition has a compressibility factor of not more than 3.

2. The method of claim 1 further comprising installing a decorative cladding over the sheathing.

3. The method of claim 1 wherein the foamed composition has the ability when dried to be compressed to a thickness of not more than 3 mm under a stress of no more than 0.0035 MPa.

4. The method of claim 1 wherein the foamed composition has the ability to self-compress to not more than 3 mm under no externally applied stress.

5. The method of claim 1 wherein at least one of the compositions (a) or (c) further comprises a polyfunctional amine or a polyethyleneimine.

6. The method of claim 1 wherein composition (a) comprises an infrared-reflective material.