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- (54) **Title:** GUIDED WAVE RADAR LEVEL GAUGE SYSTEM WITH DIELECTRIC CONSTANT COMPENSATION THROUGH MULTI-FREQUENCY PROPAGATION

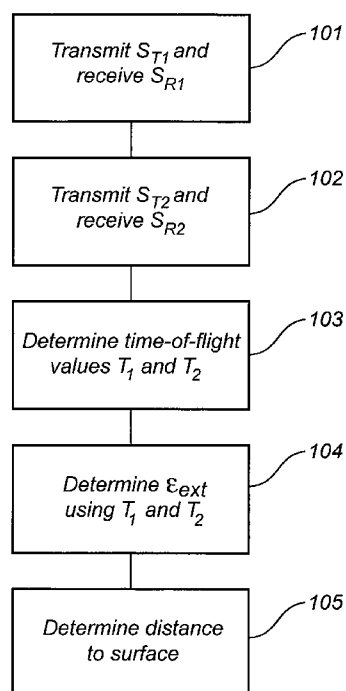


Fig. 6

- (57) **Abstract:** The present invention relates to a method of determining a filling level of a product contained in a tank by propagating a first transmitted electromagnetic signal in a first frequency range and a second transmitted electromagnetic signal in a second frequency range different from the first frequency range along a transmission line probe towards a surface of the product in the tank, receiving a first reflected electromagnetic signal in the first frequency range and a second reflected electromagnetic signal in the second frequency range, and determining the filling level based on a time-of-flight of the first reflected electromagnetic signal and a difference in time-of-flight of the first reflected electromagnetic signal and the second reflected electromagnetic signal.



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GUIDED WAVE RADAR LEVEL GAUGE SYSTEM WITH DIELECTRIC
CONSTANT COMPENSATION THROUGH MULTI-FREQUENCY
PROPAGATION

Technical Field of the Invention

The present invention relates to a guided wave radar level gauge system and to a method of determining a filling level in a tank.

5

Technical Background

Radar level gauge systems are in wide use for measuring process variables of products contained in tanks, such as filling level, temperature, pressure etc. Radar level gauging is generally performed either by means of non-contact measurement, whereby electromagnetic signals are radiated towards the product contained in the tank, or by means of contact measurement, often referred to as guided wave radar (GWR), whereby electromagnetic signals are guided towards and into the product by a transmission line probe. The transmission line probe is generally arranged vertically from top to bottom of the tank. The electromagnetic signals are subsequently reflected at the surface of the product, and the reflected signals are received by a receiver or transceiver comprised in the radar level gauge system. Based on the transmitted and reflected signals, the distance to the surface of the product can be determined.

More particularly, the distance to the surface of the product is generally determined based on the time between transmission of an electromagnetic signal and receipt of the reflection thereof in the interface between the atmosphere in the tank and the product contained therein. In order to determine the actual filling level of the product, the distance from a reference position to the surface is determined based on the above-mentioned time (the so-called time-of-flight) and the propagation velocity along the probe of the electromagnetic signals.

This propagation velocity is influenced by various factors, such as the configuration of the transmission line probe and environmental conditions inside the tank. Such environmental conditions, for example, include the composition of the atmosphere above the surface of the product contained in

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the tank, and product residue which may have adhered to the probe as the filling level of the product changes inside the tank.

In boiler applications, for example, the atmosphere inside the boiler tank may be steam under high pressure, in which case the difference in
5 dielectric constant may be quite large for different operating conditions.

US 7 525 476 discloses a guided wave radar level gauge system in which reference reflectors are provided at known positions along the transmission line probe and in which the difference between the measured distance and the known distance between a pair of reference reflectors is
10 used to compensate for variations in propagation velocity caused by variations in the propagation conditions along the transmission line probe.

Although allowing for a more accurate filling level determination in applications with varying propagation properties inside the tank, the reference reflectors reflect a portion of the signal, which means that there is some
15 reduction in the sensitivity of the radar level gauge system as compared to a corresponding guided wave radar level gauge system without reference reflectors.

Summary

20 In view of the above, it would be desirable to provide a guided wave radar level gauge system in which accurate filling level determination can be achieved in applications with varying propagation properties without the need for providing reference reflectors along the transmission line probe.

According to a first aspect of the present invention, it is therefore
25 provided a guided wave radar level gauge system, for determination of a filling level of a product contained in a tank, the guided wave radar level gauge system comprising: a transceiver for generating, transmitting and receiving electromagnetic signals in a first frequency range and in a second frequency range different from the first frequency range; a transmission line
30 probe connected to the transceiver, and arranged and configured to guide transmitted electromagnetic signals from the transceiver through a surrounding medium towards the product inside the tank, and to return reflected electromagnetic signals resulting from reflection of the transmitted electromagnetic signals by a surface of the product back towards the
35 transceiver, the transmission line probe being configured to guide electromagnetic signals in the first frequency range with a first propagation velocity exhibiting a first dependence on a dielectric constant of the

surrounding medium, and guide electromagnetic signals in the second frequency range with a second propagation velocity exhibiting a second dependence, different from the first dependence, on the dielectric constant of the surrounding medium; and processing circuitry connected to the

5 transceiver for determining the filling level based on a first reflected electromagnetic signal in the first frequency range, a second reflected electromagnetic signal in the second frequency range, and a known relation between the first dependence and the second dependence on the dielectric constant of the surrounding medium.

10 The "transceiver" may be one functional unit capable of transmitting and receiving electromagnetic signals, or may be a system comprising separate transmitter and receiver units. Moreover, the transceiver may comprise a first transceiver unit operating in the first frequency range and a second transceiver unit operating in the second frequency range.

15 The processing circuitry may be configured to control the transceiver(s) to provide a first electromagnetic transmission signal in the first frequency range and a second electromagnetic transmission signal in the second frequency range simultaneously or in sequence one after the other. For example, the first electromagnetic transmission signal may first be transmitted

20 and a reflection thereof at the surface be received, and thereafter the second electromagnetic transmission signal may be transmitted and a reflection thereof at the surface be received. Transmitting the first and second electromagnetic transmission signals in sequence may be advantageous to keep down the current consumption of the guided wave radar level gauge

25 system.

The known relation between the first dependence and the second dependence may, for example, be the ratio between the first dependence and the second dependence, or, in other words, the dependence of the ratio between the first propagation velocity and the second propagation velocity on

30 the dielectric constant of the surrounding medium.

The tank may be any container or vessel capable of containing a product, and may be metallic, or partly or completely non-metallic, open, semi-open, or closed.

The present invention is based on the realization that a transmission

35 line probe can be configured in such a way that the interaction or coupling between an electromagnetic signal and a surrounding medium is dependent on the frequency of the electromagnetic signal.

The present inventor has further realized that the stronger the interaction or coupling between an electromagnetic signal and the surrounding medium is, the more influence will the dielectric properties of the surrounding medium have on the propagation velocity of the electromagnetic signal along the transmission line probe. This insight can be utilized to achieve a correct filling level determination even when the dielectric properties of the surrounding medium, such as the tank atmosphere, are unknown.

In other words, given a suitably configured transmission line probe, two electromagnetic signals in different frequency ranges traveling along the transmission line probe are influenced differently by changes in the dielectric constant of the medium surrounding the transmission line probe. Hereby, a filling level determination that is independent of the dielectric constant of the medium surrounding the transmission line probe can be achieved.

As a consequence, the effect of probe contamination on the propagation velocity of the electromagnetic signals, in addition to the effect of the presence of vapor above the surface, can be compensated for even in cases when the probe contamination and/or the presence of vapor above the surface would result in a non-uniform change of the propagation velocity.

Accordingly, the guided wave radar level gauge system according to various embodiments of the present invention provides for accurate filling level measurement even in cases when the atmosphere in the tank has an unknown and possibly non-uniform dielectric constant, and the transmission line probe has an unknown amount of tank content adhering to it.

The dependence of the propagation velocity for each frequency range on the dielectric constant of the surrounding medium may, for example, be empirically determined. Depending on the actual configuration of the transmission line probe, it may also be feasible to determine an equation specifying the propagation velocity as a function of the dielectric constant of the surrounding medium.

To facilitate the determination of the filling level by providing for distinctly different dependencies on the dielectric properties of the surrounding medium for the first and second frequency ranges, the first frequency range may have a first center frequency and the second frequency range may have a second center frequency, the second center frequency being at least two times the first center frequency. In other words, the second frequency range may be at least twice the frequency of the first frequency range. To provide for even more distinctly different dependencies and/or allow

for greater flexibility in the design of the transmission line probe, the difference between the first and the second frequency range may be greater. For example, the second center frequency may be higher than one of three times, five times and ten times the first center frequency.

5 For each frequency range, the bandwidth may be around 1 GHz.

Advantageously, the second center frequency may be at least 3 GHz, such as at least 4 GHz, 5 GHz or 6 GHz. Suitable center frequencies of the first frequency range and the second frequency range may, for example, be 0.5 GHz and 6 GHz. For such frequency ranges, a sufficiently large difference
10 in propagation velocity dependence can be achieved, and standard components can be used in the guided wave radar level gauge system. This allows for a cost-efficient GWR system.

According to various embodiments, the transmission line probe may comprise a probe conductor and a dielectric enclosing structure at least partly
15 enclosing the probe conductor.

The dielectric enclosing structure may advantageously fully enclose substantially all of a portion of the probe conductor being arranged inside the tank.

This type of the transmission line probe will in the following be referred
20 to as a Partially External Dielectric (PED) transmission line probe.

The propagation velocity along the PED transmission line probe is characterized by an effective dielectric constant ϵ_{eff} which depends on the dielectric constant of the dielectric enclosing structure ϵ_{int} and the dielectric constant of the surrounding medium (air, steam, product vapor, probe
25 contamination etc) ϵ_{ext} . The propagation velocity of the electromagnetic signal travelling along the transmission line probe is given by the velocity of light divided by the square root of ϵ_{eff} .

The effective dielectric constant ϵ_{eff} of the PED transmission line probe depends on the dielectric constant of the dielectric enclosing structure ϵ_{int} and
30 the dielectric constant of the surrounding medium ϵ_{ext} according to the following relation:

$$\epsilon_{\text{eff}} \sim \frac{1}{\frac{\alpha}{\epsilon_{\text{ext}}} + \frac{1-\alpha}{\epsilon_{\text{int}}}}$$

where α is a number between 0 and 1 which indicates the degree of
35 coupling to the surrounding medium. With $\alpha=1$, we have naked wires (and

maximum influence of the surrounding medium) and with $\alpha = 0$ we have a line fully screened from the surrounding medium (such as a closed coaxial line).

Since ϵ_{eff} determines the propagation velocity along the transmission line probe, the transmission line probe may advantageously be configured
5 such that electromagnetic signals in different frequency ranges experience different values of α . For example, the transmission line probe may be configured such that α and ϵ_{int} are uniform along the transmission line probe, but the determination of the dielectric constant ϵ_{ext} of the surrounding medium will be possible as long as any variations of α and ϵ_{int} are known.

10 The thickness of the dielectric enclosing structure, in a radial direction in respect of the probe conductor, may be greater than one of 3 millimeters, 4 millimeters and 5 millimeters. This is the case for many suitable dielectric materials, such as PTFE. For a dielectric material having a higher dielectric constant, the dielectric enclosing structure could be made thinner.

15 According to various embodiments, the transmission line probe may have one probe conductor only. A single conductor transmission line probe may be beneficial for many applications. A single conductor transmission line probe is very simple and robust and can be used even for demanding applications, such as for measurements in hot steam under high pressure.

20 Furthermore, since no spacing structures etc. are needed as is typically the case for multiple conductor transmission line probes, a GWR system using a single conductor transmission line probe may be a particularly cost-efficient alternative. Moreover, a single conductor transmission line probe is relatively simple to feed with electromagnetic signals from the transceiver.

25 The single conductor may be rigid or flexible. In particular for a flexible single conductor transmission line probe, the probe conductor may comprise at least two twisted conducting wires being in electrically conductive contact with each other. Such conducting wires need, however, not be twisted, but the probe conductor may be provided as a stranded wire enclosed by a
30 polymeric jacket. In other words, the transmission line probe may comprise a probe core formed by a stranded wire and a polymeric jacket covering the probe core. In the case of a rigid transmission line probe, the transmission line probe may comprise a probe core formed by a metal pin and a polymeric jacket covering the probe core.

35 As an alternative (or in combination) the transmission line probe may comprise a perforated metal ribbon. The dielectric layer enclosing a PED-type transmission line probe effectively works as an inductive layer and may be

substituted by a metallic structure with similar function. For example, a perforated metal ribbon will exhibit similar signal propagation properties as a PED-type transmission line probe. To provide for a mechanically robust transmission line probe, the metal ribbon may have a curved cross-section, similar to a longitudinal segment of a pipe, for instance a half-pipe. The perforation may be in the form of elongated holes with such dimensions that the resonance frequency of the holes is close to the second frequency range. In this case, the surrounding medium (liquid or gas) will detune the holes and change the propagation properties of the metal ribbon.

By using a transmission line probe configured to propagate electromagnetic signals in different frequency ranges with different (and known) values of α , the unknown dielectric constant ϵ_{ext} of the surrounding medium can be determined, which means that the filling level can be determined accurately without prior knowledge of the dielectric constant of the surrounding medium in the tank.

According to various embodiments, furthermore, the transceiver of the guided wave radar level gauge system may advantageously comprise a first sub-transceiver for generating, transmitting and receiving electromagnetic signals in the first frequency range; and a second sub-transceiver for generating, transmitting and receiving electromagnetic signals in the second frequency range, wherein the first sub-transceiver and the second sub-transceiver are both connected to the transmission line probe.

According to a second aspect of the present invention, it is provided a method of determining a filling level of a product contained in a tank, comprising the steps of: propagating a first transmitted electromagnetic signal in a first frequency range and a second transmitted electromagnetic signal in a second frequency range different from the first frequency range along a transmission line probe towards a surface of the product in the tank; receiving a first reflected electromagnetic signal in the first frequency range resulting from reflection of the first transmitted electromagnetic signal at the surface and a second reflected electromagnetic signal in the second frequency range resulting from reflection of the second transmitted electromagnetic signal at the surface; and determining the filling level based on a time-of-flight of the first reflected electromagnetic signal and a difference in time-of-flight of the first reflected electromagnetic signal and the second reflected electromagnetic signal.

Further embodiments of, and effects obtained through this second aspect of the present invention are largely analogous to those described above for the first aspect of the invention.

5 Brief Description of the Drawings

These and other aspects of the present invention will now be described in more detail, with reference to the appended drawings showing example embodiments of the invention, wherein:

10 Fig 1a schematically illustrates a guided wave radar level gauge system according to an embodiment of the present invention installed in an exemplary tank;

Fig 1b is a schematic illustration of the measurement electronics unit comprised in the guided wave radar level gauge system in fig 1a;

15 Figs 2a-b schematically illustrate examples of pulsed signals in different frequency ranges;

Fig 3 schematically shows a first example of the transmission line probe in figs 1a-b;

Fig 4 schematically shows a second example of the transmission line probe in figs 1a-b;

20 Fig 5 is a diagram schematically illustrating the ratio between the propagation velocities for two different frequency ranges having different insulation factors α as a function of the dielectric constant of the surrounding medium; and

25 Fig 6 is a flow-chart schematically illustrating an example embodiment of the method according to the present invention.

Detailed Description of an Example Embodiment of the Invention

Fig 1a schematically illustrates a radar level gauge system 1 according to an embodiment of the present invention, comprising a measurement
30 electronics unit 2, and a transmission line probe 3. The radar level gauge system 1 is provided on a tank 5, which is partly filled with a product 6 to be gauged. By guiding a first transmitted electromagnetic signal S_{T1} in a first frequency range F_1 and a second transmitted electromagnetic signal S_{T2} in a second frequency range F_2 different from the first frequency range F_1 towards
35 the surface 7 of the product 6, and analyzing a first reflected signal S_{R1} in the first frequency range F_1 and a second reflected signal S_{R2} in the second frequency range F_2 traveling back from the surface 7 along the transmission

line probe 3, the measurement electronics unit 2 can determine the distance between a reference position (such as the tank ceiling) and the surface 7 of the product 6, whereby the filling level can be deduced even if the dielectric constant ϵ_{ext} of the medium 8 in the tank surrounding the transmission line probe 3 is unknown and/or varying. It should be noted that, although a tank 5 containing a single product 6 is discussed herein, the distance to any material interface along the transmission line probe 3 can be measured in a similar manner as long electromagnetic signals are reflected at the material interface and return to the measurement electronics unit 2.

As is schematically illustrated in fig 1b, the measurement electronics unit 2 comprises a first transceiver unit 10, a second transceiver unit 11, a processing unit 12, and a communication interface 13. The first transceiver unit 10 is configured to generate, transmit and receive electromagnetic signals in the above-mentioned first frequency range F_1 , and the second transceiver unit 11 is configured to generate, transmit and receive electromagnetic signals in the above-mentioned second frequency range F_2 . The processing unit 12 is connected to the first transceiver unit 10 and the second transceiver unit 11 for control of the transceiver units and processing of signals received by the transceivers to determine the filling level of the product 6 in the tank 5. The processing unit 12 is, furthermore, connectable to external communication lines 14 for analog and/or digital communication via the interface 13. Moreover, although not shown in fig 1b, the guided wave radar level gauge system 1 may be connectable to an external power source, may comprise a local energy store, such as a battery, or may be powered through the external communication lines 14. The radar level gauge system 1 may be configured to communicate wirelessly.

The first 10 and second 11 transceiver units may both be directly connected to the transmission line probe 3 along a common line as is schematically indicated in fig 1b, which will result in some loss of signal strength. Alternatively, the measurement electronics unit may comprise a diplexer or a switch to rout the electromagnetic signals from the first 10 and second 11 transceiver units to the probe. This latter solution, which is well-known to those skilled in the art will result in only negligible signal loss.

The GWR-system 1 in figs 1a-b may advantageously be a so-called pulsed system, in which an electromagnetic transmit signal in the form of a transmitted pulse train with a pulse repetition frequency are guide towards the surface 7 of the product 6 in the tank 5 along the transmission line probe 3.

Reflection of the electromagnetic transmit signal at the surface 7 results in a reflected pulse train with the same pulse repetition frequency as the transmitted pulse train, but with a delay corresponding to the time of flight from the transceiver to the surface and back. By determining the delay, which
 5 is usually done by well-known time expansion techniques, the filling level can be deduced.

As is schematically illustrated in figs 2a-b, at least one of the above mentioned first S_{T1} and second S_{T2} electromagnetic transmit signals may advantageously be provided as a pulse train formed by a modulated carrier
 10 signal.

Referring first to fig 2a, the first electromagnetic transmit signal S_{T1} may be provided as a first train of pulses 20a-c with a pulse repetition frequency given by a time t_{PRF} between successive pulses. As is schematically indicated in fig 2a, each pulse 20a-c is provided as a so-called
 15 DC-signal that is frequently used in so-called TDR-systems. The first center frequency f_{c1} is then about 0.5 GHz, and the first frequency range F_1 is about 0.1 GHz – 1 GHz.

Referring to fig 2b, the second electromagnetic transmit signal S_{T2} may be provided as a second train of pulses 22a-c with a pulse repetition
 20 frequency given by a time t_{PRF} between successive pulses. The pulse repetition frequency of the second electromagnetic transmit signal S_{T2} may be the same as the pulse repetition frequency of the first electromagnetic transmit signal S_{T1} or different. As is schematically indicated in fig 2b, each pulse 22a-c is provided as a modulated carrier signal having a second center
 25 frequency f_{c2} . The second center frequency f_{c2} may, for example, be 6 GHz, and the second frequency range F_2 may then be, for instance, 5.5 GHz – 6.5 GHz.

Although the first electromagnetic signal S_{T1} is shown as a pulse train of so-called DC-pulses in fig 2a, it should be understood that the first
 30 electromagnetic signal S_{T1} may equally well be a pulse train formed by a modulated carrier signal. In this case, the first center frequency f_{c1} may, for example, be about 1 GHz, and the first frequency range F_1 may then be 0.5 – 1.5 GHz.

Referring again briefly to fig 1, the transmission line probe 3 is
 35 configured to guide electromagnetic signals in the first frequency range F_1 with a first propagation velocity v_{prop1} exhibiting a first dependence on the dielectric constant ϵ_{ext} of the surrounding medium 8 and to guide

electromagnetic signals in the second frequency range F_2 with a second propagation velocity $v_{\text{prop}2}$ exhibiting a second dependence on the dielectric constant ϵ_{ext} of the surrounding medium 8.

To facilitate the analysis of received signals in the first F_1 and the
5 second F_2 frequency ranges, it may be desirable if the transmission line probe 3 is configured to allow coupling between the guided electromagnetic signal and the surrounding atmosphere 8 that is distinctly different for the first F_1 and the second F_2 frequency ranges.

Two examples of single conductor transmission line probes capable of
10 providing such distinctly different coupling will be described below with reference to fig 3 and fig 4.

Fig 3 schematically shows an example of the transmission line probe 3
in fig 1, comprising a single probe conductor, here in the form of a metal pin
25, and a dielectric enclosing structure provided in the form of a polymeric
15 jacket 26.

The metal pin 25 may, for example, be made of stainless steel.
However, many other metals are possible, such as copper, as the metal pin
25 is protected from the environment inside the tank 5 by the polymeric jacket
26. Moreover, the single probe conductor may equally well be flexible rather
20 than rigid, in which case the single probe conductor may advantageously be provided in the form of a stranded wire.

The polymeric jacket 26 may have different properties depending on
the intended field of application. Since it may be desirable to provide for
distinctly different coupling between the electromagnetic signals and the
25 surrounding medium (such as tank atmosphere 8), the polymeric jacket 26 may either be rather thick or have a rather high dielectric constant. The actual selection of material properties and dimensions of the polymeric jacket will be dependent on, for example, the properties of the material(s) in the tank 5. For instance, if the material(s) in the tank 5 are highly corrosive, it may be
30 necessary to select a very durable material for the polymeric jacket 26, such as PTFE (polytetrafluoroethylene). However, since PTFE has a rather low dielectric constant (about 2.1), it may be necessary to make the polymeric jacket rather thick, such as at least 5 mm. A jacket made of a material having a higher dielectric constant can be made thinner. An example of a material
35 with good chemical stability and a higher dielectric constant is PTFE mixed with a ceramic powder. PEEK (polyetheretherketone) is another durable polymer with a higher dielectric constant than PTFE.

Given the information and examples provided in the present application, it will be straight-forward for the skilled person to arrive at a suitable material combination of probe conductor 25 and polymeric jacket 26 for a particular application.

5 It should be noted that the transmission line probe 3 need not necessarily be provided in the form of an at least partially enclosed dielectric structure as long as the desired difference in propagation properties for the electromagnetic signals in different frequency ranges and the surrounding medium is achieved. For example, it may be possible to use a single
10 conductor probe of a "poor conductor" without any dielectric cover. For instance, the single conductor probe may be made of stainless steel or have an other layer of stainless steel or other metal having a low electrical conductivity.

Furthermore, the dielectric layer, such as the polymeric jacket 26 in fig
15 3, effectively works as an inductive layer and may be substituted by a metallic structure with similar function. Accordingly, it is expected that, for example a single probe conductor provided in the form of a twisted pair of conductive wires may exhibit similar properties as the example of the transmission line probe 3 described above with reference to fig 3.

20 Another example of the transmission line probe 3 in fig 1 will now be described with reference to fig 4.

According to the example schematically shown in fig 4, the transmission line probe 3 is provided in the form of a metal ribbon 28 that is perforated by elongated holes 29. Because of the holes, the metal ribbon 28,
25 here provided in the shape of a pipe segment, will exhibit similar properties as the partially enclosed dielectric structure described above with reference to fig 3. A suitable width of the ribbon may be about 20 mm and the length of the holes may roughly correspond to a half wavelength of the second frequency range (around 20-25 mm for a 6 GHz signal).

30 Through a suitable configuration of the transmission line probe 3, the first S_{T1} and second S_{T2} electromagnetic signals in different frequency ranges will have propagation velocities that depend on the dielectric constant of ϵ_{ext} the surrounding medium 8 according to different known relations. Based on the time-of-flight of one of the propagation modes, the difference in time-of-
35 flight of the propagations modes and the known different relations between the propagation velocities of the propagation modes and the dielectric constant of the surrounding medium 8, an accurate filling level value can be

determined without knowledge (or assumptions) about the dielectric constant ϵ_{eff} of the surrounding medium 8.

For a transmission line probe 3 such as that described above with reference to fig 3, the effective dielectric constant ϵ_{eff} of the transmission line probe 3 depends on the dielectric constant of the dielectric enclosing structure ϵ_{int} and the dielectric constant ϵ_{ext} of the surrounding medium 8 according to the following relation:

$$\epsilon_{\text{eff}} \sim \frac{1}{\frac{\alpha}{\epsilon_{\text{ext}}} + \frac{1-\alpha}{\epsilon_{\text{int}}}}$$

where α is a number between 0 and 1 which indicates the degree of coupling to the surrounding medium. Moreover, the propagation velocity is inversely proportional to the square root of the effective dielectric constant ϵ_{eff} .

In accordance with the discussion above in connection with fig 4, it should be understood that a completely metallic transmission line probe may be used, and that the effective dielectric constant ϵ_{ext} of such a transmission line probe will follow the same relation as a partially enclosed dielectric structure, with an "equivalent" dielectric constant ϵ_{int} .

To illustrate the resulting dependence of the propagation velocity on the dielectric constant ϵ_{ext} of the surrounding medium 8, a diagram with the ratio between the propagation velocities for two different frequency ranges having different insulation factors α as a function of the dielectric constant ϵ_{ext} of the surrounding medium 8 is provided in fig 5. For the exemplary case illustrated in fig 5, the insulation factor α_1 for the first frequency range F_1 (1 GHz) is 0.73, and the insulation factor α_2 for the second frequency range F_2 (6 GHz) is 0.41.

An example embodiment of the filling level determination method according to embodiments of the present invention will now be described with reference to the flow chart in fig 6 as well as to figs 1a-b.

In a first step 101, a first electromagnetic transmit signal S_{T1} in a first frequency range F_1 is transmitted along the transmission line probe 3 towards the surface 7 of the product 6 in the tank 5 and a first electromagnetic reflection signal S_{R1} is received.

In a second step 102, a second electromagnetic transmit signal S_{T2} in a second frequency range F_2 is transmitted along the transmission line probe

3 towards the surface 7 of the product 6 in the tank 5 and a second electromagnetic reflection signal S_{R2} is received.

The transmission line probe is configured to fulfil the following two conditions:

5

-The electromagnetic signals in the first frequency range F_1 and the second frequency range F_2 travel along the transmission line probe 3 with first v_{prop1} and second v_{prop2} propagation velocities that exhibit different dependencies on the dielectric constant ϵ_{ext} of the surrounding medium 8 (different α).

10

- The electromagnetic signals in the first frequency range F_1 and the second frequency range F_2 exhibit sufficient coupling to the dielectric constant ϵ_{ext} of the surrounding medium 8 to be reflected at the surface 7 of the product 6 (sufficiently large α).

15

Two different examples of transmission line probes that fulfill the above conditions for suitably selected frequency ranges have been described above with reference to fig 3 and fig 4.

20

In a third step 103, the time-of-flight (or a value indicative of the time-of-flight) T_1 for the first frequency range F_1 and the time-of-flight T_2 for the second frequency range F_2 are determined.

Subsequently, in step 104, the dielectric constant ϵ_{ext} of the surrounding medium 8 is determined using the time-of-flight values T_1 , T_2 determined in step 103 and the known relation between the time-of-flight and the dielectric constant ϵ_{ext} of the surrounding medium 8 for the two frequency ranges:

25

$$\epsilon_{eff} \sim \frac{1}{\frac{\alpha}{\epsilon_{ext}} + \frac{1-\alpha}{\epsilon_{int}}}$$

30

Since the propagation velocity v_{prop} is determined by the following relation:

$$v_{prop} = \frac{v_0}{\sqrt{\epsilon_{eff}}},$$

where v_0 is the propagation velocity of electromagnetic signals along the probe in vacuum, the time-of-flight is proportional to $\sqrt{\epsilon_{eff}}$.

Once the dielectric constant ϵ_{ext} of the surrounding medium 8 has been determined, the effective dielectric constant ϵ_{eff} can be determined, after
5 which a DC-corrected (dielectric constant corrected) distance to the surface 7 of the product 6 is determined in step 105.

In order to use the method according to various embodiments of the present invention, the relationship between the propagation velocity (or time-of-flight) and the dielectric constant ϵ_{ext} of the surrounding medium 8 should
10 be known. This relationship can, for example, be determined by simulations based on the configuration of the transmission line probe 3 (materials, dimensions etc) and/or measurements, and may be embodied as a mathematical formula or as a lookup table, or a combination of those. Such simulations and/or measurements will be well within the reach of those skilled
15 in the art to carry out without undue burden.

The person skilled in the art realizes that the present invention by no means is limited to the preferred embodiments described above. For example
may other probe configurations than those described above with reference to fig 3 and fig 4 can be used, as long as they provide for a frequency
20 dependent interaction with the surrounding medium. For instance, the dielectrically enclosed probe of fig 3 may be only partly enclosed, and the metal ribbon in fig 4 may be flat and/or have different hole configurations. Furthermore, similar propagation properties can be achieved with a metal ribbon that is not perforated, but has periodically varying widths along the
25 length of the probe.

What is claimed is:

1. A guided wave radar level gauge system, for determination of a filling level
5 of a product contained in a tank, said guided wave radar level gauge system comprising:
a transceiver for generating, transmitting and receiving electromagnetic signals in a first frequency range and in a second frequency range different from said first frequency range;
10 a transmission line probe connected to said transceiver, and arranged and configured to guide transmitted electromagnetic signals from said transceiver through a surrounding medium towards said product inside the tank, and to return reflected electromagnetic signals resulting from reflection of said transmitted electromagnetic signals by a surface of said product back
15 towards said transceiver,
the transmission line probe being configured to guide electromagnetic signals in said first frequency range with a first propagation velocity exhibiting a first dependence on a dielectric constant of the surrounding medium, and guide electromagnetic signals in said second frequency range with a second
20 propagation velocity exhibiting a second dependence, different from the first dependence, on said dielectric constant of the surrounding medium; and
processing circuitry connected to the transceiver for determining the filling level based on a first reflected electromagnetic signal in said first frequency range, a second reflected electromagnetic signal in said second
25 frequency range, and a known relation between said first dependence and said second dependence on said dielectric constant of the surrounding medium.
2. The guided wave radar level gauge system according to claim 1,
30 wherein said first frequency range has a first center frequency and said second frequency range has a second center frequency, said second center frequency being higher than one of two times, three times and five times said first center frequency.
3. The guided wave radar level gauge system according to claim 2,
35 wherein said second center frequency is higher than one of 3 GHz, 4 GHz and 6 GHz.

4. The guided wave radar level gauge system according to any one of claims 1 to 4, wherein said transmission line probe comprises a probe conductor and a dielectric enclosing structure at least partly enclosing said probe conductor.

5. The guided wave radar level gauge system according to claim 4, wherein said dielectric enclosing structure fully encloses substantially all of a portion of said probe conductor being arranged inside said tank.

10

6. The guided wave radar level gauge system according to claim 4 or 5, wherein a material thickness of said dielectric enclosing structure, in a radial direction in respect of said probe conductor, is at least 5 millimeters.

7. The guided wave radar level gauge system according to any one of claims 1 to 6, wherein said transmission line probe has one probe conductor only.

8. The guided wave radar level gauge system according to claim 7, wherein said probe conductor comprises at least two twisted conducting wires being in electrically conductive contact with each other.

9. The guided wave radar level gauge system according to any one of claims 1 to 8, wherein said transceiver comprises:

a first sub-transceiver for generating, transmitting and receiving electromagnetic signals in said first frequency range; and

a second sub-transceiver for generating, transmitting and receiving electromagnetic signals in said second frequency range,

wherein said first sub-transceiver and said second sub-transceiver are both connected to said transmission line probe.

10. The guided wave radar level gauge system according to any one of claims 1 to 9, wherein said transmission line probe comprises a probe core formed by a stranded wire and a polymeric jacket covering said probe core.

35

11. The guided wave radar level gauge system according to any one of claims 1 to 10, wherein said transmission line probe comprises a probe core formed by a metal pin and a polymeric jacket covering said probe core.

5 12. A method of determining a filling level of a product contained in a tank, comprising the steps of:

 propagating a first transmitted electromagnetic signal in a first frequency range and a second transmitted electromagnetic signal in a second frequency range different from said first frequency range along a transmission
10 line probe towards a surface of the product in the tank;

 receiving a first reflected electromagnetic signal in said first frequency range resulting from reflection of said first transmitted electromagnetic signal at said surface and a second reflected electromagnetic signal in said second frequency range resulting from reflection of said second transmitted
15 electromagnetic signal at said surface; and

 determining said filling level based on a time-of-flight of said first reflected electromagnetic signal and a difference in time-of-flight of said first reflected electromagnetic signal and said second reflected electromagnetic
20 signal.

25 13. The method according to claim 12, wherein said first frequency range has a first center frequency and said second frequency range has a second center frequency, said second center frequency being higher than one of two times, three times and five times said first center frequency.

30 14. The method according to claim 13, wherein said second center frequency is higher than one of 3 GHz, 4 GHz and 6 GHz.

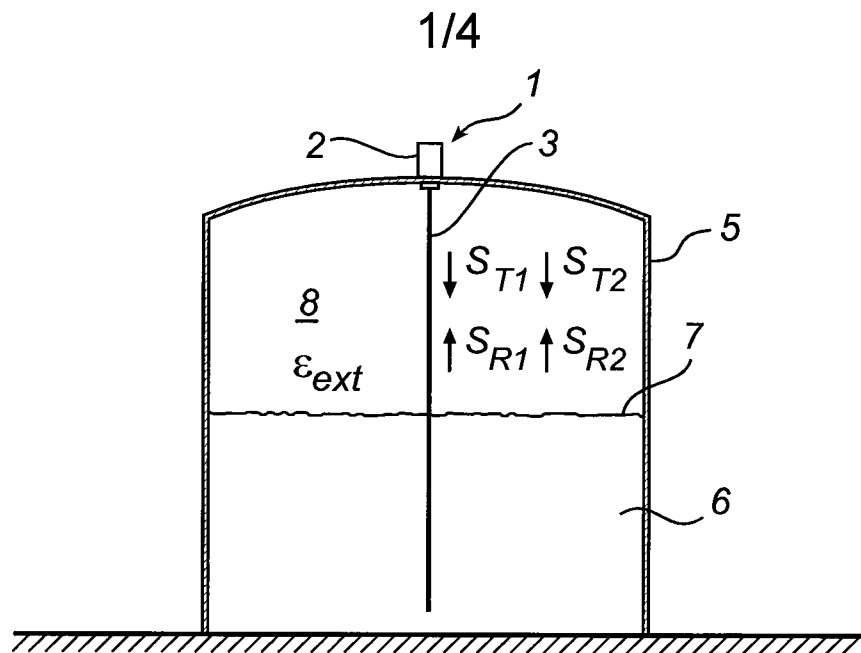


Fig. 1a

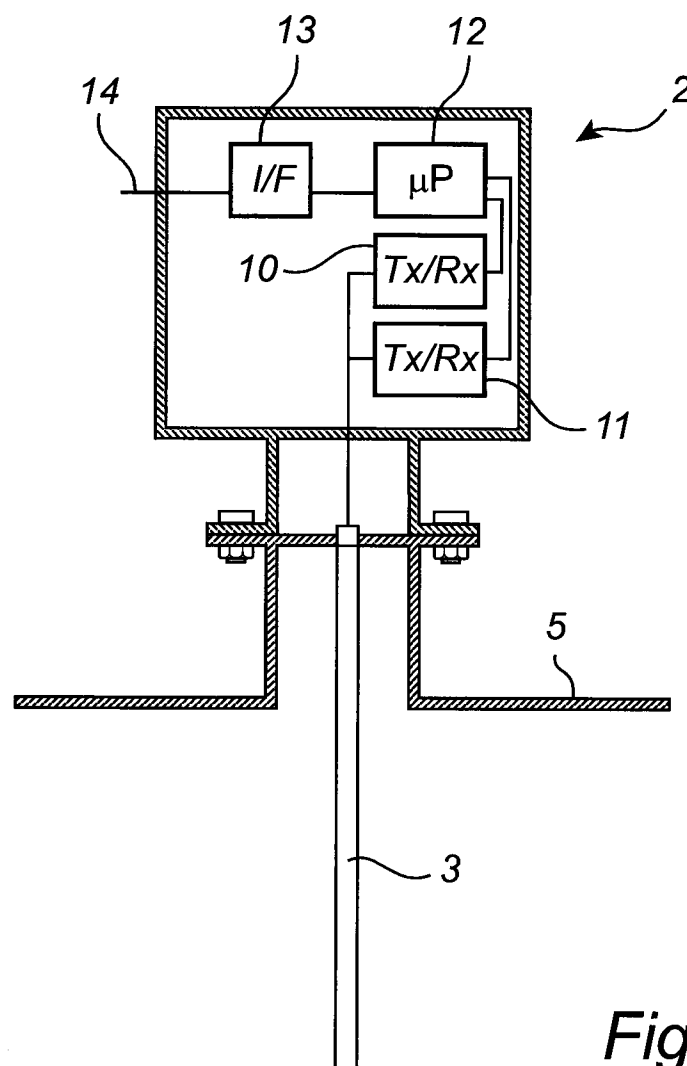
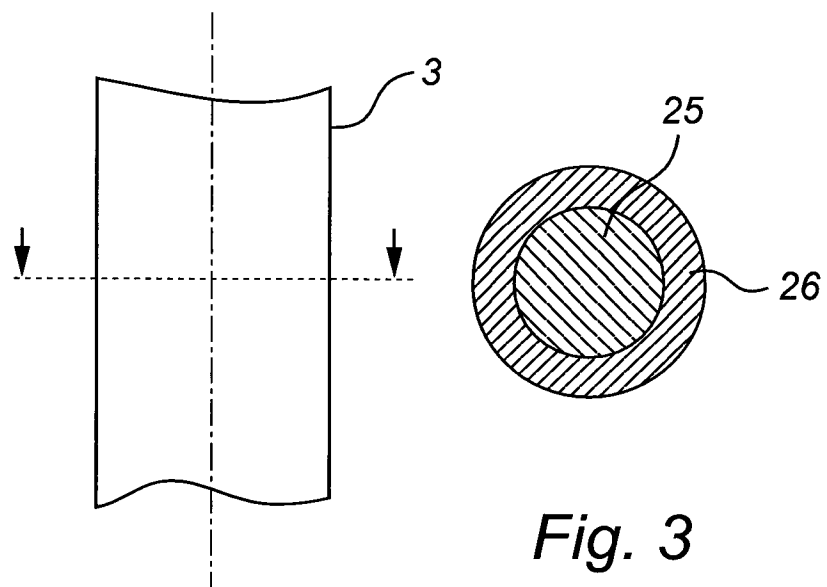
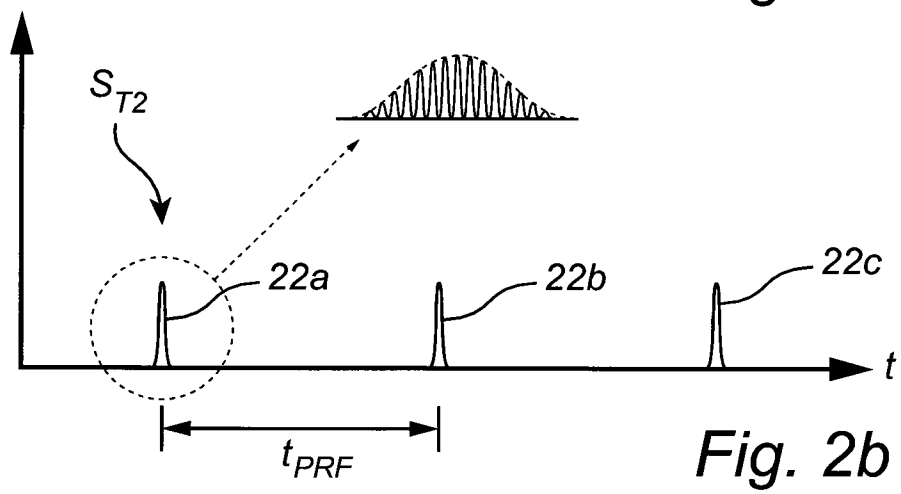
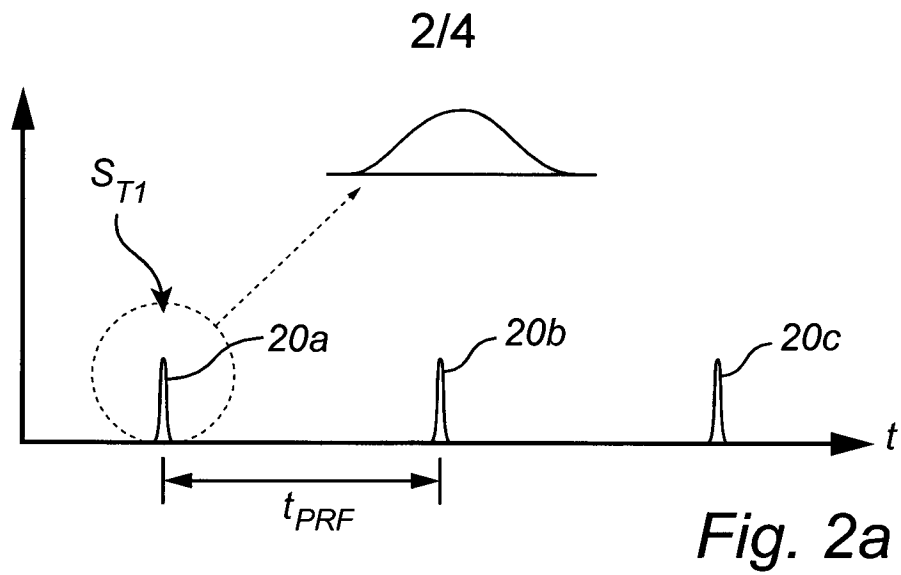
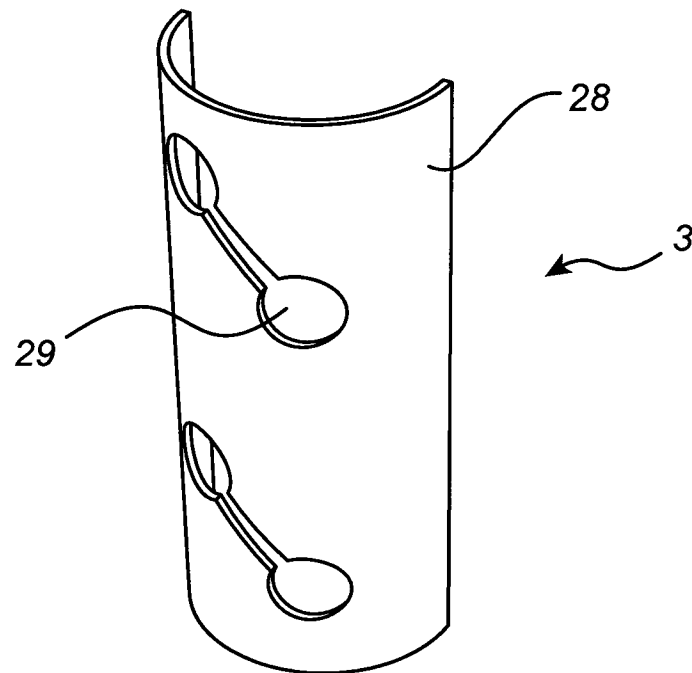
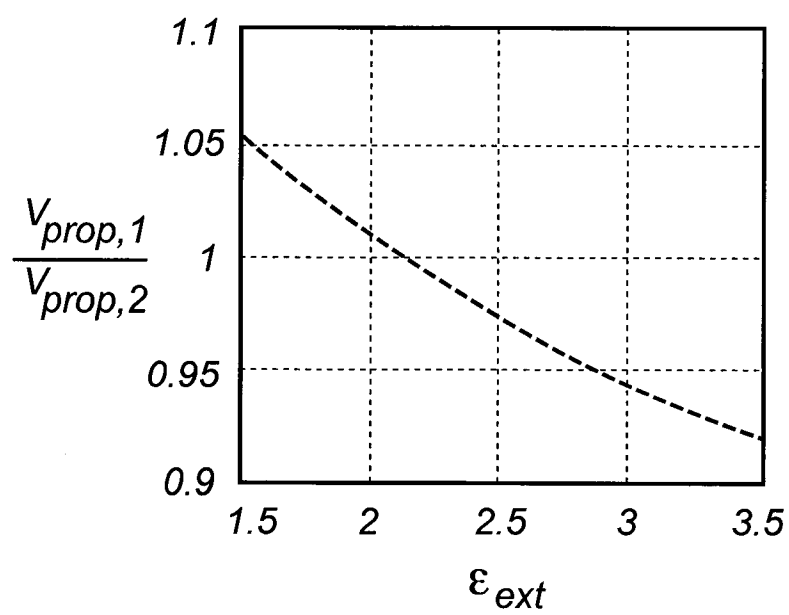


Fig. 1b



3/4

*Fig. 4**Fig. 5*

4/4

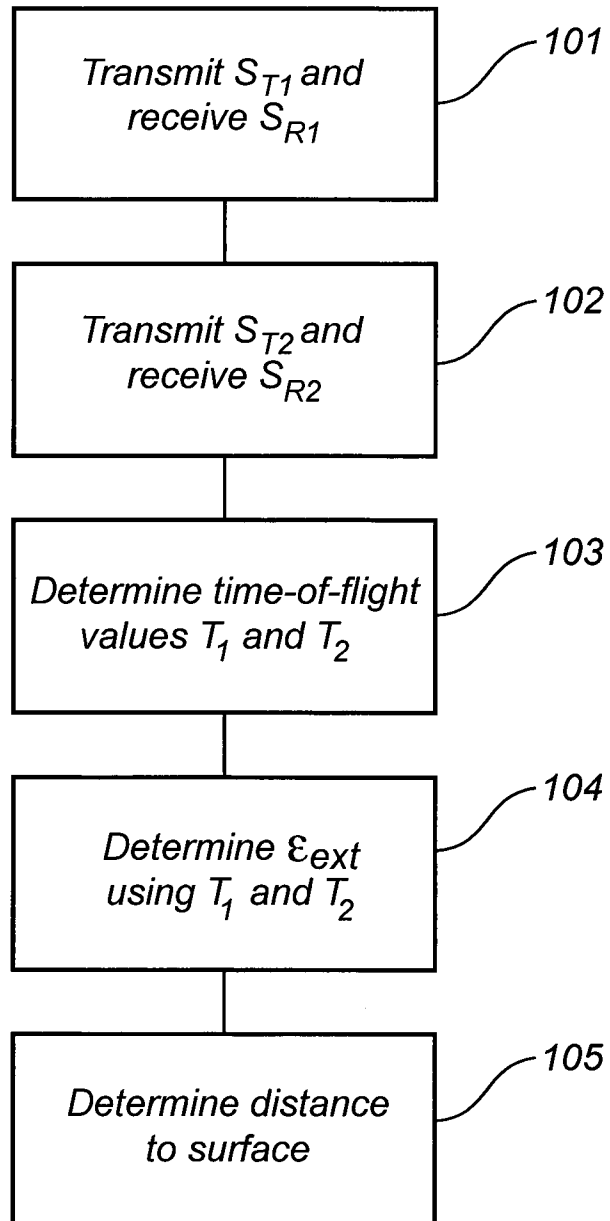


Fig. 6

INTERNATIONAL SEARCH REPORT

International application No.
PCT/SE2013/000138

A. CLASSIFICATION OF SUBJECT MATTER

IPC: see extra sheet

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC: G01F, G01S

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE, DK, FI, NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, PAJ, WPI data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 20040080324 A1 (WESTERLING JAN ET AL), 29 April 2004 (2004-04-29); abstract --	1-14
A	EP 2166321 A2 (ENRAF B V), 24 March 2010 (2010-03-24); abstract; figure 1 --	1-14
A	US 7525476 B1 (DELIN HAKAN ET AL), 28 April 2009 (2009-04-28); abstract; cited in the description --	1-14
P, A	WO 2012159682 A1 (ROSEMOUNT TANK RADAR AB ET AL), 29 November 2012 (2012-11-29); abstract; figure 4 -- -----	1-14

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents:

“A” document defining the general state of the art which is not considered to be of particular relevance

“E” earlier application or patent but published on or after the international filing date

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“O” document referring to an oral disclosure, use, exhibition or other means

“P” document published prior to the international filing date but later than the priority date claimed

“T” later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

“X” document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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“&” document member of the same patent family

Date of the actual completion of the international search

24-02-2014

Date of mailing of the international search report

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Continuation of: second sheet**International Patent Classification (IPC)*****G01F 23/284*** (2006.01)***G01S 13/08*** (2006.01)

INTERNATIONAL SEARCH REPORT

Information on patent family members

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