



- (51) International Patent Classification:  
*H01H 1/00* (2006.01)     *H01H 59/00* (2006.01)
- (21) International Application Number:  
PCT/US2013/056316
- (22) International Filing Date:  
23 August 2013 (23.08.2013)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data:  
13/592,435     23 August 2012 (23.08.2012)     US
- (71) Applicant: HARRIS CORPORATION [US/US]; 1025 W. Nasa Blvd., M/S A-11I, Melbourne, Florida 32901 (US).
- (72) Inventors: ROGERS, John E.; 6280 73rd Street, Vero Beach, Florida 32967 (US). WEATHERSPOON, Michael R.; 2108 Maeve Circle, West Melbourne, Florida 32904 (US).

- (74) Agents: EVANDER, G. Mitchell et al.; Harris Corporation, 1025 W. Nasa Blvd., M/S A-11I, Melbourne, Florida 32919 (US).
- (81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.
- (84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM,

[Continued on next page]

(54) Title: SWITCHES FOR USE IN MICROELECTROMECHANICAL AND OTHER SYSTEMS, AND PROCESSES FOR MAKING SAME

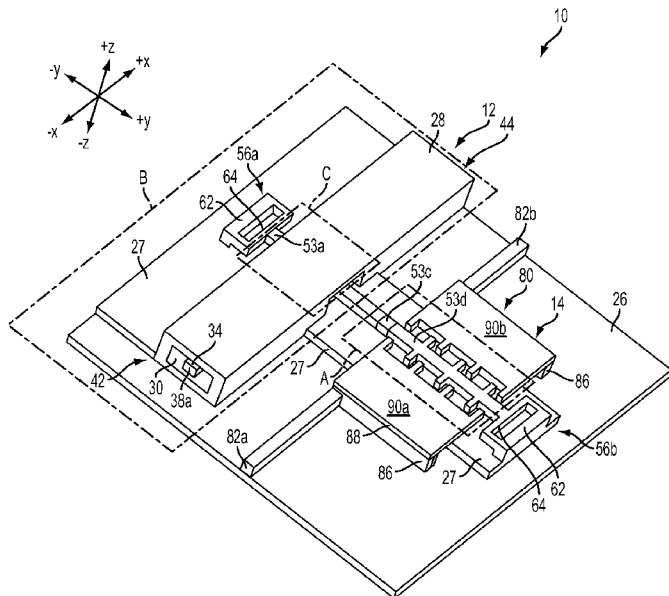


FIG. 1

(57) Abstract: Embodiments of switches (10) include first and second electrical conductors (34, 36) suspended within an electrically-conductive housing (28), and a contact element (16) having an electrically-conductive portion (53b) that establishes electrical contact between the first and second electrical conductors (34, 36) when the contact element (16) is in a closed position. The electrically-conductive portion (53b) is electrically isolated from a ground plane (27) of the switch (10) by adjacent electrically-insulative portions (53a, 53c) of the contact element (16).



TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG). **Published:**

— with international search report (Art. 21(3))

**SWITCHES FOR USE IN MICROELECTROMECHANICAL AND OTHER SYSTEMS,  
AND PROCESSES FOR MAKING SAME**

**BACKGROUND OF THE INVENTION**

5 **Statement of the Technical Field**

The inventive arrangements relate to switches, such as broad-band, low-loss radio frequency (RF) microelectromechanical systems (MEMS) switches.

**Description of Related Art**

10 Communications systems, such as broadband satellite communications systems, commonly operate at anywhere from 300MHz (UHF band) to 300GHz (mm-wave band). Such examples include TV broadcasting (UHF band), land mobile (UHF band), global positioning systems (GPS) (UHF band), meteorological (C band), and satellite TV (SHF band). Most of these bands are open to mobile and fixed satellite communications. Higher frequency bands typically come with larger bandwidths, which yield higher data rate operation. Switching  
15 devices used in these types of systems need to operate with relatively low losses, e.g., less than one decibel (dB) of insertion loss, at these ultra-high frequencies.

Miniaturized switches such as monolithic microwave integrated circuit (MMIC) and MEMS switches are commonly used in broadband communications systems due to stringent  
20 constraints imposed on the components of such systems, particularly in satellite-based applications. Currently, the best in class switches operate at 40 GHz with cumulative attributes such as insertion losses of approximately 0.6 dB, return losses of approximately 13 dB, and isolation levels of approximately 40 dB.

Three-dimensional microstructures can be formed by utilizing sequential build processes. For example, U.S. Patent Nos. 7,012,489 and 7,898,356 describe methods for  
25 fabricating coaxial waveguide microstructures. These processes provide an alternative to traditional thin film technology, but also present new design challenges pertaining to their effective utilization for advantageous implementation of various devices such as miniaturized switches.

**SUMMARY OF THE INVENTION**

30 Embodiments of switches include a ground housing; a first electrical conductor, and a second electrical conductor spaced apart from the first electrical conductor. The first and second

electrical conductors are suspended within the ground housing on electrically-insulative supports. The switches further include a contact element having an electrically-insulative first portion, an electrically-conductive second portion, and an electrically-insulative third portion. The first and third portions of the contact element adjoin the second portion. The contact element is configured for movement between a first position at which the second portion of the contact element is spaced apart and electrically isolated from the first and second electrical conductors, and a second position at which the second portion of the contact element contacts the first and second electrical conductors.

Other embodiments of switches include a ground plane, and a housing electrically connected to the ground plane and having one or more inner surfaces that define a channel. The switches also include a first and a second electrical conductor suspended within the channel, spaced apart from the one or more inner surfaces of the housing by a first air gap, and spaced apart from each other by a second air gap. The switches further include a contact element mounted on the ground plane and being operative to move between a first position at which an electrically-conductive portion of the contact element is spaced part and electrically isolated from the first and second electrical conductors by respective third and fourth air gaps, and a second position at which the electrically-conductive portion of the contact element contacts the first and second electrical conductors and bridges the second air gap to establish electric contact between the first and second electrical conductors. The contact element further includes a first electrically insulative portion configured to electrically isolate the electrically-conductive portion of the contact element from the ground plane.

In accordance with further aspects of the inventive concepts claimed herein, processes for making switches include selectively depositing a first layer of an electrically-conductive material on a substrate to form at least a portion of a ground plane and an actuator. The processes further include selectively depositing a second layer of the electrically-conductive material on the first layer and the substrate to form or further form the actuator, a portion of a housing, and a portion of a mount for a contact element configured to electrically connect a first and a second electrical conductor on a selective basis when actuated by the actuator. The processes also include selectively depositing a portion of a third layer of the electrically-conductive material on the first and second layers and the substrate to form or further form the

housing, the actuator, the mount, the contact element, and the first and second electrical conductors.

### BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments will be described with reference to the following drawing figures, in which like numerals represent like items throughout the figures and in which:

FIG. 1 is a top perspective view of a MEMS switch, depicting a shuttle of the switch in an open position;

FIG. 2 is a top perspective view of a ground housing, and a portion of a ground plane the switch shown in FIG. 1, with a top layer of the housing removed for clarity of illustration;

FIG. 3 is a magnified view of the area designated "C" in FIG. 1, depicting the housing and shuttle as transparent;

FIG. 4 front view of the switch shown FIGS. 1-3, depicting the shuttle in the open position and showing the layered structure of the switch, and with relief added to better denote the illustrated structure;

FIG. 5A is a top, magnified view of the area designated "A" in FIG. 1, depicting the shuttle in the open position;

FIG. 5B is a top, magnified view of the area designated "A" in FIG. 1, depicting the shuttle in a closed position;

FIG. 6A is a top view of the area designated "B" in FIG. 1, depicting a ground housing of the switch in phantom, and depicting the shuttle in the open position;

FIG. 6B is a top view of the area designated "B" in FIG. 1, depicting a ground housing of the switch in phantom, and depicting the shuttle in the closed position;

FIGS. 7A, 8A, 9A . . . 17A are cross-sectional views, taken through the line "E-E" of FIG. 1, depicting portions the switch shown in FIGS. 1-6B during various stages of manufacture; and

FIGS. 7B, 8B, 9B . . . 17B are cross-sectional views, taken through the line "D-D" of FIG. 1, depicting portions the switch shown in FIGS. 1-6B during various stages of manufacture.

### DETAILED DESCRIPTION

The invention is described with reference to the attached figures. The figures are not drawn to scale and they are provided merely to illustrate the instant invention. Several aspects of the invention are described below with reference to example applications for illustration. It

should be understood that numerous specific details, relationships, and methods are set forth to provide a full understanding of the invention. One having ordinary skill in the relevant art, however, will readily recognize that the invention can be practiced without one or more of the specific details or with other methods. In other instances, well-known structures or operation are not shown in detail to avoid obscuring the invention. The invention is not limited by the  
5 illustrated ordering of acts or events, as some acts may occur in different orders and/or concurrently with other acts or events. Furthermore, not all illustrated acts or events are required to implement a methodology in accordance with the invention.

The figures depict a MEMS switch 10. The switch 10 can selectively establish and  
10 disestablish electrical contact between a first and second electronic component (not shown) electrically connected thereto. The switch 10 has a maximum height (“z” dimension) of approximately 1 mm; a maximum width (“y” dimension) of approximately 3 mm; and a maximum length (“x” dimension) of approximately 3 mm. The switch 10 is described as a MEMS switch having these particular dimensions for exemplary purposes only. Alternative  
15 embodiments of the switch 10 can be scaled up or down in accordance with the requirements of a particular application, including size, weight, and power (SWaP) requirements.

The switch 10 comprises a contact portion 12, an actuator portion 14, and a contact element in the form of a shuttle 16, as shown in FIG. 1. The first and second electronic components are electrically connected to opposite ends of the contact portion 12, and are  
20 electrically connected to each other on a selective basis via the contact portion 12. As discussed below, the shuttle 16 moves in the “y” direction between an open and a closed position, in response to energization and de-energization of the actuator portion 14. The shuttle 16 facilitates the flow of electric current through the contact portion 12 when the shuttle 16 is in its closed position, thereby establishing electrical contact between the first and second electronic  
25 components. Current does not flow through the contact portion 12 when the shuttle 16 is in its open position. Thus, the first and second electronic components are electrically isolated from each other when the shuttle 16 is in its open position.

The switch 10 comprises a substrate 26 formed from a dielectric material such as silicon (Si), as shown in FIGS. 1 and 4. The substrate 26 can be formed from other materials,  
30 such as glass, silicon-germanium (SiGe), or gallium arsenide (GaAs) in alternative embodiments. The switch 10 also includes a ground plane 27 disposed on the substrate 26. The switch 10 is

formed from five layers of an electrically-conductive material such as copper (Cu). Each layer can have a thickness of, for example, approximately 50  $\mu\text{m}$ . The ground plane 27 is part of a first or lowermost layer of the electrically-conductive material. The number of layers of the electrically-conductive material is applicant-dependent, and can vary with factors such as the complexity of the design, hybrid or monolithic integration of other devices with the switch 10, the overall height (“z” dimension) of the switch 10, the thickness of each layer, etc.

The contact portion 12 of the switch 10 includes an electrically-conductive ground housing 28 disposed on the ground plane 27, as illustrated in FIGS. 1 and 4. The ground housing 28 is formed from portions of the second through fifth layers of the electrically-conductive material. The ground housing 28 and the underlying portion of the ground plane 27 define an internal channel 30 that extends substantially in the “x” direction, as depicted in FIGS. 1-4, 6A, and 6B.

The contact portion 12 further includes an electrically-conductive first inner conductor 34 and an electrically-conductive second inner conductor 36 each having a substantially rectangular cross section, as shown in FIGS. 1-4, 6A, and 6B. The first and second inner conductors 34, 36 can each be formed as part of the third layer of the electrically-conductive material.

The first and second inner conductors 34, 36 are positioned within the channel 30, as shown in FIGS. 1-4, 6A, and 6B. A first end 38a of the first inner conductor 34 is positioned at a first end of the channel 30. A first end 40a of the second inner conductor 36 is positioned at a second end of the channel 30. A second end 38b of the first inner conductor 34 is spaced apart from a second end 40b of the second inner conductor 36 by an air gap 44, and as discussed below, by a portion of the shuttle 16 positioned within the air gap 44.

The first inner conductor 34 and the surrounding portion of the ground housing 28 define an input port 42 of the contact portion 12. The second inner conductor 36 and the surrounding portion of the ground housing 28 define an output port 44 of the contact portion 12. The first electronic device can be electrically connected to the input port 42. The second electronic device can be electrically connected to the output port 44. The first and second electronic devices can be integrated with the respective input and output ports 42, 44 by, for example, hybrid integration methods such as wire-bonding and flip-chip bonding.

The first and second inner conductors 34, 36 are each suspended within the channel 34 on electrically-insulative tabs 37, as illustrated in FIGS. 2, 3, 6A and 6B. The tabs 37 are formed from a dielectric material. For example, the tabs 37 can be formed from polyethylene, polyester, polycarbonate, cellulose acetate, polypropylene, polyvinyl chloride, polyvinylidene chloride, polystyrene, polyamide, polyimide, benzocyclobutene, SU8, etc., provided the material will not be attacked by the solvent used to dissolve the sacrificial resist during manufacture of the switch 10 as discussed below. The tabs 37 can each have a thickness of, for example, approximately 15  $\mu\text{m}$ . Each tab 37 spans the width, i.e., y-direction dimension, of the channel 30. The ends of each tab 37 are sandwiched between the portions of the second and third layers of electrically-conductive material that form the sides of the ground housing 28. The first and second inner conductors 34, 36 are surrounded by, and are spaced apart from the interior surfaces of the ground housing 28 by an air gap 50. The air gap 50 acts as a dielectric that electrically isolates the first and second inner conductors 34, 36 from the ground housing 28. The type of transmission-line configuration is commonly referred to as a "recta-coax" configuration, otherwise known as micro-coax.

The shuttle 16 has an elongated body 52 that extends substantially in the "y" direction, as shown in FIGS. 1-6B. The body 52 includes an electrically-insulative first portion 53a, and an adjoining, electrically-conductive second portion 53b. The body 52 also includes an electrically-insulative third portion 53c that adjoins the second portion 53b, and an electrically-conductive fourth portion 53d that adjoins the third portion 53c. The electrically-conductive second and fourth portions 53b, 53d of the body 52 are formed as part of the third layer of the electrically-conductive material. The electrically-insulative first and third portions 53a, 53c are formed from a dielectric material such as polyethylene, polyester, polycarbonate, cellulose acetate, polypropylene, polyvinyl chloride, polyvinylidene chloride, polystyrene, polyamide, polyimide, benzocyclobutene, SU8, etc., provided the material will not be attacked by the solvent used to dissolve the sacrificial resist during manufacture of the switch 10 as discussed below.

The switch 10 includes a first mount 56a and a substantially identical second mount 56b. The first mount 56a is disposed on the portion of the ground plane 27 associated with the contact portion 12 of the switch 10, as shown in FIGS. 1, 6A, and 6B. The second mount 56b is disposed on the portion of the ground plane 27 associated with the actuator portion 14 of the switch 10, as illustrated in FIGS. 1, 5A, and 5B.

The first and second mounts 56a, 56b each include a base 62 that adjoins the ground plane 27, and a beam portion 64 that adjoins the base 62. Each base 62 is formed as part of the second and third layers of the electrically-conductive material. The beam portions 64 are formed as part of the third layer of the electrically-conductive material. It should be noted that the configuration of the beam portions 64 is application-dependent, and can vary with factors such as the amount of space available to accommodate the beam portions 64, the required or desired spring constant of the beam portions 64, etc. Accordingly, the configuration of the beam portions 64 is not limited to that depicted in FIG. 1.

An end of the first portion 53a of the shuttle 16 adjoins the beam portion 64 of the first mount 56a, as depicted in FIGS. 1, 6A, and 6B. An end of the fourth portion 53d of the shuttle 16 adjoins the beam portion 64 of the second mount 56b, as illustrated in FIGS. 1, 5A, and 5B. The shuttle 16 is thus suspended from, and fully supported by the first and second mounts 56a, 56b by virtue of the mechanical connection between the first portion 53a of the shuttle 16 and the beam portion 64 of the first mount 56a; and the mechanical connection between the fourth portion 53d of the shuttle 16 and the beam portion 64 of the second mount 56b.

The beam portions 64 are configured to deflect so as to facilitate movement of the shuttle 16 in its lengthwise direction, i.e., in the “y” direction. In particular, the shuttle 16 is in its open position when the beam portions 64 are in their neutral, or un-deflected positions, as depicted in FIGS 1, 3, 5A, and 6A. The beam portions 64 deflect when the shuttle 16 is urged in the “+y” direction, toward its closed position, due to electrostatic forces developed in the actuator portion 14 as discussed below. The beam portions 64 are shown in their deflected state in FIGS. 5B and 6B.

The second portion 53b of the shuttle 16 includes two projections in the form of fingers 74, as shown in FIGs. 3, 6A and 6B. The fingers 74 are located on opposite sides of the second portion 53b, and extend substantially perpendicular to the lengthwise direction of the body 52, i.e., in the “+/- x” directions. The shuttle 16 is configured so that one of the fingers 74 faces, and is spaced apart from the first inner conductor 34 by an air gap 76 when the shuttle 16 is in its open position. The other finger 74 faces, and is spaced apart from the second inner conductor 36 by another air gap 76 when the shuttle 16 is in its open position. The air within the

air gaps 76 acts as a dielectric insulator that electrically isolates the fingers 74 from the first and second inner conductors 34, 36 when the shuttle 16 is in its open position.

Movement of the shuttle 16 to its closed position causes each of the fingers 74 to traverse and close the associated air gap 76 as the finger 74 moves into contact with its associated first or second inner conductor 34, 36 as shown in FIG. 6B. The electrically-conductive fingers 74 and the adjoining second portion 53b of the body 52 thus bridge the air gaps 76 when the fingers 74 are in contact with the first and second inner conductors 34, 36, thereby establishing electrical contact between the first and second inner conductors 34, 36.

The air gaps 44, 76 act as a dielectric insulator that electrically isolates the first inner conductor 34 from the second inner conductor 38 when the shuttle 16 is in its open position. As shown in FIG. 6A, although the second portion 53b of the shuttle 16 extends through the air gap 44 between the second ends 38b, 40b of the first and second inner conductors 34, 36, the second portion 53b does not contact either of the second ends 38b, 40b. Thus, current is not transmitted between the first and second inner conductors 34, 36 via the second portion 53b when the shuttle 16 is in its open position.

By bridging the air gaps 76 when the shuttle 16 is in the closed position, as shown in FIG. 6B, the shuttle 16 electrically connects the first and second inner conductors 34, 36, thereby closing the switch 10 so that electric current can flow there through via a signal path formed by the first and second inner conductors 34, 36 and the second portion 53b of the shuttle 16.

The second portion 53b of the body 52 adjoins the electrically-insulative first and third portions 53a, 53c of the body 52, as depicted in FIGS. 1 and 3-6B. The first portion 53a electrically isolates the second portion 53b from the electrically-conductive first mount 56a. The third portion 53c electrically isolates the second portion 53b from the electrically-conductive fourth portion 53d. Thus, electrical isolation of the signal path through the switch 10 is achieved by way of the air gaps 50 between the first and second inner conductors 34, 36 and the adjacent internal surfaces of the ground housing 28; and by way of the first and third portions 53a, 53c of the shuttle 16.

The actuator portion 14 of the switch 10 includes a body 80, a first lead 82a, and a second lead 82b, as shown in FIGS. 1 and 4. The body 80 includes two legs 86, and an adjoining top portion 88. The legs 86 are formed as part of the first and second layers of the electrically-conductive material. The top portion 88 is formed as part of the third layer of the electrically-

conductive material. The legs 86 are disposed on the substrate 26, on opposite sides of the ground plane 27 as shown in FIG. 1. The body 80 thus straddles the ground plane 27, and is not in mechanical or electrical contact with the ground plane 27.

5 The top portion 88 of the body 80 includes a first half 90a and a second half 90b, as depicted in FIGS. 1, 5A, and 5B. The first half 90a is associated with one of the legs 86, and the second half 90b is associated with the other leg 86 as shown in FIG. 1. The first and second halves 90a, 90b are positioned on opposite sides of the fourth portion 53d of the shuttle 16. The first and second halves 90a, 90b each include three projections in the form of fingers 92 that extend substantially in the “x” direction. The optimal number of fingers 92 is application-  
10 dependent, and can vary with factors such as the amount of force that is needed to move the shuttle 16 to its closed position.

The fourth portion 53d of the body 52 of the shuttle 16 includes six projections in the form of fingers 96 that extend substantially in the “x” direction as illustrated in FIGS. 1, 5A, and 5B. Three of the fingers 96 are disposed on a first side of the fourth portion 53d, and the other  
15 three fingers 96 are disposed on the other side of the fourth portion 53d. The fourth portion 53d and the first and second halves 90a, 90b of the body 80 are configured so that the fingers 92 and the fingers 96 are interleaved or interdigitated, i.e., the fingers 92, 96 are arranged in an alternating fashion along the “y” direction. Moreover, each of the fingers 96 is positioned proximate and associated one of the fingers 92 as depicted in FIG. 5A, and is separated from the  
20 associated finger 92 by a gap of, for example, approximately 50  $\mu\text{m}$  when the shuttle 16 is in its open position.

The first and second leads 82a, 82b of the actuating portion 14 are disposed on the substrate 26 as shown in FIG. 1, and are formed as part of the first layer of the electrically  
25 conductive material. The first lead 82a adjoins the leg 86 associated with the first half 90a of the top portion 88 of the body 80. The second lead 82b adjoins the leg 86 associated with the second half 90b of the top portion 88. The first and second leads 82a, 82b can be electrically connected to a voltage source, such as a 120-volt direct current (DC) voltage source (not shown). Because the first and second halves 90a, 90b of the top portion 88 are in contact with their associated legs 86, energization of the first and second leads 82a, 82b results in energization of the first and  
30 second halves 90a, 90b, including the fingers 92.

Subjecting the first and second leads 82a, 82b to a voltage causes the shuttle 16 to move from its open to its closed position, and to remain in the closed position, due to the resulting electrostatic attraction between the shuttle 16 and the actuator portion 14, as follows. As discussed above, the first portion 53a of the shuttle 16 adjoins the beam portion 64 of the first mount 56a, and the fourth portion 53d of the shuttle 16 adjoins the beam portion 64 of the second mount 56b, so that the shuttle 16 is suspended from the first and second mounts 56a, 56b. The beam portions 64 are in their neutral or un-deflected positions when the shuttle 16 is in its open position, as depicted in FIG. 5A and 6A. Moreover, the fourth portion 53d of the shuttle 16 is electrically connected to the ground plane 26 by way of the second mount 56b, and is electrically isolated from the second portion 53b of the shuttle 16 by the third portion 53c of the shuttle 16. The fourth portion 53d, including the fingers 96 thereof, thus remains in a grounded, or zero-potential state at all times.

Subjecting the first and second leads 82a, 82b of the actuator portion 14 to a voltage potential results in energization of the fingers 92, as discussed above. The energized fingers 92 act as electrodes, i.e., an electric field is formed around each finger 92 due the voltage potential to which the finger 92 is being subjected. Each of the energized fingers 92 is positioned sufficiently close to its associated finger 96 on the grounded shuttle 16 so as to subject the associated finger 96 to the electrostatic force resulting from the electric field around the finger 92. The electrostatic force attracts the finger 96 to its corresponding finger 92.

The net electrostatic force acting on the six fingers 96 urges the shuttle 16 in the “+y” direction. The beam portions 64 of the first and second mounts 56a, 56b, which were in their neutral or un-deflected state prior to energization of the fingers 92, are configured to deflect in response to this force as shown in FIGS. 5B and 6B, thereby permitting the suspended shuttle 16 to move in the “+y” direction to its closed position.

The relationship between the amount of deflection and the voltage applied to the actuator portion 14 is dependent upon the stiffness of the beam portions 64, which in turn is dependent upon factors that include the shape, length, and thickness of the beam portions 64, and the properties, e.g., Young’s modulus, of the material from which the beam portion 64 are formed. These factors can be tailored to a particular application so as to minimize the required actuation voltage, while providing the beam portion 64 with sufficient strength for the particular application; with sufficient stiffness to tolerate the anticipated levels shock and vibration; and

with sufficient resilience to facilitate the return of the shuttle 16 to its open position when the voltage potential to the actuator portion 14 is removed.

The actuator portion 14 can have a configuration other than that described above in alternative embodiments. For example, suitable comb, plate, or other types of electrostatic  
5 actuators can be used in the alternative. Moreover, actuators other than electrostatic actuators, such as thermal, magnetic, and piezoelectric actuators, can also be used in the alternative.

As discussed above, electrical isolation of the signal path through the switch 10 is achieved by way of the air gaps 50 between the first and second inner conductors 34, 36 and the adjacent internal surfaces of the ground housing 28; and by way of the first and third portions  
10 53a, 53c of the shuttle 16. The electrical isolation is believed to result in very favorable signal-transmission characteristics for the switch 10. For example, based on finite element method (FEM) simulations, the insertion loss of the switch 10 at 40 GHz is predicted to be approximately 0.09 dB, which is believed to be an improvement of at least approximately 85% over the best in class switches of comparable capabilities. The return loss of the switch 10 at 40  
15 GHz is predicted to be approximately 24 dB, which is believed to be an improvement of at least approximately 85% over the best in class switches of comparable capabilities. The isolation of the switch 10 at 40 GHz is predicted to be approximately 40 dB, which is approximately equal to the isolation achieved by the best in class switches of comparable capabilities.

Moreover, because the switch 10 incorporates a relatively large amount of copper in  
20 comparison to other types of MEMS switches, which typically are based on thin-film technologies, the switch 10 is believed to have substantially higher power-handling capability and linearity, with respect to the transmission of both DC and RF signals, than other types of switches of comparable size. Also, the configuration of the switch 10 makes it capable of being monolithically integrated into systems through the routing of micro-coax lines. Moreover, the  
25 switch 10 can be fabricated or transferred onto a suite of various exotic substrates.

The switch 10 and alternative embodiments thereof can be manufactured using known processing techniques for creating three-dimensional microstructures, including coaxial transmission lines. For example, the processing methods described in U.S. Patent No. 7,898,356 and 7,012,489, the disclosure of which is incorporated herein by reference, can be adapted and  
30 applied to the manufacture of the switch 10 and alternative embodiments thereof.

The switch 10 can be formed in accordance with the following process which is depicted in FIGS. 7A-17B. The first layer of the electrically conductive material forms the ground plane 27; a portion of each leg 86 of the body 80 of the actuator portion 14; and a portion of each lead 82a, 82b of the actuator portion 14. A first photoresist layer (not shown) is applied to the upper surface of the substrate 26 so that the only exposed portions of the upper surface correspond to the locations at which the ground plane 27, the legs 86, and leads 82a, 82b are to be located. The first photoresist layer is formed, for example, by depositing photodefinable, or photoresist masking material on the upper surface of the substrate 26 utilizing a mask or other suitable technique.

Electrically-conductive material is subsequently deposited on the unmasked, i.e., exposed, portions of the substrate 26 to a predetermined thickness, to form the first layer of the electrically-conductive material as shown in FIGS. 7A and 7B. The deposition of the electrically-conductive material is accomplished using a suitable technique such as chemical vapor deposition (CVD). Other suitable techniques, such as physical vapor deposition (PVD), sputtering, or electroplating, can be used in the alternative. The upper surfaces of the newly-formed first layer can be planarized using a suitable technique such as chemical-mechanical planarization (CMP).

The second layer of the electrically conductive material forms portions of the sides of the ground housing 28; another portion of each leg 86; another portion of the first and second leads 82a, 82b; and a portion of each of the first and second mounts 56a, 56b. A second photoresist layer 100 is applied to the partially-constructed switch 10 by patterning additional photoresist material in the desired shape of the second photoresist layer over the partially-constructed switch 10 and over the previously-applied first photoresist layer, utilizing a mask or other suitable technique, so that so that the only exposed areas on the partially-constructed switch 10 and the partially-constructed cover 100 correspond to the locations at which the above-noted portions of the switch 10 are to be located, as shown in FIGS. 8A and 8B. The electrically-conductive material can subsequently be deposited on the exposed portions of the switch 10 to a predetermined thickness, to form the second layer of the electrically-conductive material as shown in FIGS. 9A and 9B. The upper surfaces of the newly-formed portions of the switch 10 can then be planarized.

The dielectric material that forms the tabs 37 is deposited and patterned on top of the previously-formed photoresist layer as shown in FIGS. 10A and 10B. The dielectric material that forms the first and third portions 53a, 53c of the body 52 of the shuttle 16 can be deposited and patterned on top of the previously-formed photoresist layer as also shown in FIGS. 10A and 1B, before or after the tabs 37 are formed.

The third layer of the electrically conductive material forms additional portions of the sides of the ground housing 28; the second and fourth portions 53b, 53d of the body 52 of the shuttle 16; additional portions of each of the first and second mounts 56a, 56b; and the top portion 88 of the body 80 of the actuator portion 14. A third photoresist layer 102 is applied to the partially-constructed switch 10 by patterning additional photoresist material in the desired shape of the third photoresist layer over the partially-constructed switch 10 and over the second photoresist layer, utilizing a mask or other suitable technique, so that so that the only exposed areas on the partially-constructed switch 10 correspond to the locations at which the above-noted components are to be located, as shown in FIGS. 11A and 11B. The electrically-conductive material can subsequently be deposited on the exposed portions of the switch 10 to a predetermined thickness, to form the third layer of the electrically-conductive material as shown in FIGS. 12A and 12B. The upper surfaces of the newly-formed portions of the switch 10 can then be planarized.

The fourth and fifth layers of the electrically conductive material form, respectively, additional portions of the sides of the ground housing 28, and the top of the ground housing 28. The fourth and fifth layers are formed in a manner similar to the first, second, and third layers. In particular, the fourth and fifth layers are formed by applying additional photoresist material to the previously-formed layers, utilizing a mask or other suitable technique, to form fourth and fifth photoresist layers 104, 106 as shown respectively in FIGS. 13A/13B and 15A/15B, and then depositing additional electrically-conductive material to the exposed areas to form the fourth and fifth layers as shown respectively in FIGS. 14A/14B and 16A/16B. The upper surfaces of the newly-formed portions of the switch 10 can be planarized after the application of each of the fourth and fifth layers.

The photoresist material remaining from each of the masking steps can then be released or otherwise removed after the fifth layer has been applied as depicted in FIGS. 17A and 17B, using a suitable technique such as exposure to an appropriate solvent that dissolves the

photoresist material.

**CLAIMS****We claim:**

1. A switch, comprising:  
a housing;  
5 a first electrical conductor;  
a second electrical conductor spaced apart from the first electrical conductor, wherein the first and second electrical conductors are suspended within the housing on electrically-insulative supports; and  
a contact element having an electrically-insulative first portion, an electrically-conductive  
10 second portion, and an electrically-insulative third portion, wherein: the first and third portions adjoin the second portion; and the contact element is configured for movement between a first position at which the second portion of the contact element is spaced apart and electrically isolated from the first and second electrical conductors, and a second position at which the second portion of the contact element contacts the first and second electrical conductors.  
15
2. The switch of claim 1, further comprising an electrically-insulative substrate, and a ground plane disposed on the substrate; wherein the housing is an electrically-conductive housing in electrical contact with the ground plane.
- 20 3. The switch of claim 2, further comprising a first and a second mount; wherein first and second mounts are mounted on and are in electrical contact with the ground plane, and the contact element is suspended from the first and second mounts.
4. The switch of claim 3, wherein the first and second mounts each comprise a beam portion  
25 configured to resiliently deflect to facilitate movement of the contact element between the first and second positions.
5. The switch of claim 3, wherein the first portion of the contact element is configured to electrically isolate the second portion of the contact element from the first mount and the ground  
30 plane, and the third portion of the contact element is configured to electrically isolate the second portion of the contact element from the second mount and the ground plane.

6. The switch of claim 2, wherein the first and second electrical conductors are spaced apart from and electrically isolated from the housing by an air gap .

5 7. The switch of claim 2, wherein: the second portion of the contact element includes an elongated body, and a first and a second projection that project from opposite sides of the body; the first projection is configured to be spaced apart from the first electrical conductor when the contact element is in the first position; and the second projection is configured to be spaced apart from the second electrical conductor when the contact element is in the first position.

10

8. The switch of claim 7, wherein the first projection is configured to contact the first electrical conductor when the contact element is in the second position; and the second projection is configured to contact the second electrical conductor when the contact element is in the second position.

15

9. The switch of claim 5, further comprising an actuator portion having a body operative generate a force when energized, the force moving the contact element from the first to the second position.

20

10. The switch of claim 9, wherein the body of the actuator portion comprises a first and second leg disposed on the substrate, and a top portion mounted on the first and second legs and including a first projection; the contact element comprises an electrically-conductive fourth portion that adjoins the third portion of the contact element; the fourth portion of the contact element comprises a second projection located proximate the first projection; and the first projection, when subjected to a voltage potential, is operative to develop an electrostatic force that attracts the second projection and thereby urges the contact element toward the second position.

25

30

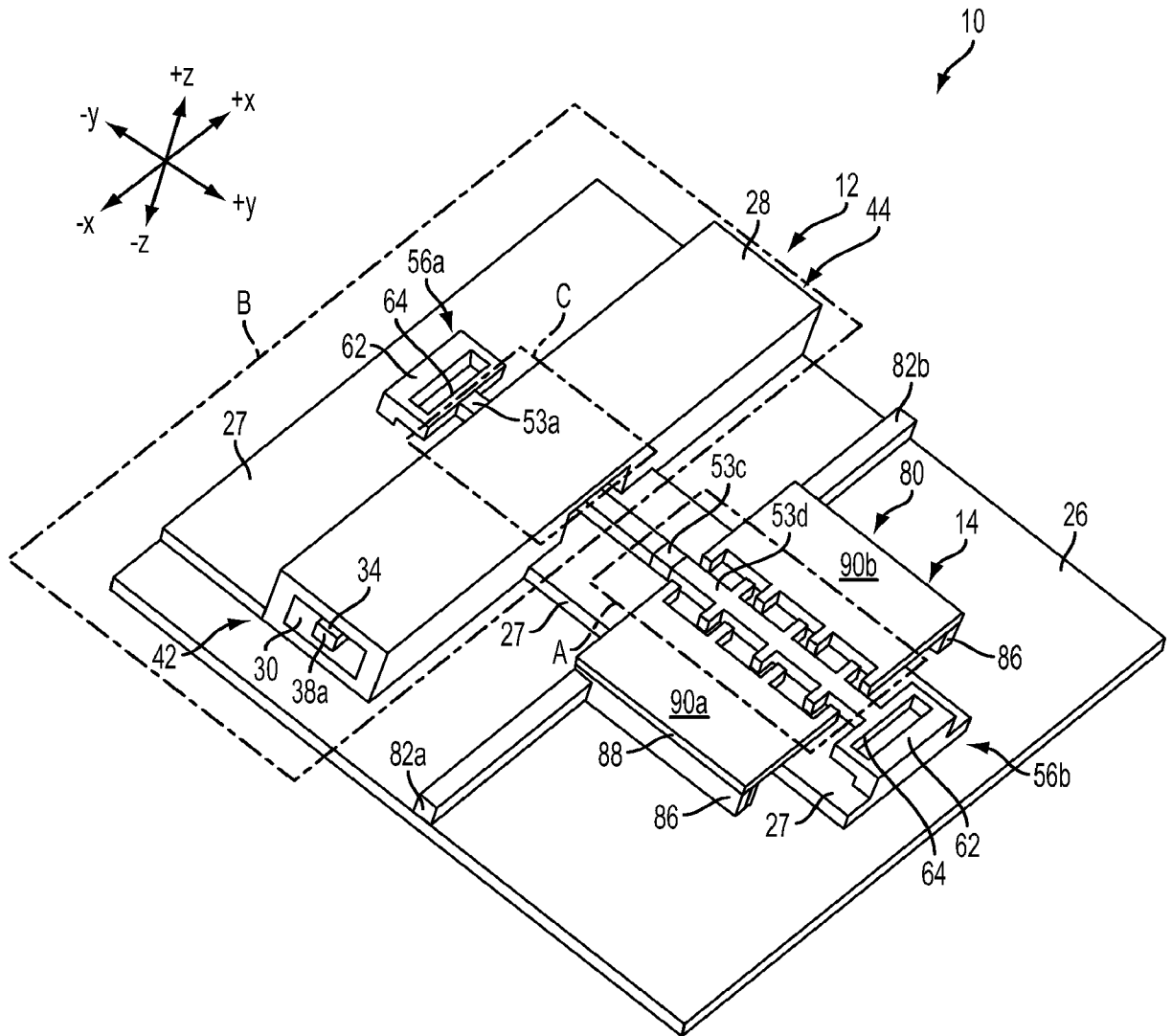


FIG. 1

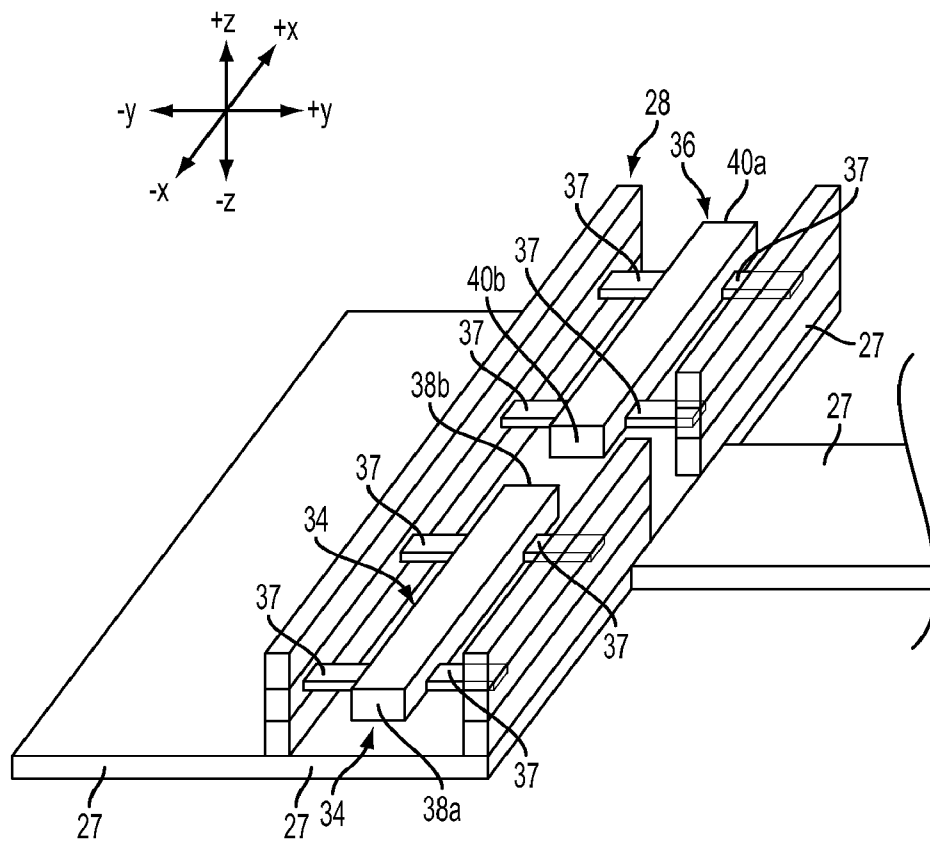


FIG. 2





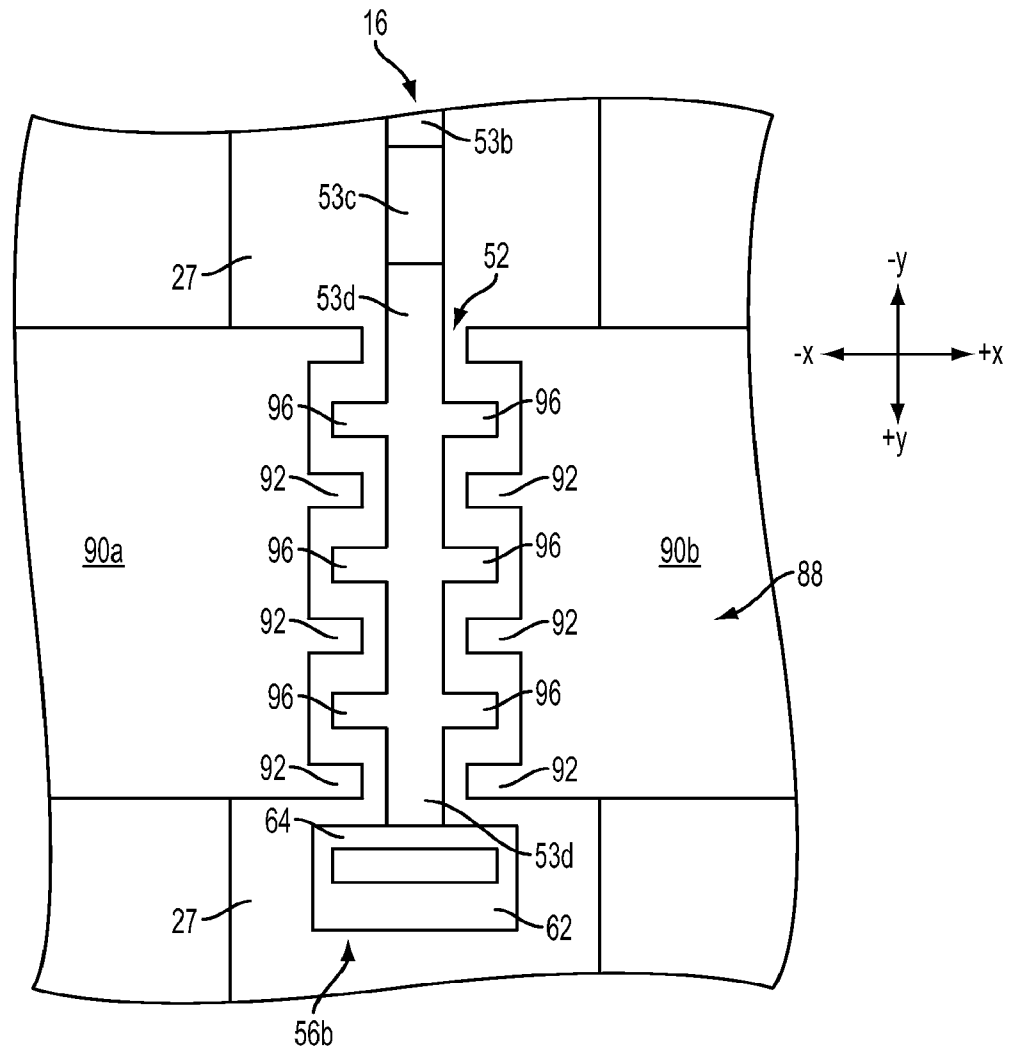


FIG. 5A

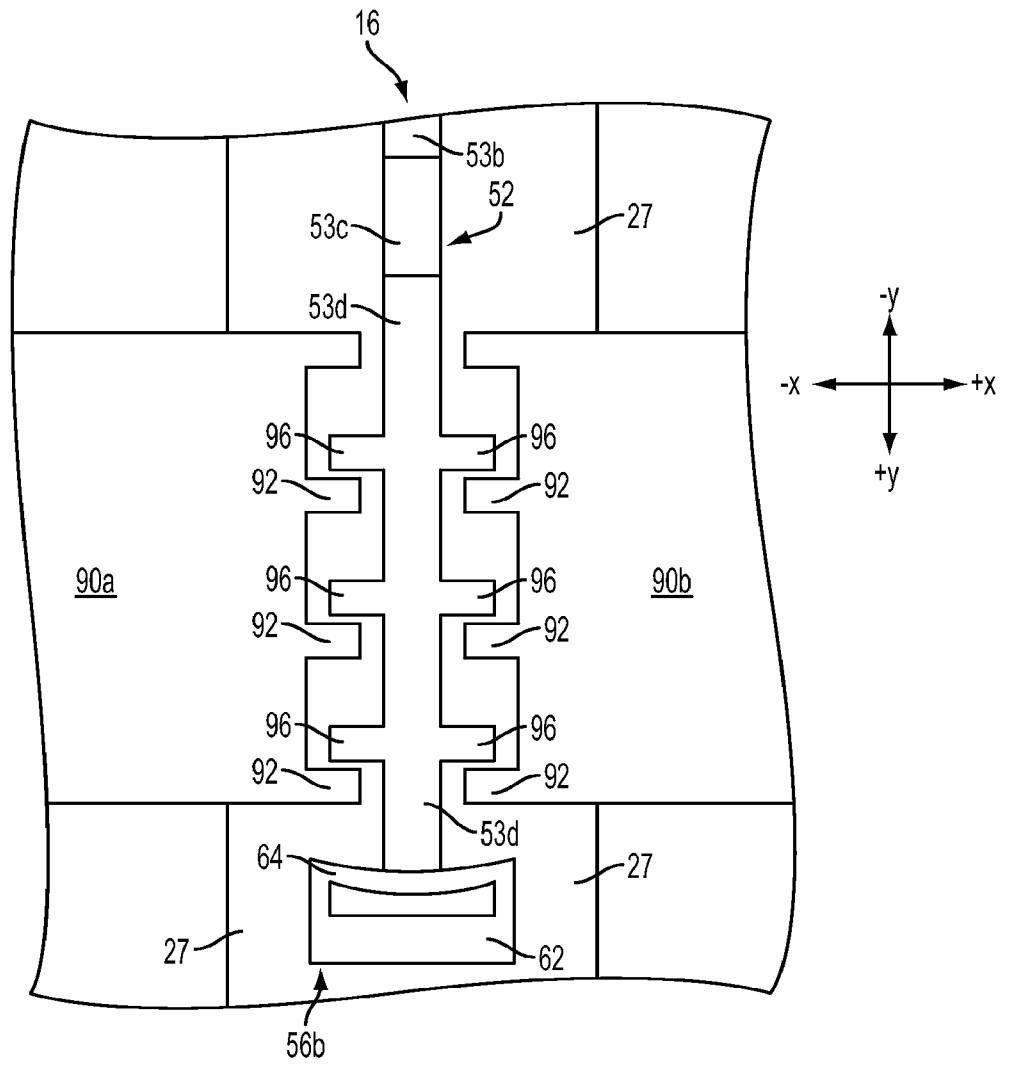


FIG. 5B

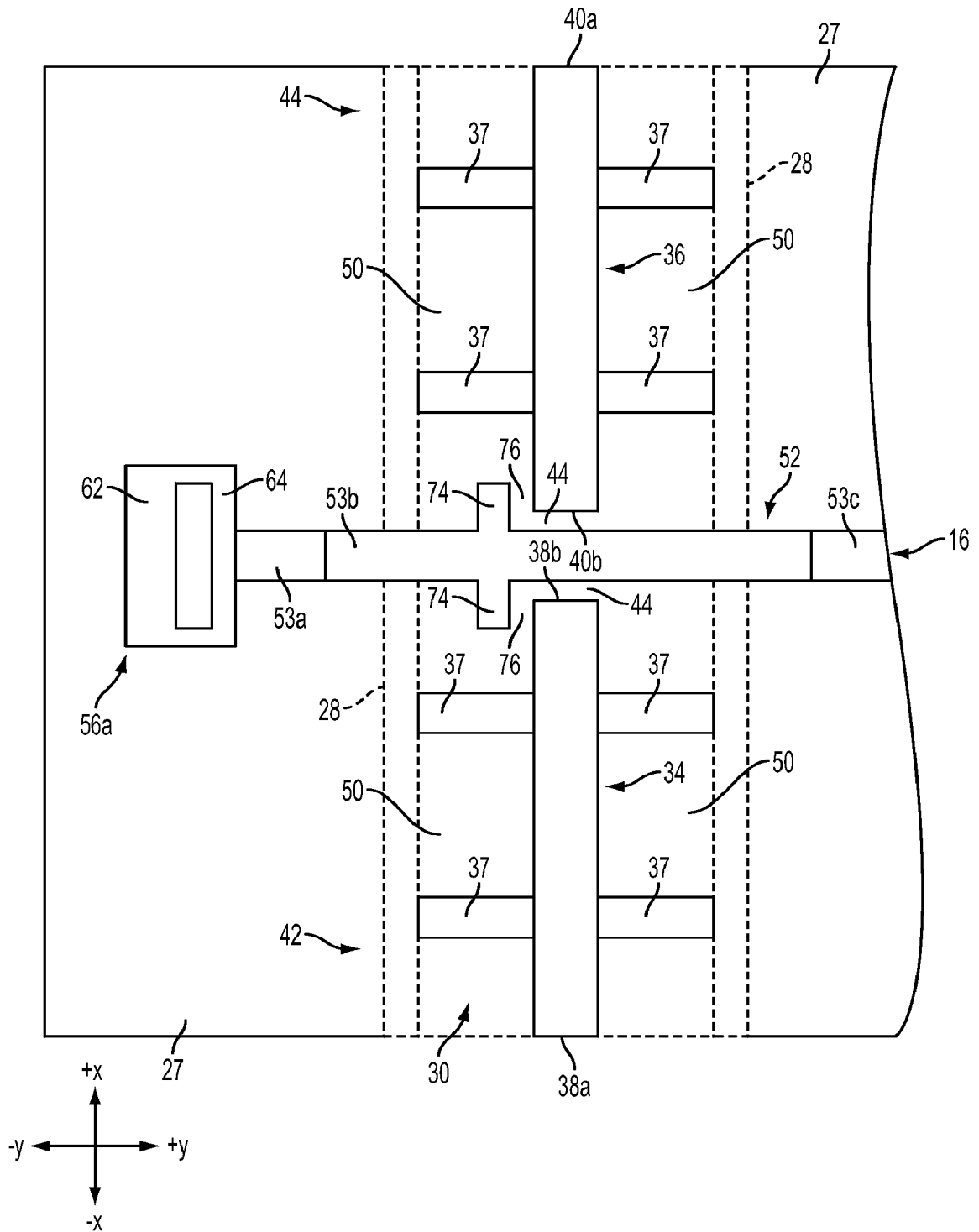


FIG. 6A

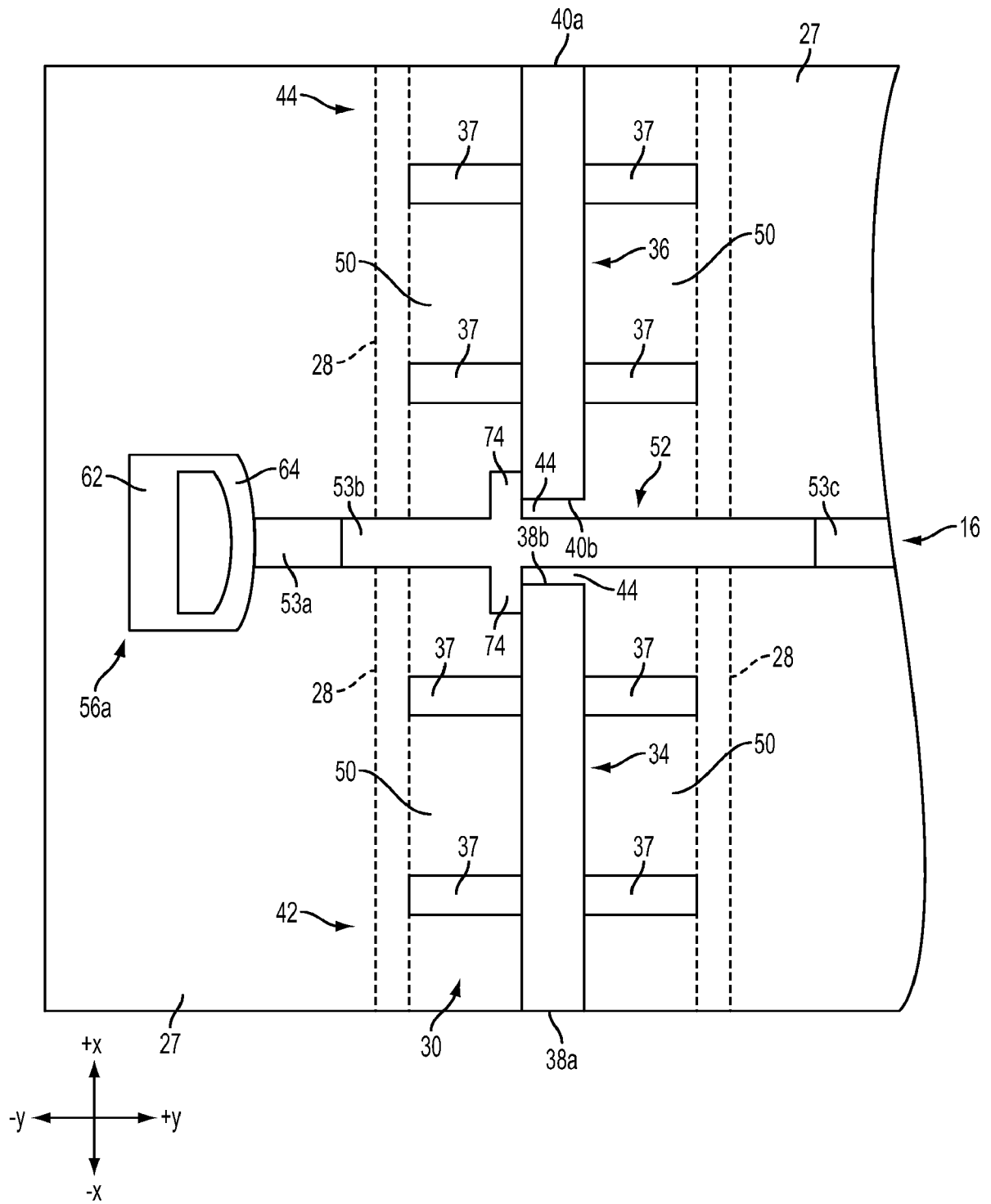


FIG. 6B

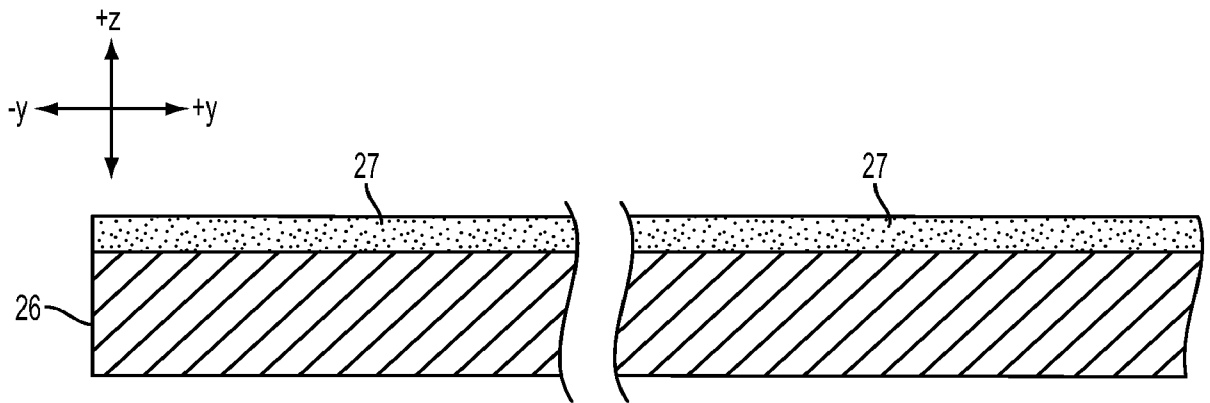


FIG. 7A

FIG. 7B

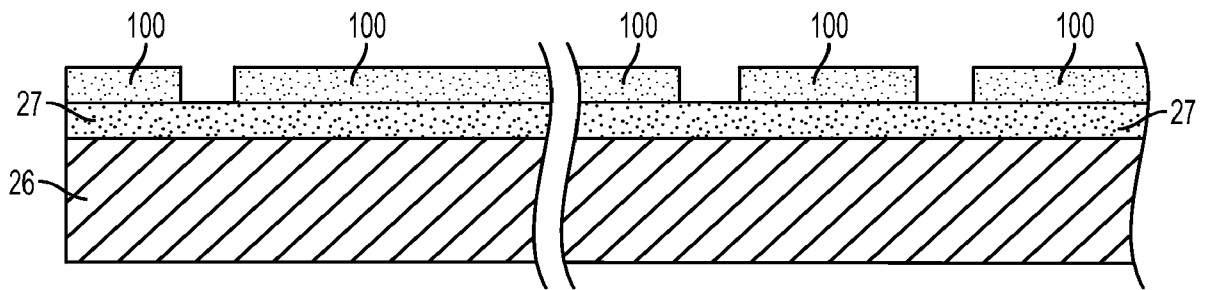


FIG. 8A

FIG. 8B

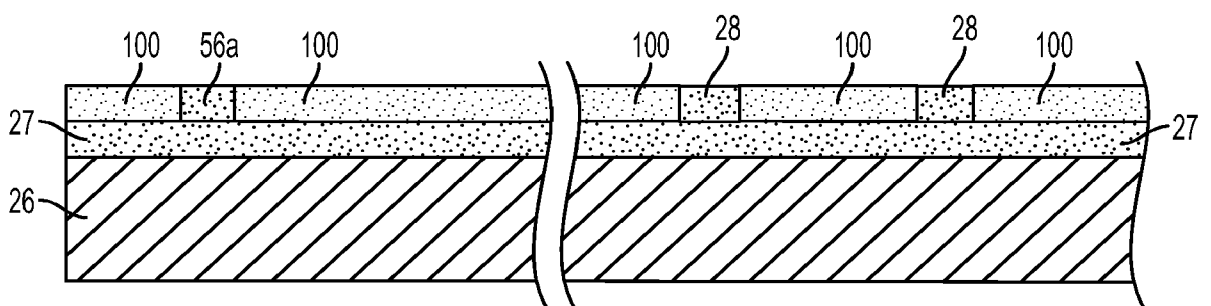


FIG. 9A

FIG. 9B

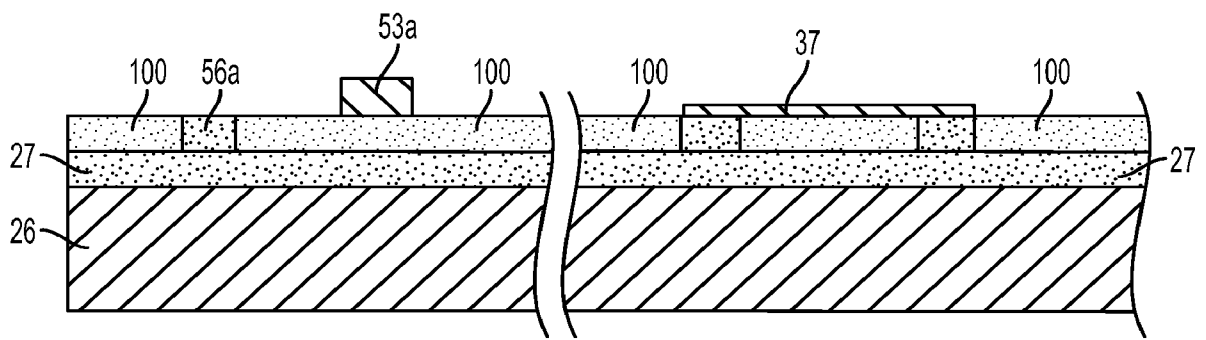


FIG. 10A

FIG. 10B

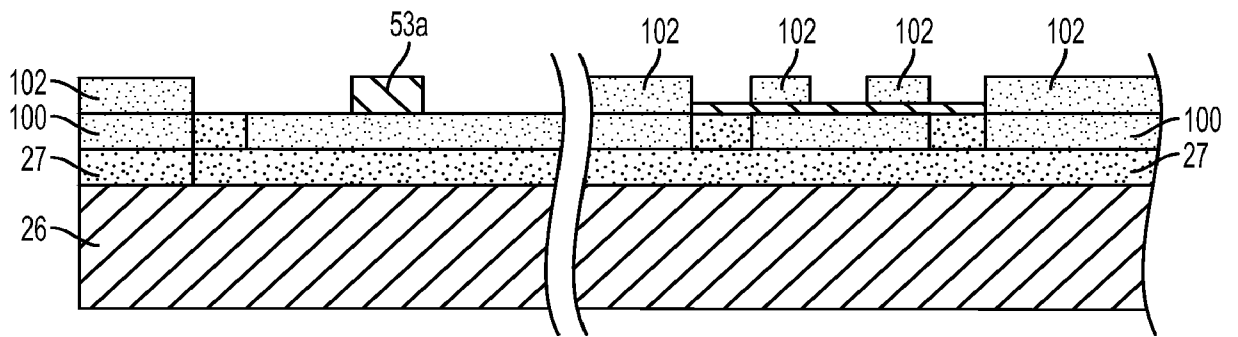


FIG. 11A

FIG. 11B

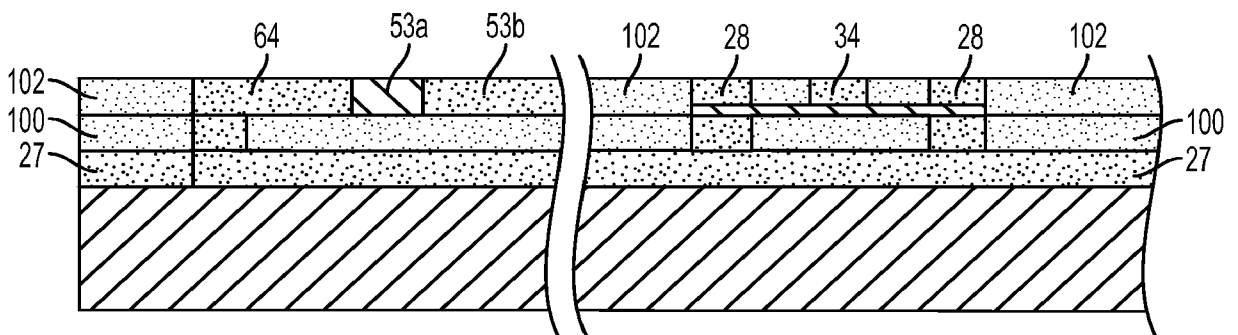


FIG. 12A

FIG. 12B

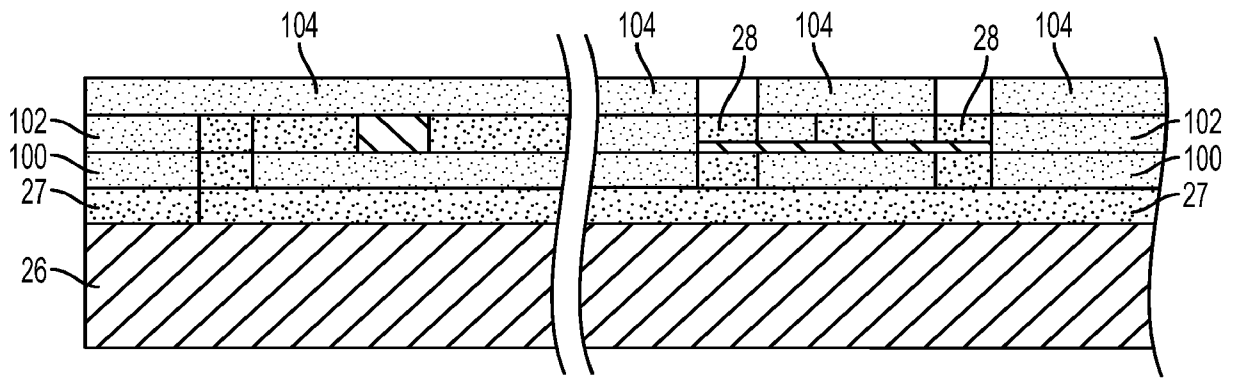


FIG. 13A

FIG. 13B

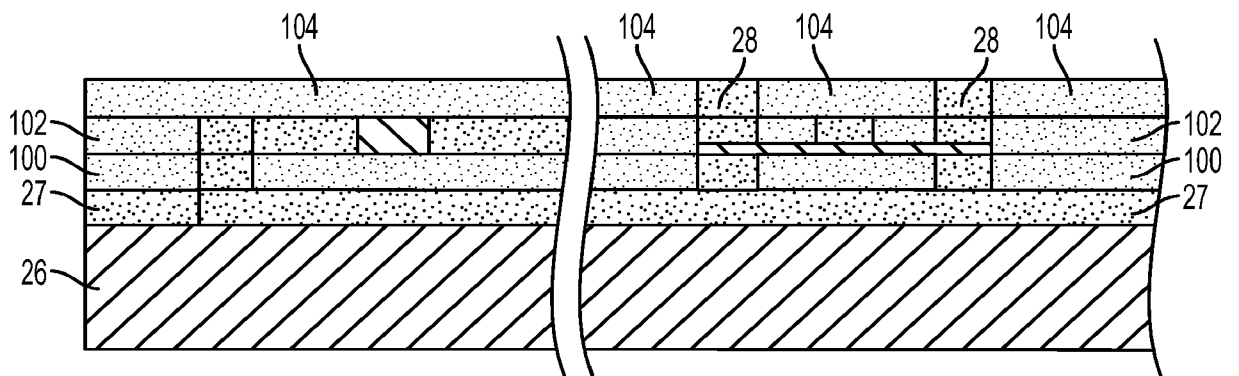


FIG. 14A

FIG. 14B

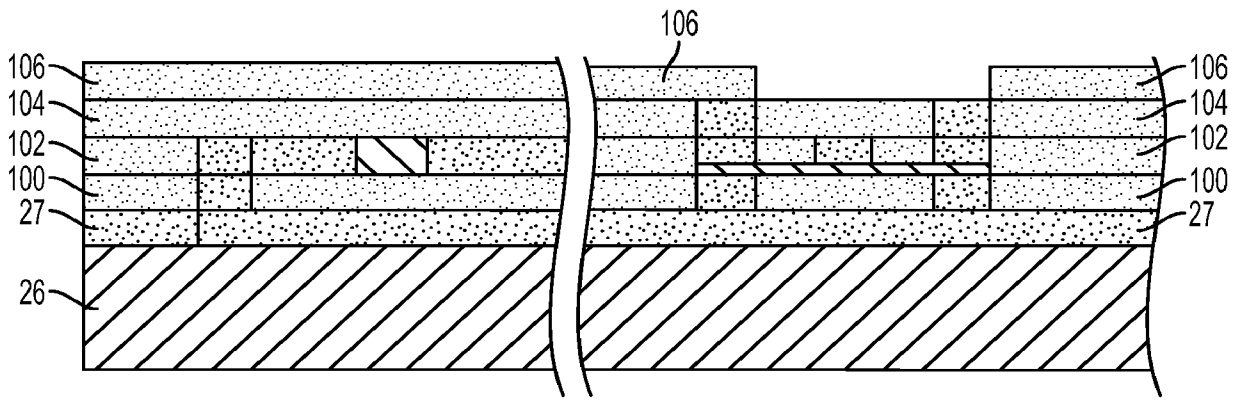


FIG. 15A

FIG. 15B

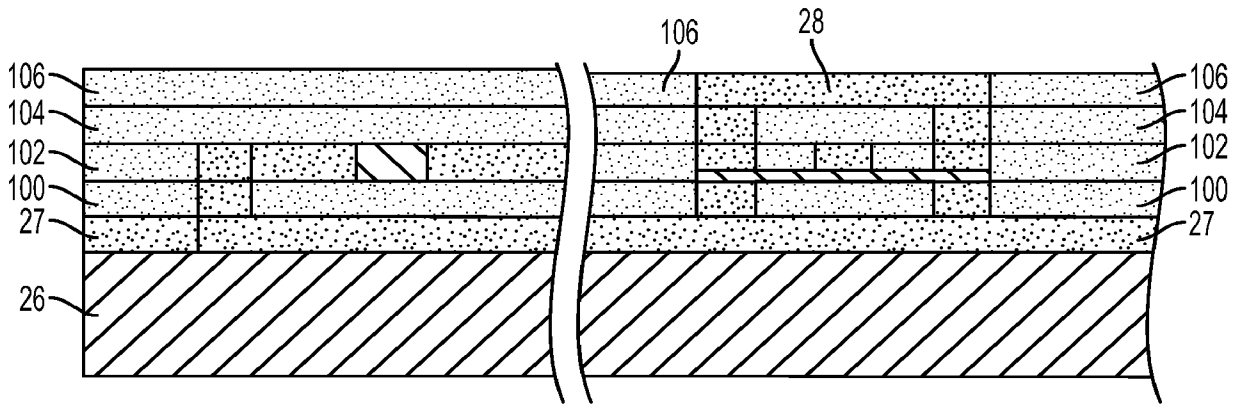


FIG. 16A

FIG. 16B

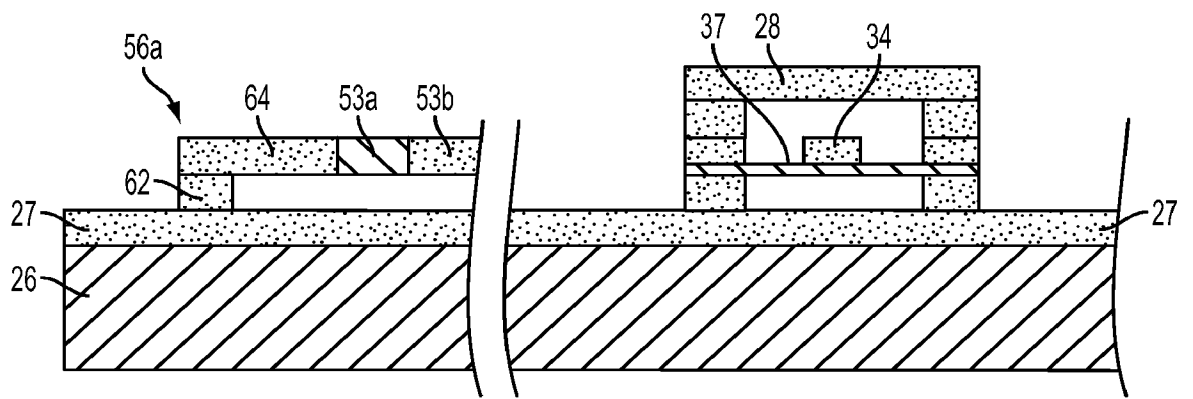


FIG. 17A

FIG. 17B

**INTERNATIONAL SEARCH REPORT**

International application No  
**PCT/US2013/056316**

**A. CLASSIFICATION OF SUBJECT MATTER**  
 INV. H01H1/00 H01H59/00  
 ADD.  
 According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**  
 Minimum documentation searched (classification system followed by classification symbols)  
**H01H**  
 Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)  
**EPO-Internal, WPI Data**

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2008/142347 A1 (LEWIS ALAN [US] ET AL) 19 June 2008 (2008-06-19)	1-4,6
Y	page 5, paragraph 0060 - page 8, paragraph 0086; figures 8A-17C	5,7-10
X	US 2005/073380 A1 (HOWELL LARRY [US] ET AL) 7 April 2005 (2005-04-07)	1
Y	page 11, paragraph 0119 - page 16, paragraph 0165; figures 8-15	2-10
X	US 7 026 899 B2 (ADAMS SCOTT G [US] ET AL) 11 April 2006 (2006-04-11)	1
Y	column 8, line 51 - column 7, line 42; figures 1,2,4	2-10
Y	US 2011/220472 A1 (MASUDA TAKAHIRO [JP] ET AL) 15 September 2011 (2011-09-15) page 3, paragraph 0032 - page 5, paragraph 0058	2-10

Further documents are listed in the continuation of Box C.       See patent family annex.

\* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"E" earlier application or patent but published on or after the international filing date	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"O" document referring to an oral disclosure, use, exhibition or other means	"&" document member of the same patent family
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search <b>20 November 2013</b>	Date of mailing of the international search report <b>28/11/2013</b>
--	---

Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer  <b>Pavlov, Valeri</b>
--	---

# INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2013/056316

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2008142347	A1	19-06-2008	EP 2095385 A1 02-09-2009
			US 2008142347 A1 19-06-2008
			WO 2008076448 A1 26-06-2008
-----			
US 2005073380	A1	07-04-2005	NONE
-----			
US 7026899	B2	11-04-2006	AU 2002368527 A1 22-07-2004
			US 2003132090 A1 17-07-2003
			WO 2004059678 A1 15-07-2004
-----			
US 2011220472	A1	15-09-2011	CN 102194612 A 21-09-2011
			EP 2365509 A1 14-09-2011
			JP 5263203 B2 14-08-2013
			JP 2011192424 A 29-09-2011
			KR 20110103301 A 20-09-2011
			US 2011220472 A1 15-09-2011
-----			