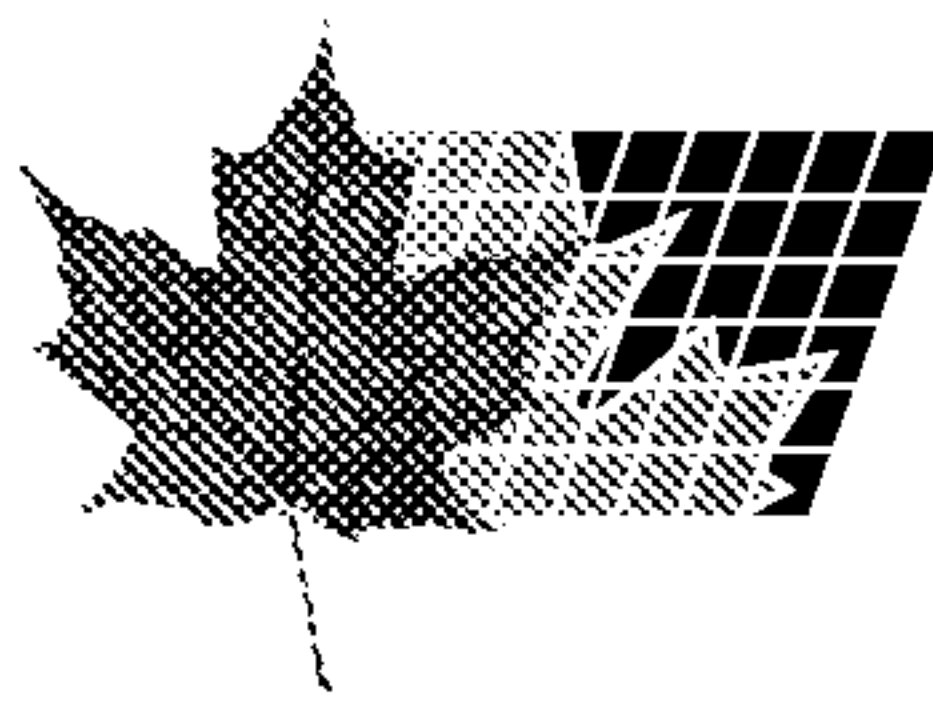
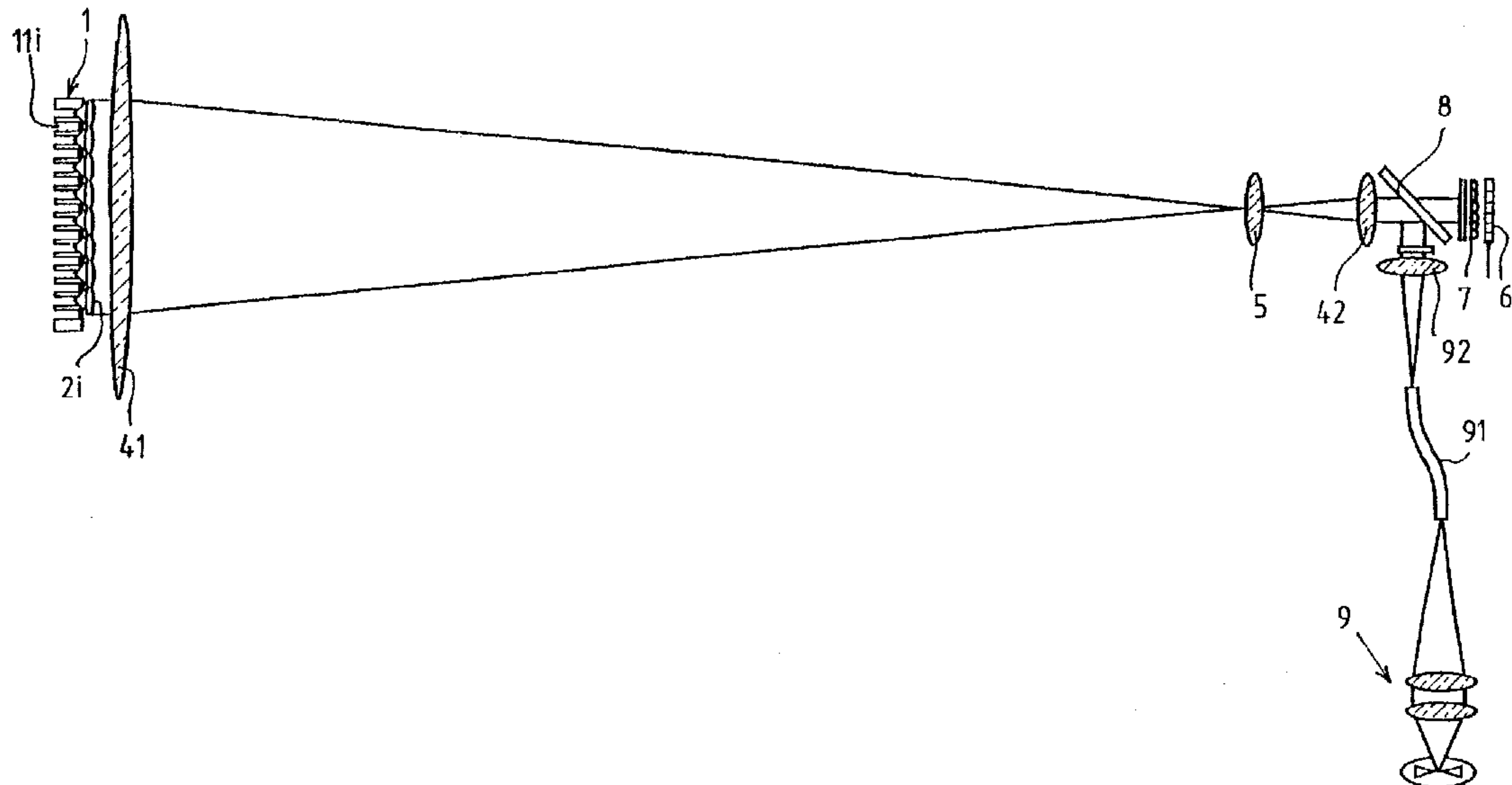




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(54) **SYSTEME DE MOSAIQUE OPTIQUE ET LECTEUR POUR
MICROPLAQUES DE TITRATION**
(54) **OPTICAL ARRAY SYSTEM AND READER FOR MICRO TITER
PLATES**



(57) Système optique comprenant des mosaïques de lentilles (2i, 7) et des lentilles normales (41, 5, 42), qui peut notamment être utilisé comme lecteur massivement parallèle (environ 10^2 canaux) de microplaques (1) et similaires, en absorption, fluorescence et luminescence.

(57) An optical system made up of lens arrays (2i, 7) and normal lenses (41, 5, 42) is particularly suitable for use as a massive parallel reader (approx. 10^2 channels) for micro titer plates (1) and the like in absorption, fluorescence and luminescence.

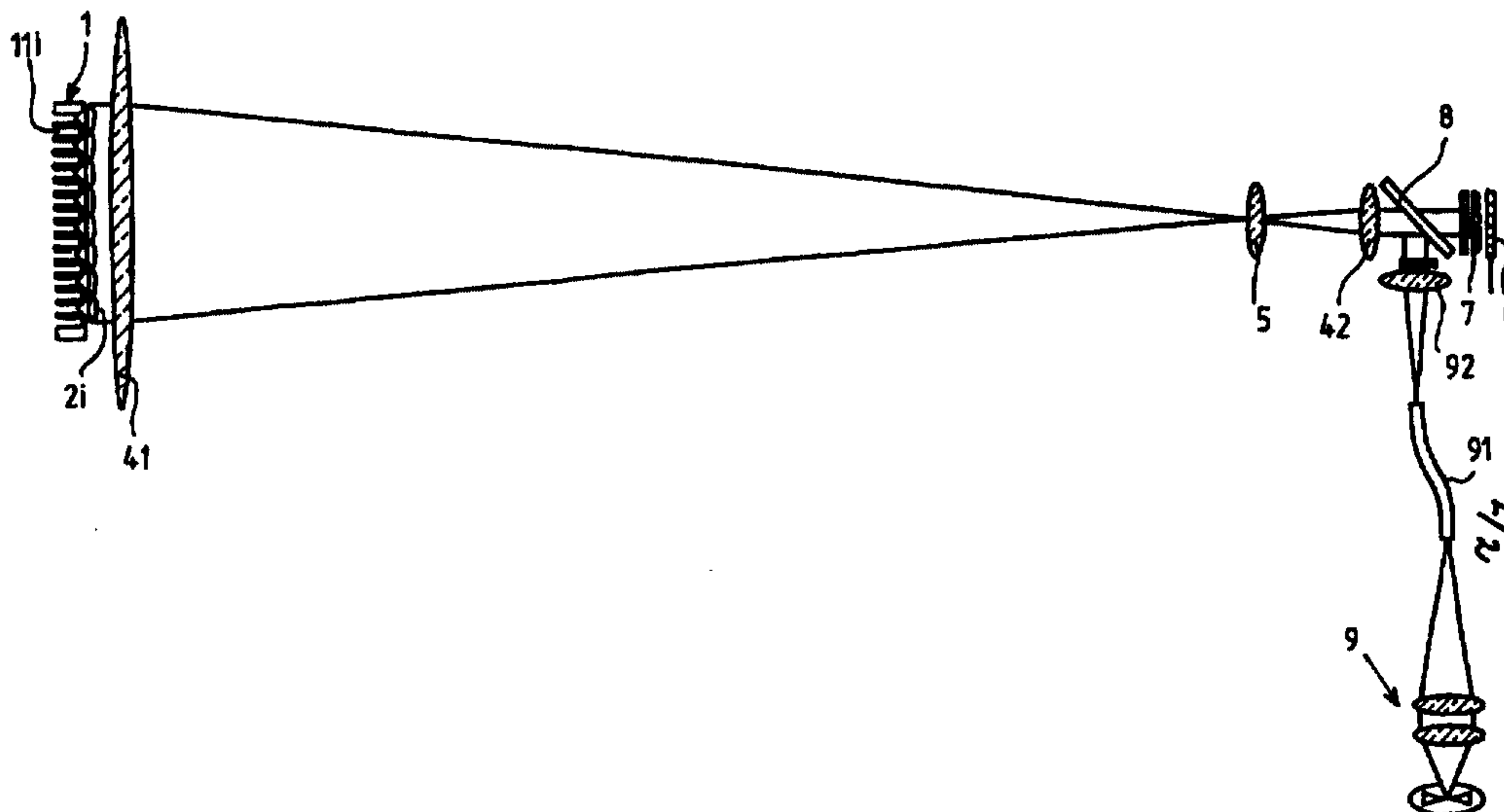


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(54) Title: OPTICAL ARRAY SYSTEM AND READER FOR MICRO TITER PLATES

(54) Bezeichnung: OPTISCHES ARRAY-SYSTEM UND READER FÜR MIKROTITERPLATTEN



(57) Abstract

An optical system made up of lens arrays (2i, 7) and normal lenses (41, 5, 42) is particularly suitable for use as a massive parallel reader (approx. 10^2 channels) for micro titer plates (1) and the like in absorption, fluorescence and luminescence.

(57) Zusammenfassung

Ein optisches System mit Linsenarrays (2i, 7) und normalen Linsen (41, 5, 42) ist besonders geeignet als massiv paralleler (ca. 10^2 Kanäle) Reader für Mikrotiterplatten (1) und dergleichen in Absorption, Fluoreszenz und Lumineszenz.

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OPTICAL ARRAY SYSTEM AND READER FOR MICRO TITER PLATES

The invention relates to a reader for microtiter plates or substance chips.

Fluorescence, luminescence, and absorption investigations of huge numbers of very small amounts of samples are necessary in the development of pharmaceutically effective materials, and also in medical molecular diagnosis. Here a high throughput of samples in the measurement is of the greatest importance.

10 Kinetic measurements are particularly in demand, with time constants which permit a high throughput.

For the preparation of the samples, microtiter plates are available, with small sample holders arranged in a grid pattern in standard configurations with, e.g., 96 or a multiple thereof, e.g., 384 or 1536, sample containers (multi-well microplates). Alternatively, so-called substance chips are also used as sample carriers.

Such a reader is, for example, offered for sale by Molecular Devices Corp., USA, under the designation SPECTRAmax (R) PLUS. A light source and a monochromator are connected by means of 8 optical fibers to 8 mirror optics, each
20 for the transmission illumination of a respective sample holder, and with 8 measuring photodetectors. Eight-fold measurement in parallel is thus possible.

A sample carrier in the form of an array with many small sample volumes is described in WO 95/01559, and at the same time has one or two microlenses for each sample volume for optical measurements. The light emitted from the individual sample volumes is to be projected onto a CCD sensor by means of these microlenses. However, it remains an open question whether, or how, a matching of

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the dimensions of the sample carrier to the dimensions of the CCD sensor takes place.

A scanning system for microlithography and/or confocal microscopy is known from WO 97/34171, and has a microlens array on the sample side or on the photomask side, and a telescopic system between the microlens array and a detector array or a wafer. A special matching of the grid pattern dimensions of the microlens array to the grid pattern dimensions of a sample array is not given there.

10 The invention has as its object to provide a reader for microtiter plates or substance chips which makes possible a massively parallel measurement and thus greatly increases the sample throughput, even for kinematic measurements. High efficiency of the light path, and a compact construction, as simple as possible, are to be attained thereby. A high measurement sensitivity is of course to be insured.

An optical system according to claim 1 attains this object. For detection, a detector array is provided which is available, for example, as a CCD array. Conventional optics with conventional lenses are combined with lens arrays over the whole cross section. Imaging of the whole sensed object region (microtiter plate) to
20 the correct scale on the CCD array, and also a suitable imaging of the individual wells of the microtiter plate on the CCD array (two different scales), with strict channel separation between the different wells, are thus both attained.

Advantageously, the features stated in the dependent claims are supplementary to this. These include a telescope, which is single-lens over the cross section; a microlens array before the detector array, and the integration of a reflected light illumination. The latter, by double use of the optical elements, results in particularly good efficiency and particularly good noise suppression, in that
30 exactly the sample volume is illuminated which is also sensed by the detection beam path.

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A further suppression of interference can be attained with an aperture array.
The invention is described in more detail with reference to the drawing.

Fig. 1 shows schematically a first optical arrangement according to the
invention, in a first embodiment;

Fig. 2 shows schematically a reader according to the invention.

10 The illustration of Fig. 1 shows only three respective examples of all the array
elements, in order to be able to illustrate the principle clearly.

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elements, in order to be able to illustrate the principle clearly. A practical embodiment provides a match to a conventional microtiter plate array of $8 \times 12 = 96$ elements (pixels).

An object array 11, 12, 13 is formed by the microtiter plate with recesses (wells) and substance samples 110, 120, 130 placed therein. The minilens array 21, 22, 23 has the same grid measurements, and is built up from conventional small lenses, with a focal length of $f = 7.8$ and a numerical aperture of about 0.6, effectively collecting together the light from a central region 11, 12, 13 of the samples 110, 120, 130. An aperture 3 is arranged in the intermediate image plane at a distance of 380 mm, and prevents crosstalk between the individual array elements.

The telescope which follows, having lenses 41 and 42, reduces the beam diameter from 130 mm to 15 mm, matching the dimensions of the CCD array. The field lens 5 arranged therebetween provides imaging of the intermediate image and thus of the array of objects 11, 12, 13 onto the elements of the CCD array 6.

The whole "collective" optics 41, 5, 42 is determined as regards its diameter only by the size of the microtiter plate 1 or of the array of objects 11, 12, 13. In contrast to this, a conventional CCD camera with the same numerical aperture of 0.6 has to have much larger lenses. This is made possible in that the numerical aperture of the optical system according to the invention is determined by the elements 21, 22, 23 of the minilens grid pattern.

The most important feature of the arrangement is that a respective image zone on the CCD array corresponds exactly, and free from crosstalk, to each of the samples 110, 120, 130.

The illumination device would have to be supplemented for fluorescence or absorption measurements, e.g., in the manner described in more detail with Fig. 2.

The arrangement of Fig. 1 is already directly suitable for luminescence

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measurements, but of course an about tenfold focal length of the lens array 21, 22, 23 is preferred for this, whereby the sensed sample volume is increased.

The arrangement of Fig. 2 is designed as a fluorescence reader. Firstly, it has the same elements as in Fig. 1, namely a microtiter plate 1 with wells 11i, minilens array 2i with 96 lenses, large (41) and small (42) telescope lenses, with the field lens 5 and the CCD array 6 therebetween. However, as a variant, the minilens array 2i collimates, and there is no aperture grid pattern plate; however, directly in front of the CCD array there is a microlens array 7, with 96 microlenses which are
10 collectively produced in microstructure technology and which effect the imaging into the detector cells of the CCD array 6.

A grid pattern dimension on the CCD array of about forty detector cells in diameter is thus attained, in which about one spot, twenty detector cells in diameter, of each sample element is illuminated.

A coupling-in mirror 8 (dichroic mirror) is arranged between the telescope lens 42 and the microlens array 7. An illuminating device 9 provides, via optical fibers 91 and condenser 92, illuminating light to the mirror 8, to be conducted by
20 means of the already described optical system precisely to the places on the microtiter plate 1 which are imaged on the CCD detector 6. The light of the illuminating device 9 is thus optimally used for the measurement. Disturbances due to illumination of the structure of the microtiter plate 1 and the like are eliminated.

The illuminating device can consist of a white light source, e.g., a xenon gas discharge lamp, and may also be combined with a monochromator for the formation of a spectrophotometer.

A line source, e.g., a laser, can also be considered for use. With a
30 discrete scanning device for the relative movement of the microtiter plate 1 and the minilens array 2i, including the whole optical arrangement, a 384-well microtiter

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plate, for example, can be completely read out with four successive positionings.

The usual filters in the illumination beam path and analyzing beam path, for the separation of illumination light and fluorescence light, can be arranged, together with the dichroic mirror, in an interchangeable module, so that a quick change of the fluorescence system is made possible.

For the same reason, preferably at least the lens array 2i on the object side is achromatized, in that each individual lens is replaced by a lens group with achromatic correction. The spectral region is then typically provided as about 350-
10 800 nm.

If the beam splitter 8 is not dichroically constituted and if a mirror is arranged over the microtiter plate 1, an arrangement can thus be derived for absorption measurement, analogous to the described equipment of the firm Molecular Dynamics. A reflected light illumination can of course also be provided.

The arrangement is confocal in the sense that a spatially bounded illumination spot in the sample is superposed with a spatially bounded detection region. The aperture in the illumination beam path can represent the fiber end or an illumination
20 field stop; the aperture in the detection beam path can be produced by selective reading-out of the CCD pixels in the region of the individual illumination spots, by an aperture array in front of the CCD camera, or by a field stop in the region of the field lens.

A transmission illumination can also be realized with this confocal character, if a corresponding lens array like the lens array 2i is provided.

In the embodiment as a reader for fluorescence measurements, a focus diameter of 50-500 μm , particularly 150 μm , with a numerical aperture of 0.6-0.7, is
30 preferably provided.

Fluorescence correlation spectroscopy (FCS) can be parallelized with the

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same optical concept and can thus be useful for high throughput applications. However, for a good signal-to-noise ratio here, the reduction of the measurement volume to the range of femtoliters, with a focus diameter of 0.1-10 μm , is advantageous. The minimum correlation time is however limited by the integrating and readout time of the CCD array. Detector arrays which can be read out in parallel, such as APD arrays, are therefore to be preferred in this application.

For easy adaptation to the different measurement processes, a reader having a modular construction is therefore proposed, in which the lens array 2i on the sample side is interchangeable.

The following advantages of the invention can thus be derived:

- High channel number with an order of magnitude of 10^2 channels is easily possible and gives effective parallelization.
- A high fluorescence detection sensitivity is provided by the large possible aperture of the individual cells 21, 22, 23 of the minilens array.
- A low power of the light source 9 is sufficient, since the illumination takes place in a structured manner, and a high fluorescence detection sensitivity is provided.
- A strong suppression, by the confocal detection, of interfering fluorescence from outside the measurement volume (typical measurement volumes in fluorescence measurements for microtiter plates and 96-channel optics: a few nanoliters) makes possible the measurement of homogeneous samples, in spite of possible strong fluorescence concentrations on the floor due to precipitates and in spite of strong inherent fluorescence of the floors and walls of the wells in the microtiter plate.
- An independence from filling height in fluorescence measurements is likewise effected by the confocal character.

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- Fluorescence filters and beam splitters with standard dimensions (diameter in the region of 25 mm) can be used, since the greatest dimensions of the microtiter plates are reduced by the telescope (diameter about 15 mm at the CCD array).
- Crosstalk between adjacent samples (wells) is in principle small due to the local illumination and the confocal detection, and can be further reduced by an aperture mask or by lands between the lens elements of the lens array, and the simultaneous use of, for example, only every other well (e.g., 96-channel detection with 384-microtiter plates).
- Data sensing is also simple with the high channel number due to the use of a CCD array.
- Flexibility in the format is provided, since the 96 grid pattern of the reader also matches more highly integrated microtiter plates (e.g., 384, 864, 1536 wells) and also so-called cell chips and DNA chips.
- Kinetic fluorescence measurements are in particular supported by the multi-channel embodiment.
- Fluorescence measurements can be carried out on cell-based arrays by focusing the lens array 2i on cells which are installed on the floor of the well. Positionally resolved reading-out of the individual spot, here as large as possible, on the CCD with a resolution of about the cell size or better makes possible a substantially more detailed, positionally resolved, analysis of the biological function of the substance to be investigated. This High Content Screening (HCS) makes possible, e.g., the comparison of the fluorescence concentrations outside, on, and within the cell, and in the cell nucleus. Here also, kinetics is important.

PATENT CLAIMS

1. Reader for microtiter plates or substance chips, with a lens array [21-23], the grid pattern dimensions of which corresponds to the grid pattern dimensions of a microtiter plate or of a substance chip, a detector array [61-63], a telescope which is provided between the lens array and the detector array and which effects a reduction to match the beam diameter defined by the lens array to the dimensions of the detector array, and with a field lens [5], a reduced image of the microtiter plate or the substance chip being formed on the detector array by the system of lens array, telescope, and field lens, so that on the detector array a strict channel separation results between the measurement signals arising from individual sample volumes of the microtiter plate or of the substance chip.
2. Reader according to claim 1, characterized in that a respective lens (41, 42) of a telescope is arranged between the lens array [21-23] and field lens [5], and between the latter and the detector array [61-63].
3. Reader according to at least one of claims 1-2, characterized in that a microlens array [7] is arranged in front of the detector array [6].
4. Reader according to at least one of claim 1-3, characterized in that a reflected light illumination [9, 91, 92] is integrated.
5. Reader according to at least one of claims 1-4, characterized in that an

aperture array [3] is arranged between the lens array [21-23] and the field lens [5].

6. Reader according to at least one of claims 1-5, characterized in that the lens array is achromatized, in that each individual lens consists of a lens group with achromatic properties.

10 7. Reader according to at least one of claims 1-6, characterized in that the detector array [6] is a CCD array or a photodiode array.

8. Reader according to at least one of claims 1-7, characterized by a modular construction with an interchangeable lens array.

9. Reader according to one of claims 1-9, characterized in that the lens array has individual lenses which are arranged with respect to each other in the formal $8 * 12$.

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10. Reader according to at least one of claims 4-9, characterized in that a dichroic mirror [8] is provided for the coupling-in of the illumination device [9].

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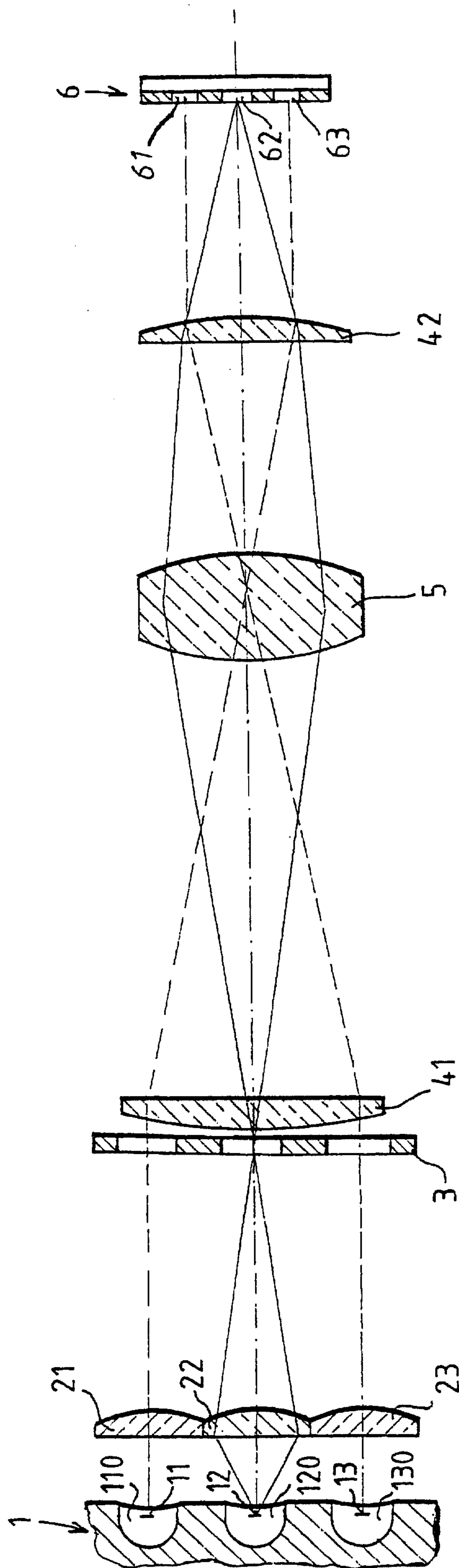
FIG. 1

FIG. 2

