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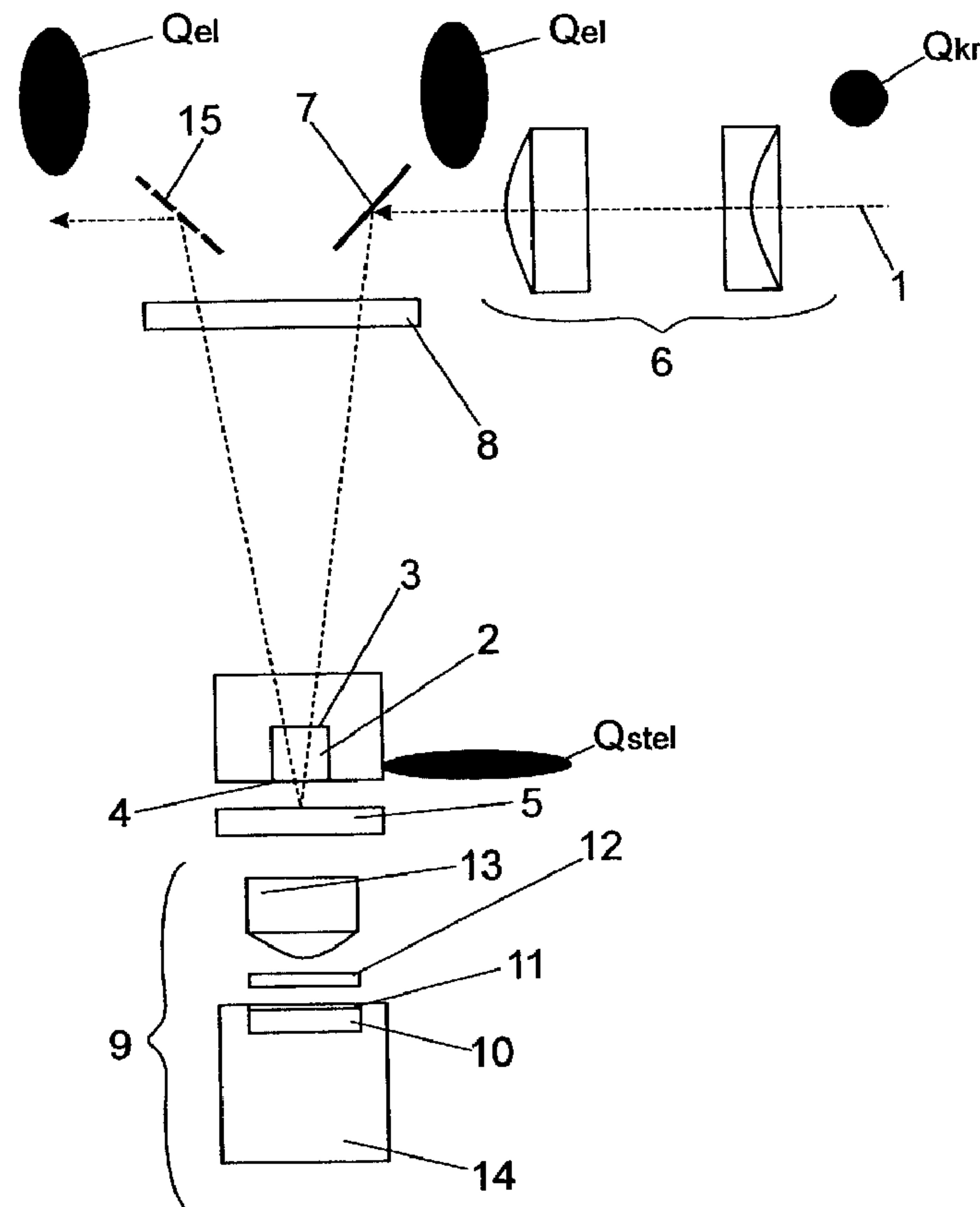
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(54) Title: DIODE-PUMPED LASER AMPLIFIER



(57) **Abrégé/Abstract:**

The object in the case of a diode-pumped laser amplifier is to increase the tolerance of the amplifier arrangement relative to variations of the input parameters significantly, so that fine-tuning is no longer necessary for guaranteeing the stability of the

(57) **Abrégé(suite)/Abstract(continued):**

amplifier. Into a laser-active solid-state medium where a thermal lens of a strength which is different in orthogonal planes is generated in consequence of the irradiated pump radiation, a laser beam to be amplified is directed into the laser--active solid-state medium while being focused in the plane with a strong thermal lens, wherein a beam waist that is being generated lies in the area of the thermal lens. The laser amplifier can be used for amplifying the radiation of an oscillator.

ABSTRACT

The object in the case of a diode-pumped laser amplifier is to increase the tolerance of the amplifier arrangement relative to variations of the input parameters significantly, so that fine-tuning is no longer necessary for guaranteeing the stability of the amplifier.

Into a laser-active solid-state medium where a thermal lens of a strength which is different in orthogonal planes is generated in consequence of the irradiated pump radiation, a laser beam to be amplified is directed into the laser-active solid-state medium while being focused in the plane with a strong thermal lens, wherein a beam waist that is being generated lies in the area of the thermal lens.

The laser amplifier can be used for amplifying the radiation of an oscillator.

DIODE-PUMPED LASER AMPLIFIER

5 The invention is directed to a diode-pumped laser amplifier with at least one laser-active solid-state medium which is permeated by the mode matched beams of a pump radiation and laser radiation to be amplified and in which a thermal lens forms because of the irradiating pump radiation whose lens strength is different in orthogonal planes.

10 It is known that in the field of solid-state lasers fundamental mode oscillators can only be scaled up to a certain output power because of the optothermal properties of the laser-active media that are being used. For the generation of a high power output, oscillators are therefore often combined with laser amplifiers arranged behind them in the beam path with which the high quality
15 of the beam of the oscillator radiation can be maintained.

 Such an oscillator-amplifier arrangement also has the advantage of making it possible to intentionally run an oscillator at relatively low power. In the case of a mode locked short pulse laser, this means that a saturable semiconductor absorber arranged inside a resonator can thus be protected from overloading.

20 Known arrangements, like, for example, the one according to US 5 237 584, have the disadvantage of having a high adjusting sensitivity. The oscillator output radiation is supplied mode matched to the multi-stage amplifier. The amplifier contains diode-pumped laser crystals with folding mirrors arranged opposite. To compensate for the strong thermal lenses forming in the crystals, a
25 highly precise tuning of the radii of curvature of the mirrors and of their distances to the laser crystals is necessary; otherwise, a stable optical system can not be guaranteed. One serious disadvantage of these serial set-ups is the fact that individual component variations must be adjusted for over and over again. Small changes, like, for example, variations of the diode parameters caused by aging or
30 other things, as well as component variations of the crystals, already lead to a system breakdown because of the very narrow tolerances.

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5 The named disadvantages are even more marked in a laser system according to US 5 696 786, since intermediate imaging elements are not used here and an opportunity for adapting the beam path with regards to the thermal lenses therefore does not exist. Such laser arrangements typically only have small operating windows when it comes to diode currents.

Alternatively, the folded beam path can also be realized in a crystal (US 5 271 031) by consecutively going through different pumped areas of this crystal a number of times. This arrangement also has the disadvantages of US 5 696 786.

10 Finally, from a longitudinally pumped solid-state laser arrangement according to DE 195 21 943, the fact is known that convex toric or cylindrical lenses can be generated spontaneously and uncontrollably by an elongated pump spot because of the isothermal field which builds up in the laser crystal and is shaped like relatively flat ellipses.

15 It is the object of the invention to increase the tolerance of the amplifier arrangement towards variations of the input parameters considerably so that fine-tuning to guarantee the stability of the amplifier is no longer necessary.

This object is met by a diode-pumped laser amplifier with at least one laser-active solid-state medium which is permeated by mode matched rays of pump radiation and laser radiation to be amplified, and in which a thermal lens is formed because of the irradiating pump radiation whose lens strength is different in orthogonal planes, and by directing the beam of the laser radiation into the laser-active solid-state medium focussed in the plane with a strong thermal lens, with the beam waist that is created lying in the area of the thermal lens.

25 For the creation of the beam waist, a focussing element like, for example, a cylindrical lens focusing in the plane of the strong thermal lens is used which is arranged in the beam path of the laser radiation at a distance to the location of the thermal lens corresponding to the element's focal length.

30 Since the distance to be established between the cylindrical lens and the laser-active medium is not a function of the thermal lens, setting the distance at the nominal focal length once is sufficient. Individual thermal lenses, like those to be found in laser-active solid-state media for amplifiers with multiple amplifier

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stages, no longer have to be taken into consideration when it comes to establishing a stable system. It has become evident that a thermal lens located in the area of a beam waist does not influence beam propagation. Contrary to prior art solutions where the influence of thermal lens effects on the beam path must be compensated for by highly sensitive adjustments, in the invention the effect of thermal lenses has
5 already been practically removed by the amplifier configuration. The laser beam undergoes a mode matching that is independent in planes with thermal lenses of differing strength. Since by this the amplification, beam quality and beam parameters of the amplifier are also insensitive to variations of the diode parameters,
10 the pump diodes realized as laser diode arrays can be operated in series in the electrical sense and at the same temperature. In contrast to prior art solutions, different thermal lenses caused by different individual diode laser characteristics and spectral properties also lose their effect and therefore do not need to be compensated for with complicated adjustments.

15 Using the invention, a compact and inexpensive amplifier can be constructed whose number of strictly modular amplifier stages is scalable since the output of each amplifier stage – with the exception of an end stage – forms the input of a subsequent amplifier stage. This provides an amplifier arrangement for which wide production tolerances of the necessary simple standard components are
20 admissible and which still only has a very low variation of the amplifier.

With the arrangement, the radiation of low-power oscillators with a mode locked operating mode can be amplified while maintaining the beam quality defined by the oscillator and determined by the times-diffraction-limit number M^2 . The construction of a serial amplifier with a high degree of stability and
25 reproducibility has been achieved. Furthermore, the use of the invention avoids having to use price-increasing beam shaping optics for the pump diodes which decrease effectivity and with which normally a rearrangement in the sense of a symmetrization of the beam parameter products for the fast and the slow axis of the diode is done.

30 Advantageously, at least one laser diode array is used as the pump radiation source for which means for the collimation of the fast axis and means for

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focusing the diode radiation in the elliptical pump focus for the generation of the thermal lens formed with different strengths in orthogonal planes are provided.

For the improvement of the beam quality of the
5 laser diode array, an additional collimation of the slow axis can also be advantageous.

For setting the polarization, a half-wave phase plate can be provided.

The pump radiation and the laser radiation are
10 directed into the solid-state medium through beam passage surfaces lying opposite to each other. Since the beam passage surface for the pump radiation is highly reflective for the wavelength of the laser radiation, the laser radiation after being reflected again passes through the
15 laser-active solid-state medium and the focusing element.

An optical element for the expansion of the laser beam in the plane where the thermal lens is weak arranged on the input side of the amplifier can be realized as a Galilean telescope with cylindrical lenses or as an
20 anamorphic prism pair.

It is advantageous if at least one image forming element is provided in the beam path of the laser radiation for the purpose of compensating the weak thermal lens in the one plane. This can either be a cylindrical mirror realized
25 as folding mirror or a spherical mirror; alternatively, a convex cylindrical lens with a long focus length or a spherical lens with a long focus length can be arranged in the beam path of the laser beam emerging from the laser-active solid-state medium.

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A Nd:YVO₄ crystal with a doping level of 0.5% can be used as the laser-active solid-state medium and pumped at a wavelength in the range from 803 nm to 809 nm.

In accordance with this invention, there is
5 provided a diode-pumped laser amplifier with at least one laser-active solid-state medium which is permeated by mode matched beams of a pump radiation and a laser radiation to be amplified and in which a thermal lens forms because of the irradiating pump radiation whose lens strength is
10 different in orthogonal planes, characterized in that the beam of the laser radiation is directed into the laser-active solid-state medium focussed in a first plane of the orthogonal planes with a strong thermal lens, wherein the beam of the laser radiation has a beam waist lying in
15 the area of the thermal lens.

The invention is subsequently to be described in more detail using the schematic drawings.

Figure 1 shows the construction of an amplifier module,

20 Figure 2 shows the beam path in the amplifier module in the sagittal plane,

Figure 3 shows the beam path in the amplifier module in the tangential plane,

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Figure 4 shows a four-stage amplifier consisting of four amplifier modules,

Figure 5 shows the profile of the beam diameter in an amplifier according to Figure 4 in the sagittal plane,

5 Figure 6 shows the beam diameter in the laser crystals of the amplifier according to Figure 4 as it depends on the strength of the thermal lens in the sagittal plane.

Figure 7 shows the beam diameter on the amplifier output of the amplifier according to Figure 4 as it depends on the strength of the thermal lens in
10 the sagittal plane,

Figure 8 shows the profile of the beam diameter in the amplifier according to Figure 4 in the tangential plane.

The amplifier module shown in Figure 1 is used for the amplification
15 of laser radiation, in particular of a collimated laser beam 1 generated by an oscillator (not shown) which in the present embodiment example has a circular beam cross-section Q_{kr} .

A laser-active solid-state medium realized as a laser crystal has two
20 opposing beam passage surfaces 3, 4 of which one is arranged directly adjacent to a pump mirror 5. The pump mirror 5 which can also be constructed as a surface coating of the beam passage surface 4 is permeable for the pump wavelength and highly reflective for the wavelength of the laser radiation. The optically active beam passage surface 3 can have an anti-reflection coating for the pump wavelength and the laser wavelength in normal incidence. The required pump wavelength for the
25 laser crystal 2 preferably realized as a Nd:YVO₄ crystal with a doping level of, for example, 0.5% lies between 803nm and 809nm. For the present embodiment example, crystals with measurements of 1 x 4 x 4 mm³ are suitable. Other crystals doped with rare earth elements apart from Nd:YVO₄ crystals can also be used.

The irradiated laser beam 1 is first expanded in a first plane, the
30 tangential plane E_{tan} , by means of a Galilean cylindrical lens telescope 6 into an elliptical beam cross-section Q_{el} with a low semiaxis ratio (expansion by a factor of 2 to 3) corresponding to the magnification factor of the telescope 6. Alternatively,

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an anamorphic prism pair can be used for this purpose. If the oscillator already supplies an elliptical laser beam, it goes without saying that in that case the beam shaping on the input side is not necessary. A first folding mirror 7 arranged further down the beam path directs the laser beam 1 through a cylindrical lens 8 which focuses the collimated laser beam 1 in the sagittal plane E_{sag} , into the laser crystal 2. The laser beam 1 still collimated in the tangential plane E_{tan} (Figure 3) permeates the laser crystal 2 mode matched to the pump beam with a strongly elliptical focus Q_{stel} . The cylindrical lens 8 is arranged at a distance to the thermal lens TL formed in the laser crystal 2 which corresponds to its focal length f_{zyl} so that the resulting beam waist lies in the area of said thermal lens (Figure 2).

After its second passage through the cylindrical lens 8, the laser beam 1 reflected by the pump mirror 5 is collimated in the sagittal plane again and has the same elliptical cross-section as before the first passage through the cylindrical lens 8.

A diode laser module 9 is provided for the generation of the pump beam and contains in a sealed housing (not shown) at least one laser diode array 10 with collimating optics 11 for the fast axis, an optional half-wave phase delay plate 12 for setting the polarization and an aspherical lens 13 for focusing the pump beam into the laser crystal 2. The optional collimation of the slow axis for the improvement of the beam quality of the laser diode array 10 is not shown. It is furthermore also possible to use a spherical lens or a lens arrangement instead of the aspherical lens 13.

The housing protects the module elements from dust, moisture, chemical fumes, electrostatic discharges and mechanical damage. The laser diode array 10 is attached to a copper body 14 serving as a heat sink by means of suitable mounting techniques.

The pump beam generated by these means is strongly elliptical like the laser beam 1, wherein the beam cross-section within the laser crystal 2 pumped quasi-longitudinally is characterized by its extension in the sagittal plane of, for example, $1\mu\text{m}$ to $500\mu\text{m}$ and in the tangential plane of, for example, 0.5mm to 3mm . Such an elliptical pump beam generates a thermal lens in the laser crystal 2 which has different strengths in the orthogonal planes E_{sag} and E_{tan} because of the

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temperature gradient which differs directionally. Thus, the focal lengths of the thermal lens can be in the range of 40mm to 200mm in the sagittal plane E_{sag} in which the fast axis of the laser diode array is also located, and in the range of 1000mm to 4000mm in the tangential plane E_{tan} . Because of its great focal length, the thermal lens in the tangential plane E_{tan} has hardly any interfering imaging function with regards to the laser beam 1 to be amplified. With an increasing focal length, this effect can be practically excluded.

A weak residual effect of the thermal lens in the tangential plane E_{tan} can also be compensated for in a simple manner by additional imaging elements arranged in the amplifier module, like, for example, by a cylindrical lens with a long focal length or a spherical lens, or also by a particular design of elements already present. For this, a second folding mirror 15 arranged in the beam path on the output of the amplifier module can be used with which the laser beam 1 can, for example, be supplied to a next amplifier stage by means of reflection. For this purpose, the folding mirror 15 (drawn with dashed lines) needs to be of a cylindrical or of a convex spherical shape and, if necessary, to be tilted correspondingly. For the use of spherical mirrors, the influence on beams in the sagittal plane E_{sag} is very small because of the great radii of curvature; this can be seen in Figure 5. The same is true for the spherical lenses with a long focal length, since in the sagittal plane E_{sag} only lenses of a short focal length determine the imaging. In each case, an independent adaptation of the modes in the tangential plane E_{tan} is possible via the setting of the lens distance in the cylindrical lens telescope 6.

If a correction of the vestigial effect of the thermal lens TL in the tangential plane E_{tan} is not required or done by correcting lenses, the second folding mirror can also be constructed as a plane mirror.

The multi-stage amplifier shown in Figure 4 contains amplifier modules whose number is adapted to the number of amplifier stages and the elements of which have the same references as those in Figure 1. The diode laser module 9 assigned to the laser crystals 2 form the pump arrangement for the amplifier. Preferably, the individual laser diode arrays 10 are operated electrically in series and at the same diode temperature.

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The laser crystal 2 provided per amplifier stage can also be assigned several laser diode arrays 10, but arrangements with several laser crystals per laser diode array can also be envisaged.

5 The means of adjustment 16 to 22 provided for the imaging elements are used for establishing an adjusted state of the amplifier. Since this state as well as the distance between the cylindrical lens 8 and the thermal lens determined by the focal length f_{zyl} are independent of the size of the strong thermal lens in the sagittal plane E_{sag} , further adaptations, in particular upon a change of the diode current, are not necessary.

10 While the mode matching in Figure 1 is only done on the input side of the amplifier module with the aid of a cylindrical lens, based on the symmetry of the arrangement, a suitable mode matching in the shape of a cylindrical lens telescope 23 can also be provided on the output, so that beams which are symmetrical to each other are created on the input and output. The laser crystals 2
15 (operated far below their breaking point) are attached to a heat sink 23 by means of suitable mounting techniques, like soldering, gluing or by being pressed into indium.

The multi-stage amplifier according to Figure 4 has the beam characteristics shown in Figures 5 to 8. Depending on the distance to the oscillator (not shown), the beam diameter of the laser beam 1 in the sagittal plane E_{sag} is
20 mainly determined by the effect that the cylinder lenses 8 have (Figure 5). The stronger the effect of the cylindrical lenses 8, the less the effect of system fluctuations. The influence of the convex spherical folding mirrors 15 is sufficiently corrected by the high focal length ratio between the long focal lengths of the mirrors in the tangential plane E_{tan} and the short focal lengths of the cylindrical lenses 9 in
25 the sagittal plane E_{sag} . The thermal lenses TL_{sag} which are strong in the sagittal plane do not interfere with the beam propagation in the laser crystal 2 (Figure 6) and on the output of the amplifier (Figure 7). In both cases, a change of the focal length of the strong thermal lenses TL_{sag} only goes with a minute variation of the beam diameters.

30 According to Figure 8, the laser beam 1 expanded in the tangential plane E_{tan} by a cylindrical lens telescope 6 passes through weak thermal lenses TL_{tan} while being corrected using the convex spherical folding mirrors. A symmetrization

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is done on the amplifier output using the cylindrical lens telescope 23. It must be noted that in the tangential plane E_{tan} the much lower pump beam quality of the slow axis is having an effect.

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CLAIMS:

1. Diode-pumped laser amplifier with at least one laser-active solid-state medium which is permeated by mode matched beams of a pump radiation and a laser radiation to
5 be amplified and in which a thermal lens forms because of the irradiating pump radiation whose lens strength is different in orthogonal planes, characterized in that the beam of the laser radiation is directed into the laser-active solid-state medium focussed in a first plane of
10 the orthogonal planes with a strong thermal lens, wherein the beam of laser radiation has a beam waist lying in the area of the thermal lens.
2. Laser amplifier according to claim 1, characterized in that an element focusing in the plane with
15 a strong thermal lens is used for creating the beam waist which is arranged in the beam path of the laser radiation at a distance equivalent to its focal length to the location of the thermal lens.
3. Laser amplifier according to claim 2,
20 characterized in that at least one laser diode array is used as the source of pump radiation which provides means for the collimation of the fast axis and means for the focusing of the diode radiation into an elliptical pump focus to generate the thermal lens whose strength varies in
25 orthogonal planes.
4. Laser amplifier according to claim 3, characterized in that an additional collimation of the slow axis is provided for the improvement of the beam quality of the laser diode array.

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5. Laser amplifier according to claim 4, characterized in that a half-wave phase plate is provided for setting the polarization.

6. Laser amplifier according to claim 5,
5 characterized in that the pump radiation and the laser radiation are directed into the laser-active solid-state medium through beam passage surfaces situated opposite to each other and in that the beam passage surface for the pump radiation is highly reflective for the wavelength of the
10 laser radiation, such that the laser radiation passes through the laser-active solid-state medium and the focusing element again after being reflected.

7. Laser amplifier according to claim 6, characterized in that an optical element is arranged in
15 front of the input of the amplifier for the expansion of the beam of laser radiation in a second plane of the orthogonal planes with a weak thermal lens.

8. Laser amplifier according to claim 7, characterized in that a Galilean telescope with cylindrical
20 lenses is used as the optical element.

9. Laser amplifier according to claim 7, characterized in that an anamorphic prism pair is used as the optical element.

10. Laser amplifier according to claim 8 or 9,
25 characterized in that at least one imaging element is provided in the beam path of the laser radiation on the output of the amplifier for the purpose of compensating the weak thermal lens.

11. Laser amplifier according to claim 10,
30 characterized in that the imaging element is a cylindrical

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mirror constructed as a folding mirror arranged on the amplifier output.

12. Laser amplifier according to claim 10, characterized in that the imaging element is a spherical mirror constructed as a folding mirror arranged on the amplifier output.

13. Laser amplifier according to claim 10, characterized in that the imaging element for the purpose of compensating the weak thermal lens is a convex cylindrical lens with a long focal length.

14. Laser amplifier according to claim 10, characterized in that the imaging element for the purpose of compensating the weak thermal lens is a spherical lens with a long focal length.

15. Laser amplifier according to claim 11 to 14, characterized in that the laser-active solid-state medium is an Nd:YVO₄ crystal with a doping level of 0.5%.

16. Laser amplifier according to claim 15, characterized in that the pump wavelength is in the range of 803 nm to 809 nm.

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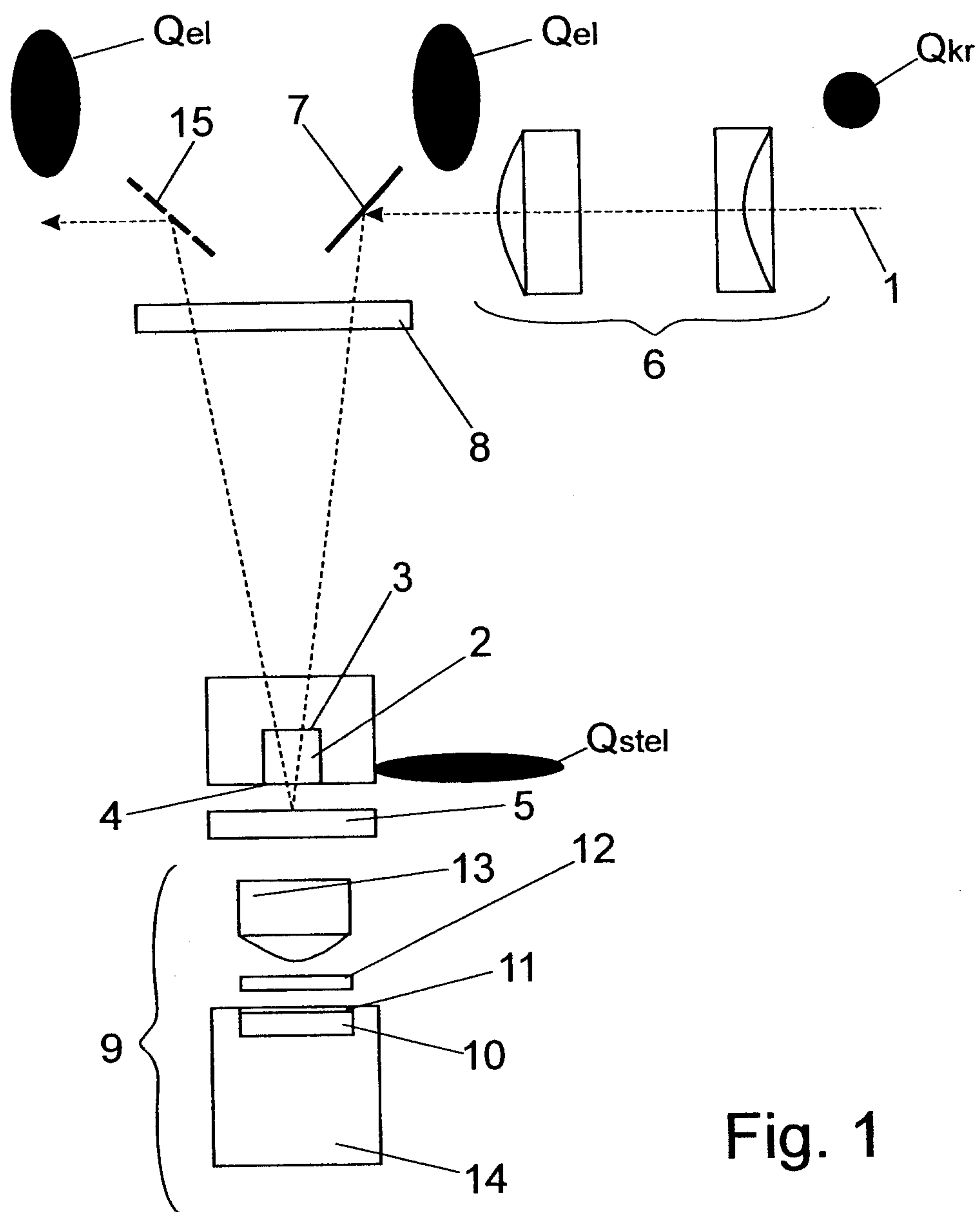


Fig. 1

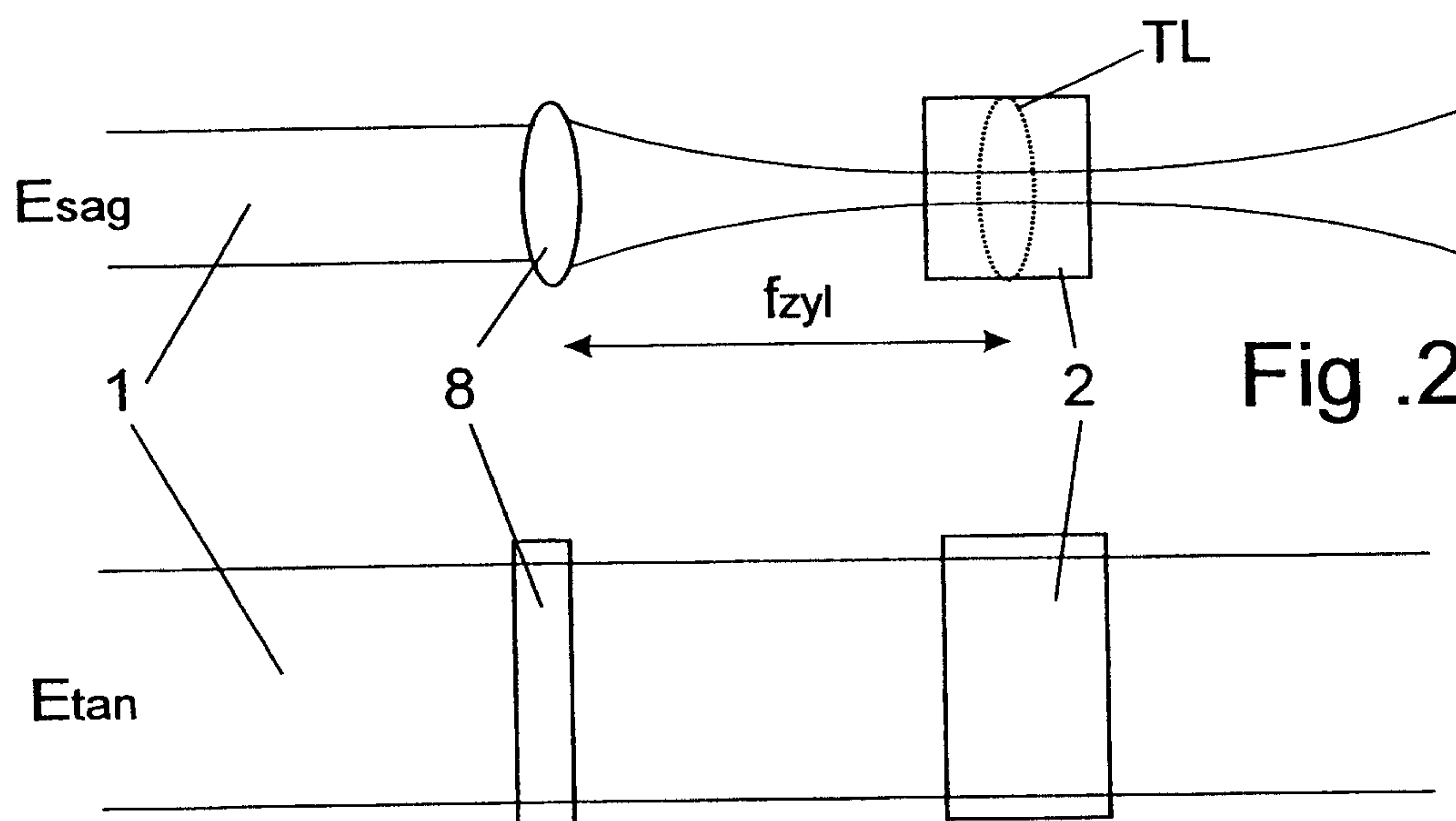


Fig .2



Fig .3

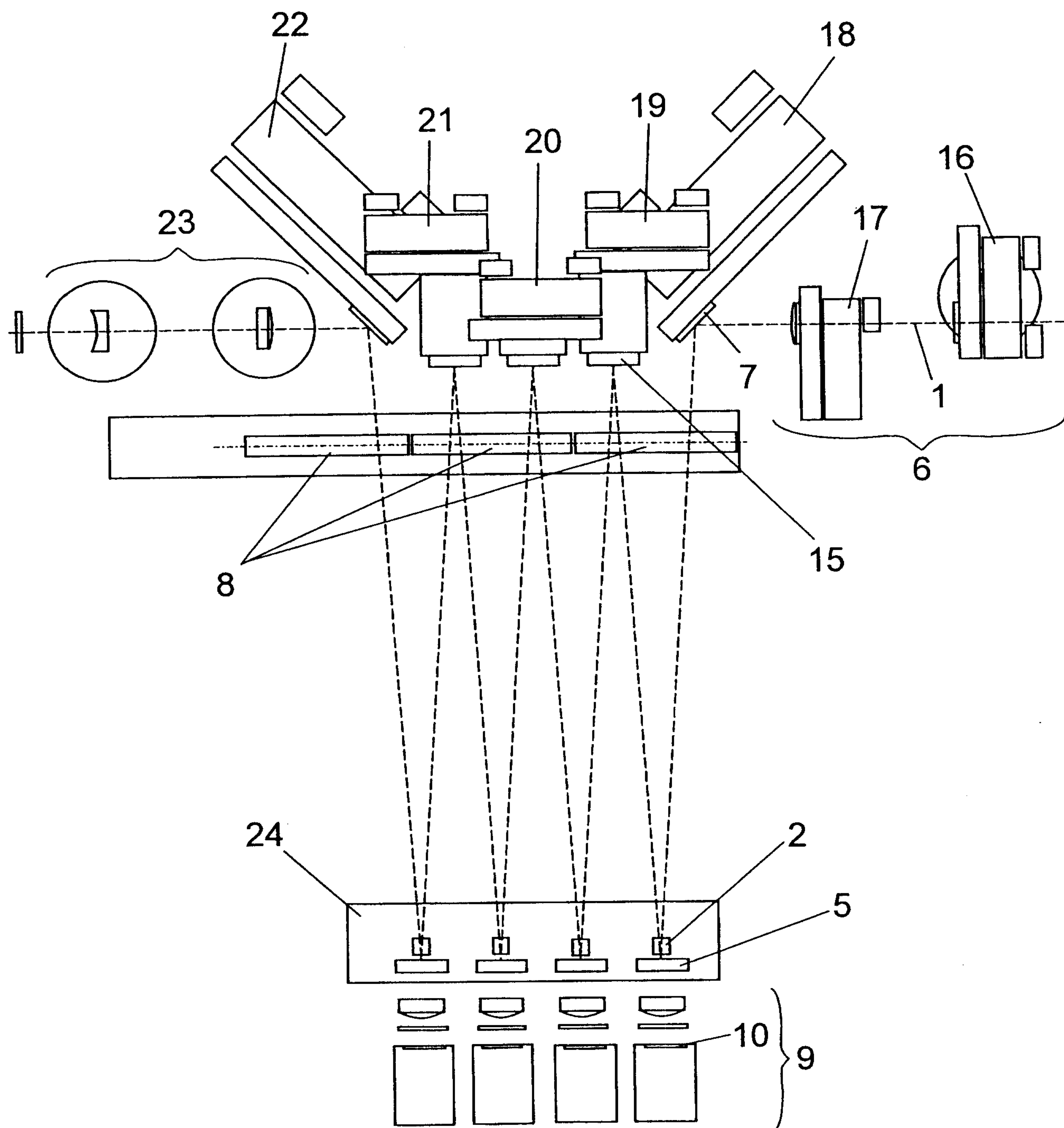


Fig. 4

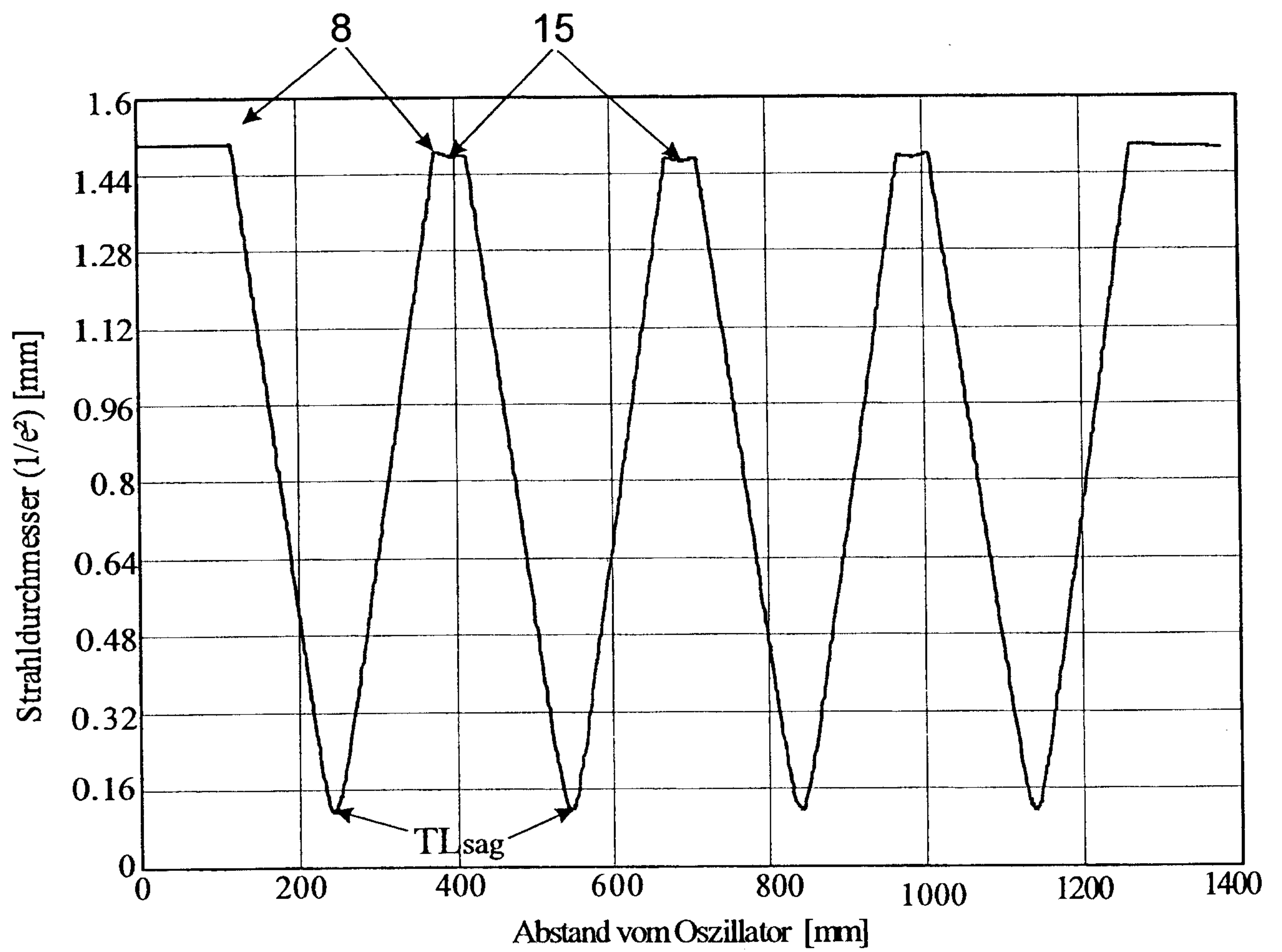


Fig. 5

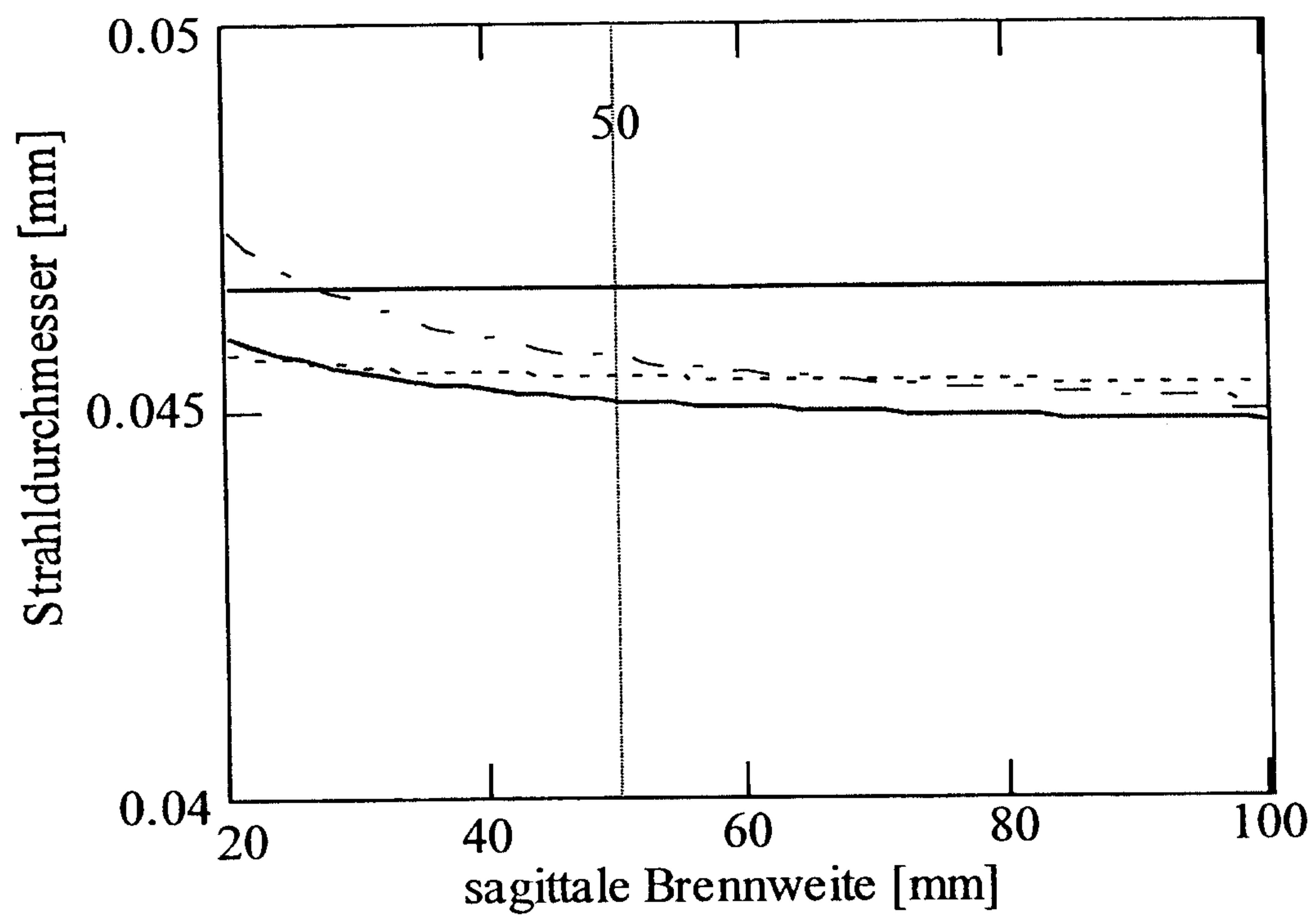


Fig. 6

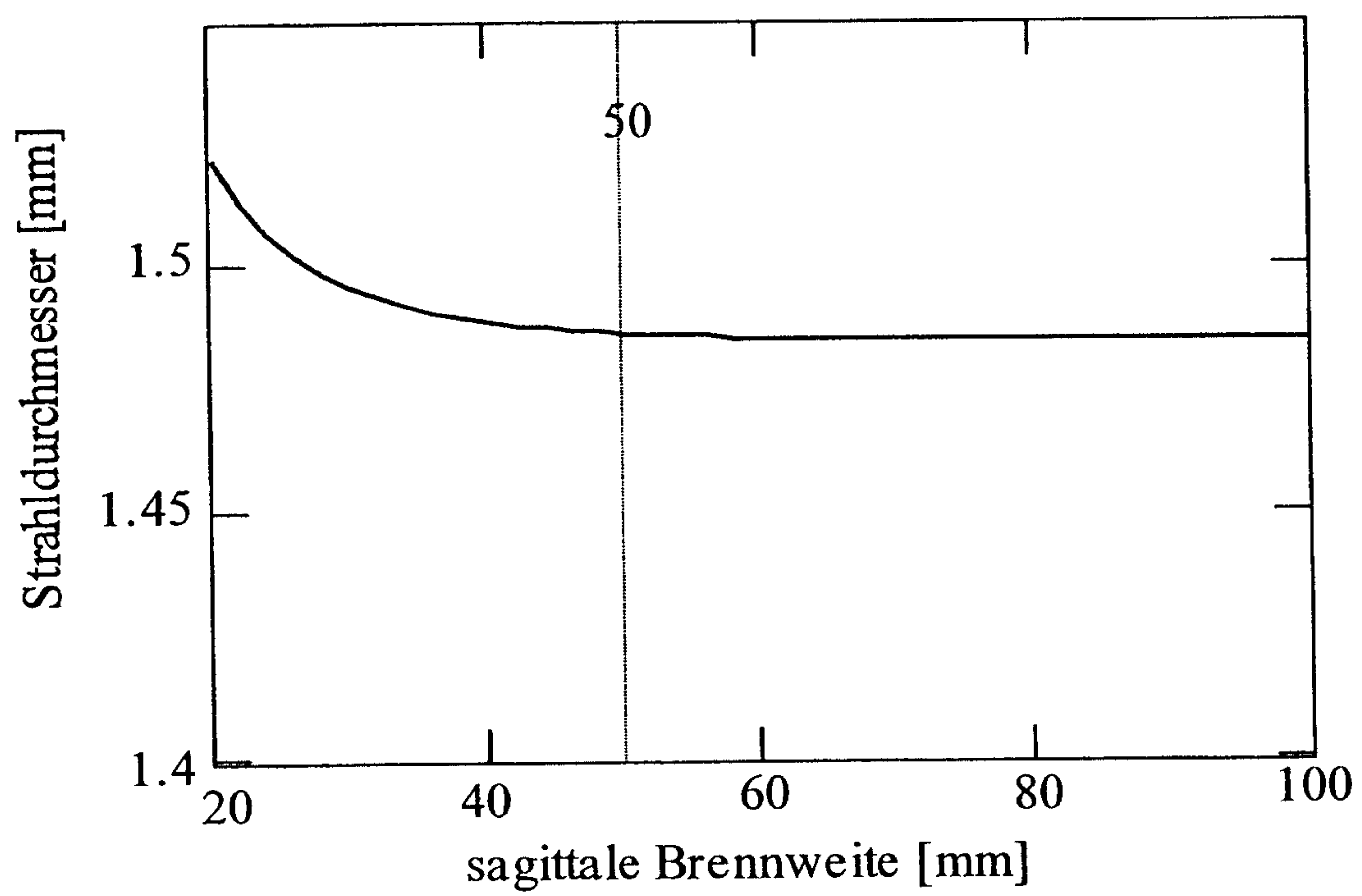


Fig. 7

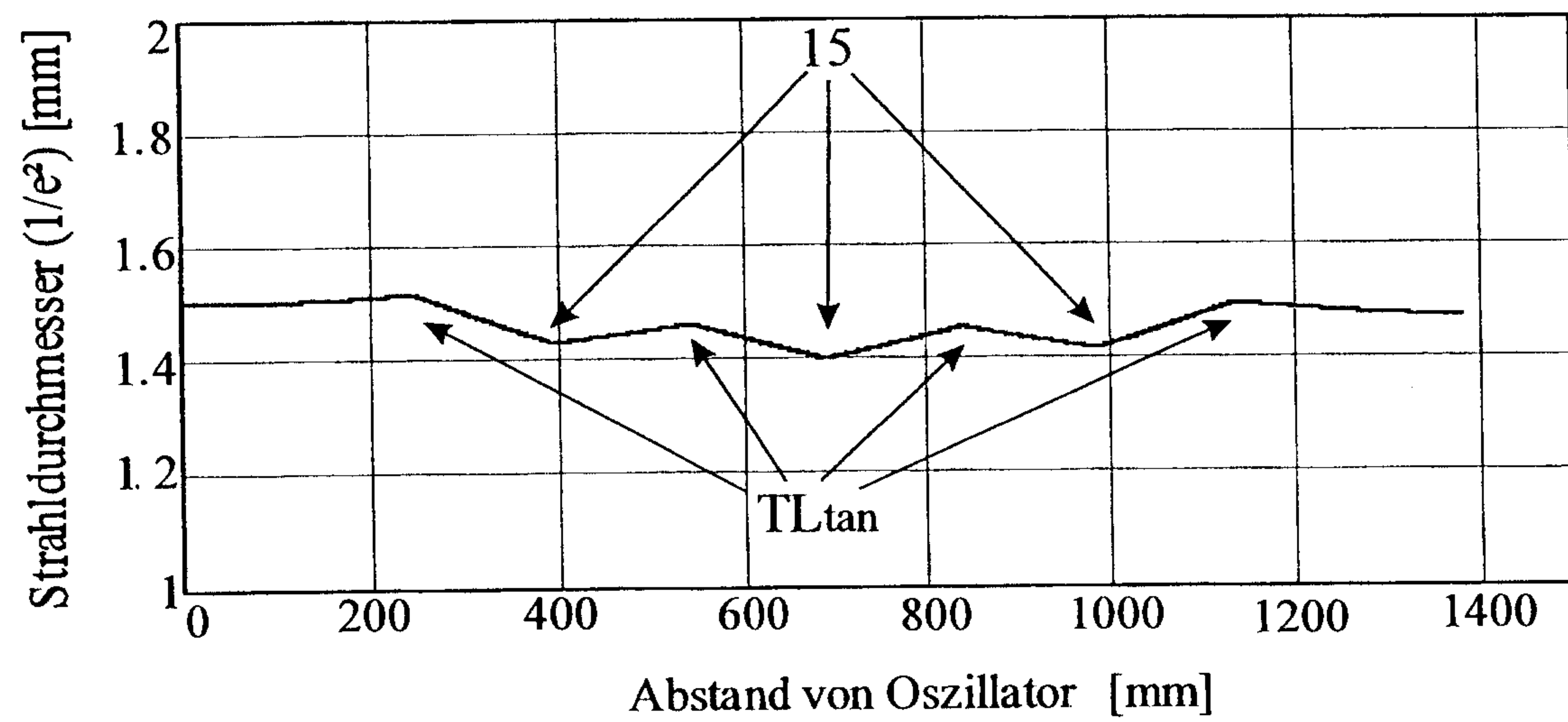


Fig. 8

