



(51) International Patent Classification:

C25B 1/04 (2021.01) C25B 3/25 (2021.01)
 C25B 1/23 (2021.01) C25B 3/26 (2021.01)
 C25B 1/27 (2021.01) C25B 9/19 (2021.01)
 C25B 1/30 (2006.01) C25B 11/042 (2021.01)
 C25B 1/50 (2021.01) C25B 15/00 (2006.01)
 C25B 3/03 (2021.01) C25B 15/031 (2021.01)
 C25B 3/07 (2021.01) C25B 15/033 (2021.01)

(21) International Application Number:

PCT/EP2024/065202

(22) International Filing Date:

03 June 2024 (03.06.2024)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

23177314.4 05 June 2023 (05.06.2023) EP

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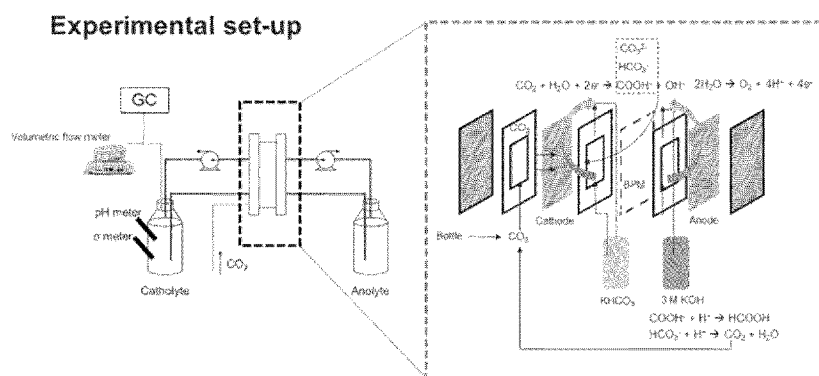
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(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CV, CZ, DE, DJ, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IQ, IR, IS, IT, JM, JO, JP, KE, KG, KH, KN, KP, KR, KW, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, MG, MK, MN, MU, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, WS, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, CV, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SC, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, ME, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

(54) Title: RE-ACTIVATION PROCESS OF GAS DIFFUSION ELECTRODE

Figure 1



(57) Abstract: The present invention relates to a method of re-activation and long-term stable operation of a metal based gas diffusion electrode (GDE), and the use thereof in the electrocatalytic conversion of gaseous reactants into economically interesting reaction products. Using the operational method of the present invention such metal based GDEs, and in particular carbon free metal based GDEs are particularly useful in the electrochemical conversion of gaseous reactants such as CO₂, CO, N₂, or O₂ into bulk chemicals and fuels such as Syngas, Formic Acid, Methanol, Ethanol, Ethane, Ethylene, Methane, Ammonia, and the like for durable operation (> 1000 hours).

Declarations under Rule 4.17:

- *as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))*
- *as to the applicant's entitlement to claim the priority of the earlier application (Rule 4.17(iii))*

Published:

- *with international search report (Art. 21(3))*
- *in black and white; the international application as filed contained color or greyscale and is available for download from PATENTSCOPE*

RE-ACTIVATION PROCESS OF GAS DIFFUSION ELECTRODE

FIELD OF THE INVENTION

The present invention relates to a method of re-activation for long-term stable operation of a metal-based gas diffusion electrode (GDE) in the electrocatalytic conversion of gaseous reactants into economically interesting reaction products. Using the operational method of the present invention such metal based GDE's, and in particular, carbon free metal based GDEs are particularly useful in the electrochemical conversion of gaseous reactants such as CO₂, CO, N₂, NO_x or O₂ into bulk chemicals and fuels such as Syngas, Formic Acid, Methanol, Ethanol, Ethane, Ethylene, Methane, Ammonia, Hydroxylamine, Hydrogen Peroxide and the like.

BACKGROUND TO THE INVENTION

A GDE is a combination of porous structures exhibiting a hydrophilic and a hydrophobic side. It is generally composed of a catalyst layer (CL), a gas diffusion layer (GDL) and optionally a current collector (CC) as shown in Figure 1. A GDE allows the direct supply of gases via the hydrophobic side to the liquid medium where electrochemical processes take place. Because of their low mass transfer resistance, the use of GDEs is promising for electrochemical processes with gaseous reactants since they overcome the poor mass transport of gases that have a limited solubility, towards the electrode. Because of their high porosity, GDEs have a reactive surface area much larger than their geometrical area (projected surface area), which is favorable for the process productivities. The GDL is a porous medium that facilitates transport of gaseous reactants to and gaseous products from the CL and consists of a macro/meso/nano-porous layer either with or without a micro-porous layer (MPL). A wide variety of GDL parameters have been investigated to enhance electrolyzer or fuel cell performance (Omrani R, Shabani B (2017) **Gas diffusion layer modifications and treatments for improving the performance of proton exchange membrane fuel cells and electrolyzers: A review.** Int J Hydrogen Energy 42:28515–28536. doi: 10.1016/j.ijhydene.2017.09.132).

The concept of CO₂ Conversion and Utilization (CCU) is considered a promising alternative method for mitigating excess greenhouse gases. Electrochemical CO₂ reduction (ECR), when powered by renewable energy sources, could be an essential tool in achieving CCU at a large scale. The products obtained from ECR (supra) are pivotal in chemical feedstock/building blocks or fuels. To promote ECR effectively, gas diffusion electrodes (GDEs) were designed to promote the three-phase boundary, increasing the reaction sites for ECR, thereby decreasing the overall wastage of CO₂ gas and increasing the valuable product yield with better Faradaic and energy efficiency.

The industrial or large-scale implementation of ECR is currently however hindered by moderate current densities, large cell potentials (thus low energetic efficiency) and poor stability of the

electrode activity. For industrial or large-scale implementation, a qualified electrode must fulfill the requirements of 1) sufficiently high current density and 2) stable and significantly high Faradaic Efficiency (FE) towards the targeted product. For instance, industrial relevant production of formic acid requires electrodes with a current density of at least 100 mA/cm² and an FE of 70 ± 10%. Over time, the present electrodes for ECR of CO₂ fail in providing stable long-term operation (≥1000 h) for electrochemical conversion activity.

Current efforts to arrive at such qualified electrodes are based on carbon based GDEs on which metals catalysts are inked or electrodeposited. Agarwal et. al. (**Patent no. US10273587B2**) for example patented a method and making of Sn-Carbon (Sn-C) particles deposited on carbon fibre for ECR. The inventors claimed three different methods for preparing the Sn-C particles, which is then claimed to have a FE of 95% for formate ions operated for 100 h.

Zhai et. al in 2017 (**patent no. US10253420B2**), claimed an electrochemical process for ECR. In this patent, inventors claimed the deposition method of Sn onto carbon fiber paper (CFP), preparing porous Sn-CFP electrodes for ECR activity. The long-term activity of this Sn-CFP electrode is however hindered due to graphite deposition on the electrode surface while operating the electrode for 20 h with a current density of 10 mA/cm² (10 times lower than the proposed commercially relevant current density of 100 mA/cm²). Using combination of deep cathodic polarization (DCP) and anodic polarization (AP) the deposited graphite from Sn-CFP electrodes could be removed, extending the operation time of a cell with the Sn-CFP up to 200 h.

The well known electrocatalyst CO₂ to formic acid conversion includes Sn, Bi, In or alloys of these metals. These metal based GDE's have not shown promising results in long-term operation (≥ 1000 h), as required for industrial set-up (**Van Daele, K., De Mot, B., Pupo, M., Daems, N., Pant, D., Kortlever, R. and Breugelmans, T., 2021. Sn-based electrocatalyst stability: a crucial piece to the puzzle for the electrochemical CO₂ reduction toward formic acid. ACS Energy Letters, 6(12), pp.4317-4327**). For example in case of Sn-based electrode, deactivation or degradation of the electrode is observed which can be associated with changes in the electrode's surface and local environment during the electrolysis process. The way the GDE is prepared and the cell configuration also significantly impacts the electrode's stability towards the long-term operation by increasing the overall cell resistance, mode of gas supply, depending on whether the cell is H-Cell, flow cell or zero-gap configuration (**Liniker de Sousa, Nieck E. Benes, and Guido Mul, ACS ES&T Engineering 2022 2 (11), 2034-2042 and Kevin Fernández-Caso, Guillermo Díaz-Sainz, Manuel Alvarez-Guerra, and Angel Irabien ACS Energy Letters 2023 8 (4), 1992-2024**).

The problem of Sn-GDE's long-term operation has been discussed numerous times. The main remedies reported involve modifying the catalyst by adding a dopant or incorporating a bimetallic system. In 2006, Oloman and Li (**patent no. US20080223727A1**) for example invented a process method for ECR, including a reactor-type design with Sn/Sn-based alloys in a granular form as working electrodes.

The aforementioned claim is about the set-up /design of the reactor, including the electrodes used in the form of Sn-doped granules comprising of Sn/Sn-Zn alloy. Still, even with these Sn-granule as cathode, the formate FE is dropped from 60% to 45% in ~4 h of operation. The cathode activity is recovered by combining two methods: 1) chemical method treating Sn-granules with 11 wt% nitric acid and 2) Polarity reversal, with 1 A applied for 5 minutes.

Although this method of catalyst modification and cathode recovery produced some encouraging results in short-term experiments (a 1-100 hours), it is not applicable to industrial applications as it will require the electrodes to be replaced after short duration and hence will negatively impact the economics/profitability of the process. It has not made much progress toward solving the original problem of the long-term operation of Sn-based electrodes (**Al - Tamreh, S.A., Ibrahim, M.H., El - Naas, M.H., Vaes, J., Pant, D., Benamor, A. and Amhamed, A., 2021. Electroreduction of carbon dioxide into formate: A comprehensive review. ChemElectroChem, 8(17), pp.3207-3220**). Moreover, the requirement of an electrode with a larger surface is not a preferred option due to electrode integrity (mechanical strength) of the large GDE, maintaining a uniform current distribution and the leakproof nature of the GDE (**Perry, S.C., de León, C.P. and Walsh, F.C., 2020. The Design, Performance and Continuing Development of Electrochemical Reactors for Clean Electrosynthesis. Journal of The Electrochemical Society, 167(15), p.155525**).

Despite the progress made, it is still a challenge to ensure the operation stability of the system and, in particular, the stability of the electrocatalyst, which it is often degraded or poisoned. Thus, for example, in the electrochemical reduction of CO₂ to obtain formic acid or other organic compounds, the activity of CO₂ conversion of some electrocatalysts (e.g. Pd) can be significantly reduced after a short period of time, due to the adsorption of the poisoning byproduct CO, which blocks the active sites of the electrocatalyst.

Poisoning of Pd catalyst by CO is for example well known in the state of the art, but most of the works related to this catalyst for CO₂ reduction try to solve this problem working at very low overpotentials, thus at very low current densities. This approach however, is not useful in industrial terms as the production rate will be very small, and it has been observed that attempts to increase the current density by applying a larger overpotential resulted in H₂ production. In

US patent publication US 2021/115576, the positioning of the Pd catalyst is resolved by operating the electrochemical cell in a direct mode for the CO₂ reduction and in a second reverse mode for a time sufficient to conduct the desorption and the consequent removal of the byproduct species generated and adsorbed onto the surface of the cathodic material during the direct EC operation mode. Still, the method disclosed in US 2021/115576 cannot prevent the degradation of the catalyst and yield a long term operation with high FE.

It has been the object of the present invention to address the foregoing problem in developing an operational method that combines the intrinsic properties of the electrolyte used and changes occurring at electrode/electrolyte interface due to inducing polarity changes at the electrode. The process has been demonstrated with the carbon-free Sn-GDE (the detail of which is described in **WO2022013042A1** – incorporated herein by reference), previously developed by the present applicant as well as with Bismuth (Bi) GDE and is being extended to alloys like Sn-Bi, Ag-Cu. As will be apparent from the examples hereinafter, in the methods of the present invention the combination of controlling the pH of the electrolyte and applying a pulse with a current density and pulsing period that is correlated to the surface area and catalyst loading, an in situ regeneration of the catalytic surface is achieved, more specifically by oxidizing the catalyst to its oxide form which is the key to regenerate the selectivity. More importantly, our method guarantees a much longer-term stabilization effect, which is in the time scale of 1 hours to 24 hours.

SUMMARY OF THE INVENTION

The present invention is directed to a method of operating an electrochemical cell comprising a metal based GDE as working electrode, a counter electrode, and an electrolyte in the electrochemical conversion of a gaseous reactant into bulk chemicals at the working electrode, said method of operation being characterized in maintaining the pH of the electrolyte within a useful range of 2 units of its initial value, and in applying an inverse electrical pulse at regular intervals to the metal based GDE working electrode which is the electrode where the electrochemical reaction of interest occurs.

Per reference to examples herein provides, in an embodiment the metal based GDE working electrode is used in the reductive conversion of gaseous reactants into bulk chemicals, such as the electrochemical CO₂ reduction into formic acid; In such instance the GDE working electrode is the cathode, and the inverse electrical pulse will be an anodic pulse.

Hence in an embodiment the present invention provides a method of operating an electrochemical cell comprising a metal based GDE working electrode as cathode, an anode, and an electrolyte in the electrochemical conversion of a gaseous reactant into bulk chemicals

at the working electrode, said method of operation being characterized in maintaining the pH and conductivity of the electrolyte within a range of 2 units of its initial value, and in applying an anodic pulse to the working electrode at regular intervals.

- 5 In an embodiment of the method according to the invention the electrochemical cell comprises an anode and a cathode compartment and wherein the method is characterized in maintaining the pH of the catholyte within a range of 2 units of its initial value, and in applying an inverse electrical pulse, in particular an anodic pulse to the GDE working electrode at regular intervals.
- 10 In an embodiment of the method according to the invention the anodic pulse applied to the working electrode (GDE) consists of a current of 50-200 mA cm⁻², preferably applied for at least 30 seconds; in particular a current of at least 100 mA cm⁻², preferably applied for at least 1 minutes.
- 15 In an embodiment of the method according to the invention the anodic pulse consists of a charge of 1.5-10 Coulomb @ cm⁻² applied to the working electrode (GDE); in particular a charge of at least 6 C cm⁻² applied to the working electrode (GDE).

- 20 In a method according to any one of the preceding embodiments wherein the anodic pulses are applied at intervals selected to maintain a sufficiently high current density and stable and significantly high Faradaic Efficiency (FE) towards the targeted product. In an embodiment the pulses are applied at intervals to maintain or restore the Faradaic Efficiency (FE) towards the targeted product within a window of 20% of its initial value before pre-pulsing. In an embodiment the anodic pulses are applied to the cathode at regular intervals, such as every hour, every 2
 - 25 hours, every 3 hours, every 4 hours, every 5 hours, or longer duration. In an embodiment the anodic pulses are applied to the cathode at intervals starting at 6 hours, in particular starting at 12 hours, more in particular, starting at 24 hours, even more in particular every 48 hours.

- 30 In a method according to any one of the preceding embodiments wherein the gaseous reactant is selected from CO₂, CO, N₂, NO_x or O₂; in particular CO₂.

- In a method according to any one of the preceding embodiments wherein the bulk chemicals are selected from Syngas, Formic Acid, Methanol, Ethanol, Ethane, Ethylene, Methane, Ammonia, Hydroxylamine, Hydrogen peroxide and the like.

- 35 In a method according to any one of the preceding embodiments wherein the electrolyte is selected from KHCO₃, NaHCO₃, K₂CO₃, Na₂CO₃, KCl, NaCl, K₂HPO₄, KH₂PO₄, Na₂HPO₄, NaH₂PO₄, H₂SO₄, HClO₄, H₃PO₄ and K₂SO₄, K₃PO₄, Na₂SO₄, NaClO₄, Na₃PO₄, KOH, NaOH; in a particular embodiment the electrolyte is selected from KHCO₃ (0.5 – 2 M), H₂SO₄ (0.05 – 0.5

M) and K_2SO_4 (0.5 - 1 M).

In a method according to any one of the preceding embodiments wherein the pH is maintained near to the original pH of the electrolyte (slightly alkaline, in particular from about 7 to 9 or acidic, in particular from about 0 to 5).

BRIEF DESCRIPTION OF THE DRAWINGS

- Figure 1. Experimental set-up for long-term duration testing of metal based GDE.
- 10 Figure 2. FE of formate/formic acid, CO and H_2 during 1000-hour operation using Sn GDE. The solid blocks are obtained from GC measurement and black dots are results of FE of formic acid calculated from HPLC measurement of the formic acid concentration in the catholyte.
- Figure 3. pH of the catholyte solution throughout the experimental period. Four bottles of the 0.5 M $KHCO_3$ are used during the experiment and the change of catholyte is indicated by dashed lines in order to mimic continuous single pass operation.
- 15 Figure 4. Anodic pulse for reactivation of electrode.
- Figure 5. Applied current density plot for the Sn-GDE in a flow cell over 1000 h operation
- Figure 6. Schematics of flow-through mode of cell operation. 1. Blocked outlet of gas chamber - 2. Outlet for catholyte - 3. Catholyte chamber - 4. Inlet of catholyte - 5. GDE - 6. Gas inlet - 7. Gas chamber.
- 20 Figure 7. Changes in working electrode potential (E_{WE}) of Sn-GDE during 1000 h operation.
- Figure 8. FE of formate/formic acid, CO and H_2 during 320-hour operation using Bi GDE. The solid blocks are obtained from GC measurement and black dots are results of FE of formic acid calculated from HPLC measurement of the formic acid concentration in the catholyte.
- 25 Figure 9. Fig 9 A. Plot of current during pulsing and its impact – Fig.9 B on the Faradaic efficiency of the formic acid from CO_2 electrochemical reduction using Bi GDE.
- Figure 10. Schematics of H-cell
- 30 Figure 11. Impact of anodic pulsing on Sn-foil electrode
- Figure 12. FE of formate/formic acid, CO and H_2 during 780-hour operation using Sn GDE conducted in acidic catholyte. The dotted vertical line represents the changing of the catholyte reservoir.

35 DETAILED DESCRIPTION OF THE INVENTION

This invention encompasses a stable ECR process using a metal-based Gas Diffusion Electrode (GDE), specifically for the electrochemical conversion of CO_2 , such as for example to formate/formic acid. The electrochemical CO_2 reduction (ECR) by metal-based GDE, such as Bi/Sn-GDE, In, Zn, and the like as working electrode well known. However, and as mentioned

herein before, these electrodes have been prone to failure for stable long-term operation (≥ 1000 h) for ECR activity, which hampers industrial application. In order to have an industrially relevant ECR catalyst, it should convert CO_2 into bulk chemicals such Formic Acid, Methanol, Ethanol, Ethane, Ethylene, Methane and the like with a commercially viable current density, having a stable and significantly high energy efficiency and yield. Failing to meet these criteria might have a severe economic impact, hence the urgency to solve the problem. In this invention, we have developed a process method to incorporate metal based GDEs for improved ECR performance.

In this invention, we have addressed this pressing and critical issue of long-term stability of electrocatalyst for CO_2 reduction and invented a method to reactivate the metal based-GDE long-term operation (≥ 1000 h). The present invention provides a method (process) and equipment needed to increase the metal-based GDEs' longevity and stability to increase the Faradaic efficiency (FE), when used in a electrochemical cell for ECR activity. This is imperative to get an overall energy efficient process as well. The process combines the intrinsic property of the electrolyte used, and changes occurring due to inducing the polarity change at the electrode to achieve the aforementioned claim and was found particularly useful for carbon free metal-based GDEs, such as the carbon free Sn-GDE disclosed in the earlier patent application of the applicant WO2022013042A1.

Thus, in an aspect of this invention, a carbon-free metal-based GDE is used; in particular a carbon free Sn-GDE; even more in particular the carbon-free Sn-GDE electrode prepared using the methodology as disclosed in patent no. WO2022013042A1.

The equipment as used, generally refers to an electrochemical cell comprising a metal based GDE working electrode as cathode, an anode, in particular an inert anode, such as an inert Pt anode, and an electrolyte, whereby a gas is fed into the GDE with electrolyte permeating the opposite side of the GDE, said cell being used for causing current to flow externally through a load circuit connecting the anode and the cathode. As is known to the skilled artisan, in electrochemical cells comprising GDEs the anode and cathode compartments are typically separated by means of ion-conducting membranes such as anion exchange membrane (AEM), Cation exchange membrane (CEM) or bipolar membrane (BPM), wherein each of the anode compartment and the cathode compartment respectively comprise an anolyte and a catholyte solution.

The method according to the invention of operating such equipment in the electrochemical conversion of gaseous reactants such as CO_2 , CO, N_2 , or O_2 into bulk chemicals and fuels such as Syngas, Formic Acid, Methanol, Ethanol, Ethane, Ethylene, Methane, Ammonia, and the like; is characterized in maintaining the pH of the electrolyte within a range of 2 units of its initial value, and in applying anodic pulsing to the GDE working electrode, i.e. the cathode, at regular

intervals. In said instances where the electrochemical cell comprises an anode and a cathode compartment, the method is characterized in maintaining the pH of the catholyte within a range of 2 units of its initial value, and in applying anodic pulsing to the GDE working electrode, i.e. the cathode, at regular intervals.

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As will be evident from the examples hereinafter, the electrocatalytic instability and observed deactivation or degradation of the metal-based GDEs can be associated with changes in the electrode's intrinsic property and its local environment (such as the concentration of K^+ , $HCOO^-$, CO_3^{2-} , etc.) during the electrolysis process. For example, in case of Electrochemical CO_2 Reduction (ECR), the observed decrease in formate ion production at the GDE cathode is directly associated with a drop in pH of the catholyte, which favours the competing hydrogen evolution reaction (HER). Controlling the pH of the catholyte and maintaining it within 2 units, in particular within 1 unit from its initial value, i.e., the pH value of the pristine catholyte at the operational start of the electrochemical process, counteracts such reaction to occur.

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In itself this operational condition can prevent the Faradaic efficiency (FE) to drop below 40%, but is insufficient to restore the FE to values close to initial value, i.e. the FE at the operational start of the electrochemical process. The Faradaic efficiency (FE) describes the selectivity of an electrochemical process towards a specific target product and is defined as the amount (moles) of collected product relative to the amount that could be produced from the total charge passed, expressed as a fraction or a percentage.

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Combining pH control of the catholyte with an anodic pulsing at the cathode restores the FE yield of the process to its initial value. Please note in this respect, that within the context of the present invention "the anodic pulse" is meant to refer to an inverse current or potential pulse applied to the working electrode, i.e. the electrode in the electrochemical system on which the reaction of interest is occurring. Depending on whether the reaction on the electrode is a reduction or an oxidation, the working electrode is called cathode or anode, respectively. In the present examples, the GDE working electrode is the cathode, but the invention is not restricted thereto.

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The pulse is inverse with respect to its operational charge in the electrochemical conversion of the gaseous reactant into bulk chemicals at the working electrode. For example, during ECR, a negative potential (reducing current) is applied to the GDE working electrode and the anodic pulse will consist of a positive (inverse) potential (oxidizing current) applied to the GDE working electrode.

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In an embodiment of the method according to the invention the anodic pulse consists of a current of 50-200 $mA\ cm^{-2}$, preferably applied for at least 30 seconds; in particular, a current of at least 100 $mA\ cm^{-2}$, preferably applied for at least 1 minutes to the GDE working electrode (cathode). In an embodiment of the method according to the invention the anodic pulse consists of a

constant current of 50-200 mA cm⁻², preferably applied for at least 30 seconds; in particular a constant current of at least 100 mA cm⁻², preferably applied for at least 1 minutes to the GDE working electrode (cathode).

- 5 In an embodiment of the method according to the invention the anodic pulse consists of a positive charge of 1.5-10 Coulomb (C) cm⁻² applied to the cathode; in particular a charge of at least 6 C cm⁻² applied to the cathode. In an embodiment of the method according to the invention the anodic pulse consists of a constant charge of 1.5-10 Coulomb (C) cm⁻² applied to the cathode; in particular a constant charge of at least 6 C cm⁻² applied to the cathode.

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- In an embodiment of the method according to the invention the anodic pulse consists of a current of 50-200 mA cm⁻², preferably applied for at least 30 seconds; in particular a current of at least 100 mA cm⁻², preferably applied for at least 1 minutes, in particular up to about 10 min, more in particular from about 4 to 8 min, to the cathode, wherein said anodic pulse is applied at regular intervals starting at 6 hours, in particular starting at 12 hours, more in particular starting at 24 hours, even more in particular every 48 hours. In an embodiment of the method according to the invention the anodic pulse consists of a constant current of 50-200 mA cm⁻², preferably applied for at least 30 seconds; in particular a constant current of at least 100 mA cm⁻², preferably applied for at least 1 minutes, in particular up to about 10 min, more in particular from about 4 to 8 min, to the cathode, wherein said anodic pulse is applied at regular intervals starting at 6 hours, in particular starting at 12 hours, more in particular starting at 24 hours, even more in particular every 48 hours.

- 25 In an embodiment of the method according to the invention the anodic pulse consists of a charge of 1.5-10 Coulomb (C) cm⁻² applied to the cathode; in particular a charge of at least 6 C cm⁻² applied to the cathode, wherein said anodic pulse is applied at regular intervals starting at 6 hours, in particular starting at 12 hours, more in particular starting at 24 hours, even more in particular every 48 hours. In an embodiment of the method according to the invention the anodic pulse consists of a constant charge of 1.5-10 Coulomb 1.1.5-10 Coulomb (C) cm⁻² applied to the cathode; in particular a constant charge of at least 6 C cm⁻² applied to the cathode, wherein said anodic pulse is applied at regular intervals starting at 6 hours, in particular starting at 12 hours, more in particular starting at 24 hours, even more in particular every 48 hours.

- 35 Alternatively, the anodic pulse can be expressed as the magnitude of electrical charge, i.e., 6 C cm⁻² applied to the cathode. With reference to the examples, it has been observed that a charge in the range of 15-60 C is not enough to increase the FE to its initial value. Without being bound to theory, where this charge is enough to change the polarity around the double-layer charging area that is majorly impacted, the recovery of FE obtained by such a small charge (15-60 C) does not have a lasting impact on the electrode's selectivity for ECR. Only a small increase of

10-15% in FE is observed, which drops to its pre-pulsing value within 24-48 h. In contrast, the FE increases by 20 to 30% at a charge between 240 C and 360 C, which has a long-lasting impact on the electrode's ECR selectivity. It is hypothesized that such high charge value is enough to oxidise the metal catalyst present within the GDE, for example from Sn metal to SnO₂, and that it also removes any impurities deposited on the electrode during the long-term process, working also as a cleaning method for the electrode. When for example the Sn-GDE is subjected to cathodic potential post the anodic pulse as herein disclosed, it reduces back to metallic tin, making the electrode more porous, increasing the three-phase interphase, and increasing the FE of formate.

The combination of maintaining catholyte pH and conductivity (condition I) and anodic pulsing (condition II), helps to restore the initial selectivity of the electrode towards ECR and operate the electrochemical cell for the duration of at least 1000 h and beyond. At any moment, failing to comply with these conditions (conditions I and II) can lead to a drop in the selectivity of the electrode's activity towards ECR.

To sum up, metal-based GDEs and in particular Bi-GDE or Sn-GDE can be reactivated to its initial form/activity, by the combined effect of condition I, i.e. keeping the electrolyte pH within 2 units from its initial pH, more in particular keeping the electrolyte, even more in particular keeping the catholyte at a slightly alkaline (pH from about 7 to 9) pH, and condition II, with anodic pulses for a few minutes (4-8 minutes) at a fixed interval of 48 h to prolong the Sn-GDE activity towards ECR. In an embodiment condition II, is expressed as anodic pulse with a charge of at least 120 Coulomb (C); in particular an anodic pulse with a charge of at least 240 C; more in particular an anodic pulse with a charge up to about 600 C; even more in particular with an anodic pulse from about and between 240 C to 360 C.

EXAMPLES

With the experimental set-up (Figure 1) mentioned in example 1, an electrochemical cell for Electrochemical CO₂ reduction (ECR) comprising a Sn-GDE as disclosed in WO2022013042A1 is initially stable for 200 h, at a current density of 100 mA/cm². The stability of the electrode is expressed in terms of the Faradaic efficiency (FE) of formate ions produced from ECR. After 500 h of operation, the FE of formate drops from 75% to 25% (Figure 2). The constant decrease in the FE of formate ions could be directly associated with the drop in pH of the catholyte, which favours HER, a competing reaction with ECR (Figure 3). To suppress HER and promote ECR, refreshing the electrolyte with fresh 0.5 M KHCO₃, bringing the pH back to its initial value of 7.5, increases the FE of formate from 25% to 40%. Furthermore, this change in FE is stable if the catholyte's pH values are 7.0 ± 0.5 , and conductivity is $\geq 45 \pm 5$ mS/cm. An anodic pulse is then applied to the cathode, as shown in Figure 4, to restore the electrode activity to its initial level.

An anodic pulse ($I = +1$ A, $j = +100$ mA/cm²) in the form of a galvanostatic pulse (i.e. the anodic pulse is applied in the form of a constant current for a given period of time) of anodic current for a few minutes is introduced every 48 h of the operation of the cell.

- 5 As evident from Examples 2 and 3, similar results could be achieved with other metal based GDEs.

Example 1 – Sn-GDE in a flow cell

10 All electrochemical experiments were carried out using VSP BioLogic potentiostat clubbed with VMP3 BioLogic current booster. ElectroCell[®] microflow cell with an effective active area of working electrode as 10 cm². All the experiments were conducted in a galvanostatic mode with a current density of 100 mA/cm² (Figure 5). Prior to each electrochemical experiment, the catholyte (0.5 M KHCO₃) was saturated with CO₂ overnight (6-8 h). BPC GO[®], a flow meter, was used at the outlet of the cell to monitor the exit flow of gas from the cell. To maintain identical
15 reaction conditions, the application of current (I) was delayed until a stable signal of outlet CO₂ was recorded for 20-30 min by the BPC GO[®] flowmeter. This ensured an identical reaction condition in terms of gas species equilibrium, pH and catholyte conductance prior to the commencement of experiment. The cell was designed with a flow-through mode of operation (Figure 6), with an carbon free Sn-GDE (as disclosed in patent no. **WO2022013042A1**) of 100
20 cm² geometrical area as Working Electrode, dimensionally stable anode (DSA) as Counter Electrode and Ag/AgCl as reference electrode (RE). The pH and conductivity of the bulk catholyte were monitored throughout these experiments. The changes in the WE potential were monitored throughout the experiment (Figure 7).

- 25 The mode of the experiment is a single partial pass, achieved by circulating the electrolyte from a large feedstock reservoir (5 L), contrary to the electrolyte volume (calculated for both anode and cathode). The catholyte is periodically refreshed to maintain the pH and conductivity of the electrolyte in the range of 7.8-6.5, and 45-80 mS/cm, respectively.

30 **Catholyte:** 0.5 M KHCO₃, 5 L (refreshed periodically), pre-saturated with CO₂

Anolyte: 2 M KOH, 2 L (never refreshed during the 1000 h operation)

Electrolyte flow: 50-60 mL/min

CO₂ Flow: 30 mL/min

Membrane: Fumasep BPM (Fumasep FBM-PK))

35

Mode of operation: Flow through mode- gas outlet from the cell was blocked and forced to pass through the electrolyte (Figure 6)

Experiments were designed in a galvanostatic mode to avoid the possible influence of external parameters such as electrolyte recirculation, flow rate, and electrode flooding.

The products of this electrochemical reaction are analyzed by a gas chromatograph (GC) (for gas products such as CO, H₂) and High-performance liquid chromatography (HPLC) (for liquid products, such as formate ions).

- 5 A constant current is applied across the electrochemical cell to achieve a current density of 100 mA/cm² (the commercially relevant current density). During the operation, the pH and conductance of the bulk catholyte were monitored (Figure 2). Liquid samples were collected periodically from the bulk catholyte and analyzed for formate ions with HPLC. For gas analysis, the experimental set-up was connected with headspace GC.

10

Example 2 – Bi-GDE in a flow cell

- Using similar experimental conditions used in the ECR experiment using Sn-GDE (example 1), the FE of formic acid production from ECR by using a Bi GDE (a GDE based on Bi powder prepared exactly the same way as Sn GDE described in WO2022013042A1) is demonstrated
- 15 in Figure 8. Notably, the FE to formic acid was significantly recovered by pulsing (starting from 280 h, every 12 h an anodic pulsing was applied) after the FE to formic acid has decreased from initially 95% to around 70% at 260 h. Figure 9 directly shows the impact of the pulsing method. After the first pulse (1000 mA for 2 min), the FE towards formic acid increased from 70% to around 87% and started to level down with time. However, with periodic pulsing (1000 mA for 1
- 20 min every 12 hour), the FE towards formic acid can be maintained in a window of 85-90%, promising a stable and controlled process to produce formic acid electrochemically from CO₂.

Example 3 – Sn-foil in H cell

- An H-cell configuration was used to understand the impact of anodic pulsing on the Sn-plate
- 25 (Figure 10).

Details of H-cell configuration:

Anolyte: 0.1 M KHCO₃, 8 mL

Catholyte: 0.1 M KHCO₃, 8 mL

CO₂ purged in the solution: 10 mL/min

- 30 **Membrane:** AEM (FAA-3-50)

- A potentiostatic measurement at a fixed potential of -1.0 V vs. RHE was applied for 30 min, and its activity towards the ECR for formate production was monitored. With an anodic pulsing at 0.1 V for 30 min prior the electrocatalysis at -1 V vs. RHE, an increase in FE of formate ion from
- 35 60% to 90% was observed (Figure 11).

Example 4 – Sn-GDE in flow cell (acidic medium)

Using exactly the same experimental set up used in the ECR experiment using Sn-GDE (example 1), with the following electrolyte as mentioned below.

Catholyte: 0.25 M K_2SO_4 , 5 L, acidified with H_2SO_4 , pH=3 (refreshed periodically), pre-saturated with CO_2

Anolyte: 2 M KOH, 2 L (never refreshed during the 1000 h operation)

Electrolyte flow: 50-60 mL/min

5 **CO_2 Flow:** 30 mL/min

Membrane: Fumasep BPM (Fumasep FBM-PK)

10 The regeneration of the Sn-GDE in an acidic electrolyte is demonstrated in Figure 12. Similar to the alkaline environment, the FE of formic acid production from ECR by using a started at a high FE (>80%) but dropped sooner than alkaline condition to 20% after 200 hours. Notably, the FE to formic acid was recovered by pulsing (starting from 240 h, every 12 h an anodic pulsing was applied) though not to the same extent as in alkaline medium but the trend was similar and consistent showing the applicability of the proposed process in both alkaline and acidic environment.

CLAIMS

1. A method of operating an electrochemical cell in the electrochemical conversion of a gaseous reactant into bulk chemicals at the working electrode, said method comprising the use of a metal based GDE working electrode as cathode, an anode, and an electrolyte, said method of operation being characterized in maintaining the pH of the electrolyte within a range of 2 units of its initial value, and in applying an anodic pulse to the working electrode with intervals.
2. The method according to claim 1, wherein the electrolyte is the catholyte present in a cathode compartment of the electrochemical cell and wherein the method is characterized in maintaining the pH of the catholyte within a range of 2 units of its initial value, and in applying an anodic pulse to the working electrode at regular intervals.
3. The method according to claims 1 or 2, wherein the anodic pulse consists of a current of 50-200 mA cm⁻², preferably applied for at least 30 seconds; in particular a current of at least 100 mA cm⁻², preferably applied for at least 1 minutes to the working electrode.
4. The method according to claims 1 or 2, wherein the anodic pulse consists of a charge of 1.5-10 Coulomb cm⁻² applied to the cathode; in particular a charge of at least 6 Coulomb cm⁻² applied to the working electrode.
5. The method according to any one of the preceding claims wherein the anodic pulses are applied at regular intervals ranging from 1 hour to 48 hours,.
6. The method according to any one of the preceding claims wherein the gaseous reactant is selected from CO₂, CO, N₂, NO_x or O₂; in particular CO₂.
7. The method according to any one of the preceding claims wherein the bulk chemicals are selected from Syngas, Formic Acid, Methanol, Ethanol, Ethane, Ethylene, Methane, Ammonia, Hydrogen, Hydrogen peroxide and the like.
8. The method according to any one of the preceding claims wherein the pH is maintained from about 7 to 9 in case of an alkaline electrolyte and from about 3 to 5 in case of an acidic electrolyte.

Figure 1

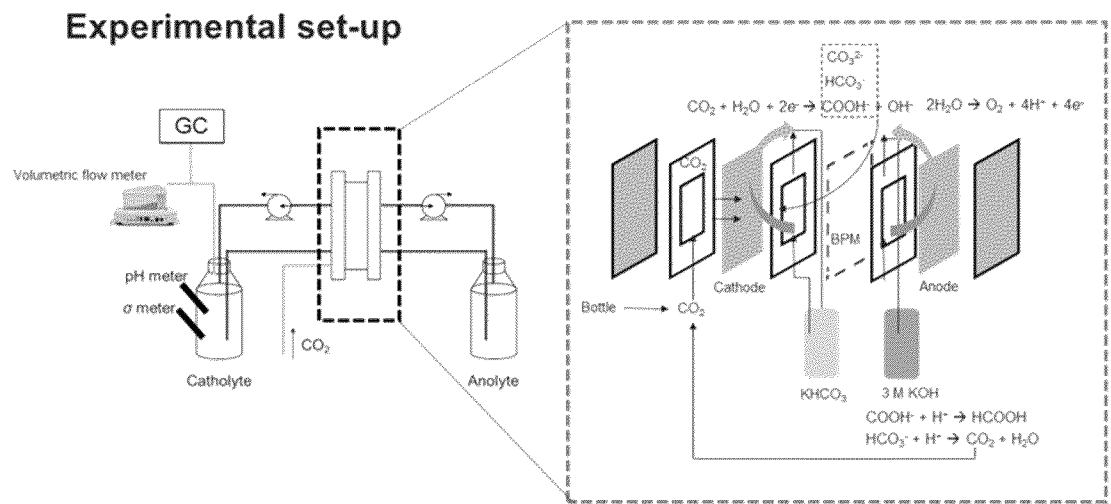


Figure 2

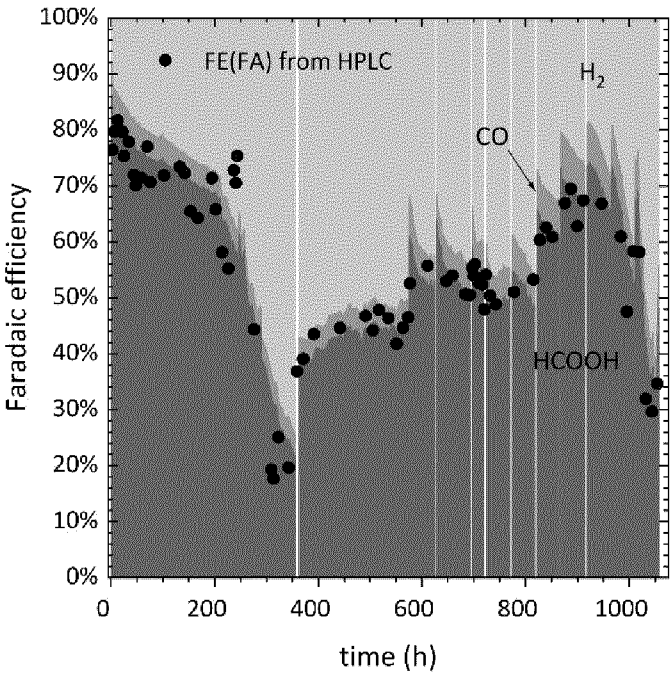


Figure 3

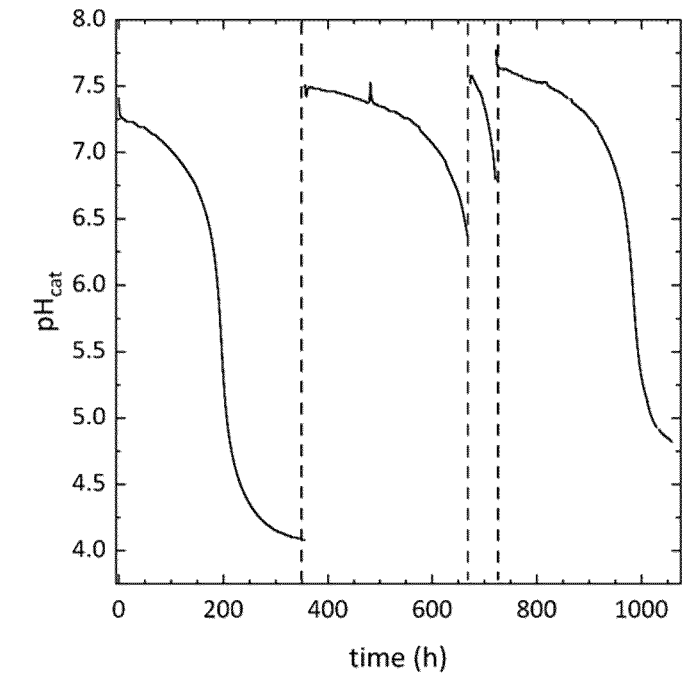


Figure 4

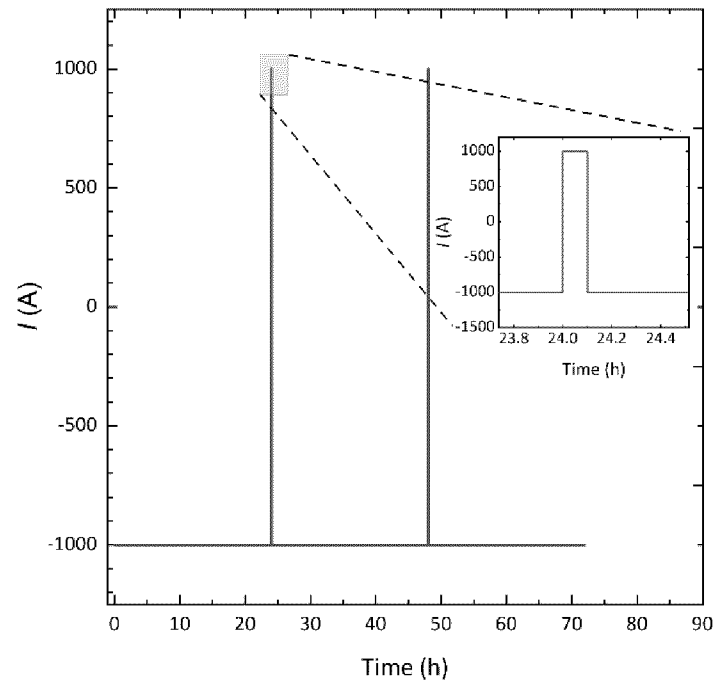


Figure 5

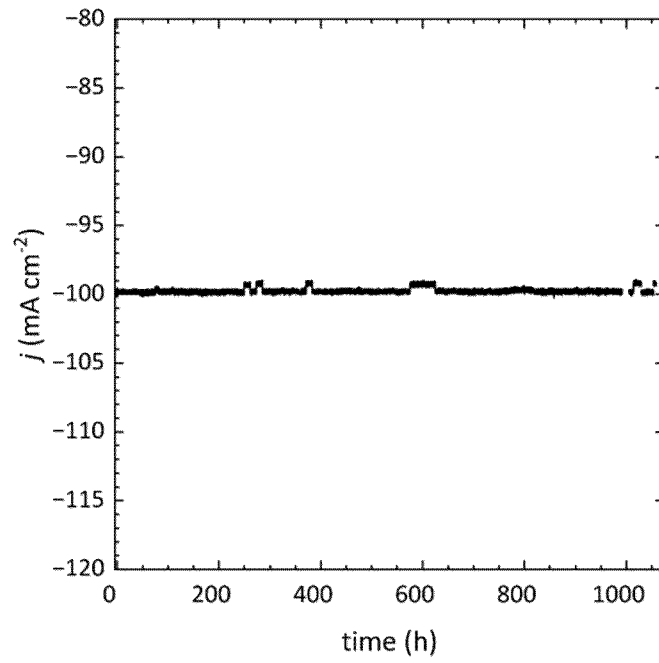


Figure 6

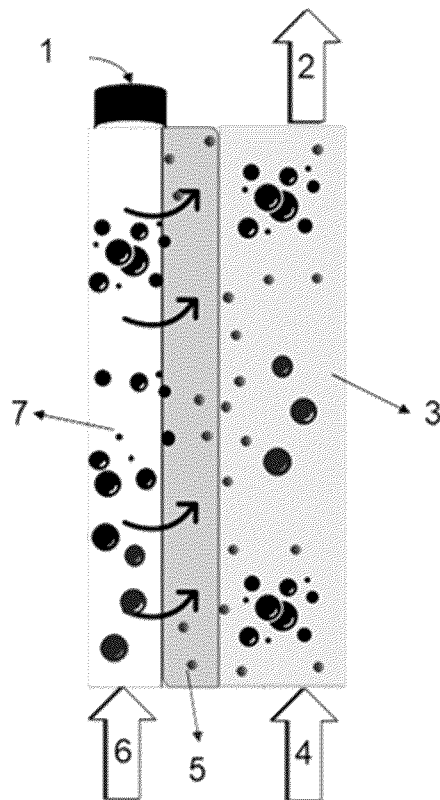


Figure 7

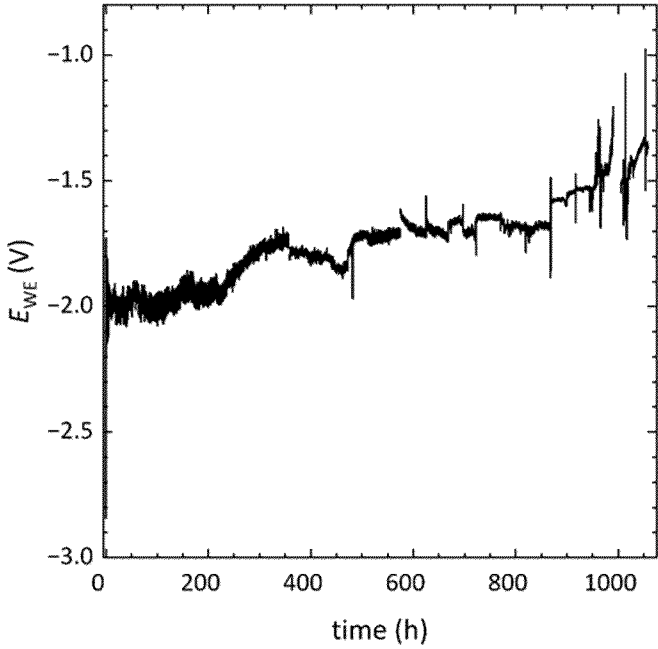


Figure 8

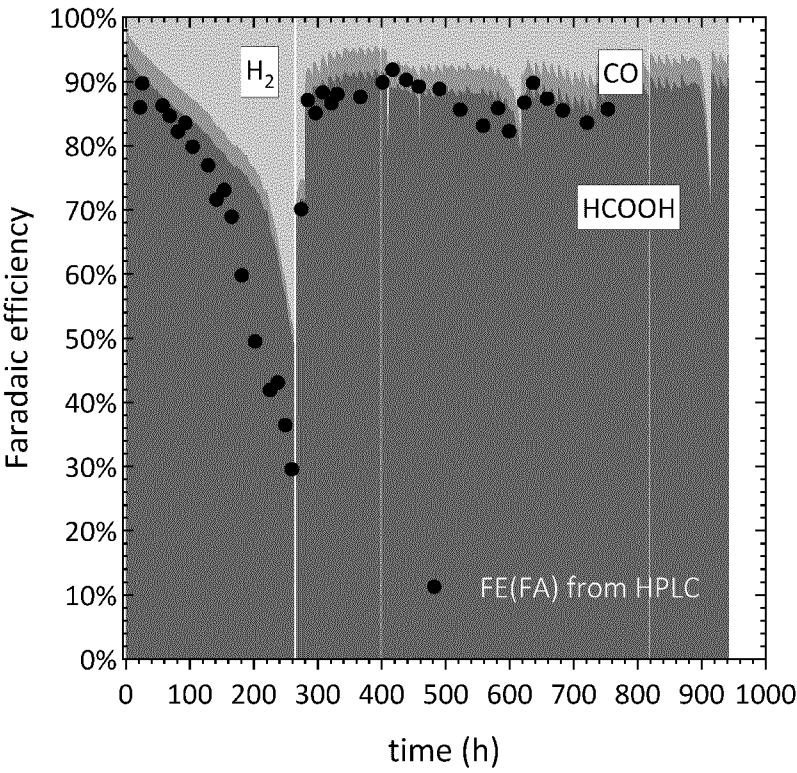


Figure 9

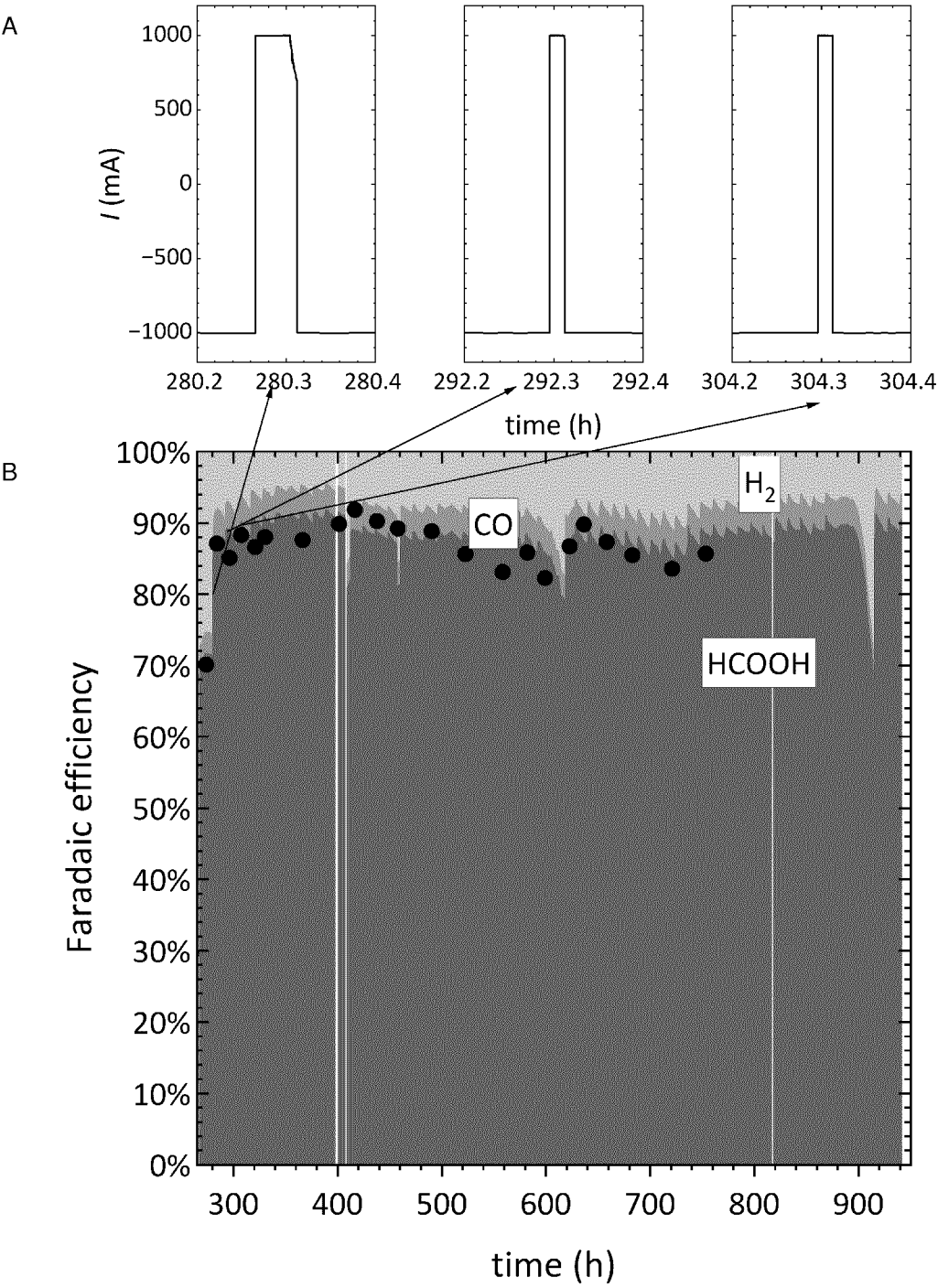


Figure 10

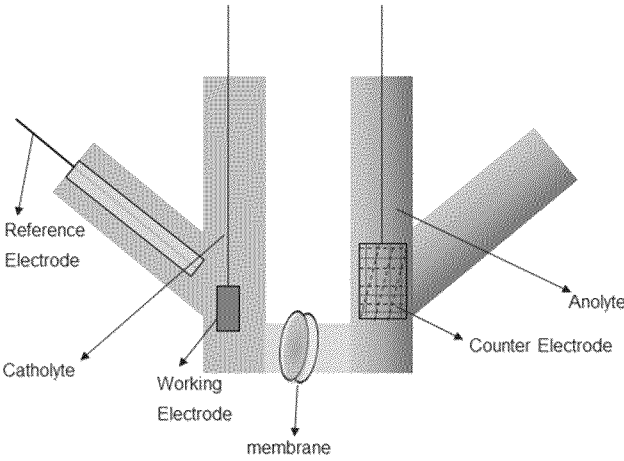


Figure 11

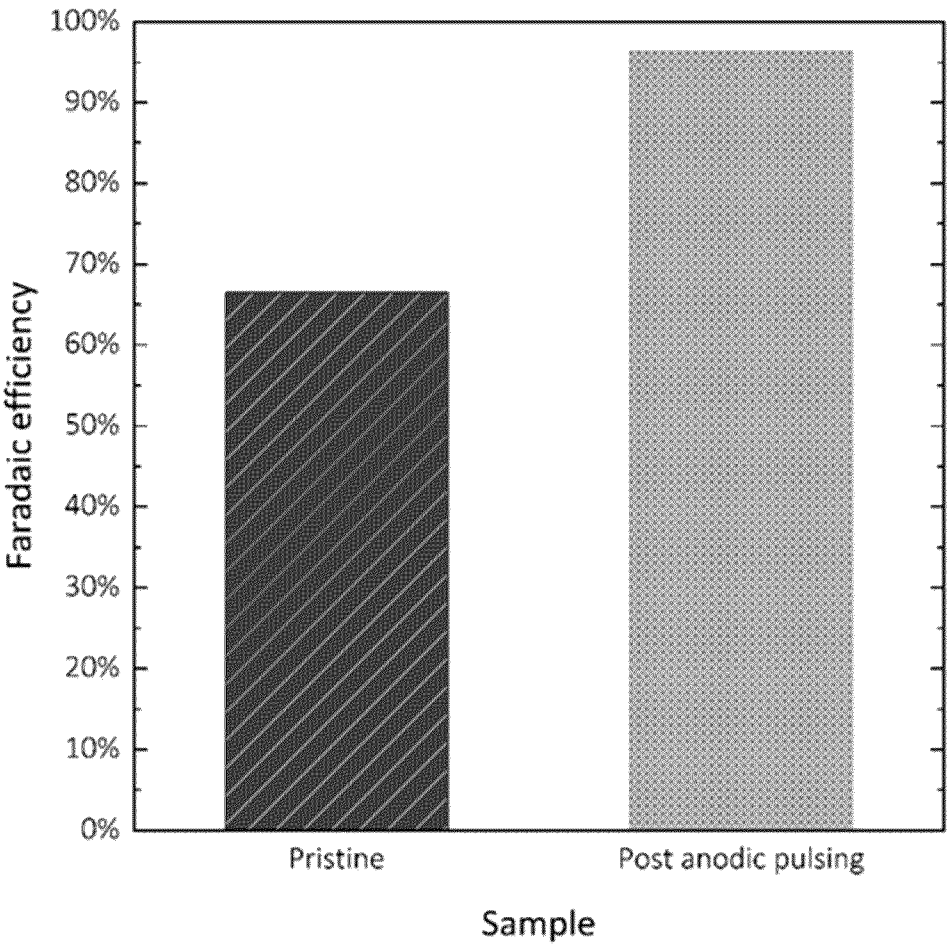
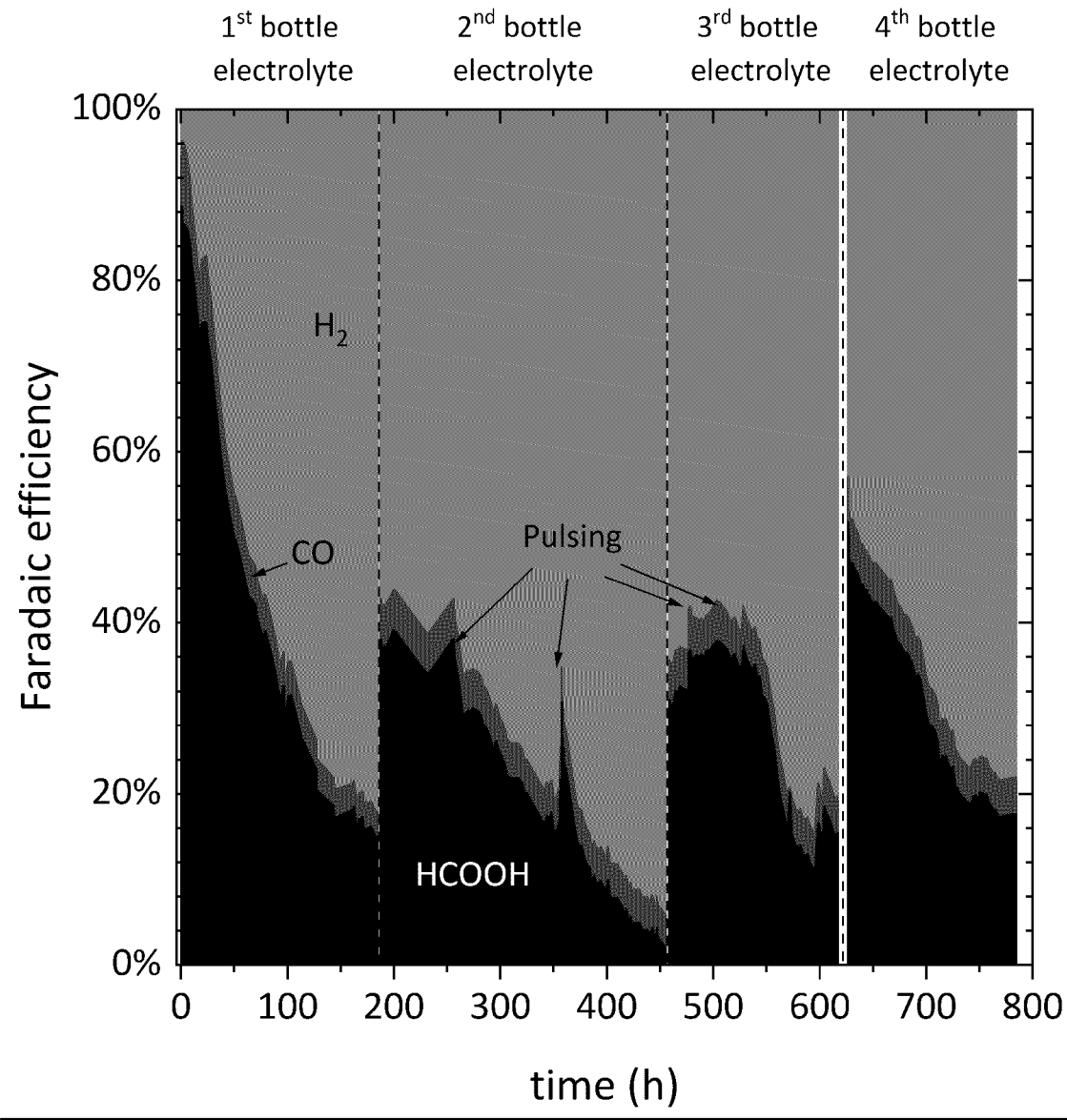


Figure 12



INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2024/065202

A. CLASSIFICATION OF SUBJECT MATTER					
INV.	C25B1/04	C25B1/23	C25B1/27	C25B1/30	C25B1/50
	C25B3/03	C25B3/07	C25B3/25	C25B3/26	C25B9/19
	C25B11/042	C25B15/00	C25B15/031	C25B15/033	
According to International Patent Classification (IPC) or to both national classification and IPC					
B. FIELDS SEARCHED					
Minimum documentation searched (classification system followed by classification symbols) C25B					
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched					
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) EPO - Internal					
C. DOCUMENTS CONSIDERED TO BE RELEVANT					
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☒ Further documents are listed in the continuation of Box C.					
☒ See patent family annex.					
* Special categories of cited documents : "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance;; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance;; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family					
Date of the actual completion of the international search 12 August 2024			Date of mailing of the international search report 26/08/2024		
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016			Authorized officer Thorner, Gentien		

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International application No

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