



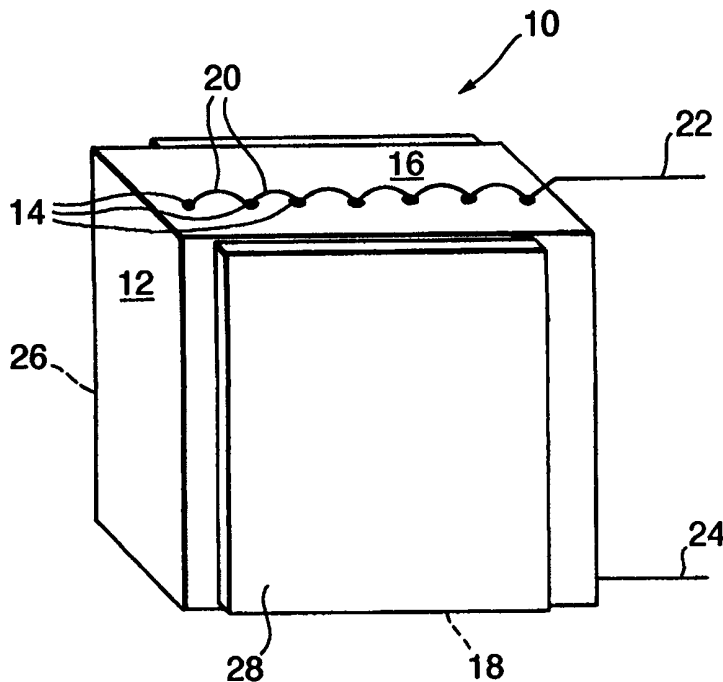
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(54) Title: MAGNETIC BEAM DEFLECTION DEVICES

(57) Abstract

A device (10) for changing the divergence of a beam of microwave radiation comprises a ferrite body (12) having an aperture through which the beam passes. Magnetic means in the form of a plurality of wires (20) passing both through the body (12) and across the aperture or in the form of a coil on either side of the aperture causes a differential phase delay as the beam passes through the aperture which broadens or narrows the beam.



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MAGNETIC BEAM DEFLECTION DEVICES

This invention relates to a device which is adapted to be positioned in the path of a beam of electromagnetic radiation propagating in free space which changes characteristics of the beam. The invention is particularly, but not exclusively, concerned with microwave
5 devices.

The term microwave refers to the part of the electromagnetic spectrum substantially in the frequency range 0.2 to 300 GHz. It includes that part of the spectrum referred to as millimetre wave (having a frequency in the range 30 to 300 GHz).

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A known device for controlling the direction of a microwave beam comprises a body of ferrite material having a first magnetic coil along a first side of the body and a second magnetic coil along a second, opposite, side of the body. Each coil generates a magnetic field which passes through faces of the body. The device is configured such that
15 magnetic field from each coil passes through the body in opposite directions. This causes a gradient in magnetisation across the body. The direction of the beam leaving the device is perpendicular to the gradient in the magnetic field across the body. Therefore the degree of deflection of the beam is controlled by the gradient in the magnetisation.

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One application for such a device is in a control system for automatic or semi-automatic control of a vehicle. Such a control system comprises a radar system to determine location and speed of a vehicle relative to other vehicles and other objects or features, for example roadside furniture. This enables the control system to operate the vehicle

automatically in cruise control and collision avoidance modes.

The radar system uses a microwave beam of narrow beam width having a half-power (3dB) beam width of 2° to 4° . A narrow beam width is used in order that, when
5 reflected from other vehicles, a relatively strong usable signal is available for processing. Furthermore, a narrow beam width is necessary for angular location of obstacles. Whilst a narrow beam width is useful for vehicle speeds which are normal for road travel, for example 15 to 100 km/hour, it is less useful for manoeuvring a vehicle at lower speeds, for example when parking, reversing, negotiating obstacles and
10 the like. Because the beam width is narrow it provides wide coverage at some distance from the vehicle but at distances close to the vehicle, there are blind spots on either side of the beam. Obstacles in the blind spots will not be detected which may be hazardous if the vehicle is under automatic control. Furthermore, at low speeds, or when the vehicle is stationary, it is relatively easy for pedestrians or other vehicles to move into
15 the blind spots and become hazards to an automatically controlled vehicle. Although it is possible to use a beam steering device such as the one described above to scan the beam horizontally from side to side to search for hazards, beam steering cannot scan beams through large angles and blind spots will still be present. For these reasons it has been proposed that certain control systems disable their radar detection means when the
20 vehicle is stationary or moving at slow speed. The control systems activate again when the vehicle moves off from stationary and reaches a pre-determined speed or when the vehicle accelerates to the pre-determined speed.

According to a first aspect the invention provides a device for changing the divergence

of a beam of electromagnetic radiation comprising a body having an aperture for the beam characterised in that magnetic means acts on the aperture such that parts of the beam passing through a central and at least one side region of the aperture undergo a differential phase delay.

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Preferably the magnitude of the phase delay in the central region is relatively large compared to that at the side regions. Alternatively the magnitude of the phase delay in the central region is relatively small compared to that of the side regions.

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The aperture may be a sub-aperture induced by activation of the magnetic means. There may be a plurality of sub-apertures having boundaries defined by elements of the magnetic means. The device may have a total aperture comprising the plurality of sub-apertures. Alternatively the device may have a single aperture.

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According to a second aspect the invention provides a device for changing the divergence of a beam of electromagnetic radiation comprising a body having an aperture for the beam characterised in that the device has magnetic means comprising at least one element located within the aperture the or each element defining one or more boundaries of a plurality of sub-apertures within the aperture.

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Preferably the magnetic means induces variations in the value of magnetisation present across the aperture or sub-apertures. Preferably the magnetic means inducing variations in the value of magnetisation is located in the body. For example, looking at a graph of magnetisation across the aperture there may be "kinks", whether peaks or troughs,

associated with each element of the magnetic means which is generating magnetic field. This applies whether an average value of gradient in magnetisation across the aperture has a positive or negative non-zero value or is zero. It may be these kinks which define the boundaries of the sub-apertures. Preferably the sub-apertures are narrower than the aperture, and parts of the beam passing through each sub-aperture will diverge more than the beam passing through the total aperture which is relatively wide in comparison. Preferably there is a lack of coherence between parts of the beam which pass through adjacent sub-apertures.

- 10 Preferably the magnetic means comprises one or more elongate sources of magnetic field. If there are a plurality of elongate sources, these may be disposed parallel to one another. Most preferably the magnetic means is one or more paths for carrying electric current. Conveniently the or each path is a metal wire. If there are a plurality of paths, current may travel in each path in a direction substantially parallel to the other paths.
- 15 Alternatively current in some paths may travel in one direction and current in other paths may travel in an opposite direction. Current may travel in opposite directions in adjacent paths. Different amounts of current may be carried by adjacent paths.

Preferably the current carried by the or each path may be altered so as to change the amount of magnetic field generated by the magnetic means and thus the amount of magnetisation induced in the body. The current carried by the or each path may be switched on and off which may switch the beam between a wider beam width and a narrower beam width. Alternatively, the current may be varied in value between on and off states. As a result the degree of kinking in magnetisation across the aperture may

be altered and the degree to which the device diverges or converges the beam (that is focusses or defocusses the beam) may also be altered. Individual paths (or groups of individual paths) may be controlled separately. For example, they may be switched on and off and varied independently of one another.

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If the device is to diverge the beam in both azimuth and elevation directions, the magnetic means may be in the form of a grid comprising a first set of one or more elongate sources of magnetic field and a second set of one or more elongate sources of magnetic field in which the first set is orientated at an angle of greater than 0° relative to the second set. Preferably the first and second sets are orientated at 90° to each other. The first and second sets of sources of magnetic field may be independently controllable in order to broaden the beam independently in azimuth and elevation directions.

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Preferably the beam of radiation is microwave radiation. Most preferably the beam of radiation is generated by a radar system.

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The device may effectively be serving as a zoom lens for the beam of radiation. By zoom lens is meant a device which can diverge or converge the beam.

A magnetic material is one in which its internal magnetisation is effected by magnetic field. Preferably the magnetic material is an electrical insulator. It may be a soft ferrite. Ferrite materials may be particularly suitable since they combine high permeability with low conductivity and low losses. Due to the low conductivity, ferrite materials are easily penetrated by microwaves.

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The magnetic means may comprise magnetic field generating means located adjacent one or more sides of the aperture. Preferably there are two magnetic field generating means. The or each magnetic field generating means may be a single wire or may be one or more coils. Preferably the magnetic field generating means are provided in one or more pairs on opposite sides of the aperture. If the device is configured to have one magnetic field generating means presenting a North pole on one face of the or each aperture and the other magnetic field generating means presenting a South pole on the face of the or each aperture this induces a positive or negative non-zero gradient in magnetisation across the aperture which can be used to steer the beam by an angle θ .

Differential operation of the or each pair of magnetic field generating means may change the value of angle θ . If the or each pair of magnetic field generating means both present the same pole (whether North or South) on each face of the or each aperture this induces a differential phase delay between a central and side regions of the beam as the beam passes through the device. In this way the device may change divergence of a beam without the need to provide separate magnetic means which, for example, divide the aperture into a plurality of sub-apertures. Alternatively, such aperture dividing magnetic means may be provided together with magnetic field generating means.

Preferably there are two gradients in magnetisation which are in directions perpendicular to one another. This enables the direction of the beam to be controlled in azimuth as well as in elevation to achieve conical beam steering. In an embodiment in which the device is used in a surface vehicle (for land or water) elevation control means may still be required. For example, in a land vehicle elevation control may be required to compensate for braking which would cause the front of the vehicle to dip. It may also

compensate for the effects of vibration. Elevation scanning may allow information to be gathered that can be used to identify roadside furniture and other objects such as bridges and the like.

5 The body may comprise a first material which contains at least one region of a second material having a magnetic permeability which is lower than the magnetic permeability of the first material. The or each region may extend from sides of the aperture or sub-apertures. The or each region may extend towards the centre of the aperture or sub-apertures. Preferably the or each region extends about two thirds of the way to the
10 midpoint between the sides of apertures or sub-apertures. Preferably the presence of the or each region having relatively lower permeability causes more of the magnetic flux to be deviated away from the sides of apertures or sub-apertures and towards the centre of the aperture or sub-apertures than would be the case in the absence of the or each region.

15 Preferably the or each region comprises a slot in the first material containing the second material as an insert or as a filler. The or each slot may taper being thinner at an end nearest to the centre of the aperture or sub-apertures. Preferably the or each slot has a linear taper. Alternatively the taper may be curved.

20 According to a third aspect the invention provides a control system comprising a radar system which incorporates a device in accordance with the first or second or both aspects of the invention.

According to a fourth aspect the invention provides a vehicle incorporating a control system in accordance with the third aspect of the invention.

Preferably the vehicle is a land vehicle. Alternatively, the vehicle may be waterborne
5 or airborne.

An embodiment of a microwave device in accordance with the invention will now be described by way of example only with reference to the accompanying drawings in which:

10 Figure 1 shows a polar plot of relative power against scan angle for an undiverged beam;

Figure 2 shows a perspective view of an embodiment of the device;

Figure 3 shows a plan view from above of the device of Figure 2;

Figure 4 shows a polar plot of relative power against scan angle for a beam diverged by the device of Figures 2 and 3;

15 Figure 5 shows another polar plot of relative power against scan angle for a beam diverged by the device of Figures 2 and 3;

Figure 6 shows a plan view from above of another embodiment of the device;

Figure 7 shows a polar plot of relative power against scan angle for a beam diverged by the device of Figure 6;

20 Figure 8 shows a plan view from above of a further embodiment of the device;

Figure 9 shows a device being used to focus a diverging wave front into a plane wave front;

Figure 10 shows a device being used to focus a diverging wave front from a scanning antenna into a plane wave front.

Figure 11 shows a plan view from above of a still further embodiment of the device; and Figure 12 shows a plan view from above of yet a still further embodiment of the device.

A control system for a vehicle comprises a radar system, having a transmitter and
5 receiver of microwaves and control means for receiving and analysing data provided by the radar system for controlling the speed and direction of the vehicle so as to enable it to travel in an optimum manner. The transmitter comprises a Gunn oscillator and a patch antenna.

10 The Gunn oscillator is a source of microwaves. The patch antenna launches the microwaves as a divergent beam having a wave front. The divergent beam is focussed by a lens which focusses a central part of the beam and produces a less divergent beam having a plane wave front. The beam is transmitted into free space. The beam is categorised by a parameter referred to as beam width w_0 . Beam width can be defined
15 as the angular separation of points across the beam which are at power values 3dB lower than the peak power value of the beam. The beam width of the beam which emerges from the lens is about 3 to 4° at 77GHz. This frequency is typical for use in a control system to be used in vehicle radar.

20 The beam may be reflected by vehicles or other objects or features and is received by the control system. Any suitable form of receiver may be used. The receiver may use the same lens/patch antenna combination as the transmitter or may use another means of receiving reflected signals. The control system obtains data from the reflected signals and uses them to control the vehicle.

Figure 1 is a polar plot of relative power against scan angle for the beam which has been launched into free space from the feed. The values given are simply a relative power level at an angle θ relative to direction of beam propagation. The beam width in this case is about 7° .

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Figure 2 shows a perspective view of a device 10 for diverging the beam of microwave radiation. The device 10 comprises a ferrite body 12 typically comprised of a material such as Transtech TTI-3000. A plurality of holes 14 pass through the body 12 from an upper surface 16 to a lower surface 18. Although each hole 14 may carry a single wire 20 for carrying electrical current, in a preferred embodiment each hole is occupied by a plurality of wires, for example two or three wires. In such an arrangement, if each wire carries the same current as a single wire, this provides a greater magnetisation. An additional benefit is that heating effects in the wires may be reduced by having a slightly lower current pass through a greater number of wires. It may be necessary to provide a plurality of power sources, a first of the power sources to power a set of first wires in the holes and others of the power sources to power a set of second and further sets of wires in the holes. The plurality of power sources may be operated independently. Clearly the wires should be insulated from one another in this arrangement. Typically, the wires are made of tungsten. The wires 20 which pass through the body are conveniently connected to leads 22 and 24 in a parallel arrangement as shown in Figure 1. Alternatively, a single wire is threaded through adjacent holes so that all of the individual sections of wire which pass through the body are arranged in series. The wires 20 have a diameter of $250\mu\text{m}$. The spacing of adjacent wires 20 is chosen to be approximately equal to the wavelength of the beam of microwave radiation passing

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through the device 10. For microwave radiation having a frequency of 77GHz, the spacing would be about 4mm. If the spacing is less than this the wires will reflect at least some of the microwave radiation and operation of the device 10 will be compromised.

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In this embodiment, the wires are the magnetic means which serve to change the divergence of the beam.

The device is placed in the path of the beam of microwave radiation such that the beam
10 passes through a rear face 26, through the body 12 and out of a front face 28. To minimise overall loss the front and rear faces are provided with anti-reflection coatings, for example layers of fused silica. The outer dimensions of the body are determined by the width of the beam of microwave radiation which is to pass through it. For use in an application such as vehicle radar the front and rear faces are approximately 70mm
15 square. The body has a thickness of 15mm.

The body is made in two halves, a front half 30 and a rear half 32. This is shown in Figure 3. Half 30 has scored into it a series of parallel grooves. Half 32 does not have any grooves. When the halves 30 and 32 are joined together to form the body 12 as
20 shown in Figure 2, the planar surface of half 32 covers the grooves of half 30 so as to form the holes 14 running through the body. Before the halves are joined together to form the body 12, it is convenient for the wires 20 to be laid along the grooves. Following this, the halves are joined together to form the body 12. The halves may be joined securely together using a thin layer of adhesive. The adhesive may also occupy

any clearance which is present between the wires 20 and the holes 14 so as to fix the wires 20 securely in the holes 14. In this embodiment there is a single wire 20 per hole 14. When they are carrying current and consequently generating magnetic field, adjacent wires define adjacent sub-apertures.

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In operation the wires 20 are energised with DC current typically 5 to 10A at 2V. This induces a magnetic field around the wires which induces a magnetisation in the ferrite. In the embodiment of Figures 2 and 3 it can be seen that between adjacent wires 20, the magnitude of magnetisation will be relatively high in the region of the wires and relatively low between. Since magnetisation in the material induces a phase delay in the wave front as it passes through the body, there will be a differential delay induced between those parts of the beam which pass through relatively high magnetisation regions and those which pass through relatively low magnetisation regions. As a result, that region of the beam will be diverged. Since divergence occurs at each sub-aperture, the net effect of the device 10 is an overall divergence of the beam if coherence is not maintained between adjacent sub-apertures.

Figure 4 shows a polar plot of relative power against scan angle for a beam which has been diverged using the device of Figures 2 and 3. In the particular embodiment of the device used to produce Figure 4, wires 20 defining sub-apertures across one half of the aperture are configured to have current running in the same direction, whilst across the other half of the aperture the wires are configured to have current running in an opposite direction. This embodiment uses two wires, each of 0.5mm diameter, per hole. Each

wire carries a current of 1A. As can be seen the effect of magnetising the wires is to broaden the beam considerably from about 7° to about 20°.

Figure 5 shows another polar plot of relative power against scan angle for a beam which has been diverged using the device of Figures 2 and 3. However, unlike Figure 4, the wires are carrying a much greater current, in this case 10A. As a consequence the beam has been split into two main sub-beams. Operating a device to alternate between the effect of Figure 1 and the effect of Figure 5 may provide a simple way of achieving a beam diverging device. A single main beam is split into two sub-beams such that the single main beam covers a central region on and about bore sight of the transmitter and the two sub-beams cover regions outside this central region.

Figure 6 shows a plan view from above of another embodiment of the device. Unlike the embodiment of Figures 2 and 3, the device 40 of Figure 5 does not have magnetic means in the form of wires running through a ferrite body 42. Instead it is provided with magnetic field generating means in the form of coils 44, 46, one coil located on each side of the body 42. Each coil is wound around a respective end piece 48, 50.

If the coils are wound or energised such that both coils present the same magnetic pole on each face 52, 54 of an aperture 56 of the device, there will be a relatively higher value of magnetisation at side regions of the aperture 56 near to the coils 44, 46 than in the centre of the aperture 56. For the reasons discussed above this will cause a beam passing through the aperture 56 to diverge.

Figure 7 shows the effect of broadening of beam width due to a beam passing through the device of Figure 6 in its energised state. As can be seen, the beam width w_0 is about 28° . Comparing Figures 1 and 7, it can be seen that the coils broaden the beam by more than three times. At a typical operating frequency of 77GHz, the insertion loss is in the
5 region of 1dB.

Normally ferrites, or a suitable magnetic material for the frequency range of interest, work with circularly polarised radiation since this is the natural mode of propagation in magnetic materials. However, linearly polarised radiation can also be used with
10 ferrites because it is effectively a combination of two circularly polarised beams rotating in opposite senses.

Figure 8 shows a plan view from above of a further embodiment of the device. The device 60 of Figure 8 is, in effect, a combination of the device shown in Figures 2 and
15 3 and the device shown in Figure 6. The device 60 is provided with magnetic field generating means in the form of coils 62, 64 which enable the device to scan a beam. In addition to the coils 62, 64, the device 60 is also provided with magnetic means in the form of wires 66 which run through a ferrite body 68. Sending current through the wires 66 enables the device 60 to cause the beam to diverge in the same manner as has
20 been described in relation to the device of Figures 2 and 3.

In the foregoing, the devices described change a plane wave front of incident radiation into a diverging wave front. As a consequence, the devices described are being used as beam broadening devices. However, the devices can be configured so as to change an

incident diverging wave front into a plane wave front. This would be equivalent to focussing or collimating the beam.

Figure 9 shows a device 70 having a feed or transmitter 72 of microwave radiation and a ferrite body 74. In this embodiment, the ferrite body 74 is divided into a plurality of sub-apertures 76 by magnetic means such as wires passing through the body. The feed 72 emits diverging wave front 78 which is focussed into a plane wave front 80 by the ferrite body 74. The ferrite body 74 may be constructed in accordance with any of the preceding embodiments of the devices discussed. In order to achieve such focussing the magnetisation gradient in the body would need to be created by suitably configured magnetic means.

Figure 10 shows the principle of Figure 9 applied to a device 90 incorporating a scanning feed or transmitter 92. The feed or transmitter 92 may scan or rotate mechanically or electronically. It is surrounded by a ferrite body 94 in the shape of a ring. The body 94 has, passing through it, a plurality of current carrying wires which divide the body into a plurality of sub-apertures 100. The wires are controlled in accordance with previous embodiments of the invention in order to generate suitable magnetisation gradients in the body 94 to control the divergence of a wave front.

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The feed or transmitter 92 emits a diverging wave front 96. If the body 94 is suitably magnetised it can focus the diverging wave front into a plane wave front 98 over a complete 360° revolution of the feed or transmitter 92. The body 94 focusses the wave front in a plane perpendicular to the axis of rotation of the feed or transmitter 92, that

is in a plane occupied by the body 94. Such a device would be suitable for an application in which it is used to focus a beam in one plane only, typically azimuth. Such an effect would be suitable for antennae which only rotate about a single axis. If the body 94 is in the shape of a doughnut with the scanning feed or transmitter located at its centre, then as the beam encounters the body, it encounters a curved surface acting as a lens both in elevation and azimuth directions. Therefore, a doughnut-shaped body 94 is able to focus in both of those directions.

Although Figures 9 and 10 have been discussed in terms of their ability to focus a diverging beam, they can, of course, also be used to defocus non-diverging beams or to cause an already diverging beam to diverge more.

Figures 11 to 13 show constructional variations of the embodiments discussed above. For example in Figure 11, one half 102 of a body 104 of a device 106 is of composite construction having wedge portions 108 and 110 of non-magnetic material attached to a body part 112 of magnetic material. The wedge portions 108 and 110 have a similar dielectric constant to the magnetic material used to form the body part 112. As magnetic material of the body part 112 becomes thinner towards sides 114 and 116 of the device, the magnetic circuit becomes less efficient. As a consequence the composite construction helps tailor a desired magnetisation gradient from one side of the body to the other.

Figure 12 shows an embodiment of a device 120 which has more than one row of holes 122 in its body and thus more than one row of wires. This provides for more flexibility

in configuring wires and thus magnetisation. For example groups of four holes such as 124, 126, 128 and 130 can be wound to provide an individual coil arrangement. In one such arrangement a wire passes down hole 124, up hole 126, down hole 130 and then up hole 128. Individual groups of four holes may be wound in a similar way to produce

5 individually controllable coil arrangements each of which can have passed through it an individually controllable current to achieve an individual magnetisation. In the example of winding described above, individual coil arrangements would direct a strong component of magnetic field between front and rear faces of the body. This arrangement may work more effectively than a simple disposition of wires such as serial

10 winding through adjacent holes.

The device 120 is provided with three layers, outer plates of magnetic material 132 and 134 and a middle part or former 136. The wires can be wound directly onto the former and then the device 120 can be assembled. The former may be of magnetic material but

15 may equally be non-magnetic material. A non-magnetic material provides a reluctance path in a direction perpendicular to the front and rear faces and thus encourages magnetic field passing through the body to be more parallel to this perpendicular direction. The former 136 ideally has the same dielectric constant as the magnetic material of the outer plates 132 and 134. However, in another embodiment the outer

20 plates 132 and 134 could be separated by an air gap. In such an embodiment the former 136 would not be present and so some alternative method of winding the wires would need to be employed.

It should also be noted that the spacing of the holes is not uniform across the aperture

from one side to an opposite side. Although embodiments of the device 120 may exist having both uniform and non-uniform spacing of holes, non-uniform spacing may be preferred in order to produce a series of sub-apertures having different sizes for the purpose of destroying coherence across the wave front of the beam in order to obtain
5 significant divergence having a relatively uniform power distribution across the resultant diverged beam. It may be that all of the spacings between adjacent holes are different or it may be that at least two spacings are the same and at least one other spacing is different. Although it is intended for individual wires or individual groups of wires to be supplied with individually controllable current supplies to disrupt coherence, if the
10 spacings of the holes are chosen correctly a single wire wound through each hole in turn may result in an embodiment which disrupts coherence sufficiently without the need to provide individually controllable current supplies.

The embodiments of the devices described above may be used in conjunction with a
15 conventional lens antenna in an arrangement in which the lens antenna emits energy in a beam having a plane wave front into free space in a desired propagation direction. Such a beam encounters the device, and diverges as it passes through it. Alternatively the lens may be omitted and the device may serve as a combined lens and diverging device. In this embodiment the feed, such as a patch antenna, would feed a divergent
20 beam directly into the device.

CLAIMS

1. A device for changing the divergence of a beam of electromagnetic radiation comprising a body having an aperture for the beam characterised in that magnetic means acts on the aperture such that parts of the beam passing through a central and at least one side region of the aperture undergo a differential phase delay.
2. A device according to claim 1 characterised in that the magnitude of the phase delay in the central region is relatively large compared to that at the side regions.
3. A device according to claim 1 characterised in that the magnitude of the phase delay in the central region is relatively small compared to that of the side regions.
4. A device according to any preceding claim characterised in that the aperture is a sub-aperture induced by activation of the magnetic means.
5. A device according to claim 4 characterised in that there are a plurality of sub-apertures having boundaries defined by elements of the magnetic means.
6. A device according to any of claims 1 to 3 characterised in that the device has a single aperture.

7. A device for changing the divergence of a beam of electromagnetic radiation comprising a body having an aperture for the beam characterised in that the device has magnetic means comprising at least one element located within the aperture the or each element defining one or more boundaries of a plurality of sub-apertures within the aperture.
8. A device according to claim 7 characterised in that the magnetic means induces variations in the value of magnetisation present across the aperture or sub-apertures.
9. A device according to claim 7 or claim 8 characterised in that the magnetic means induces variations in the value of magnetisation is located in the body.
10. A device according to any of claims 7 to 9 characterised in that the sub-apertures are narrower than the aperture, and parts of the beam passing through each sub-aperture diverge more than the beam passing through the total aperture which is relatively wide in comparison.
11. A device according to any of claims 7 to 10 characterised in that there is a lack of coherence between parts of the beam which pass through adjacent sub-apertures.
12. A device according to any of claims 7 to 11 characterised in that the magnetic means comprises one or more elongate sources of magnetic field.

13. A device according to claim 12 characterised in that the elongate sources are disposed parallel to one another.
14. A device according to any of claims 7 to 13 characterised in that the magnetic means is one or more paths for carrying electric current.
15. A device according to claim 14 characterised in that the current carried by the or each path may be altered so as to change the amount of magnetic field generated by the magnetic means and thus the amount of magnetisation induced in the body.
16. A device according to any of claims 7 to 15 characterised in that the magnetic means may be in the form of a grid comprising a first set of one or more elongate sources of magnetic field and a second set of one or more elongate sources of magnetic field in which the first set is orientated at an angle of greater than 0° relative to the second set.
17. A device according to claim 16 characterised in that the first and second sets of sources of magnetic field are independently controllable in order to broaden the beam independently in azimuth and elevation directions.
18. A device according to any of claims 7 to 17 characterised in that the device serves as a zoom lens for the beam of radiation.

19. A device according to any of claims 7 to 18 characterised in that magnetic field generating means is provided located adjacent one or more sides of the aperture.
20. A device according to claim 19 characterised in that there are two magnetic field generating means.
21. A device according to claim 19 or claim 20 characterised in that the magnetic field generating means are provided in one or more pairs on opposite sides of the aperture.
22. A device according to any of claims 7 to 21 characterised in that the beam of radiation is microwave radiation.
23. A device substantially as described herein with reference to the Figures of the accompanying drawings.
24. A control system comprising a radar system which incorporates a device in accordance with any of the preceding claims.
25. A control system substantially as described herein with reference to the Figures of the accompanying drawings.
26. A vehicle incorporating a control system in accordance with claim 24 or claim 25.

27. A vehicle according to claim 26 which is a land vehicle.
28. A vehicle according to claim 27 which is waterborne or airborne.
29. A vehicle substantially as described herein with reference to the Figures of the accompanying drawings.

Fig.1.

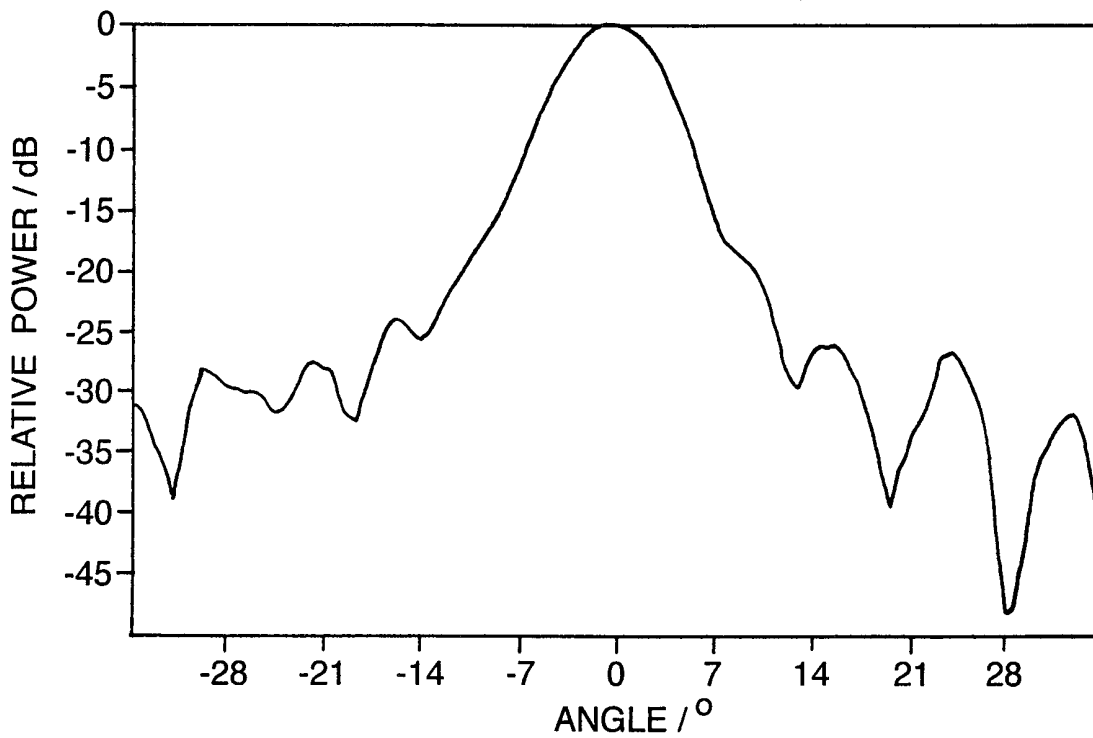


Fig.2.

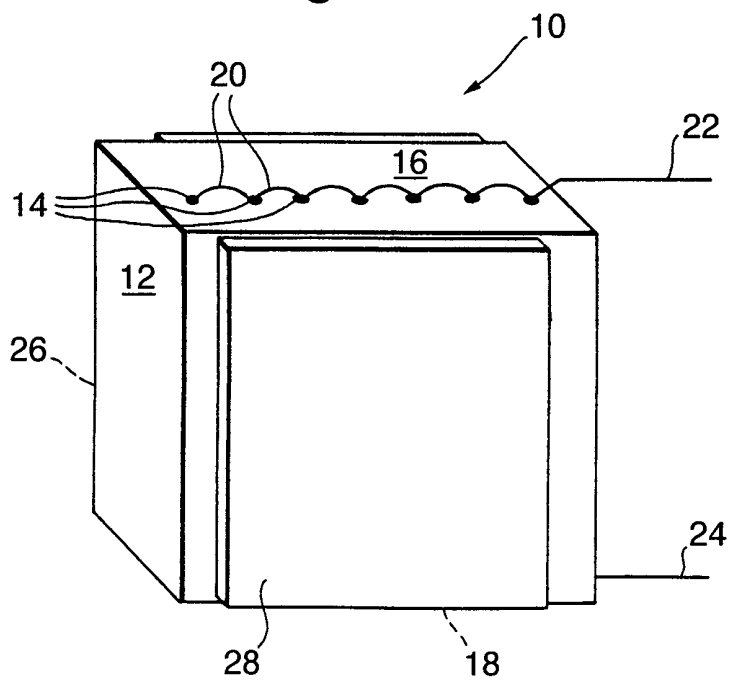


Fig.3.

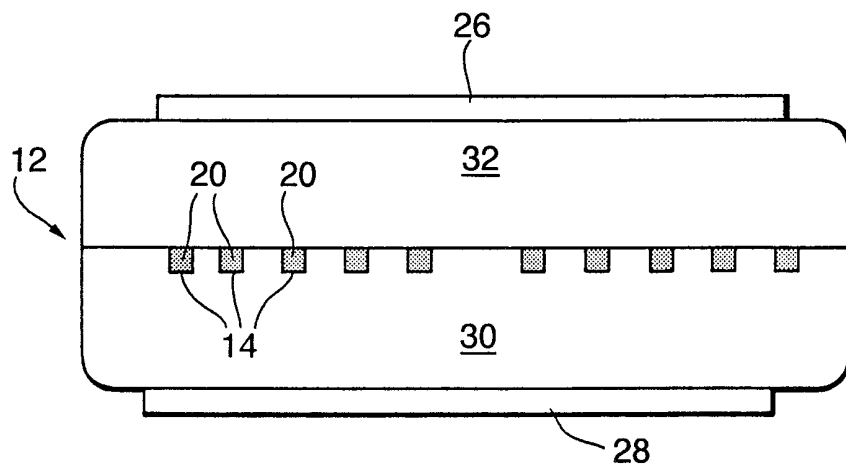


Fig.4.

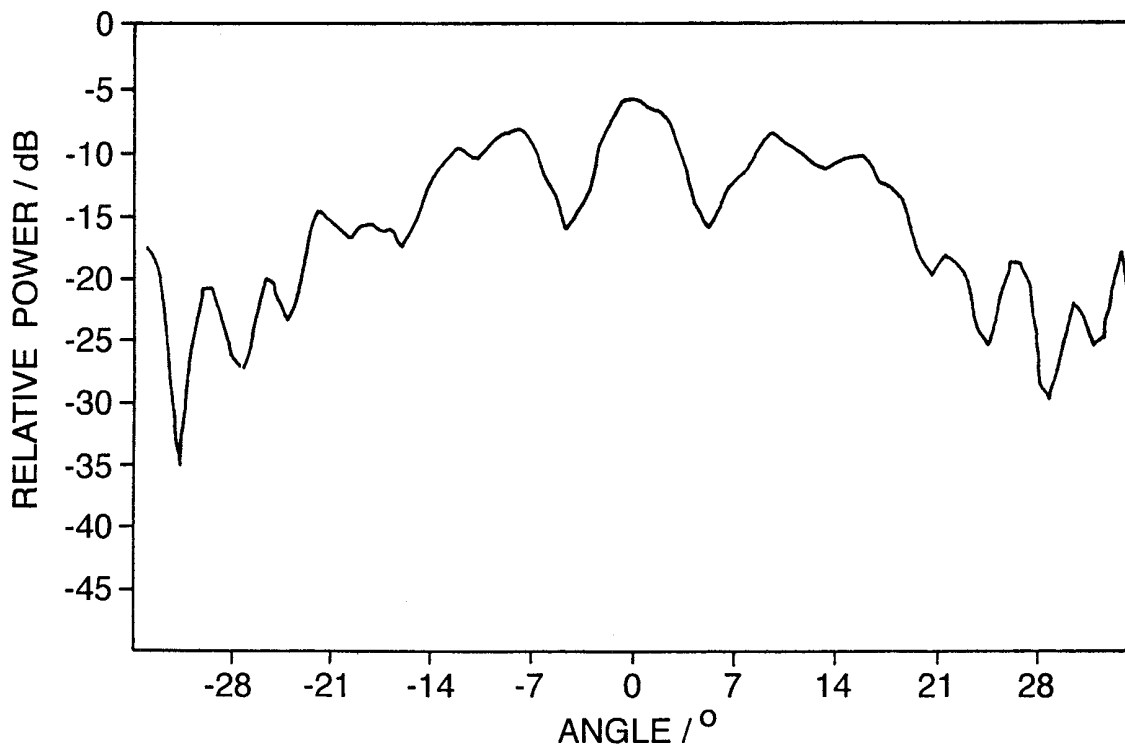


Fig.5.

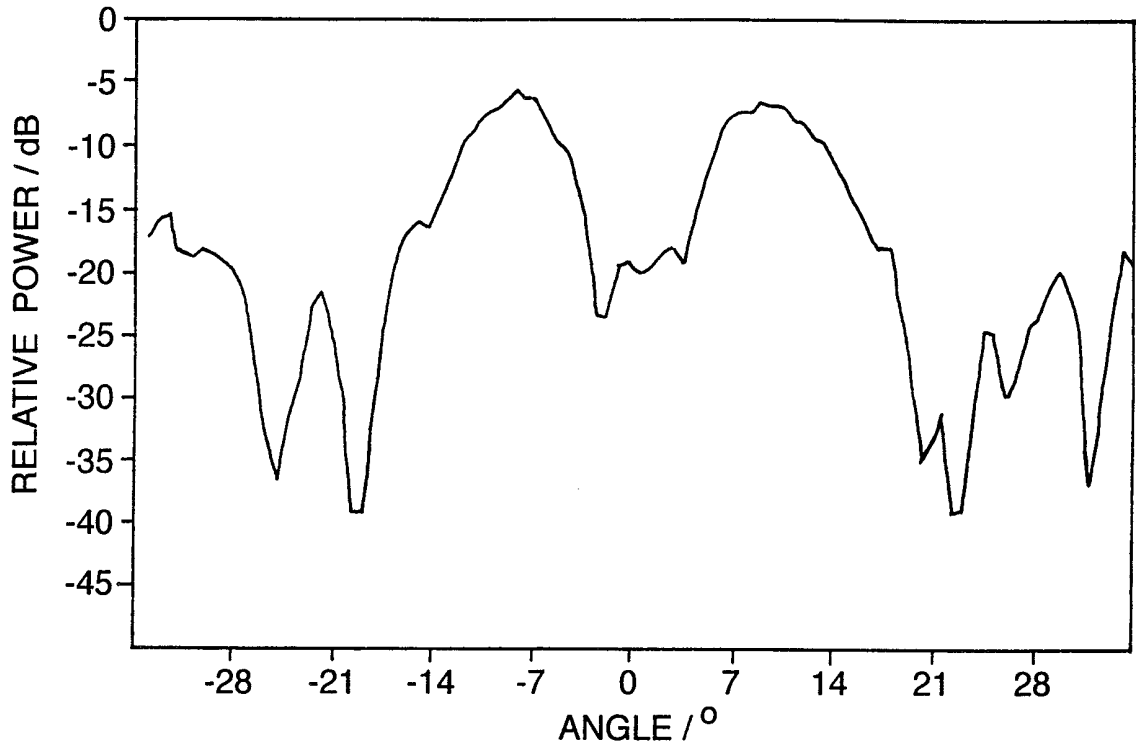


Fig.6.

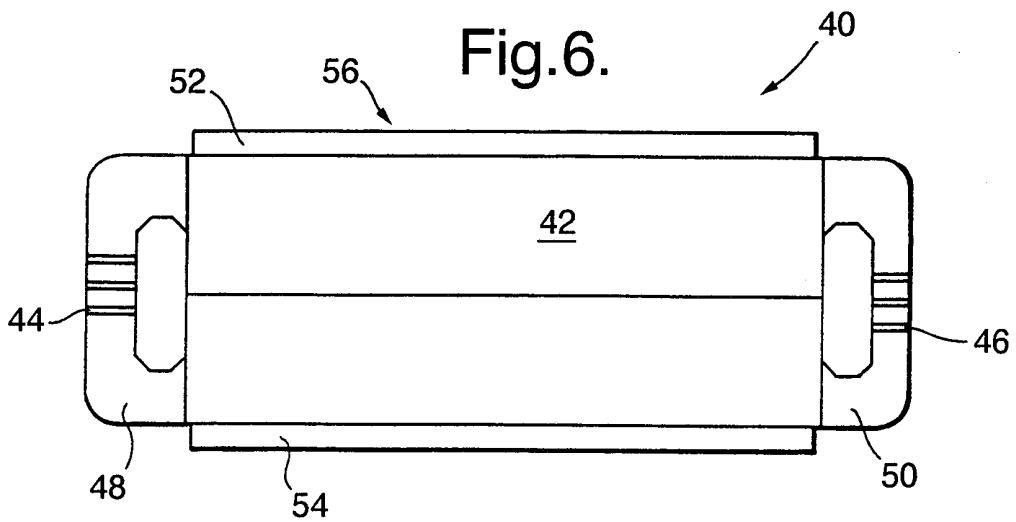


Fig.7. 4/5

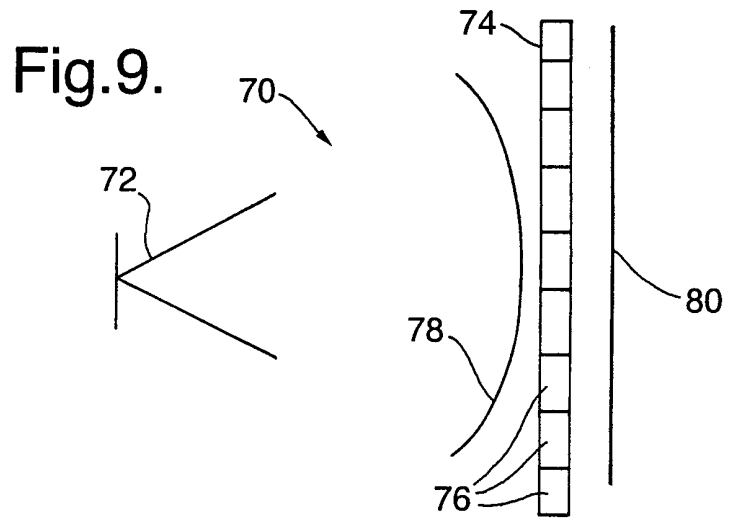
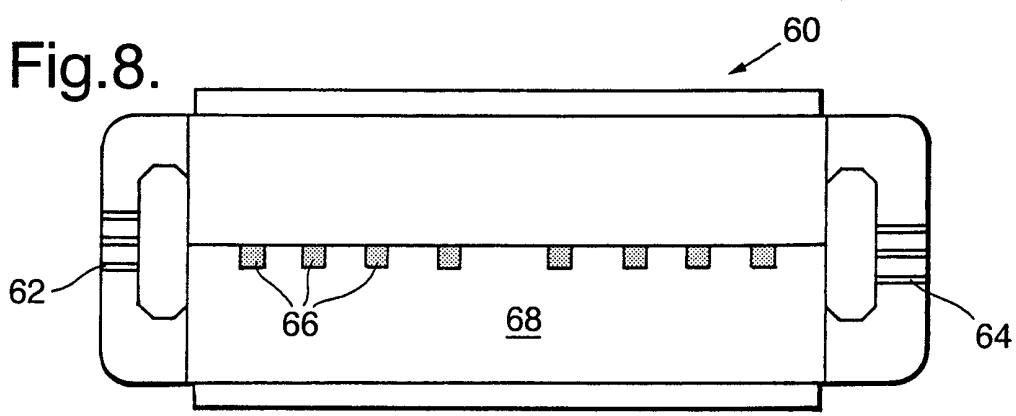
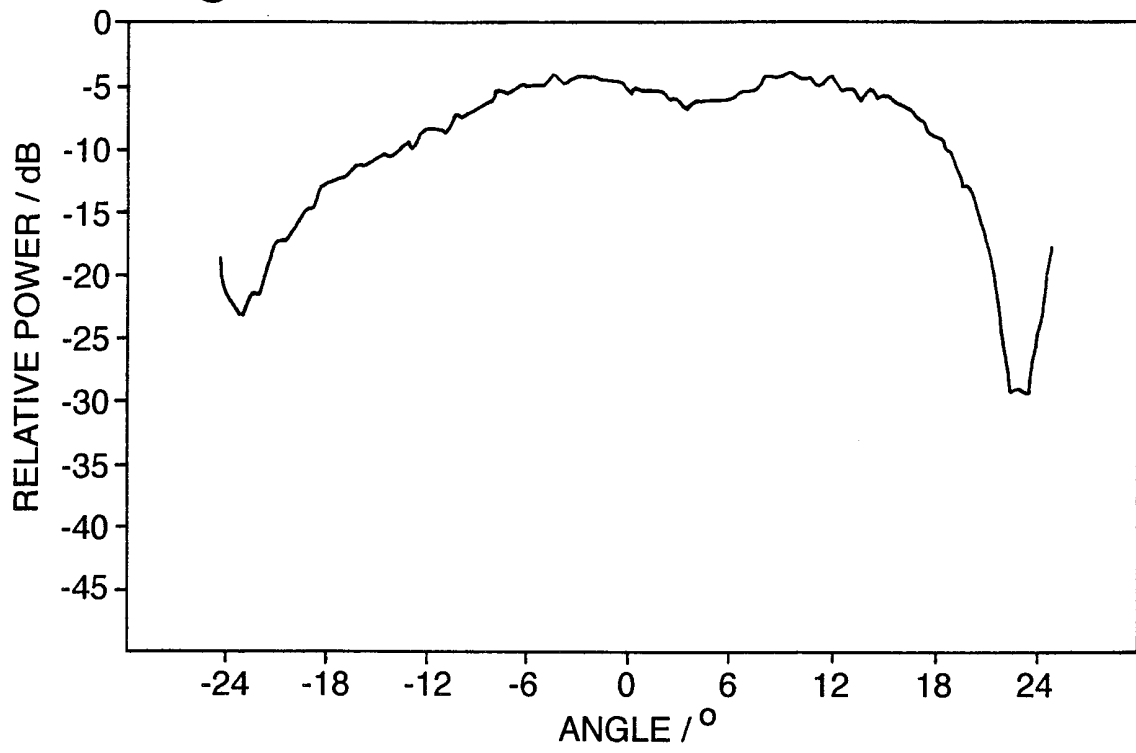


Fig.10.

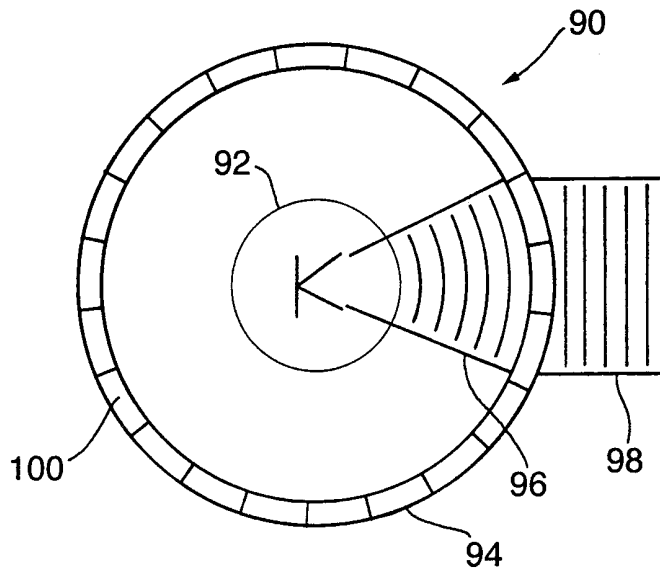


Fig.11.

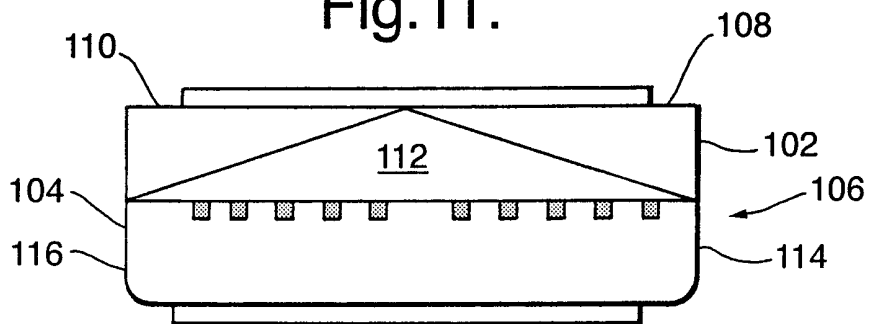
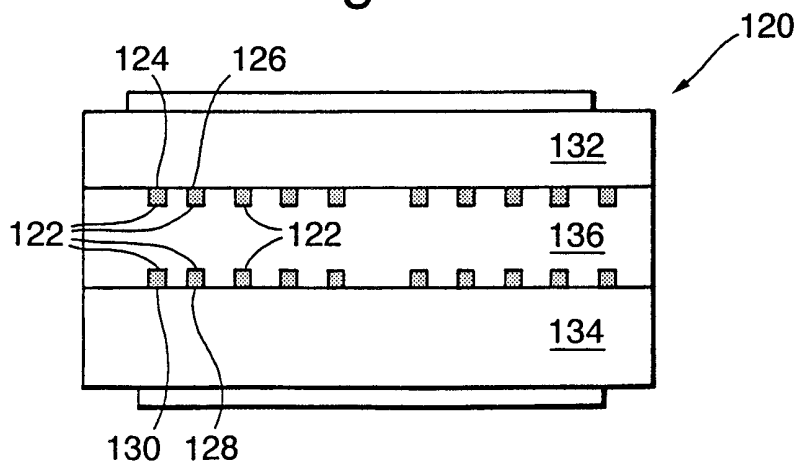


Fig.12.



INTERNATIONAL SEARCH REPORT

International Application No

PCT/GB 98/03722

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 H01Q3/44

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 H01Q G01S

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0 505 040 A (MARCONI GEC LTD) 23 September 1992 see column 1, line 48 - column 2, line 9 see column 3, line 1-18 see column 4, line 5-13; figure 1	1-3, 6-9, 14, 15, 19-25
A	---	29
X	WO 84 01669 A (HUGHES AIRCRAFT CO) 26 April 1984 see page 8, line 6 - page 11, line 32; figures 4,6 --- -/--	1, 4, 5, 7, 10, 12, 13

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

Special categories of cited documents :

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- "P" document published prior to the international filing date but later than the priority date claimed

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Date of the actual completion of the international search

9 March 1999

Date of mailing of the international search report

17/03/1999

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Van Dooren, G

INTERNATIONAL SEARCH REPORT

Int ional Application No
PCT/GB 98/03722

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 515 059 A (HOW HOTON ET AL) 7 May 1996 see column 4, line 36-44 see column 5, line 14-49 see column 6, line 30-43 see column 7, line 8-13; figures 1,2 ---	1,23-28
X	US 2 939 142 A (FERNISLER G L) 31 May 1960 see column 1, line 54 - column 2, line 72; figure 1 ---	1
X	US 3 369 242 A (JOHNSON ROBERT E) 13 February 1968 see column 7, line 33-49; figure 4 ---	1
A	WO 92 16031 A (ALENIA AERITALIA & SELENIA) 17 September 1992 see page 5, line 3-31; figure 2 ---	
A	US 3 765 024 A (CHIRON B ET AL) 9 October 1973 see column 1, line 6-29 -----	

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Information on patent family members

Int ional Application No

PCT/GB 98/03722

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