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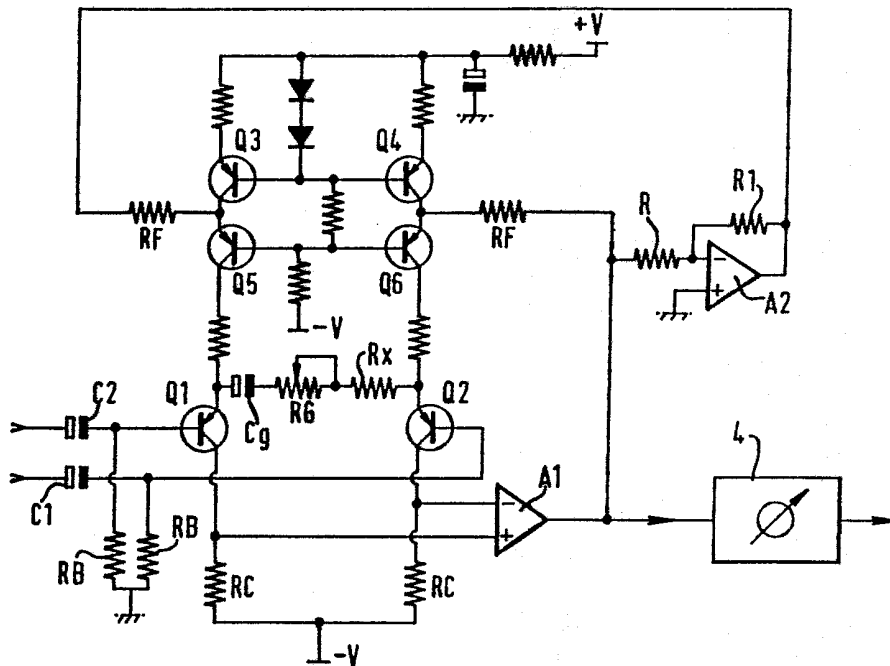
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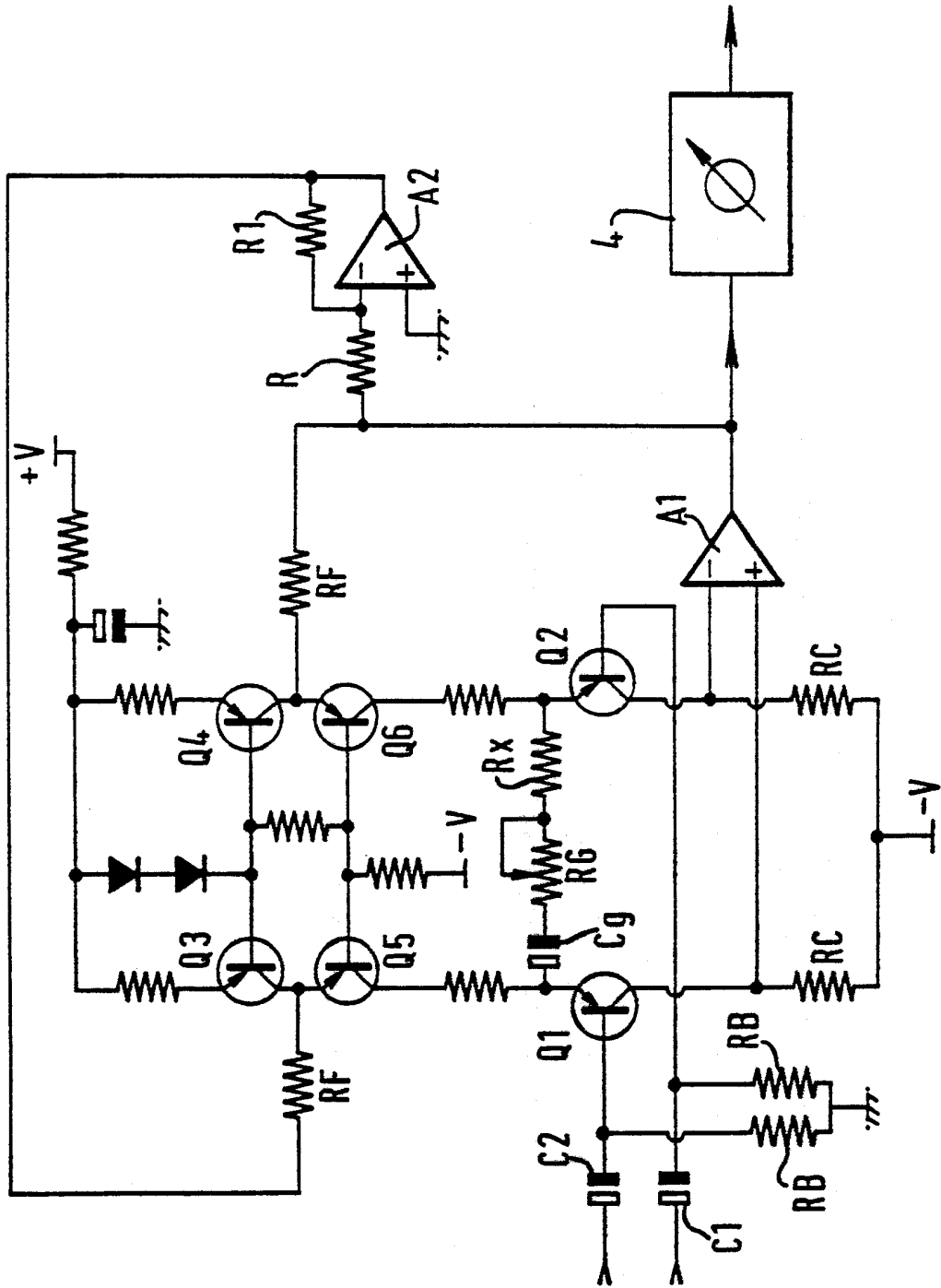
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(54) A preamplifier adjustable to low gain

(57) A preamplifier circuit for amplifying low impedance sources comprises two transistors (Q1 and Q2) connected as a differential pair. The gain is varied by a gain resistor (RG). Two feedback resistors (RF) each couple the output to the emitter of a respective one of the transistors (Q1 and Q2) of the differential pair. A further transistor (Q3, Q4) connected to form a current source is coupled to each transistor (Q1, Q2) of the differential pair.



GB 2 242 089 A



A PREAMPLIFIER

The present invention relates to a preamplifier.

5 Typically, a low impedance moving coil microphone has a source resistance of the order of 200 Ohms, and with such low source impedances the signal voltages are very low and therefore the noise performance of the preamplifier must be very good.

10 The traditional approach to the amplification of signals from such a low-impedance source is to use a transformer to raise both the signal level and the impedance before coupling to a preamplifier. However, 15 transformers are heavy components and relatively expensive and in recent years they have been omitted from commercial preamplifiers. There are existing transformerless preamplifier circuits which perform quite well over part of the gain range required. However, the preamplifier 20 circuits currently available have significant distortion at the top end of the gain range. In addition, these known preamplifiers generally cannot cover the complete gain range required, and in particular cannot provide unity gain (0dB). It is therefore currently necessary to include an 25 additional attenuator, for example a 20dB fixed attenuator or pad, to give access to the bottom end of the gain range.

30 The present invention seeks to provide a preamplifier circuit which has improved performance over a significant gain range.

35 According to the present invention there is provided a preamplifier circuit comprising an amplifying stage having two transistors connected as differential pair, a respective feedback path from the output of the stage to each transistor of the differential pair, and a variable

resistor, for varying the gain of the stage, in the input
circuits of the differential pair of transistors, wherein
the feedback paths include feedback resistors, and a
further transistor connected as a current source is coupled
5 to each transistor of the differential pair.

10 In an embodiment, a respective additional transistor
is connected in cascode with each of said current source
transistors.

Preferably, said variable resistor is a logarithmic
potentiometer.

15 In one embodiment, at least one further variable gain
amplifying stage is provided. The gain of said first
mentioned amplifying stage being arranged to rise with
respect to the movement of a control member in its high
gain region, whilst the gain of the second stage is
attributable to a reverse logarithmic potentiometer and
20 flattens in its high gain region. This enables a
substantially linear overall gain law relative to the
movement of said control member to be produced.

25 An embodiment of the present invention will
hereinafter be described, by way of example, with reference
to the accompanying drawing, in which the Figure shows a
circuit diagram of an embodiment of a preamplifier of the
invention.

30 The preamplifier illustrated is designed to amplify
very low level signals from low source impedances. For
example, the preamplifier of the invention can be used in a
mixing console to receive and amplify signals from a low
impedance moving coil microphone.

35 The Figure shows a preamplifier circuit of the present

invention which is substantially distortion free. This preamplifier has a gain range of the order of 3 to 80 dB, access to the whole range being by way of a single control knob without the need for a separate attenuator.

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The preamplifier circuit shown has a first amplifying stage comprising two pnp transistors Q1 and Q2 connected as a differential pair. The input signals from a microphone (not shown) are coupled to the bases of the transistors Q1, Q2 by way of respective capacitors C1 and C2. The transistor bases are appropriately biased by base resistors RB. A respective collector resistor RC connects the collector of each transistor to the negative supply v-. The outputs of the transistors Q1, Q2 at their collectors are fed to an operational amplifier A1 whose output is the output of the first stage.

It will be seen that the output of the first amplifying stage is fed to a second amplifying stage 4 and by way of a feedback loop to the input circuit of the two transistors Q1, Q2. The output signal is fed back to input circuit of the transistors Q1, Q2 of the differential pair by way of respective feedback resistors RF. To maintain the symmetry of the differential amplifying circuit, the output is directly coupled to the emitter of the transistor Q2 by way of its resistor RF, whereas the output coupled to the emitter of the transistor Q1 has been inverted. This inversion is accomplished by way of a further operational amplifier A2 connected to function simply as an inverter. Thus, as shown, the output of the stage is fed to the inverting input of the amplifier A2 by way of a resistor R whilst its non-inverting input is connected to ground. There is also a feedback connection from the output of the amplifier A2 by way of a resistor R1 to the inverting input. The resistors R and R1 are substantially identical in value, and it will therefore be appreciated that the

operational amplifier A2 and its associated resistors R and R1 are arranged to produce at the output of the amplifier A2 an output signal which is an inversion of that applied to the inverting input.

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The operating point of the differential amplifier is determined by transistors Q3 and Q4 which replace conventional emitter resistors and are connected between the positive supply v+ and the emitters of the transistors Q1, Q2. The transistors Q3, Q4 are connected to form current sources, and thereby effectively to have an infinite output impedance which can be discounted when assessing the gain of the circuit. The provision of current sources instead of emitter resistors enables the amplifying stage to have a practical minimum gain of about 3dB.

The gain of the first amplifying stage is set by the feedback resistors RF and by a gain resistor RG connected between the emitters of the transistors Q1, Q2. The gain resistor RG is implemented by a potentiometer such that its resistance and hence the gain of the first amplifying stage can be varied. Generally, the gain resistor RG will be a reverse logarithmic potentiometer.

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The circuit of the first amplifying stage of the preamplifier of the Figure is symmetrical and the operational amplifier A1 has a high loop gain. These factors provide high linearity over all of the gain range and a high common mode rejection ratio.

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The circuit of the preamplifier also includes additional transistors Q5 and Q6 each connected in cascode with a respective one of the current source transistors Q3 and Q4. The cascode transistors Q5 and Q6 isolate each feedback resistor RF from the gain setting resistor RG so

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that the gain is not determined by potential divider
action. In the circuit shown, the feedback voltage, and
hence the gain, is determined by the simple ratio of the
resistance of RF to that of RG and can therefore be reduced
5 almost indefinitely by increasing the value of RF.

The second amplifying stage 4 is a conventional gain
amplifier whose gain may be varied by way of a reverse
logarithmic variable resistor (not shown). The gain of the
10 second stage 4 is thus the familiar curve, flattened in the
high gain region, attributable to a reverse logarithmic
resistor. This logarithmic resistor is ganged together
with the gain resistor RG of the first amplifying stage and
controlled by a single rotatable control knob (not shown).

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The first amplifying stage of the circuit can provide
a gain in the range 0 to 50dB whilst the second stage 4 is
generally arranged to produce a gain in the range 0 to 30dB
so that the preamplifier has a useful distortionless range
20 of 0 to 80dB. All of this gain is available by adjustment
of the single control knob without the need to switch in
attenuator pads or the like. In addition, the circuit is
distortionless with a high common mode rejection ratio.

25 The circuit of the first stage includes a number of
resistors, diodes and capacitors which have not been
specifically identified. It will be appreciated that these
components set the bias conditions for the various
transistors. The reverse logarithmic potentiometer RG is
30 connected in series with a capacitor Cg and a fixed
resistor Rx whose values are chosen so that the gain
response rises sharply in the high gain region. This means
that the gain response of the first amplifying stage
relative to the rotation of the control knob will combine
35 with the flattened gain characteristic from the second
amplifying stage to approach an overall gain law which is

substantially linear in dB's with respect to the rotation of the control knob.

5 The preamplifier circuit described and claimed herein is also described and illustrated in our copending application no 8719014 (2208053) from which the present application is divided.

10 It will be appreciated that variations and modifications to the circuit particularly described may be made within the scope of the invention.

CLAIMS

1. A preamplifier circuit comprising an amplifying stage having two transistors connected as differential pair, a
5 respective feedback path from the output of the stage to each transistor of the differential pair, and a variable resistor, for varying the gain of the stage, in the input circuits of the differential pair of transistors, wherein the feedback paths include feedback resistors, and a
10 further transistor connected as a current source is coupled to each transistor of the differential pair.
2. A preamplifier circuit as claimed in Claim 1, wherein a respective additional transistor is connected in cascode
15 with each of said current source transistors.
3. A preamplifier circuit as claimed in Claim 1 or 2, wherein said variable resistor is a logarithmic potentiometer.
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4. A preamplifier circuit as claimed in any preceding claim, comprising at least one further amplifying stage coupled to the output of said first mentioned amplifying stage.
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5. A preamplifier circuit as claimed in Claim 4, wherein said further amplifying stage is a variable gain amplifier and wherein a single control knob is arranged to vary the gain of said variable amplifier stage and to adjust said
30 variable resistor.