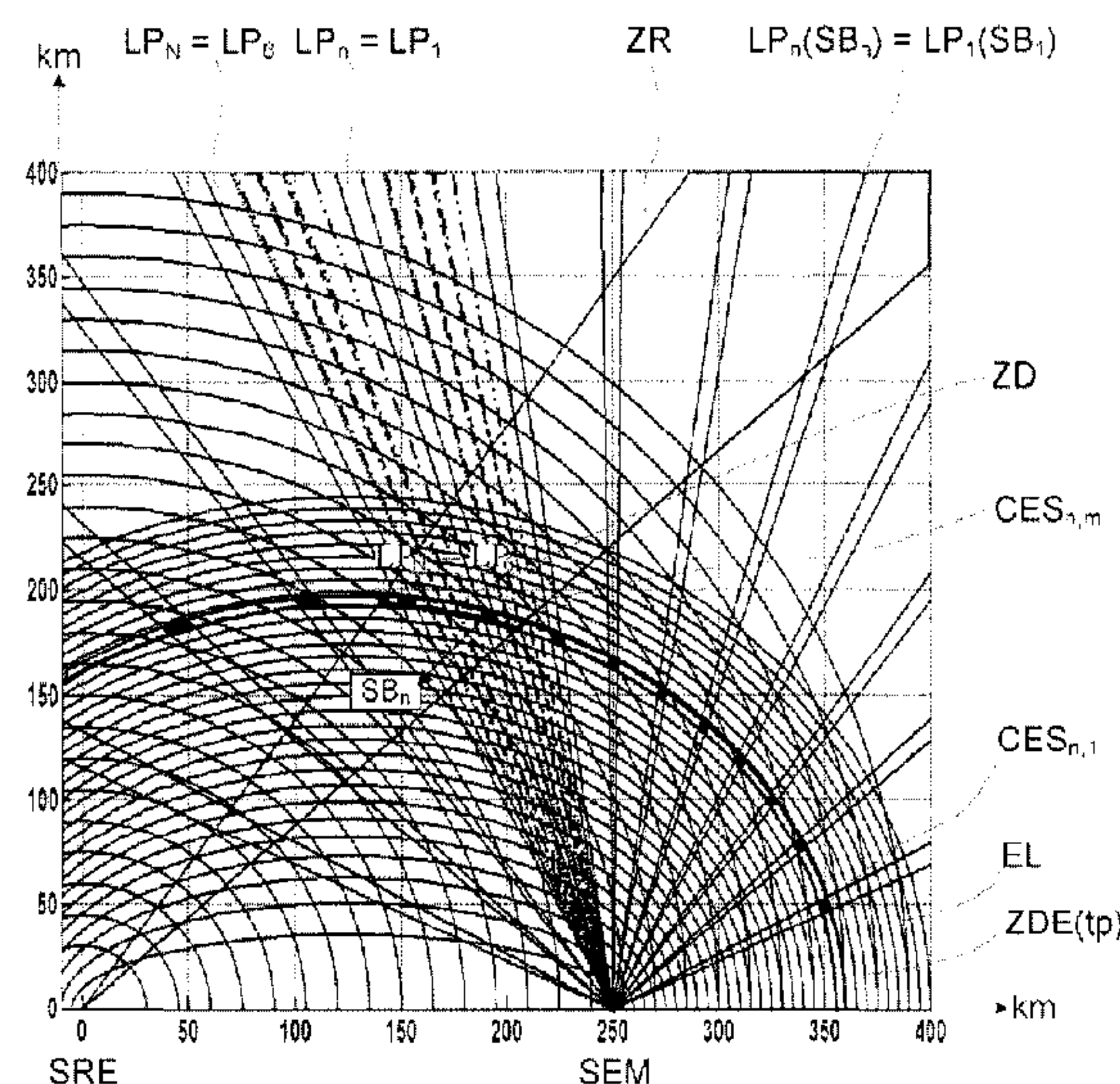




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(57) **Abrégé/Abstract:**

To reduce radar cells and to improve the detection of a radar system, particularly a high-frequency surface wave radar (HFSWR), the broadcast system (SEM) is capable of broadcasting basic orthogonal signals two by two and each orthogonal to itself, temporally shifted to form, respectively, broadcast radiation patterns, each including main radiation lobes (LP_1 , LP_N) alternating with secondary lobes, the main lobes associated with the basic signals being substantially juxtaposed in space. The receiving system (SRE) is capable of forming as many reception patterns in a monitored receiving area (ZR) as cells ($CES_{n,m}$) contained in the receiving area that are covered by main radiation lobes (LP_n) from one of the broadcast radiation patterns and located at a bistatic distance from the broadcast and receiving systems.



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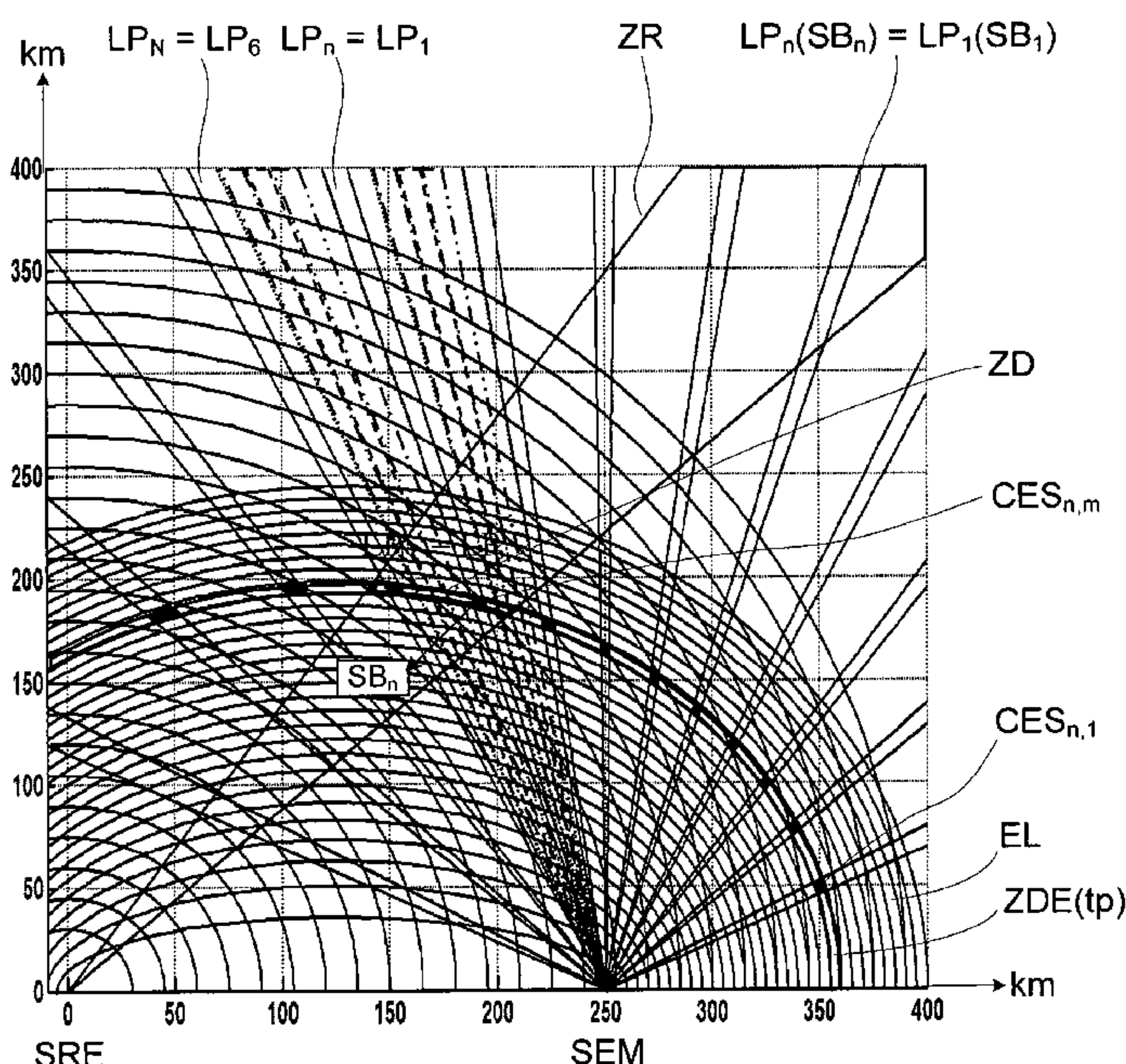
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(54) Title : METHODS AND SYSTEMS FOR ENCODED BROADCASTING AND ANTENNA RECEPTION, PARTICULARLY FOR RADAR

(54) Titre : PROCÉDÉS ET SYSTÈMES D'ÉMISSION CODÉE ET DE RÉCEPTION ANTENNAIRES NOTAMMENT POUR RADAR

FIG. 4



(57) Abstract : To reduce radar cells and to improve the detection of a radar system, particularly a high-frequency surface wave radar (HFSWR), the broadcast system (SEM) is capable of broadcasting basic orthogonal signals two by two and each orthogonal to itself, temporally shifted to form, respectively, broadcast radiation patterns, each including main radiation lobes (LP_1 , LP_N) alternating with secondary lobes, the main lobes associated with the basic signals being substantially juxtaposed in space. The receiving system (SRE) is capable of forming as many reception patterns in a monitored receiving area (ZR) as cells ($CES_{n,m}$) contained in the receiving area that are covered by main radiation lobes (LP_n) from one of the broadcast radiation patterns and located at a bistatic distance from the broadcast and receiving systems.

(57) Abrégé : Pour réduire les cellules radars et améliorer la détection d'un système radar notamment à ondes de surface HFSWR, le système d'émission (SEM) est apte à émettre des signaux de base orthogonaux deux à deux et chacun orthogonal à lui-même décalé temporellement pour former respectivement des diagrammes de rayonnement

[Suite sur la page suivante]

WO 2010/000742 A1

d'émission comprenant chacun des lobes de rayonnement principaux (LP_1 , LP_N) alternés avec des lobes secondaires, les lobes principaux associés aux signaux de base étant sensiblement juxtaposés dans l'espace. Le système de réception (SRE) est apte à former autant de diagrammes de réception dans une zone de réception surveillée (ZR) que de cellules ($CES_{n,m}$) contenues dans la zone de réception, couvertes par des lobes de rayonnement principaux (LP_n) de l'un de diagrammes de rayonnement d'émission, et situées à une distance bistatique des systèmes d'émission et de réception.

METHODS AND SYSTEMS OF ANTENNA ENCODED EMISSION AND RECEPTION, INCLUDING FOR A RADAR

5 The present invention generally relates to antenna emission and reception methods and systems for remote sensing systems, including for radar. More particularly, it relates to beyond-the-horizon detection by surface waves and using the combination of properties of antenna systems and signal coding having orthogonality properties.

10 Such a method finds an application in detecting targets beyond the horizon by surface wave radar systems of the HFSWR ("High Frequency Surface Wave Radar") type. Such a HFWSR radar system is essentially limited by the jumble due to the earth surface, more specifically upon detecting ships for which the useful echo is located, within the Doppler-distance space, in the sea jumble, referred to by specialists as "sea spectrum". The jumble, 15 whether due to the sea (sea spectrum) or to any other cause will be referred to herein as jumble. The echoes of targets are often masked by the jumble having its magnitude in direct relation with the dimension of the radar cell defined by the geometrical dimensions of the volume wherein the radar waves able to be broadcast could, at a given time, take part in forming the signal as 20 received by the radar system.

Taking into account the material possibilities for building the HFSWR radar systems, the radar cells remain, in the prior art, too large for reaching the objectives desired by the users. In order to reach such objectives, it is necessary to reduce the dimensions of such cells by a factor ranging from 25 a few tens to a few hundreds.

In order to reduce the dimensions of the radar resolution cell, the prior art leads to increasing the dimensions of the reception antenna systems, being the bulkiest, when this is possible, leading to geometrically extended systems and to using a large number of antennas. The limitations of such an 30 extension result from several factors being able to separately or simultaneously interfere and making up the drawbacks of the prior art: the footprint, the dimensions of the carrier in mobile systems, the consistency of

the wave front at the reception site, the complexity of processes relating to the number of antennas.

5 This invention aims at overcoming the above mentioned drawbacks and more particularly, at reducing the dimensions of radar resolution cells by a factor able to vary from about **50** to about **500** so as to improve the sensing abilities of radar systems without requiring from the reception antenna system large dimensions.

10 To this end, a method according to this invention for emitting basic signals having orthogonality properties by emission antennas in an emission system and for receiving basic signals by several reception antennas in a reception system, is characterized in that it comprises the following steps:

15 forming emission radiation charts for emitting respectively basic signals for all the emission antennas, each emission radiation chart being associated with a respective basic signal to be emitted by all the emission antennas and comprising main radiation lobes alternating with secondary radiation lobes, the main radiation lobes of the emission radiation charts being substantially alternated and juxtaposed in the space, and

20 forming reception radiation charts in a reception area so as to receive the basic signals for each of the reception antennas, the number of radiation charts being at least equal to the number of cells being contained in the reception area, that is covered by the main radiation lobes of one of the emission radiation charts and being located at a given bistatic distance from the emission and reception systems.

25 This invention further relates to emission and reception systems comprising several emission antennas for emitting basic signals having orthogonality properties and several reception antennas for receiving the basic signals. The emission system is characterized in that it comprises means for forming emission radiation charts for emitting respectively the basic signals for all the emission antennas, each emission radiation chart being associated with
30 a respective basic signal to be emitted by all the emission antennas and comprising main radiation lobes alternating with secondary radiation lobes, the main radiation lobes of the emission radiation charts substantially alternating and being juxtaposed in the space. The reception system is characterized in that it comprises means for forming reception radiation charts in a reception

area so as to receive the basic signals for each of the reception antennas, the number of the reception radiation charts being at least equal to the number of cells being contained in the reception area, that are covered by the main radiation lobes of one of the emission radiation charts and being located at a given bistatic distance from the emission and reception systems.

This invention finds application in radar techniques in general, as well as in channel probing, sonar sensing systems, radio-localization systems or radiography of organs in medical applications or of structures in industrial applications. All the above mentioned applications rely on the analysis of space cells, the dimensions of which are to be reduced in order to increase the performance thereof.

The antenna emission system is able to produce a radio-electric radiation characterized, for example, in a predetermined plane, for example an horizontal one passing through the emission system and the reception system, by surface density maximums of radiated energy being substantially juxtaposed according to a predetermined distribution in the predetermined plane so as to cover a monitored reception area that could cover either partially or totally the predetermined plane. The maximums correspond to the main radiation lobes associated with the radio-electric basic signals. For each basic signal, the radiated energy maximums are contained in conical angular sectors, the apex of which is the emission site and being evenly and periodically distributed in the space. The energy maximums of the basic signal are separated by conical angular sectors of minimum radiation corresponding to the secondary radiation lobes where the energy surface density is much lower than that existing in the conical angular sectors where the energy density maximums are located, corresponding to the main radiation lobes. The radiation chart associated with a basic signal in the predetermined plane is referred to as "laminated chart".

The antenna emission system could produce two or more different laminated radiation charts being substantially juxtaposed, i.e., separated, or adjacent, or not separated, practically with the main lobes juxtaposed or overlapping each other substantially laterally, so as to illuminate together from the emission site where the emission system is arranged, the whole reception area monitored by an antenna reception system according to

this invention. The emission radiation charts are distinct both in azimuth and zenith and have main radiation lobes being secant to the monitored reception area.

5 The basic signals could be digital or analog and should have specific orthogonality properties for improving determining the radar cells in the reception system. To this end, the emission antennas could emit the basic signals simultaneously and periodically, or successively and cyclically in the intervals separating them in time two by two. In the reception system, the basic signals, as reference signals, are respectively associated with respective
10 mathematical operators, that could be, for example, correlations.

According to a first orthogonality property, the basic signals are orthogonal two by two. This means that when the reception system receives all or part of the basic signals to which a mathematical operator is applied, being associated with a respective basic signal selected as the reference signal, the
15 result of the application is independent from the presence or the absence of all or part of the received basic signals other than the reference signal.

According to a second orthogonality property, each basic signal is orthogonal to itself, being offset in time. This means that when the reception system receives a replica of a basic signal to which the mathematical operator
20 is applied, being associated with the respective basic signal selected as the reference signal and being offset in time by a value that is not nil with respect to the reference signal, the result of the application is nil whatever the not nil offset in time.

Such two orthogonality properties are used for discriminating the
25 basic signals in the means for forming reception charts in the reception system. To this end, the reception system could comprise means for weighting the signals captured by the reception antennas, the signal captured by a reception antenna being weighted so as to produce as many weighted signals as reception radiation charts, and means for discriminating in basic signal and
30 bistatic distance in the set of the weighted signals, on the one hand, cells having a constant bistatic distance, on the other hand, for a given bistatic distance, cells associated with one of the basic signals able to be discriminated by their orthogonality properties.

The overall signal emitted by all the emission antennas and distributed in the space is defined by laminated emission radiation charts corresponding respectively to basic signals illuminating each the space. A laminated chart is so-called associated with the respective basic signal, the radiation of which is defined by the laminated chart.

From the reception signal where the reception system is located, there occurs a lacunar paving of the space defined by radar cells and created by the laminated radiation charts associated with the basic signals to be used and by bistatic propagation times between the emission site and the reception site. For a given bistatic propagation time, or for a given bistatic distance, between the emission site and the reception site in a bistatic radar system, the paving corresponds to propagation radar cells located on a half-ellipsoid on which the given bistatic propagation time being equal to the sum of the propagation time between the emission site and a radar cell and of the propagation time between the radar cell and the reception site is constant. In the reception system, radar cells are distinct one from the other, with respect to the substantially separated laminated emission charts, applying the first orthogonality property, and at a constant bistatic propagation time on a half-ellipsoid applying the second orthogonality property. The radar cells, which, for a given basic signal, selected as the reference signal and for a given bistatic propagation time, cannot be distinguished, make up Siamese radar cells associated with the given reference signal and with the given bistatic propagation time and make up in the monitored reception area a strongly lacunar paving of the geometric space on a part of the half-ellipsoid associated with the given bistatic propagation time.

The reception antenna system separates Siamese radar cells being associated with a given basic signal and a given bistatic propagation time and being distributed on a strongly lacunar paving, by means of different reception radiation charts within the monitored reception area. The angle distance between two Siamese radar cells associated with the given basic signal and the given bistatic propagation time and seen from the reception site is significant. The Siamese radar cells associated with the given basic signal and the given bistatic propagation time make up a discrete set in the monitored reception area according to azimuth and zenith directions under which the

Siamese radar cells of such an area are seen from the reception site. Such azimuth and zenith directions locate Siamese radar cells associated with the given basic signal and the given bistatic propagation time in the reception system. The reception antenna system simultaneously forms P reception radiation charts, each reception radiation chart having or not at least one main radiation lobe contained in the reception area.

The reception radiation charts can be laminated like the emission charts. Thus, according to this invention, radiation charts comprising each main radiation lobes alternating with secondary radiation lobes could be formed by one of the pluralities of emission antennas and reception antennas, or even by both pluralities of antennas, the main radiation lobes associated with basic signals being substantially juxtaposed in the predetermined plane.

If M is the number of Siamese radar cells contained in the monitored reception area and located at the intersection of angular sectors covered by the main radiation lobes of the emission radiation chart associated with the given basic signal and a half-ellipsoid defined by the given propagation time between the emission system and a radar cell and a propagation time between the cell and the reception system, the number P of reception radiation charts formed by the reception antenna system is at least equal to M, i.e., is equal to or higher than M.

The signal that can be sent back by each cell is determined using the orthogonality properties allowing, via the mathematical operator associated with the given basic signal, to first discriminate, by the first orthogonality property, the cells associated with basic signals different from the given basic signal selected as the reference signal, then to separate by the second orthogonality property, the cells associated with the given basic signal and having a given bistatic propagation time from the cells associated with the given basic signal and having bistatic propagation times different from the given bistatic propagation time. The radar cells, referred to as Siamese cells, associated with the given basic signal and having the same given bistatic propagation time are separated by polling the reception area by reception charts being different from the reception antenna system, the number thereof being either equal to or higher than the number of radar cells in the reception area.

The space covered by each basic signal is explored by the reception antenna system successively varying all the bistatic propagation times so as to cover all the space illuminated by the basic signal at the intersection with the reception area.

5 The full exploration of the monitored reception area is obtained repeating the above mentioned operations for all the basic signals to be used.

Finally, this invention relates to computer programs able to be implemented respectively in an emission system comprising several emission antennas for emitting basic signals having orthogonality properties and in a
10 reception system comprising several reception antennas for receiving the basic signals. Said programmes are characterized in that they comprise instructions which, when the programs are executed in the emission system and the reception system, implement the emission and the reception method according to this invention.

15 Other characteristics and advantages of the present invention will become more evident reading the following description of several embodiments of this invention given as non limitative examples, with reference to the corresponding appended drawings in which:

- FIG. 1 schematically shows in an horizontal predetermined
20 plane, a laminated radiation chart and a reception area in an angular sector for a bistatic radar system according to the invention;

- FIG. 2 is a schematic block-diagram of an antenna emission system according to this invention;

- FIG. 3 is a laminated emission radiation chart produced by the
25 emission system in FIG. 2;

- FIG. 4 is similar to FIG. 1, but with six laminated emission radiation charts being juxtaposed, only two main lobes of each radiation chart being shown;

- FIG. 5 is a schematic block-diagram of a reception system
30 according to this invention;

- FIG. 6 is a schematic block-diagram of a discriminator receiving stage in the reception system;

- FIG. 7 is similar to FIG. 1, but with a laminated reception radiation chart; and

- FIG. 8 is a time chart of cyclic emissions of basic signals in another embodiment of the emission system.

5 With reference to FIGS. 1, 2 and 5, a SEM-SRE bistatic radar system, for instance, a HFSWR surface wave radar system, for instance for detecting targets by surface wave beyond the horizon, comprises a SEM emission system with several emission antennas AE and a SRE reception system with several reception antennas AR. The emission system is located
10 on an emission site located, for instance, at $D=250$ km from the reception site where the reception system is located.

The SEM emission system produces at least one radio-electric signal defined by a laminated emission radiation chart associated with a SB_n basic signal, when the latter is applied simultaneously under predetermined conditions, to the emission antennas AE, as will be explained further later on.
15 The laminated emission radiation chart associated with the basic signal SB_n is defined essentially by the main radiation lobes LP_n being only shown in FIG. 1. However, the emission system SEM produces the main radiation lobes LP_1 to LP_N of N laminated emission radiation charts associated respectively with
20 basic signals SB_1 to SB_N having orthogonality properties therebetween, with $1 \leq n \leq N$. The main lobes LP_1 to LP_N occur as conical angular sectors having an angle at the predetermined apex in a predetermined radiation plane, for example horizontal passing through the site of the emission system SEM. FIG. 1 is located in a radiation horizontal plane crossing both the emission and
25 the reception sites.

The emission system SEM of the invention producing laminated radiation charts can have an antenna structure belonging to the known class of antenna networks with ambiguous radiation charts, also so-called ambiguous networks. For example, an ambiguous network is got from a linear network of
30 S emission antennas AE_1 to AE_S , with $2 \leq S$, wherein the antennas are separated from each other by a distance DA higher than $\lambda/2$, where λ is the wavelength of a carrier modulated by the basic signals being emitted.

In FIG. 2 showing a first embodiment of the emission system SEM schematically functional blocks only are shown, ensuring useful functions for understanding this invention et having a link with the latter. Such functional blocks can correspond to dedicated or programmable hardware modules and/or to software modules implemented in at least one microprocessor.

The emission system SEM comprises $S = 7$ antennas AE_1 to $AE_S = AE_7$ evenly spaced by $DA = 12.5 \lambda$ for example. The emission system SEM further comprises emitting stages EM and weighting circuitry CPE_1 to CPE_S interconnected respectively between the outlet of a power distributor in the emitting stages EM and inlets of antennas AE_1 to AE_S . A weighting circuit CPE_s , with $1 \leq s \leq S$, weights the amplitude and/or the phase of the basic signals $SB_1, \dots, SB_n, \dots, SB_N$ distributed respectively by the emitting stages EM with respective complex weighting coefficients $w_{1,s}, \dots, w_{n,s}, \dots, w_{N,s}$. The basic signal SB_n distributed at the antennas AE_1 to $AE_S = AE_7$ is weighted respectively by complex weighting coefficients $w_{n,1}$ to $w_{n,S} = w_{n,7}$ in the weighting circuits CPE_1 to CPE_S so that the antennas AE_1 to AE_S emit a radio-electric signal characterized by a laminated radiation chart according to this invention and associated with the basic signal SB_n . This ensures a sufficiently significant protection on the secondary lobes of the charts and allows the orientation of the main lobes LP_n associated with the basic signal SB_n . The larger the distance DA between the antennas, the more the number of main lobes of the laminated radiation charts increases. The larger the number of antennas, the more the number N of laminated emission radiation charts increases.

In this first embodiment, the basic signals are made up by families of orthogonal basic signals with a perfect or nearly perfect correlation being emitted by the emission system SEM simultaneously by the addition of basic signals or simultaneously by intertwining the basic signals.

On FIG. 3, two laminated radiation charts with main lobes LP_n and LP_m are juxtaposed, respectively associated with two distinct basic signals SB_n and SB_m to which complex weighting coefficients $w_{n,1}$ to $w_{n,S}$ and $w_{m,1}$ to $w_{m,S}$ have been applied by the weighting circuitry CPE_1 to CPE_S . The protection on the secondary lobes LS is of 26 dB. The chart with the main

lobes LP_n is oriented so as to locate a main lobe according to the direction 0 degree. The other chart with main lobes LP_m is oriented so as to locate a main lobe according to the direction 1,2 degrees.

Those skilled in the art will understand that such lacunar radiation charts could be achieved by other emission systems having the antennas with other linear, surface or volume, even or uneven distributions. For example, the emission system could comprise an antenna network according to an uneven structure such as a fractal structure according to article "THEORIE FRACTALE DES GRANDS RESEAUX D'ANTENNES LACUNAIRES" C. GOUTELARD, AGARD Conference Proceedings **528**, Radiolocation Techniques, Londres, 1^{er} au 5 juin 1992.

The antenna reception system SRE monitors one or more reception areas. In FIG. 1, it is assumed that the reception system only monitors one single conical reception area ZR being secant to at least one of the main radiation lobes of the laminated emission radiation chart associated with each basic signal SB_n . In practice, the reception area ZR is secant to several main radiation lobes associated with each basic signal.

FIG. 1 also shows partially with thin lines the elliptic parallel tracks of half-ellipsoids EL having as foci the emission system SEM and the reception system SRE. Each half-ellipsoid EL is defined by a surface on which any radar cell CE receives a radio-electric signal from the emission system SEM and is likely to broadcast it to the reception system SRE for a respective given bistatic propagation time t_p , corresponding to a bistatic distance. The given bistatic propagation time t_p equal to the sum of the propagation time between the emission system SEM and the radar cell CE and of the propagation time between the radar cell CE and the reception system SRE is constant for any radar cell on the surface of the ellipsoid EL.

The half-ellipsoids become half-spheres when the radar system SEM-SRE is monostatic, i.e., the emission and the reception systems are located on the same site, or half-ellipsoids nearly as half-spheres when the emission and the reception systems are close so that the distance separating them remains small with respect to the distances from the cells contained in the monitored reception area.

Extended distance resolution areas ZDE, one of them being illustrated in FIG. 4 are defined between the half-ellipsoids EL so that the difference in bistatic propagation times is equal to the time resolution, for example, 1.5 km, of the radar. The intersection of an extended distance resolution area ZDE and of the reception area ZR determines a monitored distance resolution area ZD corresponding to a respective bistatic propagation time t_p and also to a selected time resolution.

The intersections of an ellipsoid extended distance resolution area ZDE and of the main radiation lobes LP_n define Siamese radar cells CES_n associated with the basic signal SB_n and with the bistatic propagation time t_p defining the area ZDE, as shown in FIG. 4. The Siamese radar cells CES_n associated with the basic signal SB_n and the bistatic propagation time t_p and located in the reception area ZR are geographical areas being common to the distance resolution area ZD, to the main lobes LP_n of the laminated chart associated with the basic signal SB_n and to the reception area ZR of the radiation chart of the antenna reception system SRE, as shown in FIG. 1.

The radar system of this invention delimits the Siamese radar cells CES_n particularly through the space delimitation brought by the main lobes LP_n of the laminated emission chart associated with the basic signal SB_n in the antenna emission system SEM, of the reception area ZR of the antenna reception system SRE and through the orthogonality of the basic signals provided in the emission system.

Referring to FIG. 5 illustrating an embodiment of the reception system SRE, it schematically shows only functional blocks filling functions useful for understanding this invention and related to the latter. Such functional blocks could correspond to dedicated or programmable hardware modules and/or to software modules implemented in at least one microprocessor.

The reception system SRE comprises several reception antennas, for example $U = 4$ antennas AR_1 to AR_4 and P receiving stages RE_1 to RE_P associated respectively with P reception antenna charts so as to discriminate Siamese cells on a half-ellipsoid EL relating to each laminated emission chart and thus with each basic signal SB_n . In the reception system SRE, each reception antenna AR_u , with $1 \leq u \leq U$, distributes the signal it

receives to P receiving stages RE_1 to RE_P respectively through weighting circuitry $CPR_{1,u}$ to $CPR_{P,u}$.

The U weighting circuitry $CPR_{p,1}$ to $CPR_{p,U}$ connected to a receiving stage RE_p , with $1 \leq p \leq P$, weight the amplitude and/or the phase of the signals captured by the antennas AR_1 to AR_U respectively by complex weighting coefficients $v_{p,1}$ to $v_{p,U}$ defining the angular orientation of a respective reception chart. The receiving stage RE_p is associated with a case of angular positioning of radar cells covered by at least one main lobe of the respective reception chart. To this end, as shown in FIG. 6, the receiving stage RE_p comprises N parallel discriminators $DIS_{p,1}$ to $DIS_{p,N}$ for discriminating into basic signal and bistatic propagation time in the set of the weighted signals received essentially in a respective reception area. Each discriminator $DIS_{p,n}$ of the receiving stage RE_p is associated with a basic signal SB_n as a reference signal S_{ref} for discriminating in the jumble of weighted signals received according to the reception area, the radar cells on the one hand having a constant bistatic propagation time and thus, a constant bistatic distance, on the other hand, for a given bistatic propagation time, the Siamese radar cells associated with the basic signal SB_n among the basic signals SB_1 to SB_N able to be discriminated through their orthogonality properties. The discriminators $DIS_{p,1}$ to $DIS_{p,N}$ thus distinguish the radar cells associated with the basic signals SB_1 to SB_N according to a respective reception area and for different bistatic propagation times.

Each one of the discriminators $DIS_{1,n}$ to $DIS_{P,n}$ in the reception system SRE selects the main lobes LP_n of the laminated chart specific to the basic signal SB_n by means of the first and the second orthogonality properties of the basic signals SB_1 to SB_N . The reception system knows a priori the basic signals SB_1 to SB_N , for example as predetermined numeral sequences, which, as reference signals are periodically read out in the memory of the reception system and respectively applied to the discriminators. Through implementing the first orthogonality property relating to the orthogonality of the basic signals two by two, each one of the discriminators $DIS_{1,n}$ to $DIS_{P,n}$ operates, for example, as a correlator or a convolution device selects the basic signal SB_n in the mixed signal received by the respective receiving stage RE_1 to RE_P ,

independently from the fact that the mixed signal contains all or part of the other received basic signals SB_1 to SB_{n-1} and SB_{n+1} to SB_N . The discriminators $DIS_{1,n}$ to $DIS_{P,n}$ thus select the radar cells at the intersection of the main emission radiation lobes LP_n and of the reception area ZR covered by the reception chart.

In the case of a prior art detection with a monostatic radar system located at the reception site, the reception cell is limited by the main lobe of the reception network and the time resolution. In FIG. 1, the reception area ZR has been selected in proximity to the main lobe of the reception chart used according to the prior art. The time resolution according to the prior art is lower than achieved in this invention as the used known signals do not impart the detection performance that is achieved with the basic signals used in this invention. The main lobes of the laminated emission charts according to this invention conjugated to the basic signals used in the invention help to reduce the time resolution by a factor K_r of the order of 3 to 5 and by the same factor the dimension of the radar cells obtained with this invention. A radar cell obtained according to the prior art is shown in FIG. 1 at the intersection of the space between the reception area ZR and two half-circles centred on the receiving system SRE and distant by a distance resolution increment of 15 km for example.

FIG. 4 partially shows an exemplary paving of radar cells obtained according to this invention with the assumptions taken for FIG. 1, through the use of all the basic signals and the associated processing in the radar system SEM-SRE. The partial paving is at the intersection of the reception area ZR, of an extended ellipsoid distance resolution area ZDE for a given bistatic propagation time t_p and of the main lobes LP_1 to $LP_N = LP_6$ being juxtaposed and intertwined. In order to avoid overloading FIG. 4, the main lobes LP_1 to LP_N are shown on two angular periods of $N = 6$ laminated charts attributed to different basic signals SB_1 to $SB_N = SB_6$. The main lobes are, as has been previously indicated, able to be discriminated by the orthogonality of the basic signals in the discriminators $DIS_{1,1}$ to $DIS_{P,N}$.

The different Siamese radar cells CES_1 to CES_N associated with a bistatic propagation time t_p and to all the basic signals SB_1 to SB_N pave the

distance resolution area ZD. The Siamese radar cells respectively associated with couples (SB_1, tp) to (SB_N, tp) can be separated as long as the basic signals with which they are associated are different.

FIG. 4 also shows the extended distance resolution area ZDE corresponding to a given bistatic propagation time tp and a selected resolution distance being extended to the space able to be monitored. The Siamese radar cells $CES_n = CES_1$ associated with the couple (SB_n, tp) are located at the intersection of the extended distance resolution area ZDE and the main lobes LP_n of the laminated emission chart associated with the basic signal SB_n .

The m^{th} Siamese radar cell $CES_{n,m}$ associated with the couple (SB_n, tp) and covered by the reception area ZR is able to broadcast toward the reception system SRE a signal:

$$Sr_{n,m} = \alpha_{nm} \times SER_{n,m} \times SB_n(tp),$$

α_{nm} being a propagation attenuation, and $SER_{n,m}$ the radar equivalent surface of the Siamese radar cell $CES_{n,m}$ associated with the couple (SB_n, tp) . Such a couple defines the replica $SB_n(tp)$ of the signal SB_n temporally offset from the bistatic propagation time tp .

The antenna reception system SRE forms, via the antennas AR_1 to AR_U and the weighting circuitry $CP_{1,1}$ to $RE_{P,U}$, P reception radiation charts with respective main lobes LP_1 to LP_P . For a reception area ZR containing M Siamese radar cells associated with the couple (SB_n, tp) , for example, two cells CES_n in FIG. 4, with $M \leq P$, each signal S_p captured by the reception antenna networks AR_1 to AR_U for the p^{th} reception chart processed by the receiving stage RE_p , with $1 \leq p \leq P$, is expressed as follows:

$$S_p = \sum_{m \in M} G_p(\theta_{r,n,m}, \varphi_{r,n,m}) \times Sr_{n,m} + T(SB_e, tp_e),$$

where $(\theta_{r,n,m}, \varphi_{r,n,m})$ is the angular direction in azimuth $\theta_{r,n,m}$ and zenith $\varphi_{r,n,m}$ of the m^{th} Siamese radar cell $CES_{n,m}$ associated with the couple (SB_n, tp) . $G_p(\theta_{r,n,m}, \varphi_{r,n,m})$ is the gain of the p^{th} reception radiation chart according to the azimuth and the zenith direction $(\theta_{r,n,m}, \varphi_{r,n,m})$. The signal $T(SB_e, tp_e)$ represents the sum of all the signals received by the antenna reception system and able to be retro-broadcast by radar cells illuminated by the emission charts associated with the other basic signals SB_1 to SB_{n-1} and SB_{n+1} to SB_N than the signal SB_n and by the radar cells illuminated by the chart associated with the

basic signal SB_n and located in correspondence to bistatic propagation times tp_e being different from the given propagation time tp .

The discriminators $DIS_{1,n}$ to $DIS_{P,n}$ using the basic signal SB_n as the reference signal eliminate as a result of the first orthogonality property previously being defined the radar cells helping to form the signal $T(SB_e, tp_e)$ associated with one or more other basic signals than the signal SB_n . For the given bistatic propagation time tp , the discriminators $DIS_{1,n}$ to $DIS_{P,n}$ also eliminate the radar cells helping to form the signal $T(SB_e, tp_e)$ and associated with the basic signal SB_n and to other bistatic propagation times tp_e than the given bistatic propagation time tp , applying the second previously defined orthogonality property, for example relying on an autocorrelation, wherein each basic signal is orthogonal to itself being offset in time.

Both orthogonality properties can be achieved with families of encoded symbol sequences making up periodically and respectively the basic signals SB_1 to SB_N , such that the cross-correlation function between the sequences is strictly nil, whatever the time offset between the sequences and the perfect or nearly perfect character of the cross-correlation and of the autocorrelation functions applied to the basic signals received in the discriminators. The sequences are emitted cyclically modulating a common carrier in the emission system SEM. A correlation function of a sequence is referred to as nearly perfect if the correlation function is not nil for any point that differs from the central peak with a nil offset of the sequence and a few evenly spaced points on the correlation function of a predetermined number of symbols. As an example, the sequences GQ (Goutelard Q-ary sequences) built according to the article "LES SEQUENCES GQ SEQUENCES Q-AIRE ORTHOGONALES A CORRELATION PARFAITE", C. GOUTELARD, AGARD CONFERENCE PROCEEDINGS **574**, SPP Symposium, "Digital Communications Systems: Propagation Effects, Technical Solutions, Systems Design", Athènes, Grèce, **18 au 21 septembre 1995**, CP-**574**, meet the first and the second orthogonality properties.

The discriminators $DIS_{1,n}$ to $DIS_{P,n}$ associated with the basic signal SB_n perform, for example, a correlation, or an equivalent operation such

as, for example, a convolution. The discriminator $DIS_{p,n}$ delivers a standardized signal $R_{p,n}$ of the type:

$$R_{p,n} = \sum_{m \in M} Kop \times G_p(\theta_{r,n,m}, \varphi_{r,n,m}) \times \alpha_{n,m} \times SER_{n,m},$$

Kop being a transformation coefficient for the mathematical operator in the discriminators $DIS_{1,n}$ to $DIS_{P,n}$ between the signal S_p and the signal R_p .

For the given bistatic propagation time tp , the discriminators $DIS_{1,n}$ to $DIS_{P,n}$ supply a system of P equations corresponding to the P signals $R_{1,n}$ to $R_{P,n}$ being measured with the P reception radiation charts, having M unknown factors $\alpha_{n,1} \times SER_{n,1}$ to $\alpha_{n,M} \times SER_{n,M}$ corresponding to the Siamese radar cells $CES_{n,1}$ to $CES_{n,M}$ associated with the couple (SB_n, tp) and included in the monitored reception area, the number P being equal to or higher than M . If $P = M$, the equation system is determined and makes up a Cramer's system. If $P > M$, the equation system is over-determined and can be operated for increasing the accuracy of calculations.

For each one of the bistatic propagation times and thus, for each one of the bistatic distances, the discriminators $DIS_{1,n}$ to $DIS_{P,n}$ supply a system of P equations corresponding to P signals $R_{1,n}$ to $R_{P,n}$ measured with the P reception radiation charts, having as many unknown factors as Siamese radar cells being associated with the couple of the basic signal SB_n and of the said each one of the bistatic propagation times and included in the monitored reception area. The number P is equal to or higher than the number of above mentioned Siamese radar cells.

More generally, all the signals $R_{1,1}$ to $R_{P,N}$ supplied by the discriminators $DIS_{1,1}$ to $DIS_{P,N}$ are used for determining all the basic signals sent back by the Siamese cells illuminated by the main lobes LP_1 to LP_N of the emission charts and located in the reception area ZR .

According to various embodiments, the reception system can cover a more or less extended reception area ZR .

In the embodiment as illustrated in FIG. 1, the reception area ZR is limited to part of the area to be monitored and the exploration of the monitored reception area is made by the antenna reception system SRE by a set of Q reception areas completely paving the monitored area. Q linear equation systems are to be solved.

In the embodiment as illustrated in FIG. 4, the reception area ZR is extended to all the monitored reception area. One single linear equation system ($Q = 1$) is to be solved.

5 In the embodiment illustrated in FIG. 7, the monitored reception area ZR is achieved with a set of laminated charts at the reception, the main lobes LP_p of a single one of which, alternating with secondary radiation lobes, are shown. The antennas in the reception system could make up a lacunar network or a network producing ambiguous radiation charts. Main lobes of the laminated reception radiation charts are substantially juxtaposed so as to cover
10 the monitored reception area, similarly to the juxtaposition of the main lobes of the laminated emission charts shown in FIG. 4. Such a solution increases the number Q of linear equation systems, but reduces the number of unknown factors of each equation system. The main lobes of each emission chart can be in any number or reduced to only one.

15 The dimensions of the antenna reception system SRE vary as a function of the solution being adopted.

In FIG. 1, there is shown a reception area ZR the dimension of which is typically that of a main reception lobe of a prior art reception system. FIG. 4 shows $M = 12$ Siamese radar cells associated with the couple
20 ($SB_n = SB_1$, tp) in the quadrant delimited by FIG. 4.

The dimensions of the reception area remain unchanged, but the size of the radar cells according to this invention is reduced with respect to the prior art, i.e. $M \times N = 72$ in FIG. 4. Such a reduction according to the invention could be as high as several hundreds.

25 This invention relies on basic signals that should have the first and the second above mentioned orthogonality properties. Any signal having such orthogonality properties can be used in this invention for forming a family of basic signals.

The time chart in FIG. 8 shows a second embodiment such that
30 the emission system SEM emits basic signals having the first and the second orthogonality properties.

At the beginning of a cycle of N periods, the emission system emits a basic signal SB_1 of a duration T_{sb} followed with a nil signal, the

duration of which is equal to or higher than the maximum bistatic propagation time $tp_{\max}$ so as to cover the monitored reception area. Then, during the following period, the emission system emits a basic signal SB_2 followed by a duration being at least equal to $tp_{\max}$, then the other signals being separated temporally two by two by at least $tp_{\max}$ up to the last basic signal SB_N . Another cycle of successive emissions of basic signals then starts, similar to that previously described.

The double orthogonality condition is met.

The first orthogonality is met by the temporal separation of laminated emission charts that are associated with the signals SB_1 to SB_N and only occur at different times, whatever the time. The reception system could only receive one single non nil basic signal at a time. In such a case, the signals SB_1 to SB_N could be identical to a same signal showing the second orthogonality.

The second orthogonality is met if each non nil basic signal possesses such a property, i.e. if the replicas thereof can be separated over time. Such a property is met for a large number of sequences, but also for a single isolated pulse. The basic non nil signal SB_1 to SB_N could be made up of a sequence or a string of identical or not identical sequences, or an isolated pulse or a string of isolated pulses.

In addition to a large reduction of a radar cell, this invention provides a significant improvement of the performance of any sensing, electromagnetic or acoustic system, being faced to the problem of detecting a target, the signature of which should be extracted from a signal containing a jumble dependent on the dimension of the radar cell of the sensing system. The invention further provides a significant gain with respect to the space discrimination of targets able to be present in the monitored reception area.

The invention finds numerous applications in all the electromagnetic sensing systems including radars, sonars, radio-localisation systems, systems for probing channels, medical radiography systems and industrial radiography systems.

The advantages being provided are particularly important in cases where it is impossible, whatever the reason, to impart to antenna

systems, more particularly, to an antenna reception system being most often the bulkiest, dimensions that it should have for achieving resolutions obtained with this invention and that could only be achieved in the prior art after the significant increase, of a factor of about several tens, of the dimensions of the antenna reception system.

The invention as described herein relates to an emission and reception method and to emission and reception systems for emitting basic signals having orthogonality properties by antennas in the emission system and several reception antennas in the reception system for receiving basic signals. According to an implementation, the emission and reception method according to this invention is determined by the instructions of computer programs incorporated into emission and reception systems. The programs comprise program instructions that, when said programs are carried out in emission and reception systems, the operation of which is then controlled, more specifically, through carrying out programs, implement the emission and reception method according to this invention.

Consequently, the invention further applies on computer programs, more specifically computer programs recorded on or in one or more of computer readable recording media and any data processing device, adapted for implementing this invention. Such programs could use any programming language, and be in the form of a source code, an object code or a code intermediary between a source code and an object objet such as in a partially compiled form, or in any other form desired for implementing the method of this invention.

A recording medium could be any unit or device able to store programs.

CLAIMS

1. A radar detection method for emitting basic signals (SB_1, SB_N) having orthogonality properties by emission antennas (AE_1, AE_S) in an emission system (SEM) and receiving the basic signals by several reception antennas (AR_1, AR_U) in a reception system (SRE), characterized in that it comprises the following steps of:
 forming emission radiation charts for emitting respectively basic signals for all the emission antennas (AE_1, AE_S), each emission radiation chart being associated with a respective basic signal (SB_n) to be emitted by all the emission antennas and comprising the main radiation lobes (LP_1, LP_N) alternating with secondary radiation lobes (LS), the main radiation lobes of the emission radiation charts substantially alternating and juxtaposed in the space,
 forming reception radiation charts in a reception area (ZR) so as to receive the basic signals by each one of the reception antennas (AR_1, AR_U), the number of the reception radiation charts being at least equal to the number of cells ($CES_{n,m}$) being contained in the reception area, that are covered by the main radiation lobes (LP_n) of one of the emission radiation charts and being located at a given bistatic distance from the emission and reception systems,
 weighting, in the SRE, the signals captured by the reception antennas (AR_1, AR_U), the signal captured by a reception antenna being weighted so as to produce as many weighted signals as reception radiation charts, and
 discriminating, in the SRE, in basic signal and bistatic distance in the set of weighted signals for discriminating, on the one hand, cells having a constant bistatic distance, on the other hand, for a given bistatic distance, cells associated with one (SB_n) of the basic signals able to be discriminated by their orthogonality properties.
2. The method according to claim 1, wherein the basic signals are orthogonal two by two.
3. The method according to claim 1 or 2, wherein each basic signal is orthogonal to itself being offset in time.
4. The method according to any one of claims 1 to 3, comprising successive and cyclic emissions of basic signals.
5. The method according to any one of claims 1 to 4, wherein the reception charts cover the reception area (ZR).
6. The method according to claim 5, wherein at least one of the reception charts has several main lobes alternating with secondary radiation lobes.

7. Emission and reception systems for radar detection comprising several emission antennas (AE_1, AE_S) for emitting basic signals (SB_1, SB_N) having orthogonality properties and several reception antennas (AR_1, AR_U) for receiving the basic signals, characterized in that:

the emission system (SEM) comprises means (EM, CPE) for forming emission radiation charts for emitting respectively basic signals for all the emission antennas (AE_1, AE_S), each emission radiation chart being associated with a respective basic signal (SB_n) for emitting by all the emission antennas and comprising main radiation lobes (LP_1, LP_N) alternating with secondary radiation lobes (LS), the main radiation lobes of the emission radiation charts substantially alternating and being juxtaposed in the space,

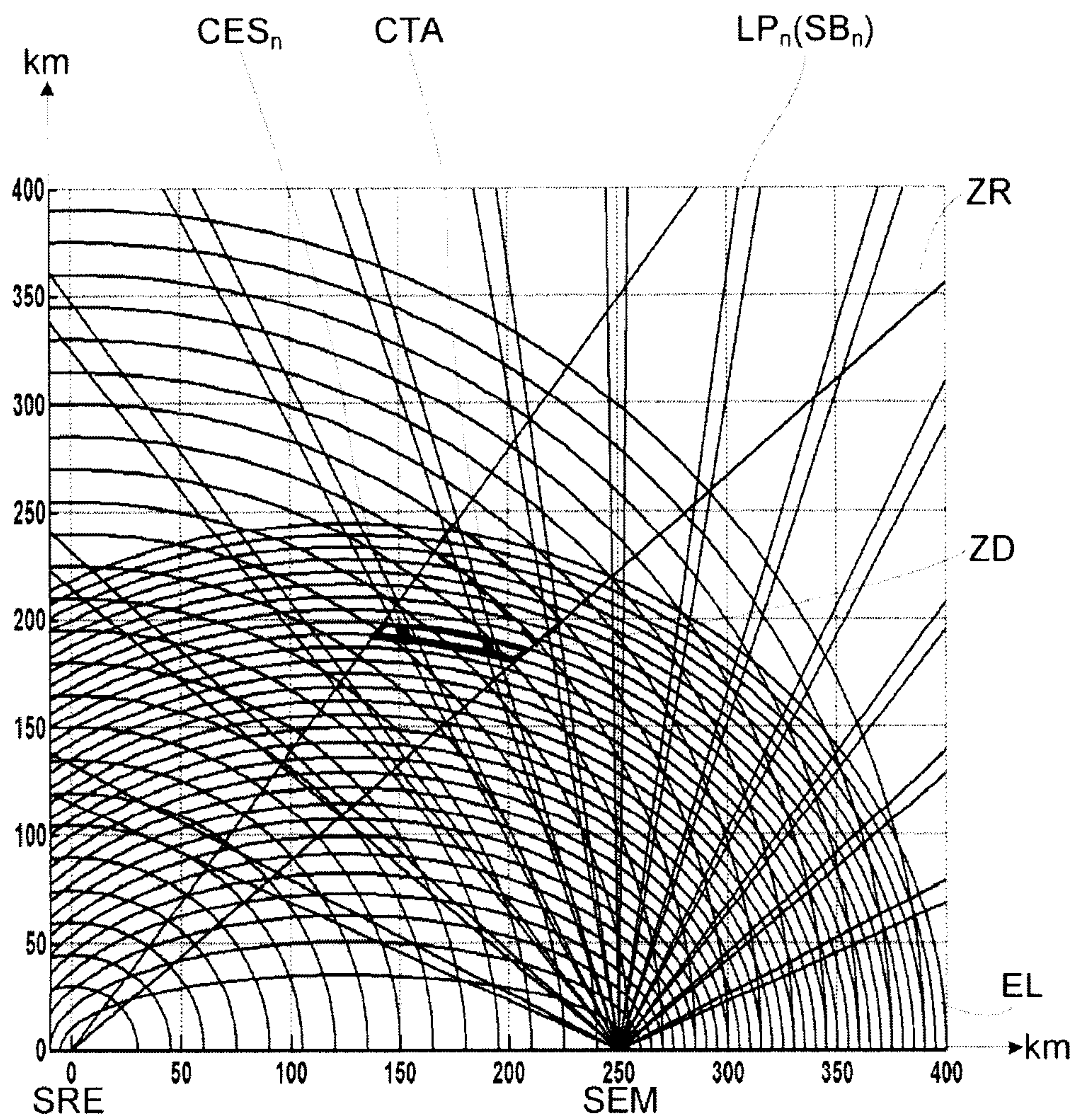
the reception system (SRE) comprises means (CPR) for forming reception radiation charts in a reception area (ZR) so as to receive the basic signals by each one of the reception antennas (AR_1, AR_U), the number of reception radiation charts being at least equal to the number of cells ($CES_{n,m}$) contained in the reception area, that are covered by the main radiation lobes (LP_n) of one of the emission radiation charts and that are located at a given bistatic distance from the emission and reception systems,

the SRE further comprises:

means ($CPR_{1,1}, CPR_{p,U}$) for weighting signals captured by the reception antennas (AR_1, AR_U), the signal captured by a reception antenna (AR_u) being weighted so as to produce as many weighted signals as reception radiation charts, and

means ($DIS_{p,n}$) for discriminating in basic signal and bistatic distance in the set of weighted signals, on the one hand, cells having a constant bistatic distance, on the other hand, for a given bistatic distance, cells associated with one (SB_n) of the basic signals able to be discriminated by their orthogonality properties.

1/5
FIG. 1



2/5

FIG. 2

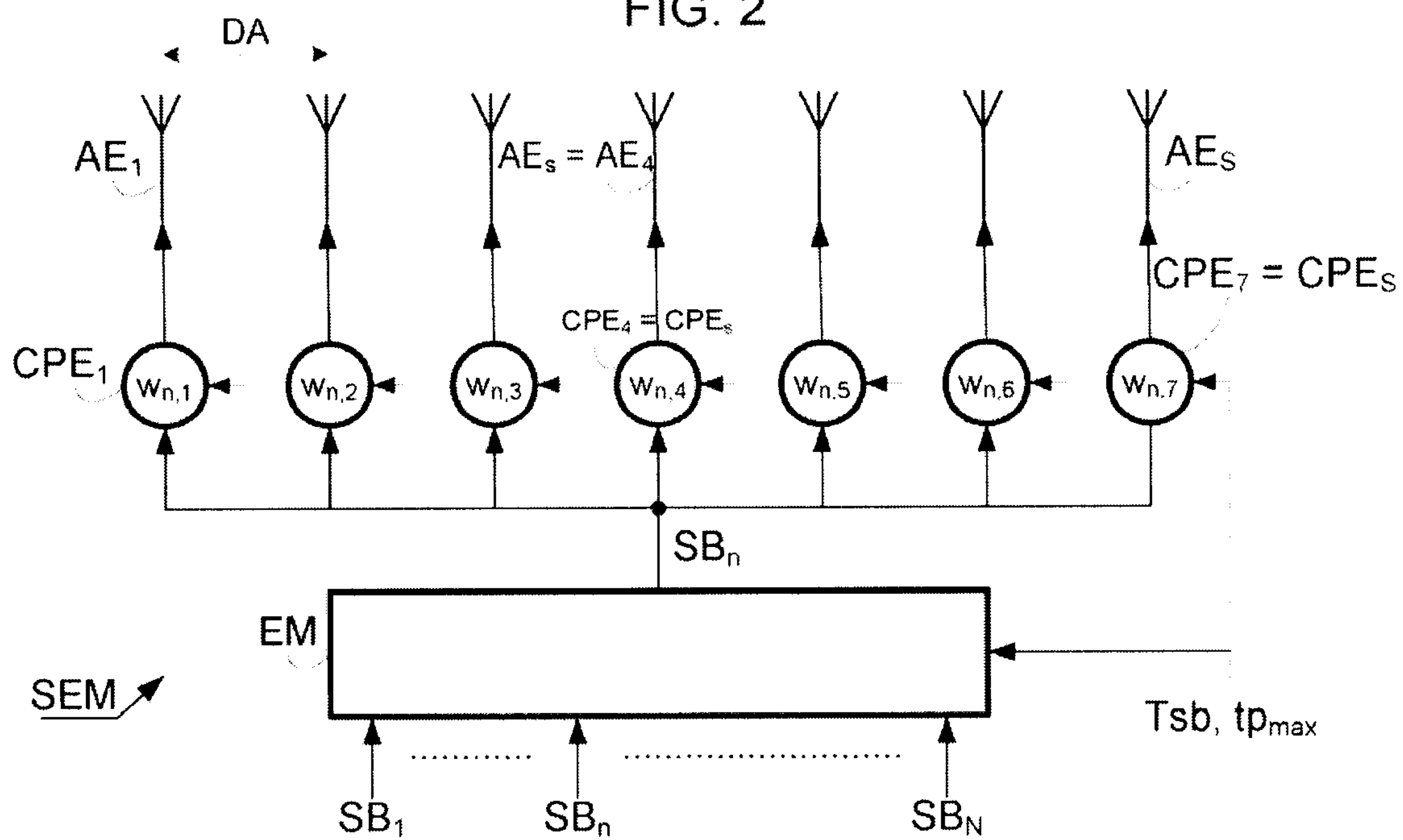
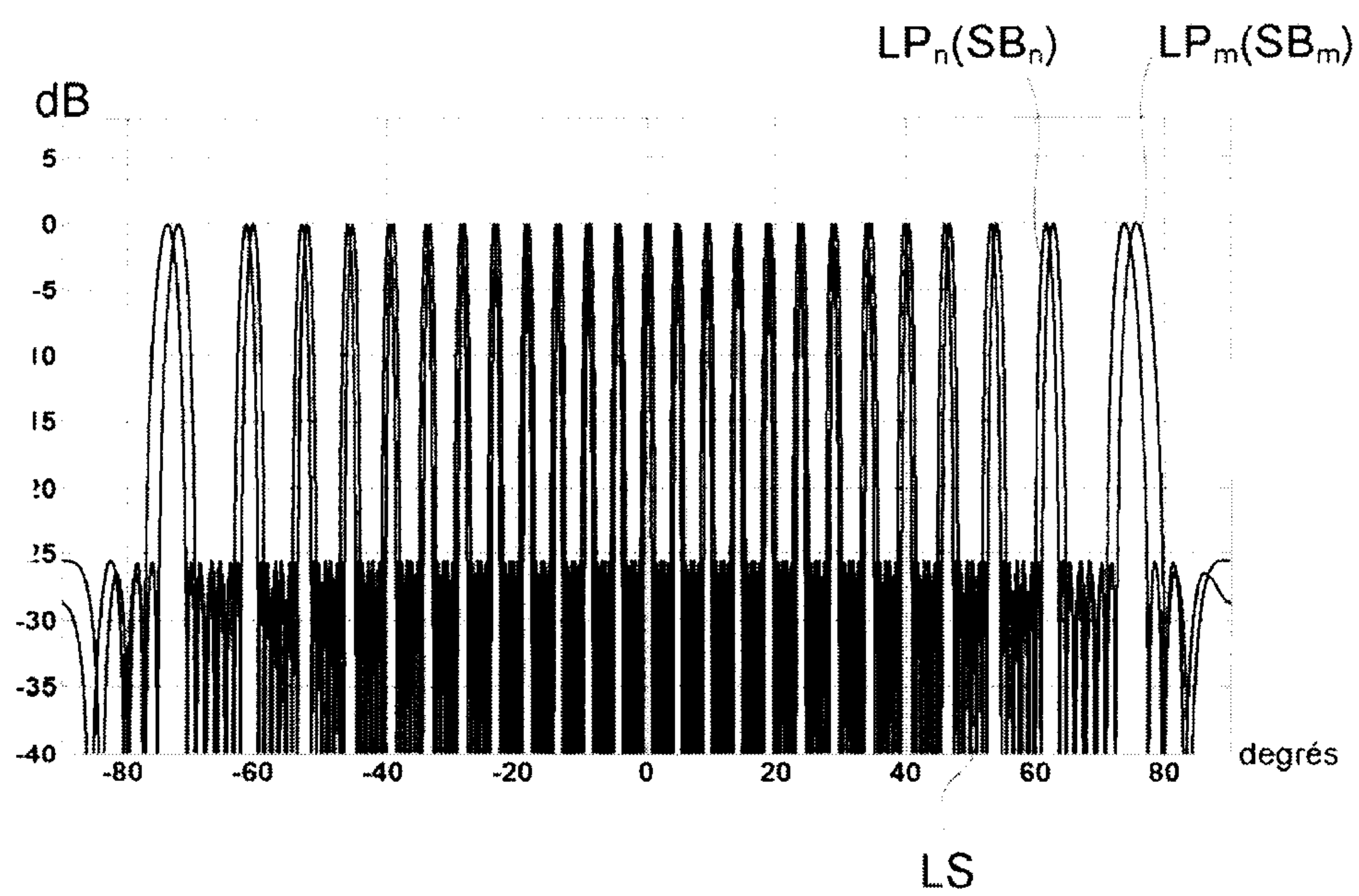
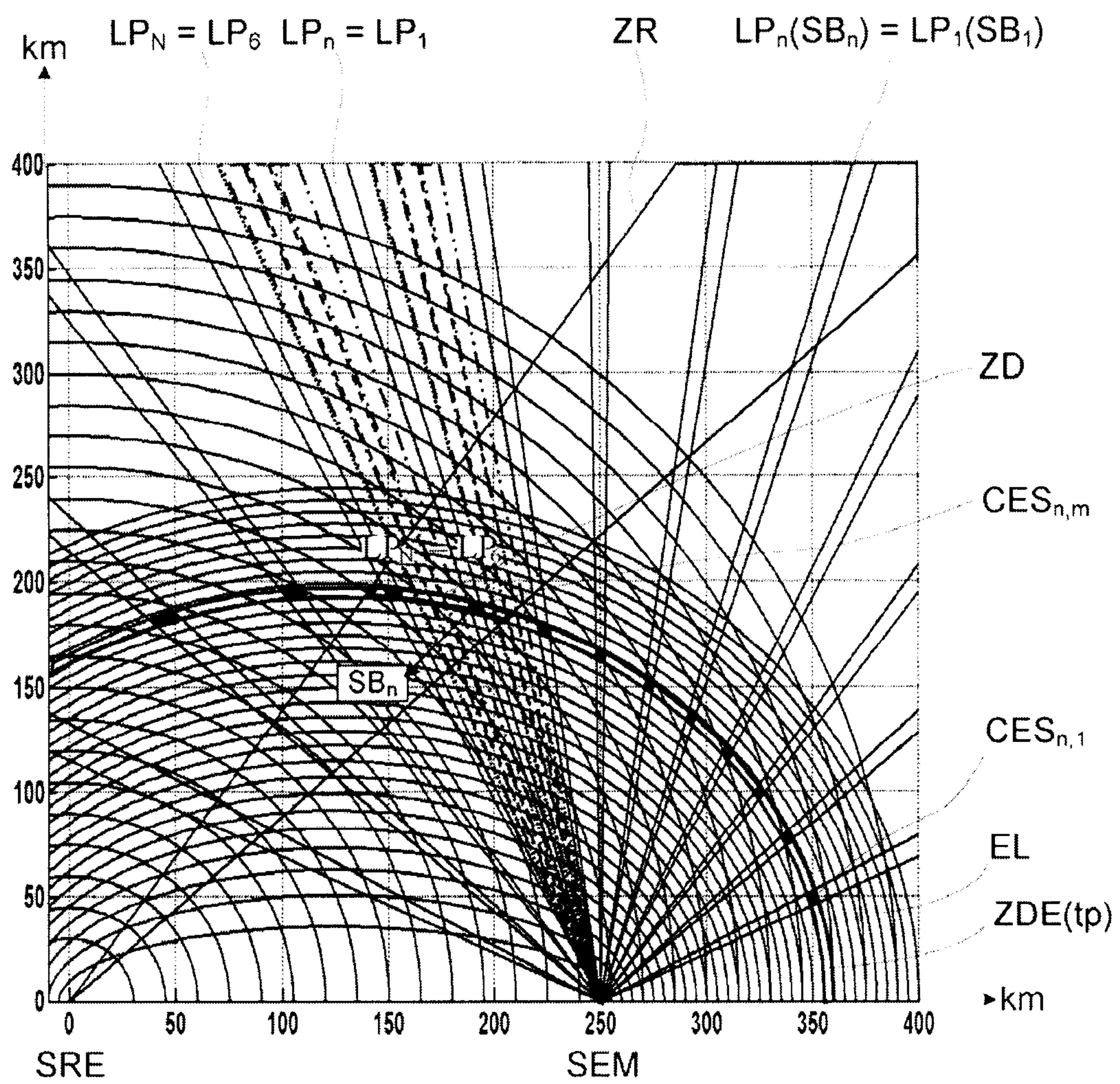


FIG. 3



3/5

FIG. 4



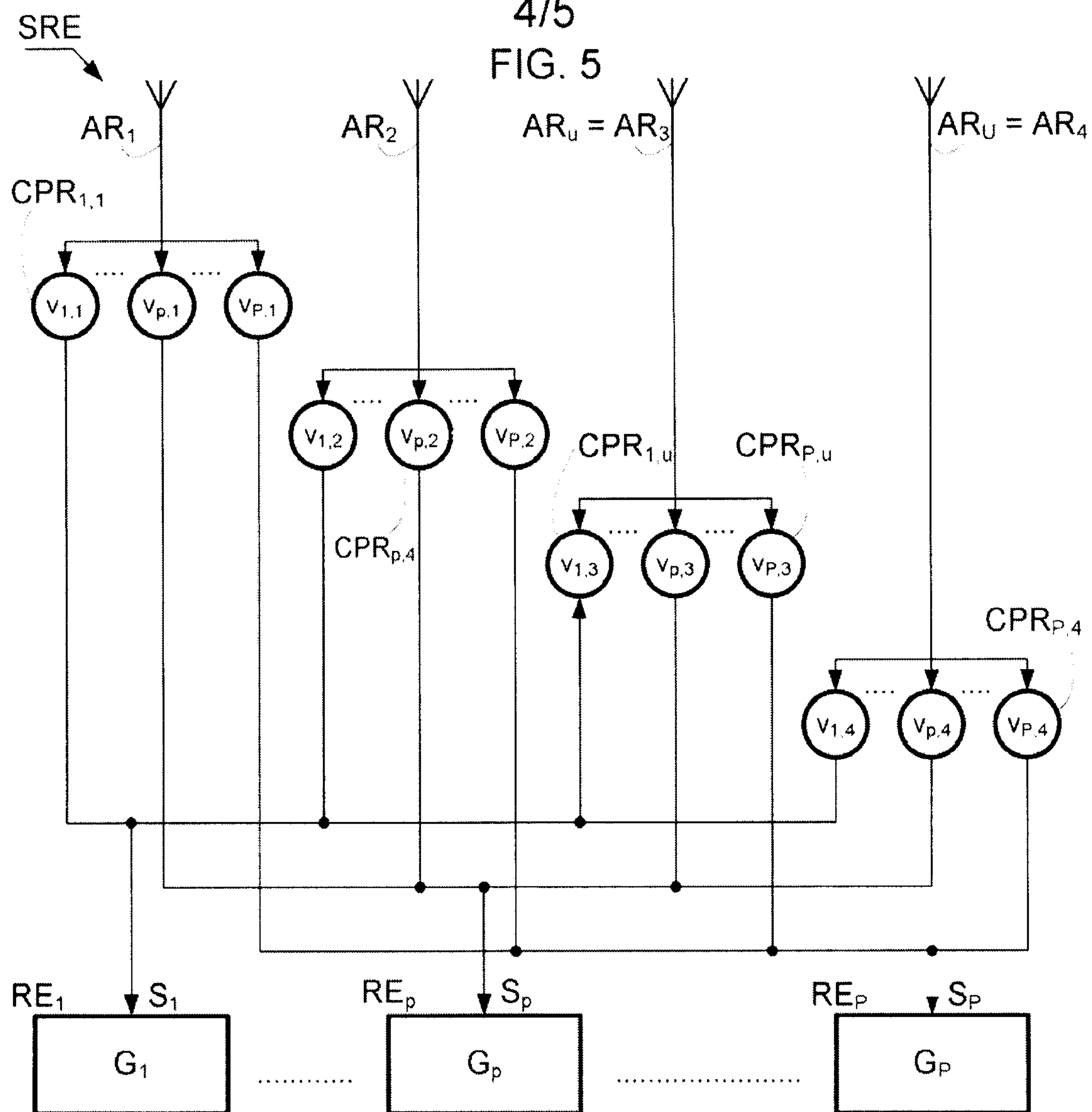
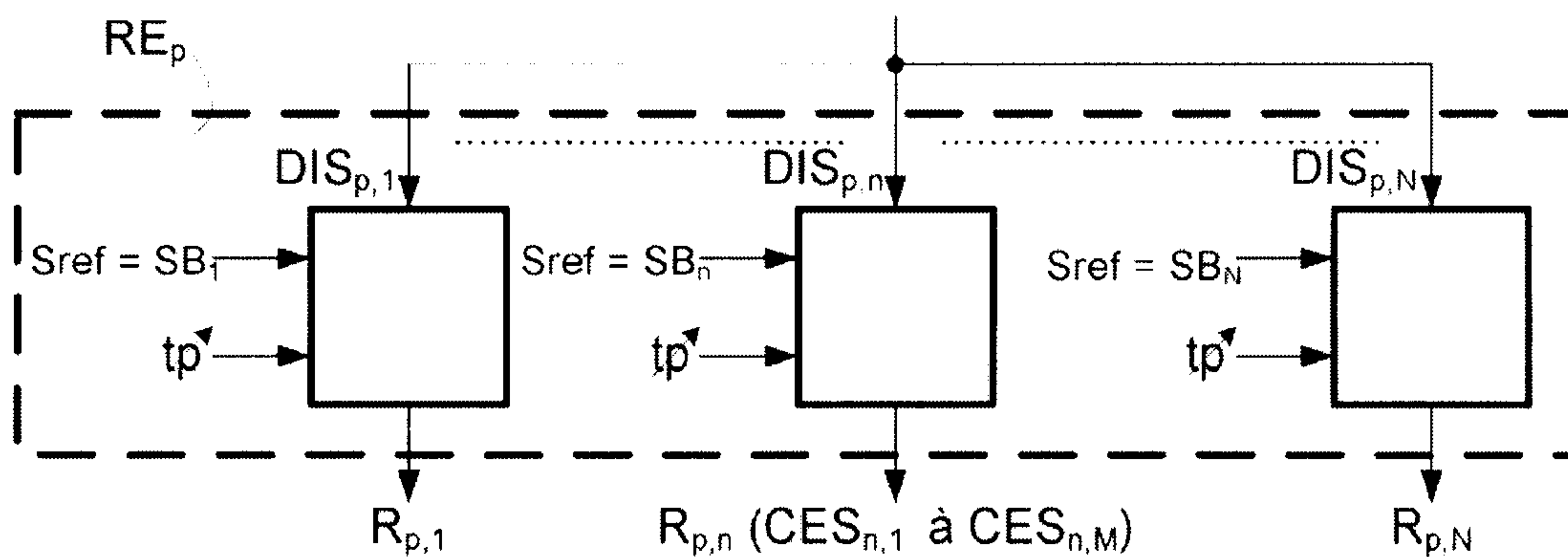
4/5
FIG. 5

FIG. 6



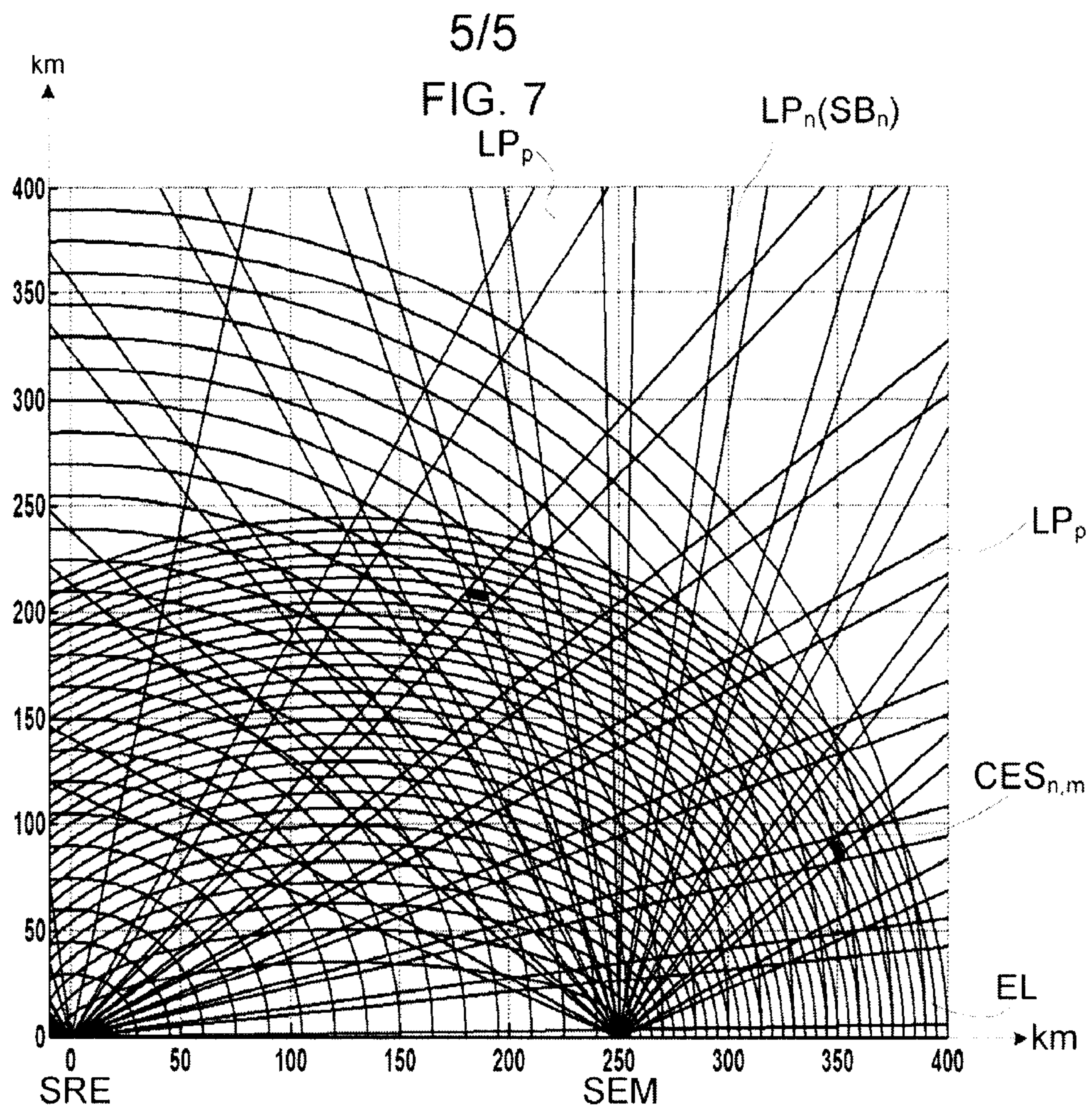


FIG. 8

