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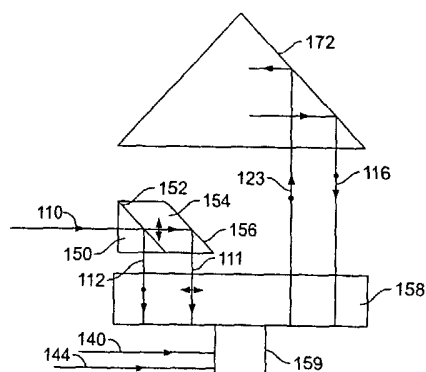
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(54) Title: INTERFEROMETRY SYSTEMS INVOLVING A DYNAMIC BEAM-STEERING ASSEMBLY



(57) Abstract: An apparatus including: a multi-axis interferometry system configured to receive an input beam and direct at least two beams derived from the input beam to contact different locations on a measurement object to monitor changes in an angular orientation of the measurement object; a beam steering assembly having a beam steering element positioned to direct the input beam into the interferometry system and a positioning system to selectively orient the beam steering element relative to the interferometry system; and a control circuit which during operation orients the beam steering element based on the changes in the angular orientation of the measurement object monitored by the interferometry system.

INTERFEROMETRY SYSTEMS INVOLVING A DYNAMIC BEAM-STEERING ASSEMBLY

Cross-Reference to Related Applications

5 This application claims priority to U.S. Provisional Patent Application Serial No. 60/389,527 entitled "MULTI-AXIS INTERFEROMETRY SYSTEMS INVOLVING A DYNAMIC BEAM-STEERING ASSEMBLY" and filed June 17, 2002, the contents of which are incorporated herein by reference.

 This application is also a continuation-in-part application of, and claims
10 priority to, U.S. Patent Application Serial No. 09/968,887 entitled "SINGLE-PASS AND MULTI-PASS INTERFEROMETRY SYSTEMS HAVING A DYNAMIC BEAM-STEERING ASSEMBLY FOR MEASURING DISTANCE, ANGLE, AND DISPERSION" and filed October 10, 2001, which is a continuation application of U.S. Patent Application Serial No. 09/305,876 filed May 5, 1999, now issued as U.S.
15 Patent No. 6,313,918, which is a continuation-in-part application of U.S. Patent Application Serial No. 09/157,131 filed September 18, 1998, now issued as U.S. Patent No. 6,252,667. The contents of said patent applications being incorporated herein by reference.

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Background of the Invention

 Displacement measuring interferometers monitor changes in the position of a measurement object relative to a reference object based on an optical interference signal. The interferometer generates the optical interference signal by overlapping and
25 interfering a measurement beam reflected from the measurement object with a reference beam reflected from the reference object.

 In many applications, the measurement and reference beams have orthogonal polarizations and different frequencies. The different frequencies can be produced, for example, by laser Zeeman splitting, by acousto-optical modulation, or internal to
30 the laser using birefringent elements or the like. The orthogonal polarizations allow a polarizing beam splitter to direct the measurement and reference beams to the measurement and reference objects, respectively, and combine the reflected

measurement and reference beams to form overlapping exit measurement and reference beams. The overlapping exit beams form an output beam that subsequently passes through a polarizer.

The polarizer mixes polarizations of the exit measurement and reference beams to form a mixed beam. Components of the exit measurement and reference beams in the mixed beam interfere with one another so that the intensity of the mixed beam varies with the relative phase of the exit measurement and reference beams. A detector measures the time-dependent intensity of the mixed beam and generates an electrical interference signal proportional to that intensity. Because the measurement and reference beams have different frequencies, the electrical interference signal includes a “heterodyne” signal having a beat frequency equal to the difference between the frequencies of the exit measurement and reference beams. If the lengths of the measurement and reference paths are changing relative to one another, *e.g.*, by translating a stage that includes the measurement object, the measured beat frequency includes a Doppler shift equal to $2\nu np/\lambda$, where ν is the relative speed of the measurement and reference objects, λ is the wavelength of the measurement and reference beams, n is the refractive index of the medium through which the light beams travel, *e.g.*, air or vacuum, and p is the number of passes to the reference and measurement objects. Changes in the relative position of the measurement object correspond to changes in the phase of the measured interference signal, with a 2π phase change substantially equal to a distance change L of $\lambda/(np)$, where L is a round-trip distance change, *e.g.*, the change in distance to and from a stage that includes the measurement object.

Unfortunately, this equality is not always exact. In addition, the amplitude of the measured interference signal may be variable. A variable amplitude may subsequently reduce the accuracy of measured phase changes. Many interferometers include non-linearities such as what are known as “cyclic errors.” The cyclic errors can be expressed as contributions to the phase and/or the intensity of the measured interference signal and have a sinusoidal dependence on the change in optical path length pnL . In particular, the first harmonic cyclic error in phase has a sinusoidal

dependence on $(2\pi pnL)/\lambda$ and the second harmonic cyclic error in phase has a sinusoidal dependence on $2(2\pi pnL)/\lambda$. Higher harmonic cyclic errors and sub-harmonic cyclic errors can also be present.

There are also "non-cyclic non-linearities" such as those caused by a change in lateral displacement (*i.e.*, "beam shear") between the reference and measurement beam components of an output beam of an interferometer when the wavefronts of the reference and measurement beam components have wavefront errors. This can be explained as follows.

Inhomogeneities in the interferometer optics may cause wavefront errors in the reference and measurement beams. When the reference and measurement beams propagate collinearly with one another through such inhomogeneities, the resulting wavefront errors are identical and their contributions to the interferometric signal cancel each other out. More typically, however, the reference and measurement beam components of the output beam are laterally displaced from one another, *i.e.*, they have a relative beam shear. Such beam shear causes the wavefront errors to contribute an error to the interferometric signal derived from the output beam.

Moreover, in many interferometry systems beam shear changes as the position or angular orientation of the measurement object changes. For example, a change in relative beam shear can be introduced by a change in the angular orientation of a plane mirror measurement object. Accordingly, a change in the angular orientation of the measurement object produces a corresponding error in the interferometric signal.

The effect of the beam shear and wavefront errors will depend upon procedures used to mix components of the output beam with respect to component polarization states and to detect the mixed output beam to generate an electrical interference signal. The mixed output beam may for example be detected by a detector without any focusing of the mixed beam onto the detector, by detecting the mixed output beam as a beam focused onto a detector, or by launching the mixed output beam into a single mode or multi-mode optical fiber and detecting a portion of the mixed output beam that is transmitted by the optical fiber. The effect of the beam shear and wavefront errors will also depend on properties of a beam stop should a beam stop be used in the procedure to detect the mixed output beam. Generally, the

errors in the interferometric signal are compounded when an optical fiber is used to transmit the mixed output beam to the detector.

Amplitude variability of the measured interference signal can be the net result of a number of mechanisms. One mechanism is a relative beam shear of the reference and measurement components of the output beam that is for example a consequence of a change in orientation of the measurement object.

In dispersion measuring applications, optical path length measurements are made at multiple wavelengths, *e.g.*, 532 nm and 1064 nm, and are used to measure dispersion of a gas in the measurement path of the distance measuring interferometer.

The dispersion measurement can be used in converting the optical path length measured by a distance measuring interferometer into a physical length. Such a conversion can be important since changes in the measured optical path length can be caused by gas turbulence and/or by a change in the average density of the gas in the measurement arm even though the physical distance to the measurement object is unchanged.

The interferometers described above are often crucial components of scanner systems and stepper systems used in lithography to produce integrated circuits on semiconductor wafers. Such lithography systems typically include a translatable stage to support and fix the wafer, focusing optics used to direct a radiation beam onto the wafer, a scanner or stepper system for translating the stage relative to the exposure beam, and one or more interferometers. Each interferometer directs a measurement beam to, and receives a reflected measurement beam from, a plane mirror attached to the stage. Each interferometer interferes its reflected measurement beams with a corresponding reference beam, and collectively the interferometers accurately measure changes in the position of the stage relative to the radiation beam. The interferometers enable the lithography system to precisely control which regions of the wafer are exposed to the radiation beam.

In many lithography systems and other applications, the measurement object includes one or more plane mirrors to reflect the measurement beam from each interferometer. Small changes in the angular orientation of the measurement object, *e.g.*, pitch and yaw of a stage, can alter the direction of each measurement beam

reflected from the plane mirrors. If left uncompensated, the altered measurement beams reduce the overlap of the exit measurement and reference beams in each corresponding interferometer. Furthermore, these exit measurement and reference beams will not be propagating parallel to one another nor will their wave fronts be aligned when forming the mixed beam. As a result, the interference between the exit measurement and reference beams will vary across the transverse profile of the mixed beam, thereby corrupting the interference information encoded in the optical intensity measured by the detector.

To address this problem, many conventional interferometers include a retroreflector that redirects the measurement beam back to the plane mirror so that the measurement beam “double passes” the path between the interferometer and the measurement object. The presence of the retroreflector insures that the direction of the exit measurement is insensitive to changes in the angular orientation of the measurement object. When implemented in a plane mirror interferometer, the configuration results in what is commonly referred to as a high-stability plane mirror interferometer (HSPMI). However, even with the retroreflector, the lateral position of the exit measurement beam remains sensitive to changes in the angular orientation of the measurement object. Furthermore, the path of the measurement beam through optics within the interferometer also remains sensitive to changes in the angular orientation of the measurement object.

In practice, the interferometry systems are used to measure the position of the wafer stage along multiple measurement axes. For example, defining a Cartesian coordinate system in which the wafer stage lies in the x-y plane, measurements are typically made of the x and y positions of the stage as well as the angular orientation of the stage with respect to the z axis, as the wafer stage is translated along the x-y plane. Furthermore, it may be desirable to also monitor tilts of the wafer stage out of the x-y plane. For example, accurate characterization of such tilts may be necessary to calculate Abbe offset errors in the x and y positions. Thus, depending on the desired application, there may be up to five degrees of freedom to be measured. Moreover, in some applications, it is desirable to also monitor the position of the stage with respect to the z-axis, resulting in a sixth degree of freedom.

To measure each degree of freedom, an interferometer is used to monitor distance changes along a corresponding metrology axis. For example, in systems that measure the *x* and *y* positions of the stage as well as the angular orientation of the stage with respect to the *x*, *y*, and *z* axes, at least three spatially separated measurement beams reflect from one side of the wafer stage and at least two spatially separated measurement beams reflect from another side of the wafer stage. See, e.g., U.S. Patent No. 5,801,832 entitled "Method of and Device for Repetitively Imaging a Mask Pattern on a Substrate Using Five Measuring Axes," the contents of which are incorporated herein by reference. Each measurement beam is recombined with a reference beam to monitor optical path length changes along the corresponding metrology axes. Because the different measurement beams contact the wafer stage at different locations, the angular orientation of the wafer stage can then be derived from appropriate combinations of the optical path length measurements. Accordingly, for each degree of freedom to be monitored, the system includes at least one measurement beam that contacts the wafer stage. Furthermore, as described above, each measurement beam may double-pass the wafer stage to prevent changes in the angular orientation of the wafer stage from corrupting the interferometric signal. The measurement beams may generated from physically separate interferometers or from multi-axes interferometers that generate multiple measurement beams.

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Summary of the Invention

The invention features an interferometry system which includes at least one dynamic beam steering assembly for redirecting one or more beams within the interferometry system in response to changes in the angular orientation or position of the measurement object. The dynamic beam steering assembly can be incorporated into interferometry systems that measure distances, angle, and/or dispersion. It may be positioned within an interferometer to direct one or both of a measurement beam and reference beam after they have been separated from an input beam, or it may be positioned to direct an input beam (or portions thereof) into one or more interferometers. The dynamic beam steering assembly improves the performance of

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the interferometry system by reducing negative consequences of changes in the angular orientation or position of the measurement object.

In some embodiments, the interferometry system includes multiple measurement axes that can be used to determine a change in the angular orientation of the measurement object. A servo signal derived from that determined change can be used to orient a beam steering element in the beam steering assembly and thereby cause the measurement beam(s) to contact the measurement object at a preset angle of incidence (e.g., normal incidence) for a range of orientations of the measurement object. This can reduce the transverse displacement of the beams within the interferometer and the transverse displacement between the measurement and reference beam components upon exiting the interferometer that are otherwise caused by changes in the orientation of the measurement object because, at least for normal incidence, the path of the measurement beam to the measurement object is collinear with its return path back to the interferometer. As described above, this can reduce non-cyclic errors that can otherwise degrade the interferometric measurement, especially where the output measurement and reference beam components are coupled to a detector via a fiber-optic pick-up.

In general, in one aspect, the invention features an apparatus including: a multi-axis interferometry system configured to receive an input beam and direct at least two beams derived from the input beam to contact different locations on a measurement object to monitor changes in an angular orientation of the measurement object; a beam steering assembly having a beam steering element positioned to direct the input beam into the interferometry system and a positioning system to selectively orient the beam steering element relative to the interferometry system; and a control circuit which during operation orients the beam steering element based on the changes in the angular orientation of the measurement object monitored by the interferometry system.

Embodiments of the apparatus may include any of the following features.

The control circuit may cause the beams to contact the measurement object at substantially normal incidence over a range of angular orientations of the measurement object.

In one example, the two beams that contact the measurement object may be measurement beams, and the multi-axis interferometry system may be configured to combine each of the two measurement beams with a corresponding reference beam after they contact the measurement object to produce a pair of output beams including
5 interferometric information about changes in distance to the different locations on the measurement object.

During operation the control circuit may calculate a control signal using the interferometric information in the output beams and cause the positioning system to orient the beam steering element based on the control signal. Furthermore, the control
10 circuit may include multiple detectors for measuring an intensity of each output beam, a signal processor for calculating the changes in distance to the different locations of the measurement object from the measured intensities and generating the control signal based on the calculated distance changes, and a control system for causing the
15 positioning system to orient the beam steering element in response to the control signal. Also, the apparatus may further include a polarizer prior to each detector to cause the measured intensity of each output beam to correspond to the intensity of a selected polarization component of that output beam.

The multi-axis interferometry system may direct each measurement beam to make an even number of passes to the measurement object before combining it with
20 its corresponding reference beam.

The multi-axis interferometry system may direct each measurement beam to make only one pass to the measurement object before combining it with its corresponding reference beam.

The multi-axis interferometry system may include separate single-axis
25 interferometers each producing a corresponding measurement beam and optics for directing a portion of the input beam to each of the interferometers.

The multi-axis interferometry system may include an integral multi-axis interferometer including multiple measurement axes each corresponding to one of the measurement beams.

30 In another example, the multi-axis interferometry system may be configured to combine the two beams with one another after they contact the measurement object to

produce an output beam including interferometric information about the changes in the angular orientation of the measurement object.

During operation the control circuit may calculate a control signal using the interferometric information in the output beam and causes the positioning system to orient the beam steering element based on the control signal. Furthermore, the control circuit may include a detector for measuring an intensity of the output beam, a signal processor for calculating the changes in the angular orientation of the measurement object from the measured intensity and generating the control signal from the calculated changes in angular orientation, and a control system for causing the positioning system to orient the beam steering element in response to the control signal. Also, the apparatus may further include a polarizer prior to the detector to cause the measured intensity of the output beam to correspond to the intensity of a selected polarization component of the output beam.

In either example, the multi-axis interferometry system may direct at least three measurement beams to contact the measurement object at different locations.

In either example, the changes in the angular orientation of the measurement object monitored by the interferometry system may be relative to a reference object. For example, the reference object may be fixed in the interferometry system.

In general, in another aspect, the invention features an apparatus including: a multi-axis interferometry system configured to direct at least two beams to contact different locations on a measurement object to monitor changes in an angular orientation of the measurement object, the interferometry system including a beam steering assembly having a beam steering element positioned to direct and contact at least one of the beams and a positioning system to selectively orient the beam steering element within the interferometry system; and a control circuit which during operation orients the beam steering element based on the changes in the angular orientation of the measurement object monitored by the interferometry system.

Embodiments of the apparatus may include any of the following features.

The beam steering element may be positioned to direct multiple ones of the beams that contact the measurement object.

The multi-axis interferometry system may include at least one additional beam steering assembly having a beam steering element positioned to direct and contact another one of the beams that contact the measurement object and a positioning system to selectively orient the beam steering element in the additional beam steering assembly. For example, during operation the control circuit may cause the positioning system in the additional beam steering assembly to orient the beam steering element in the additional beam steering assembly in response to the control signal.

The control circuit may cause the beams to contact the measurement object at substantially normal incidence over a range of angular orientations of the measurement object.

In one example, the two beams that contact the measurement object may be measurement beams, and the multi-axis interferometry system may be configured to combine each of the two measurement beams with a corresponding reference beam after they contact the measurement object to produce a pair of output beams including interferometric information about changes in distance to the different locations on the measurement object.

During operation the control circuit may calculate a control signal using the interferometric information in the output beams and cause the positioning system to orient the beam steering element based on the control signal. Furthermore, the control circuit may include multiple detectors for measuring an intensity of each output beam, a signal processor for calculating the changes in distance to the different locations of the measurement object from the measured intensities and generating the control signal based on the calculated distance changes, and a control system for causing the positioning system to orient the beam steering element in response to the control signal. Also, the apparatus may further include a polarizer prior to each detector to cause the measured intensity of each output beam to correspond to the intensity of a selected polarization component of each output beam.

The multi-axis interferometry system may direct each measurement beam to make an even number of passes to the measurement object before combining it with its corresponding reference beam.

The multi-axis interferometry system may direct each measurement beam to make only one pass to the measurement object before combining it with its corresponding reference beam.

5 The multi-axis interferometry system may include separate single-axis interferometers each producing a corresponding measurement beam and optics for directing a portion of the input beam to each of the interferometers.

The multi-axis interferometry system may include an integral multi-axis interferometer including multiple measurement axes each corresponding to one of the measurement beams.

10 In another example, the multi-axis interferometry system may be configured to combine the two beams with one another after they contact the measurement object to produce an output beam including interferometric information about the changes in the angular orientation of the measurement object.

15 During operation the control circuit may calculate a control signal using the interferometric information in the output beam and cause the positioning system to orient the beam steering element based on the control signal. Furthermore, the control circuit may include a detector for measuring an intensity of the output beam, a signal processor for calculating the changes in the angular orientation of the measurement object from the measured intensity and generating the control signal from the
20 calculated changes in angular orientation, and a control system for causing the positioning system to orient the beam steering element in response to the control signal.

In either example, the multi-axis interferometry system may direct at least three measurement beams to contact the measurement object at different locations.

25 In either example, the changes in the angular orientation of the measurement object monitored by the interferometry system may be relative to a reference object. For example, the reference object may be fixed in the interferometry system.

In another aspect, the invention features a lithography system for use in fabricating integrated circuits on a wafer, the system including: a stage for supporting
30 the wafer; an illumination system for imaging spatially patterned radiation onto the wafer; a positioning system for adjusting the position of the stage relative to the

imaged radiation; and either interferometry apparatus described above for monitoring the position of the wafer relative to the imaged radiation. For example, the measurement object may include the stage, or the multi-axis interferometry system may be supported by the stage.

5 In another aspect, the invention features a lithography system for use in fabricating integrated circuits on a wafer, the system including: a stage for supporting the wafer; and an illumination system including a radiation source, a mask, a positioning system, a lens assembly, and either interferometry apparatus described above, wherein during operation the source directs radiation through the mask to
10 produce spatially patterned radiation, the positioning system adjusts the position of the mask relative to the radiation from the source, the lens assembly images the spatially patterned radiation onto the wafer, and the apparatus monitors the position of the mask relative to the radiation from the source. For example, the measurement object may include the mask, or the multi-axis interferometry system may be attached to the
15 mask.

 In another aspect, the invention features a beam writing system for use in fabricating a lithography mask, the system including: a source providing a write beam to pattern a substrate; a stage supporting the substrate; a beam directing assembly for delivering the write beam to the substrate; a positioning system for positioning the
20 stage and beam directing assembly relative one another; and either interferometry apparatus described above for monitoring the position of the stage relative to the beam directing assembly.

 In another aspect, the invention features a method for fabricating integrated circuits including using any of the lithography systems described above.

25 In general, in another aspect, the invention features an interferometry system including: an interferometer which during operation directs a measurement beam along a measurement path contacting a measurement object and combines at least a portion of the measurement beam with another beam to form an overlapping pair of exit beams, the interferometer including a beam steering assembly having a beam
30 steering element and a positioning system to orient the beam steering element, the beam steering element positioned to direct the measurement beam, the measurement

beam contacting the beam steering element; and a control circuit which during operation causes the positioning system to reorient the beam steering element in response to a change in at least one of angular orientation and position of the measurement object. The interferometer can direct the measurement beam to contact
5 the measurement object a single time (single-pass), two times (double pass), or an even or odd numbers of times.

During operation the control circuit can cause the positioning system to reorient the beam steering element in response to a change in angular orientation of the measurement object. In one such embodiment, the interferometry system can
10 further include a signal processor. During operation the interferometer directs a second measurement beam along a second measurement path contacting the measurement object and combines at least a portion of the second measurement beam with an additional beam to form a second overlapping pair of exit beams. The measurement beams contact the measurement object at separate locations, and during
15 operation the signal processor determines the change in angular orientation of the measurement object based on signals derived from the overlapping pairs of exit beams. In the latter embodiment, the beam steering element can be positioned to direct both of the measurement beams, both of the measurement beams contacting the beam steering element.

20 In general, in another aspect, the invention features an interferometry system including: an interferometer which during operation receives an input beam, splits the input beam into a measurement beam and at least one other beam, directs the measurement beam along a measurement path contacting a measurement object, and combines at least a portion of the measurement beam with the other beam to form an
25 overlapping pair of exit beams; a beam steering assembly having a beam steering element and a positioning system to orient the beam steering element, the beam steering element positioned to direct the input beam and the overlapping pair of exit beams, the input beam and the overlapping pair of exit beams contacting the beam steering element; a control circuit which during operation causes the positioning
30 system to reorient the beam steering element in response to a change in at least one of angular orientation and position of the measurement object. The interferometer can

direct the measurement beam to contact the measurement object a single time (single-pass), two times (double pass), or an even or odd numbers of times.

During operation the control circuit can cause the positioning system to reorient the beam steering element in response to a change in angular orientation of the measurement object. In one such embodiment, the interferometry system can further include a signal processor. During operation the interferometer directs a second measurement beam along a second measurement path contacting the measurement object and combines at least a portion of the second measurement beam with an additional beam to form a second overlapping pair of exit beams. The measurement beams contact the measurement object at separate locations, and during operation the signal processor determines the change in angular orientation of the measurement object based on signals derived from the overlapping pairs of exit beams. In the latter embodiment, the beam steering element can be positioned to direct the input beam and both of the overlapping pairs of exit beams, all of which contact the beam steering element.

In either of the interferometry systems described above, the system can further include a signal processor and the measurement beam can include components at two wavelengths. In one such embodiment, the interferometer produces the first mentioned overlapping pair of exit beams and a second overlapping pair of exit beams. The first pair of exit beams is indicative of changes in optical path length to the measurement object at a first of the two wavelengths, and the second pair of exit beams is indicative of changes in optical path length to the measurement object at a second of the two wavelengths. During operation the signal processor processes signals derived from the overlapping pairs of exit beams. For example, the signal processor can calculate dispersion along the measurement path based on the signals, and/or the signal processor can calculate changes in geometric distance to the measurement object based on the signals. The two wavelengths are sufficiently separated to permit such calculations, e.g., they are harmonically related or are separated by at least one 1 nm.

In another such embodiment, the interferometry system further includes the signal processor, and the measurement beam, the other beam, and the overlapping pair

of exit beams each include components at the two wavelengths. The overlapping pair of exit beams is indicative of changes in optical path length to the measurement object at each of the two wavelengths, and during operation the signal processor processes signals derived from the overlapping pair of exit beams. For example, the signal processor can calculate dispersion along the measurement path based on the signals, and/or the signal processor can calculate changes in geometric distance to the measurement object based on the signals. Again, the two wavelengths are sufficiently separated to permit such calculations, e.g., they are harmonically related or are separated by at least one 1 nm.

In general, in another aspect, the invention features an interferometry method including: directing a measurement beam along a measurement path contacting a measurement object; combining at least a portion of the measurement beam with another beam to form an overlapping pair of exit beams; and using an electronic control system to redirect the measurement beam in response to a change in at least one of the angular orientation and position of the measurement object. The measurement path can contact the measurement object one time, two times, or more generally, an even or odd number of times. The method can further include: directing a second measurement beam along a second measurement path contacting the measurement object; combining at least a portion of the second measurement beam with an additional beam to form a second overlapping pair of exit beams, the first and second pairs of exit beams indicative of changes in optical path length to two separate locations on the measurement object; and calculating the change in angular orientation of the measurement object based on signals derived from the overlapping pairs of exit beams.

In general, in another aspect, the invention features an interferometry method including: directing a measurement beam having components at two wavelengths along a measurement path contacting a measurement object; calculating changes in geometric distance to the measurement object based on interferometric signals derived from the measurement beam; and using an electronic control system to redirect the measurement beam in response to a change in at least one of the angular orientation and position of the measurement object. Alternatively, in another aspect, the

invention features an interferometry method including: directing a measurement beam having components at two wavelengths along a measurement path contacting a measurement object; calculating dispersion along the measurement path based on interferometric signals derived from the measurement beam; and using an electronic control system to redirect the measurement beam in response to a change in at least one of the angular orientation and position of the measurement object. The electronic control system in either of these aspects can redirect the measurement beam in response to a change in the angular orientation of the measurement object, and in particular, can redirect the measurement beam to contact the measurement object at substantially normal incidence over a range of angular orientations of the measurement object. Also, in either of these aspects, the two wavelengths are sufficiently separated to permit the geometric length or dispersion calculation, e.g., they are harmonically related or are separated by at least one 1 nm.

The invention also features a lithography system for fabricating integrated circuits including first and second components, which are movable relative to one another. One of interferometry systems described above is secured to the second component and the measurement object is a mirror rigidly secured to the first component. During operation the interferometry system measures the position of the first component relative to the second component. In some embodiments, the second component is a movable stage used to support a wafer and during operation the beam steering element causes the measurement beam to contact the mirror at substantially normal incidence over a range of angular orientations of the measurement object.

The interferometry systems and methods described above can further include one or more features of any of the following additional aspects of the invention.

In general, in another aspect, the invention features an interferometry system for measuring changes in distance to a measurement object. The system includes an interferometer which during operation directs a reference beam along a reference path and a measurement beam along a measurement path contacting the measurement object and combines the reference and measurement beams to produce overlapping exit reference and measurement beams. The overlapping exit reference and measurement beams are indicative of changes in a relative optical path length between

the reference and measurement paths. The interferometer includes a beam steering assembly having a beam steering element and a positioning system to orient the beam steering element. The beam steering element is positioned to direct at least one of the reference and measurement beams and the at least one of the reference and measurement beams contact the beam steering element. The system also includes a control circuit which during operation causes the positioning system to reorient the beam steering element in response to changes in at least one of angular orientation and position of the measurement object.

The system can include any of the following features.

The interferometer can separate an input beam into a pair of spatially separated beams to define the reference and measurement beams. Alternatively, during operation the interferometer receives a pair of spatially separated input beams to define the reference and measurement beams.

The interferometer can be a single-pass interferometer in which the measurement beam contacts the measurement object only a single time. Also, in some embodiments, the interferometer can include the measurement object, and in other embodiments, the measurement object can be separate from the interferometer. During operation the control circuit can cause the positioning system to reorient the beam steering element based on a signal generated from the exit measurement beam.

Also, during operation, the control circuit can cause the positioning system to reorient the beam steering element to do any of the following: 1) maintain the exit reference and measurement beams substantially parallel to one another over a range of angular orientations of the measurement object; 2) reduce changes in direction of the exit measurement beam caused by changes in the angular orientation of the measurement object; 3) reduce a transverse displacement between the exit reference and measurement beams caused by changes in the angular orientation of the measurement object or a translation of the measurement object; 4) reduce a transverse displacement of the measurement beam caused by changes in the angular orientation of the measurement object or a translation of the measurement object; and 5) insure that the measurement beam contacts the measurement object at substantially normal incidence over a range of angular orientations of the measurement object.

In embodiments in which the measurement object is a plane mirror and during operation the measurement beam contacts the measurement object at non-normal incidence, the control circuit can cause the positioning system to reorient the beam steering element to reduce transverse displacements between the exit reference and measurement beams caused by translations of the measurement object.

In some embodiments, the beam steering element can include a polarizing beam splitter that separates the input beam into the reference and measurement beams, and the positioning system can include at least one transducer mounted to the polarizing beam splitter and operative to adjust an orientation of the polarizing beam splitter in response to a control signal from the control circuit. Alternatively, the beam steering element can include a polarizing beam splitter that directs the reference beam along the reference path and the measurement beam along the measurement path, and the positioning system can include at least one transducer mounted to the polarizing beam splitter and operative to adjust an orientation of the polarizing beam splitter in response to a control signal from the control circuit.

In other embodiments, the interferometer can further include a polarizing beam splitter that separates the input beam into the reference and measurement beams, and wherein the beam steering element includes a beam steering mirror and the positioning system includes at least one transducer mounted to the beam steering mirror and operative to adjust an orientation of the beam steering mirror in response to a control signal from the control circuit. Alternatively, the interferometer can further include a polarizing beam splitter that directs the reference beam along the reference path and the measurement beam along the measurement path, and wherein the beam steering element includes a beam steering mirror and the positioning system includes at least one transducer mounted to the beam steering mirror and operative to adjust an orientation of the beam steering mirror in response to a control signal from the control circuit.

The system can further include a polarizer which during operation receives the exit reference and measurement beams and mixes polarizations of the exit reference and measurement beams to produce a mixed beam having a phase indicative of the changes in the optical path length difference between the reference and measurement

paths. The control circuit can include a detector having spatially resolved detector elements operative to measure directions and/or positions of the exit reference and measurement beams and generate a measurement signal indicative of the directions and/or positions. The control circuit can further include a controller operative to
5 receive the measurement signal from the detector and send a control signal based on the measurement signal to the positioning system, the control signal causing the positioning system to reorient the beam steering element.

In addition to a polarizing beam splitter, beam steering mirror, and transducers mounted to the beam steering mirror, the interferometer can further include a
10 measurement retroreflector, a reference retroreflector, and a reflective reference object. During operation, the polarizing beam splitter directs the reference beam to the reference object and the measurement beam to the measurement retroreflector, receives the reference beam from the reference object and the measurement beam from the measurement retroreflector, and then directs the reference and measurement
15 beams to the beam steering mirror. The beam steering mirror directs the reference beam to the reference retroreflector and the measurement beam to the measurement object, receives the reference beam from the reference retroreflector and the measurement beam from the measurement object, and then directs the reference and measurement beams back to the polarizing beam splitter. The polarizing beam splitter
20 combines the reference and measurement beams to produce the overlapping exit reference and measurement beams. The measurement retroreflector can have an aperture through which the reference beam travels to and from the reference object and the reference retroreflector can have an aperture through which the measurement beam travels to and from the measurement object. The interferometer can further
25 include a reference quarter wave plate through which the reference beam travels to and from the reference object and a measurement quarter wave plate through which the measurement beam travels to and from the measurement object.

The beam steering mirror can have front and back faces. During operation the front face of the beam steering mirror can direct the measurement beam to the
30 measurement object and the back face of the beam steering mirror can receive the measurement beam from the measurement object. The interferometer can further

include a second polarizing beam splitter which during operation receives the reference beam from the reference path and the measurement beam from the back face of the beam steering mirror and produces the exit reference and measurement beams.

The interferometer can further include at least one additional beam steering assembly including an additional beam steering element and an additional positioning system to orient the additional beam steering element. During operation the additional beam steering element directs the measurement beam. The measurement beam contacts the additional beam steering element and during operation the control circuit causes the positioning systems to reorient the beam steering elements to optimize the overlap of the exit reference and measurement beams and maintain the exit reference and measurement beams substantially parallel over a range of angular orientations and positions of the measurement object. The control circuit can include two detectors having spatially resolved detector elements operative to measure a position and direction of the exit measurement beam and generate measurement signals indicative of the position and direction. The control circuit can further include a controller operative to receive the measurement signals from the detectors and send control signals to the positioning systems based on the signals from the detectors, the control signals causing the positioning systems to reorient the beam steering elements.

In general, in another aspect, the invention features an interferometry system for measuring changes in distance to a measurement object. The system includes an interferometer which during operation receives one or more input beams to define a reference beam and a measurement beam, directs the reference beam along a reference path and the measurement beam along a measurement path contacting the measurement object, and combines the reference and measurement beams to produce an output beam including overlapping exit reference and measurement beams. The output beam is indicative of changes in a relative optical path length between the reference and measurement paths. The system further includes a beam steering assembly including a beam steering element and a positioning system to orient the beam steering element. During operation the beam steering element directs the input and output beams, the input and output beams contacting the beam steering element. The system further includes a control circuit which during operation causes the

positioning system to reorient the beam steering element in response to changes in at least one of angular orientation and position of the measurement object.

The system can include any of the following features.

5 The interferometer can receive a single input beam and separate the single input beam into a pair of spatially separated beams to define the reference and measurement beams. Alternatively, the interferometer can receive a pair of spatially separated input beams to define the reference and measurement beams.

10 The beam steering element can include a beam steering mirror, and the positioning system can include at least one transducer mounted to the beam steering mirror and operative to adjust an orientation of the beam steering mirror in response to a control signal from the control circuit. The beam steering mirror can include front and back faces, and wherein during operation the input beam contacts the front face of the beam steering mirror and the output beam contacts the back face of the beam steering mirror. The interferometer can be a single-pass interferometer in which the measurement beam contacts the measurement object only a single time.

15 The control circuit can cause the positioning system to reorient the beam steering element to do any of the following: 1) maintain the exit reference and measurement beams substantially parallel to one another over a range of angular orientations of the measurement object; 2) reduce changes in direction of the exit measurement beam caused by changes in the angular orientation of the measurement object; 3) to reduce a transverse displacement between the exit reference and measurement beams caused by changes in angular orientation of the measurement object or a translation of the measurement object; 4) reduce a transverse displacement of the measurement beam caused by changes in angular orientation of the measurement object or a translation of the measurement object; 5) to insure that the measurement beam contacts the measurement object at substantially normal incidence over a range of angular orientations of the measurement object.

25 In general, in a further aspect, the invention features an interferometry system including an interferometer which during operation directs a reference beam along a reference path and a measurement beam along a measurement path contacting a measurement object at non-normal incidence, and combines the reference and

measurement beams to form overlapping exit reference and measurement beams. The overlapping exit measurement and reference beams are indicative of changes in a relative optical path length between the reference and measurement paths. The interferometer includes a beam steering assembly positioned to direct the measurement beam. The system includes a control circuit which during operation causes the beam steering assembly to redirect the measurement beam to reduce transverse displacements between the exit reference and measurement beams caused by translations of the measurement object.

In general, in another aspect, the invention features an interferometry system including an interferometer which during operation directs a reference beam along a reference path and a measurement beam along a measurement path contacting a measurement object, and combines the reference and measurement beams to form overlapping exit reference and measurement beams. The overlapping exit measurement and reference beams are indicative of changes in a relative optical path length between the reference and measurement paths. The interferometer includes a beam steering assembly positioned to direct at least one of the reference and measurement beams.

The system further includes a control circuit which during operation causes the beam steering assembly to redirect one of the reference and measurement beams to do at least one of the following: 1) maintain the exit reference and measurement beams substantially parallel to one another over a range of angular orientations of the measurement object; 2) reduce changes in direction of the exit measurement beam caused by changes in the angular orientation of the measurement object; 3) reduce a transverse displacement between the exit reference and measurement beams caused by changes in angular orientation of the measurement object; 4) reduce a transverse displacement between the exit reference and measurement beams caused by translations of the measurement object; 5) to insure that the measurement beam contacts the measurement object at substantially normal incidence over a range of angular orientations of the measurement object; 6) to reduce a transverse displacement of the measurement beam caused by translations of the measurement object; and 7) to

reduce a transverse displacement of the measurement beam caused by changes in angular orientation of the measurement object.

In general, in another aspect, the invention features an interferometry system including an interferometer which during operation directs a reference beam along a reference path and a measurement beam along a measurement path contacting a measurement object, and combines the reference and measurement beams to form overlapping exit reference and measurement beams. The overlapping exit measurement and reference beams are indicative of changes in a relative optical path length between the reference and measurement paths. The interferometer includes a beam steering assembly positioned to direct at least one of the reference and measurement beams. The system further includes a control circuit which during operation causes the beam steering assembly to redirect the at least one of the reference and measurement beams in response to changes in angular orientation of the measurement object based on a signal generated from the exit measurement beam.

In general, in another aspect, the invention features a single-pass interferometry system including an interferometer which during operation directs a reference beam along a reference path and a measurement beam along a measurement path contacting a measurement object, and combines the reference and measurement beams to form overlapping exit reference and measurement beams. The overlapping exit measurement and reference beams are indicative of changes in a relative optical path length between the reference and measurement paths. The measurement path contacts the measurement object only a single time. The interferometer includes a beam steering assembly positioned direct at least one of the reference and measurement beams. The system further includes a control circuit which during operation causes the beam steering assembly to redirect the at least one of the reference and measurement beams in response to changes in angular orientation of the measurement object.

In another aspect, the invention also features a lithography system for use in fabricating integrated circuits on a wafer. The lithography system includes: a stage for supporting the wafer; an illumination system for imaging spatially patterned radiation onto the wafer; a positioning system for adjusting the position of the stage relative to

the imaged radiation; and at least one of any of the interferometry systems described above. The interferometry system(s) measures the position of the wafer relative to the imaged radiation.

In another aspect, the invention features a lithography system for use in
5 fabricating integrated circuits on a wafer. The lithography system includes a stage for supporting the wafer and an illumination system. The illumination system includes a radiation source, a mask, a positioning system, a lens assembly, and at least one of any of the interferometry systems described above. During operation the source directs radiation through the mask to produce spatially patterned radiation. The positioning
10 system adjusts the position of the mask relative to the radiation from the source. The lens assembly images the spatially patterned radiation onto the wafer. The interferometry system(s) measures the position of the mask relative to the radiation from the source.

In another aspect, the invention features a lithography system for fabricating
15 integrated circuits. The lithography system includes first and second components, the first and second components being movable relative to each other. The lithography system also includes at least one of any of the interferometry systems described above, wherein the first component includes the measurement object and the interferometry system(s) monitors the position of the first component relative to the second
20 component.

In another aspect, the invention features a beam writing system for use in fabricating a lithography mask. The beam writing system includes: a source providing a write beam to pattern a substrate; a stage supporting the substrate; a beam directing assembly for delivering the write beam to the substrate; a positioning system for
25 positioning the stage and beam directing assembly relative one another; and at least one of any of the inteferometry systems described above for measuring the position of the stage relative to the beam directing assembly.

In general, in another aspect, the invention features a method for interferometry. The interferometry method includes: directing a reference beam along
30 a reference path and a measurement beam along a measurement path contacting a measurement object; combining the reference and measurement beams to form

overlapping exit reference and measurement beams, the overlapping exit measurement and reference beams indicative of changes in a relative optical path length between the reference and measurement paths; and using an electronic control system to redirect the measurement beam in response to changes in at least one of angular orientation and position of the measurement object.

In general, in another aspect, the invention features a method for interferometry. The interferometry method includes: receiving one or more input beams to define a reference beam and a measurement beam; directing the reference beam along a reference path and the measurement beam along a measurement path contacting a measurement object; combining the reference and measurement beams to form an output beam including overlapping exit reference and measurement beams, the overlapping exit measurement and reference beams indicative of changes in a relative optical path length between the reference and measurement paths; and using an electronic control system to redirect the input and output beams in response to changes in at least one of angular orientation and position of the measurement object.

In another aspect, the invention features a lithography method for use in fabricating integrated circuits. The lithography method includes: imaging spatially patterned radiation onto a wafer; positioning the wafer relative to the imaged radiation; and measuring the position of the wafer relative to the imaged radiation using at least one of the interferometry methods described above.

In another aspect, the invention features a lithography method for use in the fabrication of integrated circuits. The lithography method includes: directing input radiation through a mask to produce spatially patterned radiation; positioning the mask relative to the input radiation; measuring the position of the mask relative to the input radiation using at least one of the interferometry methods described above; and imaging the spatially patterned radiation onto a wafer.

In another aspect, the invention features a lithography method for use in fabricating integrated chips. The lithography method includes: positioning a first component of a lithography system relative to a second component of a lithography system to expose a wafer to spatially patterned radiation; and measuring the position

of the first component relative to the second component using any of the interferometry methods described above.

In another aspect, the invention features a beam writing method for use in fabricating a lithography mask. The method includes: directing a write beam to a
5 substrate to pattern the substrate; positioning the substrate relative to the write beam; and measuring the position of the substrate relative to the write beam using any of the interferometry methods described above.

Finally, in general, in another aspect, the invention features an interferometry system for measuring changes in distance to a measurement object. The
10 interferometry system includes an interferometer, a beam steering assembly for redirecting at least one beam within the interferometer, and a control circuit for reorienting the beam steering assembly in response to changes in the angular orientation or position of the measurement object.

Embodiments of the interferometry systems and methods described above
15 include many advantages.

For example, the system can maintain the exit reference and measurement beams substantially parallel to one another over a range of orientations of the measurement object, and can do so with only a single pass of the measurement beam to the measurement object. The single-pass system reduces the bandwidth of
20 electronics needed to process electrical interference signals having Doppler shifts, relative to those of a double-pass interferometer. Furthermore, the single-pass system reduces the likelihood of depolarization, scattering, and undesired spurious reflections from transmissive optics within the interferometer, relative to those for a double-pass interferometer. Such effects can introduce errors, *e.g.*, cyclic errors, in the measured
25 phase of the electrical interference signal. Nonetheless, embodiments can also include multi-pass, *e.g.*, double-pass, configurations.

In both single-pass and multi-pass configurations, the system can minimize the transverse displacement of the exit reference and measurement beams or the transverse displacement of components of the reference and measurement beams
30 within the interferometer caused by changes in the angular orientation or position of the measurement object. As a result, the average amplitude of the electrical

interference signal produced from the mixed exit reference and measurement beams can be substantially independent of changes in the angular orientation and position of the measurement object. In addition, the system reduces changes of the paths of the measurement and reference beams through transmissive optics of the interferometer, *e.g.*, polarizing beam splitters and quarter wave plates, caused by changes in the angular orientation or position of the measurement object. Such transmissive optics can have imperfections in their surface figures and local variations in refractive index. Thus, changes in the paths of the beams through such optics can change the optical path length measured by the interferometer even though the distance between the measurement object and the interferometer has not changed. Such negative effects can be compounded if the transmissive optic has dispersive properties, such as those produced by a wedge.

Furthermore, in some embodiments, the system includes one or more polarizing beam splitters as the only transmissive optics, with all other optics being reflective. In particular, quarter wave plates are not required. Minimizing the number of transmissive optics in the system optics reduces depolarization, scattering, and undesired spurious reflections of the reference and measurement beams, which can introduce errors, *e.g.*, cyclic errors, in the measured phase of the electrical interference signal.

The interferometry systems can also include multiple interferometers and at least one beam steering assembly to measure angular orientation, in addition to displacement, of the measurement object. Such angle-measuring embodiments can enjoy many of the advantages described above.

Furthermore, the interferometer systems can involve beam components at multiple wavelengths to measure dispersion along the measurements path(s). Such dispersion measurements can be used to convert optical path length changes into geometric path length changes. Again such dispersion-measuring embodiments can enjoy many of the advantages described above.

Unless otherwise defined, all technical and scientific terms used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this invention belongs. In case of conflict with publications, patent applications,

patents, and other references mentioned incorporated herein by reference, the present specification, including definitions, will control.

Other features, aspects, and advantages will be apparent from the following detailed description and from the claims.

5

Brief Description of the Drawings

FIGS. **1a-1f** are schematic drawings of a first embodiment of the interferometry system. FIGS. **1a** and **1b** depict beam propagation in lower and upper planes, respectively. FIG. **1c** depicts beam propagation from the left end of the system shown in FIGS. **1a** and **1b**, the plane of FIG. **1c** being orthogonal to the planes of
10 FIGS. **1a** and **1b**. FIG. **1d** is a cross-sectional view of beams entering and exiting a component of the system. FIG. **1e** is a schematic drawing of a detector system and FIG. **1f** is a diagram used to discuss path length variations.

FIGS. **2a-2f** are schematic drawings of a second embodiment of the interferometry system. FIGS. **2a** and **2d** depict beam propagation in upper and lower
15 planes, respectively. FIG. **2c** depicts beam propagation as seen from the left end of the system shown in FIGS. **2a** and **2d**, the plane of FIG. **2c** being orthogonal to the planes of FIGS. **2a** and **2d**. FIG. **2b** is an inset for FIG. **2a**. FIG. **2e** depicts beam propagation as seen from a bottom view of portions of system shown in FIGS. **2a** and
20 **2d**. FIG. **2f** is a cross-sectional view of beams entering and exiting a component of the system.

FIGS. **3a-3f** are schematic drawings of a third embodiment of the interferometry system. FIGS. **3a** and **3e** are insets for FIG. **3d**. FIGS. **3b** and **3d** depict beam propagation in upper and lower planes, respectively. FIG. **3c** depicts
25 beam propagation orthogonal to the planes of FIGS. **3b** and **3d**. FIG. **3f** is a cross-sectional view of the beams as seen from the right end of the system shown in FIGS. **3b** and **3d** in a plane orthogonal to the planes of FIGS. **3b** and **3d** and also orthogonal to the plane of FIG. **3c**.

FIGS. **4a-4f** are schematic drawings of a fourth embodiment of the interferometry system. FIGS. **4a** and **4e** are insets for FIG. **4d**. FIGS. **4b** and **4d**
30 depict beam propagation in upper and lower planes, respectively. FIG. **4c** depicts

beam propagation orthogonal to the planes of FIGS. **4b** and **4d**. FIG. **4f** is a cross-sectional view of beams as seen from the right side of FIG. **4b** in a plane orthogonal to the planes of FIGS. **4b** and **4d** and also orthogonal to the plane of FIG. **4c**.

FIG. **5** is a schematic drawing of a fifth embodiment of the interferometry system.

FIGS. **6a-6b** are schematic drawings of a sixth embodiment of the interferometry system. FIGS. **6a** and **6b** depict beam propagation in orthogonal planes.

FIGS. **7a-7b** are schematic drawings of a seventh embodiment of the interferometry system. FIGS. **7a** and **7b** depict beam propagation in orthogonal planes.

FIGS. **8a-8c** are schematic drawings of an eighth embodiment of the interferometry system. FIGS. **8b** and **8c** depict beam propagation in planes that are orthogonal to the plane of FIG. **8a**.

FIGS. **9a-9c** are schematic drawings of a ninth embodiment of the interferometry system. FIGS. **9b** and **9c** depict beam propagation in planes that are orthogonal to the plane of FIG. **9a**.

FIGS. **10a-10c** are schematic drawings of a tenth embodiment of the interferometry system. FIGS. **10b** and **10c** depict beam propagation in planes that are orthogonal to the plane of FIG. **10a**.

FIGS. **11a-11f** are schematic drawings of an eleventh embodiment of the interferometry system. FIGS. **11b** and **11c** depict beam propagation in planes that are orthogonal to the plane of FIG. **11a**. FIG. **11d** is an extension of FIG. **11a**. FIGS. **11e** and **11f** are insets of FIG. **11d**.

FIGS. **12a-12e** are schematic drawings of a twelfth embodiment of the interferometry system. FIGS. **12b** depicts beam propagation in a plane that is orthogonal to the plane of FIG. **12a**. FIG. **12c** is an extension of FIG. **12a**. FIGS. **12d** and **12e** are insets of FIG. **12c**.

FIGS. **13a-13b** are schematic drawings of a thirteenth embodiment of the interferometry system. FIGS. **13b** depicts beam propagation in a plane that is orthogonal to the plane of FIG. **13a**.

FIG. 14a-c relate to lithography and its application to manufacturing integrated circuits. FIG. 14a is a schematic drawing of a lithography exposure system employing the interferometry system. FIGS. 14b and 14c are flow charts describing steps in manufacturing integrated circuits.

5 FIGS. 15a-15d are schematic drawings of additional embodiments of the interferometry system.

FIG. 16 is a schematic of a beam writing system employing the interferometry system.

10 FIGS. 17a-17c are schematic drawings of an angle and distance-measuring embodiment of the interferometry system.

FIGS. 17a and 17c are cross-sectional views in perpendicular planes, and FIG. 17b is a plan view looking into a plane perpendicular to that of FIG. 17a.

15 FIGS. 18a-18f are schematic drawings of multi-pass embodiments of the interferometry system. FIGS. 18a-18d relate to a first such embodiment, with FIGS. 18a and 18d being cross-sectional views in a first plane, FIG. 18c being a cross-sectional view in a perpendicular plane, and FIG. 18b being a plan view looking into a plane perpendicular to that of FIG. 18a. FIGS. 18e-f are schematic drawings of a second such embodiment, with both FIGS. 18e-f being cross-sectional views in a common plane.

20 FIGS. 19a-19c relate to a dispersion-measuring embodiment of the interferometry system. FIG. 19a is schematic drawing of the optical arrangement for the embodiment, FIG. 19b is a schematic drawing of a signal processor used in the embodiment, and FIG. 19c is a variation of the interferometer unit used in the optical arrangement.

25 FIG. 20 is a schematic drawing of an apparatus including a multi-axis interferometry system for providing interferometric angle information about the orientation of a measurement object and a beam steering assembly for directing an input beam into the multi-axis interferometry system based on the interferometric angle information.

30 FIG. 21 is a schematic drawing of another apparatus including an interferometry system for providing interferometric angle information about the

orientation of a measurement object and a beam steering assembly for directing an input beam into the interferometry system based on the interferometric angle information.

5

Detailed Description

The invention features an interferometry system including an interferometer and at least one beam steering assembly controlled by a control circuit. In some embodiments, the beam steering assembly is a component of the interferometer, directing at least one of the reference and measurement beams within the
10 interferometer. In other embodiments, the beam steering assembly is separate from the interferometer, directing an input beam to the interferometer, and optionally, the output beam from the interferometer. The beam steering assembly redirects one or more of the input, output, reference, and measurement beams to minimize undesired consequences of changes in the angular orientation or position of the measurement
15 object.

Four embodiments of the invention will be first described wherein these embodiments involve relatively few components and beam propagation in only one plane. Nonetheless, these embodiments demonstrate important features of the invention that will be expanded upon in additional embodiments described
20 subsequently.

A schematic of an embodiment of the invention is shown in FIG. **15a**. A polarizing beam splitter **1512** in an interferometer **1510** receives an input beam **1514** from a laser source (not shown) and separates input beam **1514** into reference beam **1516** (dotted line) and measurement beam **1518** (solid line), which are linearly
25 polarized orthogonal to one another. The polarizing beam splitter **1512** includes a polarizing interface **1562** for reflecting beams having a polarization orthogonal to the plane of FIG. **15a** and a back reflective surface **1564** for reflecting beams transmitted through polarizing interface **1562**.

In the described embodiment, the orthogonally polarized reference and
30 measurement beams are frequency-shifted with respect one another, *e.g.*, by Zeeman splitting, acousto-optic modulation, or by use of birefringent elements internal to the

laser, prior to entering interferometer **1510** as components of input beam **1514**. The different frequencies enable the interferometry system to generate a heterodyne interference signal. Although the described embodiment is a heterodyne system, the instant invention is readily adapted for use in a homodyne system in which the
5 reference and measurement beams have the same frequencies.

Polarizing beam splitter **1512** directs the measurement beam **1518** to a beam steering assembly **1520**, which includes a beam steering mirror **1522** and a pair of piezoelectric transducers **1524** and **1526**. The transducers are coupled to the beam steering mirror **1522** by flexures to orient the beam steering mirror in response to a
10 signal **1528** from a servo controller **1530**. The beam steering assembly may include capacitance gauges to measure changes in orientation and/or position of the beam steering mirror **1522**. The capacitance gauges may also be used to measure and/or monitor the properties of the piezoelectric transducers **1524** and **1526**.

Beam steering assembly **1520** directs the measurement beam through reference
15 retroreflector **1532**, reference retroreflector **1532** being truncated so that a beam passing centrally through retroreflector **1532** is not retroreflected, to contact a stage mirror **1534**, *i.e.*, the measurement object, at substantially normal incidence. Stage mirror **1534** then reflects the measurement beam back to retrace its path to beam steering assembly **1520** and polarizing beam splitter **1512**. The measurement beam
20 double passes a quarter wave plate **1536**, which is positioned between the beam steering assembly **1520** and polarizing beam splitter **1512** and which rotates the linear polarization of the measurement beam by 90°.

Polarizing beam splitter **1512** directs the reference beam **1516** to the beam steering assembly **1520**, which in turn directs the reference beam to reference
25 retroreflector **1532**. The reference retroreflector then directs the reference beam back to beam steering assembly **1520** and onto polarizing beam splitter **1512**. The reference beam also double passes quarter wave plate **1536**, which rotates the linear polarization of the reference beam by 90°.

Polarizing beam splitter **1512** then recombines the polarization-rotated
30 reference and measurement beams to form overlapping exit reference and measurement beams, which together form an output beam **1540**. A beam splitter **1542**

sends a portion of output beam **1540** to a detector system **1544**, which measures the difference in directions of propagation of the exit reference and measurement beams. The detector system sends an error signal **1550** indicative of any such difference to servo controller **1530**, which sends signal **1528** to beam steering assembly **1520** in response to the error signal. The beam steering assembly **1520** changes, in response to signal **1528**, the orientation of beam steering mirror **1522** preferably about a nodal point of reference retroreflector **1532**, changes in orientation of beam steering mirror **1522** about a nodal point of reference retroreflector **1532** producing substantially reduced lateral shear effects experienced by the reference beam.

Alternatively when the direction of the input beam **1514** is constant, detector system **1544** can measure the difference in position of the exit measurement beam from a reference position in the detector system and generate error signal **1550** indicative of that difference in position, a difference in position of the exit measurement beam being the consequence of a change in direction of propagation of the exit measurement beam component of output beam **1540**. For example, the reference position can be the position of the exit measurement beam in the detector system corresponding to the measurement beam retroreflecting from stage mirror **1534**, *i.e.*, contacting the stage mirror at normal incidence, and the stage mirror **1534** being at a nominal null orientation. In other embodiments, the detector system can include multiple detectors for determining the direction and position of the exit reference and measurement beams and can generate an error signal based on such information.

Changes in the angular orientation of stage mirror **1534** change the direction of the measurement beam and the direction of subsequent exit measurement beam. This causes detector system **1544** to generate error signal **1550**. Servo-controller **1530** responds to the error signal by directing beam steering assembly **1520** to reorient beam steering mirror **1522** so as to minimize the error signal, *e.g.*, by directing the measurement beam to the stage mirror at normal incidence. As a result, the exit reference and measurement beams remain substantially parallel to one another and the position of the exit measurement beam remains substantially constant over a range of angular orientations of the stage mirror. Furthermore, since beam steering assembly

1520 redirects each of the reference and measurement beams twice, there is no change in the relative optical path length between the reference and measurement beams to first order in a translation of beam steering mirror 1522 in a direction normal to the reflecting surface of beam steering mirror 1522. In addition, when the measurement
5 beam is directed to the stage mirror at normal incidence and the paths of the measurement and reference beams have substantially the same centroids, there is no change in the relative optical path length between the reference and measurement beams to first order in any angular orientation change of the stage mirror (about the center of a measurement beam spot on the stage mirror) and any corresponding change
10 in the beam steering element.

The remainder of output beam 1540, after beam splitter 1542 passes through a polarizer 1545, which mixes polarizations of the exit reference and measurement beams to form a mixed beam 1546. A signal processing system 1548 measures the intensity of the mixed beam, *e.g.*, by photoelectric detection, to produce an electrical
15 interference signal or electrical heterodyne signal, extracts the phase of the electrical heterodyne signal, and determines from that phase the difference in optical path length between the paths of the reference and measurement beams.

In other embodiments, detector system 1544 could be part of a separate angle sensing system (not shown), comprised of an additional light beam (not shown)
20 directed towards stage mirror 1534. The separate angle sensing system would measure the absolute or relative angular orientation of stage mirror 1534 using the additional light beam and would send a measurement signal to servo-controller 1530 indicative of that orientation. As in the embodiment of FIG. 15a, servo-controller 1530 would control beam steering assembly 1520 based on the signal from the
25 detector system. In addition, in embodiments in which several interferometry systems each direct a measurement beam to a measurement object, a single angle sensing system can be used to guide control of the beam steering assembly in each of the interferometry systems.

Furthermore, in an interferometry systems (e.g., a multi-axis interferometry
30 system) configured to measure the angular orientation of measurement stage, the angle

measurement itself could be used to provide the error signal used to orient the beam steering element.

In another embodiment similar to that of FIG. 15a, a polarizing beam splitter 1512 and the beam steering assembly 1520 are combined into a single unit, as shown
5 by polarizing beam splitter and beam steering assembly 1560 in FIG. 15b. In this variation, transducers 1524 and 1526 are coupled through flexures directly to polarizing beam splitter 1512. As a result, servo controller 1530 orients the polarizing interface 1562 and reflective back surface 1564 of polarizing beam splitter 1512 via transducers 1524 and 1526 to direct the reference and measurement beams to
10 reference retroreflector 1532 and stage mirror 1534, respectively. Quarter wave plate 1536 is positioned between reference retroreflector 1532 and beam steering assembly 1560. Other features of this embodiment are the same as those of the embodiment in FIG. 15a and are numbered the same.

In a further embodiment, similar to that of FIG. 15a and shown in FIG. 15c,
15 input beam 1514 first contacts beam steering assembly 1520, which then directs the input beam into the interferometer 1570. In this embodiment, the interferometer includes polarizing beam splitter 1512, quarter wave plate 1536, and reference retroreflector 1532, but does not include beam steering assembly 1520, which is outside the interferometer. As in the embodiment of FIG. 15b, the polarizing beam
20 splitter 1512 directs the reference and measurement beams to reference retroreflector 1532 and stage mirror 1534, respectively, and recombines the reflected reference and measurement beams to form the overlapping exit reference and measurement beams, which are the components of output beam 1540. Beam steering assembly 1520 then receives output beam 1540 and directs it to detection system 1544 and signal
25 processing system 1548, as in the embodiment of FIG. 15a.

As in the embodiment of FIG. 15a, servo controller 1530 in FIG. 15c orients beam steering mirror 1522 of assembly 1520 to minimize the error signal generated by detection system 1544. To do so, servo controller 1530 orients beam steering mirror 1522 of assembly 1520 to direct the input beam into interferometer 1570 such that the
30 measurement beam contacts stage mirror 1534 at normal incidence over a range of angular orientations of the stage mirror. The beam steering assembly 1520 changes, in

response to signal **1528**, the orientation of beam steering mirror **1522** preferably about a nodal point of reference retroreflector **1532**, changes in orientation of beam steering mirror **1522** about a nodal point of reference retroreflector **1532** producing substantially reduced lateral shear effects (transverse displacement) on the reference beam. As a result, the exit reference and measurement beams, which form the output beam, emerge from the interferometer substantially parallel and with reduced transverse separation. Changes in the direction of the output beam emerging from the interferometer caused by the beam steering assembly redirecting the input beam are compensated when the output beam contacts the beam steering assembly, which directs the output beam to detection system **1544** and signal processing system **1548**. Although this compensation of the output beam direction by the beam steering assembly is preferable, it is not necessary because changes in the angular orientation of the stage mirror are typically small enough so as to not prevent the output beam from reaching the detection system **1544** and signal processing system **1548**. Thus in additional embodiments, the output beam need not contact the beam steering element.

In another embodiment similar to FIG. **15a** and shown in FIG. **15d**, the interferometry system receives a pair of spatially separated input beams to define the reference and measurement beams rather than separating a single input beam into the reference and measurement beams. In this embodiment, an interferometer **1580** receives spatially separated input beams **1582** and **1584** polarized orthogonal to one another and a polarizing beam splitter **1586** directs the received input beams along different paths to define reference beam **1516** and measurement beam **1518**. Prior to entering polarizing beam splitter **1586**, a portion of the input beams is split off by a non-polarizing beam splitter **1588** and directed to a reference phase detector **1590**. The reference phase detector includes optics to optically mix the input beams and electronics to measure the relative optical phase of the mixed beams. Reference phase detector **1590** sends a reference phase signal **1592** indicative of the relative phase difference between input beams **1582** and **1584** upon entering interferometer **1580** to signal processing system **1548**, which uses signal **1592** to determine the difference in optical path length between the paths of the reference and measurement beams.

The remaining description for the embodiment of FIG. 15d is identical to that for FIG. 15a with polarizing beam splitter 1586 recombining reference beam 1516 and measurement beam 1518 to form output beam 1540. The embodiment of FIG. 15d and other such embodiments in which the interferometer receives spatially separated input beams to define the reference and measurement beams reduces paths within optics of the interferometer in which the reference and measurement beams overlap one another. Such a reduction reduces polarization mixing between the reference and measurement beams that can cause cyclic errors in the heterodyne signal measured by system 1548. For a reference describing such cyclic errors, see, *e.g.*, N. Bobroff, *Appl. Opt.*, 26:2676-2681, 1986. Also, in other embodiments such as that of FIG. 15c in which the beam steering assembly is outside the interferometer, the beam steering mirror can direct spatially separated input beams into the interferometer to define the reference and measurement beams.

The concepts inherent in the systems described above and shown in FIGS. 15a-15d can be extended to other applications. For example, other embodiments can address changes in the angular orientation and position of the measurement object along multiple dimensions. Also, other embodiments can insure that the transverse spatial profile of the exit reference beam is not inverted relative to that of the exit measurement beam when these beams are mixed to produce the interference signal. Also, other embodiments can include additional beam steering assemblies. Such alternative embodiments are described further below.

In general, these embodiments relate to apparatus and methods for measuring and monitoring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, wherein the lateral displacement is orthogonal to the linear displacement. An example of an important application is in using an interferometry system to measure and monitor along a given dimension the location of one or more stages in a lithographic tool that is stepping and/or scanning in either one, two, or three orthogonal dimensions.

The embodiments described below comprise an interferometer and at least one beam steering assembly, which can be a component of, or separate from, the

interferometer. The embodiments generally fall into one of three classes. In the first class, the beam steering assembly is positioned to direct components of both a measurement beam and a reference beam. In the second class, the beam steering assembly is positioned to direct components of the measurement but not the reference beam. And, in the third class, the beam steering assembly is positioned to direct an input beam to and an output beam from, the interferometer.

Within each class, the interferometry systems can function in one or both of two different modes of operation. The first mode of operation compensates for changes in the direction of the measurement beam or exit measurement beam caused by changes in the angular orientation of the measurement object. The changes in angular orientation can be along one or more directions, *e.g.*, changes in pitch and yaw. The second mode of operation compensates for changes in the transverse position of the measurement beam or exit measurement beam caused by changes in the position of the measurement object. The changes in position can be along any of two transverse directions, *i.e.*, directions orthogonal to the displacement being measured, and a longitudinal direction, *i.e.*, a direction along the displacement being measured.

The modes of operation for a particular interferometry system depend on the reflective properties of the measurement object. For example, if the measurement beam reflects from a plane mirror, changes in the angular orientation of the plane mirror about two orthogonal axes in the plane of the mirror causes changes the direction of the reflected measurement beam relative to the two axes. However, translations of the plane mirror along either of these two axes do not affect the direction or transverse position of the reflected measurement beam. Therefore, for applications in which the measurement beam reflects from a plane mirror of the measurement object, the system typically operates in the first mode.

In a different example, if the measurement beam reflects from a retroreflector, the direction of the reflected measurement beam is independent of changes in the angular orientation or position of the measurement object. However, translations of the retroreflector along directions orthogonal to an incoming measurement beam cause changes in the transverse position of the reflected measurement beam. Therefore, for

an application in which the measurement beam retroreflects from a measurement object in a given plane, the system typically operates in the second mode for translations of the measurement object in that plane and orthogonal to the incoming measurement beam.

5 As would be clear to those skilled in the art, applications in which the measurement object includes a roof prism to reflect the measurement beam combine features of the previous two examples. In such an application, the system operates in both the first and second modes.

10 The system can also operate in both first and second modes for applications in which the measurement object includes a plane mirror to reflect the measurement beam, and the measurement beam contacts the plane mirror at non-normal incidence. In such applications longitudinal translations of the measurement object change the transverse position of the reflected measurement beam and changes in the angular orientation of the measurement object change the direction of the reflected
15 measurement beam.

 Embodiments of the interferometry system can also include single and multiple passes of the measurement beam to the measurement object. In single-pass systems, changes in the angular orientation or position of the measurement object cause changes in the direction or transverse position of the exit measurement beam.
20 The changes to the exit measurement beam as detected by a detector system provide the basis for an error signal used to control the beam steering assembly. In some multiple pass arrangements, changes in the angular orientation or position of the measurement object do not change the direction and/or transverse position of the exit measurement beam but do change the direction and/or transverse position of the
25 measurement beam within the interferometer. To compensate for changes in the direction and/or transverse position of the measurement beam within the interferometer, some embodiments of the interferometry system split off an intermediate beam from the measurement beam after the measurement beam has contacted the measurement object an odd number of times. The direction and/or
30 position of the intermediate beam as detected by a detector system provide the basis for an error signal used to control the beam steering assembly.

For each of the embodiments of the present invention, the interferometer and at least one beam steering assembly are configured such that a displacement of certain optical elements of the at least one beam steering assembly as a unit does not effect in at least first order the difference between the optical path length of the measurement and reference beams. For the first mode of operation, the interferometer and at least one beam steering assembly are configured such that changes in the orientations of the measurement object and/or of certain optical elements of a beam steering assembly as a unit substantially do not effect in at least first order the difference between the optical path length of the measurement and reference beams. For the second mode of operation, the interferometer and at least one beam steering assembly are configured such that a displacement in the location of the measurement object orthogonal to the linear displacement substantially does not effect in at least first order the difference between the optical path length of the measurement and reference beams.

FIGS. **1a-1f** depict, in schematic form, a first embodiment of the present invention for measuring a linear displacement of a measurement object substantially independent of the orientation of the measurement object and substantially independent of a lateral displacement of the measurement object, the lateral displacement being orthogonal to the linear displacement. The first embodiment is from the first class of embodiments and variants thereof of the present invention, which operate in the first mode of operation for changes in orientation of the measurement object about two orthogonal axes.

The first embodiment comprises light beam **110**, a beam steering assembly, a first and second beam splitting assemblies, retroreflector **172**, measurement object mirror **170** comprised of a single reflecting surface, and reference beam mirror **178** comprised of a single reflecting surface. Prism **150** and rhomboidal prism **154** comprise the first beam splitting assembly depicted in FIG. **1a** wherein interface **152** is a polarizing beam splitting interface and surface **156** is a reflector. Rhomboidal prism **160**, prisms **166** and **186**, and dove prism **182** comprise the second beam splitting assembly depicted in FIG. **1b** wherein interface **162** is a reflector, interfaces surfaces **164** and **174** are polarizing beam splitting interfaces, interface surface **184** in

a nonpolarizing beam splitting interface, and interface surface **180** shown as a dotted line in FIG. **1b** is antireflection coated.

The first embodiment is adapted for use as a heterodyne interferometer system. A source (not shown in FIGS. **1a-1f**) provides for the first embodiment an entrance
5 beam **110** comprised of two orthogonally polarized components of differing frequencies.

The light source such as a laser can be any of a variety of frequency modulation apparatus and/or lasers. For example, the laser can be a gas laser, *e.g.* a HeNe, stabilized in any of a variety of conventional techniques known to those skilled
10 in the art, see for example, T. Baer *et al.*, "Frequency Stabilization of a 0.633 μm He-Ne-longitudinal Zeeman Laser," *Applied Optics*, **19**, 3173-3177 (1980); Burgwald *et al.*, U.S. Pat. No. 3,889,207, issued June 10, 1975; and Sandstrom *et al.*, U.S. Pat. No. 3,662,279, issued May 9, 1972. Alternatively, the laser can be a diode laser frequency stabilized in one of a variety of conventional techniques known to those skilled in the
15 art, see for example, T. Okoshi and K. Kikuchi, "Frequency Stabilization of Semiconductor Lasers for Heterodyne-type Optical Communication Systems," *Electronic Letters*, **16**, 179-181 (1980) and S. Yamaaguchi and M. Suzuki, "Simultaneous Stabilization of the Frequency and Power of an AlGaAs Semiconductor Laser by Use of the Optogalvanic Effect of Krypton," *IEEE J.*
20 *Quantum Electronics*, **QE-19**, 1514-1519 (1983).

Two optical frequencies may be produced by one of the following techniques:
(1) use of a Zeeman split laser, see for example, Bagley *et al.*, U.S. Patent No. 3,458,259, issued Jul. 29, 1969; G. Bouwhuis, "Interferometrie Mit Gaslasers," Ned. T. Natuurk, **34**, 225-232 (Aug. 1968); Bagley *et al.*, U.S. Patent No. 3,656,853, issued
25 Apr. 18, 1972; and H. Matsumoto, "Recent interferometric measurements using stabilized lasers," *Precision Engineering*, **6**(2), 87-94 (1984); (2) use of a pair of acousto-optical Bragg cells, see for example, Y. Ohtsuka and K. Itoh, "Two-frequency Laser Interferometer for Small Displacement Measurements in a Low Frequency Range," *Applied Optics*, **18**(2), 219-224 (1979); N. Massie *et al.*, "Measuring Laser
30 Flow Fields With a 64-Channel Heterodyne Interferometer," *Applied Optics*, **22**(14), 2141-2151 (1983); Y. Ohtsuka and M. Tsubokawa, "Dynamic Two-frequency

Interferometry for Small Displacement Measurements,” *Optics and Laser Technology*, 16, 25-29 (1984); H. Matsumoto, *op. cit.*; P. Dirksen, *et al.*, U.S. Patent No. 5,485,272, issued Jan. 16, 1996; N. A. Riza and M. M. K. Howlader, “Acousto-optic system for the generation and control of tunable low-frequency signals,” *Opt. Eng.*, 35(4), 920-925 (1996); (3) use of a single acousto-optic Bragg cell, see for example, 5 G. E. Sommargren, commonly owned U.S. Patent No. 4,684,828, issued Aug. 4, 1987; G. E. Sommargren, commonly owned U.S. Patent No. 4,687,958, issued Aug. 18, 1987; P. Dirksen, *et al.*, *op. cit.*; (4) use of two longitudinal modes of a randomly polarized HeNe laser, see for example, J. B. Ferguson and R. H. Morris, “Single Mode 10 Collapse in 6328 Å HeNe Lasers,” *Applied Optics*, 17(18), 2924-2929 (1978); or (5) use of birefringent elements or the like internal to the laser, see for example, V. Evtuhov and A. E. Siegman, “A “Twisted-Mode” Technique for Obtaining Axially Uniform Energy Density in a Laser Cavity,” *Applied Optics*, 4(1), 142-143 (1965).

The specific device used for the source of beam 110 will determine the 15 diameter and divergence of beam 110. For some sources, *e.g.* a diode laser, it will likely be necessary to use conventional beam shaping optics, *e.g.* a conventional microscope objective, to provide beam 110 with a suitable diameter and divergence for the elements that follow. When the source is a HeNe laser, for example, beam shaping optics may not be required.

20 Beam 110 impinges on the first beam splitting assembly, as illustrated in FIG. 1a, with a portion of beam 110 transmitted by interface 152 and reflected by surface 156 as measurement beam 111. Beam 111 is polarized in the plane of FIG. 1a. A second portion of beam 110 is reflected by interface 152 as reference beam 112 orthogonally polarized to the plane of FIG. 1a.

25 Beam 111 enters beam steering element 158 (*cf.* FIG. 1a) and exits beam steering element 158 as beam 113 (*cf.* FIG. 1b) displaced laterally from beam 111 and propagating in a direction nominally opposite to the direction of propagation of beam 111. The projections of beam 113 and beam 111 in the plane of FIG. 1b are superimposed. In beam steering element 158, beam 111 is reflected in sequential 30 order, *e.g.*, by total internal reflection, by each of the surfaces 158A, 158B, and 158C (*cf.* FIG. 1c which presents an end view of the interferometer depicted in FIG. 1a and

which shows the path of reference beam 112 in beam steering element 158). A beam steering assembly that redirects measurement beam 113 comprises beam steering element 158 and orientation/translation transducer 159. Orientation/translation transducer 159 preferably alters the orientation of beam steering element 158 about a nodal point of retroreflector 172 for a change in orientation in the plane of FIG. 1c, and/or alters the location of steering element 158 in the nominal direction of propagation of beam 111, wherein changes in orientation of beam steering element 158 about a nodal point of retroreflector 172 substantially reduce lateral shear effects experienced by the reference beam. The orientation of beam steering element 158 is controlled by electronic signal 140 and the location of beam steering element 158 is controlled by electronic processor and computer 194 through electronic signal 144.

Beam 113 enters the second beam splitting assembly, depicted in FIG. 1b, wherein it is reflected at interface 162 as beam 115 and then transmitted by polarizing beam splitting interface 164 as beam 117. Beam 117, polarized in the plane of FIG. 1b, is transmitted by quarter wave phase retardation plate 168 as a circularly polarized beam, reflected by measurement object mirror 170 as a beam with opposite-handed circular polarization, and subsequently transmitted by phase retardation plate 168 as beam 119 linearly polarized orthogonal to the plane of FIG. 1b. Beam 119 enters the second beam splitting assembly and is reflected by polarizing beam splitting interface 164 as beam 121.

Beam 121 exits the second beam splitting assembly, enters beam steering element 158 (*cf.* FIG. 1b), and exits beam steering element 158 as beam 123 (*cf.* FIG. 1a) propagating in a direction nominally opposite to the direction of propagation of beam 121. Beam 123 enters retroreflector 172 (*cf.* FIG. 1a) and is retroreflected as beam 125 (*cf.* FIG. 1b). Beams 123 and 125 are shown in FIG. 1d as entering and exiting beams, respectively, to and from retroreflector 172, respectively.

Reference beam 112 enters beam steering element 158 (*cf.* FIG. 1a) and exits beam steering element 158 as beam 114 (*cf.* FIGS. 1b and 1c) propagating in a direction nominally opposite to the direction of propagation of beam 112. The projections of beams 114 and beam 112 are superimposed in the plane of FIG. 1a. The projections of the paths of beams 111 and 112 through beam steering element 158

are superimposed in the plane of FIG. 1c. Beam 114 enters retroreflector 172 (*cf.* FIG. 1b) and is retroreflected as beam 116 (*cf.* FIG. 1a). In FIG. 1d, beams 114 and 116 are shown as entering and exiting beams, respectively, to and from retroreflector 172, respectively. Beam 116 enters beam steering element 158 (*cf.* FIG. 1a) and exits
5 beam steering element 158 as beam 118 (*cf.* FIG. 1b) propagating in a direction nominally opposite to the direction of propagation of beam 116.

Beam 118 enters the second beam splitting assembly and a portion of beam 118 is reflected by polarizing beam splitting interface 174 as beam 120 (*cf.* FIG. 1b). Beam 120, orthogonally polarized to the plane of FIG. 1b, is transmitted by quarter
10 wave phase retardation plate 176 as a circularly polarized beam, reflected by reference mirror 178 as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate 176 as beam 122 linearly polarized in the plane of FIG. 1b. Beam 122 enters the second beam splitting assembly and 122 is transmitted by polarizing beam splitting interface 174 as beam
15 124. Beam 124 is transmitted by antireflection coated interface 180 as beam 126.

Measurement beam 125 enters, as shown in FIG. 1b, the second beam splitting assembly and a first portion of beam 125 is transmitted by nonpolarizing beam splitting interface 184 as one component of a first output beam 128. A first portion of beam 126 is reflected by nonpolarizing beam splitter interface 184 as a second
20 component of the first output beam 128. First output beam 128 is reflected by reflecting interface 162 as output beam 130. Output beam 130 impinges on detector 188 to produce an electrical signal 140 with two components related to any difference in the directions of propagation of measurement and reference beam components in output beam 130 in two orthogonal planes, respectively.

25 A second portion of beam 125 is reflected by nonpolarizing beam splitting interface 184 as one component of a second output beam 132. A second portion of beam 126 is transmitted by nonpolarizing beam splitting interface 184 as a second component of the second output beam 132. Beam 132 is transmitted by a polarizer 190 orientated to produce a mixed optical beam 134. Beam 134 impinges on detector
30 192 to generate electrical signal 142 related to the difference in phase of the measurement and reference beam components of mixed beam 134. Electrical signal

142 is transmitted to electronic processor and computer 194 for subsequent processing to obtain information about the difference in phase of the measurement and reference beam components of mixed beam 134. The detection of mixed beam is typically by photoelectric detection to produce a heterodyne signal, the phase of which is related to the difference in optical path lengths of the measurement and reference beams. The phase of the heterodyne signal may be determined by electronic processor and computer 194 for example from a Fourier transform or Hilbert transform of the heterodyne signal.

The elements of detector 188 are depicted, in schematic form, in FIG. 1e. Beam 130 enters a polarizing beam splitter comprising prisms 188A and 188C with polarizing interface 188B. The measurement beam component of beam 130, being polarized orthogonal to the plane of FIG. 1e is reflected by polarizing interface 188B as beam 130M. Beam 130M is focused by lens 188D to a spot on detector 188E such as a quad cell detector, a two-dimensional high speed CCD camera, or a lateral effect photodiode. Two-dimensional data arrays are transmitted as electronic signal 140A to electronic processor 188H for subsequent processing. The location of the spot on detector 188E is not effected by a lateral shear of beam 130M but a change in the direction of propagation beam 130M does shift the location of the spot on detector 188E. Thus the electronic signal contains information about the direction of propagation of beam 130M.

The reference beam component of beam 130, being polarized in the plane of FIG. 1e is transmitted by polarizing interface 188B as beam 130R. Beam 130R is focused by lens 188F to a second spot on a second detector 188G such as a quad cell detector, a two-dimensional high speed CCD camera, or a lateral effect photodiode. Two-dimensional data arrays are transmitted as electronic signal 140B to electronic processor 188H for subsequent processing. The location of the second spot on detector 188G is not effected by a lateral shear of beam 130R but a change in the direction of beam 130R does shift the location of the second spot on detector 188G. Thus the electronic signal 130R contains information about the direction of propagation of beam 130R.

Electronic processor **188H** processes the electronic signals **140A** and **140B** to generate two electronic signals **140C** and **140D** where the two electronic signals **140C** and **140D** are proportional to the difference in the directions of propagation of the measurement and reference beam components of beam **130** in two orthogonal planes.

5 Electronic signals **140C** and **140D** comprise electronic signal **140**.

Electrical signal **140** is transmitted to orientation/translation transducer **159**. Information contained in signal **140** is used as the error signal in a servo system to alter the orientation of beam steering mirror **158** by orientation/translation transducer **159** so as to maintain in two dimensions the direction of propagation of measurement beam **123** substantially constant independent of changes of orientation of measurement object mirror **170** about two orthogonal axes. Under the condition that the physical path length of the measurement beam from the location of the first redirection of the measurement beam by the beam steering element **158** to measurement object mirror **170** is equal to the physical path length of the measurement beam from measurement object mirror **170** to the location of the second redirection of the measurement beam by the beam steering mirror **158**, there will be no lateral shear of beam **123** at beam steering element **158** when changes in orientation of measurement object mirror **170** are compensated by changes in orientation of beam steering element **158**. This condition with respect to physical path lengths will be referenced as the first embodiment condition.

Compliance with the first embodiment condition eliminates the lateral shear of measurement beam **123** at beam steering element **158** when changes in orientation of measurement object mirror **170** are compensated by changes in orientation of beam steering element **158**. However, there will be introduced lateral shear of reference beam **126** when changes in orientation of measurement object mirror **170** are compensated by changes in orientation of beam steering element **158**. Although a lateral shear will be introduced in reference beam **126**, the magnitude of the lateral shear is significantly reduced in relation to the lateral shear introduced in measurement beam components of prior art plane mirror interferometers due to changes in orientation of the measurement object mirror, the reduction factor being

proportional to the ratio of the physical length of the reference leg to the physical length of the measurement leg of an interferometer.

For certain end use applications, it may be desirable to introduce a translation of beam steering element **158** in a direction nominally parallel to the direction of propagation of **123**. A translation of this type for beam steering element **158** is controlled by the signal processor and computer **194** through electrical signal **144** transmitted to orientation/translation transducer **159**.

The inventive use of an active servo control of an adjustable element makes it possible to perform accurate displacement measurements to measurement object mirror **170** using a single pass of a measurement beam to measurement object mirror **170**. For applications where the first embodiment condition is satisfied to a certain relative precision, the inventive technique reduces (to the certain relative precision) measurement object mirror **170** orientation-dependent errors in the phase of the measurement beam relative to the phase of reference beam caused by lateral beam shear and uncompensated dispersive properties of the elements of the interferometer.

The interferometer and beam steering assembly of the first embodiment are configured such that a displacement of beam steering element **158** does not effect in at least in second order the optical path length of the measurement beam relative to the optical path length of the reference beam; both the reference and measurement beams have their directions of propagation redirected twice by beam steering element **158** with substantially the same angles of incidence in each instance of redirection, the centroids of the paths of the reference and measurement beams entering beam steering element **158** are substantially coextensive, and the centroids of the paths of the reference and measurement beams exiting beam steering element **158** are substantially coextensive. An example from the set of lowest order effects of a displacement of beam steering element **158** on the optical path length of the measurement beam relative to the optical path length of the reference beam will be first order in the magnitude of the displacement of beam steering element **158**, first order in the magnitude of a change of orientation of the measurement object mirror **170**, and first order in some uncompensated errors in the figure of one or more surfaces of elements of the interferometer.

The interferometer and the beam steering assembly are configured such that changes in the orientations of the object mirror (about the center of a measurement beam spot on the object mirror) and/or of beam steering element 158 do not effect in first order the optical path length of the measurement beam relative to the optical path length of the reference beam; the residual second order effect is proportional the difference in the path lengths of the measurement and reference beams and proportional to a factor which is second order in the angular change in orientation of the object mirror about an orientation corresponding to the measurement beam spot. The magnitude of the second order effect is reduced by the single-pass of the measurement beam to the measurement object relative to multiple-pass arrangements.

The second order effect cited in the preceding paragraph is described with the aid of FIG. 1f. FIG. 1f depicts in schematic form the equivalent path of the measurement beams for a first case of object mirror at initial angular orientation and for a second case of measurement object mirror 170 with a change in orientation in the plane of FIG. 1f. Measurement object mirror 170 for the second case is shown as measurement object mirror 170A rotated about point a by an angle β . The distance measured by the interferometer for case one is twice the distance between the points a and b, the distance between the points a and b being denoted by ab . The line from point b to point c is orthogonal to the surface of measurement object mirror 170A as a consequence of the action of the beam steering element 158 controlled of the servo system. Therefore the distance measured by the interferometer for case two is twice the distance between the points b and c, the distance between the points b and c being denoted by bc . The distance $2bc$ is related to the distance $2ab$ as

$$2bc = 2ab \cos \beta \quad (1)$$

The cosine factor in equation (1) differs from the value of one by a term that is second order β , i.e. $\beta^2/2$.

Another feature of the first embodiment is that there will be no lateral shear of either the measurement or reference beams and beam components in at least first order

produced by a translation of beam steering element **158** in the nominal direction of propagation of beams exiting beam steering element **158**; the directions of propagation of the reference and measurement beams entering and exiting beam steering element **158** are substantially parallel.

5 A notable feature of the first embodiment is that the interferometer and the beam steering assembly is of the noninverting type, *i.e.* corresponding points in the wavefront amplitudes of the reference and measurement beam components of input beam **110** map to substantially superimposed points in the wavefront amplitudes of the reference and measurement beam components of output beam **130** and of the
10 reference and measurement beam components of output beam **132**. Associated with this latter feature is a concomitant feature that the angle between the reference and measurement beam components of beam **130** and the angle between the reference and measurement beam components of beam **132** are not effected in first and higher orders by changes in the direction of propagation of input beam **110**.

15 It will be apparent to those skilled in the art that as a consequence of the concomitant feature cited in the last paragraph, detector **188** can perform its function in the servo system by detecting changes in a lateral position in one or two orthogonal directions of the measurement beam component of the first output beam **130** if the direction of propagation of the input beam **110** is fixed without departing from either
20 the spirit or the scope of the present invention. To change the properties of detector **188** from the detection of a change in direction of propagation of a particular beam in one plane to the detection of a lateral shear in the one plane, a portion of the particular beam is split off by a nonpolarizing beam splitter and transmitted without passing through a focusing lens directly to a detector such as a dual cell detector, the dual cell
25 detector being orientated to detect the lateral shear. The dual cell detector is sensitive to a lateral shear of the particular beam but not sensitive to a change at the dual cell detector in the direction of propagation of the particular beam. To change the properties of detector **188** from the detection of changes in direction of propagation in two orthogonal planes of a particular beam to the detection of a lateral shear in two
30 orthogonal directions, the particular beam is transmitted without passing through a focusing lens directly to a detector such as a quad cell detector. The quad cell detector

is sensitive to a lateral shear of the particular beam but not sensitive to a change at the quad cell detector in the direction of propagation of the particular beam.

It will further be evident to those skilled in the art that in an application of the first embodiment to a lithographic stepper/scanner, the measurement object mirror can
5 be attached to a wafer stage and the reference mirror can be attached to a lens assembly, the lens assembly used to focus an exposure radiation beam onto a wafer, to form a column reference without departing from the scope or spirit of the invention.

There are several additional advantages of the first embodiment. One additional advantage is that the paths for the measurement beam and reference beam
10 are highly symmetric, meaning generally that for each segment of the measurement beam path there is a substantially parallel corresponding segment of the reference beam path except for the variable air path defined by the location of the measurement object mirror 170 and quarter wave phase retardation plate 168. Further, the measurement beam and the reference beam can be made to pass through the same
15 amount of glass and air, exclusive only of the variable air path defined by the location of measurement object mirror 170 and quarter wave phase retardation plate 168, by replacing with glass a section of the path of reference beam 114 that is in air (*cf.* FIG. 1b). This symmetry leads to high thermal and mechanical stability.

Another additional advantage is that the measurement beam and reference
20 beam each reflect from the same flat surfaces, including the surfaces of the retroreflector 172, an equal number of times except for surfaces 152 and 156 of rhomboidal prism 154 of the first beam splitting assembly, surfaces 162 and 184 of dove prism 182 of the second beam splitting assembly, and measurement object mirror 170 and reference mirror 178. This greatly reduces the requirements for
25 parallelism of the various reflecting surfaces of the first embodiment.

Another additional advantage is that the first embodiment is comprised of easily fabricated optical components. Retroreflector 172 may be of the common type, either solid or hollow. The first and second beam splitting assemblies may be fabricated from ordinary right angle prisms, dove prisms, and rhomboidal prisms. The
30 beam steering element 158 being a trapezoidal shape prism which may be easily

fabricated, either solid or hollow. The trapezoidal shape prism may be fabricated in particular by truncating an equilateral prism.

Another additional advantage is that there are very few opportunities for ghost reflections, that is spurious reflections, particularly with regard to spurious multiple
5 passing of beams to measurement object mirror 170. This characteristic reduces the possibility for generation of cyclic errors in the relative phase of the measurement and reference beams measured by the inventive apparatus, cyclic errors that are common to prior-art plane-mirror interferometers.

Another feature of the first embodiment is that beam steering element 158
10 effects changes in the ellipticity of reflected beams that is of the order of or less than the changes in orientation of beam steering element 158. The effect on the cyclic errors in the measured relative phase difference between the measurement and reference beams is typically a third order effect; an example of one effect is an effect first order in the size of the initial value of the cyclic error and second order in the
15 change in orientation of beam steering element 158 about a preselected orientation.

Another feature of the first embodiment is a simple alignment procedure. The existence of a relative angle detector in detector 188 simplifies alignment of the apparatus as follows. By blocking the measurement beam between quarter wave
phase retardation plate 168 and measurement object mirror 170, electrical error signal
20 188 becomes indicative of the alignment of entrance beam 110, assuming that all other alignments are correct. Viewing this signal through additional display means (not shown) provides information on how best to align entrance beam 110.

As a further improvement upon the alignment procedure, the first and second beam splitting assemblies may be provided with additional servo control and
25 additional orientation/translation transducers (not shown) to automatically align the apparatus of the first embodiment by adjustment of the angular orientation and/or position of the first and second beam splitting assemblies. As an alternative to the further improvement upon the alignment procedure, reference mirror 178 may be provided with additional servo control and additional orientation transducers (not
30 shown) to automatically align the apparatus of the first embodiment by adjustment of the angular orientation of reference mirror 178.

All surfaces of elements of the first embodiment through which beams are transmitted are antireflection coated to maintain a high transmission efficiency for the interferometer.

It will be evident to those skilled in the art that depending upon the end use application, the first embodiment may be implemented to compensate for changes in orientation of the measurement object mirror about only one axis of rotation instead of two orthogonal axes of rotation without departing either from the scope or spirit of the present invention.

FIGS. 2a-2f depict, in schematic form, the second embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The second embodiment is from the first class of embodiments and variants thereof operating in the first mode of operation for changes in orientation of the object about two orthogonal axes. The second embodiment uses beam polarization encoding for beam identification and control of beam paths in certain steps relating to a steering element where the first embodiment uses spatial separation of beams for keeping track of the identity of reference and measurement beams in other certain steps relating to the steering element.

The second embodiment comprises light beam 210, a light beam steering assembly comprising beam steering element 270 and orientation/translation transducer 271, a first, second, third, and fourth beam splitting assemblies BAS1, BAS2, BAS3, and BAS4, respectively, retroreflector 293, measurement object mirror 284 comprised of a single reflecting surface, and reference beam mirror 265 comprised of a single reflecting surface. Prisms 250, 254, 258, 262, 267, 269, 272, and 296, half-wave phase retardation plates 260 and 294, and quarter wave phase retardation plate 268 comprise the first beam splitting assembly BAS1 wherein interface surfaces 252, 256, 266, and 298 are polarizing beam splitting interfaces, and surfaces 264 and 274 are reflecting surfaces (*cf.* FIG. 2b). Prisms 276 and 277 comprise the second beam splitting assembly BAS2 wherein interface 280 is a polarizing beam splitting interface and surface 278 is a reflecting surface (*cf.* FIG. 2e). Prisms 286 and 292 comprise the

third beam splitting assembly **BAS3** wherein interface **288** is a polarizing beam splitting interface (*cf.* FIG. **2d**). Prisms **251** and **255** comprise the fourth beam splitting assembly **BAS4** wherein interface **253** is a nonpolarizing beam splitting interface (*cf.* FIG. **2a**).

5 The second embodiment is adapted for use as a heterodyne interferometer system. The descriptions of light beam **210** and the source of beam **210** are the same as the corresponding descriptions given for light beam **110** and the source of beam **110** of the first embodiment.

10 Beam **210** as illustrated in FIG. **2b**, impinges on **BAS1** with a portion of beam **210** reflected by interface **252** as beam **211** and beam **211** is reflected by interface **256** as measurement beam **213**. Beam **213** is polarized orthogonal to the plane of FIG. **2b**. A second portion of beam **210** is transmitted by interface **252** as reference beam **212** polarized in the plane of FIG. **2b**.

15 Beam **213** is transmitted by quarter wave phase retardation plate **268** as a circularly polarized beam, reflected by beam steering element **270** as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate **268** as beam **215** linearly polarized in the plane of FIG. **2a** (*cf.* FIG. **2b**). Beam steering element **270** is comprised of a single reflecting surface. Beam **215** is transmitted by polarizing interface **256** as beam **217** of **BAS1**. Beam **217** is reflected by reflecting interface **274** and exits **BAS1** as beam **219**.

20 Beam **219** enters **BAS2** (*cf.* FIG. **2e**) and is reflected by reflecting surface **278** as beam **221** and beam **221** is reflected by polarizing beam splitting interface **280** as beam **223**.

25 Beam **223**, being polarized orthogonal to the plane of FIG. **2e**, is transmitted by quarter wave phase retardation plate **282** as a circularly polarized beam, reflected by measurement object mirror **284** as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate **282** as beam **225** linearly polarized in the plane of FIG. **2e** and orthogonal to the plane of FIG. **2a**.

30 Beam **225** enters **BAS2** and is transmitted by polarizing beam splitting interface **280** as beam **227**. Beam **227** exits **BAS2**, enters **BAS3** (*cf.* FIG. **2d**), and is

reflected by the polarizing beam splitting interface 288 as beam 229. Beam 229, being polarized orthogonal to the plane of FIG. 2d, is transmitted by quarter wave phase retardation plate 290 as a circularly polarized beam, reflected by steering mirror 270 as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate 290 as beam 231 linearly polarized in the plane of FIG. 2d. Beam 231 is transmitted by polarizing beam splitting interface 288 as beam 233.

Beam 233 enters retroreflector 293 (*cf.* FIG. 2d) and is retroreflected as beam 235 (*cf.* FIG. 2a). Beams 233 and 235 are shown in FIG. 2f as beams entering and exiting, respectively, retroreflector 293.

Reference beam 212, polarized in the plane of FIG. 2b, is transmitted by half-wave phase retardation plate 260 as beam 214, half-wave phase retardation plate 260 being orientated so the beam 214 is polarized orthogonal to the plane of FIG. 2b.

Beam 214 is reflected by reflecting surface 264 as beam 216 and beam 216 is reflected by polarizing beam splitting interface 266 as beam 218. Beam 218, being polarized orthogonal to the plane of FIG. 2b, is transmitted by quarter wave phase retardation plate 268 as a circularly polarized beam, reflected by steering mirror 270 as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate 268 as beam 220 linearly polarized in the plane of FIG. 2b. Beam 220 is transmitted by polarizing beam splitting interface 266 as beam 222.

Beam 222 enters retroreflector 293 (*cf.* FIG. 2a) and is retroreflected as beam 224 (*cf.* FIG. 2d). In FIG. 2f, beams 222 and 224 are shown as beams entering and exiting, respectively, retroreflector 293. Beam 224 enters BAS3 and is transmitted by polarizing beam splitting interface 288 as beam 226 (*cf.* FIG. 2d). Beam 226, being polarized in the plane of FIG. 2d, is transmitted by quarter wave phase retardation plate 290 as a circularly polarized beam, reflected by beam steering mirror 270 as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate 290 as beam 228 linearly polarized orthogonal to the plane of FIG. 2d. Beam 228 is reflected by polarizing beam splitting interface 288 as beam 230.

Beam 230 enters **BAS2** (*cf.* FIG. 2d) and is transmitted by polarizing beam splitting interface 280 as beam 232. The projections of beam 223 and 232 are superimposed in the plane of FIG. 2e. Beam 232, being polarized orthogonal to the plane of FIG. 2d, is transmitted by quarter wave phase retardation plate 282 as a circularly polarized beam, reflected by reference mirror 265 as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate 282 as beam 234 linearly polarized in the plane of FIG. 2d.

Beam 234 enters **BAS2**, reflected by polarizing beam splitting interface 280, and subsequently reflected by reflecting surface 278 as beam 238 (*cf.* FIG. 2a).

Beam 235 enters **BAS1** and, being polarized in the plane of FIG. 2b, is transmitted by half-wave phase retardation plate 294 as beam 237. Half-wave phase retardation plate 294 is orientated so that beam 237 is polarized orthogonal to the plane of FIG. 2b. Beam 237 is reflected by polarizing beam splitting interface 298 as one component of output beam 240. Beam 238 is transmitted by polarizing beam splitter interface 298 as a second component of output beam 240.

As shown in FIG. 2a, beam 240 enters **BAS4** and a first portion of output beam 240 is transmitted by nonpolarizing beam splitting interface 253 as the first output beam 241. First output beam 241 impinges on detector 257 to produce an electrical signal 244 related to any difference in the directions of propagation of measurement and reference beam components in first output beam 241 in two orthogonal planes.

A second portion of beam 240 is reflected by nonpolarizing beam splitting interface 253 as the second output beam 242. Beam 242 is transmitted by a polarizer 259 orientated to produce a mixed optical beam 243. Beam 243 impinges on detector 261 to generate electrical signal 245 related to the difference in phase of the measurement and reference beam components of mixed beam 243. Electrical signal 245 is transmitted to electronic processor and computer 263 for subsequent processing for information about the difference in phase of the measurement and reference beam components of mixed beam 243.

Electrical signal 244 is transmitted to orientation/translation transducer 271. Information contained in signal 244 is used as the error signal in a servo system to

alter the orientation of beam steering mirror **270** by orientation/translation transducer **271** so as to maintain the direction of propagation of measurement beam **237** substantially constant independent of changes of orientation of object mirror **284**.

The remaining description of the second embodiment is the same as
5 corresponding portions of the description of the first embodiment except with regard to generation of cyclic errors. The additional phase retardation plates in the second embodiment in relation to the first embodiment increase the number of possibilities for the generation of cyclic errors in the relative phase measured between the reference and measurement beam components of the output beam. However, the
10 cyclic errors generated in the second embodiment as a result of the additional phase retardation plates are generally substantially less than corresponding cyclic errors present in prior art plane mirror interferometers, a consequence principally because there is only one pass to the measurement object mirror **284** by the measurement beam in the second embodiment in comparison to the double pass to a measurement object
15 mirror by the measurement beam in many prior art plane mirror interferometers.

FIGS. **3a-3f** depict, in schematic form, the third embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.
20 The third embodiment is from the first class of embodiments and variants thereof operating in the first mode of operation for changes in orientation of the object about a first axis and in the second mode of operation for changes in orientation of the object about a second axis orthogonal to the first axis and/or a lateral displacement of the object, the lateral displacement being orthogonal to both the second axis and the linear
25 displacement.

The interferometer system of the first and third embodiments are generically similar except with respect to the reflecting properties of the object: the reflecting properties of the object for the first embodiment are those of a plane mirror and the reflecting properties of the object for the third embodiment are those of a roof prism.

30 The third embodiment comprises light beam **310**, a light beam steering assembly comprising beam steering element **362** and orientation/translation transducer

363, a first, second, third, and fourth beam splitting assemblies **BAS1**, **BAS2**, **BAS3**, and **BAS4**, respectively, retroreflector 368, measurement object roof prism 366, and reference beam prism 364. Rhomboidal prism 350 and prism 354 comprise the first beam splitting assembly **BAS1** wherein interface 352 is a polarizing beam splitting
5 interface and surface 356 is a reflecting surface (*cf.* FIG. 3b). Prisms 358 and 370 comprise the second beam splitting assembly **BAS2** wherein interface 360 is a reflecting interface (*cf.* FIG. 3a). Prisms 372 and 376 comprise the third beam splitting assembly **BAS3** wherein interface 374 is a reflecting interface (*cf.* FIG. 3d). Rhomboidal prisms 378 and 384 comprise the fourth beam splitting assembly **BAS4**
10 wherein interface 380 is a nonpolarizing beam splitting interface and surfaces 382 and 386 are reflecting surfaces (*cf.* FIG. 3e).

The third embodiment is adapted for use as a heterodyne interferometer system. The descriptions of light beam 310 and the source of beam 310 are the same as the corresponding descriptions given for the light beam 110 and the source of beam
15 110 of the first embodiment.

Beam 310, as illustrated in FIG. 3a, impinges **BAS1** with a portion of beam 310 reflected by interface 352 and reflected by surface 356 as measurement beam 311. Beam 311 is polarized orthogonal to the plane of FIG. 3a. A second portion of beam 310 is transmitted by interface 352 as reference beam 312 polarized in the plane of
20 FIG. 3a.

Beam 311, as illustrated in FIG. 3b, impinges on **BAS2** and is reflected by interface 360 as measurement beam 313. Beam 313 is polarized in the plane of FIG. 3b.

Beam 313 enters beam steering element 362 (*cf.* FIG. 3b) and exits beam
25 steering element 362 as beam 315 (*cf.* FIG. 3d) displaced laterally from beam 313 and propagating in a direction nominally opposite to the direction of propagation of beam 313. The projections of beam 313 and of beam 315 on the plane of FIG. 3b are superimposed. In beam steering element 362, beam 313 is reflected in a sequence, *e.g.*, by total internal reflection, by each of the surfaces 362A, 362B, and 362C (*cf.*
30 FIG. 3c which presents a side view of the interferometer depicted in FIGS. 3b and 3d). Beam steering element 362 and orientation/translation transducer 363 comprise

the beam steering assembly that redirects measurement beam 313. Orientation/translation transducer 363 preferably alters the orientation of beam steering element 362 about a nodal point of retroreflector 368 for a change in orientation in the plane of FIG. 3c, changes in orientation of beam steering element 362 about a nodal point of retroreflector 368 producing substantially reduced lateral shear effects experienced by the reference beam, and/or the location beam steering element 362 in the nominal direction of propagation of beam 313. The orientation of beam steering element 362 is controlled by electronic signal 340. The location of beam steering element 362 is controlled by electronic processor and computer 394 through electronic signal 344.

Beam 315 is transmitted by dove prism 364 as beam 317 (*cf.* FIG. 3d). Beam 317 is reflected by measurement object roof prism 366 as beam 319 linearly polarized in the plane of FIG. 3d. The projections of beam 317 and beam 319 on the plane of FIG. 3c are superimposed. Measurement object roof prism 366 may be of either solid or hollow construction. Beam 319 is transmitted by dove prism 364 as beam 321.

Beam 321 enters beam steering element 362 (*cf.* FIG. 3d) and exits beam steering element 362 as beam 323 (*cf.* FIG. 3b) propagating in a direction nominally opposite to the direction of propagation of beam 321. Beam 323 enters retroreflector 368 (*cf.* FIG. 3b) and is retroreflected as beam 325. An end view of retroreflector 368 and dove prism 364 is depicted in FIG. 3f. Beam 325 enters BAS2 and is reflected by interface 360 as beam 327.

Reference beam 312 enters BAS3 and is reflected by interface 374 as beam 314 (*cf.* FIG. 3d). Beam 314 enters beam steering element 362 (*cf.* FIG. 3d) and exits beam steering element 362 as beam 316 (*cf.* FIGS. 3b and 3d) propagating in a direction nominally opposite to the direction of propagation of beam 314. The projections of beam 316 and of beam 314 on the plane of FIG. 3b are superimposed. The projections of beam 316 and of beam 313 on the plane of FIG. 3c are superimposed. Beam 316 enters retroreflector 368 and is retroreflected as beam 318 (*cf.* FIG. 3b). Beam 318 enters beam steering element 362 (*cf.* FIG. 3b) and exits beam steering element 362 as beam 320 (*cf.* FIG. 3d) propagating in a direction nominally opposite to the direction of propagation of beam 318.

Measurement beams **323** and **325** and reference beams **316** and **318** lie in the same top beam plane (*cf.* FIG. **3b**). Measurement beams **315** and **321** and reference beams **314** and **320** lie in the same bottom beam plane (*cf.* FIG. **3d**).

Beam **320** enters dove prism **364** and is reflected by surfaces **364A** and **364B** as beam **324**. Dove prism **364** functions as a roof prism in redirecting beam **320** as beam **324** in the same manner as measurement object roof prism **366** functions in redirecting beam **317** as beam **319**. Beam **324**, orthogonally polarized to the plane of FIG. **3d**, enters **BAS3** and is reflected by interface **374** as beam **326**.

Beam **327** enters **BAS4** (*cf.* FIG. **3e**) and a first portion of beam **327** is reflected by nonpolarizing beam splitting interface **380** as one component of a first output beam **330**. Beam **326** enters **BAS4** and is reflected by surface **386** as beam **328**. A first portion of beam **328** is transmitted by beam splitting interface **380** as a second component of the first output beam **330**. First output beam **330** is reflected by surface **382** as output beam **332**. Output beam **332** impinges on detector **390** to produce an electrical signal **340** with one component related to any lateral shear of the measurement beam component of output beam **332** in the plane of FIG. **3d**, *i.e.* orthogonal to the plane of FIG. **3e**, and a second component related to any difference in the directions of propagation of measurement and reference beam components in output beam **332** orthogonal to the plane of FIG. **3d**, *i.e.* in the plane of FIG. **3e**.

A second portion of beam **327** is transmitted by nonpolarizing beam splitting interface **380** as one component of a second output beam **334**. A second portion of beam **328** is reflected by nonpolarizing beam splitting interface **380** as a second component of the second output beam **334**. Beam **334** is transmitted by a polarizer **388** that is orientated to produce a mixed optical beam **336**. Beam **336** impinges on detector **392** to generate electrical signal **342** related to the difference in phase of the measurement and reference beam components of mixed beam **336**. Electrical signal **342** is transmitted to electronic processor and computer **394** for subsequent processing for information about the difference in phase of the measurement and reference beam components of mixed beam **336**.

Electrical signal 340 is transmitted to orientation/translation transducer 363. Information contained in signal 340 is used as the error signals in a servo system to alter the orientation of beam steering element 362 by orientation/translation transducer 363 so as to maintain both the lateral shear of beam 327 in the plane of FIG. 3b and the direction of propagation of measurement beam 327 in a plane orthogonal to the plane of FIG. 3b substantially constant independent of changes of orientation of measurement object roof prism 366. Under the condition that the physical path length of the measurement beam from the first redirection by the beam steering element 362 to measurement object roof prism 366 is equal to the physical path length of the measurement beam from measurement object roof prism 366 to the second redirection by beam steering element 362, there will be no lateral shear of beam 327 orthogonal to the plane of FIG. 3b when changes in orientation of measurement object roof prism 366 are compensated by changes in orientation of beam steering mirror 362. This condition with respect to physical path lengths will be referenced as the third embodiment condition.

Compliance with the third embodiment condition eliminates the lateral shear of measurement beam 323 at beam steering element 362 when changes in orientation of measurement object roof prism 366 are compensated by changes in orientation of beam steering element 362. However, there will be introduced lateral shear of reference beam 316 when changes in orientation of measurement object roof prism 366 are compensated by changes in orientation of beam steering element 362. Although a lateral shear will be introduced in reference beam 316, the magnitude of the lateral shear is significantly reduced in relation to the lateral shear introduced in measurement beam components of prior art plane mirror interferometers due to changes in orientation of the object mirror, the reduction factor being proportional to the ratio of the physical length of the reference leg to the physical length of the measurement leg of an interferometer.

The remaining description of the third embodiment is the same as corresponding portions of the description given for the first embodiment.

A first variant of the third embodiment of the present invention is described for measuring the linear displacement of an object substantially independent of the

orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The first variant of the third embodiment is from the first class of embodiments and variants thereof operating in the second mode of operation for changes in orientation of the object about two orthogonal axes and/or for a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.

The interferometer system and at least one beam steering assembly of the first variant of the third embodiment comprise the same elements as the interferometer system and at least one beam steering assembly of the third embodiment except for the object element, the detector of a certain optical beam, a signal produced by the detector of the certain optical beam, and a respective servo system.

The measurement object element of the third embodiment, roof prism **366**, is replaced by a measurement object retroreflector **366A** (not shown in a figure) in the first variant of the third embodiment. As a consequence, the relative directions of propagation of the reference and measurement beam components of output beam **332A**, the output beam of the first variant of the third embodiment corresponding to output beam **332** of the third embodiment, is substantially independent of changes in orientation of the beam steering element **362** of the first variant of the third embodiment. However a lateral translation of measurement object retroreflector **366A** in a plane orthogonal to the direction of the linear displacement and/or a change in orientation of measurement object retroreflector **366A** will generate a lateral displacement of measurement beam component of output beam **332A**.

Detector **390A** of the first variant of the third embodiment, corresponding to detector **390** of the third embodiment, detects the lateral displacement or shear of the measurement beam component of output beam **332A** in two orthogonal directions and generates electrical signal **340A**, the electrical signal corresponding to electrical signal **340** of the third embodiment.

Electrical signal **340A** is transmitted to orientation/translation transducer **363** of the first variant of the third embodiment. Information contained in signal **340A** is used as the error signal in a servo system to alter the orientation of beam steering element **362** by orientation/translation transducer **363** so as to maintain the lateral

location of measurement beam component of output beam **332A** substantially constant independent of a lateral translation of measurement object retroreflector **366A** in a plane orthogonal to the direction of the linear displacement and/or substantially independent of changes in orientation of measurement object retroreflector **366A**
5 about two orthogonal axes.

The remaining description of the first variant of the third embodiment is the same as corresponding portions of the description given for the third embodiment.

FIGS. **4a-4f** depict, in schematic form, the fourth embodiment of the present invention for measuring a linear displacement of an object substantially independent
10 of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The fourth embodiment is from the first class of embodiments and variants thereof operating in the first mode of operation for changes in orientation of the object about a first axis and in the second mode of operation for changes in orientation of the object
15 about a second axis orthogonal to the first axis and/or a lateral displacement of the object, the lateral displacement being orthogonal to both the second axis and the linear displacement.

The interferometer system of the third and fourth embodiments are generically similar except with respect to the number of passes the measurement beam makes to
20 the object and the associated number of passes made by the reference beam to a reference mirror: the measurement (reference) beam of the fourth embodiment traverses certain sections of the measurement (reference) path in two opposite directions of propagation where in the third embodiment, the corresponding measurement (reference) beam transits the certain sections in only one direction of
25 propagation. Efficient separation of an output measurement (reference) beam component from an input measurement (reference) beam component in the multiple pass configuration of the fourth embodiment is effected by use of polarization encoding and polarizing beam splitters.

Many elements of the third and fourth embodiments perform like functions
30 and these elements are indicated by a numeric numbering scheme wherein the numeric number of elements performing like functions for the fourth embodiment are equal to

the numeric number of corresponding elements of the third embodiment incremented by 100. The certain sections of the reference and measurement beam paths are indicated by the numeric numbering scheme wherein the numeric number of the certain section of the reference or measurement path of the fourth embodiment having the same description as a corresponding path section of the third embodiment is equal to the numeric number of corresponding path section of the third embodiment incremented by 100.

For the certain sections of the measurement (reference) beam path for the fourth embodiment, there is a measurement (reference) beam traversing the certain sections in a reverse direction of propagation, the nonreverse or forward direction of propagation being associated with a first pass to the measurement object roof prism 466 (reference beam dove prism 464) and the reverse direction of propagation being associated with a second pass to the measurement object roof prism 466 (reference beam dove prism 464). The description of the additional measurement (reference) beam traversing the certain sections in a reverse direction are otherwise the same as the corresponding portions of the description given associated measurement (reference) beam traversing in a nonreverse direction of propagation for the third embodiment, the alphanumeric number of a measurement (reference) beam traversing in a reverse direction being equal to the numeric number of the associated measurement (reference) beam traversing in a nonreverse direction augmented with the suffix R.

The fourth embodiment comprises light beam 410, a light beam steering assembly comprising beam steering element 462 and orientation/translation transducer 463, a first, second, third, and fourth beam splitting assemblies, retroreflector 468, measurement object element 466 comprising a roof prism, reference beam element 464 comprising a dove prism, mirror 461, and quarter wave phase retardation plate 457. Rhomboidal prism 450 and prism 454 comprise the first beam splitting assembly BAS1 wherein interface 452 is a polarizing beam splitting interface and surface 456 is a reflecting surface (*cf.* FIG. 4a). Prisms 458 and 470 (*cf.* FIG. 4b) comprise the second beam splitting assembly BAS2 wherein interface 460 is a reflecting interface. Prisms 472 and 476 (*cf.* FIG. 4d) comprise the third beam splitting assembly BAS3

wherein interface **474** is a reflecting interface. Prisms **451**, **453**, and **465** and rhomboidal prism **467** comprise the fourth beam splitting assembly **BAS4** (*cf.* FIG. **4e**) wherein interface **455** is a nonpolarizing beam splitting interface, interface **469** is a polarizing beam splitting interface, and surface **471** is a reflecting surface.

5 The descriptions of the generation of measurement beam **427** and reference beam **426** is the same as the descriptions given for corresponding descriptions of the generation of measurement beam **327** and reference beam **326** of the third embodiment. As shown in FIG. **4e**, beam **427** enters the fourth beam splitting assembly and a first portion of beam **427** is transmitted by nonpolarizing beam
10 splitting interface **455** as measurement beam component **401** polarized orthogonal to the plane of FIG. **4e**. A second portion of beam **427** is reflected by nonpolarizing beam splitting interface **455** as measurement beam component **403** polarized orthogonal to the plane of FIG. **4e**. Beam **426** enters **BAS4** and a first portion of beam **426** is transmitted by nonpolarizing beam splitting interface **455** as reference beam
15 component **400** polarized in the plane of FIG. **4e**. A second portion of beam **426** is reflected by nonpolarizing beam splitting interface **455** as measurement beam component **402** polarized in the plane of FIG. **4e**.

Beam **401** is reflected by polarizing beam splitting interface **469** as one component of a first output beam **406**. Beam **402** is reflected by reflecting surface
20 **404** and beam **404** is transmitted by polarizing beam splitting interface **469** as a second component of the first output beam **406**. First output beam **406** impinges on detector **496** to produce an electrical signal **441** with a first component related to any lateral shear of the measurement beam component of output beam **406** produced by a displacement of measurement object roof prism **466** in the plane of FIG. **4d** and
25 nominally orthogonal to the direction of propagation of beam **417** and/or a change in orientation of measurement object roof prism **466** about an axis perpendicular to the plane of FIG. **4d** and with a second component related to any difference in the directions of propagation of measurement and reference beam components in output beam **406** produced by a change in orientation of the measurement object roof prism
30 **466** about an axis in the plane of FIG. **4d** and nominally orthogonal to the direction of propagation of beam **417**.

In FIG. 4e, beam 403, polarized orthogonal to the plane of FIG. 4d, is transmitted by quarter wave phase retardation plate 457 as a circularly polarized beam, reflected by mirror 461 as a beam with opposite-handed circular polarization, and subsequently transmitted by phase retardation plate 457 as beam 405 linearly polarized in the plane of FIG. 4e. Beam 405 enters BAS4 and a portion of beam 405 is reflected by nonpolarizing beam splitting interface 455 as beam 427R. Beam 427R has polarization orthogonal to the polarization of beam 427.

Beam 402, polarized in the plane of FIG. 4e, is transmitted by quarter wave phase retardation plate 457 as a circularly polarized beam, reflected by mirror 461 as a beam with opposite-handed circular polarization, and subsequently transmitted by phase retardation plate 457 as beam 408 polarized orthogonal to the plane of FIG. 4e. Beam 408 enters BAS4 and a portion of beam 408 is reflected by nonpolarizing beam splitting interface 455 as beam 426R. Beam 426R has polarization orthogonal to the polarization of beam 426.

Beam 427R is substantially coextensive with beam 427 and beam 427R has a direction of propagation substantially opposite to the direction of propagation of 427. As a consequence, beam 427R substantially retraces the pass through portions of the interferometer, the pass leading to the generation of beam 427, to generate beam 411R. The retrace through portions of the interferometer includes in particular a pass to the measurement object roof prism 466. Beam 411R is substantially coextensive with beam 411 and beam 411R has a direction of propagation substantially opposite to the direction of propagation of beam 411.

Beam 426R is substantially coextensive with beam 426 and beam 426R has a direction of propagation substantially opposite to the direction of propagation of 426. As a consequence, beam 426R substantially retraces the pass through portions of the interferometer, the pass leading to the generation of beam 426, to generate beam 412R. The retrace through portions of the interferometer includes a pass to the reference dove prism 464. Beam 412R is substantially coextensive with beam 412 and beam 412R has a direction of propagation substantially opposite to the direction of propagation of 412.

As shown in FIG. 4a, beam 411R being polarized in the plane of FIG. 4a enters the first beam splitting assembly to be reflected by reflecting surface 456 and transmitted by polarizing beam splitting interface 452 as a first component of a second output beam 446. Beam 412R being polarized orthogonal to the plane of FIG. 4a enters the first beam splitting assembly to be reflected by polarizing beam splitting interface 452 as a second component of the second output beam 446.

Beam 446 is transmitted by a polarizer 497 orientated to produce a mixed optical beam 448. Beam 448 impinges on detector 498 to generate electrical signal 443 related to the difference in phase of the measurement and reference beam components of mixed beam 448. Electrical signal 443 is transmitted to electronic processor and computer 499 for subsequent processing for information about the difference in phase of the measurement and reference beam components of mixed beam 448.

The significant feature of the fourth embodiment is the generation of a double pass to the measurement object roof prism 466 over the same optical path normally traversed in a single pass with prior art interferometry.

The remaining description of the fourth embodiment is the same as corresponding portions of the description given for the third embodiment.

A first variant of the fourth embodiment is described wherein the generation of the electrical signals used in the servo system used to control the beam steering element 462 differs from that used in the fourth embodiment. In the first variant of the fourth embodiment, detector 496 generates only the first component of electrical signal 441 related to any lateral shear of the measurement beam component of output beam 406 produced by a displacement of measurement object roof prism 466 in the plane of FIG. 4d and nominally orthogonal to the direction of propagation of beam 417 and/or a change in orientation of measurement object roof prism 466 about an axis perpendicular to the plane of FIG. 4d and a third detector 498A (not shown in a figure) is added to generate an electrical signal 441A to serve the function of the second component of signal 441 of the fourth embodiment related to any difference in the directions of propagation of measurement and reference beam components in output beam 406 produced by a change in orientation of the measurement object roof

prism 466 about an axis in the plane of FIG. 4d and nominally orthogonal to the direction of propagation of beam 417.

The third detector 498A detects a first portion of the second output beam 446 reflected by a nonpolarizing beam splitter inserted in the path of beam 446, a second
5 portion of second output beam 446 being transmitted by inserted beam splitter, transmitted by polarizer 497 orientated to produce a mixed beam, and detected by detector 499.

The advantage of the first variant of the fourth embodiment is that the first portion of the second output beam 446 has a difference in the directions of
10 propagation of its measurement and reference beam components that is twice the difference in the directions of propagation of the measurement and reference beam components in output beam 406 produced by a change in orientation of the object roof prism 466 about an axis in the plane of FIG. 4d and nominally orthogonal to the direction of propagation of beam 417. In addition, the measurement and reference
15 beam components of the first portion of the second output beam 446 have substantially no lateral shear produced by a displacement of measurement object roof prism 466 in the plane of FIG. 4d and nominally orthogonal to the direction of propagation of beam 417 and/or a change in orientation of measurement object roof prism 466 about an axis perpendicular to the plane of FIG. 4d.

20 A second variant of the fourth embodiment of the present invention is described for measuring the linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The second variant of the fourth embodiment is from the first class of embodiments
25 and variants thereof operating in the second mode of operation for changes in orientation of the object about two orthogonal axes and/or for a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.

The interferometer system and at least one beam steering assembly of the second variant of the fourth embodiment comprise the same elements as the
30 interferometer system and at least one beam steering assembly of the fourth embodiment except for the object element, the detector of a certain optical beam, a

signal produced by the detector of the certain optical beam, and a respective servo systems.

The measurement object element of the fourth embodiment, measurement object roof prism **466**, is replaced by an measurement object retroreflector **466B** (not shown in a figure) in the second variant of the fourth embodiment. As a consequence, the relative directions of propagation of the reference and measurement beam components of output beam **401B**, the output beam of the second variant of the fourth embodiment corresponding to output beam **401** of the fourth embodiment, are substantially independent of changes in orientation of the beam steering element **462** of the second variant of the fourth embodiment. However a lateral translation of measurement object retroreflector **466B** in a plane orthogonal to the direction of the linear displacement will generate a lateral displacement of measurement beam component of output beam **401B**.

Detector **496B** of the second variant of the fourth embodiment, corresponding to detector **496** of the fourth embodiment, detects the lateral displacement or shear of the measurement beam component of output beam **401B** in two orthogonal directions and generates electrical signal **441B**, the electrical signal corresponding to electrical signal **441** of the fourth embodiment. Electrical signal **441B** is comprised of two components, one component related to any lateral shear of the measurement beam component of output beam **406** produced by a displacement of measurement object retroreflector **466B** in the plane of FIG. **4d** and nominally orthogonal to the direction of propagation of beam **417** and/or a change in orientation of measurement object retroreflector **466B** about an axis perpendicular to the plane of FIG. **4d** and a second component related to any lateral shear of the measurement beam component of output beam **406** produced by a displacement of measurement object retroreflector **466B** perpendicular to the plane of FIG. **4d** and nominally orthogonal to the direction of propagation of beam **417** and/or a change in orientation of measurement object retroreflector **466B** about an axis parallel to the plane of FIG. **4d**.

Electrical signal **441B** is transmitted to orientation/translation transducer **463** of the second variant of the fourth embodiment. Information contained in signal **441B** is used as error signals in a servo system to alter the orientation of beam steering

element **462** by orientation/translation transducer **463** so as to maintain the lateral location of measurement beam component of output beam **401B** substantially constant independent of a lateral translation of measurement object retroreflector **466B** in a plane orthogonal to the direction of the linear displacement and/or substantially independent of changes in orientation of measurement object retroreflector **466B** about two orthogonal axes.

The remaining description of the second variant of the fourth embodiment is the same as corresponding portions of the description given for the fourth embodiment.

FIG. 5 depicts, in schematic form, the fifth embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The first embodiment is from the first class of embodiments and variants thereof of the present invention operating in the first mode of operation for changes in orientation of the object about two orthogonal axes.

The embodiment is comprised principally of a beam division and recombination optic **530**, beam steering mirror **540** attached to a orientation/translation transducer **542**, a relative beam angle sensor assembly **550**, a reference mirror **536**, two retroreflectors **531** and **533**, a photodetector **534**, two quarter wave retardation plates **538** and **539**, and a measurement object mirror **590**. Retroreflectors **531** and **533** are truncated so that a beam passing centrally through either one is not retroreflected.

The fifth embodiment is adapted for use with a heterodyne interferometer system. The description of the source of beam **510** and of beam **510** is the same as the description of the source of beam **110** and beam **110** given for the first embodiment. Entrance beam **510** impinges upon a polarizing beam splitter surface **570** of beam division and recombination optic **530**. Polarizing beam splitter surface **570** separates the orthogonally polarized components of entrance beam **510** into a measurement beam **512** and a reference beam **520**. Measurement beam **512** initially has a linear polarization perpendicular to the plane of the FIG. 5. Reference beam **520** initially

has a linear polarization in the plane of FIG. 5. Polarizing beam splitter surface **570** reflects light polarized orthogonal to the plane of FIG. 5 and transmits light polarized in the plane of FIG. 5.

Measurement beam **512** initially traveling from left to right in FIG. 5 after a first reflection from polarizing beam splitter surface **570** reverses direction after reflection from retroreflector **531**. Measurement beam **512**, now traveling from right to left, reflects a second time from polarizing beam splitter surface **570** and subsequently travels upwards. Measurement beam **512** reflects a first time from adjustable mirror **540** and passes centrally a first time through retroreflector **533** and then a first time through quarter wave phase retardation plate **539**. Quarter wave retardation plate **539** converts measurement beam **512** with an initial linear polarization orthogonal to the plane of FIG. 5, now denoted **514** in the figure, to circular. Measurement beam **514** then reverses direction after reflecting from measurement object mirror **590** and passes a second time through quarter wave phase retardation plate **539**, resulting in a net change to linear polarization in the plane of FIG. 5. Measurement beam **514** passes centrally a second time through retroreflector **533**, then reflects a second time from adjustable mirror **540** and travels downwards. Measurement beam **514** passes a first time through polarization beam splitter surface **570** and reflects once from a reflective back surface **571** of beam division and recombination optic **530**. Measurement beam **514** then passes a second time through polarization beam splitter surface **570** and continues traveling from left to right as a component of exit beam **516** polarized in the plane of FIG. 5.

Reference beam **520** initially traveling downwards after passing a first time through polarizing beam splitter surface **570** reflects once from reflective back surface **571** of beam division and recombination optic **530**. Reference beam **520**, now traveling from left to right, passes a second time through polarizing beam splitter surface **570**, passes centrally a first time through retroreflector **531** and then a first time through quarter wave phase retardation plate **538**. Quarter wave phase retardation plate **538** converts the polarization of reference beam **520**, polarized in the plane of FIG. 5, to circularly polarized beam now denoted **522**. Reference beam **522** then reverses direction after reflecting from reference mirror **536** and passes a second

time through quarter wave retardation plate **538**, resulting in a net change to linear polarization orthogonal to the plane of FIG. **5**. Reference beam **522**, now traveling from right to left, passes centrally a second time through retroreflector **531**, then reflects a first time from polarizing beam splitter surface **570** and travels upwards.

5 Reference beam **522** reflects a first time from adjustable mirror **540** and travels from left to right, then reverses direction after reflection from retroreflector **533**. Reference beam **522** then reflects a second time from adjustable mirror **540**, travels downward, reflects a second time from polarizing beam splitter surface **570** and continues traveling from left to right as a component of exit beam **516** polarized orthogonal to
10 the plane of FIG. **5**.

Exit beam **516** comprises orthogonally polarized components corresponding to measurement beam **514** and reference beam **522**, respectively. Exit beam **516** passes through a pick-off mirror **559** and through a mixing polarizer **532** onto photodetector **534**. Mixing polarizer **532**, oriented at approximately 45° with respect to the plane of
15 the FIG. **5**, combines the orthogonally polarized components of exit beam **516** into mixed beam comprising a single linear polarization component. Photodetector **534** converts the mixed beam into an electronic interference signal, *e.g.*, by photoelectric detection, with signal **580** being transmitted to a signal processing system (not shown in FIG. **5**). Electronic interference signal **580** has the same frequency as the optical
20 frequency difference between the orthogonal components of entrance beam **510** shifted by any Doppler shifts introduced by a relative motion of measurement mirror **590** and reference mirror **536**. The phase of electronic interference signal **580** varies in accordance with the difference between the optical paths of measurement beam **514** and reference beam **522**. Thus electronic interference signal **580** provides a means of
25 monitoring displacement of measurement object mirror **590** with respect to reference mirror **536**, using optical interference phenomena.

At the same time, a sample beam **518** from exit beam **516** reflects from pick-off mirror **559** and travels into relative beam angle sensor assembly **550**. Within relative beam angle sensor assembly **550** there is a polarizer **558** which selects a
30 measurement beam component out of sample beam **518**. Beam **519** then travels through a lens **556** to detector **554** such as a quad cell detector, a high-speed CCD

camera, or a lateral effect photodiode or like means for determining the angular orientation of the measurement beam component of beam **519**. Information from detector **554** passes as an electrical error signal **591** to servo control **552**.

Servo control **552** sends an electronic drive signal **592** to
5 orientation/translation transducer **542**, which modifies the angular orientation of beam steering mirror **540** in response to changes in the detected angle of measurement beam **514** as it exits beam division and recombination optic **530**. Orientation/translation transducer **542** changes, in response to signal **592**, the orientation of beam steering mirror **540** preferably about a nodal point of retroreflector **533**, changes in orientation
10 of beam steering mirror **542** about a nodal point of reference retroreflector **533** producing substantially reduced lateral shear effects experienced by the reference beam. In normal operation, electronic servo control **552** maintains the angle of measurement beam **514** as it exits beam division and recombination optic **530** at some fixed value with respect to the angle of reference beam **522** as it exits beam division
15 and recombination optic **530**. Most often, it is desirable to minimize the difference in angle between the reference beam **522** and measurement beam **514** as they exit the beam division and recombination optic **530**, so as to maximize the strength of electronic interference signal **580** and minimize errors attributable to beam shear.

The combined action of relative beam angle sensor assembly **550**, beam
20 steering mirror **540**, and orientation/translation transducer **542** is to compensate for changes in orientation of measurement object mirror **590**. In the present embodiment, this compensation is typically achieved without disturbing the measured linear displacement of measurement object mirror **590**. Thus the optical path difference between measurement beam **514** and reference beam **522** is substantially independent
25 of changes in angle or position of beam steering mirror **540**.

There are several advantages of the fifth embodiment. Firstly, the paths for measurement beam **514** and reference beam **522** are highly symmetric, meaning that measurement beam **514** and reference beam **522** pass through the same amount of glass and air, exclusive only of the variable air path defined by the displacement of
30 measurement object mirror **590**. Measurement beam **514** and reference beam **522** also have substantially parallel paths, although they are spatially separated to minimize

contamination of the measurement and reference beams, one by the other, which generate cyclic errors in the measured phase of the electronic interference signal **580**. This symmetry leads to high thermal and mechanical stability.

Secondly, measurement beam **514** and reference beam **522** each reflect from the same flat surfaces an equal number of times, in particular, from reflective back surface **571** and polarizing beam splitter surface **570** of beam division and recombination optic **530**. This greatly reduces the requirements for parallelism of the two surfaces of beam division and recombination optic **530**.

Thirdly, the embodiment is comprised of easily fabricated optical components. The retroreflectors may be of the common type, either solid or hollow, with the apex ground down and polished flat. Beam division and recombination optic **530** may be an ordinary cube beam splitter with one edge ground flat and polished to become reflective back surface **571**. Pick-off mirror **559** may be a small piece of uncoated glass, in this case oriented to favor the component of exit beam **516** polarized orthogonal to the plane of FIG. **5**.

Fourthly, there are very few opportunities for ghost reflections, also known as spurious reflections, particularly with regard to spurious multiple passing to measurement object mirror **590**. This characteristic reduces the possibility of cyclic errors that are common to the majority of prior-art plane-mirror interferometers.

The remaining description of the fifth embodiment is the same as corresponding portions of the description given for the first embodiment except with respect to lateral shears introduced into the measurement and reference beams by a translation of the beam steering mirror **530** in a direction nominally orthogonal to the surface of the beam steering mirror **540**.

FIGS. **6a** and **6b** depict in schematic form a sixth embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The sixth embodiment is from the second class of embodiments and variants thereof of the present invention operating in the first mode about two orthogonal axes.

The description of light beam **610** shown in FIG. **6a** and of a source of light beam **610** is the same as the description of light beam **110** and of a source of light beam **110** given for the first embodiment. As shown in FIG. **6a**, beam **610** impinges on beam splitter **650**, *e.g.*, a polarizing type beam splitter. A portion of beam **610** is transmitted as measurement beam **611** polarized in the plane of FIG. **6a** and a second
5 portion of beam **610** is reflected as reference beam **612** orthogonally polarized to the plane of FIG. **6a**.

In FIG. **6a**, beam **611** is reflected by a first surface of beam steering mirror **652** as beam **613**. Beam steering mirror **652** and orientation transducers **653A** and **653B**
10 comprise a beam steering assembly that redirects measurement beam **613**. Beam **613** is reflected by mirror **654** and enters mirror assembly **656** as beam **615**. As shown in FIG. **6b**, mirror assembly **656** is comprised of three mirrors **656A**, **656B**, and **656C**. The plane of FIG. **6b** is orthogonal to the plane of FIG. **6a**. Beam **615** is reflected by each of the three mirrors **656A**, **656B**, and **656C** and exits mirror assembly **656** as
15 beam **621**. Mirror assembly **656** is an image inverter about an axis in the plane of FIG. **6a** and orthogonal to the direction of propagation of beam **615**. However, the primary function of mirror assembly **656** is to transform a change in the direction of propagation of beam **615** in the plane of FIG. **6b** to a change in the opposite direction of propagation of beam **621** in the plane of FIG. **6b** and to translate a change in
20 direction of beam **615** in the plane of FIG. **6a** to the same change in direction of propagation of beam **621** in the plane of FIG. **6a**.

Beam **621**, being polarized in the plane of FIG. **6a**, is transmitted by polarizing beam splitter **658** as beam **623**. Beam **623**, polarized in the plane of FIG. **6a**, is transmitted by a quarter wave phase retardation plate **660** as a circularly polarized
25 beam, reflected by measurement object mirror **662** as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate **660** as beam **627** linearly polarized perpendicular to the plane of FIG. **6a**. Beam **627** is reflected by beam splitter **658** as beam **629**.

Beam **629** is reflected by mirrors **664A** and **664B** to form beam **631**. Mirrors
30 **664A** and **664B** together produce a constant deviation between beams **629** and **631** in the plane of FIG. **6a**, the same as a penta prism. Beam **631** is reflected from a second

surface of beam steering mirror **652** as beam **633**. A change in the orientation of measurement object mirror **662** will effect a change in direction of propagation and lateral shear of beam **633** at beam steering mirror **652**. It is possible to compensate for both of the effects on beam **633** by an appropriate change in the orientation of beam steering mirror **652** in conjunction with image inverter **656**, beam splitter **658**, constant deviation mirror assembly comprising mirrors **664A** and **664B**, and measurement object mirror **662** located in the path of the measurement beam between the first and second reflections from beam steering mirror **652**.

Beam **633** is reflected by mirror **666** as beam **635**. Beam **635** is polarized perpendicular to the plane of FIG. **6a**.

Reference beam **612** is transmitted by a quarter wave phase retardation plate **668A** as a circularly polarized beam, reflected by retroreflector **670**, and transmitted by quarter wave phase retardation plate **668B** as beam **616** linearly polarized in the plane of FIG. **6a**.

A portion of beam **635** is reflected by polarizing beam splitter **672** as one component of output beam **636**. A portion of beam **616** is transmitted by polarizing beam splitter **672** as a second component of output beam **636**.

A portion of output beam **636** is reflected by nonpolarizing beam splitter **674** as beam **638**. Beam **638** impinges on detector **676** to produce an electrical signal **644** related to any difference in the directions of propagation of measurement and reference beam components in beam **638**.

A second portion of output beam **636** is transmitted by nonpolarizing beam splitter **674** as beam **640**. Beam **640** is transmitted by a polarizer **678** orientated to produce a mixed optical beam **642**. Beam **642** impinges on detector **680** to generate electrical signal **646** related to the difference in phase of the measurement and reference beam components of mixed beam **642**. Electrical signal **646** is transmitted to electronic processor and computer **682** for subsequent processing for the information about the difference in phase of the measurement and reference beam components of mixed beam **642**.

Electrical signal **644** is transmitted to orientation transducers **653A** and **653B**. Information contained in signal **644** is used as the error signal in a servo system to

alter the orientation of beam steering mirror **652** by orientation transducers **653A** and **653B** so as to maintain the direction of propagation of beam **633** substantially constant independent of changes of orientation of measurement object mirror **662**.

Orientation transducers **653A** and **653B** changes, in response to signal **644**, the

5 orientation of beam steering mirror **652** preferably about a point of reference retroreflector **1532**, changes in orientation of beam steering mirror **1522** about a nodal point of reference retroreflector **1532** producing substantially reduced lateral shear effects experienced by the reference beam. As a result, the exit reference and Under the condition that the physical path length of the measurement beam from the first
10 surface of beam steering mirror **652** to measurement object mirror **662** is equal to the physical path length of the measurement beam from measurement object mirror **662** to the second surface of beam steering mirror **652**, there will be no lateral shear of beam **633** at beam steering mirror **652** when changes in orientation of measurement object mirror **662** are compensated by changes in orientation of beam steering mirror **652**.

15 This condition with respect to physical path lengths will be referenced as the sixth embodiment condition.

Under the sixth embodiment condition, projections of measurement beams **611** and **633** at the surface of beam steering mirror **652** onto a plane parallel to and in the center of the surface planes of beam steering mirror **652** can be maintained

20 superimposed, changes in orientation of beam steering mirror **652** by orientation transducers **653A** and **653B** in response to signal **644** being about the center of the projections of measurement beams **611** and **633** at the surface of beam steering mirror **652** onto the plane parallel to and in the center of the surface planes of beam steering mirror **652**.

25 The remaining description of the sixth embodiment is the same as corresponding portions given for the first embodiment.

The six embodiment of the present invention exhibits advantages additional to those described for the first embodiment of the present invention. The additional advantages include no changes in any part of the path of the reference beam associated
30 with changes in orientation of the beam steering mirror **652** and/or the measurement object mirror **662** and no changes in the path of the measurement beam **611**,

measurement beam 633, and measurement beams and beam components for which beam 633 is a progenitor that are associated with changes in orientation of the steering mirror 652 and/or the measurement object mirror 662. Further, under the sixth embodiment condition, the size of the beam steering mirror 652 need only be large enough to accommodate the projected size of measurement beam 611, the location of measurement beams 611 and 633 being stationary at beam steering mirror 652. This leads to an additional advantage for the sixth embodiment with respect to a reduced minimum size permitted for beam steering mirror 652 and orientation transducers 653A and 653B and concomitant improvement in frequency response of beam steering mirror assembly.

FIGS. 7a and 7b depict, in schematic form, the seventh embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The seventh embodiment is from the second class of embodiments and variants operating in the first mode of operation for changes in orientation of the object about a first axis and in the second mode of operation for changes in orientation of the object about a second axis orthogonal to the first axis and/or a lateral displacement of the object, the lateral displacement being orthogonal to both the second axis and the linear displacement.

The interferometer system of the seventh embodiment is the same as the interferometer system of the sixth embodiment except with respect to the reflecting properties of the object: the reflecting properties of the object for the sixth embodiment are those of a plane mirror and the reflecting properties of the object for the seventh embodiment are those of a roof prism. There are also important similarities between the third embodiment and the seventh embodiment, the reflecting properties of object for both the third and seventh embodiments being those of a roof prism.

In the seventh embodiment, the separation of the measurement beam components incident on and reflected from the object is accomplished by spatially separating the measurement beam components incident on and reflected from the

object with a roof prism furnishing the reflection function of the object, the same as for the third embodiment. In the sixth embodiment, the separation of the measurement beam components incident on and reflected from the object is accomplished by use of polarization encoding, a quarter wave phase retardation plate, and a polarizing beam splitter.

Many elements of the sixth and seventh embodiments perform like functions and these elements are indicated by a numeric numbering scheme wherein the numeric number of elements performing like functions for the seventh embodiment are equal to the numeric number of corresponding elements of the sixth embodiment incremented by 100. The description of certain sections of the reference and measurement beam paths for the seventh embodiment are the same as the description given for corresponding paths of the sixth embodiment. The certain sections are indicated for the seventh embodiment by a numeric numbering scheme wherein the numeric number of the certain section of the reference or measurement path of the seventh embodiment having the same description as a corresponding path section of the sixth embodiment is equal to the numeric number of corresponding path section of the sixth embodiment incremented by 100.

The descriptions of the generation of measurement beam 713 and reference beam 716 are the same as the descriptions given for corresponding descriptions of the generation of measurement beam 613 and reference beam 616 of the sixth embodiment. As shown in FIG. 7a, beam 613 is reflected by mirrors 754A and 754B to form beam 701. Mirrors 754A and 754B together produce a constant deviation between beams 713 and 701 in the plane of FIG. 6a, the same as a penta prism. Beam 701 is reflected by measurement object roof prism 762 as beam 703 polarized in the plane of FIG. 7a. Beam 703 enters image inverter 756 and exits as beam 705. Image inverter 756 inverts an image about one axis and the description of image inverter 756 is the same as the description of image inverter 656 of the sixth embodiment. The primary function of image inverter 756 in the seventh embodiment is the same as the primary function of image inverter 656 in the sixth embodiment.

Reference beam 712 enters retroreflector 770 and is retroreflected as 718 polarized orthogonal to the plane of FIG. 7a. The description of the generation of

beams **738** and **742** from beams **705** and **718** in the seventh embodiment is the same as the corresponding description given for the generation of beams **638** and **642** from beams **631** and **616** in the sixth embodiment.

The description of the generation of electronic signal **744** from the detection of beam **738** in the seventh embodiment is the same as the description given in the third embodiment for the generation of electronic signal **340** from beam **332**. The description of the generation of electronic signal **746** from the detection of beam **746** in the seventh embodiment is the same as the description given in the third embodiment for the generation of electronic signal **342** from beam **336**.

The remaining description of the seventh embodiment is the same as corresponding portions of descriptions given for the third and sixth embodiments.

The advantage of the seventh embodiment in relation to the sixth embodiment is the same advantage the third embodiment has with respect to the first embodiment.

A first variant of the seventh embodiment of the present invention is described for measuring the linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The first variant of the seventh embodiment is from the second class of embodiments and variants thereof operating in the second mode of operation for changes in orientation of the object about two orthogonal axes and/or for a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.

The interferometer system and at least one beam steering assembly of the first variant of the seventh embodiment comprise the same elements as the interferometer system and at least one beam steering assembly of the seventh embodiment except for the object element, the detector of a certain optical beam, signal produced by the detector of the certain optical beam, and respective servo system.

The measurement object element of the seventh embodiment, roof prism **762**, is replaced by a measurement retroreflector **762A** (not shown in a figure) in the first variant of the seventh embodiment. As a consequence, the relative directions of propagation of the reference and measurement beam components of output beam **738A**, the output beam of the first variant of the seventh embodiment corresponding

to output beam 738 of the seventh embodiment, is substantially independent of changes in orientation of the measurement object retroreflector 762A of the first variant of the seventh embodiment. However a lateral translation of measurement object retroreflector 762A in a plane orthogonal to the direction of the linear displacement will generate a lateral displacement of measurement beam component of output beam 738A.

Detector 776A of the first variant of the seventh embodiment, corresponding to detector 776 of the seventh embodiment, detects the lateral displacement or shear of the measurement beam component of output beam 738A and generates electrical signal 744A, the electrical signal corresponding to electrical signal 744 of the seventh embodiment.

Electrical signal 744A is transmitted to orientation transducers 753A and 753B of the first variant of the seventh embodiment. Information contained in signal 744A is used as the error signal in a servo system to alter the orientation of beam steering mirror 752 by orientation transducers 753A and 753B of the first variant of the seventh embodiment so as to maintain the lateral location of measurement beam component of output beam 738A substantially constant independent of a lateral translation of measurement object retroreflector 762A in a plane orthogonal to the direction of the linear displacement and/or substantially independent of changes in orientation of measurement object retroreflector 762A about two orthogonal axes which are nominally orthogonal to the direction of propagation of beam 701 of the first variant of the seventh embodiment

The remaining description of the first variant of the seventh embodiment is the same as corresponding portions of the description given for the seventh embodiment.

FIGS. 8a-8c depict in schematic form an eighth embodiment of the present invention for measuring a linear displacement of an object with a fixed orientation wherein the direction of propagation of the measurement beam reflected from the object is sensitive to changes in orientation of the object and a high transmission efficiency is maintained for the measurement beam without the use of polarization encoding. The eighth embodiment is from the second class of embodiments and

variants operating in the second mode of operation for changes in the linear displacement of the object.

The description of light beam 810 shown in FIG. 8a and of a source of light beam 810 is the same as the description of light beam 110 and of a source of light beam 110 given for the first embodiment. As shown in FIG. 8a, beam 810 impinges on polarizing beam splitter 850. A portion of beam 810 is transmitted as measurement beam 811 polarized in the plane of FIG. 8a and a second portion of beam 810 is reflected as reference beam 812 orthogonally polarized to the plane of FIG. 8a.

In FIG. 8a, beam 811 is reflected by a first surface of mirror 852 as beam 813. Beam 813 enters image inverter 854. As shown in FIG. 8b, image inverter 854 is comprised of three mirrors 854A, 854B, and 854C. Beam 813 is reflected by each of the three mirrors 854A, 854B, and 854C and exits mirror assembly 854 as beam 817. Image inverter 854 inverts an image about one axis and the description of image inverter 854 is the same as the description of image inverter 656 of the sixth embodiment.

Beam 817 is reflected by beam steering mirror 856 as beam 819. Beam steering mirror 856 and orientation transducers 857A and 857B comprise a beam steering assembly that redirects beam 819. Beam 819 is reflected by measurement object mirror 858 as beam 823. Beam 823 is reflected by mirror 860 as beam 825 and beam 825 is reflected by beam steering mirror 862 as beam 827. Beam steering mirror 862 and orientation transducers 863A and 863B comprise a beam steering assembly that redirects beam 827.

Beam 827 is reflected by mirrors 864A, 864B, and 864C to form beam 829. Mirrors 864A, 864B, and 864C together comprise an image inverter which inverts an image about one axis orthogonal to plane of FIG. 8a and the description of which is the same as the description of image inverter 656 of the sixth embodiment. The primary function of the image inverter comprised of mirrors 864A, 864B, and 864C is the same as the primary function of image inverter 656 in the sixth embodiment. The angle of incidence of beam 829 on mirror 852 is nominally the same as the angle of incidence of beam 811 on mirror 852.

Beam 829 is reflected from a second surface of mirror 852 as beam 833. A translation of measurement object mirror 858 with a fixed orientation in a direction parallel to the average directions of propagation of beams 819 and 823 will effect a change in the lateral location of beam 833 at mirror 852. It is possible to compensate
5 for the effect on beam 833 by appropriate changes in the orientations of beam steering mirrors 856 and 862, the appropriate changes being accomplished by the respective orientation transducers in conjunction with the combination of mirror 860 and measurement object mirror 858 located in the path of the measurement beam between beam steering mirrors 856 and 862.

10 Beam 833 is reflected by mirror 866 as beam 835. Beam 835 is polarized in the plane of FIG. 8a.

Reference beam 812 enters image inverter 868. As shown in FIG. 8c, image inverter 868 is comprised of three mirrors 868A, 868B, and 868C. The plane of FIG. 8c is orthogonal to the plane of FIG. 8a. Beam 812 is reflected by each of the three
15 mirrors 868A, 868B, and 868C and exits mirror assembly 868 as beam 816. The primary function of the image inverter 868 is the same as the primary function of image inverter 656 in the sixth embodiment.

Reference beam 816 is subsequently reflected by mirrors 870A and 870B to form beam 818. Mirrors 870A and 870B function together as a roof prism. Beam 818
20 is polarized perpendicular to the plane of FIG. 8a.

Beam 835 is transmitted by polarizing beam splitter 872 as one component of output beam 836, beam 835 being polarized in the plane of FIG. 8a. A portion of beam 816 is transmitted by polarizing beam splitter 872 as a second component of output beam 836, beam 816 being polarized orthogonal to the plane of FIG. 8a.

25 A portion of output beam 836 is reflected by nonpolarizing beam splitter 874 as beam 838. Beam 838 impinges on detector 876 to produce an electrical signal 845 related to the lateral location of the measurement beam component in beam 838.

A second portion of output beam 836 is transmitted by nonpolarizing beam splitter 874 as beam 840. Beam 840 is transmitted by a polarizer 878 orientated to
30 produce a mixed optical beam 842. Beam 842 impinges on detector 880 to generate electrical signal 846 related to the difference in phase of the measurement and

reference beam components of mixed beam **842**. Electrical signal **846** is transmitted to electronic processor and computer **882** for subsequent processing for the information about the difference in phase of the measurement and reference beam components of mixed beam **842**.

5 The electronic signal **845** is used by orientation transducers **857A** and **857B** to effect a rotation of steering mirror **856** in the plane of FIG. **8a** about point R_1 shown in FIG. **8a**. Similarly, electronic signal **845** is used by orientation transducers **863A** and **863B** to effect a rotation of steering mirror **862** about point R_2 in the plane of FIG. **8a**. For each rotation of beam steering mirror **856** produced by orientation
10 transducers **857A** and **857B** resulting from a given signal **845**, the same angular rotation of beam steering mirror **862** is generated by orientation transducers **863A** and **863B** also based on signal **845**. Thus the direction of propagation of beam **827** is unaltered by the combined rotations of beam steering mirrors **856** and **862** arising from a given signal **845**.

15 The line of length y_1 from R_1 to the point where beam **817** intersects beam steering mirror **856** is orthogonal to the direction of propagation of beam **817**. The line of length y_2 from R_2 to the point where beam **827** intersects beam steering mirror **862** is orthogonal to the direction of propagation of beam **827**. Under a set of eighth embodiment conditions comprising the condition that

20

$$y_1 = y_2 \quad , \quad (2)$$

the condition that the physical path length of beam **819** is equal to the combined physical path lengths of beams **823** and **825**, and the condition that points R_1 and R_2
25 are coextensive, beam steering mirrors **856** and **862** can each be rotated by an angle γ in the plane of FIG. **8a** about points R_1 and R_2 , respectively, such that for a translation of measurement object mirror **858** of fixed orientation in a direction parallel to the average direction of propagation of beams **819** and **823** before the translation,

1) there will be no change in the average direction of propagation of beams 819 and 823;

2) there will be no lateral shear introduced in beam 819 at measurement object mirror 858;

5 3) there will be no lateral shear introduced in beam 817 at beam steering mirror 856 or in beams which are progenitors of beam 817; and

4) there will be no lateral shear introduced in beam 827 at beam steering mirror 862 or in measurement beams or measurement beam components for which beam 827 is a progenitor.

10 The absolute magnitude of the changes in angles of rotation γ will be equal to the absolute magnitude of changes in $\eta/2$ where η is the angle of incidence of beam 819 at measurement object mirror 858. The magnitude of the changes in angles of rotation γ encountered in typical operation of a distance measuring interferometer will be of the order of 0.005 radians for measurement leg lengths varying between 0.4
15 m and 1.0 m.

The remaining description of the eighth embodiment is the same as corresponding portions of the descriptions given for the sixth embodiment.

An advantage of the eighth embodiment is a high transmission efficiency of the measurement beam without the use of polarization encoding and without the
20 introduction of variable lateral displacements of measurement beam 811, measurement beam 833, and measurement beams and measurement beam components for which beam 833 is a progenitor, the advantage being present for a measurement of a linear displacement of an object of a fixed orientation wherein the direction of propagation of the measurement beam reflected from the object is sensitive to changes
25 in orientation of the object.

FIGS. 9a-9c depicts in schematic form a ninth embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.
30 The ninth embodiment is from the second class of embodiments and variants operating in the first mode of operation for changes in orientation of the object about

two orthogonal axes, the orthogonal axes being orthogonal to the linear displacement and/or a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.

The ninth embodiment incorporates the beam steering beam assemblies of the sixth and eighth embodiments. In this role, the elements of the ninth embodiment shown in FIG. 9a perform like functions as like numbered elements of the eighth embodiment shown in FIG. 8a incremented by 100 except for beam steering mirror 952 and orientation transducers 953A and 953B. The description of beam steering mirror 952 and orientation transducers 953A and 953B is the same as the description given for beam steering mirror 652 and orientation transducers 653A and 653B of the sixth embodiment.

Detector 976 performs the functions of detector 676 of the sixth embodiment and generates electronic signal 944, the description of electronic signal 944 of the ninth embodiment being the same as corresponding portions of the description given for electronic signal 644 of the sixth embodiment. Detector 976 in addition performs the functions of detector 876 of the eighth embodiment and generates electronic signal 945, the description of electronic signal 945 being the same as the description given for electronic signal 845 of the eighth embodiment.

In the normal mode operation of the ninth embodiment, if the orientation of beam steering mirror 952 is not correct for a given orientation of measurement object mirror 958, there will be a difference in the directions of propagation of the measurement beam and reference beam components of beam 938 and a lateral shear of the measurement beam component relative to the reference beam component of beam 938. Detector 976 detects the difference in directions of propagation of the measurement and reference beam components of beam 938 and generates electronic signal 944. Electronic signal 944 is transmitted to orientation transducers 953A and 953B which adjust the orientation of beam steering mirror 952 so that the directions of propagation of the measurement and reference beam components of beam 938 are the same. The lateral shear of the measurement beam component relative to the reference beam component of beam 938 due to the incorrect orientation of beam steering mirror 952 is compensated simultaneously with the compensation of the difference in the

directions of propagation of the measurement beam and reference beam components of beam 938.

There will be a residual lateral shear of the measurement beam component relative to the reference beam component of beam 938 should there be an incorrect
5 orientation of beam steering mirrors 956 and 962. Detector 976 detects the residual lateral shear of the measurement and reference beam components of beam 938 and generates electronic signal 945. Electronic signal 945 is transmitted to orientation transducers 957A and 957B which adjust the orientation of beam steering mirror 956 and to orientation transducers 963A and 963B which adjust the orientation of beam
10 steering mirror 962 so that the residual lateral shear of the measurement and reference beam components of beam 938 is compensated.

The remaining description of the ninth embodiment is the same as that given for corresponding portions of the descriptions given for the sixth and eighth embodiments.

15 FIGS. 10a-10c depict in schematic form a tenth embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement, and wherein a high transmission efficiency of the measurement beam is maintained
20 without the use of polarization encoding. The tenth embodiment is from the second class of embodiments and variants operating in the first mode of operation for changes in orientation of the object about two orthogonal axes, two orthogonal axes being orthogonal to the linear displacement and/or a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.

25 The tenth embodiment may be considered a variant of the ninth embodiment of the present invention. The function performed by mirror assembly comprised of beam steering mirror 1052 and orientation transducers 1053A and 1053B of the tenth embodiment is the same function performed by the mirror assembly comprised of mirror 952 and orientation transducers 953A and 953B of the ninth embodiment. The
30 function performed by mirror assembly comprised of beam steering mirror 1058 and orientation transducers 1059A and 1059B of the tenth embodiment is the same as the

combined functions performed by the mirror assembly comprised of beam steering mirror **956** and orientation transducers **957A** and **957B** and beam steering mirror assembly comprised of mirror **962** and orientation transducers **963A** and **963B** of the ninth embodiment.

5 The description of electronic signals **1026** and **1028** of the tenth embodiment is the same as the corresponding portions of the descriptions given for electronic signals **944** and **945**, respectively, of the ninth embodiment. The description of the remaining elements of the tenth embodiment shown in FIG. **10a** perform like functions as like numbered elements of the ninth embodiment shown in FIG. **9a**
10 incremented by **100**.

 The relevant tenth embodiment conditions are that:

 1) the physical path length from measurement beam **1013** at beam steering mirror **1058** to measurement beam **1021** at beam steering mirror **1052** is equal to the physical path length from measurement beam **1039** at beam steering mirror **1052** to
15 measurement beam **1041** at steering mirror **1058**;

 2) the physical path length from measurement beam **1023** at beam steering mirror **1052** to measurement beam **1031** at measurement object mirror **1064** is equal to the physical path length from measurement beam **1033** at measurement object mirror **1064** to measurement beam **1037** at beam steering mirror **1052**;

20 3) the angle of incidence of beam **1011** and the angle of incidence of beam **1041** at beam steering mirror **1058** are nominally the same; and

 4) the angle of incidence of beam **1021** and the angle of incidence of beam **1037** at beam steering mirror **1052** are nominally the same.

 It will be evident to those skilled in the art that under the tenth embodiment
25 conditions that the location of beam **1011** and the location of beam **1043** at beam steering mirror **1058** will be substantially one above the other and that the location of beam **1021** and the location of beam **1039** at beam steering mirror **1052** will be substantially one above the other.

 The description of the steering beam assembly comprising steering mirror **652**
30 of the sixth embodiment with respect to the size of respective components and

frequency response is applicable for both of the beam steering assemblies of the tenth embodiment comprising beam steering mirrors **1052** and **1058**.

The remaining description of the tenth embodiment is the same as corresponding portions of the description given for the ninth embodiment.

5 FIGS. **11a-11f** depict, in schematic form, the eleventh embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The eleventh embodiment is from the second class of embodiments
10 and variants thereof operating in the first mode of operation for changes in orientation of the object about two orthogonal axes, two orthogonal axes being orthogonal to the linear displacement, and/or a lateral displacement of the object, the lateral displacement being orthogonal to both the linear displacement.

The interferometer system of the tenth and eleventh embodiments are
15 generically similar except with respect to the number of passes the measurement beam makes to the object: the measurement beams of the eleventh embodiment traverse certain sections of the measurement path in two opposite directions of propagation where in the tenth embodiment, the corresponding measurement beam transits the certain sections in only one direction of propagation. Efficient separation of an output
20 measurement beam component from an input measurement beam component in the multiple pass configuration of the eleventh embodiment is effected by use of polarization encoding and polarizing beam splitters.

Many elements of the tenth and eleventh embodiments perform like functions and these elements are indicated by a numeric numbering scheme wherein the numeric
25 number of elements performing like functions for the eleventh embodiment are equal to the numeric number of corresponding elements of the tenth embodiment incremented by **100**. The certain sections of the reference and measurement beam paths are indicated by the numeric numbering scheme wherein the numeric number of the certain section of the reference or measurement path of the eleventh embodiment
30 having the same description as a corresponding path section of the tenth embodiment

is equal to the numeric number of corresponding path section of the tenth embodiment incremented by 100.

For the certain sections of the measurement beam paths for the eleventh embodiment, there are measurement beams traversing the certain sections in a reverse direction of propagation, the nonreverse or forward direction of propagation being associated with a first pass to measurement object mirror 1164 and the reverse direction of propagation being associated with a second pass to the measurement object mirror 1164. The description of the additional measurement beams traversing the certain sections in a reverse direction are otherwise the same as the corresponding portions of the description given associated measurement beams traversing in a nonreverse direction of propagation for the tenth embodiment, an alphanumeric number of a measurement beam traversing in a reverse direction being equal to the numeric number of the associated measurement beam traversing in a nonreverse direction augmented with the suffix R.

The descriptions of the generation of measurement beam 1143 and reference beam 1112 is the same as the descriptions given for corresponding descriptions of the generation of measurement beam 1043 and reference beam 1012 of the tenth embodiment. As shown in FIG. 11d, a first portion of beam 1143 is transmitted by nonpolarizing beam splitter 1171 as beam 1145. Beam 1145 impinges on detector 1190 to generate electrical signal 1128. A second portion of beam 1143, being polarized in the plane of FIG. 11d, is reflected by nonpolarizing beam splitter 1171, is transmitted by quarter wave phase retardation plate 1172 as a circularly polarized beam, reflected by mirror 1173 as a beam with opposite-handed circular polarization, transmitted by phase retardation plate 1172 as a beam orthogonally polarized to the plane of FIG. 11d, and subsequently a portion thereof reflected by nonpolarizing beam splitter 1171 as beam 1143R. Beam 1143R is orthogonally polarized to the plane of FIG. 11d.

The elements of detector 1190 are depicted, in schematic form, in FIG. 11e. Beam 1145 enters detector 1190 and a first portion of beam 1145 is reflected by nonpolarizing beam splitter 1190A as beam 1145A. Beam 1145A is focused by lens 1190B to a spot on detector 1190C such as a quad cell detector, a two-dimensional

high speed CCD camera, or a lateral effect photodiode. Two-dimensional data arrays are transmitted as electronic signal **1128A**. The location of the spot on detector **1190C** is not effected by a lateral shear of beam **1145A** but a change in the direction of propagation of beam **1145A** does shift the location of the spot on detector **1190C**.
5 Thus the electronic signal **1128A** contains information about the direction of propagation of beam **1145A**.

A second portion of beam **1145** is transmitted as beam **1145B**. Beam **1145B** impinges on detector **1190D** such as a quad cell to generate electronic signal **1128B**. The location of beam **1145B** on detector **1190D** is effected by a lateral shear of beam
10 **1145B** but a change in the direction of propagation of beam **1145B** at detector **1190D** does shift the location of beam **1145B** on detector **1190D**. Thus the electronic signal **1128B** contains information about lateral shear of beam **1145B**. Electronic signals **1128A** and **1128B** comprise electronic signal **1128**.

As shown in FIG. **11a**, a first portion of reference **1112** is transmitted by
15 nonpolarizing beam splitter **1174** as beam **1114** and a second portion of reference **1112** is reflected by nonpolarizing beam splitter **1174** as beam **1116**. As shown in FIGS. **11d** and **11f**, beam **1114** impinges on detector **1192** to generate electrical signal **1130**.

The elements of detector **1192** are depicted, in schematic form, in FIG. **11f**.
20 Beam **1114** enters detector **1192** and a first portion of beam **1114** is reflected by nonpolarizing beam splitter **1192A** as beam **1114A**. Beam **1114A** is focused by lens **1192B** to a spot on detector **1192C** such as a quad cell detector, a two-dimensional high speed CCD camera, or a lateral effect photodiode. Two-dimensional data arrays are transmitted as electronic signal **1130A**. The location of the spot on detector
25 **1192C** is not effected by a lateral shear of beam **1114A** but a change in the direction of beam **1114A** does shift the location of the spot on detector **1192C**. Thus the electronic signal **1130A** contains information about the direction of propagation of beam **1114A**.

A second portion of beam **1114** is transmitted by nonpolarizing interface
30 **1192A** as beam **1114B**. Beam **1114B** impinges on detector **1192D** such as a quad cell to generate electronic signal **1130B**. The location of beam **1114B** on detector **1192D**

is effected by a lateral shear of beam **1114B** but a change in the direction of propagation of beam **1114B** at detector **1192D** does shift the location of beam **1114B** on detector **1192D**. Thus the electronic signal **1130B** contains information about lateral shear of beam **1114B**. Electronic signals **1130A** and **1130B** comprise
5 • electronic signal **1130**.

Electronic signals **1128** and **1130** are transmitted to electronic signal processor **1194** (*cf.* FIG. **11d**). From the components of electronic signals **1128** and **1130** that contain information about the directions of propagation of measurement beam **1145A** and reference beam **1114A**, electronic processor **1194** generates electronic signal
10 **1132**. From the components of electronic signals **1128** and **1130** that contain information about the lateral shear of measurement beam **1145B** and reference beam **1114B**, electronic processor **1194** generates electronic signal **1134**.

Electrical signal **1132** is transmitted to orientation transducers **1153A** and **1153B** and electronic signal **1134** is transmitted to orientation transducers **1159A** and
15 **1159B**. Information contained in signal **1132** is used as the error signal in a servo system to alter the orientation of beam steering mirror **1152** by orientation transducers **1153A** and **1153B** so as to maintain in two orthogonal dimensions the direction of propagation of measurement beam **1143** substantially constant independent of changes of orientation of measurement object mirror **1164**. Information contained in signal
20 **1134** is used as the error signal in a servo system to alter the orientation of beam steering mirror **1158** by orientation transducers **1159A** and **1159B** so as to maintain in two orthogonal dimensions the lateral position of measurement beam **1143** substantially constant independent of changes in the location of measurement object mirror **1164** along the average of the paths of beams **1131** and **1133**. Under a set of
25 eleventh embodiment conditions that the physical path length of the measurement beam from the location of the first redirection of the measurement beam by the beam steering element **1158** to the first redirection of the measurement beam by the beam steering element **1152** is equal to the physical path length of the measurement beam from the second redirection of the measurement beam by the beam steering element
30 **1152** to the second redirection of the measurement beam by the beam steering element **1158** and that the physical path length of the measurement beam from the location of

the first redirection of the measurement beam by the beam steering element **1152** to measurement object mirror **1164** is equal to the physical path length of the measurement beam from measurement object mirror **1164** to the location of the second redirection of the measurement beam by the beam steering mirror **1152**, there
5 will be no lateral shear of beam **1143** at beam steering element **1158** when changes in orientation of measurement object mirror **1164** are compensated by changes in orientation of beam steering element **1152** and when the effects of changes in the location of measurement object mirror **1164** along the average of the paths of beams **1131** and **1133** are compensated by changes in orientation of beam steering mirror
10 **1158**. These conditions with respect to physical path lengths will be referenced as the eleventh embodiment conditions.

Beam **1143R** is substantially coextensive with beam **1143** and beam **1143R** (*cf.* FIG. **11a**) has a direction of propagation substantially opposite to the direction of propagation of **1143**. As a consequence, beam **1143R** substantially retraces the pass
15 through portions of the interferometer, the pass leading to the generation of beam **1143**, to generate beam **1111R**. The retrace through portions of the interferometer includes in particular a pass to the measurement object mirror **1164**. Beam **1111R** is substantially coextensive with beam **1111** and beam **1111R** has a direction of propagation substantially opposite to the direction of propagation of beam **1111**.

20 Beam **1111R**, being polarized orthogonal to the plane of FIG. **11a**, is reflected by polarizing beam splitter **1150** as beam **1147**. Beam **1147** is reflected by mirror **1177** as beam **1149**.

Reference beam **1116** is reflected by mirrors **1176A** and **1176B** to form beam **1118**. Mirrors **1176A** and **1176B** together produce a constant deviation between
25 beams **1116** and **1118** in the plane of FIG. **11a**, the same as a penta prism.

A portion of beam **1149** is transmitted by nonpolarizing beam splitter **1178** as one component of output beam **1124**. A portion of beam **1118** is transmitted by nonpolarizing beam splitter **1178** as a second component of the output beam **1124**. Beam **1124** is a mixed optical beam, beams **1149** and **1118** being both polarized
30 orthogonal to the plane of FIG. **11a** and beam splitter **1178** being of the nonpolarizing type. Beam **1124** impinges on detector **1186** to generate electrical signal **1136** related

to the difference in phase of the measurement and reference beam components of mixed beam 1124. Electrical signal 1136 is transmitted to electronic processor and computer 1188 for subsequent processing to obtain information about the difference in phase of the measurement and reference beam components of mixed beam 1124.

5 The detection of mixed beam is typically by photoelectric detection to produce a heterodyne signal, the phase of which is related to the difference in optical path lengths of the measurement and reference beams. The phase of the heterodyne signal may be determined by electronic processor and computer 1188 for example from a Fourier transform or Hilbert transform of the heterodyne signal.

10 The remaining description of the eleventh embodiment is the same as corresponding portions given for the descriptions of the fourth and tenth embodiments.

FIGS. 12a-12e depict, in schematic form, the twelfth embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The twelfth embodiment is from the second class of embodiments and variants thereof operating in the first mode of operation for changes in orientation of the object about a first axis and in the second mode of operation for changes in orientation of the object about a second axis orthogonal to the first axis, the first and second axes being orthogonal to the linear displacement, and/or a lateral displacement of the object, the lateral displacement being orthogonal to both the second axis and the linear displacement.

25 The interferometer system of the seventh and twelfth embodiments are generically similar except with respect to the number of passes the measurement beam makes to the object: the measurement beams of the twelfth embodiment traverse certain sections of the measurement path in two opposite directions of propagation where in the seventh embodiment, the corresponding measurement beam transits the certain sections in only one direction of propagation. Efficient separation of an output measurement beam component from an input measurement beam component in the

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multiple pass configuration of the twelfth embodiment is effected by use of polarization encoding and polarizing beam splitters.

Many elements of the seventh and twelfth embodiments perform like functions and these elements are indicated by a numeric numbering scheme wherein the numeric number of elements performing like functions for the twelfth embodiment are equal to the numeric number of corresponding elements of the eleventh embodiment incremented by 500. The certain sections of the measurement beam paths are indicated by a numeric numbering scheme wherein the numeric number of the certain section of the measurement path of the twelfth embodiment having the same description as a corresponding path section of the seventh embodiment is equal to the numeric number of corresponding path section of the seventh embodiment incremented by 500.

For the certain sections of the measurement beam paths for the twelfth embodiment, there are measurement beams traversing the certain sections in a reverse direction of propagation, the nonreverse or forward direction of propagation being associated with a first pass to measurement object roof prism 1262 and the reverse direction of propagation being associated with a second pass to the measurement object roof prism 1262. The description of the additional measurement beams traversing the certain sections in a reverse direction are otherwise the same as the corresponding portions of the description given associated measurement beams traversing in a nonreverse direction of propagation for the seventh embodiment, an alphanumeric number of a measurement beam traversing in a reverse direction being equal to the numeric number of the associated measurement beam traversing in a nonreverse direction augmented with the suffix **R**.

The descriptions of the generation of measurement beam 1233 and reference beam 1212 is the same as the descriptions given for corresponding descriptions of the generation of measurement beam 733 and reference beam 712 of the seventh embodiment. As shown in FIG. 12c, a first portion of beam 1233 is transmitted by nonpolarizing beam splitter 1271 as beam 1235. Beam 1235 impinges on detector 1290 to generate electrical signal 1228. A second portion of beam 1233, being polarized in the plane of FIG. 12c, is reflected by nonpolarizing beam splitter 1271, is

transmitted by quarter wave phase retardation plate **1272** as a circularly polarized beam, reflected by mirror **1273** as a beam with opposite-handed circular polarization, transmitted by quarter wave phase retardation plate **1272** as a beam orthogonally polarized to the plane of FIG. **12c**, and subsequently a portion thereof reflected by
5 nonpolarizing beam splitter **1271** as beam **1233R**. Beam **1233R** is orthogonally polarized to the plane of FIG. **12c**.

The elements of detector **1290** are depicted, in schematic form, in FIG. **12d**. Beam **1235** enters detector **1290** and a first portion of beam **1235** is reflected by nonpolarizing beam splitter **1290A** as beam **1235A**. Beam **1235A** is focused by lens
10 **1290B** to a spot onto a one dimensional detector **1290C** such as a dual cell detector, a linear array, high speed CCD camera, or a lateral effect photodiode. An one-dimensional data array is transmitted as electronic signal **1228A**. The location of the spot on one dimensional detector **1290C** is not effected by a lateral shear of beam **1235A** but a change in the direction of beam **1235A** in the plane defined by the one
15 dimensional detector **1290C** and the nominal direction of beam **1235A** does shift the location of the spot on detector **1290C**. Thus the electronic signal **1228A** contains information about the direction of propagation of beam **1235A** in the plane defined by the one dimensional detector **1290C** and the nominal direction of beam **1235A**, a plane corresponding to a plane orthogonal to the plane of FIG. **12a** and orthogonal to
20 the nominal direction of propagation of measurement beam **1201**.

A second portion of beam **1235** is transmitted as beam **1235B**. Beam **1235B** impinges on one dimensional detector **1290D** such as a dual cell detector to generate electronic signal **1228B**. The location of beam **1235B** on detector **1290D** is effected by a lateral shear of beam **1235B** but a change in the direction of propagation of beam
25 **1235B** at detector **1290D** does shift the location of beam **1235B** on one dimensional detector **1290D**. Thus the electronic signal **1228B** contains information about lateral shear of beam **1235B**, the plane defined by the one dimensional detector **1290D** being orthogonal to the plane defined by the one dimensional detector **1290C**. Electronic signals **1228A** and **1228B** comprise electronic signal **1228**.

30 As shown in FIG. **12a**, a first portion of reference **1212** is transmitted by nonpolarizing beam splitter **1274** as beam **1214** and a second portion of reference

1212 is reflected by nonpolarizing beam splitter 1274 as beam 1216. As shown in FIGS. 12c and 12e, beam 1214 impinges on detector 1292 to generate electrical signal 1230.

The elements of detector 1292 are depicted, in schematic form, in FIG. 12e.

5 Beam 1214 enters detector 1292 and a first portion of beam 1214 is reflected by nonpolarizing beam splitter 1292A as beam 1214A. Beam 1214A is focused by lens 1292B to a spot on a one dimensional detector 1292C such as a dual cell detector, linear array high, speed CCD camera, or a lateral effect photodiode. A one-dimensional data array is transmitted as electronic signal 1230A. The location of the
10 spot on the one dimensional detector 1292C is not effected by a lateral shear of beam 1214A but a change in the direction of propagation of beam 1214A does shift the location of the spot on the one dimensional detector 1292C. Thus the electronic signal 1230A contains information about the direction of propagation of beam 1214A in the plane defined by the one dimensional detector 1292C and the nominal direction
15 of beam 1214A the plane of one dimensional detector 1292C arranged to correspond to the plane of one dimensional detector 1290C.

A second portion of beam 1214 is transmitted as beam 1214B. Beam 1214B impinges on a one dimensional detector 1292D such as a dual cell detector to generate electronic signal 1230B. The location of beam 1214B on detector 1292D is effected
20 by a lateral shear of beam 1214B but a change in the direction of propagation of beam 1214B at detector 1292D does shift the location of beam 1214B on detector 1292D. Thus the electronic signal 1230B contains information about lateral shear of beam 1214B, the plane defined by the one dimensional detector 1292D arranged to correspond to the plane defined by the one dimensional detector 1290D. Electronic
25 signals 1230A and 1230B comprise electronic signal 1230.

Electronic signals 1228 and 1230 are transmitted to electronic signal processor 1294 (*cf.* FIG. 12c). From the components of electronic signals 1228 and 1230 that contain information about the directions of propagation of measurement beam 1235A and reference beam 1214A in a plane orthogonal to the plane of FIG. 12c and parallel
30 to the nominal direction of propagation of beam 1235A, electronic processor 1294 generates electronic signal 1232. From the components of electronic signals 1228 and

1230 that contain information about the lateral shear of measurement beam **1235B** and reference beam **1214B** in the plane of FIG. **12c**, electronic processor **1294** generates electronic signal **1234**.

Electrical signal **1232** is transmitted to orientation transducers **1253A** and **1253B**. Information contained in signal **1232** is used as the error signal in a servo system to alter the orientation of beam steering mirror **1252** by orientation transducers **1253A** and **1253B** so as to maintain in a first plane the direction of propagation of measurement beam **1233** substantially constant independent of changes of orientation of measurement object roof prism **1262**, the first plane being orthogonal to the plane of FIG. **12a** and parallel to the nominal direction of propagation of beam **1201**, and to maintain in a plane orthogonal to the first plane the lateral position of measurement beam **1233** substantially constant independent of translations of measurement object roof prism **1262** nominally orthogonal to the direction of propagation of measurement beam **1201** and substantially independent of changes in the orientation of measurement object roof prism **1262** about a axis orthogonal to the plane of FIG. **12a** and orthogonal to the nominal direction of propagation of beam **1201**. Under the condition that the physical path length of the measurement beam from the location of the first redirection of the measurement beam by the beam steering element **1252** to measurement object roof prism **1262** is equal to the physical path length of the measurement beam from measurement object roof prism **1262** to the location of the second redirection of the measurement beam by the beam steering mirror **1252**, there will be no lateral shear of beam **1233** at beam steering element **1252** when changes in orientation of measurement object roof prism **1262** are compensated by changes in orientation of beam steering element **1252** and when the effects of displacements in the location of measurement object roof prism **1262** nominally orthogonal to the path of beam **1233** are compensated by changes in orientation of beam steering element **1252**. This condition with respect to physical path lengths will be referenced as the twelfth embodiment condition.

Beam **1233R** is substantially coextensive with beam **1233** and beam **1233R** (*cf.* FIG. **12c**) has a direction of propagation substantially opposite to the direction of propagation of **1233**. As a consequence, beam **1233R** substantially retraces the pass

through portions of the interferometer, the pass leading to the generation of beam 1233, to generate beam 1211R. The retrace through portions of the interferometer includes in particular a pass to the object roof prism 1262. Beam 1211R is substantially coextensive with beam 1211 and beam 1211R has a direction of propagation substantially opposite to the direction of propagation of beam 1211.

Beam 1211R, being polarized orthogonal to the plane of FIG. 12a, is reflected by polarizing beam splitter 1250 as beam 1247. Beam 1247 is reflected by mirror 1177 as beam 1249.

Reference beam 1216 is reflected by mirrors 1276A and 1276B to form beam 1218. Mirrors 1276A and 1276B together produce a constant deviation between beams 1216 and 1218 in the plane of FIG. 12a, the same as a penta prism.

A portion of beam 1249 is transmitted by nonpolarizing beam splitter 1278 as one component of output beam 1224. A portion of beam 1218 is transmitted by nonpolarizing beam splitter 1278 as a second component of the output beam 1224.

Beam 1224 is a mixed optical beam, beams 1249 and 1218 being both polarized orthogonal to the plane of FIG. 12a and beam splitter 1278 being of the nonpolarizing type. Beam 1224 impinges on detector 1286 to generate electrical signal 1236 related to the difference in phase of the measurement and reference beam components of mixed beam 1224. Electrical signal 1236 is transmitted to electronic processor and computer 1288 for subsequent processing to obtain information about the difference in phase of the measurement and reference beam components of mixed beam 1224. The detection of mixed beam is typically by photoelectric detection to produce a heterodyne signal, the phase of which is related to the difference in optical path lengths of the measurement and reference beams. The phase of the heterodyne signal may be determined by electronic processor and computer 1288 for example from a Fourier transform or Hilbert transform of the heterodyne signal.

The remaining description of the twelfth embodiment is the same as corresponding portions given for the descriptions of the fourth and eleventh embodiments.

A first variant of the twelfth embodiment of the present invention is described for measuring the linear displacement of an object substantially independent of the

orientation of the object and substantially independent of a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement. The first variant of the twelfth embodiment is from the second class of embodiments and variants thereof operating in the second mode of operation for changes in orientation
5 of the object about two orthogonal axes and/or for a lateral displacement of the object, the lateral displacement being orthogonal to the linear displacement.

The interferometer system and at least one beam steering assembly of the first variant of the twelfth embodiment comprise the same elements as the interferometer system and at least one beam steering element of the twelfth embodiment except for
10 the object element, the detector of a certain optical beam, signal produced by the detector of the certain optical beam, and respective servo system.

The object element of the twelfth embodiment, measurement object roof prism **1262**, is replaced by a measurement object retroreflector **1262A** (not shown in a figure) in the first variant of the twelfth embodiment. As a consequence, the relative
15 directions of propagation of the reference and measurement beam components of output beam **1238A**, the output beam of the first variant of the twelfth embodiment corresponding to output beam **738** of the seventh embodiment, is substantially independent of changes in orientation of the measurement object retroreflector **1262A** of the first variant of the twelfth embodiment. However a lateral translation of
20 measurement object retroreflector **1262A** in a plane orthogonal to the direction of the linear displacement will generate a lateral displacement of measurement beam component of output beam **1238A**.

Detector **1276A** of the first variant of the twelfth embodiment, corresponding to detector **776** of the seventh embodiment, detects the lateral displacement or shear of
25 the measurement beam component of output beam **1238A** and generates electrical signal **1244A**, the electrical signal corresponding to electrical signal **744** of the seventh embodiment.

Electrical signal **1244A** is transmitted to orientation transducers **1253A** and **1253B** of the first variant of the twelfth embodiment. Information contained in signal
30 **1244A** is used as the error signal in a servo system to alter the orientation of beam steering mirror **1252** by orientation transducers **1253A** and **1253B** of the first variant

of the twelfth embodiment so as to maintain the lateral location of measurement beam component of output beam **1238A** substantially constant independent of a lateral translation of measurement object retroreflector **1262A** in a plane orthogonal to the direction of the linear displacement and/or substantially independent of changes in orientation of measurement object retroreflector **1262A** about two orthogonal axes which are nominally orthogonal to the direction of propagation of beam **1201** of the first variant of the twelfth embodiment.

The remaining description of the first variant of the twelfth embodiment is the same as corresponding portions of the description given for the twelfth embodiment.

FIGS. 13a-13b depict in schematic form an thirteenth embodiment of the present invention for measuring a linear displacement of an object substantially independent of the orientation of the object and lateral displacements of the object, the lateral displacements being orthogonal to the linear displacement. The thirteenth embodiment is from a third class of embodiments and variants thereof of the present invention operating in the first mode of operation for changes in orientation of the object about two orthogonal axes.

The description of light beam **1310** shown in **FIG. 13a** and of a source of light beam **1310** is the same as the description of light beam **110** and of a source of light beam **110** given for the first embodiment. As shown in **FIG. 13a**, beam **1310** is reflected by a surface of beam steering mirror **1350** as beam **1312**. Beam steering mirror **1350** and orientation transducers **1351A** and **1351B** comprise a beam steering assembly that redirects the input beam **1310**. Beam **1312** is reflected by mirrors **1352A** and **1352B** to form beam **1314**. Mirrors **1352A** and **1352B** together produce a constant deviation between beams **1312** and **1314** in the plane of **FIG. 13a**, the same as a penta prism.

Continuing with **FIG. 13a**, beam **1314** impinges on polarizing beam splitter **1354** with a portion of beam **1314** transmitted as measurement beam **1315** polarized in the plane of **FIG. 13a** and a second portion of beam **1314** reflected as reference beam **1316** orthogonally polarized to the plane of **FIG. 13a**.

Beam **1315** is transmitted by polarizing beam splitter **1356** as beam **1317**. Beam **1317**, polarized in the plane of **FIG. 13a**, is transmitted by a quarter wave phase

retardation plate 1358 as a circularly polarized beam, reflected by measurement object mirror 1360, comprised of a single reflecting surface, as a beam with opposite-handed circular polarization, and subsequently transmitted by quarter wave phase retardation plate 1358 as beam 1319 linearly polarized orthogonal to the plane of FIG. 13a.

5 Beam 1319 is reflected by polarizing beam splitter 1356 as beam 1321. Beam 1321 is reflected by mirror 1362 as beam 1323.

Reference beam 1316 is transmitted by half-wave phase retardation plate 1364 as beam 1318 linearly polarized in the plane of FIG. 13a. Beam 1318 is retroreflected by retroreflector 1366 as beam 1320.

10 Measurement beam 1323 is reflected by polarizing beam splitter 1368 as one component of output beam 1328. Beam 1320 is transmitted by polarizing beam splitter 1368 as a second component of output beam 1328. Beam 1328 is reflected by mirror 1370 as beam 1330 and beam 1330 is reflected by a second surface of beam steering mirror 1350 as output beam 1332.

15 Output beam 1332 enters optical system 1398 and exits as beam 1338. The reference beam component of output beam 1332 has experienced image inversions about two orthogonal axes and the measurement beam component of output beam 1332 has experienced an image inversion about one of the orthogonal axes. Optical system 1398 in FIG. 13a introduces an additional image inversion in the measure
20 beam component of beam 1332 relative to the reference beam component of beam 1332 so that reference beam component of beam 1338 has experienced the same number of image inversions about for each of two orthogonal axes modulo two as number of image inversions experienced by the measurement beam component of beam 1338.

25 The reference beam component of beam 1332 is transmitted by polarizing beam splitter 1372 and reflected by mirror 1374 as beam 1334. Beam 1334 enters image inverter 1376. As shown in FIG. 13b, image inverter 1376 is comprised of three mirrors 1376A, 1376B, and 1376C. The plane of FIG. 13b is orthogonal to the plane of FIG. 13a. Beam 1334 is reflected by each of the three mirrors 1376A,
30 1376B, and 1376C and exits image inverter 1376 as beam 1336.

The measurement beam component of beam **1332** is reflected by polarizing beam splitter **1372** as beam **1333**. Beam **1333** is reflected by mirrors **1378A** and **1378B** to form beam **1335**. Mirrors **1378A** and **1378B** together produce a constant deviation between beams **1333** and **1333** in the plane of FIG. **13a**, the same as a penta prism.

Beam **1336** is transmitted by polarizing beam splitter **1380** as one component of output beam **1338**. Beam **1335** is reflected by polarizing beam splitter **1380** as a second component of output beam **1338**.

A portion of beam **1338** is reflected by nonpolarizing beam splitter **1382** as beam **1340**. Beam **1340** impinges on detector **1384** to produce an electrical signal **1348** related to any difference in the directions of propagation of measurement and reference beam components in beam **1340**.

A second portion of output beam **1338** is transmitted by nonpolarizing beam splitter **1382** as beam **1342**. Beam **1342** is transmitted by a polarizer **1386** orientated to produce a mixed optical beam **1344**. Beam **1344** impinges on detector **1388** to generate electrical signal **1346** related to the difference in phase of the measurement and reference beam components of mixed beam **1344**. Electrical signal **1346** is transmitted to electronic processor and computer **1390** for subsequent processing for information about the difference in phase of the measurement and reference beam components of mixed beam **1344**.

Electrical signal **1348** is transmitted to orientation transducers **1351A** and **1351B**. Information contained in signal **1348** is used as the error signal in a servo system to alter the orientation of beam steering mirror **1350** by orientation transducers **1351A** and **1351B** so as to maintain the direction of propagation of the measurement beam component of beam **1332** substantially constant relative to the direction of propagation of the reference beam component of beam **1332** independent of changes of orientation of measurement object mirror **1360**. Under the condition that the physical path length of the measurement beam from the first surface of beam steering mirror **1350** to measurement object mirror **1360** is equal to the physical path length of the measurement beam from measurement object mirror **1360** to the second surface of steering mirror **1350**, there will be no lateral shear of measurement beam component

of beam **1332** at steering mirror **1350** when changes in orientation of measurement object mirror **1360** are compensated by changes in orientation of steering mirror **1350**. This condition with respect to physical path lengths will be referenced as the thirteenth embodiment condition.

5 The remaining description of the thirteenth embodiment is the same as corresponding portions of the descriptions given for preceding embodiments and variants thereof.

 The thirteenth embodiment of the present invention exhibits an advantage additional to those described for the first embodiment of the present invention. The
10 additional advantage relates to the size of the beam steering mirror **1350** and orientation transducers **1351A** and **1351B**. Under the thirteenth embodiment condition, the size of beam steering mirror **1350** need only be large enough to accommodate the projected size of input beam **1310**, the location of input beam **1310** and output beam **1332** being stationary at beam steering mirror **1350**. This leads to an
15 additional advantage for the thirteenth embodiment with respect to a reduced minimum size permitted for beam steering mirror **1350** and orientation transducers **1351A** and **1351B** and concomitant improvement in frequency response of beam steering mirror assembly.

 For end use applications where the image inversion in beam **1332** does not
20 present undesired complications, inverter **1398** of the thirteenth embodiment may be omitted to form a variant of the thirteenth embodiment without departing from the scope or spirit of the present invention. The remaining description of the variant of the thirteenth embodiment is the same as corresponding portions of the descriptions given for the thirteenth embodiment. Other variations of the thirteenth embodiment
25 can include those in which the measurement object includes a roof prism or a retroreflector to reflect the measurement beam. In such variations the system can operate in the second mode as required to compensate for changes in the position of the measurement object.

 In some of the embodiments described above, the beam steering assembly and
30 control circuit can be used to reduce negative effects of spurious reflections on the laser source generating the reference and measurement beams. Spurious reflections

resulting from imperfections in the polarizing beam splitting surfaces or the quarter wave plates can, in some cases, reflect back to the laser source and destabilize or alter the performance of the laser source. To reduce such negative effects, the system can be aligned as follows.

5 If spurious reflections that negatively affect the performance of the source laser are identified, one of the optics that direct the reference beam is adjusted to slightly alter the direction of the reference beam and produce a corresponding change in the direction or position of the exit reference beam. For example, if the system includes a plane mirror as a reference object, the angular orientation of the plane
10 mirror can be adjusted, or if the system includes mirrors that form a reference retroreflector, these mirrors can be adjusted so that their surfaces are not exactly normal to one another. Alternatively, a wedge or prism can be introduced into the reference path to introduce a small angular offset in the reference beam. Whatever the optic, that optic is adjusted until the spurious reflections derived from the reference
15 beam no longer propagate back to the laser source.

 In addition, the detector in the control circuit detects the change in the direction or position of the exit reference beam and causes the servo controller to reorient the beam steering mirror in response to a change in the relative position and/or direction of the exit reference and measurement beams. The beam steering
20 mirror redirects the measurement beam such that the exit measurement beam tracks the changes to the exit reference beam, *e.g.*, such that the exit reference and measurement beams remain substantially parallel and/or coextensive. As a result, the spurious reflections derived from the measurement beam should no longer propagate back to the laser source. Moreover, the beam steering assembly and control circuit
25 maintains the alignment of the reference and measurement beams.

 This procedure can be implemented during fabrication of the interferometry system to determine an alignment for the optics of the system that prevents or reduces propagation of spurious reflections back to the laser source. In general, the procedure optically introduces a bias offset to the control circuit and its control of the orientation
30 of the beam steering assembly. Alternatively, an offset can be introduced electronically in the servo controller. However introduced, the offset should be large

enough to prevent, or at least minimize, propagation of spurious reflections back to the laser source over the typical range of orientations exercised by the beam steering element in response to changes in the angular orientation or position of the measurement object.

5 Embodiments of the interferometry system having one or more beam steering assemblies can also be used to measure the angular orientation of a measurement object, in addition to measuring changes in displacement to the measurement object. To measure angular orientation of, e.g., a stage mirror, the interferometry system includes multiple displacement measuring interferometers that are "stacked" to
10 measure distance to multiple, spatially separated locations on the stage mirror, from which the angular orientation of the stage mirror can be determined. For example, the distance from a reference plane to each of three non-collinear points on the stage mirror completely defines the position and angular orientation of the stage mirror. The interferometry system can include a beam steering assembly that directs beam(s)
15 into and/or out of the stacked set of interferometers. Alternatively, the interferometry system can include a common beam steering assembly that directs at least one of the measurement and reference beams for each of the stacked set of interferometers. FIGS. 17a-c illustrates such an embodiment for two stacked interferometers. In either case, the angle information obtained by the interferometry system can be used to
20 provide a control loop for orienting the beam steering element in the beam steering assembly.

 The interferometer 1710 of FIGS. 17a-c is similar to that of FIG. 15a described above except that retroreflector 1532 is replaced with a composite retroreflector 1732 (as illustrated in FIG. 17b) and that the system further includes a
25 splitting rhomb 1713 (as illustrated in FIG. 17c) connected to polarizing beam splitter 1512. As shown in FIG. 17c, splitting rhomb 1713 receives input beam 1514 and separates it into two intermediate beams 1715a and 1715b. Splitting rhomb 1713 contains a non-polarizing beam splitting surface 1717a to split the input beam 1514 and a reflective surface 1717b to redirect intermediate beam 1715b parallel to
30 intermediate beam 1715a. FIG. 17c is in a plane perpendicular to that of FIG. 17a and containing input beam 1514.

Polarizing beam splitter **1512** separates intermediate beams **1715a** and **1715b** into reference beams **1716a** and **1716b** (dotted line) and measurement beams **1718a** and **1718b** (solid line), which are linearly polarized orthogonal to one another. FIG. **17a** illustrates only one set of reference and measurement beams with the other set propagating parallel to the first set in a second plane parallel to that of FIG. **17a**. Subsequent description of the reference and measurement beams will refer to both sets simultaneously as beams **1716** and **1718** unless otherwise specified.

Polarizing beam splitter **1512** directs the measurement beams **1718** to beam steering assembly **1520**, which directs the measurement beams through composite reference retroreflector **1732**. The composite reference retroreflector is truncated so that beams passing centrally through it are not retroreflected. As a result, beam steering assembly **1520** directs measurement beams **1718** to contact a stage mirror **1534**, *i.e.*, the measurement object, at substantially normal incidence. Stage mirror **1534** then reflects the measurement beams back to retrace their paths to beam steering assembly **1520** and polarizing beam splitter **1512**. The measurement beams double passes a quarter wave plate **1536**, which is positioned between the beam steering assembly **1520** and polarizing beam splitter **1512** and which rotates their linear polarizations by 90°.

Polarizing beam splitter **1512** directs the reference beams **1716** to beam steering assembly **1520**, which in turn directs the reference beams to composite reference retroreflector **1732**. The composite reference retroreflector then directs the reference beams back to beam steering assembly **1520** and onto polarizing beam splitter **1512**. The reference beams also double passes quarter wave plate **1536**, which rotates their linear polarizations by 90°. Polarizing beam splitter **1512** then recombines polarization-rotated reference and measurement beams **1716a** and **1718a** to form output beam **1740a**, which includes overlapping exit reference and measurement beams, and recombines polarization-rotated reference and measurement beams **1716b** and **1718b** to form output beam **1740b**, which includes overlapping exit reference and measurement beams.

FIG. **17b** is a view of the system looking towards a plane perpendicular to the plane of FIG. **17a** and containing the surface of stage mirror **1534**. FIG. **17b** shows

transverse profiles of input beam **1514** on rhomb **1713**, reference beams **1716a** and **1716b** on composite reference retroreflector **1732**, measurement beams **1718a** and **1718b** on stage mirror **1534**, and output beams **1740a** and **1740b** exiting from polarizing beam splitter **1512**.

5 Beam splitter **1542** sends a portion of output beam **1740a** to detector system **1544**, which measures the difference in directions of propagation of the exit reference and measurement beams of the output beam. The detector system sends an error signal **1550** indicative of any such difference to servo controller **1530**, which sends signal **1528** to beam steering assembly **1520** to reorient the beam steering assembly in
10 response to the error signal, as described previously.

 Output beam **1740b** and the remainder of output beam **1740a** each pass through a polarizer that mixes the polarizations of their exit reference and measurement beam components. Signal processing system **1748** receives the mixed beams and determines changes in optical path length between reference beam **1716a**
15 and measurement beam **1718a** and between reference beam **1716b** and measurement beam **1718b**, as described above. Based on the changes in measured optical path length and the separation between measurement beams **1718a** and **1718b** on stage mirror **1534**, signal processing system **1748** also determines changes in the angular orientation of the stage mirror.

20 In other embodiments, the angle information determined by signal processing system **1748** can be used to produce error signal **1550** for servo controller **1530** rather than detector system **1544**. In such embodiments, therefore, beam splitter **1542** and detector system **1544** are not required.

 Moreover, in further embodiments, the beam steering assembly can be outside
25 the interferometer. One such embodiment includes an interferometry system identical to that of FIG. **15b**, except that like the embodiment of FIG. **17a**, a splitting rhomb (e.g., splitting rhomb **1713**) is attached to polarizing beam splitter **1512** to split input beam **1514** into two parallel propagating beams, and retroreflector **1532** is replaced with composite retroreflector **1732**. Because of the splitting rhomb and the composite
30 retroreflector, the interferometer produces two exit beams, just as the embodiment of FIG. **17a** produces exit beams **1540a** and **1540b**. The treatment of the exit beams is

identical to that of the embodiment of FIG. 17a in which a signal processor such as signal processor 1748 calculates angle based on signals derived from the two exit beams. Once again, in further embodiments, the angle information determined by signal processing system 1748 can be used to produce error signal 1550 for servo
5 controller 1530 rather than detector system 1544. In such embodiments, therefore, beam splitter 1542 and detector system 1544 are not required.

In further embodiments that measure displacement, angle, or both, the beam steering assembly can be used with interferometers that double pass the measurement object. Although such a double pass can passively maintain the parallelism of the exit
10 reference and measurement beams over a range of angular orientations of the measurement object, the dynamic beam steering assembly still provides many of the advantages described above. For example, the beam steering assembly can minimize the transverse displacement of the exit reference and measurement beams or the transverse displacement of components of the reference and measurement beams
15 within the interferometer caused by changes in the angular orientation or position of the measurement object. FIGS. 18a-c schematically illustrate such an embodiment.

The interferometer 1810 of FIGS. 18a-c is identical to that of FIG. 15a described above except that retroreflector 1532 is replaced with a composite retroreflector 1832 (as illustrated in FIG. 18b) and that the system further includes a
20 recirculating prism 1813 (as illustrated in FIG. 18c) connected to polarizing beam splitter 1512 to double pass the beams through the system.

Polarizing beam splitter 1512 separates input beam 1514 into reference beam 1816 (dotted line) and measurement beam 1818 (solid line) and directs the measurement beam 1818 to beam steering assembly 1520, which directs the
25 measurement beam through composite reference retroreflector 1832. The composite reference retroreflector is truncated so that beams passing centrally through it are not retroreflected. As a result, beam steering assembly 1520 directs measurement beam 1818 to contact a stage mirror 1534, *i.e.*, the measurement object, at substantially normal incidence. Stage mirror 1534 then reflects the measurement beam back to
30 retrace its path to beam steering assembly 1520 and polarizing beam splitter 1512. The measurement beam double passes a quarter wave plate 1536, which is positioned

between the beam steering assembly **1520** and polarizing beam splitter **1512** and which rotates its linear polarization by 90° .

Polarizing beam splitter **1512** directs the reference beam **1816** to beam steering assembly **1520**, which in turn directs the reference beams to composite reference retroreflector **1832**. The composite reference retroreflector then directs the reference beam back to beam steering assembly **1520** and onto polarizing beam splitter **1512**. The reference beam also double passes quarter wave plate **1536**, which rotates its linear polarization by 90° . Polarizing beam splitter **1512** then recombines polarization-rotated reference and measurement beams **1816** and **1818** to form intermediate beam **1841**.

As shown in FIG. **18c**, recirculating prism **1813** receives intermediate beam **1841** and redirects it back to polarizing beam splitter **1512** with a transverse displacement into the plane of FIG. **18a**. In particular, FIG. **18c** is in a plane perpendicular to that of FIG. **18a** and containing input beam **1514**. Thus, recirculating prism **1813** causes intermediate beam **1841** to retrace its path back through the system in a second plane parallel to that of FIG. **18a**. As a result, output beam **1840** including overlapping exit reference and measurement beams emerges from the interferometer parallel to input beam **1514** but in the second plane.

FIG. **18b** is a view of the system looking towards a plane perpendicular to the plane of FIG. **18a** and containing the surface of stage mirror **1534**. FIG. **18b** shows transverse profiles of input beam **1514** on beam splitter **1512**, reference beam **1816** on composite reference retroreflector **1832**, measurement beam **1818** on stage mirror **1534**, intermediate beam **1841** on recirculating prism **1813**, and output beam **1840** exiting from polarizing beam splitter **1512**.

The subsequent treatment of output beam **1840**, shown in FIG. **18d**, is similar to that described for output beam **1540** with reference to FIG. **15a**. In particular, beam splitter **1542** sends a first portion of output beam **1840** to a detector system **1844** and a second portion through polarizer **1545** to signal processing system **1548**. Unlike detector system **1544**, however, detector system **1844** operates in a hybrid mode. In particular, in a plane parallel to the plane of FIG. **18a**, detector system **1844** measures the change in the propagation direction the measurement beam component of output

beam 1840 relative to the reference beam component, and in a plane perpendicular to the planes of FIGs. 18a and 18b, it measures the change in position of the measurement beam component of output beam 1840 relative to the reference beam component. Alternatively, detector system 1844 can measure the propagation
5 direction and position of the measurement beam component of output beam 1840 relative to some absolute propagation direction and position, respectively. The measured change in propagation direction of the measurement beam component indicates a change in the angular orientation of stage mirror 1534 in the plane of FIG. 18a, whereas the measured change in position of the measurement beam component
10 indicates a change in the angular orientation of stage mirror 1534 within a plane perpendicular to that of FIG. 18a. Detector system 1844 sends an error signal 1550 indicative of a change in the angular orientation of the stage mirror 1534 to servo controller 1530 based on the measured changes of the measurement beam component. Servo controller 1530 then sends control signal 1528 to beam steering assembly 1512
15 to reorient beam steering element 1522 in response to the indicated change in angular orientation of stage mirror 1534.

Other double-pass embodiments can include interferometry systems that combine the beam steering assembly described above with double-pass plane mirror interferometers or double-pass differential plane mirror interferometers, such as those
20 described in C.A. Zaroni, "Differential Interferometer Arrangements for Distance and Angle Measurements: Principles, Advantages, and Applications" (*VDI Berichte Nr. 749:93-106*, 1989). Also, in other embodiments the beam steering assembly can be outside the interferometer and the interferometer can double pass the measurement beam to the measurement object. For example, in a manner similar to the
25 incorporation of recirculating prism 1813 and composite retroreflector 1832 in FIG. 18a, which allowed the interferometer to double pass the reference and measurement beams, a recirculating prism and a composite retroreflector can be added to the interferometry system of FIG. 15c to double pass the reference and measurement beams. In this latter case, the location of the recirculating prism is not between the
30 interferometer and beam steering assembly, but rather downstream of the beam

steering assembly. Alternatively, the beam steering assembly can be outside a high-stability plane-mirror interferometer as shown in FIG. 18e.

Referring to FIG. 18e, beam steering assembly 1520 directs input beam 1514 into a high-stability, plane-mirror interferometer (HSPMI) 1870 comprising a polarizing cube beam splitter 1812, a retroreflector 1882, a reference mirror 1884, and two quarter wave plates 1836 and 1837. Beam splitter 1812 has polarizing beam-splitting interface 1862. Beam splitter 1812 separates input beam 1514 into reference beam 1816 (dotted line) and measurement beam 1818 (solid line), reflecting reference beam towards reference mirror 1884 and transmitting measurement beam 1818 towards stage mirror 1534. Reference mirror 1884 reflects reference beam 1816 back to beam splitter 1812, which now transmits reference beam 1816 to retroreflector 1882 because it double passes quarter wave plate 1836. Retroreflector 1882 in turn directs reference beam 1816 back to beam splitter 1812, which transmits reference beam 1816 back towards reference mirror 1884. Once again, reference mirror 1884 reflects reference beam 1816 back to beam splitter 1812 with reference beam 1816 again double passing quarter wave plate 1836. Similarly, stage mirror 1534 reflects measurement beam 1818 back to beam splitter 1812, which now reflects measurement beam 1818 to retroreflector 1882 because it double passes quarter wave plate 1837. Retroreflector 1882 in turn directs measurement beam 1818 back to beam splitter 1812, which reflects measurement beam 1818 back towards stage mirror 1534. Once again, stage mirror 1534 reflects measurement beam 1818 back to beam splitter 1812 with measurement beam 1818 again double passing quarter wave plate 1837. Note that the reference and measurement beams between beam splitter 1812 and retroreflector 1882 are collinear but FIG. 18e depicts them as separate for clarity.

At this point, reference beam 1816 has contacted reference mirror 1884 twice, double passing it, and the measurement beam 1818 has contacted stage mirror 1534 twice, double passing it. Now, beam splitter 1812 recombines the double-passed reference and measurement beams into intermediate beam 1889, which is then directed by beam steering assembly 1520 to form output beam 1880.

The subsequent treatment of output beam 1880, shown in FIG. 18f, is similar to that described for output beam 1540 with reference to FIG. 15a. In particular, beam

splitter **1542** sends a first portion of output beam **1880** to a detector system **1884** and a second portion through polarizer **1545** to signal processing system **1548**. Unlike detector system **1544**, however, detector system **1884** measures the change in position of the measurement beam component of output beam **1840** relative to the reference beam component and not the change in propagation of direction of the measurement beam component relative to the reference beam component. This is because the double-pass in interferometer **1870** causes the measurement and reference beam components in the output beam **1840** to be parallel to one another despite a change in angular orientation of stage mirror **1534**. Such a change, however, imparts a transverse displacement to the measurement beam components of output beam **1880**. Thus, a measured change in the position of the measurement beam component of output beam **1880** along a transverse axis in the plane of FIG. **18e** indicates a change in the angular orientation of stage mirror **1534** in the plane of FIG. **18e**, and a measured change in the position of the measurement beam component of output beam **1880** along a transverse axis perpendicular to the plane of FIG. **18e** indicates a change in the angular orientation of stage mirror **1534** in a plane perpendicular to that of FIG. **18e**. In other embodiments, detector system **1884** measures changes in the position of the measurement beam component of output beam **1840** relative to some absolute position, rather than relative to the reference beam component, to determine changes in the angular orientation of stage mirror **1534**. In any case, detector system **1884** sends an error signal **1550** indicative of a change in the angular orientation of the stage mirror **1534** to servo controller **1530** based on the measured changes in the position of the measurement beam component. Servo controller **1530** then sends control signal **1528** to beam steering assembly **1512** to reorient beam steering element **1522** in response to the indicated change in angular orientation of stage mirror **1534**.

As described above, the beam steering assembly redirects the input beam to minimize the transverse displacement between the exit reference and measurement beams caused by a change in the angular orientation or position of the measurement object. As a consequence, the beam steering assembly also reduces transverse displacements of beam components within the interferometer caused by a change in the angular orientation or position of the measurement object. As shown in FIG. **18e**,

the beam steering assembly may also be positioned to redirect the output beam to compensate for the angular deviation of the output beam as a whole caused by the beam steering element's redirection of the input beam. In additional embodiments, however, such compensation is not necessary.

5 In other embodiments, rather than determining the control signal for the beam steering assembly based on a portion of the output beam, the control signal can be determined from a measurement beam component within the interferometer.

Furthermore, in additional embodiments, multiple double-pass interferometers such as those shown in FIGS. **18a-f** can be used to provide interferometric angle
10 information about the orientation of the measurement object in a manner similar to the stacked interferometer embodiments described above with reference to FIGS. **17a-c**. Moreover, in such embodiments the interferometric angle information may be used to produce the control signal for orienting the beam steering element.

FIG. **20** shows an apparatus including a multi-axis interferometry system **2000**
15 for providing interferometric angle information about the orientation of a measurement object **2010** and a beam steering assembly **2020** for directing an input beam **2002** into the multi-axis interferometry system based on the interferometric angle information.

Beam steering assembly **2020** includes a beam steering mirror **2022** and a pair
20 of piezoelectric transducers **2024** and **2026**. The transducers are coupled to the beam steering mirror **2020** by flexures to orient the beam steering mirror in response to a signal **2028** from a servo controller **2030**. The beam steering assembly may include capacitance gauges to measure changes in orientation and/or position of the beam steering mirror. The capacitance gauges may also be used to measure and/or monitor
25 the properties of the piezoelectric transducers.

Input beam **2002** contacts beam steering mirror **2022**, which redirects it into multi-axis interferometry system **2000**. In the presently described embodiment the input beam includes orthogonal polarization components having a frequency splitting suitable for heterodyne interferometry. Multi-axis interferometer **2000** includes two
30 high stability plane mirror interferometers (HSPMI) **2040** and **2042**, like that shown in FIG. **18e**, and a pair of penta-prisms **2044** and **2046** for directing a portion of the input

beam to each of interferometers **2040** and **2042**. Penta-prism **2044** includes a non-polarizing beam splitting surface **2045** to allow a first portion **2004** of the input beam to transmit to interferometer **2040** and reflect a second portion **2006** of the input beam to penta-prism **2042**, which in turn directs the second portion of the input beam to
5 interferometer **2042**. The penta-prisms are positioned to maintain the first and second portions of the input beam parallel to one another as they enter their respective interferometers **2040** and **2042** even as the beam steering assembly changes the propagation direction of the input beam.

In other embodiments, penta-prisms **2044** and **2046** can be replaced with a
10 polarizing beam-splitter surface and a mirror, respectively, which are oriented parallel to one another to likewise maintain the first and second portions of the input beam parallel to one another as they enter their respective interferometers **2040** and **2042** even as the beam steering assembly changes the propagation direction of the input beam.

15 Interferometer **2040** separates input beam portion **2004** into a measurement beam and a reference beam (not shown), and directs the measurement beam **2041** to make two passes to the measurement object **2010** (which, for example, is a plane mirror attached to a lithography stage). Thereafter, interferometer **2040** recombines the reflected measurement beam with the reference beam to produce an output beam
20 including interferometric information indicative of changes in distance to the measurement object along the measurement axis defined by interferometer **2040**.

Similarly, interferometer **2042** separates input beam portion **2006** into a measurement beam **2043** and a reference beam (not shown), and directs the measurement beam **2043** to make two passes to the measurement object **2010** (which,
25 for example, is a plane mirror attached to a lithography stage). Thereafter, interferometer **2043** recombines the reflected measurement beam with the reference beam to produce an output beam including interferometric information indicative of changes in distance to the measurement object along the measurement axis defined by interferometer **2042**.

30 Interferometer **2040** is oriented to direct measurement beam **2041** to propagate parallel to input beam portion **2004** during its first pass to the measurement object.

Similarly, interferometer **2042** is oriented to direct measurement beam **2043** to propagate parallel to input beam portion **2006** during its first pass to the measurement object. Thus, beam steering assembly **2020** can redirect input beam **2002** to cause both measurement beams **2041** and **2043** to contact the measurement object at substantially normal incidence over a range of angular orientations of the measurement object in the plane of the of FIG. **20**. As described above, such normal incidence can reduce lateral shear between the reference and measurement beams within the interferometer and the lateral shear between the reference and measurement beam components of the output beams.

In the presently described embodiment, interferometers **2040** and **2042** each include polarizer (not shown) to mix the reference and measurement beam components of the output beam to produce a signal beam having a heterodyne intensity component whose phase corresponds to distance changes to the measurement object. Optical fibers **2050** and **2052** respectively carry the signal beam from each interferometer to corresponding detectors **2051** and **2053**. In other embodiments, optical fibers are not used and the detectors are positioned proximate to the interferometers to directly measure the intensities of the signal beams.

A signal processor **2060** is coupled to the detectors and determines changes in the angular orientation of the measurement object in the plane of FIG. **20** based on the distance information from each signal beam and the separation between the measurement axes of interferometers **2040** and **2042** (which is shown as distance "A" in FIG. **20**). Signal processor then sends a servo control signal **2062** based on the changes in angular orientation to servo controller **2030**, which in turn causes one or both transducers **2024** and **2026** to orient the beam steering mirror **2022** to cause the measurement beams **2041** and **2043** to contact the measurement object at substantially normal incidence.

The embodiment of FIG. **20** can be extended to address changes in the angular orientation of the measurement object out of the plane of FIG. **20** (i.e., about an axis corresponding to the distance arrow "A") by replacing HSPMI interferometer **2040** with a stacked HSPMI interferometer that separates input beam portion **2004** into two pairs of measurement and reference beams, and directs the additional measurement

beam to contact the measurement object above (or below) the plane of the FIG. 20 and recombines that measurement beam with its corresponding reference beam to produce a third output beam indicative of change of distance to the measurement object about a third metrology axis. This third output beam can be processed in the same manner
5 as the other output beams, which all together provide information about changes in distance, pitch, and yaw of the measurement object relative to the interferometry system. The latter two quantities can be used to orient the beam steering mirror in two dimensions to maintain the three measurement beams substantially normal to the measurement object despite changes in its angular orientation in both pitch and yaw.

10 Furthermore, in additional embodiments, additional portions of the input beam can be used to provide additional metrology axes which may also be used to control the servo loop for beam steering assembly 2020 or additional beam steering elements. For example, for applications in which the measurement object is a stage that moves along multiple dimensions, the multi-axis interferometry system can provide
15 metrology axes to multiple sides of the stage. Furthermore, in such embodiments, the multi-axis interferometry system may be stationary relative to the movable stage. Alternatively, the multi-axis interferometry system can be supported by the movable stage and the measurement object can defined a fixed reference frame (e.g., an L-shaped mirror). See, e.g., U.S. Patent 5,757,160 to Kreuzer, the contents of which are
20 incorporated herein by reference. Furthermore, in additional embodiments, interferometers 2040 and 2042 can be replaced with different types of interferometers, e.g., single-pass interferometers or other types of double-pass interferometers, including any of those described above. Moreover, rather than having separate interferometers providing different axes of metrology, an integral multi-axis
25 interferometer may be used. See, e.g., U.S. Patent No. 5,064,289 to Bockman and U.S. Patent 4,883,357 to Zaroni, the contents of which are incorporated herein by reference.

In yet further embodiments, the interferometry system that provides information about the angular orientation of the measurement object can include an
30 angle-measuring interferometer that directs two beams to contact different locations of the measurement object and combines those beams after they contact measurement

object to provide an output beam that directly includes interferometric information about the angular orientation of the measurement object. Such information can be used to generate the control signal to the dynamic beam steering element, which may be positioned to redirect one or both of the beams in the angle-measuring
5 interferometer, another measurement beam in the interferometer (e.g., if the angle-measuring interferometer is part of multi-axis interferometer), or an input beam into the interferometer, wherein the beams that contact the measurement object are derived from the input beam.

Such an embodiment is shown in FIG. 21. Source 2302 provides an input
10 beam 2310, which includes orthogonally polarized components having a heterodyne frequency splitting as described previously. Input beam 2310 is incident on, and is redirected as input beam 2312 by, a dynamic beam steering assembly, which includes beam steering mirror 2314 and transducers 2316 and 2318 for dynamically orienting mirror 2314 in response to a control signal 2304 from a controller 2311. As described
15 in previous embodiments, controller 2311 generates control signal 2304 to orient beam steering mirror 2314 in response to changes in the angular orientation of a measurement object 2380. In the present embodiment, controller 2311 generates the control signal based on intensity information 2313 measured by a detector 2376 of an angle-measuring output beam 2378 produced by an interferometry system 2306.

20 Still referring to FIG. 21, interferometry system 2306 functions as follows. A non-polarizing beamsplitter 2320 splits input beam 2312 into an angle-measuring input beam 2382 and a distance-measuring input beam 2384. The distance-measuring portion of the interferometry system involves a high-stability plane mirror interferometer (HSPMI). The angle-measuring portion of the interferometry system
25 directs angle-measuring beams to make single-passes to different points on the measurement object to produce an angle-measuring output beam based on optical differencing. As will be described in further detail below, the angle-measuring portion of the interferometry system shares a number of components with the distance-measuring HSPMI portion to produce an integrated system providing
30 multiple measurement axes.

Referring still to FIG. 21, non-polarizing beamsplitter 2320 reflects distance-measuring input beam 2384 (via mirror 2331) to polarizing beamsplitter 2330, which splits it into two distance-measuring beams: a reflected reference beam 2395 and a transmitted measurement beam 2391. Reference beam 2395 then reflects from reference mirror 2338 and is then transmitted by polarizing beam splitter 2330 to retroreflector 2332 following a double pass through quarter wave plate 2336. Retroreflector 2332 then directs reference beam 2395 back to polarizing beamsplitter 2330, which transmits it back to reference mirror 2338, which in turn reflects it back to the polarizing beamsplitter after another double pass through quarter-wave plate 2336. Because of the double pass through the quarter-wave plate, polarizing beam splitter 2330 now reflects the reference beam as a reference beam component of a distance-measuring output beam 2374. Measurement beam 2391 reflects from measurement mirror 2380 and is then reflected by polarizing beam splitter 2330 to retroreflector 2332 following a double pass through quarter wave plate 2334. Retroreflector 2332 then directs measurement beam 2391 back to polarizing beamsplitter 2330, which reflects it back to measurement mirror 2380, which in turn reflects it back to the polarizing beamsplitter after another double pass through quarter-wave plate 2334. Because of the double pass through the quarter-wave plate, polarizing beam splitter 2330 now transmits the measurement beam as a measurement beam component of a distance-measuring output beam 2374.

Thus, following the double pass of measurement beam 2391 to measurement object 2380 and the double pass of reference beam 2395 to reference object 2338, polarizing beamsplitter 2330 recombines measurement and reference beams 2391 and 2395, respectively, to form distance-measuring output beam 2374. A polarizer 2371 mixes the polarization components of the distance-measuring output beam before it impinges on detector 2372. The phase of the distance-measuring output beam is derived from the measurement by detector 2372 and used to determine linear displacements of the plane mirror object along a measurement axis X_1 .

Non-polarizing beamsplitter 2320 transmits angle-measuring input beam 2382 to polarizing beamsplitter 2330, which separates angle-measuring input beam 2382 into angle-measuring beams 2393 and 2394. Polarizing beamsplitter 2330 transmits

angle-measuring beam 2393, which is then reflected by plane mirror measurement object 2380. After double passing quarter-wave plate 2334, angle-measuring beam 2393 returns to polarizing beamsplitter 2330, which reflects it as a first component of an intermediate beam 2390. Polarizing beamsplitter 2330 reflects beam 2394, which is then reflected by plane mirror reference object 2338. After double passing quarter-wave plate 2336, angle-measuring beam 2394 returns to polarizing beamsplitter 2330, which transmits it as a second component of an intermediate beam 2390.

Intermediate beam 2390 then makes three respective reflections from mirrors 2347, 2348, and 2349, which direct the intermediate beam back to polarizing beamsplitter 2330, which in turn separates the intermediate beam back into beams 2393 and 2394. Before reaching polarizing beamsplitter 2330, however, intermediate beam 2390 passes through half-wave retardation plate 2350, which rotates the linear polarizations of the components of the intermediate beam by 90 degrees. Because of the polarization rotation, polarizing beamsplitter 2330 subsequently reflects angle-measuring beam 2394 to plane mirror measurement object 2380 and transmits angle-measuring beam 2393 to plane mirror reference object 2338. Following reflections of beams 2394 and 2393 from the measurement and reference objects 2380 and 2338, respectively, and double-passes through quarter-wave plates 2334 and 2336, respectively, polarizing beamsplitter 2330 recombines the angle-measuring beams as components of angle-measuring output beam 2378. Accordingly, beams 2393 and 2394 are recombined to form angle-measuring output beam 2378 after they each contact the plane mirror measurement object a single time at different points. A polarizer 2375 mixes the polarization components of angle-measuring output beam 2378 before it impinges on detector 2376.

Components including retroreflector 2332, mirrors 2347, 2348, and 2349, and half-wave retardation plate 2350 collectively define a return beam optical assembly 2351 that returns distance-measuring beams 2391 and 2395 back to polarizing beam-splitter 2330 between their first and second passes to the measurement and reference objects, respectively, and returns angle-measuring beams 2393 and 2394 back to polarizing beam-splitter 2330 after their pass to the measurement and reference

objects, respectively, and before their pass to the reference and measurement objects, respectively.

Because each angle-measuring beam contacts the measurement object once, any angular deviation introduced by a tilt in measurement object **2380** will effect both components, and hence the beam components remain parallel at the output of the angular displacement interferometer. Furthermore, the angle-measuring output beam includes a relative phase shift φ_1 that is related to an angular change of the measurement object, θ_1 (relative to the propagation direction of input beam **2312**), according to the formula $\varphi_1 = 2k_1 n_1 b_1 \theta_1$ where b_1 is the spacing between beams **2393** and **2394** at the plane mirror measurement object, wavenumber $k_1 = 2\pi/\lambda_1$ for wavelength λ_1 of the input beam **2310**, and n_1 is the index of refraction of a gas in the beam paths.

The return mirror system fold system including the three mirrors, **2347**, **2348**, and **2349** for redirecting angle measuring beams **2393** and **2394** (when they are components of intermediate beam **2390**) back to polarizing beam splitter **2330** ensures that both components in angle-measuring output beam **2378** are parallel.

One advantage of the angle-measuring portion of interferometry system **2306** is that the differential beam shear of the components of the angle-measuring output beam at a detector or fiber-optic pickup (FOP) is substantially reduced compared for example to the differential beam shear in the output beam at the detector or FOP of the HSPMI. This is because both components of the angle-measuring output beams (i.e., angle-measuring beams **2393** and **2394**) undergo substantially equal amounts of shear upon a non-normal reflection from the measurement plane mirror and subsequent propagation back to the interferometer.

In yet further embodiments, interferometry system **2306** can be replaced with other interferometry system that include angle-measuring interferometers, such as those disclosed in commonly owned application U.S. Patent Application Serial No. 10/351,708 entitled "Multi-Axis Interferometer" by Henry A. Hill and filed January 27, 2003, the contents of which are incorporated by reference. Also in further embodiments, the dynamic beam steering element may be positioned to direct one of

the beams within the angle measuring interferometer (e.g., one or both of the beams that contact the measurement object).

In any of the interferometry systems described above, the input, reference, measurements, intermediate, and output beams can include multiple, well-separated wavelengths to measure dispersion along the measurement path to the measurement object. The well-separated wavelengths can come from, for example, fundamental and frequency-doubled wavelengths of a laser, e.g., fundamental and doubled Nd:Yag at 1064 and 532 nm or doubled and quadrupled Nd:Yag at 532 and 266 nm. One such source is a Helium-Neon laser light source as described in U.S. Patent Application No 09/305,808 entitled "Helium-Neon Laser Light Source Generating Two Harmonically Related, Single-Frequency Wavelengths for Use in Displacement and Dispersion Measuring Interferometry" by William A. Shull and Carl A. Zaroni filed April 28, 1999, the contents of which are incorporated herein by reference. The measurement of changes in optical path length to the measurement object at multiple wavelengths can be used to correct the displacement measurement for air turbulence along the measurement path and convert the optical path length change to a geometric path length change.

FIGS. 19a-b schematically illustrate a displacement and dispersion interferometry system. A laser light source 1980 generates a light beam 1981 that is a coextensive superposition of two beams having well-separated, single-frequency wavelengths λ_1 and λ_2 . The ratio of the wavelengths (λ_1/λ_2) has a known value that can be expressed, at least approximately, as l_1/l_2 where l_1 and l_2 are integers. In some embodiments, the two-wavelengths are harmonically related. A dichroic beam splitter 1983 splits superposed beam 1981 into two single-wavelength beams 1982 and 1988, beam 1982 at wavelength λ_1 and beam 1988 at λ_2 . Beam 1982 passes through a first acousto-optical modulation system 1993 powered by driver 1995 to become beam 1999. Similarly, beam 1988, after being redirected by mirror 1989, passes through a second acousto-optical modulation system 1994 powered by driver 1996 to become beam 1990. Acousto-optical modulation systems 1993 and 1994

each produce a frequency splitting between orthogonal linear polarization components of beams 1999 and 1990, respectively.

In particular, acousto-optical modulation system 1993 shifts the optical frequency of the x-polarization component of beam 1982 by an amount f_1 with respect to its y-polarization component to produce beam 1999. Similarly, acousto-optical modulation system 1994 shifts the optical frequency of the x-polarization component of beam 1988 by an amount f_2 with respect to its y-polarization component to produce beam 1990. In this description, the z-axis is collinear with the propagation direction of the beam, the x-axis is in the plane of FIG. 19a perpendicular to the z-axis, and the y-axis is perpendicular to the plane of FIG. 19a. The values of the frequency shifts f_1 and f_2 are determined by drivers 1995 and 1996, respectively, and are many orders of magnitudes smaller (e.g., about 10^{-7} smaller) than the optical frequencies defined by λ_1 and λ_2 . Acousto-optical modulation systems 1993 and 1994 each include at least one acousto-optical modulator and one or more additional optical elements such as a prism and a birefringent element. Suitable acousto-optical modulation systems are described by G.E. Sommargren in U.S. Patent Nos. 4,684, 828 and 4,687,958, and by H.A. Hill in U.S. Patent Application No. 09/061,928 filed 4/17/98, the contents of all of which are incorporated herein by reference. The frequency splittings produced by the acousto-optical modulation systems permit the use of heterodyne interferometry techniques. Other frequency splitting techniques known in the art can also be used to produce heterodyne frequency splittings. Alternatively, in other embodiments, homodyne interferometry techniques can be used in which case the frequency splittings are not necessary.

In some embodiments, either or both of acousto-optical modulation systems 1993 and 1994 can additionally introduce a frequency offset to both polarization components of beams 1982 and 1988, respectively. For example, acousto-optical modulation system 1993 can shift the x-polarization component of beam 1982 by f_0 and its y-polarization component by $f_0 + f_1$, and acousto-optical modulation system 1994 can shift the x-polarization component of beam 1988 by f_0' and its y-

polarization component by $f_0' + f_2$. The frequency offsets can improve isolation between source 1980 and the interferometer downstream.

Beam 1999 is directed by mirror 1912 to dichroic beam splitter 1914, which combines beams 1999 and beam 1990 into beam 1920. Beam 1920 thus comprises
 5 frequency-shifted orthogonal polarization components at λ_1 and frequency-shifted orthogonal polarization components at λ_2 , all of which are substantially coextensive and collinear. Beam-shaping optics 1910 modify the transverse spatial profile of beam 1999 so that the components of beam 1920 at λ_1 have similar diameters and, more particularly, similar transverse intensity profiles as those of the components of
 10 beam 1920 at λ_2 . In other embodiments, beam-shaping optics 1910 can be positioned either before or after the acousto-optical modulation systems and can vary the beam at λ_1 or the beam at λ_2 where ever they are separated from one another. Suitable beam-shaping optics include, for example, beam expanders, beam compressors, variable density filters, and apodizing masks. Such elements can be used separately or in
 15 combination to produce the similar transverse intensity profiles.

Beam 1920 is directed into an interferometer unit 1960 that includes an interferometer and a beam steering assembly, as described in any of the embodiments above. Interferometer unit 1960 produces exit beam 1915 comprising an overlapping pair of exit reference and measurement beams at each of two wavelengths λ_1 and λ_2 .
 20 As described above, the dynamic control system in interferometry unit 1960 reduces the consequences of changes in angular orientation or position of the measurement object on exit beam 1915. The separate reference and measurement paths in interferometry unit 1960 a phase shift ϕ_1 between the x-polarized and y-polarized components of exit beam 1915 at wavelength λ_1 and introduces a phase shift ϕ_2
 25 between the x-polarized and y-polarized components of exit beam 1915 at wavelength λ_2 . An expression for the phase shifts is given by:

$$\phi_j = Lpk_j n_j + \zeta_j, \quad \text{where } j=1 \text{ or } 2, \quad (3)$$

where L is the round trip distance traversed by measurement beam 1918, p is the number of round-trip passes in the interferometer ($p = 1$ for the presently described interferometer), n_j is the average refractive index of gas 1998 at wavenumber $k_j = (2\pi)/\lambda_j$, and ζ_j is a phase-offset for wavelength λ_j , which includes all contributions to the phase shifts ϕ_j that are not related to the path traversed by measurement beam 1918. Because the components of measurement beam 1918 at wavelengths λ_1 and λ_2 traverse the same geometric distance L but experience different refractive indices n_1 and n_2 , the phases ϕ_j can be used to determine dispersion in along the measurement path to the measurement object.

Polarizer 1944 (oriented, e.g., at 45 degrees to the plane of the FIG. 19a) mixes the x- and y-polarization components of exit beam 1915 at each of wavelengths λ_1 and λ_2 to produce a mixed beam 1919. A dichroic beam splitter 1980 then separates mixed beam 1919 into a first signal beam 1917 at wavelength λ_1 and a second signal beam 1918 at wavelength λ_2 . Photoelectric detectors 1985 and 1986 measure the time-varying intensities of signal beams 1917 and 1918, respectively, to produce interference, heterodyne signals s_1 and s_2 , respectively. The signals s_j have the form

$$s_j = A_j \cos[\alpha_j(t)] \quad , \quad j = 1 \text{ and } 2, \quad (4)$$

where the time-dependent arguments $\alpha_j(t)$ are given by

$$\alpha_j(t) = 2\pi f_j t + \phi_j \quad , \quad j = 1 \text{ and } 2, \quad (5)$$

Heterodyne signals s_1 and s_2 are transmitted to processing system 1909 for analysis as electronic signals 1903 and 1904, respectively, in either digital or analog format. Processing system 1909 also receives electronic signals 1901 and 1902 from drivers

1995 and 1996, respectively, indicative of their respective driving frequencies (e.g., heterodyne split frequencies f_1 and f_2) and phases.

Referring to FIG. 19b, processing system 1909 further includes electronic processors 1094A and 1094B to determine the phases ϕ_1 and ϕ_2 , respectively.

5 Processor 1094A determines ϕ_1 based on signal 1903 (s_1) and signal 1901 (heterodyne reference phase at f_1 for driver 1995), and processor 1094B determines ϕ_2 based on signal 1904 (s_2) and signal 1902 (heterodyne reference phase at f_2 for driver 1996). The processors can use either digital or analog signal processing techniques, including, e.g., time-based phase detection such as a digital Hilbert
10 transform phase detector. See, e.g., section 4.1.1 of R.E. Best, "Phase-locked loops: theory, design, and applications" 2nd ed. (McGraw-Hill, New York, 1993). In other embodiments, signals 1901 and 1902 can be derived from mixed reference phase beams produced by mixing the polarization components of a portion of each of beams 1999 and 1990, respectively.

15 Phases ϕ_1 and ϕ_2 determined by processors 1094A and 1094B are next multiplied by l_1/p and l_2/p , respectively, in electronic processors 1095A and 1095B, respectively, preferably by digital processing, resulting in phases $(l_1/p)\phi_1$ and $(l_2/p)\phi_2$, respectively. The phases $(l_1/p)\phi_1$ and $(l_2/p)\phi_2$ are next added together in electronic processor 1096A and subtracted one from the other in electronic processor
20 1097A, preferably by digital processes, to create the phases Θ and Φ , respectively. Formally,

$$\Theta = \left(\frac{l_1}{p} \phi_1 + \frac{l_2}{p} \phi_2 \right) \quad , \quad (6)$$

$$\Phi = \left(\frac{l_1}{p} \phi_1 - \frac{l_2}{p} \phi_2 \right) \quad . \quad (7)$$

25

Referring again to FIG. 19a, the phases ϕ_1 , Θ , and Φ are transmitted to computer 1910 as signal 1905, in either digital or analog format.

The refractivity of the gas in the measurement path to the measurement object, $(n_1 - 1)$, can be calculated using the formula

$$n_1 - 1 = \frac{\Gamma}{\chi L [1 - (K/\chi)^2]} \left\{ [\Im(K/\chi) - \Phi] - Q \right\} \quad , \quad (8)$$

5

where

$$\chi = (l_1 k_1 + l_2 k_2) / 2 \quad , \quad (9)$$

10

$$K = (l_1 k_1 - l_2 k_2) / 2 \quad , \quad (10)$$

$$\Gamma = \frac{n_1 - 1}{n_2 - n_1} \quad , \quad (11)$$

the quantity Γ being the reciprocal dispersive power of the gas which is substantially independent of environmental conditions and turbulence in the gas. The offset term Q is defined as

15

$$Q = \xi(K/\chi) - Z \quad , \quad (12)$$

20 where

$$\xi = \left(\frac{l_1}{p} \zeta_1 + \frac{l_2}{p} \zeta_2 \right) \quad , \quad (13)$$

$$Z = \left(\frac{l_1}{p} \zeta_1 - \frac{l_2}{p} \zeta_2 \right) \quad . \quad (14)$$

25

Values of Γ may be computed from knowledge of the gas composition and from knowledge of the wavelength dependent refractivities of the gas constituents. For example, for the wavelengths λ_1 equal to 632.8 nm and λ_2 equal to 316.4 nm, Γ equals about 21.4.

5 For those applications related to displacement measuring interferometry, the heterodyne phase ϕ_1 and phases ϑ and Φ may be used to determine the geometric distance L , independent of the effects of the refractive index of gas 1998 in the measurement path, using the formula:

$$10 \quad L = \frac{1}{(\chi + K)} \left\{ \frac{l_1}{p} (\phi_1 - \zeta_1) - \frac{\Gamma}{[1 - (K/\chi)]} [(K/\chi)\vartheta - \Phi - \mathcal{Q}] \right\} . \quad (15)$$

The ratio of the wavelengths can be expressed in terms of (K/χ) from Eqs. (9) and (10) with the result

$$15 \quad \frac{\lambda_1}{\lambda_2} = \left(\frac{l_1}{l_2} \right) \left[\frac{1 - (K/\chi)}{1 + (K/\chi)} \right] . \quad (16)$$

When operating under the condition

$$|K/\chi| \ll \frac{(n_2 - n_1)}{(n_2 + n_1)} , \quad (17)$$

20

the ratio of the phases Φ and ϑ has the approximate value

$$(\Phi/\vartheta) \cong - \frac{(n_2 - n_1)}{(n_2 + n_1)} . \quad (18)$$

Where ε is the relative precision desired for the measurement of the refractivity of the gas or of the change in the optical path length of the measurement leg due to the gas, and the following inequality applies:

$$5 \quad \left| \frac{\lambda_1}{\lambda_2} - \frac{l_1}{l_2} \right| \ll \left(\frac{l_1}{l_2} \right) (n_2 - n_1) \varepsilon \quad , \quad (19)$$

Eqs. (8) and (15) reduce to more simple forms of

$$n_1 - 1 = -\frac{\Gamma}{\chi L} (\Phi + Q) \quad , \quad (20)$$

10

$$L = \frac{1}{\chi} \left[\frac{l_1}{p} (\phi_1 - \zeta_1) + \Gamma (\Phi + Q) \right] \quad , \quad (21)$$

respectively. Using the equations above, computer **1910** calculates $(n_1 - 1)$, L , and/or changes in L based on signal **1905** from processing system **1909**. Similar
15 calculations for L can also be performed with respect to n_2 .

In the presently described embodiment, interferometer unit **1960** receives input beam **1920** and produces exit beam **1915**, each of which include both wavelengths λ_1 and λ_2 . In other embodiments, the interferometer unit can include polarizer **1944** and dichroic beam splitter **1980** to directly produce signal beams **1917** and **1918**. Also,
20 rather than mixing polarizations of exit beam **1915** when it includes both wavelengths λ_1 and λ_2 , the interferometer unit can split beam **1915** into beams having either wavelength λ_1 or wavelength λ_2 , and then mix the polarizations of each of the split beams to produce signal beams **1917** and **1918**. Furthermore, in other embodiments, the interferometer unit can include dichroic beam splitter **1914** to combine two input
25 beams at wavelengths λ_1 and λ_2 , respectively, into one input beam at both wavelengths. Also, the interferometer unit can receive separate input beams at wavelengths λ_1 and λ_2 , respectively, and include one or more dichroic beam splitters

to separate each of the input beams into reference and measurement beams at their respective wavelengths. In the latter case, the interferometer unit directs the measurement beams at wavelengths λ_1 and λ_2 along a common path contacting the measurement object, and then recombine each of the measurement beams with its
5 respective reference beam.

FIG. 19c schematically illustrates such an interferometer unit 1961. Polarizing beam splitter 1948a separates input beam 1950a at wavelength λ_1 into reference beam 1952a and measurement beam 1954a, both at wavelength λ_1 . Similarly, polarizing beam splitter 1948b separates input beam 1950b at wavelength λ_2 into
10 reference beam 1952b and measurement beam 1954b, both at wavelength λ_2 . For example, input beams 1950a and 1950b can be beams 1990 and 1999, respectively, from FIG. 19a. Polarizing beam splitters 1948a and 1948b have polarizing beam splitting surfaces 1961a and 1961b, respectively, and reflective surfaces 1962a and 1962b, respectively. Dichroic beam splitter 1956 combines reference beams 1952a
15 and 1952b into reference beam 1962 having both wavelengths λ_1 and λ_2 , and combines measurement beams 1954a and 1954b into measurement beam 1964 having both wavelengths λ_1 and λ_2 . Reference beams 1952a, 1952b, and 1962 are depicted as dashed lines in FIG. 19c, whereas measurement beams 1954a, 1954b, and 1964 are depicted as solid lines in FIG. 19c.

20 Reference beam 1962 and measurement beam 1964 propagate to beam steering assembly 1520, which directs reference beam to retroreflector 1532 and measurement beam to stage mirror 1534. Retroreflector 1532 and stage mirror 1534 reflect the reference and measurement beam, respectively, back to beam steering assembly 1520, which redirects the beams back to dichroic beam splitter 1956. Dichroic beam splitter
25 1956 then separates reference beam 1962 back into reference beams 1952a and 1952b having wavelengths λ_1 and λ_2 , respectively, and separates reference beam 1964 back into measurement beams 1954a and 1954b having wavelengths λ_1 and λ_2 , respectively. Reference and measurement beams 1952a and 1954a then propagate to polarizing beam splitter 1948a, where because they doubled pass quarter wave plate

1968a, polarizing beam splitter 1948a recombines them to form exit beam 1970a having wavelength λ_1 . Similarly, reference and measurement beams 1952b and 1954b then propagate to polarizing beam splitter 1948b, where because they doubled pass quarter wave plate 1968b, polarizing beam splitter 1948b recombines them to
5 form exit beam 1970b having wavelength λ_2 . A portion of one of exit beams 1970a and 1970b is sent to a detector system (not shown) such as detector system 1544 to generate a control signal that causes beam steering assembly 1512 to redirect reference and measurement beams 1962 and 1964 in response to changes in the angular orientation of stage mirror 1534. The description of such a control system is identical
10 that described previously with reference to the embodiment of FIG. 15a.

Exit beams 1970a and 1970b are indicative of changes in optical path length to stage mirror 1534 at wavelengths λ_1 and λ_2 , respectively, from which dispersion along the measurement path to the stage mirror can be determined. In particular, a polarizer can be used to mix the reference and measurement beam components of each
15 of the exit beams to produce signal beams 1917 and 1918, described above with reference to FIG. 19a.

The interferometry systems described above can be especially useful in lithography applications that fabricate large-scale integrated circuits such as computer chips and the like. Lithography is the key technology driver for the semiconductor
20 manufacturing industry. Overlay improvement is one of the five most difficult challenges down to and below 100 nm line widths (design rules), see for example the *Semiconductor Industry Roadmap*, p82 (1997). Overlay depends directly on the performance, *i.e.* accuracy and precision, of the distance measuring interferometers used to position the wafer and reticle (or mask) stages. Since a lithography tool may
25 produce \$50-100M/year of product, the economic value from improved performance distance measuring interferometers is substantial. Each 1% increase in yield of the lithography tool results in approximately \$1M/year economic benefit to the integrated circuit manufacturer and substantial competitive advantage to the lithography tool vendor.

The function of a lithography tool is to direct spatially patterned radiation onto a photoresist-coated wafer. The process involves determining which location of the wafer is to receive the radiation (alignment) and applying the radiation to the photoresist at that location (exposure).

5 To properly position the wafer, the wafer includes alignment marks on the wafer that can be measured by dedicated sensors. The measured positions of the alignment marks define the location of the wafer within the tool. This information, along with a specification of the desired patterning of the wafer surface, guides the alignment of the wafer relative to the spatially patterned radiation. Based on such
10 information, a translatable stage supporting the photoresist-coated wafer moves the wafer such that the radiation will expose the correct location of the wafer.

During exposure, a radiation source illuminates a patterned reticle, which scatters the radiation to produce the spatially patterned radiation. The reticle is also referred to as a mask, and these terms are used interchangeably below. In the case of
15 reduction lithography, a reduction lens collects the scattered radiation and forms a reduced image of the reticle pattern. Alternatively, in the case of proximity printing, the scattered radiation propagates a small distance (typically on the order of microns) before contacting the wafer to produce a 1:1 image of the reticle pattern. The radiation initiates photo-chemical processes in the resist that convert the radiation
20 pattern into a latent image within the resist.

The interferometry systems described above are important components of the positioning mechanisms that control the position of the wafer and reticle, and register the reticle image on the wafer.

In general, the lithography system, also referred to as an exposure system,
25 typically includes an illumination system and a wafer positioning system. The illumination system includes a radiation source for providing radiation such as ultraviolet, visible, x-ray, electron, or ion radiation, and a reticle or mask for imparting the pattern to the radiation, thereby generating the spatially patterned radiation. In addition, for the case of reduction lithography, the illumination system can include a
30 lens assembly for imaging the spatially patterned radiation onto the wafer. The imaged radiation exposes resist coated onto the wafer. The illumination system also

includes a mask stage for supporting the mask and a positioning system for adjusting the position of the mask stage relative to the radiation directed through the mask. The wafer positioning system includes a wafer stage for supporting the wafer and a positioning system for adjusting the position of the wafer stage relative to the imaged radiation. Fabrication of integrated circuits can include multiple exposing steps. For a general reference on lithography, see, for example, J. R. Sheats and B. W. Smith, in *5 Microlithography: Science and Technology* (Marcel Dekker, Inc., New York, 1998), the contents of which is incorporated herein by reference.

The interferometry systems described above can be used to precisely measure the positions of each of the wafer stage and mask stage relative to other components of the exposure system, such as the lens assembly, radiation source, or support structure. In such cases, the interferometry system can be attached to a stationary structure and the measurement object attached to a movable element such as one of the mask and wafer stages. Alternatively, the situation can be reversed, with the interferometry system attached to a movable object and the measurement object attached to a stationary object.

More generally, the interferometry systems can be used to measure the position of any one component of the exposure system relative to any other component of the exposure system, in which the interferometry system is attached to, or supported by, one of the components and the measurement object is attached, or is supported by the other of the components.

An example of a lithography scanner **1400** using an interferometry system **1426** is shown in Fig. **14a**. The interferometry system is used to precisely measure the position of a wafer within an exposure system. Here, stage **1422** is used to position the wafer relative to an exposure station. Scanner **1400** comprises a frame **1402**, which carries other support structures and various components carried on those structures. An exposure base **1404** has mounted on top of it a lens housing **1406** atop of which is mounted a reticle or mask stage **1416**, which is used to support a reticle or mask. A positioning system for positioning the mask relative to the exposure station is indicated schematically by element **1417**. Positioning system **1417** can include, *e.g.*, piezoelectric transducer elements and corresponding control electronics.

Although, it is not included in this described embodiment, one or more of the interferometry systems described above can also be used to precisely measure the position of the mask stage as well as other moveable elements whose position must be accurately monitored in processes for fabricating lithographic structures (see *supra* 5 Sheats and Smith Microlithography: Science and Technology).

Suspended below exposure base 1404 is a support base 1413 that carries wafer stage 1422. Stage 1422 includes a plane mirror 1428 for reflecting a measurement beam 1454 directed to the stage by interferometry system 1426. A positioning system for positioning stage 1422 relative to interferometry system 1426 is indicated 10 schematically by element 1419. Positioning system 1419 can include, *e.g.*, piezoelectric transducer elements and corresponding control electronics. The measurement beam reflects back to the interferometry system, which is mounted on exposure base 1404. The interferometry system can be any of the embodiments described previously.

15 During operation, a radiation beam 1410, *e.g.*, an ultraviolet (UV) beam from a UV laser (not shown), passes through a beam shaping optics assembly 1412 and travels downward after reflecting from mirror 1414. Thereafter, the radiation beam passes through a mask (not shown) carried by mask stage 1416. The mask (not shown) is imaged onto a wafer (not shown) on wafer stage 1422 via a lens assembly 20 1408 carried in a lens housing 1406. Base 1404 and the various components supported by it are isolated from environmental vibrations by a damping system depicted by spring 1420.

In other embodiments of the lithographic scanner, one or more of the interferometry systems described previously can be used to measure distance along 25 multiple axes and angles associated for example with, but not limited to, the wafer and reticle (or mask) stages. Also, rather than a UV laser beam, other beams can be used to expose the wafer including, *e.g.*, x-ray beams, electron beams, ion beams, and visible optical beams.

In addition, the lithographic scanner can include a column reference in which 30 interferometry system 1426 directs the reference beam to lens housing 1406 or some other structure that directs the radiation beam rather than a reference path internal to

the interferometry system. The interference signal produced by interferometry system 1426 when combining measurement beam 1454 reflected from stage 1422 and the reference beam reflected from lens housing 1406 indicates changes in the position of the stage relative to the radiation beam. Furthermore, in other embodiments the interferometry system 1426 can be positioned to measure changes in the position of reticle (or mask) stage 1416 or other movable components of the scanner system. Also, in other embodiments, the positions of interferometry system 1426 and plane mirror 1428 can be reversed, with the interferometry system on the movable stage and the plane mirror fixed to support structure. Finally, the interferometry systems can be used in a similar fashion with lithography systems involving steppers, in addition to, or rather than, scanners.

As is well known in the art, lithography is a critical part of manufacturing methods for making semiconducting devices. For example, U.S. Patent 5,483,343 outlines steps for such manufacturing methods. These steps are described below with reference to FIGS. 14b and 14c. FIG. 14b is a flow chart of the sequence of manufacturing a semiconductor device such as a semiconductor chip (e.g. IC or LSI), a liquid crystal panel or a CCD. Step 1451 is a design process for designing the circuit of a semiconductor device. Step 1452 is a process for manufacturing a mask on the basis of the circuit pattern design. Step 1453 is a process for manufacturing a wafer by using a material such as silicon.

Step 1454 is a wafer process which is called a pre-process wherein, by using the so prepared mask and wafer, circuits are formed on the wafer through lithography. Step 1455 is an assembling step, which is called a post-process wherein the wafer processed by step 1454 is formed into semiconductor chips. This step includes assembling (dicing and bonding) and packaging (chip sealing). Step 1456 is an inspection step wherein operability check, durability check and so on of the semiconductor devices produced by step 1455 are carried out. With these processes, semiconductor devices are finished and they are shipped (step 1457).

FIG. 14c is a flow chart showing details of the wafer process. Step 1461 is an oxidation process for oxidizing the surface of a wafer. Step 1462 is a CVD process for forming an insulating film on the wafer surface. Step 1463 is an electrode forming

process for forming electrodes on the wafer by vapor deposition. Step 1464 is an ion implanting process for implanting ions to the wafer. Step 1465 is a resist process for applying a resist (photosensitive material) to the wafer. Step 1466 is an exposure process for printing, by exposure, the circuit pattern of the mask on the wafer through the exposure apparatus described above. Step 1467 is a developing process for developing the exposed wafer. Step 1468 is an etching process for removing portions other than the developed resist image. Step 1469 is a resist separation process for separating the resist material remaining on the wafer after being subjected to the etching process. By repeating these processes, circuit patterns are formed and superimposed on the wafer.

The interferometry systems described above can also be used in other applications in which the relative position of an object needs to be measured precisely. For example, in applications in which a write beam such as a laser, x-ray, ion, or electron beam, marks a pattern onto a substrate as either the substrate or beam moves, the interferometry systems can be used to measure the relative movement between the substrate and write beam.

As an example, a schematic of a beam writing system 1600 is shown in FIG. 16. A source 1610 generates a write beam 1612, and a beam focusing assembly 1614 directs the radiation beam to a substrate 1616 supported by a movable stage 1618. To determine the relative position of the stage, an interferometry system 1620 directs a reference beam 1622 to a mirror 1624 mounted on beam focusing assembly 1614 and a measurement beam 1626 to a mirror 1628 mounted on stage 1618. Interferometry system 1620 can be any of the interferometry systems described previously. Changes in the position measured by the interferometry system correspond to changes in the relative position of write beam 1612 on substrate 1616. Interferometry system 1620 sends a measurement signal 1632 to controller 1630 that is indicative of the relative position of write beam 1612 on substrate 1616. Controller 1630 sends an output signal 1634 to a base 1636 that supports and positions stage 1618. In addition, controller 1630 sends a signal 1638 to source 1610 to vary the intensity of, or block, write beam 1612 so that the write beam contacts the substrate with an intensity sufficient to cause photophysical or photochemical change only at selected positions

of the substrate. Furthermore, in some embodiments, controller 1630 can cause beam focusing assembly 1614 to scan the write beam over a region of the substrate, *e.g.*, using signal 1644. As a result, controller 1630 directs the other components of the system to pattern the substrate. The patterning is typically based on an electronic
5 design pattern stored in the controller. In some applications the write beam patterns a resist coated on the substrate and in other applications the write beam directly patterns, *e.g.*, etches, the substrate.

An important application of such a system is the fabrication of masks and reticles used in the lithography methods described previously. For example, to
10 fabricate a lithography mask an electron beam can be used to pattern a chromium-coated glass substrate. In such cases where the write beam is an electron beam, the beam writing system encloses the electron beam path in a vacuum. Also, in cases where the write beam is, *e.g.*, an electron or ion beam, the beam focusing assembly includes electric field generators such as quadrupole lenses for focusing and directing
15 the charged particles onto the substrate under vacuum. In other cases where the write beam is a radiation beam, *e.g.*, x-ray, UV, or visible radiation, the beam focusing assembly includes corresponding optics and for focusing and directing the radiation to the substrate.

It is understood that while the invention has been described in conjunction
20 with the detailed description thereof, the foregoing description is intended to illustrate and not limit the scope of the invention, which is defined by the scope of the appended claims.

For example, although embodiments described above use heterodyne detection to determine changes in the optical path length difference between the reference and
25 measurement paths, the interferometry systems can also use homodyne detection, in which the frequencies of the reference and measurement beams are the same. In such cases, a non-polarizing beam splitter splits the output beam formed by the overlapping exit reference and measurement beams into two components, one of which passes through a quarter wave plate. Thereafter, each of the two components passes through
30 a polarizer to produce a pair of mixed optical signals, which are measured by a pair of detectors, respectively. The electronic signals measured by the detectors are in phase

quadrature with one another and can be processed by a computer to determine the changes in the optical path length difference using well-known homodyne processing techniques.

Furthermore, in other embodiments in which the reference beam reflects from a reference object, the interferometry system can include one or more additional beam steering assemblies (and corresponding controllers and detectors) that redirect the reference beam in response to changes in the angular orientation or position of the reference object.

Finally, in other embodiments the beam steering assembly can be different from a mirror oriented by a positioning system. For example, the beam steering assembly can include one or more of the following elements: an electro-optic or acousto-optic beam deflector, a pair of rotating optical wedges (Risely prisms), a variable wedge element, and any other such element that can alter the direction of a light beam.

Other aspects, advantages, and modifications are within the scope of the following claims.

What is claimed is:

1. Apparatus comprising:

a multi-axis interferometry system configured to receive an input beam and direct at least two beams derived from the input beam to contact different locations on a measurement object to monitor changes in an angular orientation of the

5 measurement object;

a beam steering assembly having a beam steering element positioned to direct the input beam into the interferometry system and a positioning system to selectively orient the beam steering element relative to the interferometry system; and

10 a control circuit which during operation orients the beam steering element based on the changes in the angular orientation of the measurement object monitored by the interferometry system.

2. The apparatus of claim 1, wherein the control circuit causes the beams to contact the measurement object at substantially normal incidence over a range of
15 angular orientations of the measurement object.

3. The apparatus of claim 1, wherein the two beams that contact the measurement object are measurement beams, and wherein the multi-axis interferometry system is configured to combine each of the two measurement beams
20 with a corresponding reference beam after they contact the measurement object to produce a pair of output beams comprising interferometric information about changes in distance to the different locations on the measurement object.

4. The apparatus of claim 3, wherein during operation the control circuit
25 calculates a control signal using the interferometric information in the output beams and causes the positioning system to orient the beam steering element based on the control signal.

5. The apparatus of claim 4, wherein the control circuit comprises multiple
30 detectors for measuring an intensity of each output beam, a signal processor for calculating the changes in distance to the different locations of the measurement

object from the measured intensities and generating the control signal based on the calculated distance changes, and a control system for causing the positioning system to orient the beam steering element in response to the control signal.

5 6. The apparatus of claim 5, further comprising a polarizer prior to each detector to cause the measured intensity of each output beam to correspond to the intensity of a selected polarization component of that output beam.

10 7. The apparatus of claim 3, wherein the multi-axis interferometry system directs each measurement beam to make an even number of passes to the measurement object before combining it with its corresponding reference beam.

15 8. The apparatus of claim 3, wherein the multi-axis interferometry system directs each measurement beam to make only one pass to the measurement object before combining it with its corresponding reference beam.

20 9. The apparatus of claim 3, wherein the multi-axis interferometry system comprises separate single-axis interferometers each producing a corresponding measurement beam and optics for directing a portion of the input beam to each of the interferometers.

25 10. The apparatus of claim 3, wherein the multi-axis interferometry system comprises an integral multi-axis interferometer comprising multiple measurement axes each corresponding to one of the measurement beams.

30 11. The apparatus of claim 1, wherein the multi-axis interferometry system is configured to combine the two beams with one another after they contact the measurement object to produce an output beam comprising interferometric information about the changes in the angular orientation of the measurement object.

12. The apparatus of claim 11, wherein during operation the control circuit calculates a control signal using the interferometric information in the output beam and causes the positioning system to orient the beam steering element based on the control signal.

5

13. The apparatus of claim 12, wherein the control circuit comprises a detector for measuring an intensity of the output beam, a signal processor for calculating the changes in the angular orientation of the measurement object from the measured intensity and generating the control signal from the calculated changes in angular orientation, and a control system for causing the positioning system to orient the beam steering element in response to the control signal.

10

14. The apparatus of claim 13, further comprising a polarizer prior to the detector to cause the measured intensity of the output beam to correspond to the intensity of a selected polarization component of the output beam.

15

15. The apparatus of claim 1, wherein the multi-axis interferometry system directs at least three measurement beams to contact the measurement object at different locations.

20

16. The apparatus of claim 1, wherein the changes in the angular orientation of the measurement object monitored by the interferometry system are relative to a reference object.

25

17. The apparatus of claim 16, wherein the reference object is fixed in the interferometry system.

18. Apparatus comprising:

a multi-axis interferometry system configured to direct at least two beams to contact different locations on a measurement object to monitor changes in an angular orientation of the measurement object, the interferometry system comprising a beam

30

steering assembly having a beam steering element positioned to direct and contact at least one of the beams and a positioning system to selectively orient the beam steering element within the interferometry system; and

5 a control circuit which during operation orients the beam steering element based on the changes in the angular orientation of the measurement object monitored by the interferometry system.

19. The apparatus of claim 18, wherein the beam steering element is positioned to direct multiple ones of the beams that contact the measurement object.
10

20. The apparatus of claim 18, wherein the multi-axis interferometry system comprises at least one additional beam steering assembly having a beam steering element positioned to direct and contact another one of the beams that contact the measurement object and a positioning system to selectively orient the beam steering
15 element in the additional beam steering assembly.

21. The apparatus of claim 20, wherein during operation the control circuit causes the positioning system in the additional beam steering assembly to orient the beam steering element in the additional beam steering assembly in response to the
20 control signal.

22. The apparatus of claim 18, wherein the control circuit causes the beams to contact the measurement object at substantially normal incidence over a range of angular orientations of the measurement object.
25

23. The apparatus of claim 18, wherein the two beams that contact the measurement object are measurement beams, and wherein the multi-axis interferometry system is configured to combine each of the two measurement beams with a corresponding reference beam after they contact the measurement object to
30 produce a pair of output beams comprising interferometric information about changes in distance to the different locations on the measurement object.

24. The apparatus of claim 23, wherein during operation the control circuit calculates a control signal using the interferometric information in the output beams and causes the positioning system to orient the beam steering element based on the control signal.

25. The apparatus of claim 24, wherein the control circuit comprises multiple detectors for measuring an intensity of each output beam, a signal processor for calculating the changes in distance to the different locations of the measurement object from the measured intensities and generating the control signal based on the calculated distance changes, and a control system for causing the positioning system to orient the beam steering element in response to the control signal.

26. The apparatus of claim 25, further comprising a polarizer prior to each detector to cause the measured intensity of each output beam to correspond to the intensity of a selected polarization component of that output beam.

27. The apparatus of claim 23, wherein the multi-axis interferometry system directs each measurement beam to make an even number of passes to the measurement object before combining it with its corresponding reference beam.

28. The apparatus of claim 23, wherein the multi-axis interferometry system directs each measurement beam to make only one pass to the measurement object before combining it with its corresponding reference beam.

29. The apparatus of claim 23, wherein the multi-axis interferometry system comprises separate single-axis interferometers each producing a corresponding measurement beam and optics for directing a portion of the input beam to each of the interferometers.

30. The apparatus of claim 23, wherein the multi-axis interferometry system comprises an integral multi-axis interferometer comprising multiple measurement axes each corresponding to one of the measurement beams.

5 31. The apparatus of claim 18, wherein the multi-axis interferometry system is configured to combine the two beams with one another after they contact the measurement object to produce an output beam comprising interferometric information about the changes in the angular orientation of the measurement object.

10 32. The apparatus of claim 31, wherein during operation the control circuit calculates a control signal using the interferometric information in the output beam and causes the positioning system to orient the beam steering element based on the control signal.

15 33. The apparatus of claim 32, wherein the control circuit comprises a detector for measuring an intensity of the output beam, a signal processor for calculating the changes in the angular orientation of the measurement object from the measured intensity and generating the control signal from the calculated changes in angular orientation, and a control system for causing the positioning system to orient
20 the beam steering element in response to the control signal.

 34. The apparatus of claim 18, wherein the multi-axis interferometry system directs at least three measurement beams to contact the measurement object at different locations.

25 35. The apparatus of claim 18, wherein the changes in the angular orientation of the measurement object monitored by the interferometry system are relative to a reference object.

30 36. The apparatus of claim 35, wherein the reference object is fixed in the interferometry system.

37. A lithography system for use in fabricating integrated circuits on a wafer, the system comprising:

a stage for supporting the wafer;

5 an illumination system for imaging spatially patterned radiation onto the wafer;

a positioning system for adjusting the position of the stage relative to the imaged radiation; and

10 the apparatus of claim 1 for monitoring the position of the wafer relative to the imaged radiation.

38. The system of claim 37, wherein the measurement object comprises the stage.

15 39. The system of claim 37, wherein the multi-axis interferometry system is supported by the stage.

40. A lithography system for use in fabricating integrated circuits on a wafer, the system comprising:

20 a stage for supporting the wafer;

an illumination system for imaging spatially patterned radiation onto the wafer;

a positioning system for adjusting the position of the stage relative to the imaged radiation; and

25 the apparatus of claim 18 for monitoring the position of the wafer relative to the imaged radiation.

41. The system of claim 40, wherein the measurement object comprises the stage.

30

42. The system of claim 40, wherein the multi-axis interferometry system is attached to the stage.

5 43. A lithography system for use in fabricating integrated circuits on a wafer, the system comprising:
a stage for supporting the wafer; and
an illumination system including a radiation source, a mask, a positioning system, a lens assembly, and the apparatus of claim 1, wherein during operation the source directs radiation through the mask to produce spatially patterned radiation, the
10 positioning system adjusts the position of the mask relative to the radiation from the source, the lens assembly images the spatially patterned radiation onto the wafer, and the apparatus monitors the position of the mask relative to the radiation from the source.

15 44. The system of claim 43, wherein the measurement object comprises the mask.

20 45. The system of claim 43, wherein the multi-axis interferometry system is attached to the mask.

46. A lithography system for use in fabricating integrated circuits on a wafer, the system comprising:
a stage for supporting the wafer; and
an illumination system including a radiation source, a mask, a positioning
25 system, a lens assembly, and the apparatus of claim 18, wherein during operation the source directs radiation through the mask to produce spatially patterned radiation, the positioning system adjusts the position of the mask relative to the radiation from the source, the lens assembly images the spatially patterned radiation onto the wafer, and the apparatus monitors the position of the mask relative to the radiation from the
30 source.

47. The system of claim 46, wherein the measurement object comprises the mask.

48. The system of claim 46, wherein the multi-axis interferometry system is
5 attached to the mask.

49. A beam writing system for use in fabricating a lithography mask, the system comprising:

a source providing a write beam to pattern a substrate;
10 a stage supporting the substrate;
a beam directing assembly for delivering the write beam to the substrate;
a positioning system for positioning the stage and beam directing assembly relative one another; and
the apparatus of claim 1, for monitoring the position of the stage relative to the
15 beam directing assembly.

50. A beam writing system for use in fabricating a lithography mask, the system comprising:

a source providing a write beam to pattern a substrate;
20 a stage supporting the substrate;
a beam directing assembly for delivering the write beam to the substrate;
a positioning system for positioning the stage and beam directing assembly relative one another; and
the apparatus of claim 18, for monitoring the position of the stage relative to
25 the beam directing assembly.

51. A method for fabricating integrated circuits comprising using the lithography system of claim 43.

30 52. A method for fabricating integrated circuits comprising using the lithography system of claim 46.

53. A method for fabricating a lithography mask comprising using the beam writing system of claim 50.

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1/41

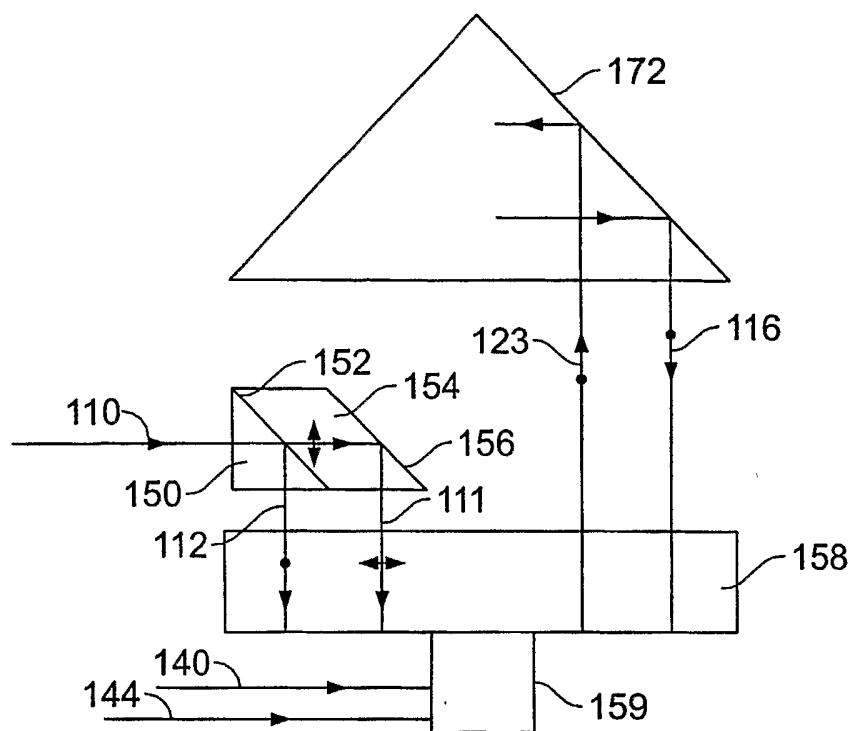


FIG. 1A

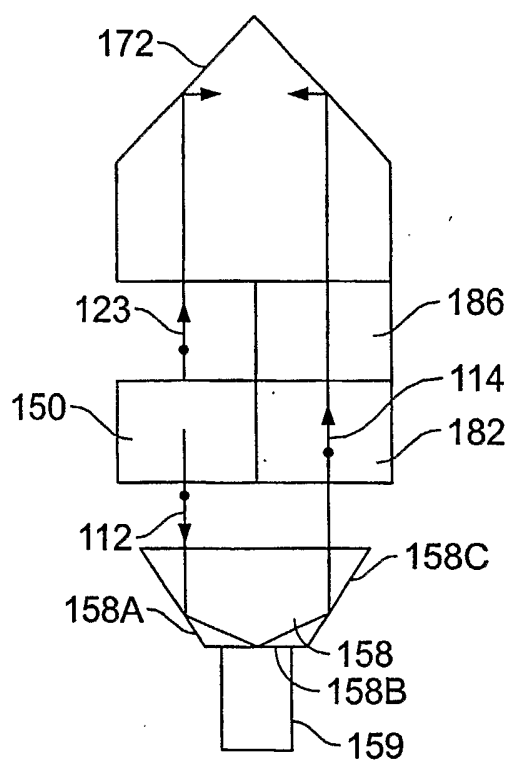


FIG. 1C.

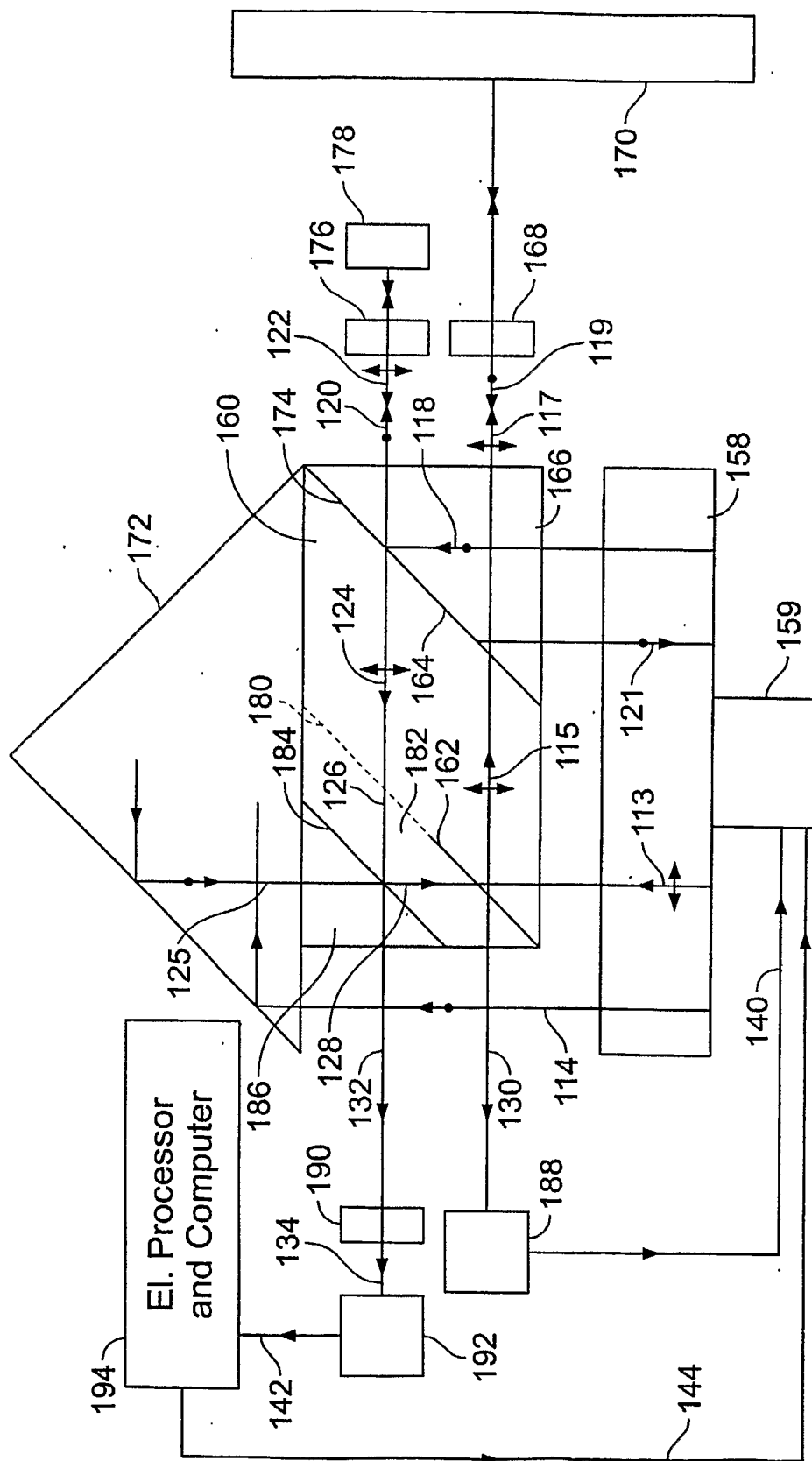


FIG. 1B

3/41

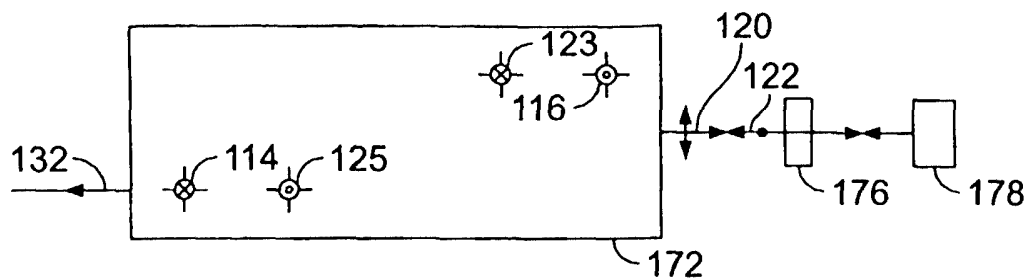


FIG. 1D

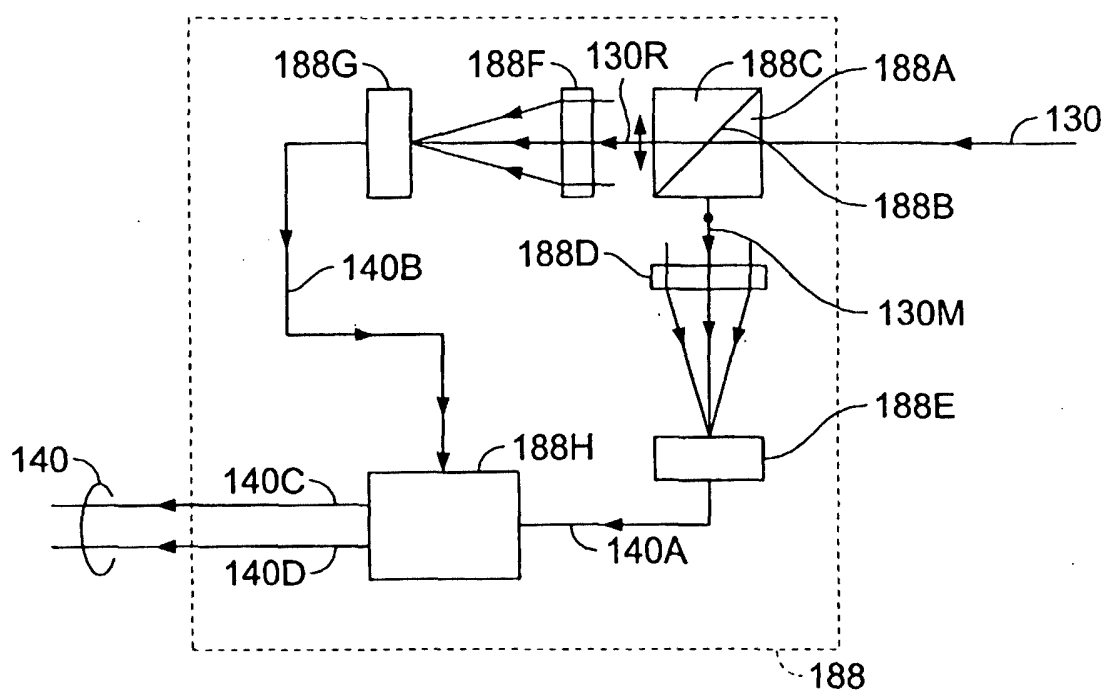


FIG. 1E

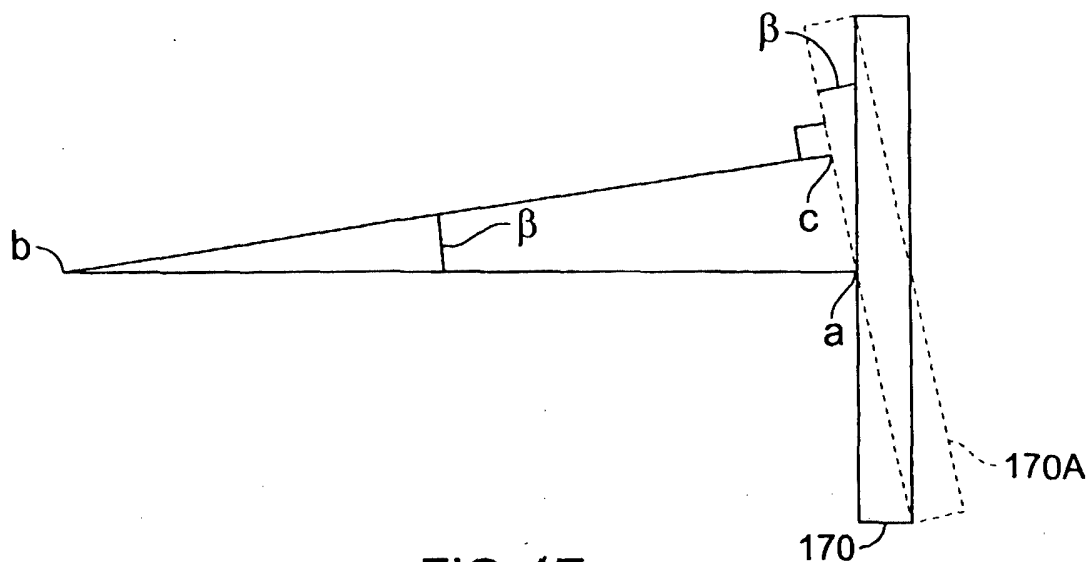


FIG. 1F

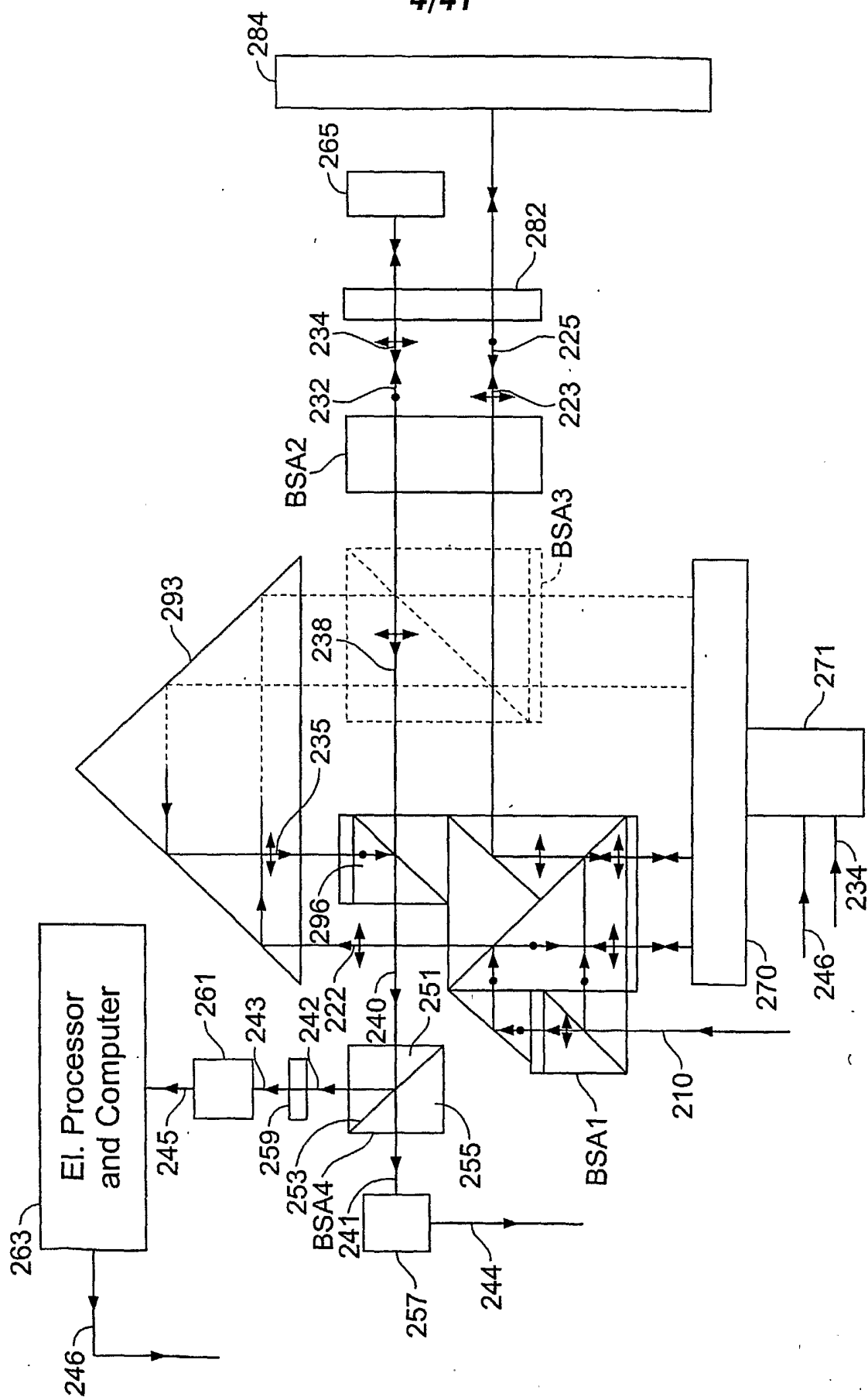


FIG. 2A

5/41

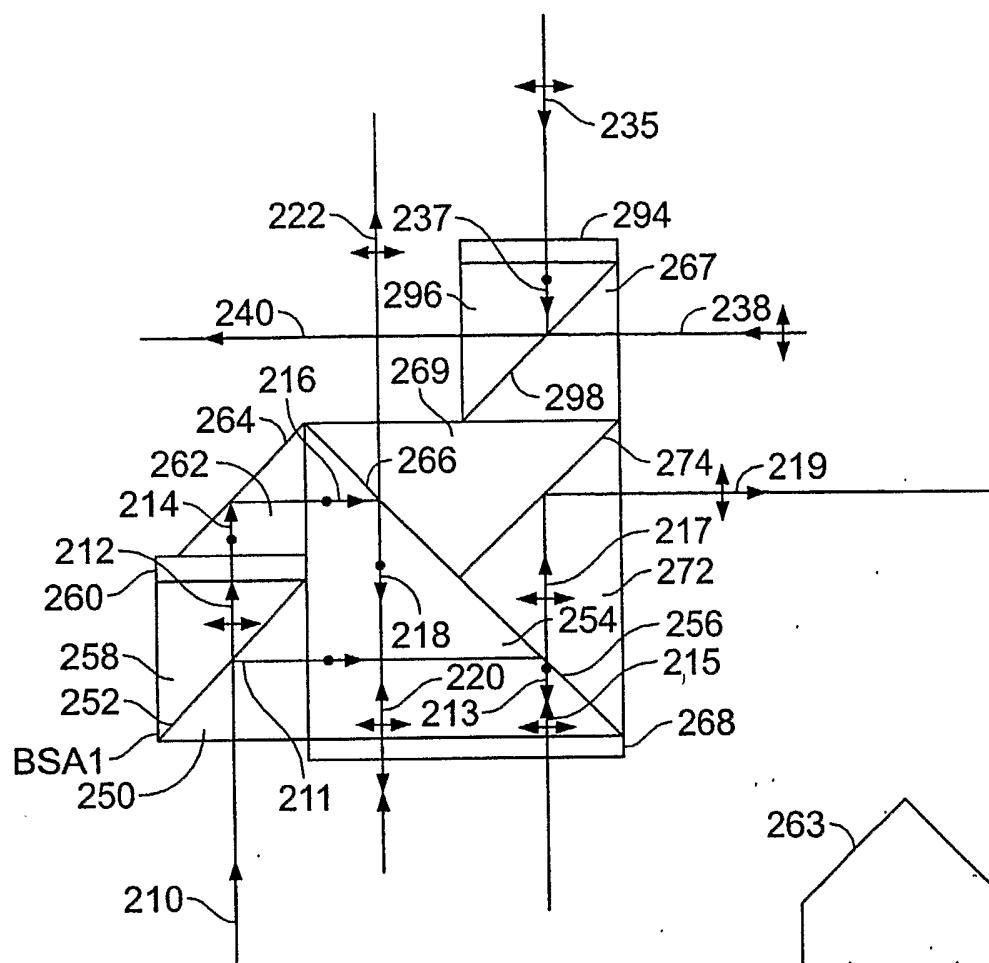


FIG. 2B

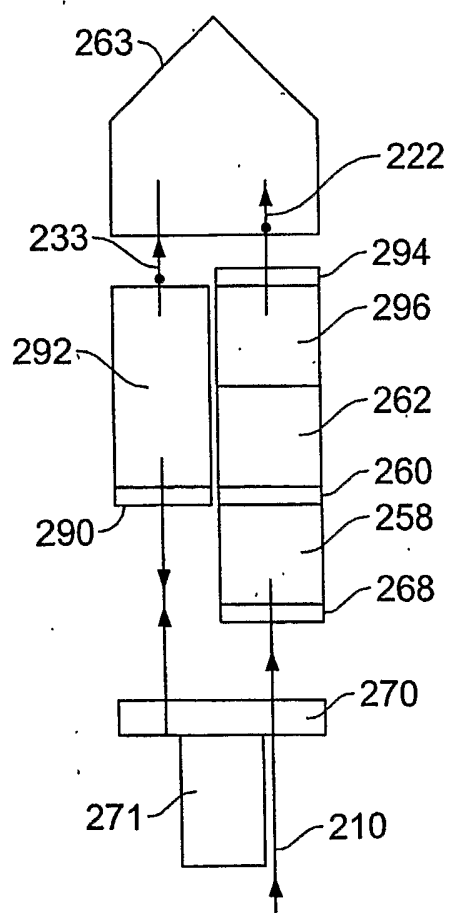


FIG. 2C

6/41

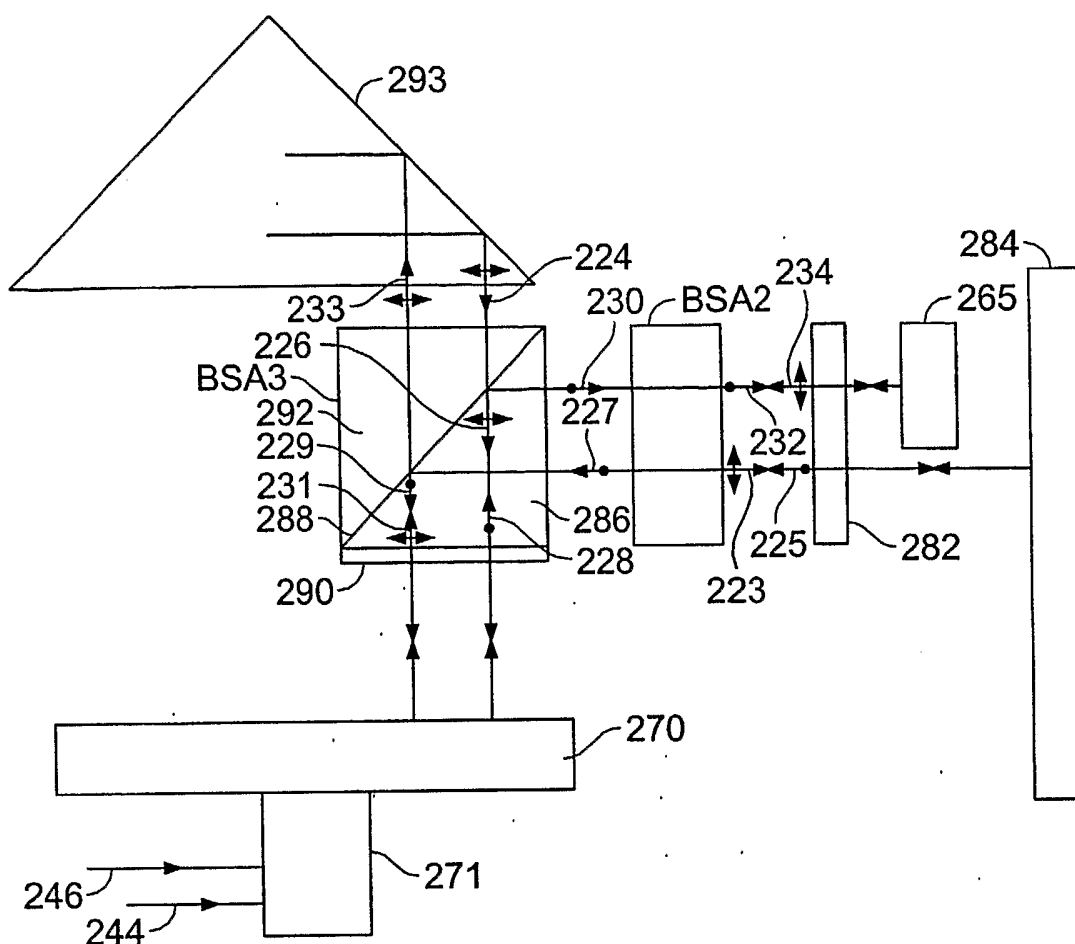


FIG. 2D

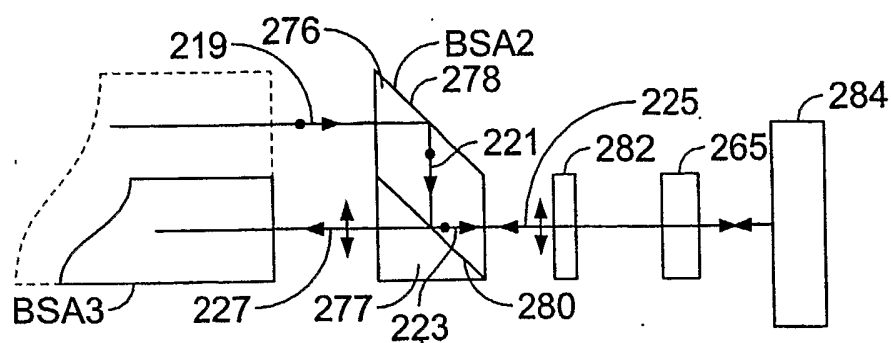


FIG. 2E

7/41

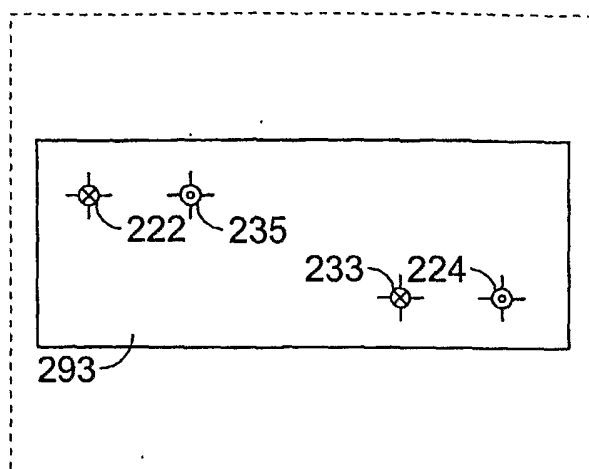


FIG. 2F

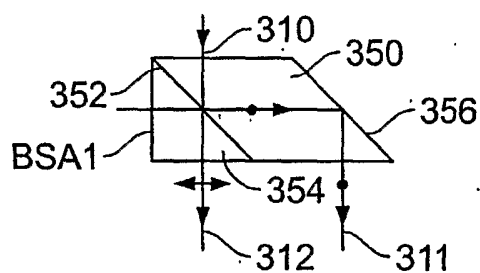


FIG. 3A

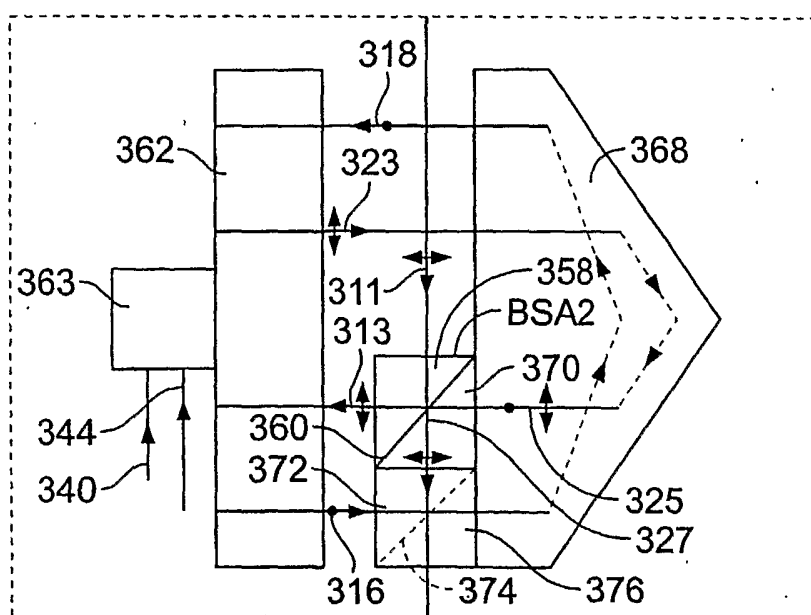


FIG. 3B

8/41

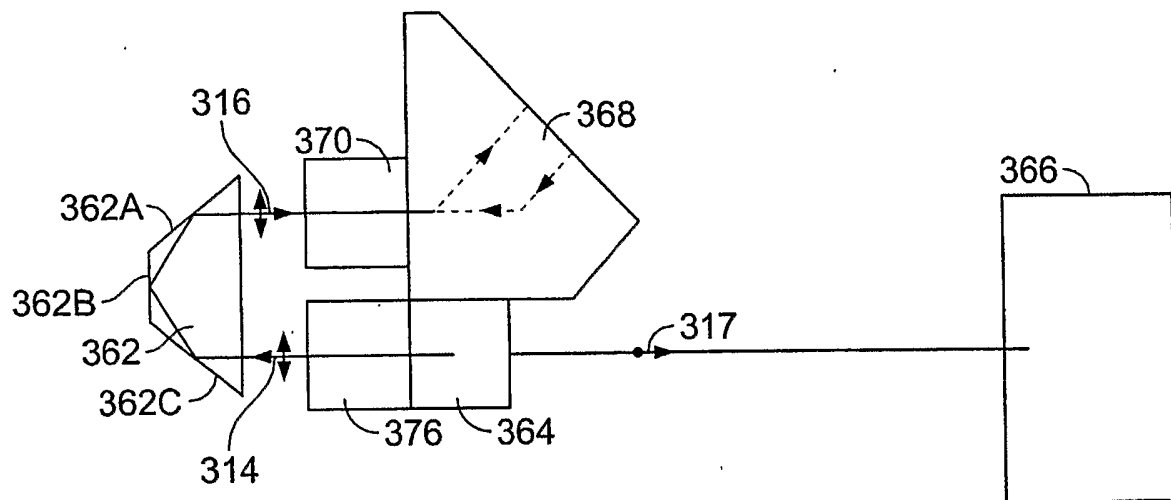


FIG. 3C

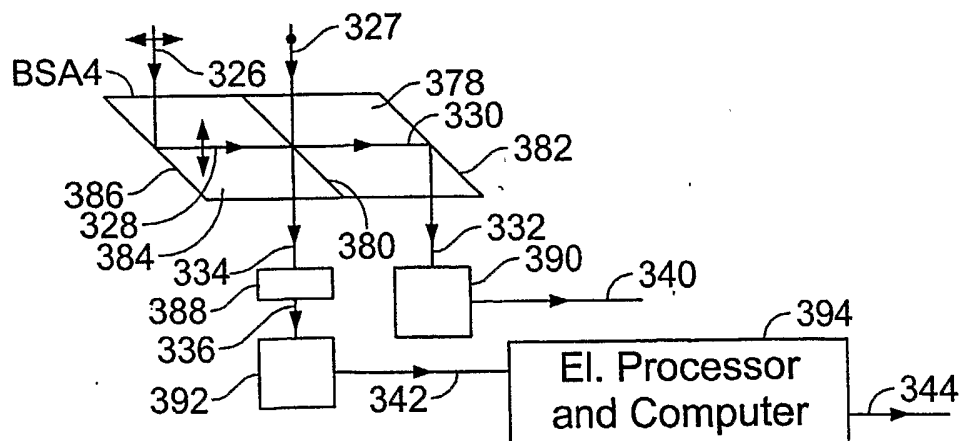


FIG. 3E

9/41

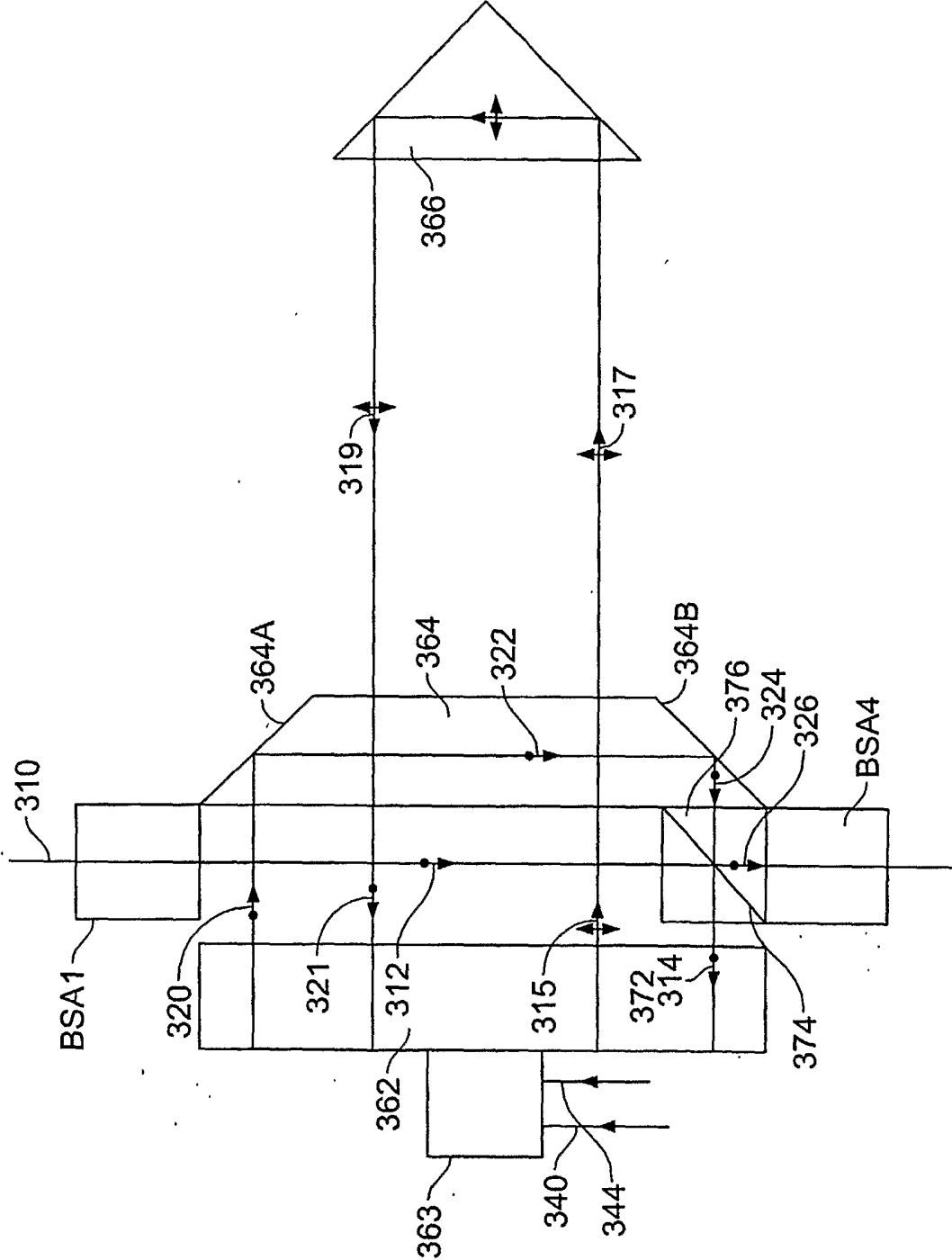


FIG. 3D

10/41

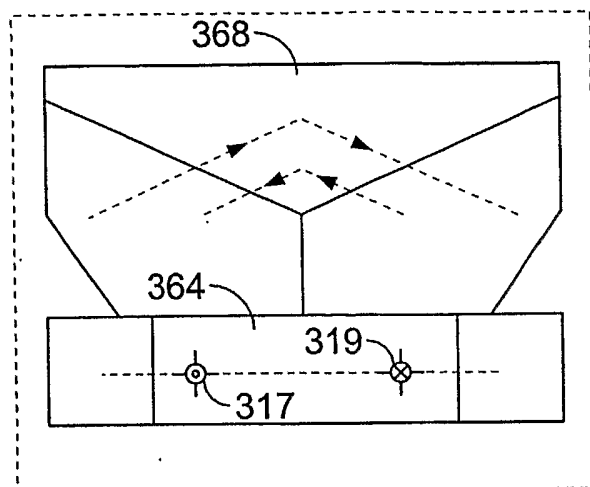


FIG. 3F

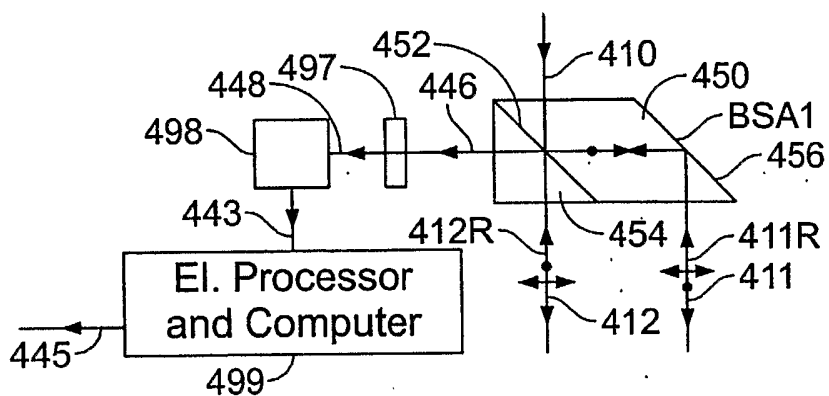
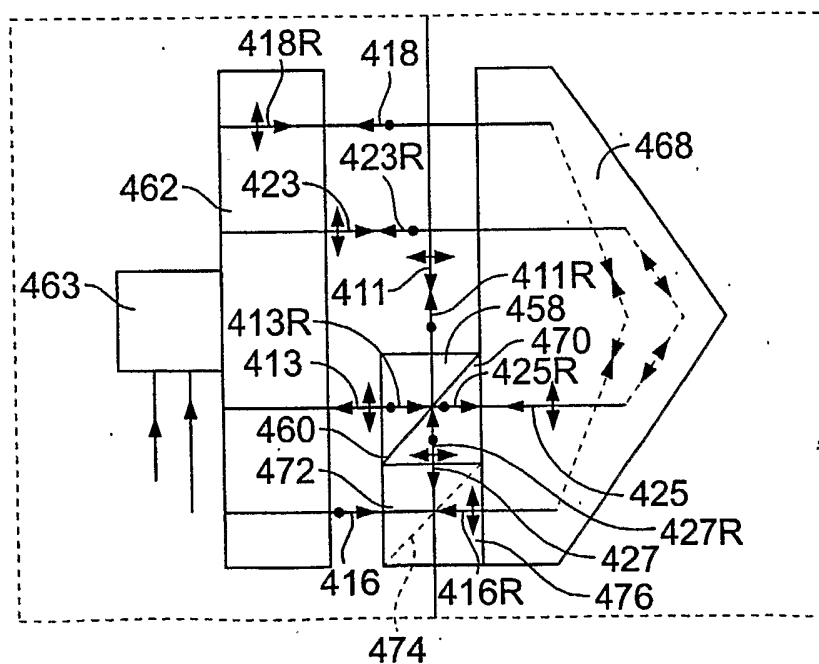


FIG. 4A



11/41

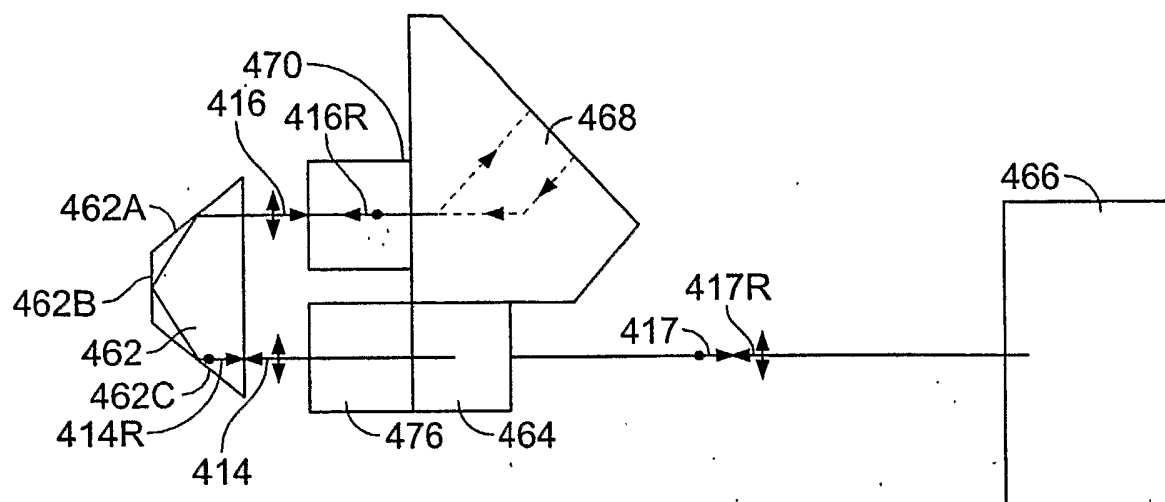


FIG. 4C

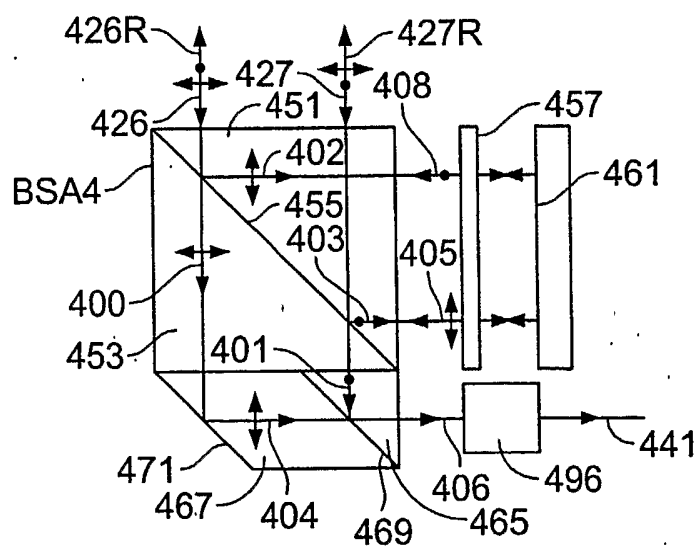


FIG. 4E

12/41

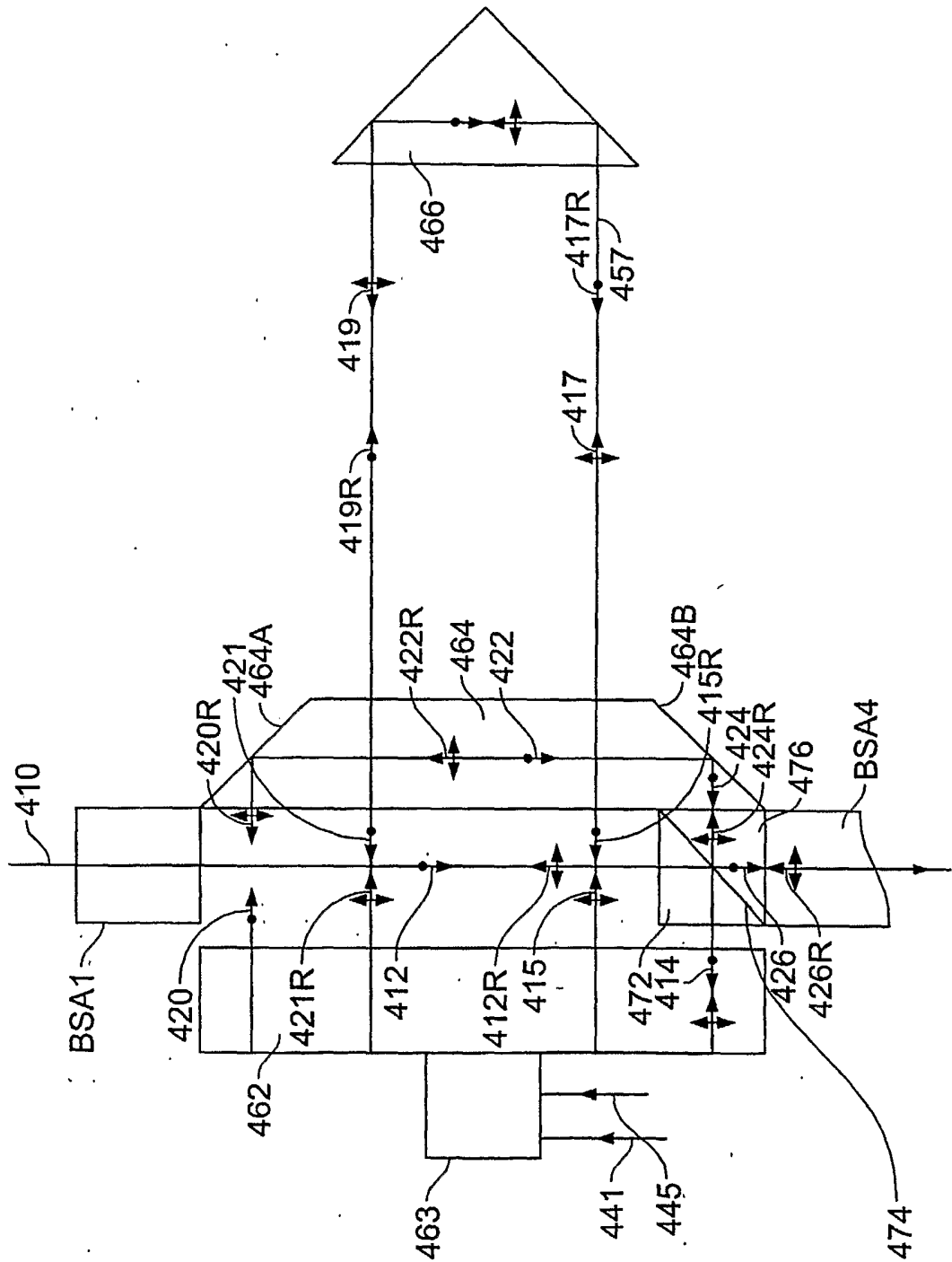


FIG. 4D

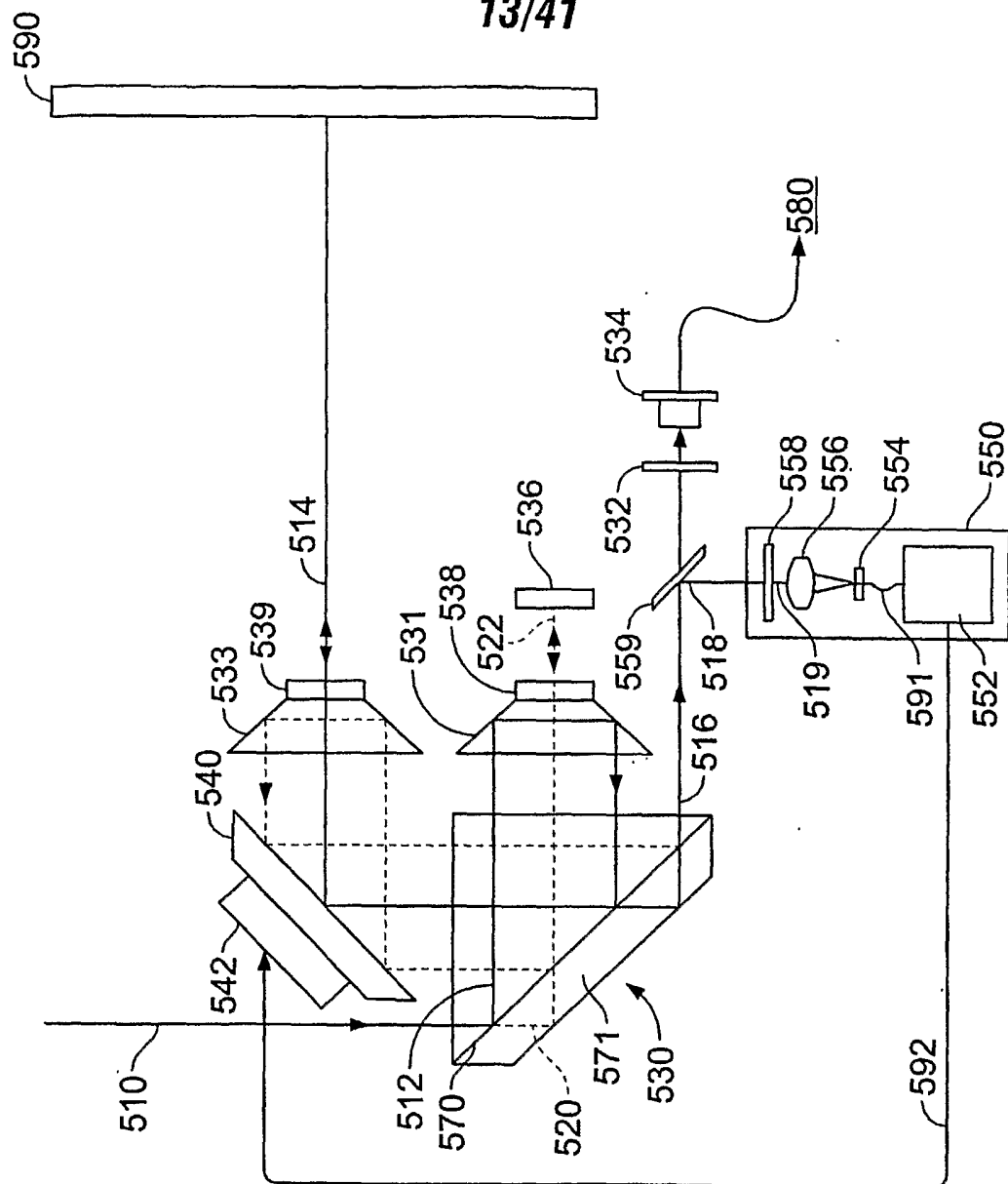


FIG. 5

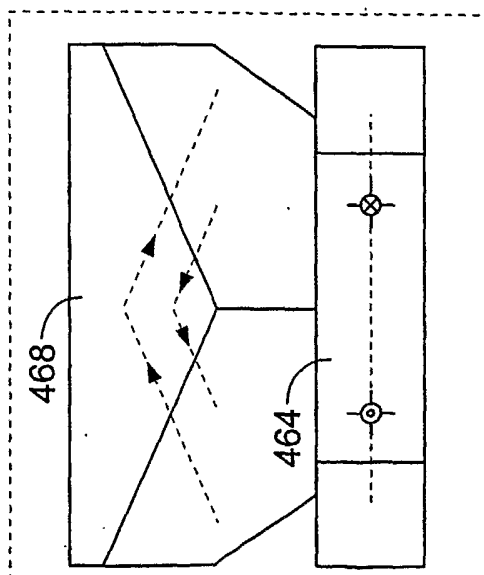


FIG. 4F

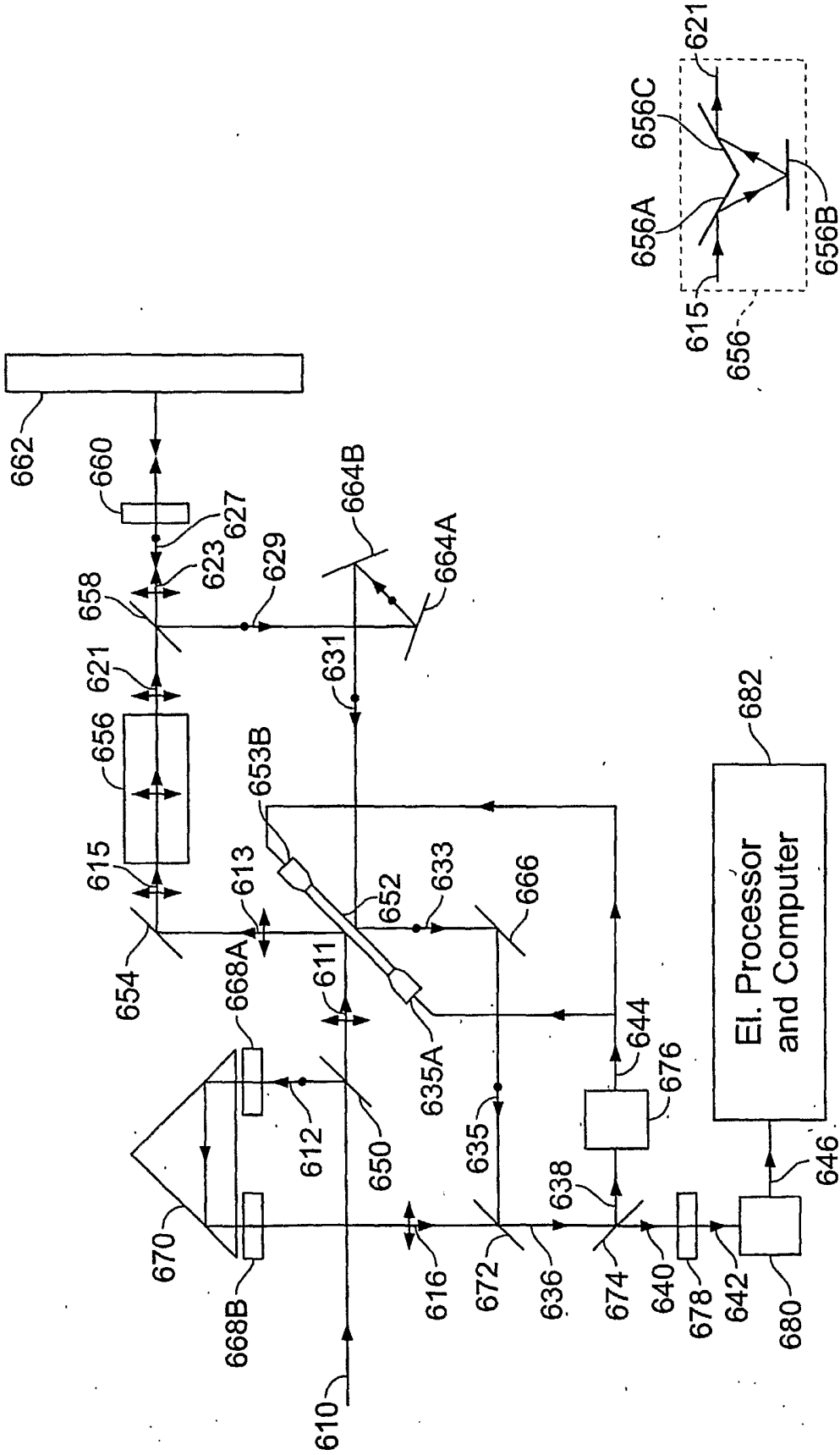


FIG. 6A

FIG. 6B

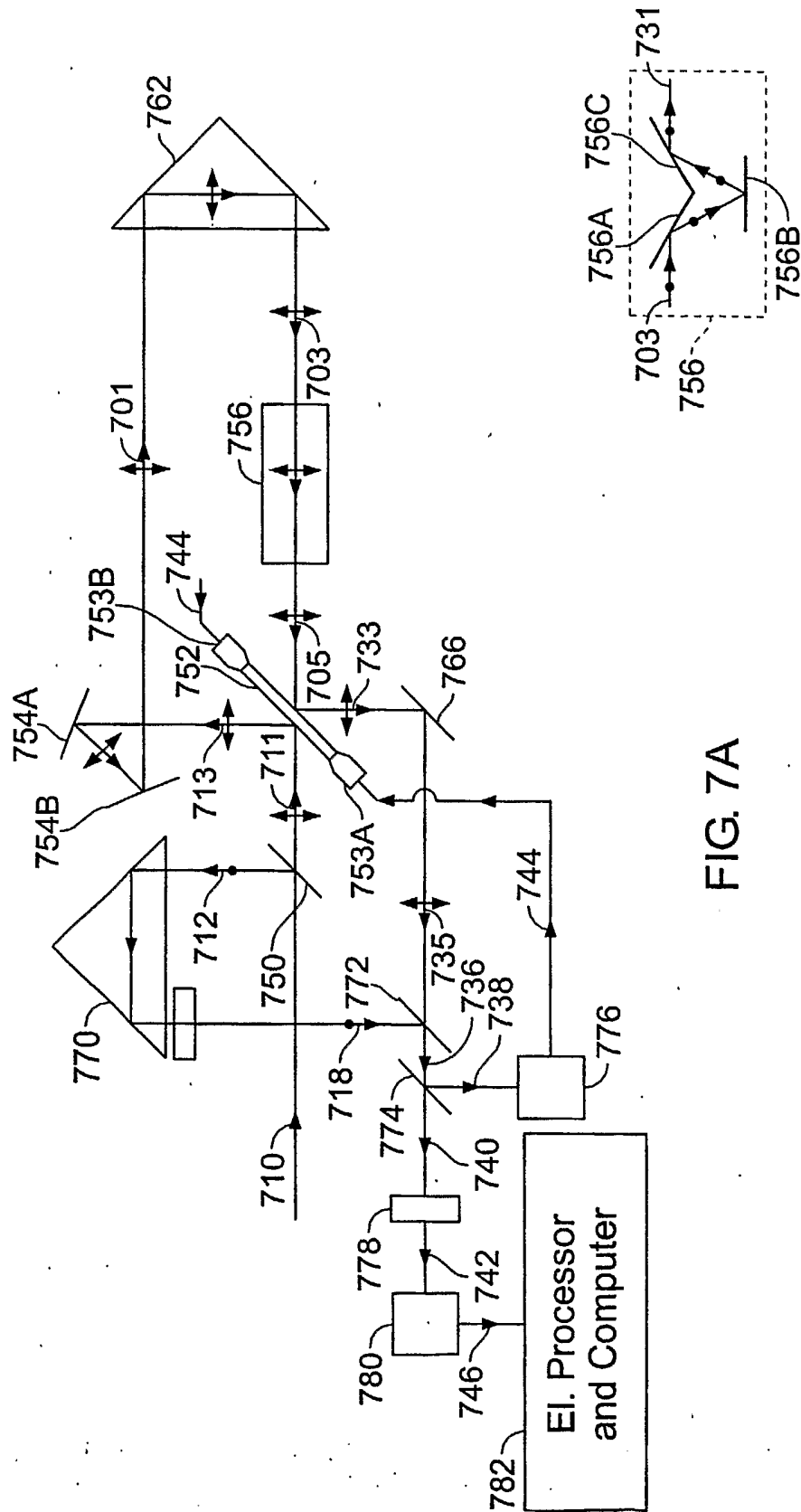


FIG. 7A

FIG. 7B

16/41

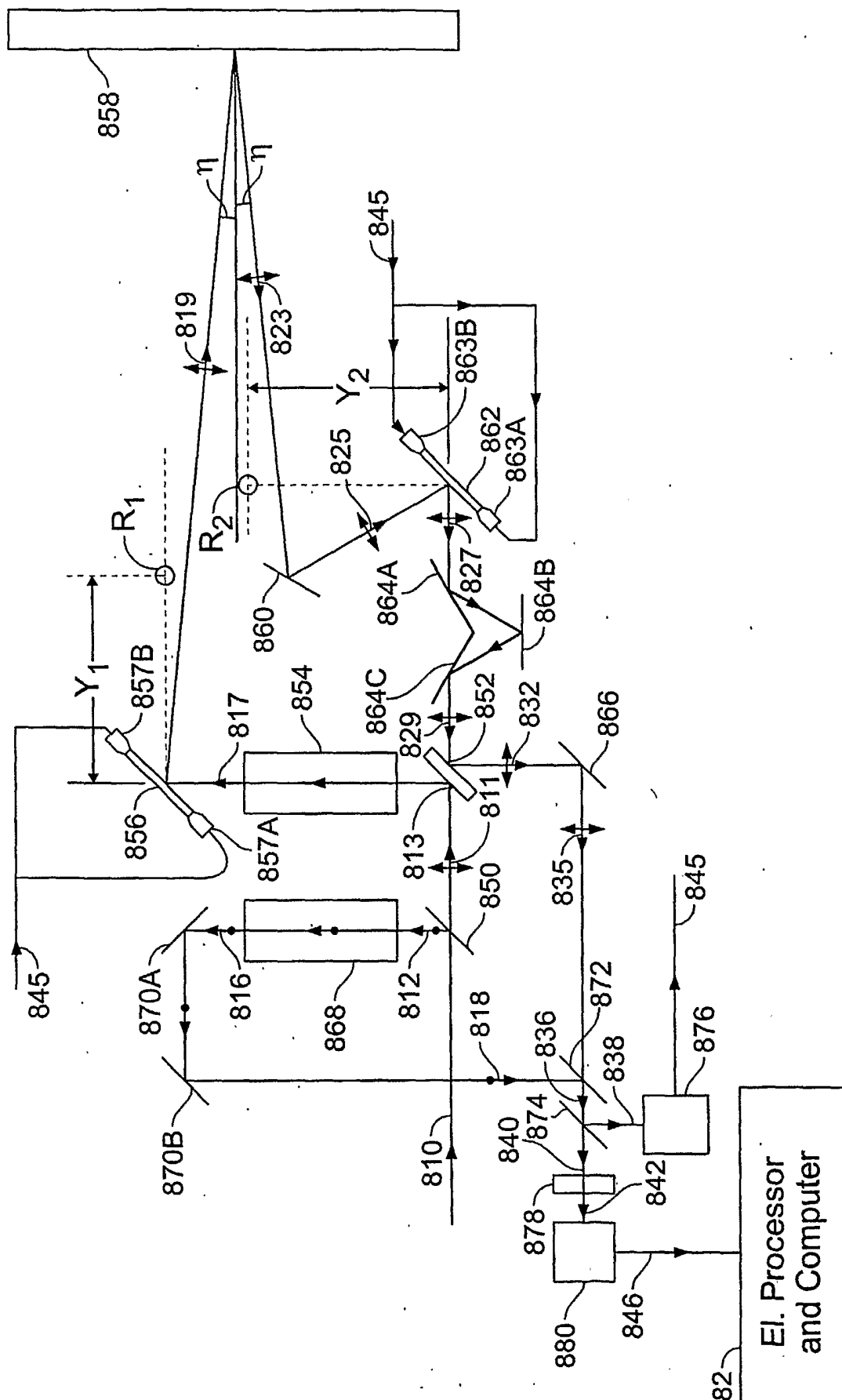
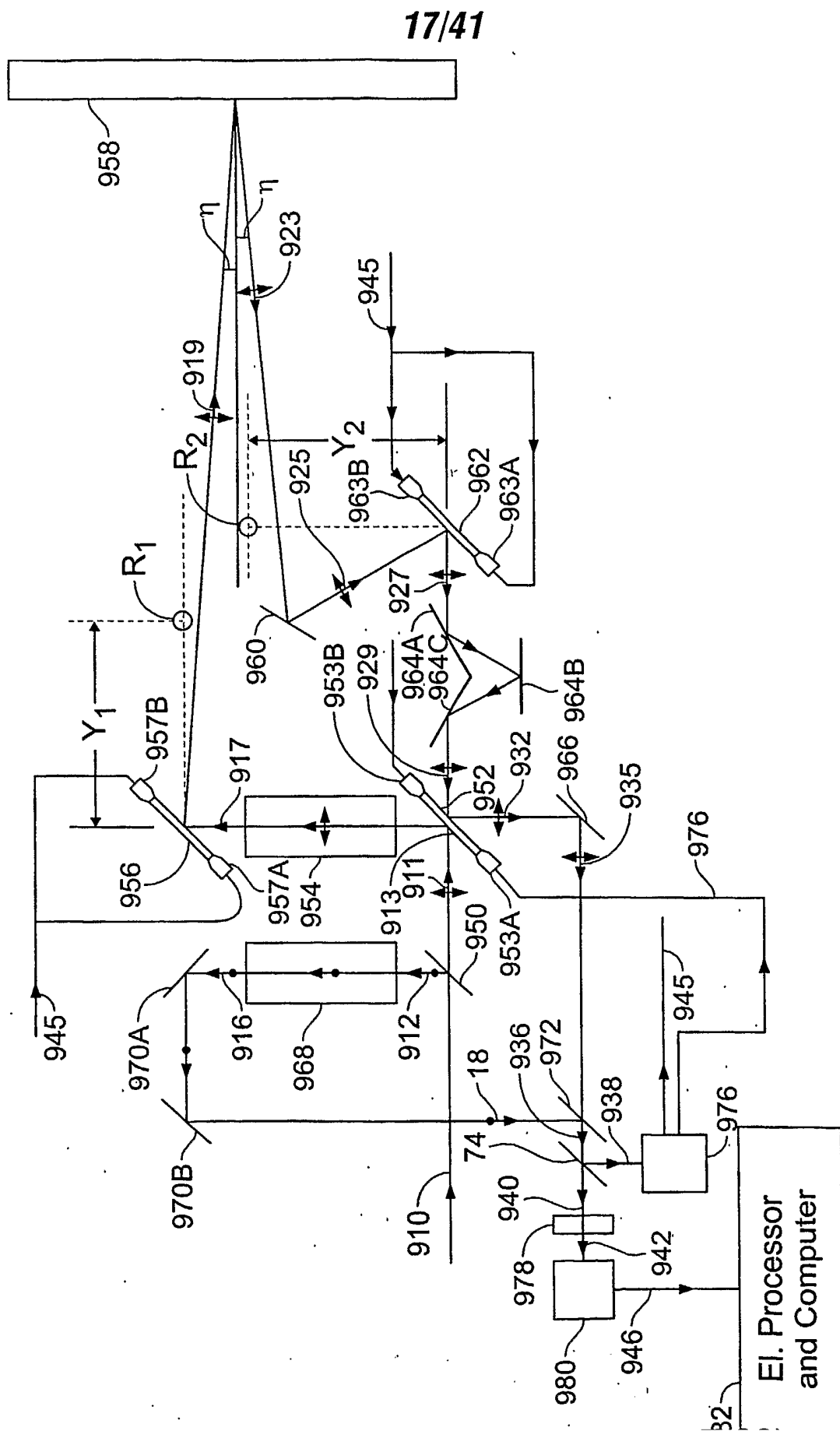


FIG. 8A



18/41

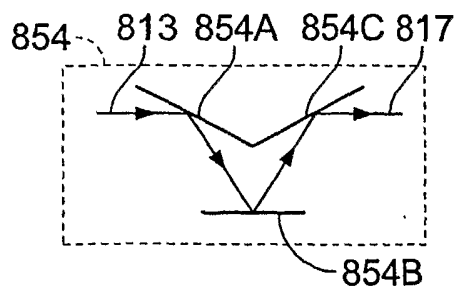


FIG. 8B

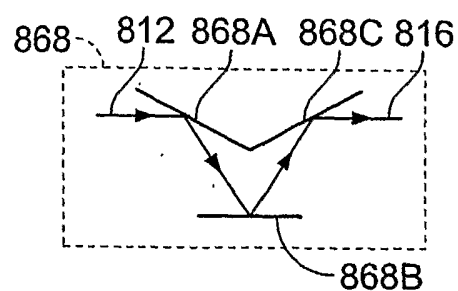


FIG. 8C

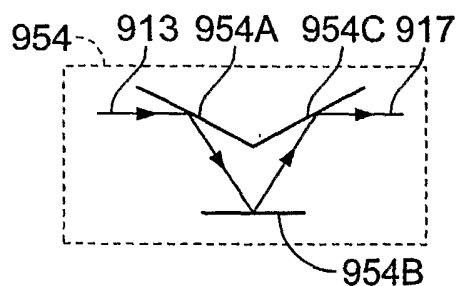


FIG. 9B

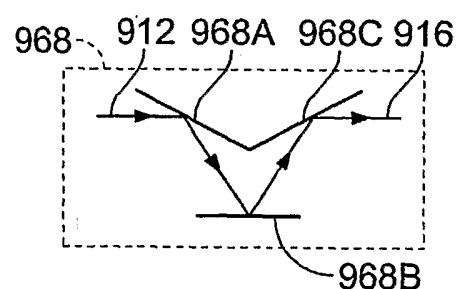


FIG. 9C

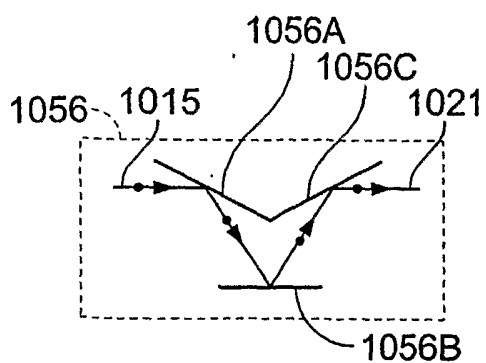


FIG. 10B

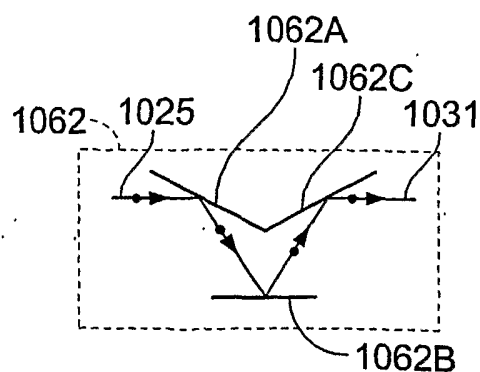


FIG. 10C

19/41

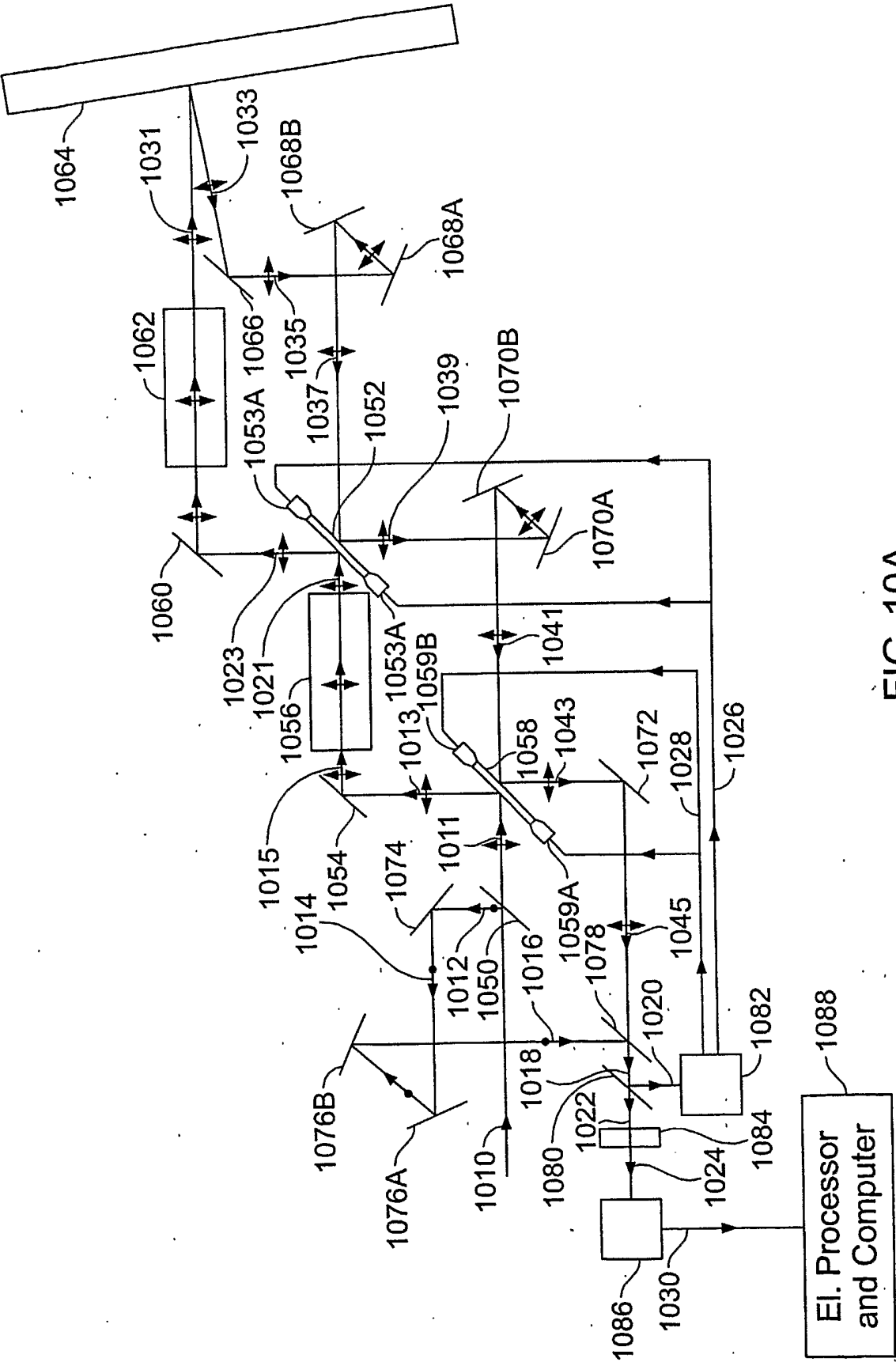


FIG. 10A

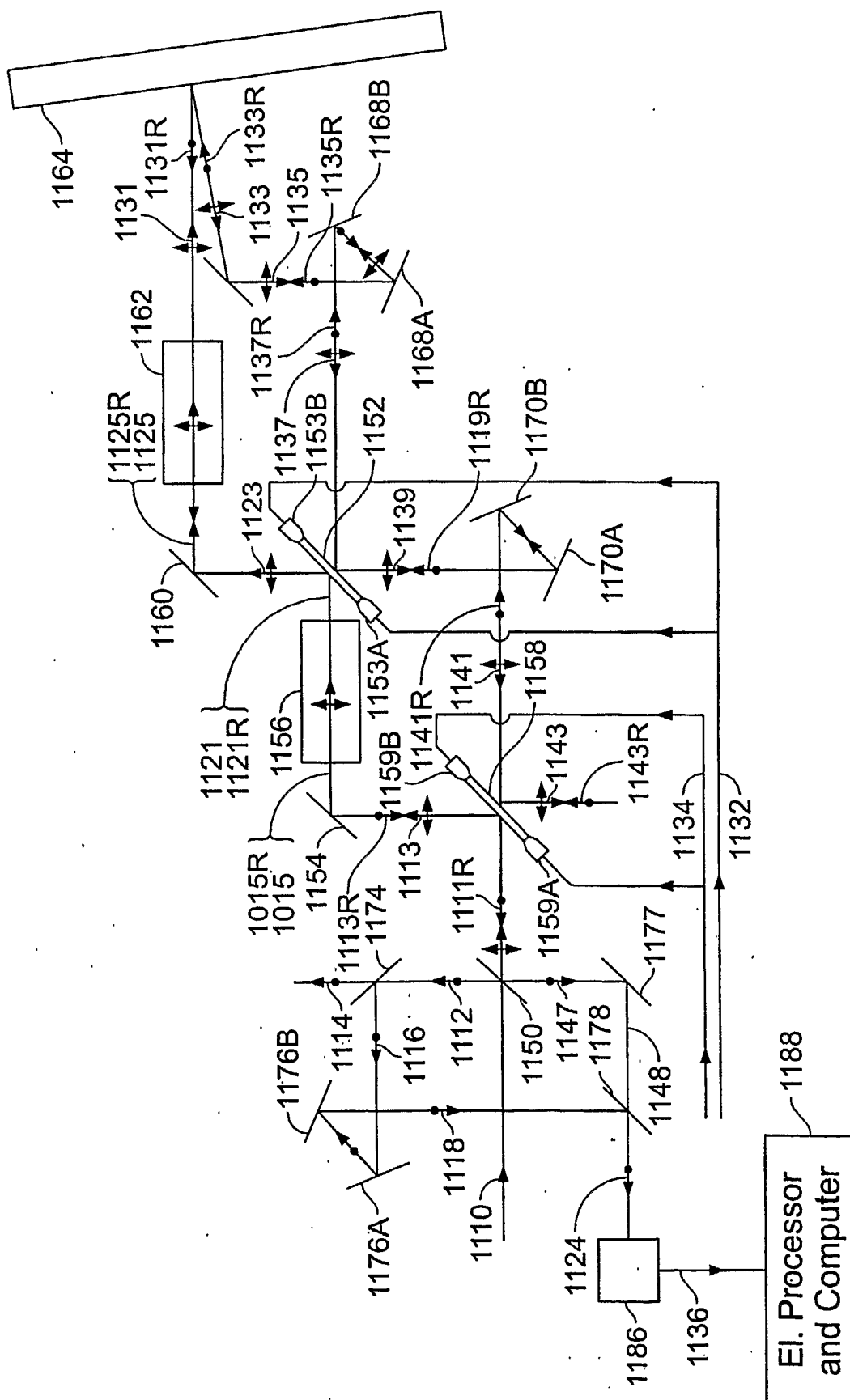


FIG. 11A

21/41

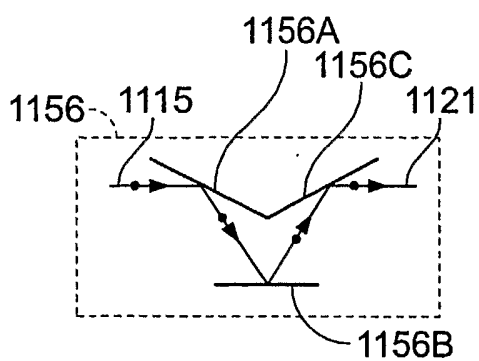


FIG. 11B

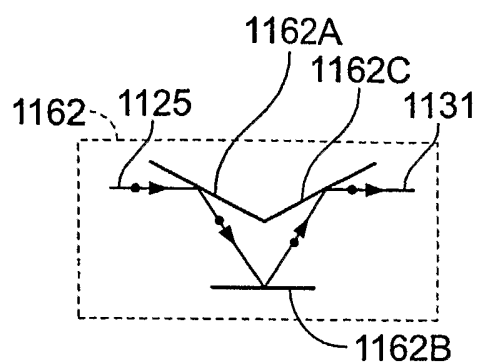


FIG. 11C

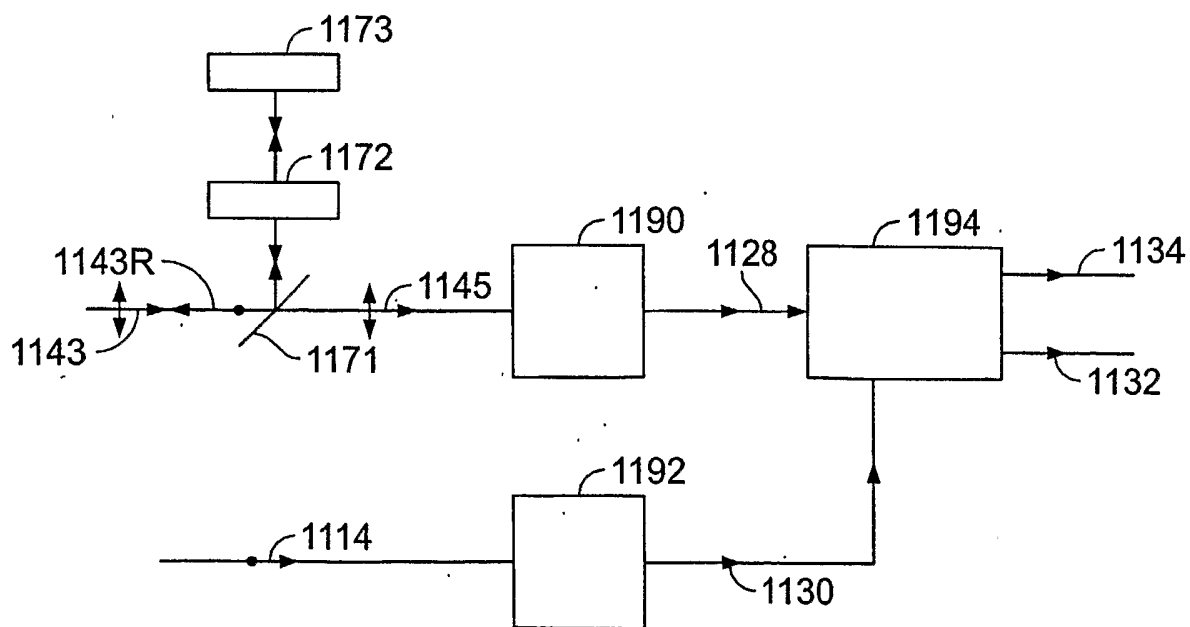


FIG. 11D

22/41

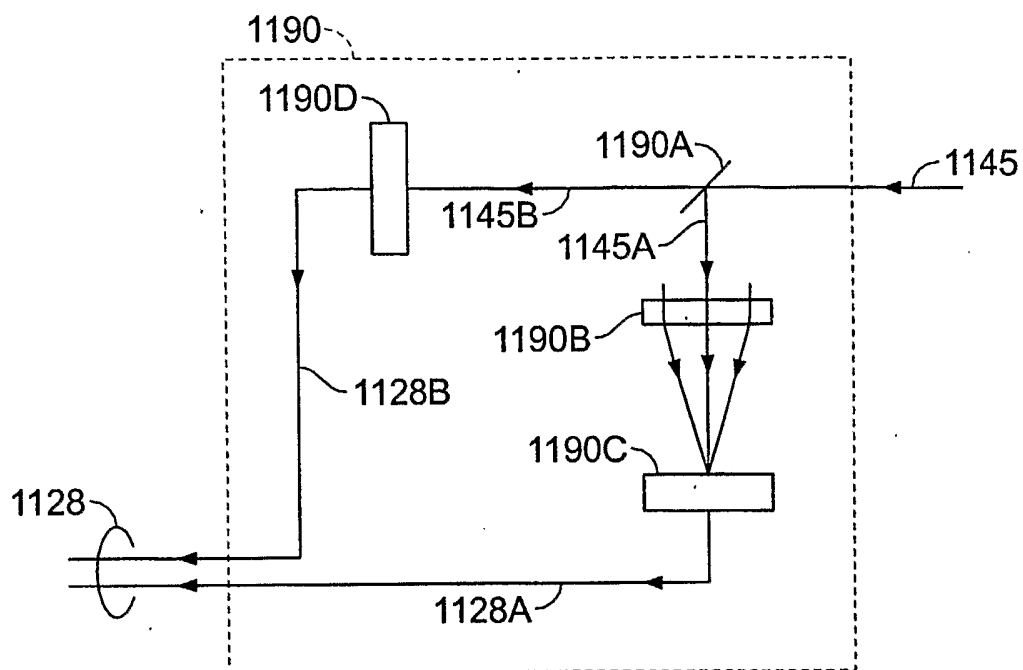


FIG. 11E

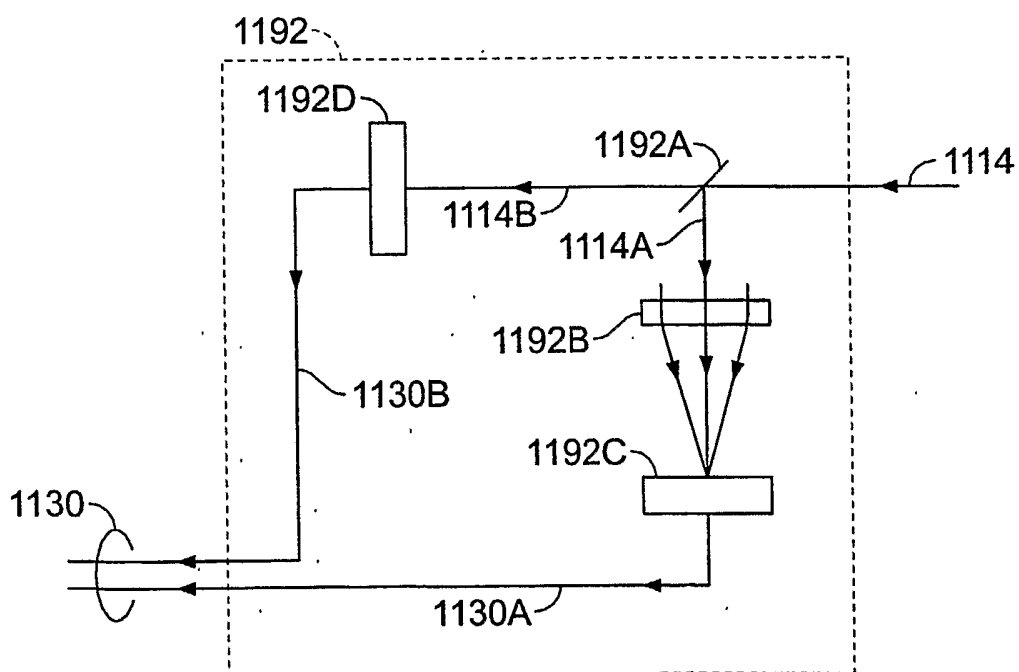


FIG. 11F

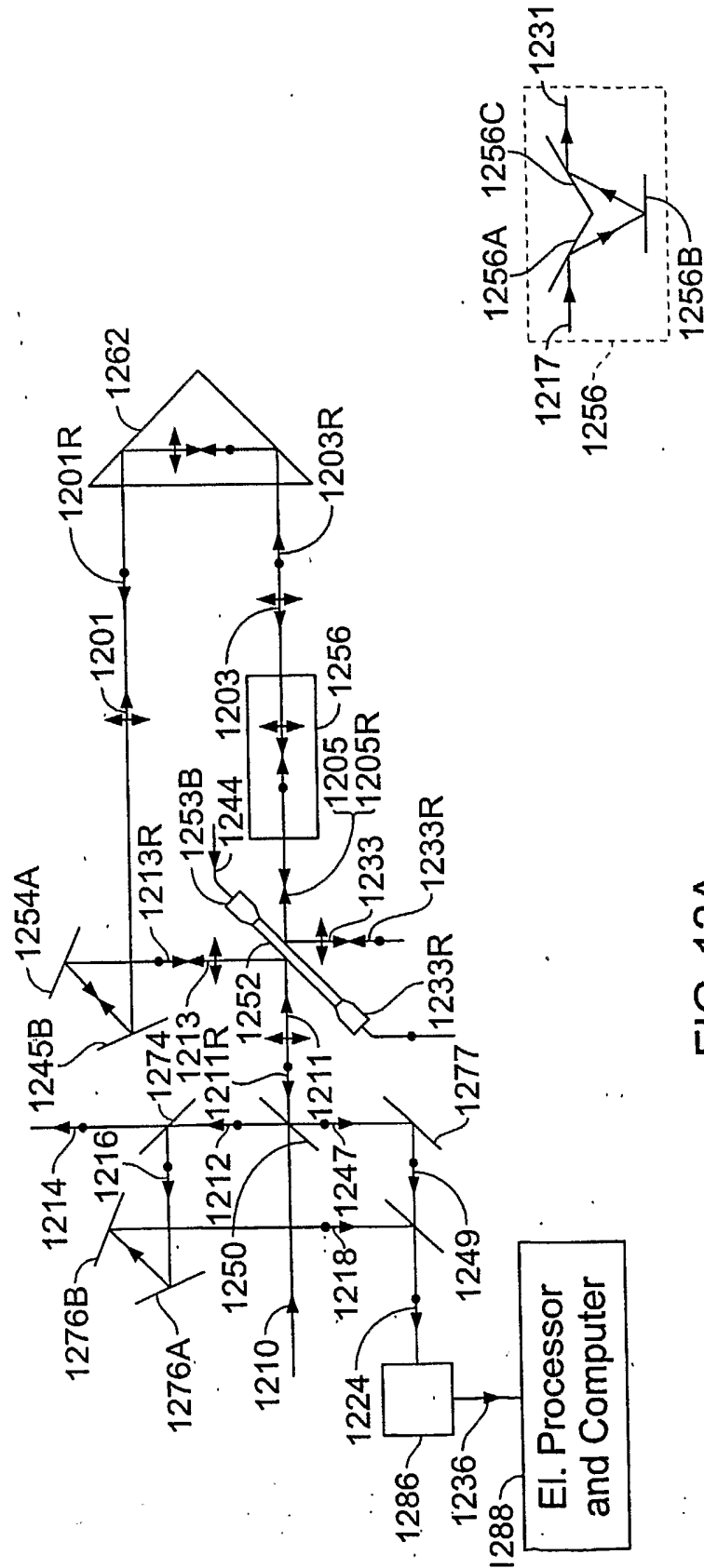


FIG. 12A

FIG. 12B

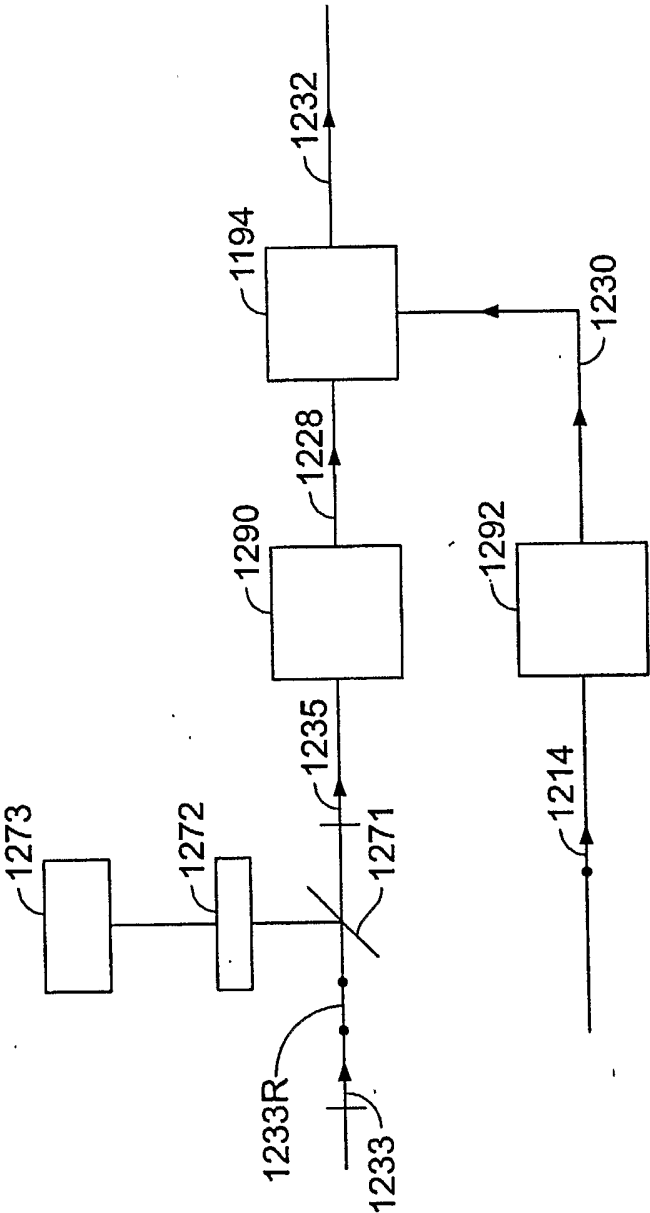


FIG. 12C

25/41

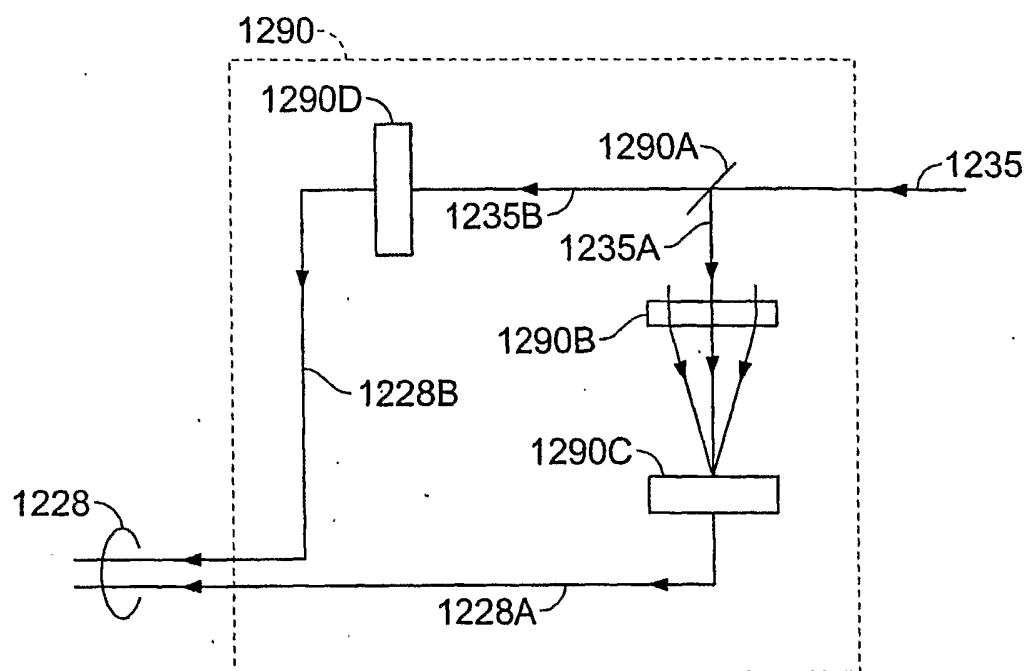


FIG. 12D

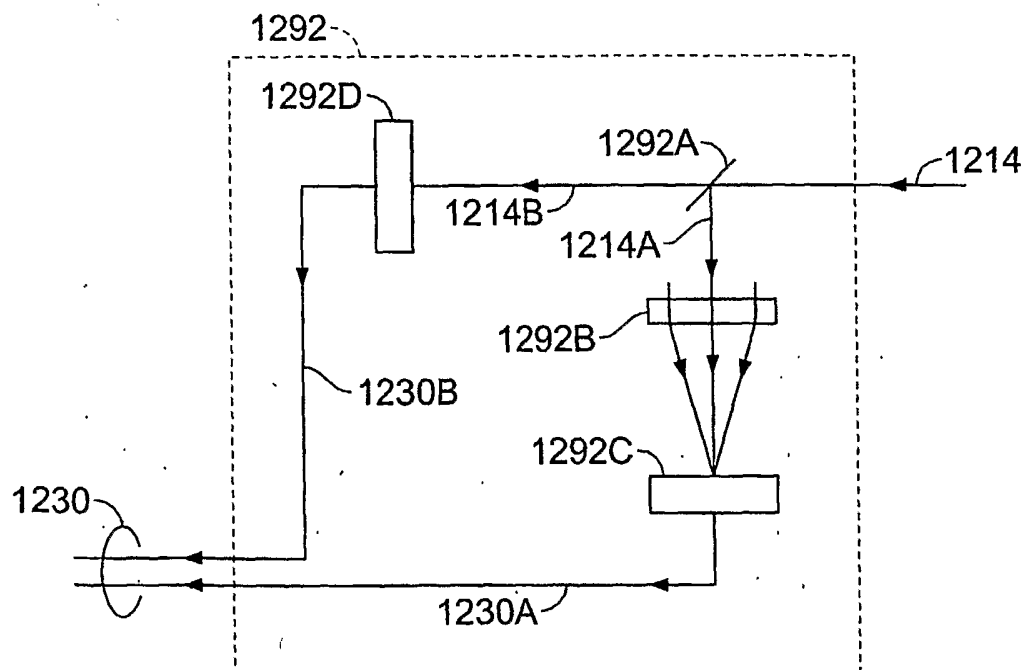


FIG. 12E

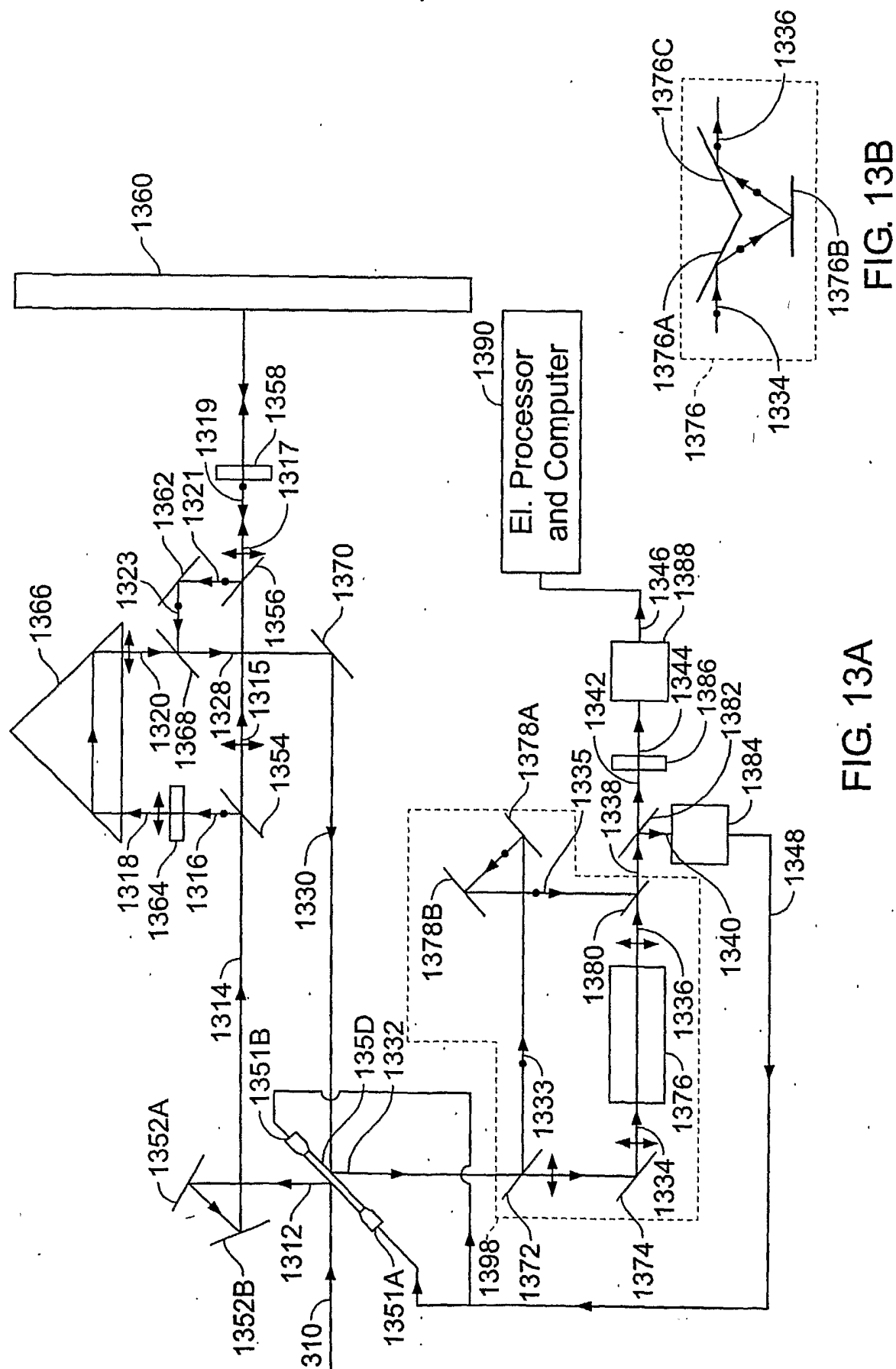


FIG. 13A

FIG. 13B

27/41

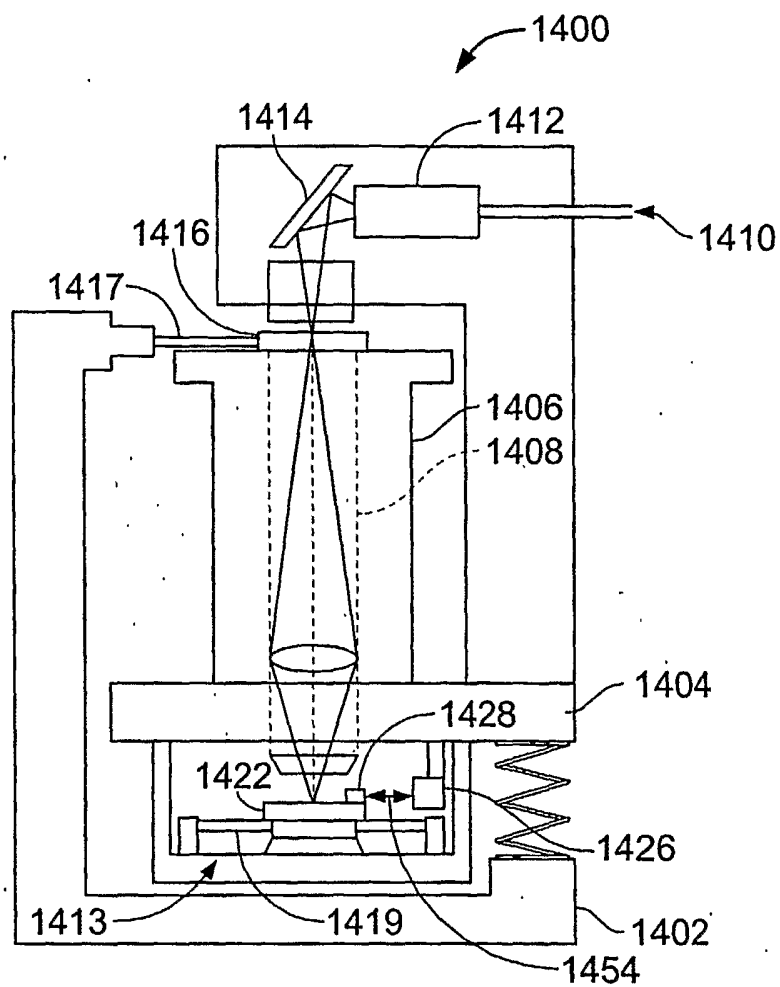


FIG. 14A

28/41

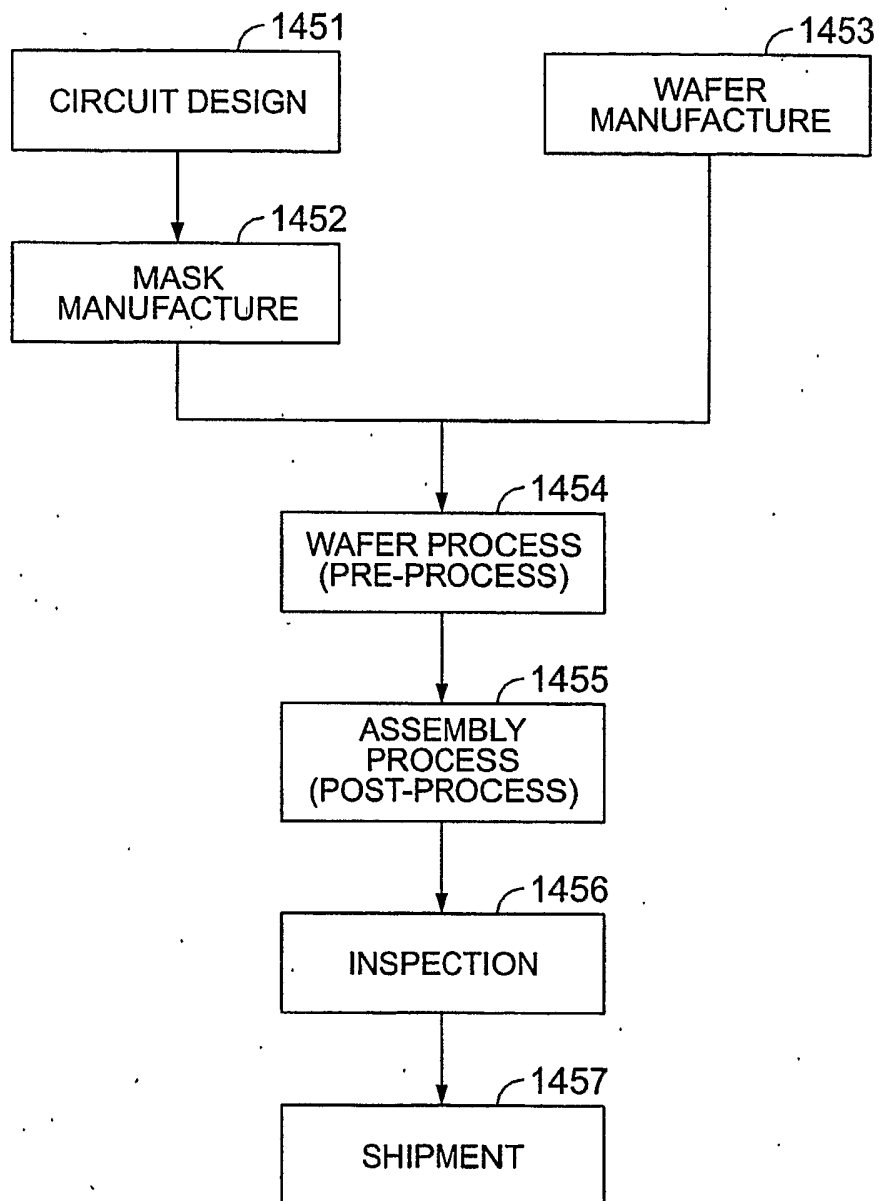


FIG. 14B

29/41

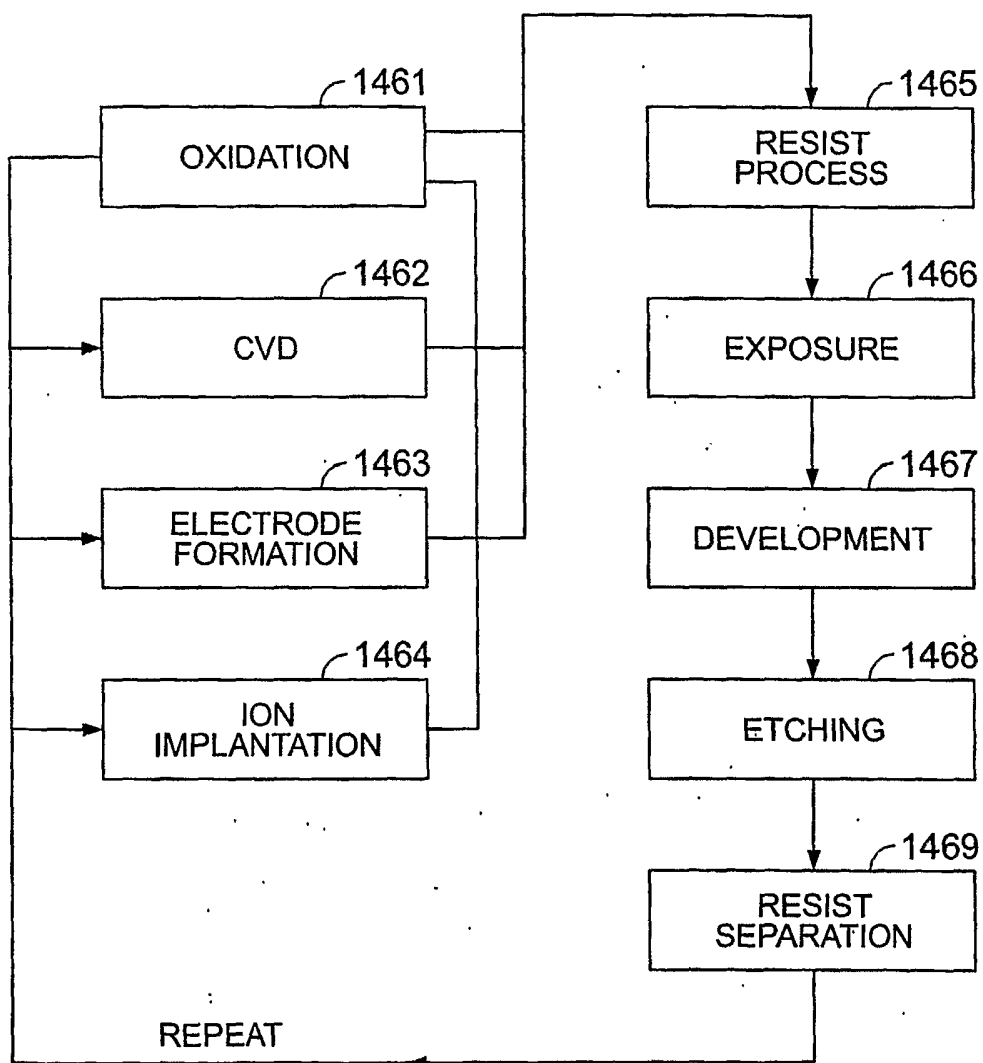


FIG. 14C

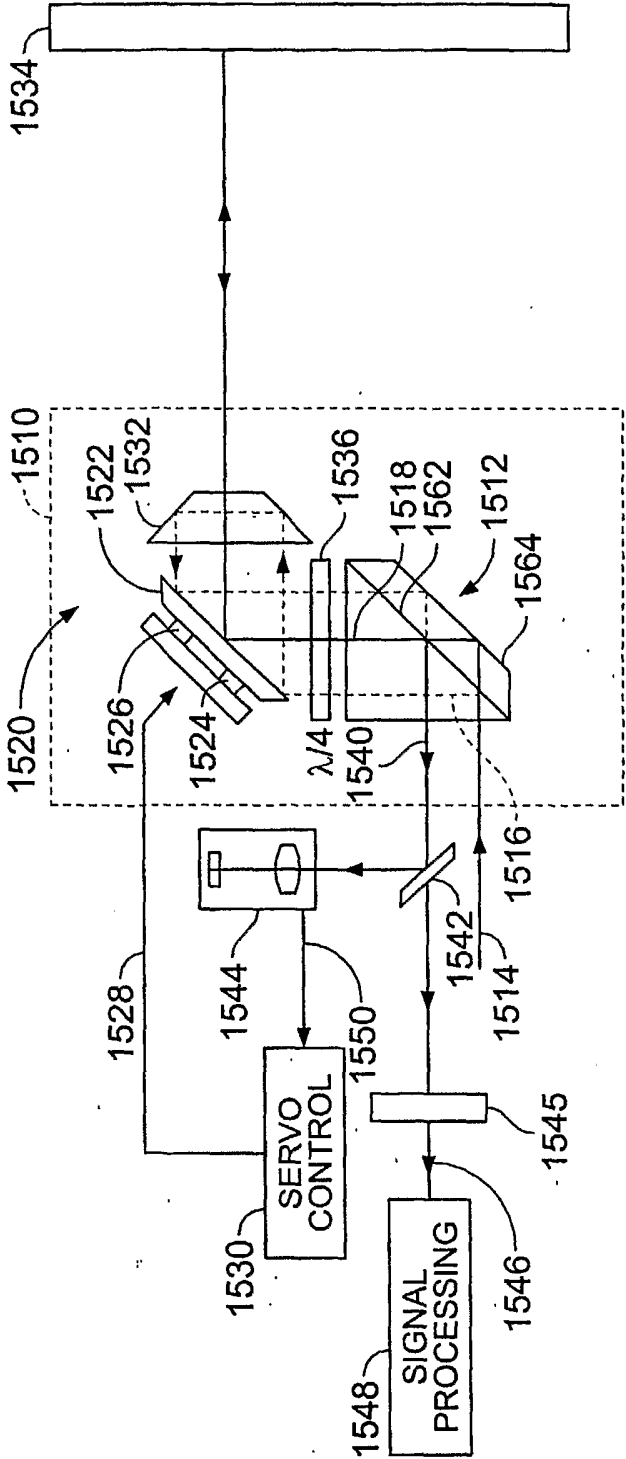


FIG. 15A

31/41

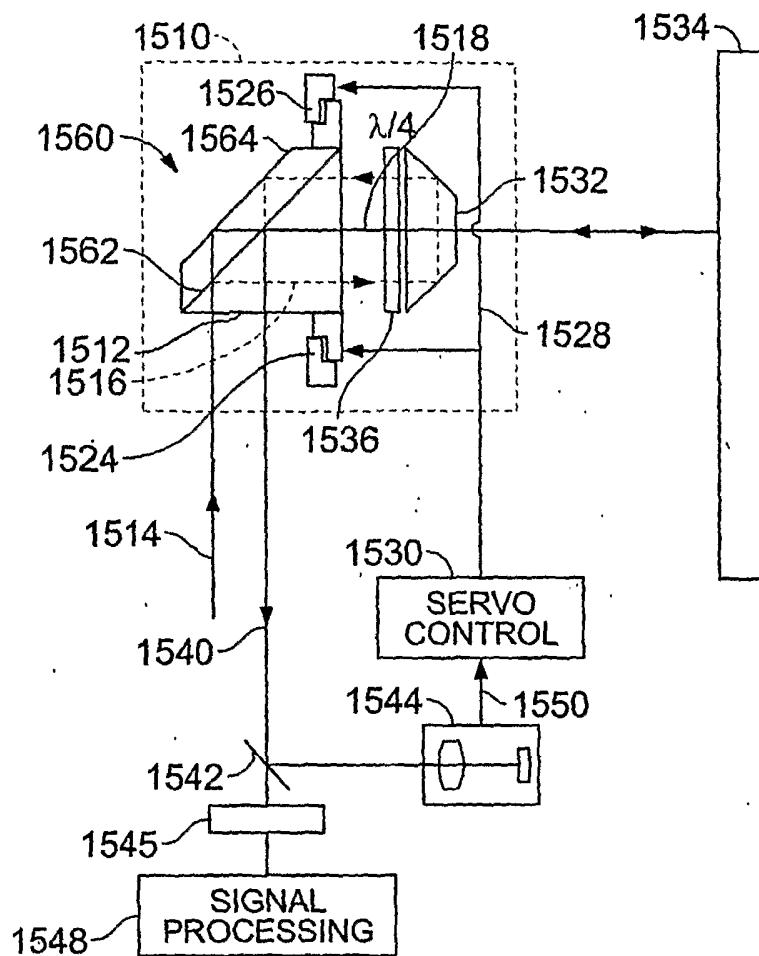


FIG. 15B

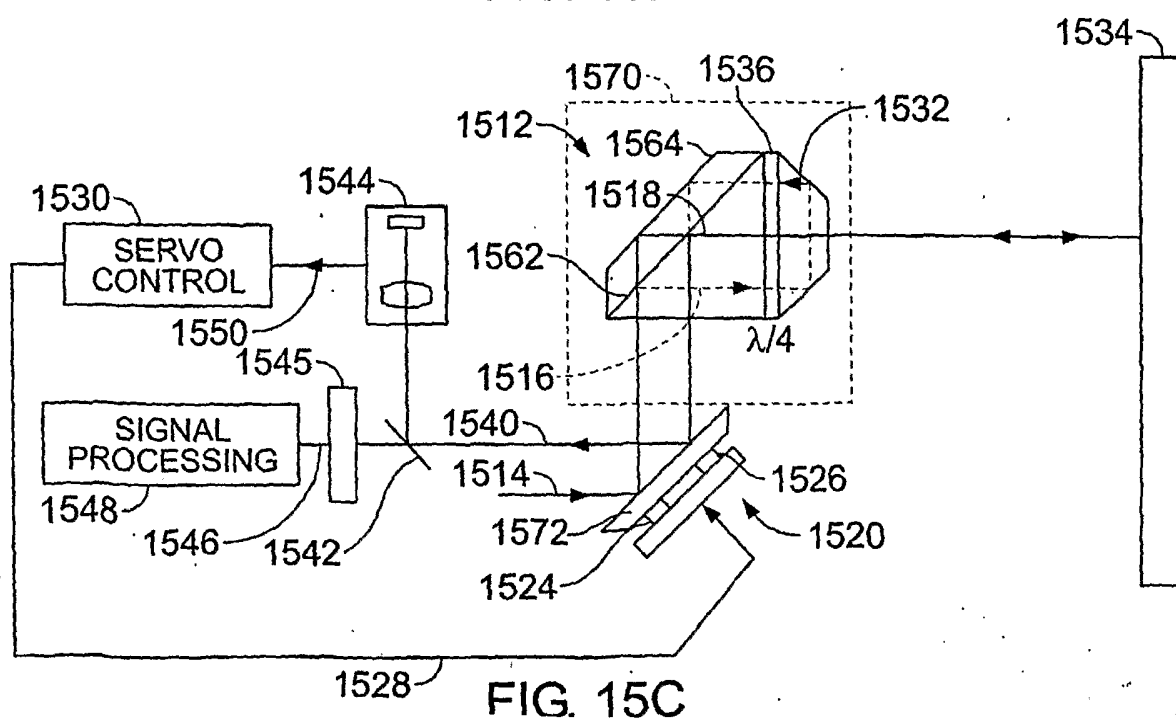


FIG. 15C

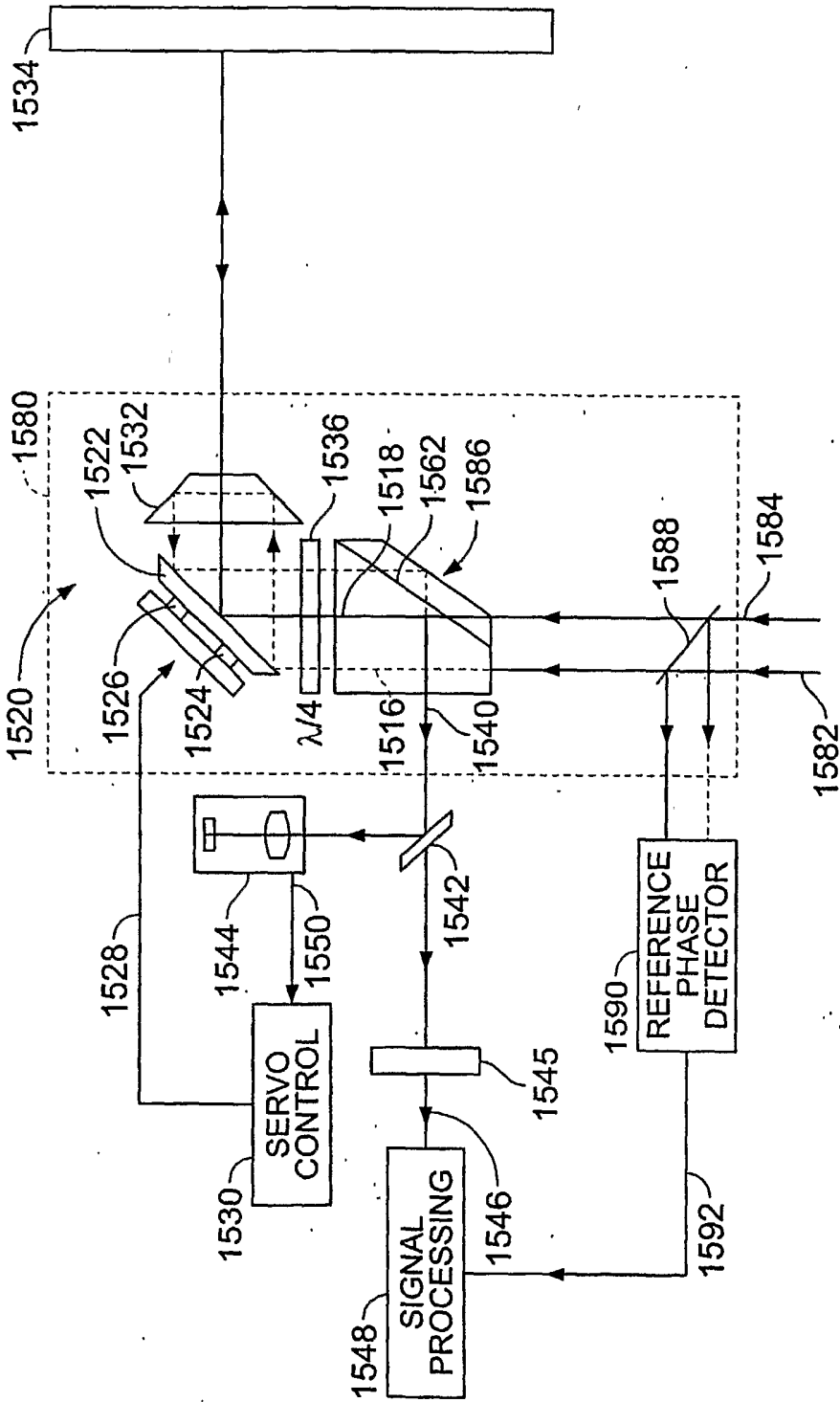


FIG. 15D

33/41

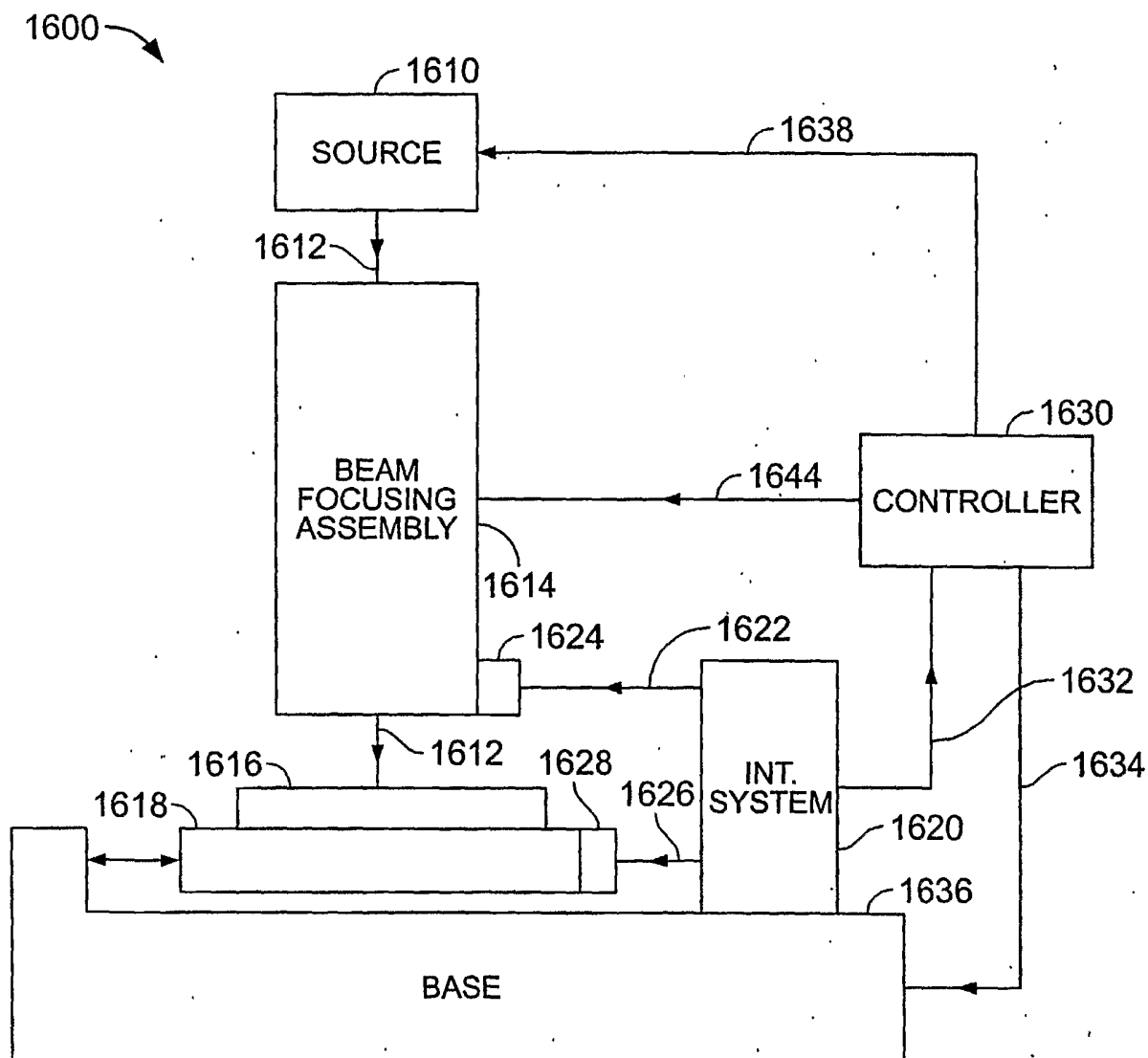


FIG. 16

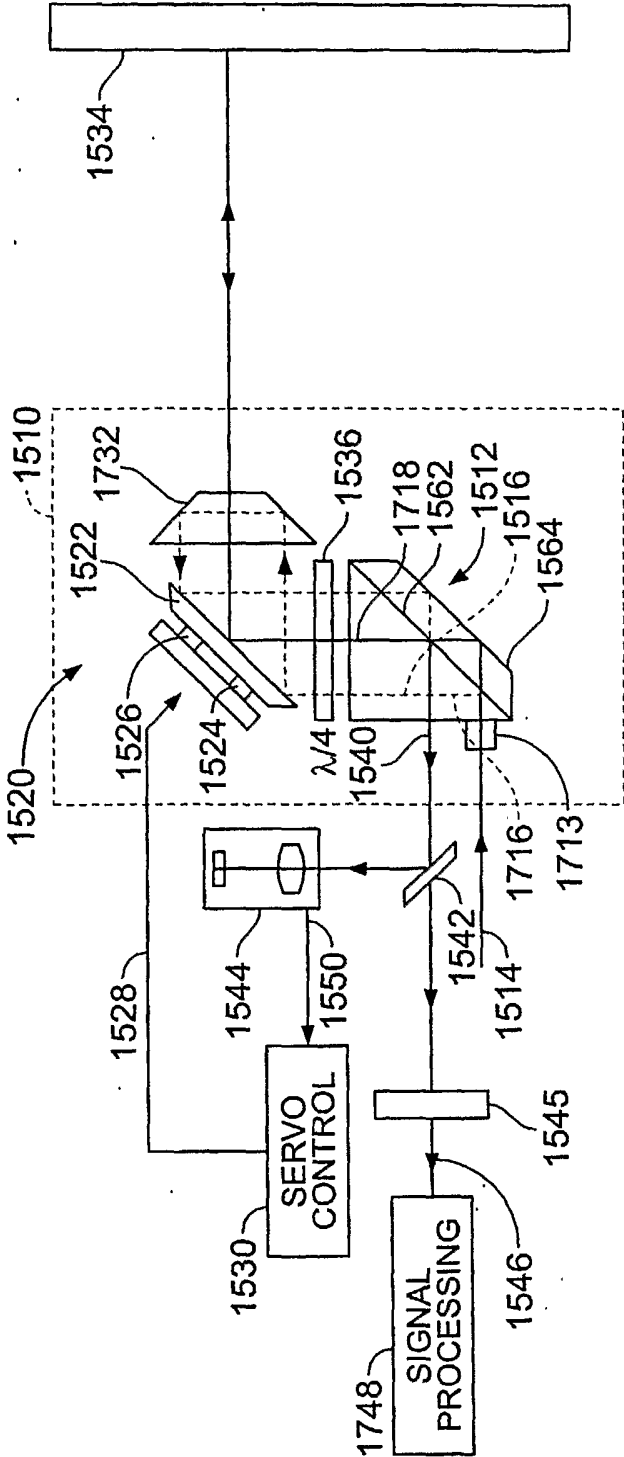


FIG. 17A

35/41

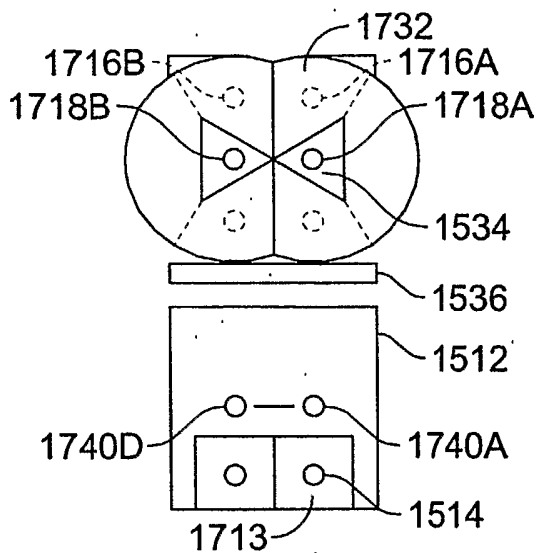


FIG. 17B

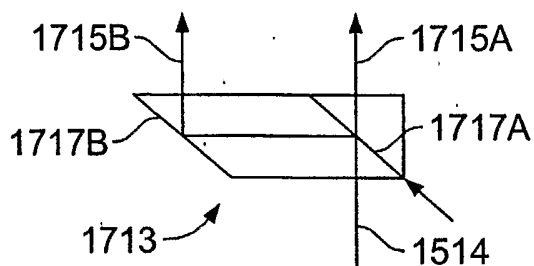


FIG. 17C

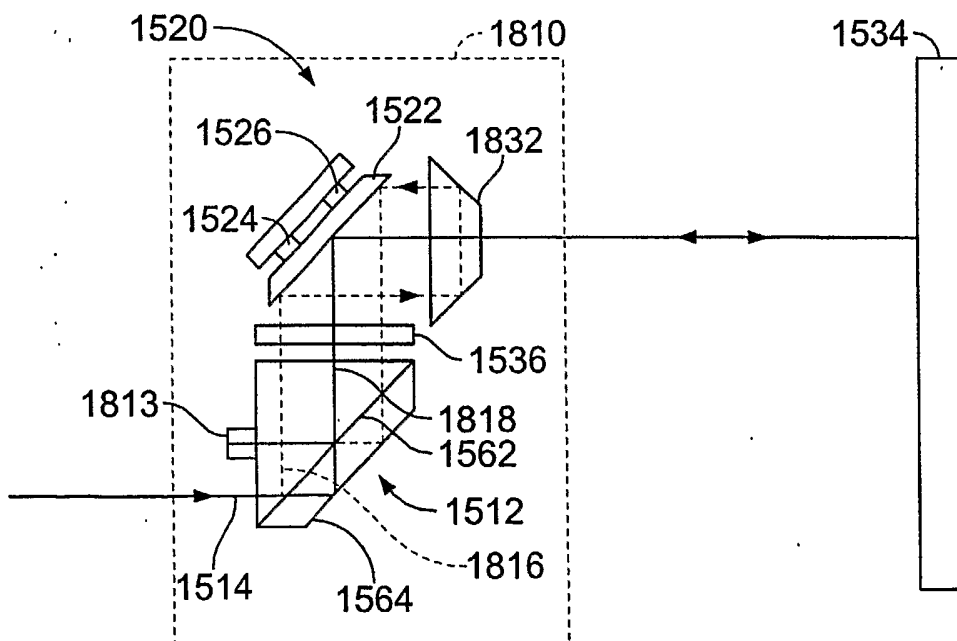


FIG. 18A

36/41

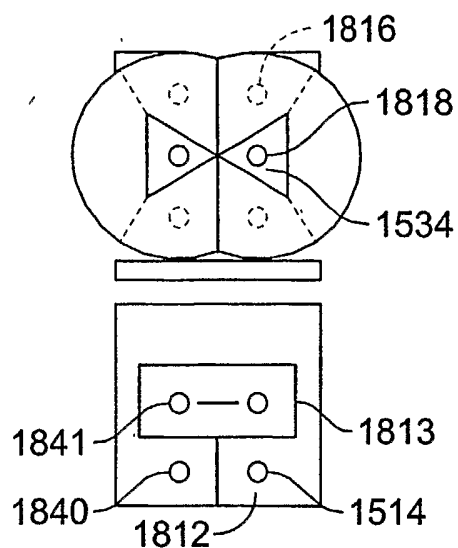


FIG. 18B

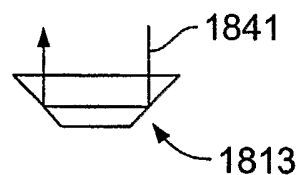


FIG. 18C

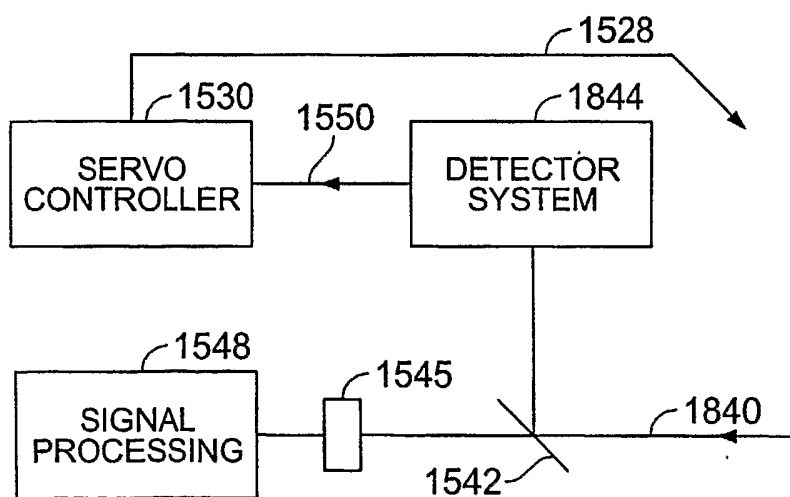


FIG. 18D

37/41

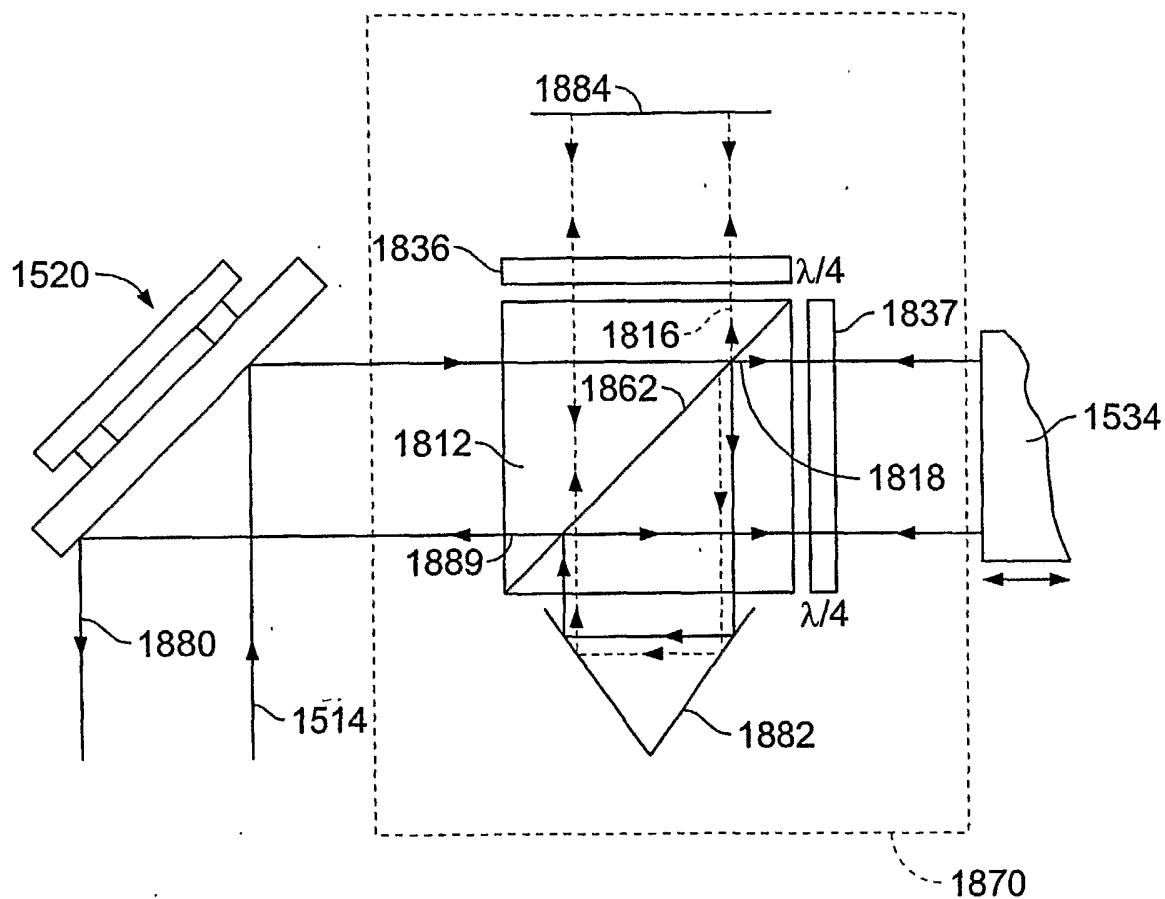


FIG. 18E

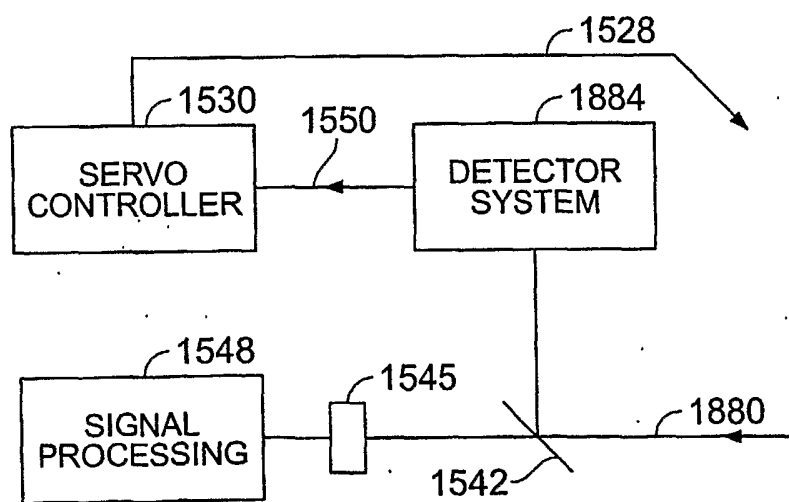
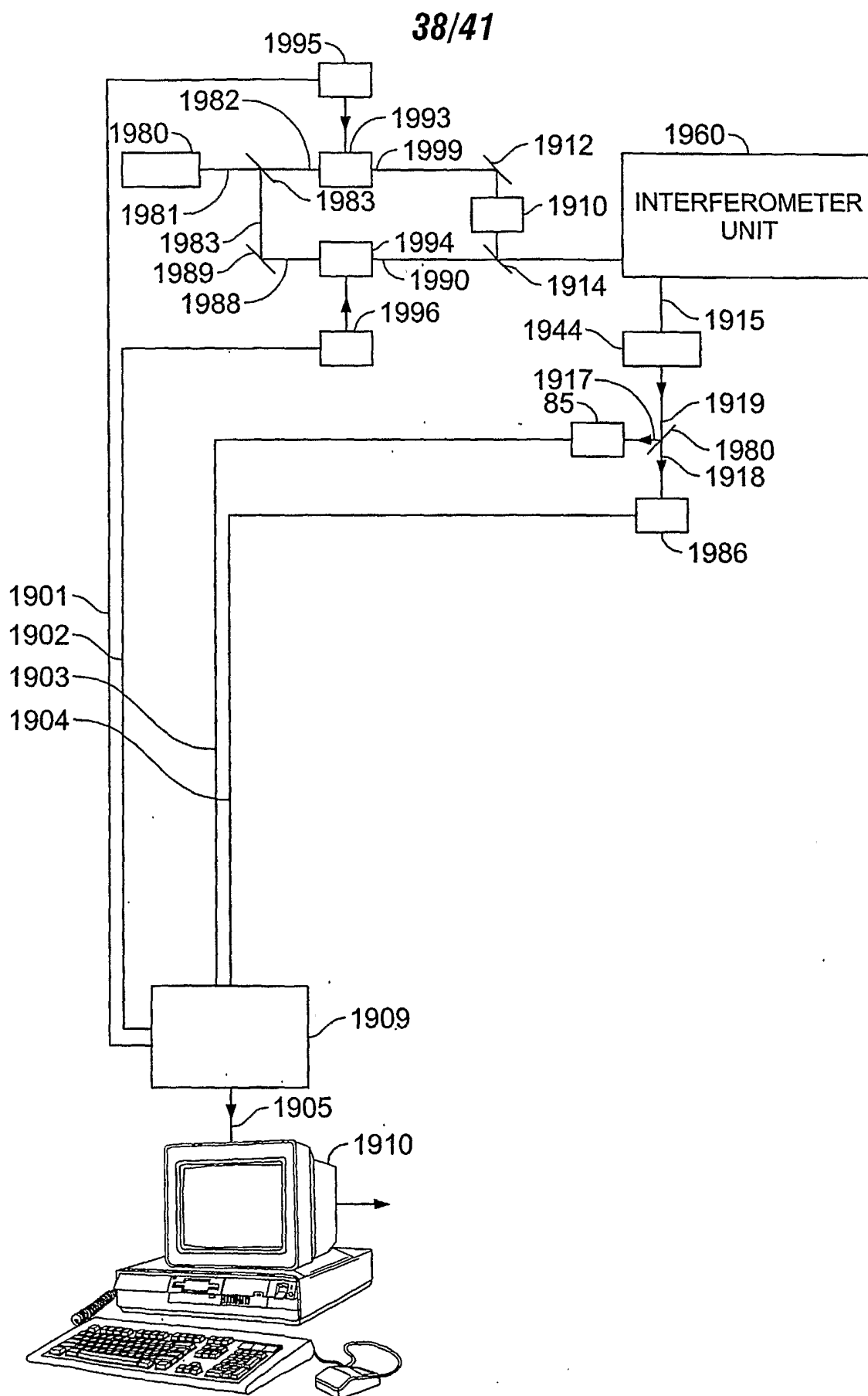


FIG. 18F



39/41

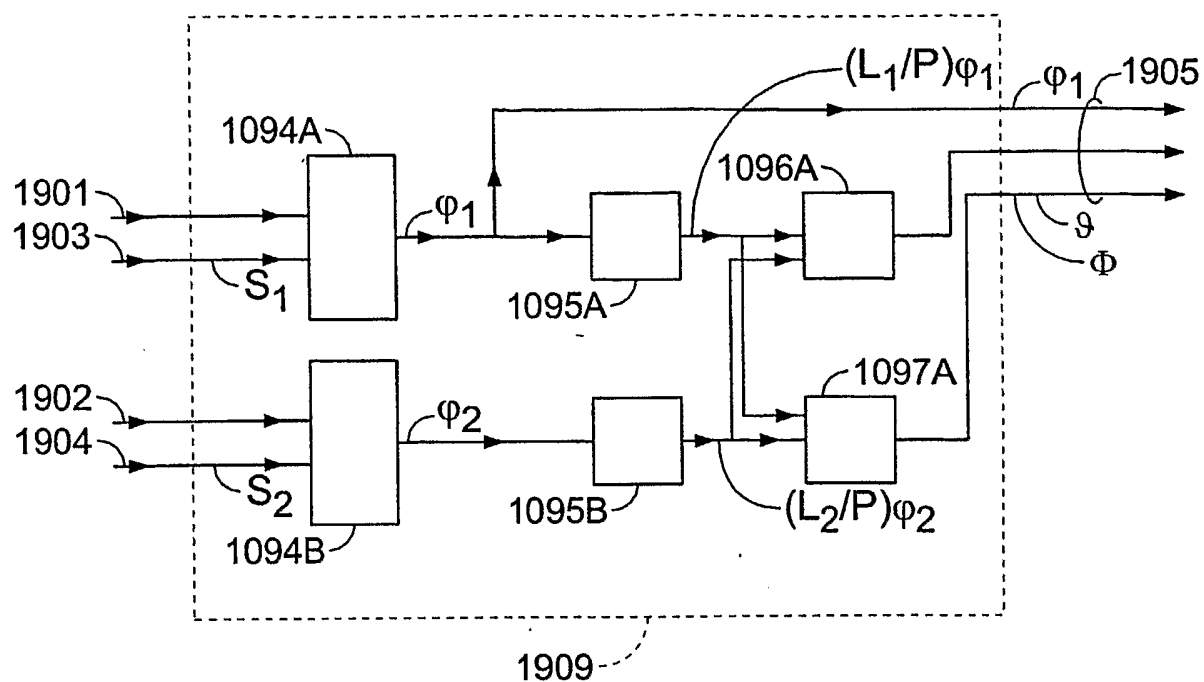
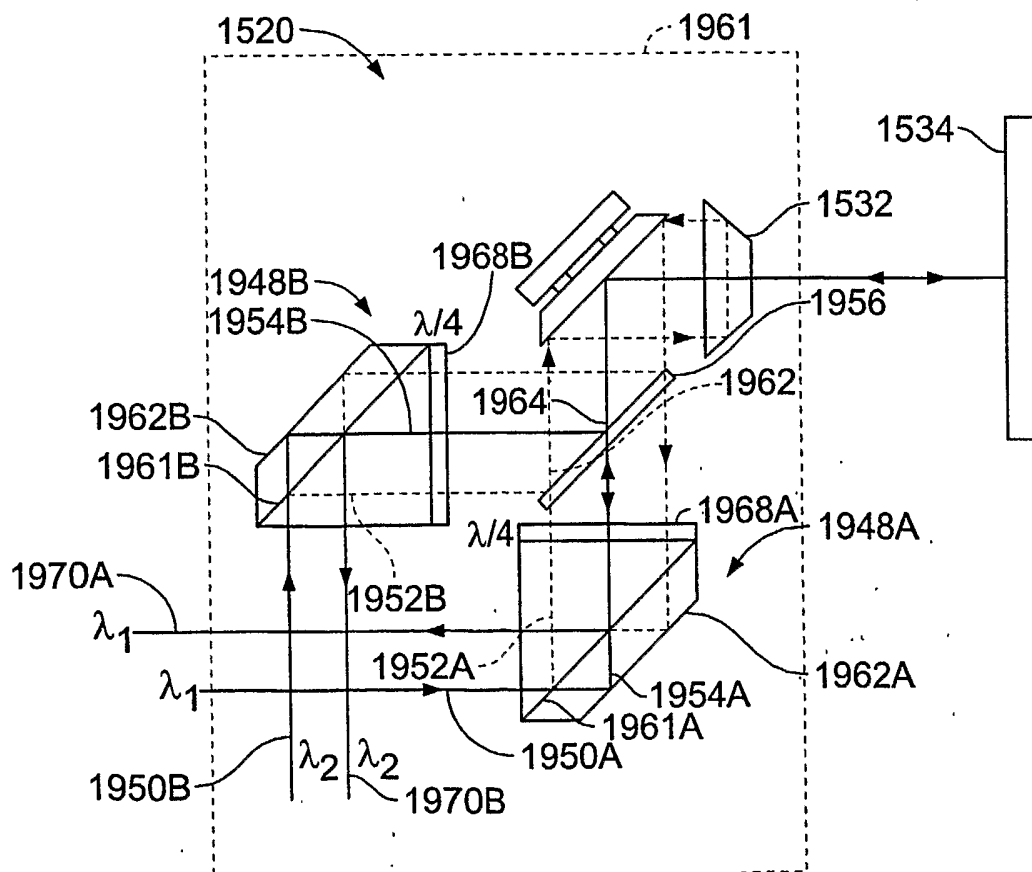


FIG. 19B



40/41

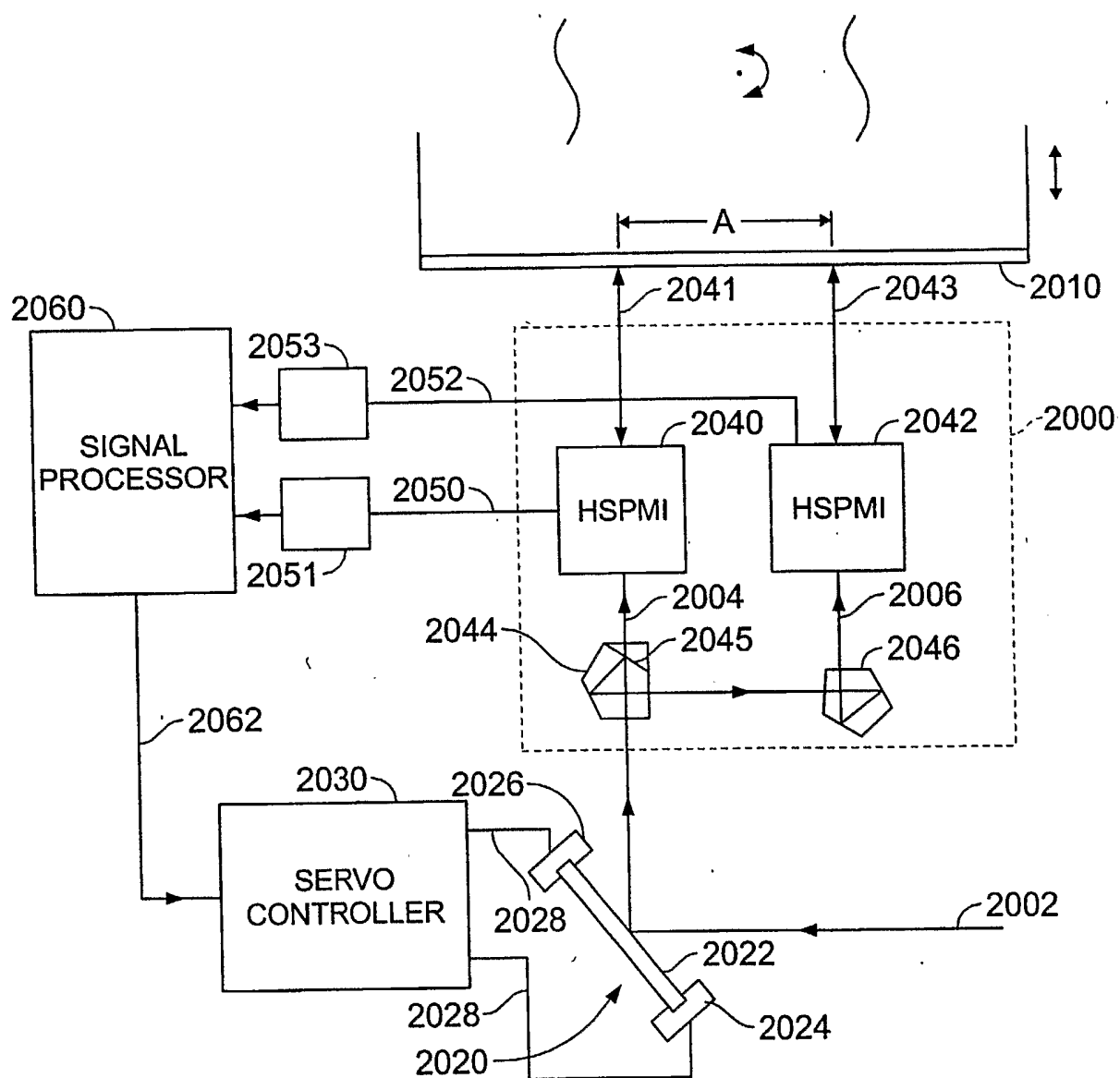


FIG. 20

41/41

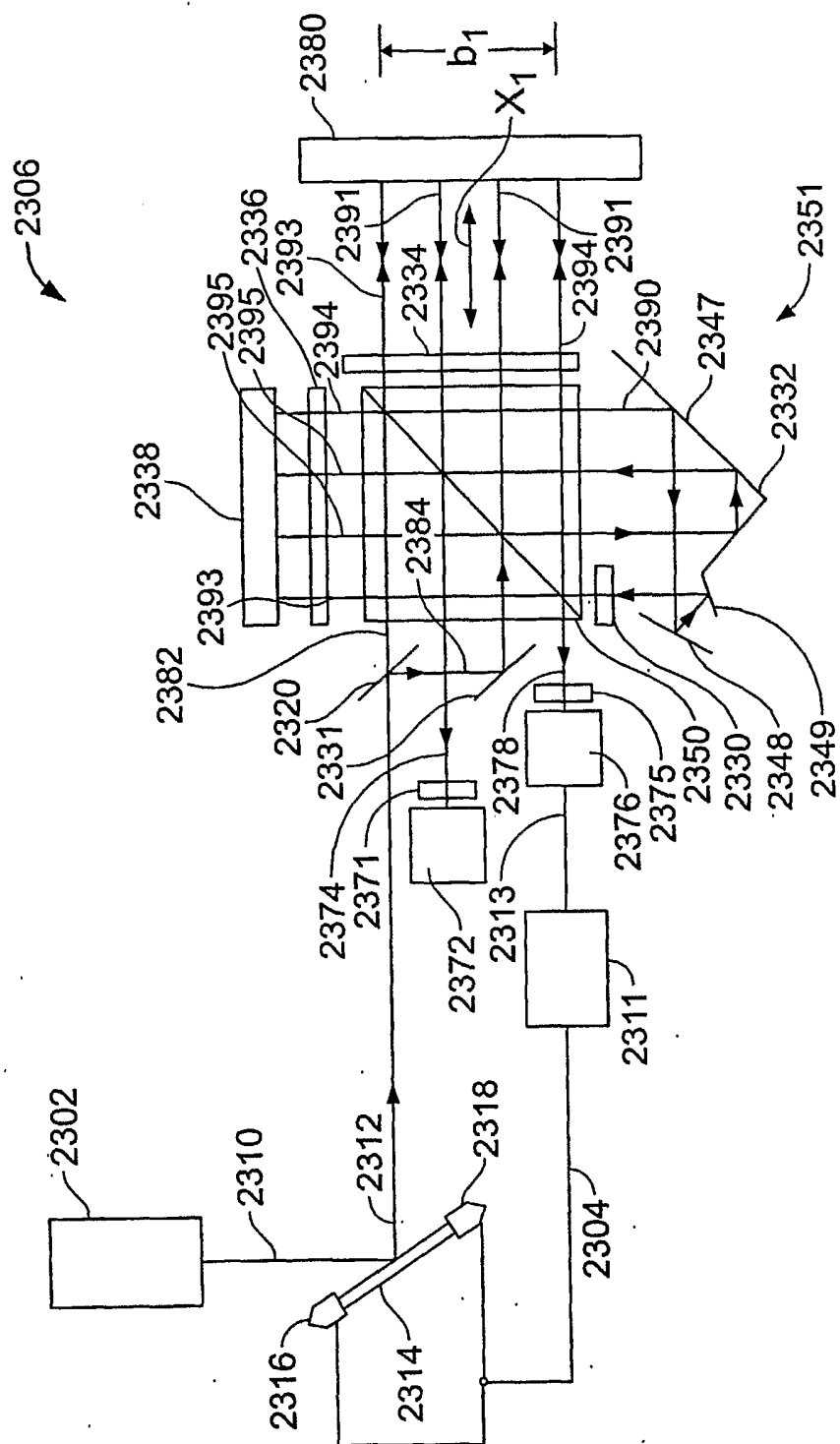


FIG. 21