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**Liao et al.**

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(54) **OPTICAL IMAGE CAPTURING SYSTEM**

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**G02B 13/00** (2006.01)

**G02B 9/60** (2006.01)

(52) **U.S. Cl.**

CPC ..... **G02B 13/0045** (2013.01); **G02B 9/60** (2013.01)

(58) **Field of Classification Search**

CPC ..... G02B 13/0045; G02B 9/60

USPC ..... 359/746, 763-769

See application file for complete search history.

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*Primary Examiner* — Scott J Sugarman

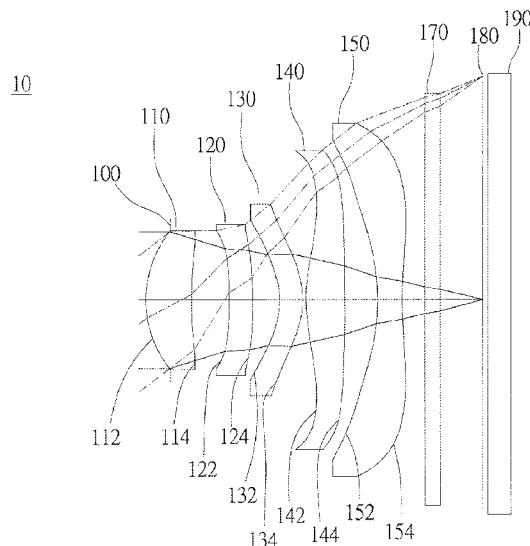
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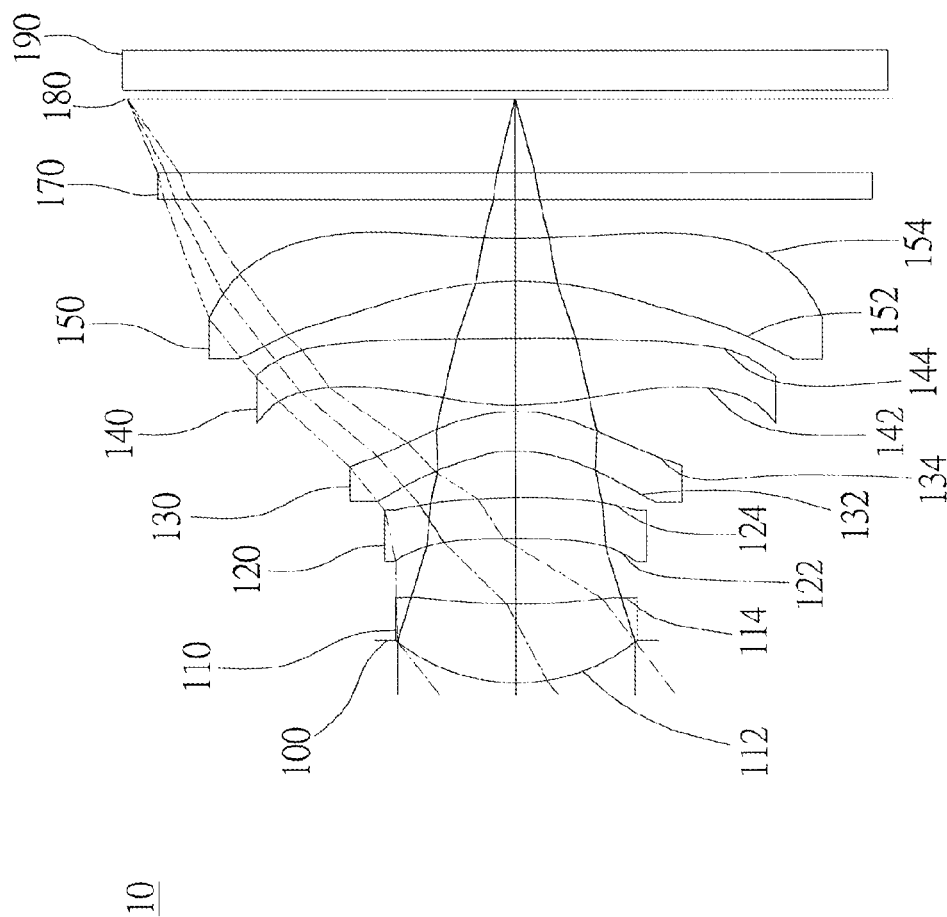
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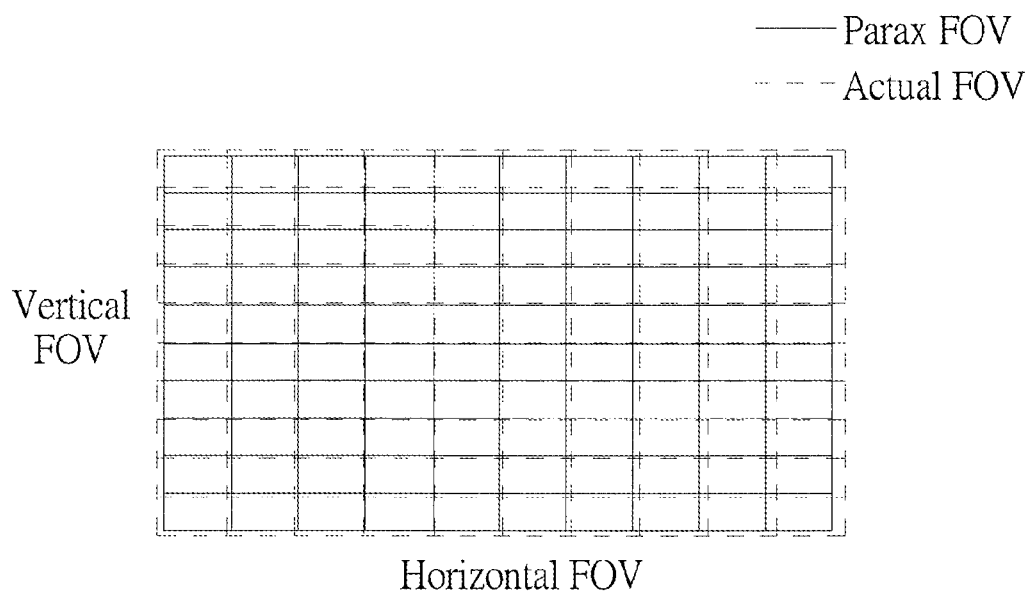
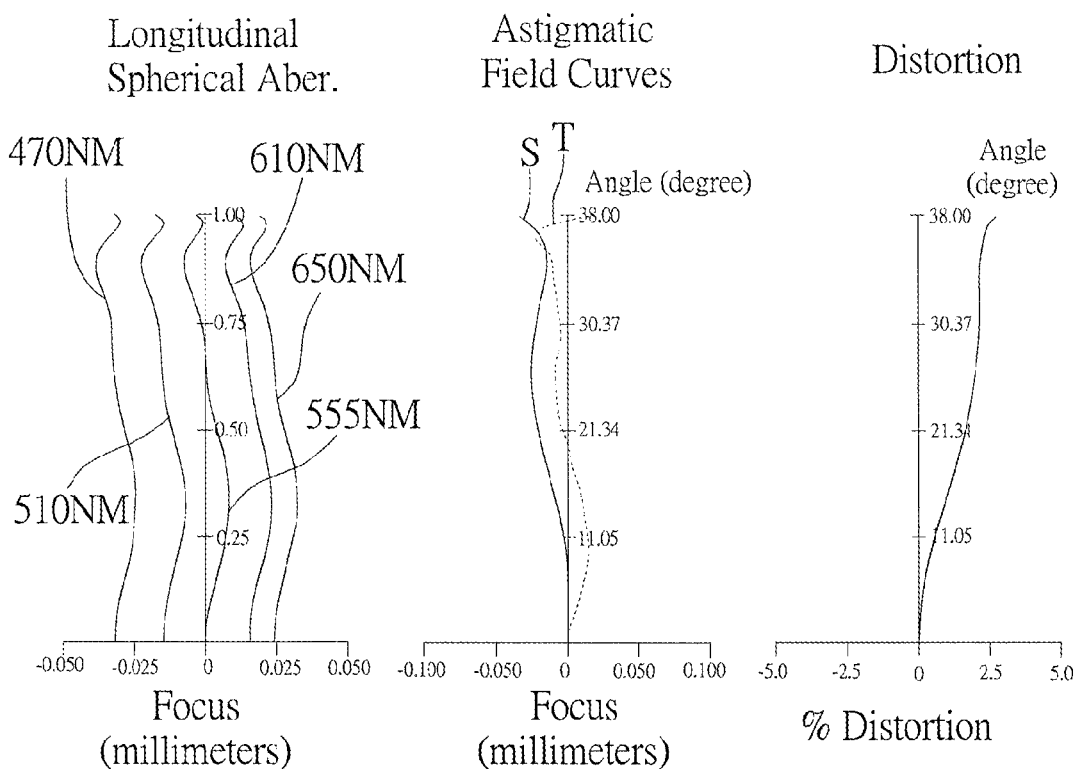
(57) **ABSTRACT**

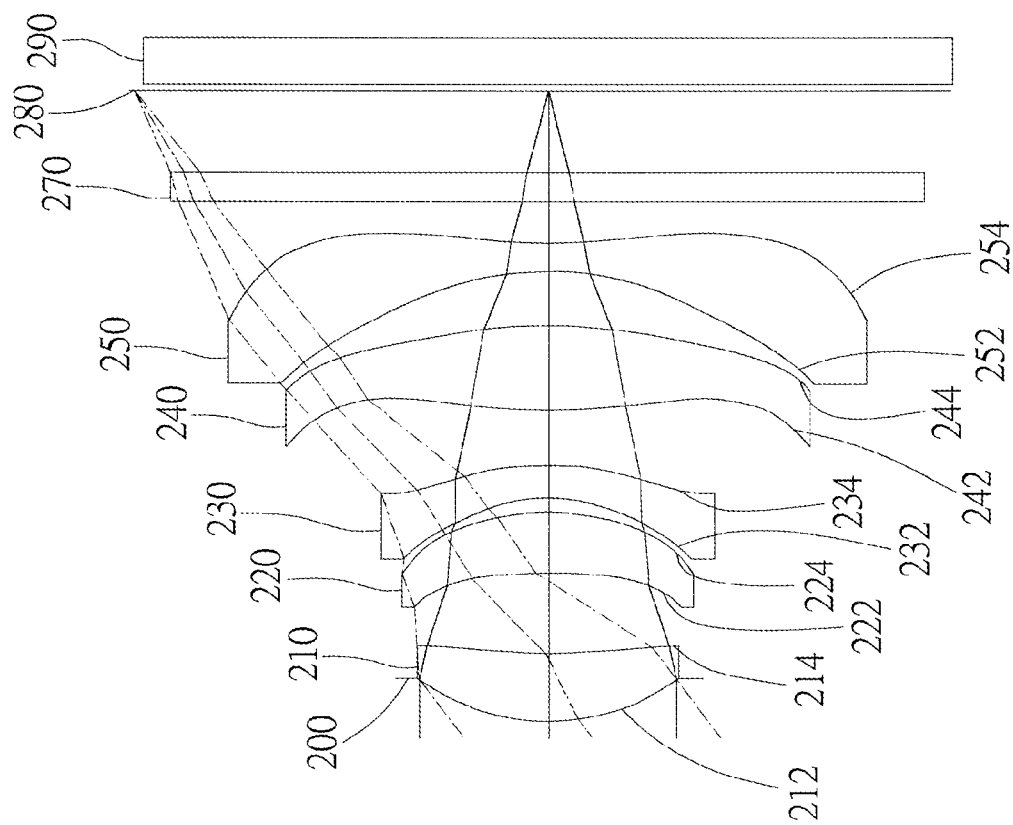
A five-piece optical lens for capturing image and a five-piece optical module for capturing image, along the optical axis in order from an object side to an image side, include a first lens with positive refractive power having a convex object-side surface; a second lens with refractive power; a third lens with refractive power; a fourth lens with refractive power; and a fifth lens with negative refractive power; and at least one of the image-side surface and object-side surface of each of the five lens elements are aspheric. The optical lens can increase aperture value and improve the imagining quality for use in compact cameras.

**24 Claims, 12 Drawing Sheets**









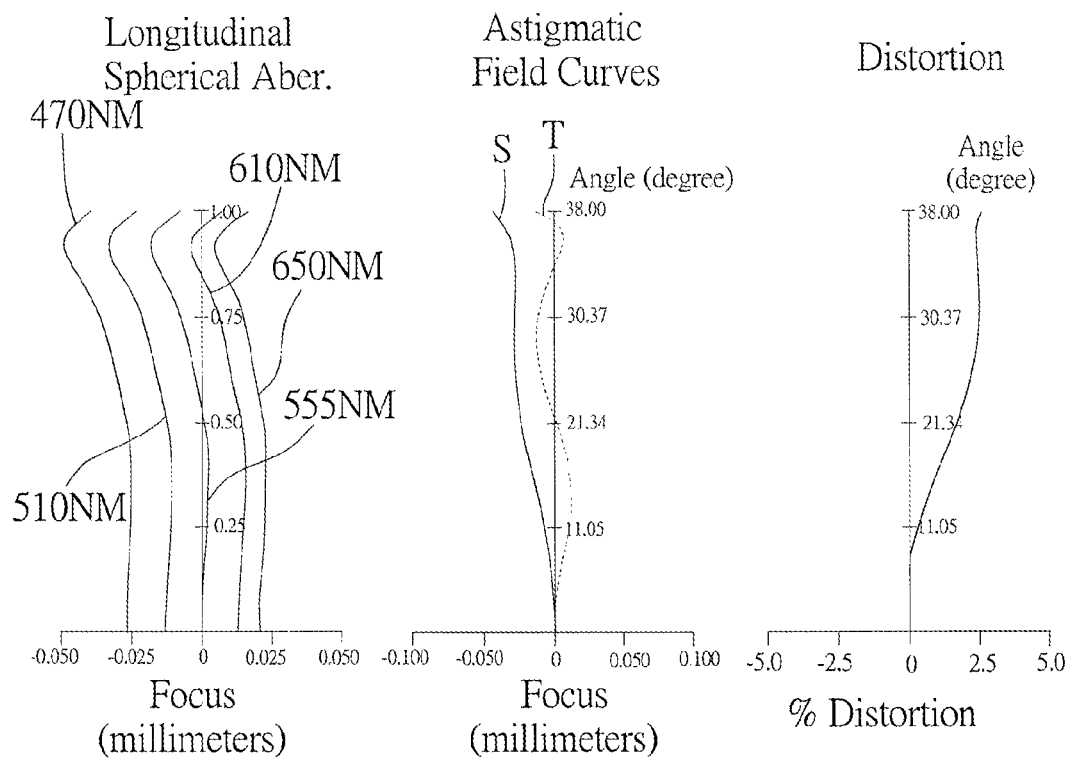


FIG. 2 B

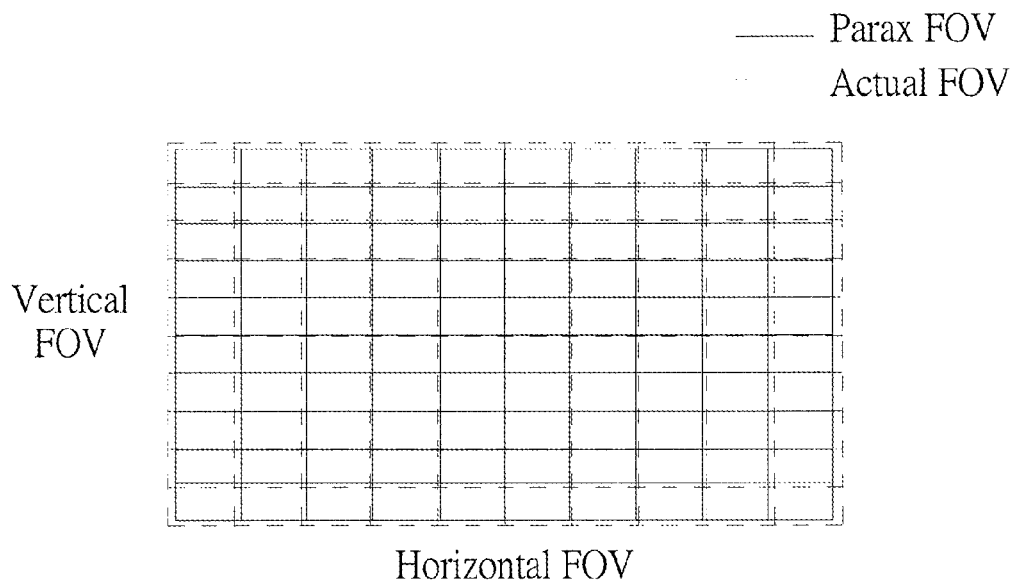


FIG. 2 C

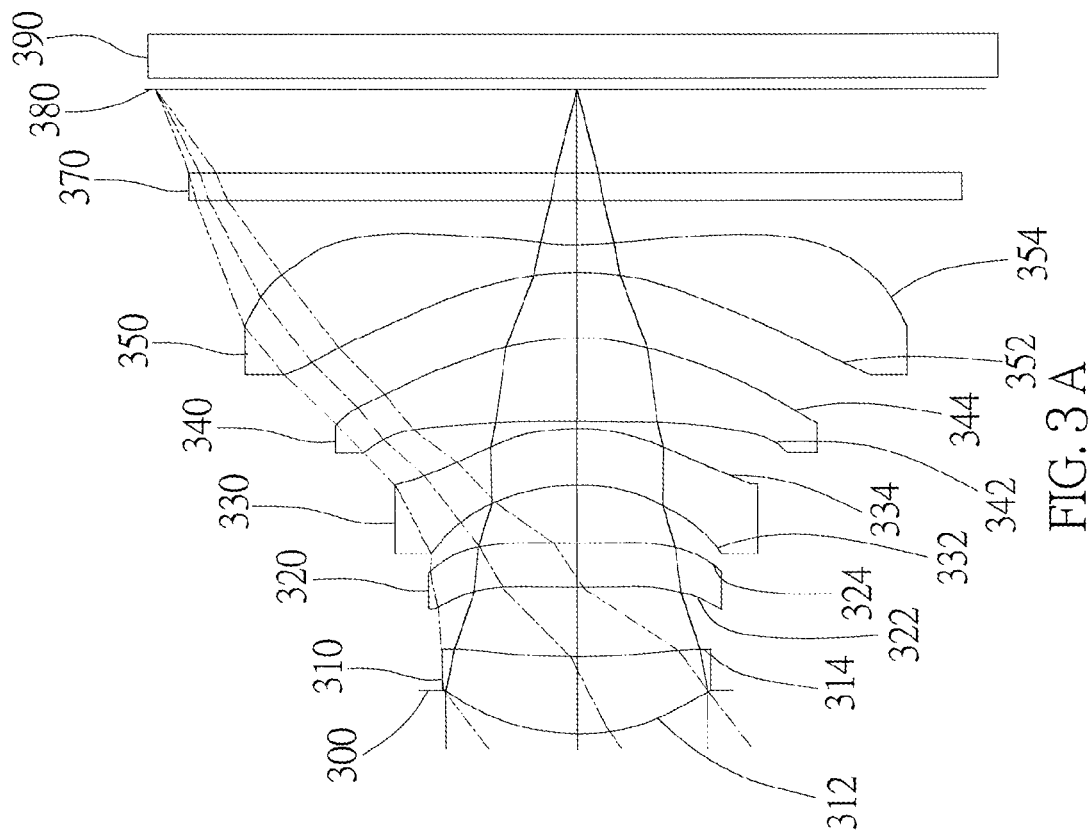


FIG. 3A

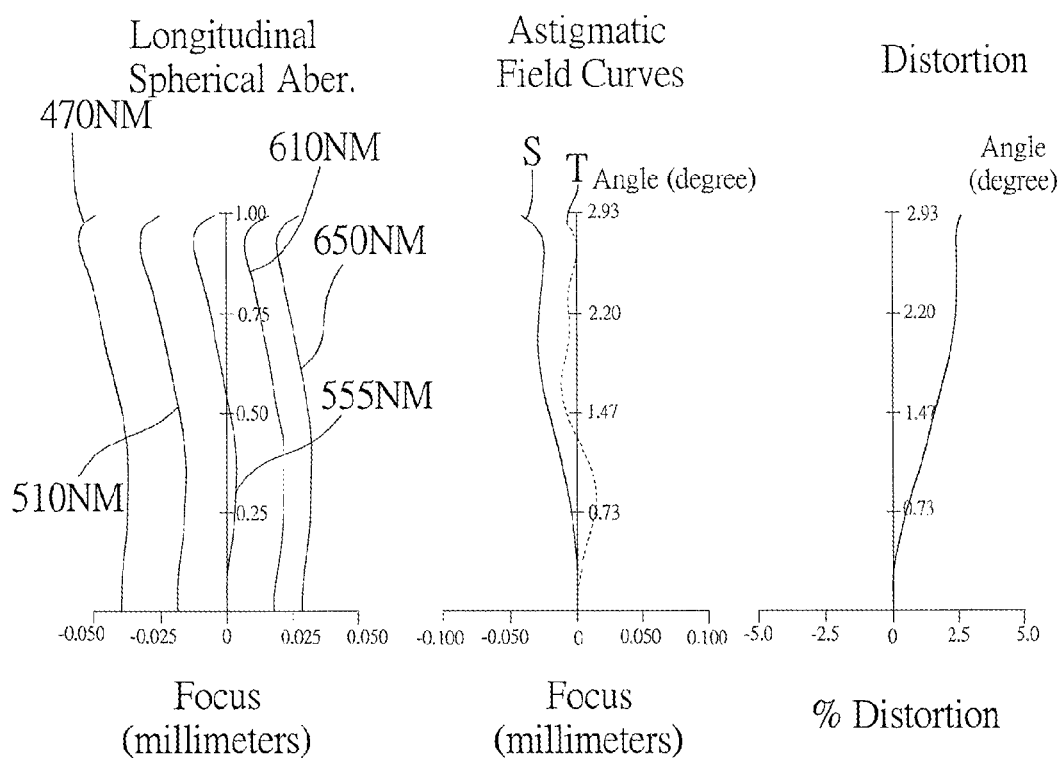


FIG. 3 B

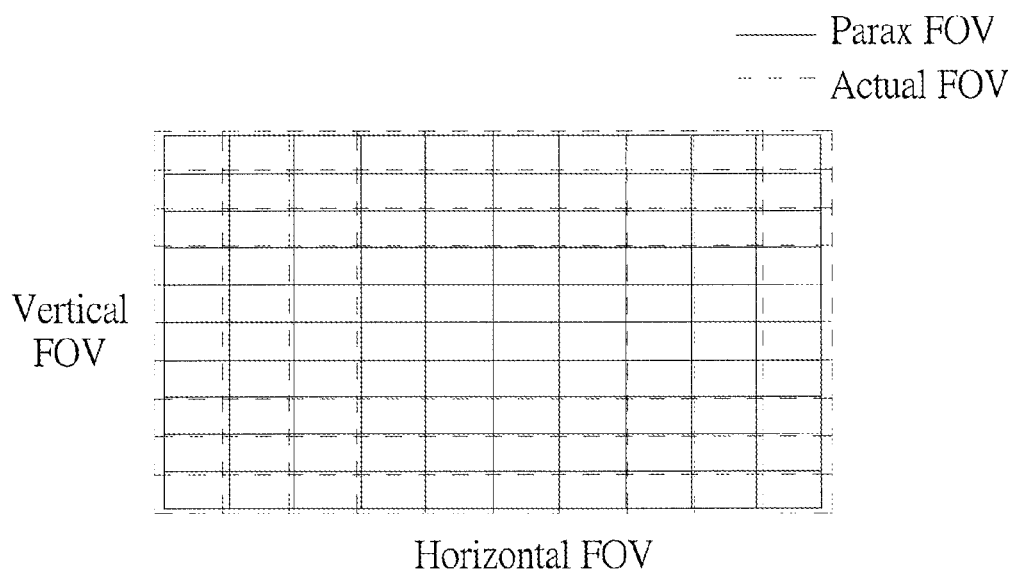


FIG. 3 C

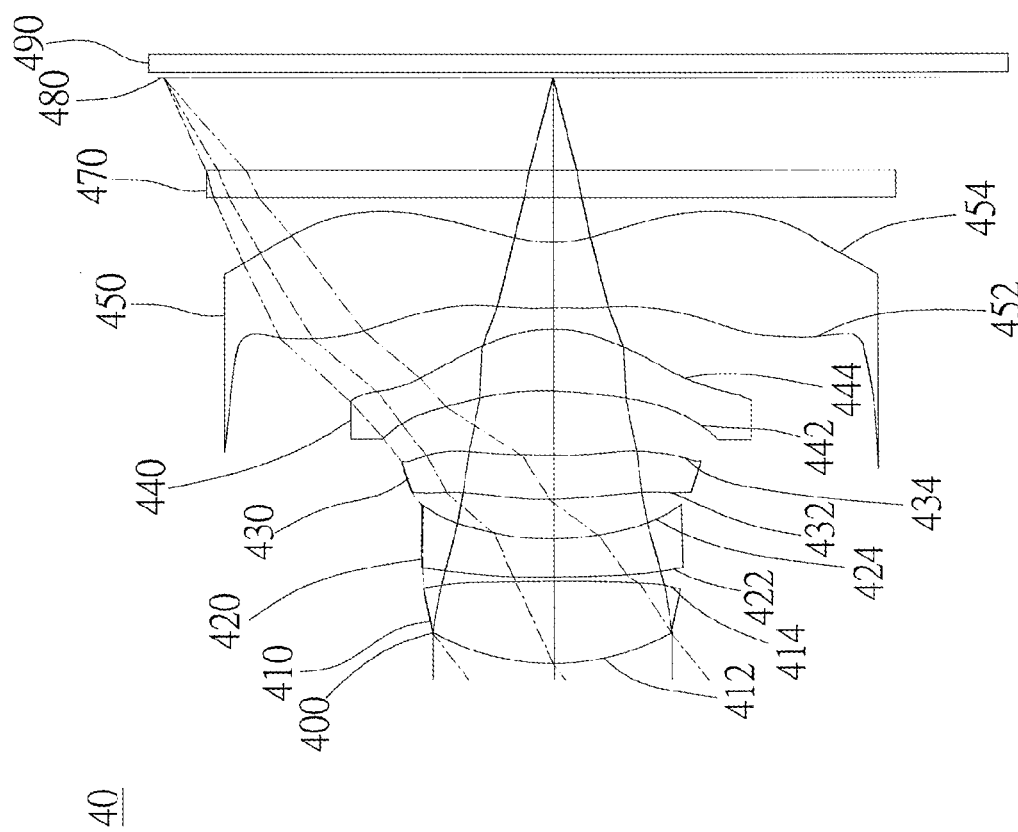


FIG. 4 A



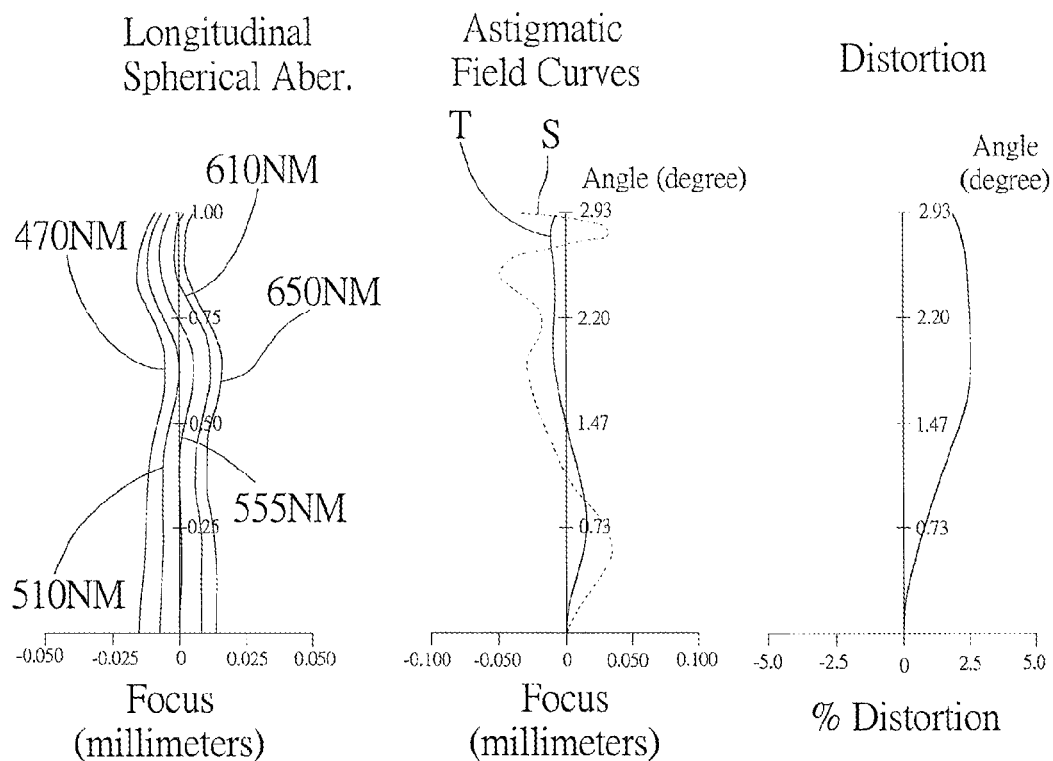


FIG. 4 B

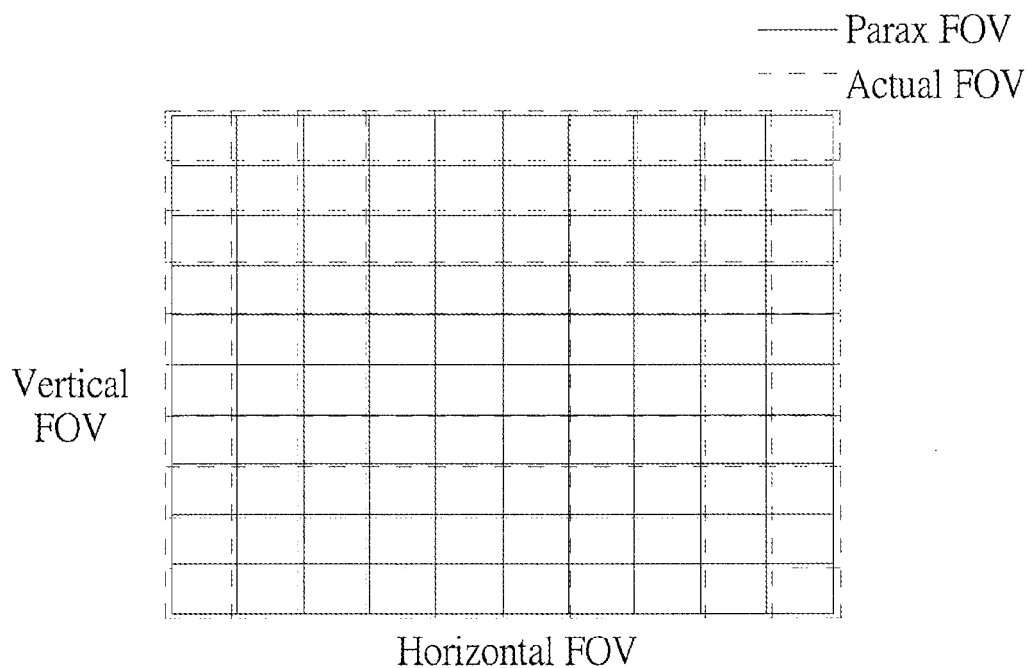


FIG. 4 C

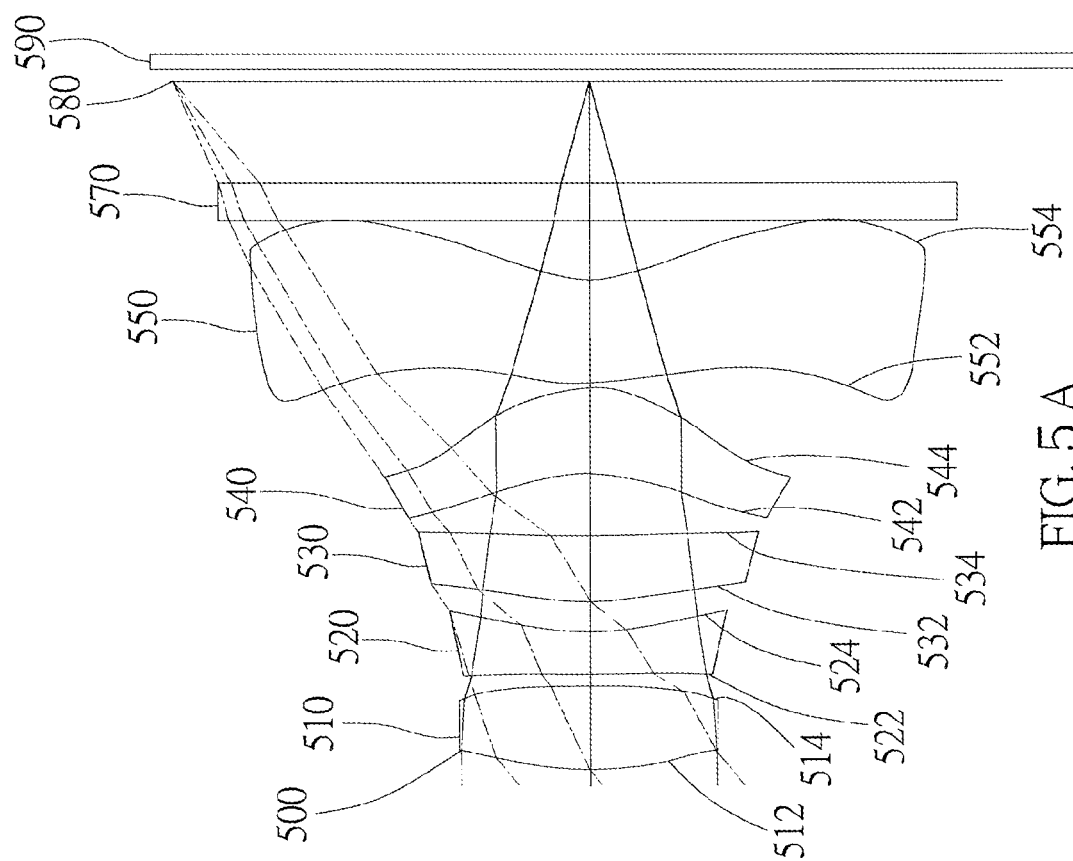
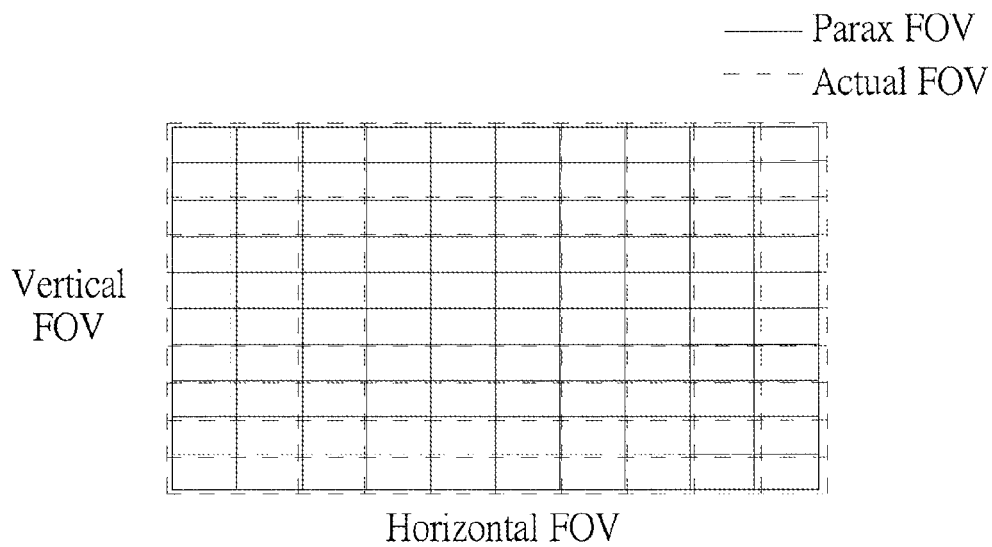
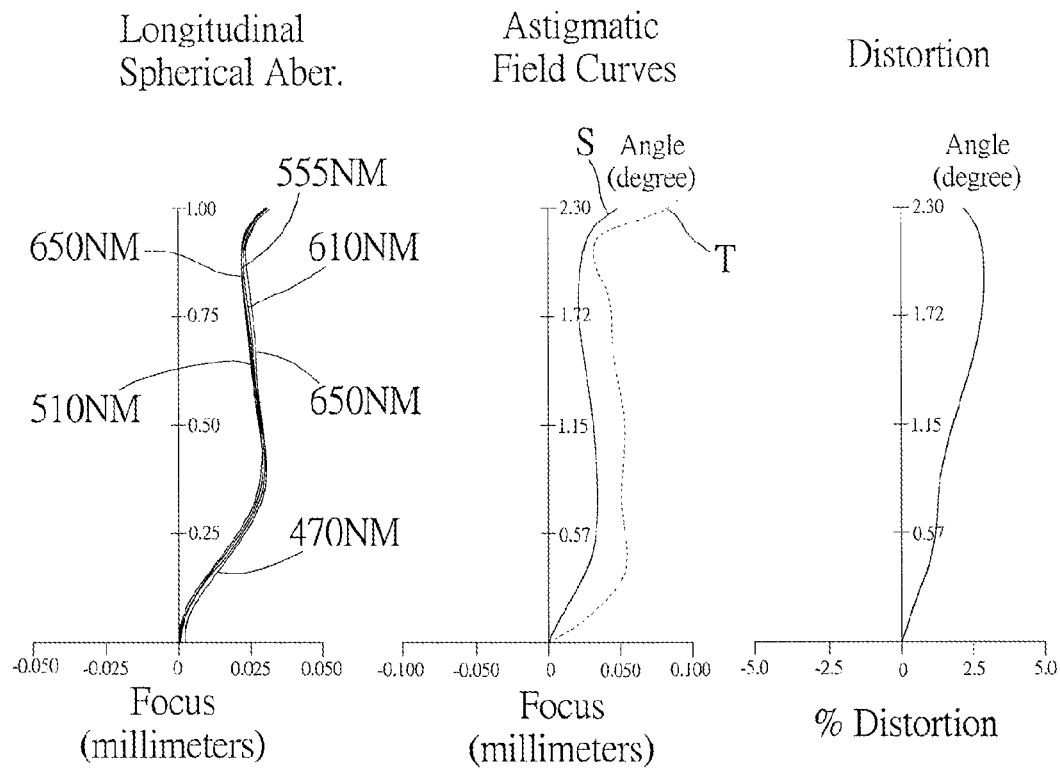
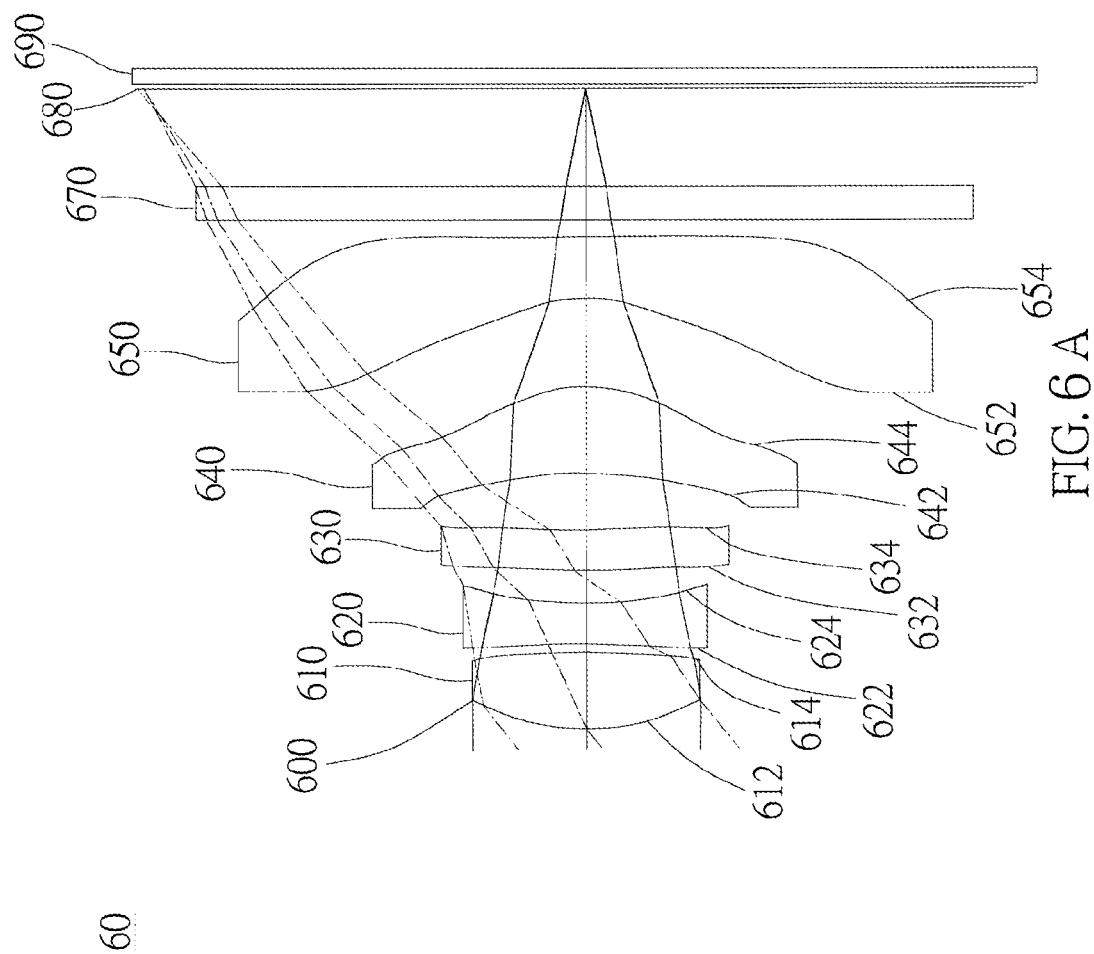


FIG. 5 A





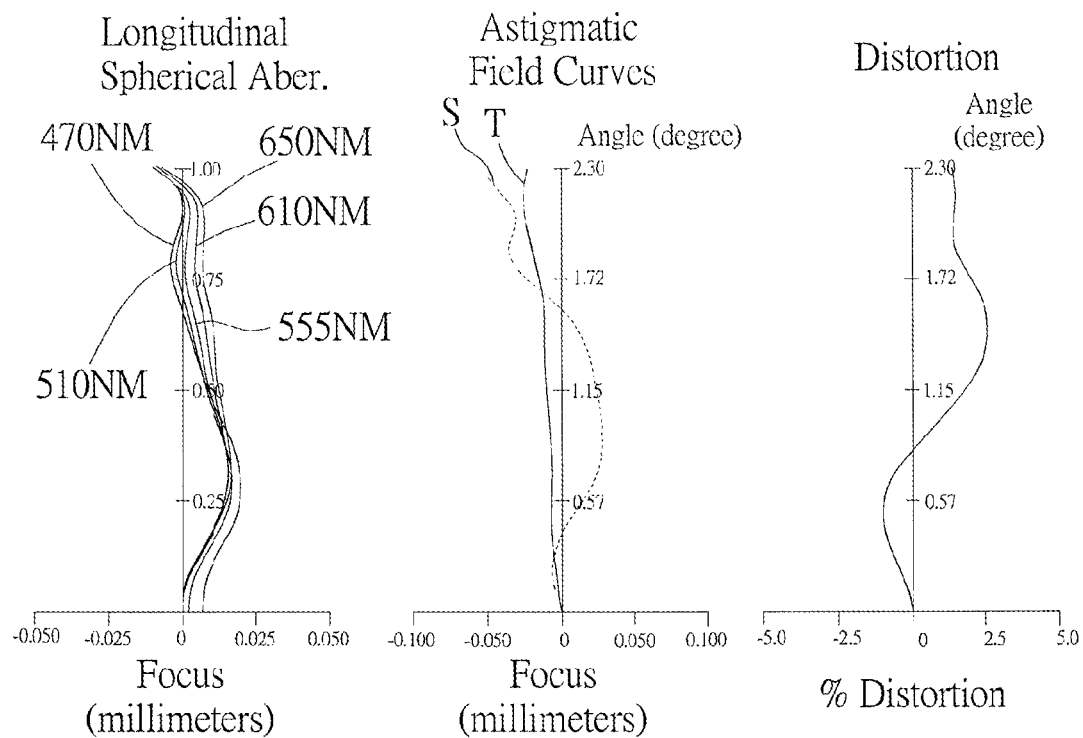


FIG. 6 B

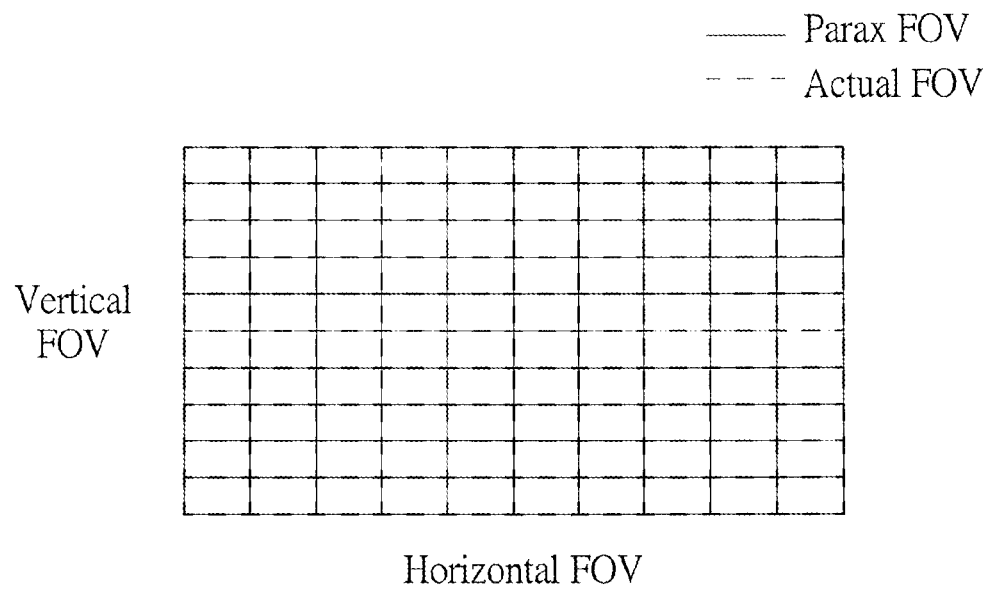


FIG. 6 C

## OPTICAL IMAGE CAPTURING SYSTEM

## BACKGROUND OF THE INVENTION

## 1. Technical Field

The present invention relates generally to an optical system, and more particularly to a compact optical image capturing system for an electronic device.

## 2. Description of Related Art

In recent years, with the rise of portable electronic devices having camera functionalities, the demand for an optical image capturing system is raised gradually. The image sensing device of ordinary photographing camera is commonly selected from charge coupled device (CCD) or complementary metal-oxide semiconductor sensor (CMOS Sensor). In addition, as advanced semiconductor manufacturing technology enables the minimization of pixel size of the image sensing device, the development of the optical image capturing system towards the field of high pixels. Therefore, the requirement for high imaging quality is rapidly raised.

The conventional optical system of the portable electronic device usually has a three or four-piece lens. However, the optical system is asked to take pictures in a dark environment, in other words, the optical system is asked to have a large aperture. An optical system with large aperture usually has several problems, such as large aberration, poor image quality at periphery of the image, and hard to manufacture. In addition, an optical system of wide-angle usually has large distortion. Therefore, the conventional optical system provides high optical performance as required.

It is an important issue to increase the quantity of light entering the lens and the angle of field of the lens. In addition, the modern lens is also asked to have several characters, including high pixels, high image quality, small in size, and high optical performance.

## BRIEF SUMMARY OF THE INVENTION

The aspect of embodiment of the present disclosure directs to an optical image capturing system and an optical image capturing lens which use combination of refractive powers, convex and concave surfaces of five-piece optical lenses (the convex or concave surface in the disclosure denotes the geometrical shape of an image-side surface or an object-side surface of each lens on an optical axis) to increase the quantity of incoming light of the optical image capturing system, and to improve imaging quality for image formation, so as to be applied to minimized electronic products.

The term and its definition to the lens parameter in the embodiment of the present are shown as below for further reference.

The lens parameter related to a length or a height in the lens element:

A height for image formation of the optical image capturing system is denoted by HOI. A height of the optical image capturing system is denoted by HOS. A distance from the object-side surface of the first lens element to the image-side surface of the fifth lens element is denoted by InTL. A distance from the image-side surface of the fifth lens to the image plane is denoted by InB.  $InTL + InB = HOS$ . A distance from the first lens element to the second lens element is denoted by IN12 (instance). A central thickness of the first lens element of the optical image capturing system on the optical axis is denoted by TPI (instance).

The lens parameter related to a material in the lens:

An Abbe number of the first lens element in the optical image capturing system is denoted by NA1 (instance). A refractive index of the first lens element is denoted by Nd1 (instance).

The lens parameter related to a view angle in the lens:

A view angle is denoted by AF. Half of the view angle is denoted by HAF. A major light angle is denoted by MRA.

The lens parameter related to exit/entrance pupil in the lens

An entrance pupil diameter of the optical image capturing system is denoted by HEP.

The lens parameter related to a depth of the lens shape

A distance in parallel with an optical axis from a maximum effective diameter position to an axial point on the object-side surface of the fifth lens is denoted by InRS51 (instance). A distance in parallel with an optical axis from a maximum effective diameter position to an axial point on the image-side surface of the fifth lens is denoted by InRS52 (instance).

The lens parameter related to the lens shape:

A critical point C is a tangent point on a surface of a specific lens, and the tangent point is tangent to a plane perpendicular to the optical axis and the tangent point cannot be a crossover point on the optical axis. To follow the past, a distance perpendicular to the optical axis between a critical point C41 on the object-side surface of the fourth lens and the optical axis is HVT41 (instance). A distance perpendicular to the optical axis between a critical point C51 on the object-side surface of the fifth lens and the optical axis is HVT51 (instance). A distance perpendicular to the optical axis between a critical point C52 on the image-side surface of the fifth lens and the optical axis is HVT52 (instance). The object-side surface of the fifth lens has one inflection point IF511 which is nearest to the optical axis, and the sinkage value of the inflection point IF511 is denoted by SGI511. A distance perpendicular to the optical axis between the inflection point IF511 and the optical axis is HIF511 (instance). The image-side surface of the fifth lens has one inflection point IF521 which is nearest to the optical axis, and the sinkage value of the inflection point IF521 is denoted by SGI521 (instance). A distance perpendicular to the optical axis between the inflection point IF521 and the optical axis is HIF521 (instance). The object-side surface of the fifth lens has one inflection point IF512 which is the second nearest to the optical axis, and the sinkage value of the inflection point IF512 is denoted by SGI512 (instance). A distance perpendicular to the optical axis between the inflection point IF512 and the optical axis is HIF512 (instance). The image-side surface of the fifth lens has one inflection point IF522 which is the second nearest to the optical axis, and the sinkage value of the inflection point IF522 is denoted by SGI522 (instance). A distance perpendicular to the optical axis between the inflection point IF522 and the optical axis is HIF522 (instance).

The lens element parameter related to an aberration:

Optical distortion for image formation in the optical image capturing system is denoted by ODT. TV distortion for image formation in the optical image capturing system is denoted by TDT. Further, the range of the aberration offset for the view of image formation may be limited to 50%-100% field. An offset of the spherical aberration is denoted by DFS. An offset of the coma aberration is denoted by DFC.

The present invention provides an optical image capturing system, in which the fifth lens is provided with an inflection point at the object-side surface or at the image-side surface to adjust the incident angle of each view field and modify the

ODT and the TDT. In addition, the surfaces of the fifth lens are capable of modifying the optical path to improve the imaging quality.

The optical image capturing system of the present invention includes a first lens, a second lens, a third lens, a fourth lens, and a fifth lens in order along an optical axis from an object side to an image side. The first lens has positive refractive power, and the fifth lens has refractive power. Both the object-side surface and the image-side surface of the fifth lens are aspheric surfaces. The optical image capturing system satisfies:

$$1.2 \leq f/HEP \leq 2.8 \text{ and } 0.5 \leq HOS/f \leq 2.5;$$

where  $f$  is a focal length of the optical image capturing system; HEP is an entrance pupil diameter of the optical image capturing system; and HOS is a distance in parallel with the optical axis between an object-side surface, which face the object side, of the first lens and the image plane.

The present invention further provides an optical image capturing system, including a first lens, a second lens, a third lens, a fourth lens, and a fifth lens in order along an optical axis from an object side to an image side. The first lens has positive refractive power, and both the object-side surface and the image side surface thereof are aspheric surfaces. The second lens has negative refractive power, and the third and the fourth lenses have refractive power. The fifth lens has negative refractive power, and both an object-side surface and an image side surface thereof are aspheric surfaces. The optical image capturing system satisfies:

$$1.2 \leq f/HEP \leq 2.8; 0.5 \leq HOS/f \leq 2.5; 0.4 \leq |\tan(HAF)| \leq 1.5; |TDT| < 1.5\%; \text{ and } |ODT| \leq 2.5\%;$$

where  $f$  is a focal length of the optical image capturing system; HEP is an entrance pupil diameter of the optical image capturing system; HOS is a distance in parallel with the optical axis between an object-side surface, which face the object side, of the first lens and the image plane; HAF is a half of the view angle of the optical image capturing system; TDT is a TV distortion; and ODT is an optical distortion.

The present invention further provides an optical image capturing system, including a first lens, a second lens, a third lens, a fourth lens, and a fifth lens in order along an optical axis from an object side to an image side. At least two of these five lenses each has at least an inflection point on a side thereof. The first lens has positive refractive power, and both an object-side surface and an image side surface thereof are aspheric surfaces. The second and the third lens have refractive power, and the fourth lens has positive refractive power. The fifth lens has negative refractive power, and both an object-side surface and an image side surface thereof are aspheric surfaces. The optical image capturing system satisfies:

$$1.2 \leq f/HEP \leq 2.8; 0.4 \leq HOS/f \leq 1.5; 0.5 \leq |\tan(HAF)| \leq 2.5; |TDT| < 1.5\%; \text{ and } |ODT| \leq 2.5\%;$$

where  $f$  is a focal length of the optical image capturing system; HEP is an entrance pupil diameter of the optical image capturing system; HOS is a distance in parallel with the optical axis between an object-side surface, which face the object side, of the first lens and the image plane; HAF is a half of the view angle of the optical image capturing system; TDT is a TV distortion; and ODT is an optical distortion.

In an embodiment, the optical image capturing system further includes an image sensor with a size less than 1/1.2" in diagonal, and a pixel less than 1.4  $\mu\text{m}$ . A preferable pixel size of the image sensor is less than 1.2  $\mu\text{m}$ , and more

preferable pixel size is less than 0.9  $\mu\text{m}$ . A 16:9 image sensor is available for the optical image capturing system of the present invention.

In an embodiment, the optical image capturing system of the present invention is available to high-quality (4K and 2K, so called UHD and QHD) recording, and provides high quality of image.

In an embodiment, a height of the optical image capturing system (HOS) can be reduced while  $|f1| > f5$ .

In an embodiment, when the lenses satisfy  $|f2| + |f3| + |f4| > |f1| + |f5|$ , at least one of the lenses from the second lens to the fourth lens could have weak positive refractive power or weak negative refractive power. The weak refractive power indicates that an absolute value of the focal length is greater than 10. When at least one of the lenses from the second lens to the fourth lens could have weak positive refractive power, it may share the positive refractive power of the first lens, and on the contrary, when at least one of the lenses from the second lens to the fourth lens could have weak negative refractive power, it may finely modify the aberration of the system.

In an embodiment, the fifth lens has negative refractive power, and an image-side surface thereof is concave, it may reduce back focal length and size. Besides, the fifth lens has at least an inflection point on a surface thereof, which may reduce an incident angle of the light of an off-axis field of view and modify the aberration of the off-axis field of view. It is preferable that both surfaces of the fifth lens have at least an inflection point on a surface thereof.

#### BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

The present invention will be best understood by referring to the following detailed description of some illustrative embodiments in conjunction with the accompanying drawings, in which

FIG. 1A is a schematic diagram of a first preferred embodiment of the present invention;

FIG. 1B shows curve diagrams of longitudinal spherical aberration, astigmatic field, and optical distortion of the optical image capturing system in the order from left to right of the first embodiment of the present application;

FIG. 1C shows a curve diagram of TV distortion of the optical image capturing system of the first embodiment of the present application;

FIG. 2A is a schematic diagram of a second preferred embodiment of the present invention;

FIG. 2B shows curve diagrams of longitudinal spherical aberration, astigmatic field, and optical distortion of the optical image capturing system in the order from left to right of the second embodiment of the present application;

FIG. 2C shows a curve diagram of TV distortion of the optical image capturing system of the second embodiment of the present application;

FIG. 3A is a schematic diagram of a third preferred embodiment of the present invention;

FIG. 3B shows curve diagrams of longitudinal spherical aberration, astigmatic field, and optical distortion of the optical image capturing system in the order from left to right of the third embodiment of the present application;

FIG. 3C shows a curve diagram of TV distortion of the optical image capturing system of the third embodiment of the present application;

FIG. 4A is a schematic diagram of a fourth preferred embodiment of the present invention;

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FIG. 4B shows curve diagrams of longitudinal spherical aberration, astigmatic field, and optical distortion of the optical image capturing system in the order from left to right of the fourth embodiment of the present application;

FIG. 4C shows a curve diagram of TV distortion of the optical image capturing system of the fourth embodiment of the present application;

FIG. 5A is a schematic diagram of a fifth preferred embodiment of the present invention;

FIG. 5B shows curve diagrams of longitudinal spherical aberration, astigmatic field, and optical distortion of the optical image capturing system in the order from left to right of the fifth embodiment of the present application;

FIG. 5C shows a curve diagram of TV distortion of the optical image capturing system of the fifth embodiment of the present application;

FIG. 6A is a schematic diagram of a sixth preferred embodiment of the present invention;

FIG. 6B shows curve diagrams of longitudinal spherical aberration, astigmatic field, and optical distortion of the optical image capturing system in the order from left to right of the sixth embodiment of the present application; and

FIG. 6C shows a curve diagram of TV distortion of the optical image capturing system of the sixth embodiment of the present application.

#### DETAILED DESCRIPTION OF THE INVENTION

An optical image capturing system of the present invention includes a first lens, a second lens, a third lens, a forth lens, and a fifth lens from an object side to an image side. The optical image capturing system further is provided with an image sensor at an image plane.

The optical image capturing system works in five wavelengths, including 470 nm, 510 nm, 555 nm, 610 nm, 650 nm, and 555 nm.

The optical image capturing system of the present invention satisfies  $0.5 \leq \Sigma PPR / \Sigma NPR \leq 2.5$ , and a preferable range is  $1 \leq \Sigma PPR / \Sigma NPR \leq 2.0$ , where PPR is a ratio of the focal length  $f$  of the optical image capturing system to a focal length  $f_p$  of each of lenses with positive refractive power; NPR is a ratio of the focal length  $f$  of the optical image capturing system to a focal length  $f_p$  of each of lenses with negative refractive power; and  $\Sigma NPR$  is a sum of the PNRs of each negative lens. It is helpful to control of an entire refractive power and an entire length of the optical image capturing system.

HOS is a height of the optical image capturing system, and when the ratio of  $HOS/f$  approaches to 1, it is helpful to decrease of size and increase of imaging quality.

In an embodiment, the optical image capturing system of the present invention satisfies  $0 < \Sigma PP \leq 200$  and  $f1/\Sigma PP \leq 0.85$ , and a preferable range is  $0 < \Sigma PP \leq 150$  and  $0.01 \leq f1/\Sigma PP \leq 0.6$ , where  $\Sigma PP$  is a sum of a focal length  $f_p$  of each lens with positive refractive power, and  $\Sigma NP$  is a sum of a focal length  $f_p$  of each lens with negative refractive power. It is helpful to control of focusing capacity of the system and redistribution of the positive refractive powers of the system to avoid the significant aberration in early time. The optical image capturing system further satisfies  $\Sigma NP < 0$  and  $0.01 \leq f5/\Sigma NP \leq 0.5$ , which is helpful to control of an entire refractive power and an entire length of the optical image capturing system.

The first lens has positive refractive power, and an object-side surface, which faces the object side, thereof is convex.

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It may modify the positive refractive power of the first lens as well as shorten the entire length of the system.

The second lens has negative refractive power, which may correct the aberration of the first lens.

The third lens has negative refractive power, which may correct the aberration of the first lens.

The fourth lens has positive refractive power, and an image-side surface thereof, which faces the image side, is concave. The fourth lens may share the positive refractive power of the first lens to reduce an increase of the aberration and reduce a sensitivity of the system.

The fifth lens has negative refractive power, and an image-side surface thereof, which faces the image side, is concave. It may shorten a rear focal length to reduce the size of the system. In addition, the fifth lens is provided with at least an inflection point on at least a surface to reduce an incident angle of the light of an off-axis field of view and modify the aberration of the off-axis field of view. It is preferable that each surface, the object-side surface and the image-side surface, of the fifth lens has at least an inflection point.

The image sensor is provided on the image plane. The optical image capturing system of the present invention satisfies  $HOS/HOI \leq 3$  and  $0.5 \leq HOS/f \leq 2.5$ , and a preferable range is  $1 \leq HOS/HOI \leq 2.5$  and  $1 \leq HOS/f \leq 2$ , where HOI is height for image formation of the optical image capturing system, i.e., the maximum image height, and HOS is a height of the optical image capturing system, i.e. a distance on the optical axis between the object-side surface of the first lens and the image plane. It is helpful to reduction of size of the system for used in compact cameras.

The optical image capturing system of the present invention further is provided with an aperture to increase image quality.

In the optical image capturing system of the present invention, the aperture could be a front aperture or a middle aperture, wherein the front aperture is provided between the object and the first lens, and the middle is provided between the first lens and the image plane. The front aperture provides a long distance between an exit pupil of the system and the image plane, which allows more elements to be installed. The middle could enlarge a view angle of view of the system and increase the efficiency of the image sensor. The optical image capturing system satisfies  $0.6 \leq \ln S / HOS \leq 1.1$ , and a preferable range is  $0.8 \leq \ln S / HOS \leq 1$ , where  $\ln S$  is a distance between the aperture and the image plane. It is helpful to size reduction and wide angle.

The optical image capturing system of the present invention satisfies  $0.45 \leq \Sigma TPI / \ln TL \leq 0.95$ , where  $\ln TL$  is a distance between the object-side surface of the first lens and the image-side surface of the fifth lens, and  $\Sigma TPI$  is a sum of central thicknesses of the lenses on the optical axis. It is helpful to the contrast of image and yield rate of manufacture, and provides a suitable back focal length for installation of other elements.

The optical image capturing system of the present invention satisfies  $0.1 \leq |R1/R2| \leq 0.5$ , and a preferable range is  $0.1 \leq |R1/R2| \leq 0.45$ , where  $R1$  is a radius of curvature of the object-side surface of the first lens, and  $R2$  is a radius of curvature of the image-side surface of the first lens. It provides the first lens with a suitable refractive power to reduce the increase rate of the spherical aberration.

The optical image capturing system of the present invention satisfies  $-10 < (R9 - R10) / (R9 + R10) < 30$ , where  $R9$  is a radius of curvature of the object-side surface of the fifth lens, and  $R10$  is a radius of curvature of the image-side surface of the fifth lens. It may modify the astigmatic field curvature.



The optical image capturing system of the present invention satisfies  $0 < \text{IN12}/f \leq 0.25$ , and a preferable range is  $0.01 \leq \text{IN12}/f \leq 0.20$ , where IN12 is a distance on the optical axis between the first lens and the second lens. It may correct chromatic aberration and improve the performance.

The optical image capturing system of the present invention satisfies  $1 \leq (\text{TP1} + \text{IN12})/\text{TP} \leq 210$ , where TP1 is a central thickness of the first lens on the optical axis, and TP2 is a central thickness of the second lens on the optical axis. It may control the sensitivity of manufacture of the system and improve the performance.

The optical image capturing system of the present invention satisfies  $0.2 \leq (\text{TP5} + \text{IN45})/\text{TP4} \leq 3$ , where TP4 is a central thickness of the fourth lens on the optical axis, TP5 is a central thickness of the fifth lens on the optical axis, and N45 is a distance between the fourth lens and the fifth lens. It may control the sensitivity of manufacture of the system and improve the performance.

The optical image capturing system of the present invention satisfies  $0.1 \leq (\text{TP2} + \text{TP3} + \text{TP4})/\Sigma\text{TP} \leq 0.8$ , and a preferable range is  $0.4 \leq (\text{TP2} + \text{TP3} + \text{TP4})/\Sigma\text{TP} \leq 0.8$ , where TP2 is a central thickness of the second lens on the optical axis, TP3 is a central thickness of the third lens on the optical axis, TP4 is a central thickness of the fourth lens on the optical axis, TP5 is a central thickness of the fifth lens on the optical axis, an  $\Sigma\text{TP}$  is a sum of the central thicknesses of all the lenses on the optical axis. It may finely modify the aberration of the incident rays and reduce the height of the system.

The optical image capturing system of the present invention satisfies  $-1 \text{ mm} \leq \text{InRS51} \leq 1 \text{ mm}$ ;  $-1 \text{ mm} \leq \text{InRS52} \leq 1 \text{ mm}$ ;  $1 \text{ mm} \leq \text{InRS51} + \text{InRS52} \leq 2 \text{ mm}$ ;  $0.01 \leq |\text{InRS51}|/\text{TP5} \leq 5$ ; and  $0.01 \leq |\text{InRS52}|/\text{TP5} \leq 5$ , where InRS51 is a displacement in parallel with the optical axis from a point on the object-side surface 152 of the fifth lens, through which the optical axis passes, to a point at the maximum effective radius of the object-side surface 152 of the fifth lens, wherein InRS51 is positive while the displacement is toward the image side, and InRS51 is negative while the displacement is toward the object side; InRS52 is a displacement in parallel with the optical axis from a point on the image-side surface 154 of the fifth lens, through which the optical axis passes, to a point at the maximum effective radius of the image-side surface 154 of the fifth lens; and TP5 is a central thickness of the fifth lens 150 on the optical axis. It may control the positions of the maximum effective radius on both surfaces of the fifth lens, correct the aberration of the spherical field of view, and reduce the size.

The optical image capturing system of the present invention satisfies  $0 < \text{SGI511}/(\text{SGI511} + \text{TP5}) \leq 0.9$  and  $0 < \text{SGI521}/(\text{SGI521} + \text{TP5}) \leq 0.9$ , and a preferable range is  $0.01 < \text{SGI511}/(\text{SGI511} + \text{TP5}) \leq 0.7$  and  $0.01 < \text{SGI521}/(\text{SGI521} + \text{TP5}) \leq 0.7$ , where SGI511 is a displacement in parallel with the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to an inflection point, which is the closest to the optical axis, on the object-side surface of the fifth lens; SGI521 is a displacement in parallel with the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to an inflection point, which is the closest to the optical axis, on the image-side surface of the fifth lens, and TP5 is a thickness of the fifth lens on the optical axis.

The optical image capturing system of the present invention satisfies  $0 < \text{SGI512}/(\text{SGI512} + \text{TP5}) \leq 0.9$  and  $0 < \text{SGI522}/(\text{SGI522} + \text{TP5}) \leq 0.9$ , and a preferable range is  $0.1 \leq \text{SGI512}/(\text{SGI512} + \text{TP5}) \leq 0.8$  and  $0.1 \leq \text{SGI522}/(\text{SGI522} + \text{TP5}) \leq 0.8$ , where SGI512 is a displacement in parallel with the optical axis from a point on the object-side surface of the fifth lens,

through which the optical axis passes, to an inflection point, which is the second closest to the optical axis, on the image-side surface of the fifth lens, and SGI522 is a displacement in parallel with the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to an inflection point, which is the second closest to the optical axis, on the image-side surface of the fifth lens.

The optical image capturing system of the present invention satisfies  $\text{HIF511}/\text{HOI} \leq 0.9$  and  $0.01 \leq \text{HIF521}/\text{HOI} \leq 0.9$ , and a preferable range is  $0.09 \leq \text{HIF511}/\text{HOI} \leq 0.5$  and  $0.09 \leq \text{HIF521}/\text{HOI} \leq 0.5$ , where HIF511 is a distance perpendicular to the optical axis between the inflection point, which is the closest to the optical axis, on the object-side surface of the fifth lens and the optical axis, and HIF521 is a distance perpendicular to the optical axis between the inflection point, which is the closest to the optical axis, on the image-side surface of the fifth lens and the optical axis.

The optical image capturing system of the present invention satisfies  $0.01 \leq \text{HIF512}/\text{HOI} \leq 0.9$  and  $0.01 \leq \text{HIF522}/\text{HOI} \leq 0.9$ , and a preferable range is  $0.09 \leq \text{HIF512}/\text{HOI} \leq 0.8$  and  $0.09 \leq \text{HIF522}/\text{HOI} \leq 0.8$ , where HIF512 is a distance perpendicular to the optical axis between the inflection point, which is the second the closest to the optical axis, on the object-side surface of the fifth lens and the optical axis, and HIF522 is a distance perpendicular to the optical axis between the inflection point, which is the second the closest to the optical axis, on the image-side surface of the fifth lens and the optical axis.

In an embodiment, the lenses of high Abbe number and the lenses of low Abbe number are arranged in an interlaced arrangement that could be helpful to correction of aberration of the system.

An equation of aspheric surface is

$$z = ch^2/[1 + \{1 + (k+1)c^2h^2\}^{0.5}] + A4h^4 + A6h^6 + A8h^8 + A10h^{10} + A12h^{12} + A14h^{14} + A16h^{16} + A18h^{18} + A20h^{20} \quad (1)$$

where  $z$  is a depression of the aspheric surface;  $k$  is conic constant;  $c$  is reciprocal of radius of curvature; and  $A4$ ,  $A6$ ,  $A8$ ,  $A10$ ,  $A12$ ,  $A14$ ,  $A16$ ,  $A18$ , and  $A20$  are high-order aspheric coefficients.

In the optical image capturing system, the lenses could be made of plastic or glass. The plastic lenses may reduce the weight and lower the cost of the system, and the glass lenses may control the thermal effect and enlarge the space for arrangement of refractive power of the system. In addition, the opposite surfaces (object-side surface and image-side surface) of the first to the fifth lenses could be aspheric that can obtain more control parameters to reduce aberration. The number of aspheric glass lenses could be less than the conventional spherical glass lenses that is helpful to reduction of the height of the system.

When the lens has a convex surface, which means that the surface is convex around a position, through which the optical axis passes, and when the lens has a concave surface, which means that the surface is concave around a position, through which the optical axis passes.

The optical image capturing system of the present invention further is provided with a diaphragm to increase image quality.

In the optical image capturing system, the diaphragm could be a front diaphragm or a middle diaphragm, wherein the front diaphragm is provided between the object and the first lens, and the middle is provided between the first lens and the image plane. The front diaphragm provides a long distance between an exit pupil of the system and the image

plane, which allows more elements to be installed. The middle diaphragm could enlarge a view angle of view of the system and increase the efficiency of the image sensor. The middle diaphragm is helpful to size reduction and wide angle.

The optical image capturing system of the present invention could be applied in dynamic focusing optical system. It is superior in correction of aberration and high imaging quality so that it could be allied in lots of fields.

We provide several embodiments in conjunction with the accompanying drawings for the best understanding, which are:

#### First Embodiment

As shown in FIG. 1A and FIG. 1B, an optical image capturing system **100** of the first preferred embodiment of the present invention includes, along an optical axis from an object side to an image side, an aperture **100**, a first lens **110**, a second lens **120**, a third lens **130**, a fourth lens **140**, a fifth lens **150**, an infrared rays filter **170**, an image plane **180**, and an image sensor **190**.

The first lens **110** has positive refractive power, and is made of plastic. An object-side surface **112** thereof, which faces the object side, is a convex aspheric surface, and an image-side surface **114** thereof, which faces the image side, is a concave aspheric surface, and the image-side surface has an inflection point. The first lens **110** satisfies  $SGI121=0.0387148$  mm and  $|SGI121|/(|SGI121|+TP1)=0.061775374$ , where  $SGI121$  is a displacement in parallel with the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The first lens **110** further satisfies  $HIF121=0.61351$  mm and  $HIF121/HOI=0.209139253$ , where  $HIF121$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens **120** has negative refractive power, and is made of plastic. An object-side surface **122** thereof, which faces the object side, is a concave aspheric surface, and an image-side surface **124** thereof, which faces the image side, is a convex aspheric surface, and the image-side surface **124** has an inflection point. The second lens **120** satisfies  $SGI221=-0.0657553$  mm and  $|SGI221|/(|SGI221|+TP2)=0.176581512$ , where  $SGI221$  is a displacement in parallel with the optical axis from a point on the image-side surface of the second lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The second lens further satisfies  $HIF221=0.84667$  mm and  $HIF221/HOI=0.288621101$ , where  $HIF221$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The third lens **130** has negative refractive power, and is made of plastic. An object-side surface **132**, which faces the object side, is a concave aspheric surface, and an image-side surface **134**, which faces the image side, is a convex aspheric surface, and each of them has two inflection points. The third lens **130** satisfies  $SGI311=-0.341027$  mm;  $SGI321=-0.231534$  mm and  $|SGI311|/(|SGI311|+TP3)=0.525237108$  and  $|SGI321|/(|SGI321|+TP3)=0.428934269$ , where  $SGI311$  is a displacement in parallel with the optical axis,

from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI321$  is a displacement in parallel with the optical axis, from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The third lens **130** satisfies  $SGI312=-0.376807$  mm;  $SGI322=-0.382162$  mm;  $|SGI312|/(|SGI312|+TP5)=0.550033428$ ;  $|SGI322|/(|SGI322|+TP3)=0.55352345$ , where  $SGI312$  is a displacement in parallel with the optical axis, from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis, and  $SGI322$  is a displacement in parallel with the optical axis, from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis.

The third lens **130** further satisfies  $HIF311=0.987648$  mm;  $HIF321=0.805604$  mm;  $HIF311/HOI=0.336679052$ ; and  $HIF321/HOI=0.274622124$ , where  $HIF311$  is a distance perpendicular to the optical axis between the inflection point on the object-side surface of the third lens, which is the closest to the optical axis, and the optical axis, and  $HIF321$  is a distance perpendicular to the optical axis between the inflection point on the image-side surface of the third lens, which is the closest to the optical axis, and the optical axis.

The third lens **130** further satisfies  $HIF312=1.0493$  mm;  $HIF322=1.17741$  mm;  $HIF312/HOI=0.357695585$ ; and  $HIF322/HOI=0.401366968$ , where  $HIF312$  is a distance perpendicular to the optical axis between the inflection point on the object-side surface of the third lens, which is the second the closest to the optical axis, and the optical axis, and  $HIF322$  is a distance perpendicular to the optical axis, between the inflection point on the image-side surface of the third lens, which is the second the closest to the optical axis, and the optical axis.

The fourth lens **140** has positive refractive power, and is made of plastic. Both an object-side surface **142**, which faces the object side, and an image-side surface **144**, which faces the image side, thereof are convex aspheric surfaces, and the object-side surface **142** has an inflection point. The fourth lens **140** satisfies  $SGI411=0.0687683$  mm and  $|SGI411|/(|SGI411|+TP4)=0.118221297$ , where  $SGI411$  is a displacement in parallel with the optical axis from a point on the object-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The fourth lens **140** further satisfies  $HIF411=0.645213$  mm and  $HIF411/HOI=0.21994648$ , where  $HIF411$  is a distance perpendicular to the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fifth lens **150** has negative refractive power, and is made of plastic. Both an object-side surface **152**, which faces the object side, and an image-side surface **154**, which faces the image side, thereof are concave aspheric surfaces. The object-side surface **152** has three inflection points, and the image-side surface **154** has an inflection point. The fifth lens **150** satisfies  $SGI511=-0.236079$  mm;  $SGI521=0.023266$  mm;  $|SGI511|/(|SGI511|+TP5)=0.418297214$ ; and  $|SGI521|/(|SGI521|+TP5)=0.066177809$ , where  $SGI511$  is a displacement in parallel with the optical axis, from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the

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inflection point on the object-side surface, which is the closest to the optical axis, and SGI521 is a displacement in parallel with the optical axis, from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fifth lens 150 further satisfies  $SGI512 = -0.325042$  mm and  $|SGI512|/(|SGI512|+TP5) = 0.497505143$ , where SGI512 is a displacement in parallel with the optical axis, from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis.

The fifth lens 150 further satisfies  $SGI513 = -0.538131$  mm; and  $|SGI513|/(|SGI513|+TP5) = 0.621087839$ , where SGI513 is a displacement in parallel with the optical axis, from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the third closest to the optical axis.

The fifth lens 150 further satisfies  $HIF511 = 1.21551$  mm;  $HIF521 = 0.575738$  mm;  $HIF511/HOI = 0.414354866$ ; and  $HIF521/HOI = 0.196263167$ , where HIF511 is a distance perpendicular to the optical axis between the inflection point on the object-side surface of the fifth lens, which is the closest to the optical axis, and the optical axis, and HIF521 is a distance perpendicular to the optical axis between the inflection point on the image-side surface of the fifth lens, which is the closest to the optical axis, and the optical axis.

The fifth lens 150 further satisfies  $HIF512 = 1.49061$  mm and  $HIF512/HOI = 0.508133629$ , where HIF512 is a distance perpendicular to the optical axis between the inflection point on the object-side surface of the fifth lens, which is the second the closest to the optical axis, and the optical axis.

The fifth lens 150 further satisfies  $HIF513 = 2.00664$  mm and  $HIF513/HOI = 0.684042952$ , where HIF513 is a distance perpendicular to the optical axis between the inflection point on the object-side surface of the fifth lens, which is the third closest to the optical axis, and the optical axis.

The infrared rays filter 170 is made of glass, and between the fifth lens 150 and the image plane 180. The infrared rays filter 170 gives no contribution to the focal length of the system.

The optical image capturing system of the first preferred embodiment has the following parameters, which are  $f = 3.73172$  mm;  $f/HEP = 2.05$ ; and  $HAF = 37.5$  degrees and  $\tan(HAF) = 0.7673$ , where  $f$  is a focal length of the system; HAF is a half of the maximum field angle; and HEP is an entrance pupil diameter.

The parameters of the lenses of the first preferred embodiment are  $f1 = 3.7751$  mm;  $|f1/f1| = 0.9885$ ;  $f5 = -3.6601$  mm;  $|f1| > |f5|$ ; and  $|f1/f5| = 1.0314$ , where  $f1$  is a focal length of the first lens 110; and  $f5$  is a focal length of the fifth lens 150.

The first preferred embodiment further satisfies  $|f2|+|f3|+|f4| = 77.3594$  mm;  $|f1|+|f5| = 7.4352$  mm; and  $|f2|+|f3|+|f4| > |f1|+|f5|$ , where  $f2$  is a focal length of the second lens 120;  $f3$  is a focal length of the third lens 130; and  $f4$  is a focal length of the fourth lens 140.

The optical image capturing system of the first preferred embodiment further satisfies  $\Sigma PPR = f/f1 + f/f4 = 1.9785$ ;  $\Sigma NPR = f/f2 + f/f3 + f/f5 = -1.2901$ ;  $\Sigma PPR/\Sigma NPR = 1.5336$ ;  $|f/f1| = 0.9885$ ;  $|f/f2| = 0.0676$ ;  $|f/f3| = 0.2029$ ;  $|f/f4| = 0.9900$ ; and  $|f/f5| = 1.0196$ , where PPR is a ratio of a focal length  $f$  of the optical image capturing system to a focal length  $f_p$  of each of the lenses with positive refractive power; and NPR

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is a ratio of a focal length  $f$  of the optical image capturing system to a focal length  $f_p$  of each of lenses with negative refractive power.

The optical image capturing system of the first preferred embodiment further satisfies  $\ln TL + \ln B = HOS$ ;  $HOS = 4.5$  mm;  $HOI = 2.9335$  mm;  $HOS/HOI = 1.5340$ ;  $HOS/f = 1.2059$ ;  $\ln S = 4.19216$  mm; and  $\ln S/HOS = 0.9316$ , where  $\ln TL$  is a distance between the object-side surface 112 of the first lens 110 and the image-side surface 154 of the fifth lens 150;  $HOS$  is a height of the image capturing system, i.e. a distance between the object-side surface 112 of the first lens 110 and the image plane 180;  $\ln S$  is a distance between the aperture 100 and the image plane 180;  $HOI$  is height for image formation of the optical image capturing system, i.e., the maximum image height; and  $\ln B$  is a distance between the image-side surface 154 of the fifth lens 150 and the image plane 180.

The optical image capturing system of the first preferred embodiment further satisfies  $\Sigma TP = 2.044092$  mm and  $\Sigma TP/\ln TL = 0.5979$ , where  $\Sigma TP$  is a sum of the thicknesses of the lenses 110-150 with refractive power. It is helpful to the contrast of image and yield rate of manufacture, and provides a suitable back focal length for installation of other elements.

The optical image capturing system of the first preferred embodiment further satisfies  $|R1/R2| = 0.3261$ , where  $R1$  is a radius of curvature of the object-side surface 112 of the first lens 110, and  $R2$  is a radius of curvature of the image-side surface 114 of the first lens 110. It provides the first lens with a suitable refractive power to reduce the increase rate of the spherical aberration.

The optical image capturing system of the first preferred embodiment further satisfies  $(R9-R10)/(R9+R10) = -2.9828$ , where  $R9$  is a radius of curvature of the object-side surface 152 of the fifth lens 150, and  $R10$  is a radius of curvature of the image-side surface 154 of the fifth lens 150. It may modify the astigmatic field curvature.

The optical image capturing system of the first preferred embodiment further satisfies  $\Sigma PP = f1+f4 = 7.5444$  mm and  $f1/(f1+f4) = 0.5004$ , where  $\Sigma PP$  is a sum of the focal lengths  $f_p$  of each lens with positive refractive power. It is helpful to sharing the positive refractive powers of the first lens 110 to the other positive lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the first preferred embodiment further satisfies  $\Sigma NP = f2+f3+f5 = -77.2502$  mm and  $f5/(f2+f3+f5) = 0.0474$ , where  $f2$ ,  $f3$ , and  $f5$  are focal lengths of the second, the third, and the fifth lenses, and  $\Sigma NP$  is a sum of the focal lengths  $f_p$  of each lens with negative refractive power. It is helpful to sharing the negative refractive powers of the fifth lens 150 to the other negative lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the first preferred embodiment further satisfies  $\ln I2 = 0.511659$  mm and  $\ln I2/f = 0.1371$ , where  $\ln I2$  is a distance on the optical axis between the first lens 110 and the second lens 120. It may correct chromatic aberration and improve the performance.

The optical image capturing system of the first preferred embodiment further satisfies  $TP1 = 0.587988$  mm;  $TP2 = 0.306624$  mm; and  $(TP1+\ln I2)/TP2 = 3.5863$ , where  $TP1$  is a central thickness of the first lens 110 on the optical axis, and  $TP2$  is a central thickness of the second lens 120 on the optical axis. It may control the sensitivity of manufacture of the system and improve the performance.

The optical image capturing system of the first preferred embodiment further satisfies  $TP4 = 0.5129$  mm;  $TP5 = 0.3283$

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mm; and (TP5+IN45)/TP4=1.5095, where TP4 is a central thickness of the fourth lens 140 on the optical axis, TP5 is a central thickness of the fifth lens 150 on the optical axis, and N45 is a distance on the optical axis between the fourth lens and the fifth lens. It may control the sensitivity of manufacture of the system and improve the performance.

The optical image capturing system of the first preferred embodiment further satisfies TP3=0.3083 mm and (TP2+TP3+TP4)/ΣTP=0.5517, where TP2, TP3, and TP4 are thicknesses on the optical axis of the second, the third, and the fourth lenses, an ΣTP is a sum of the central thicknesses of all the lenses with refractive power on the optical axis. It may finely modify the aberration of the incident rays and reduce the height of the system.

The optical image capturing system of the first preferred embodiment further satisfies InRS51=-0.576871 mm; InRS52=-0.555284 mm; |InRS51|+|InRS52|=1.132155 mm; |InRS51|/TP5=1.757135199; and |InRS52|/TP5=1.6914, where InRS51 is a displacement in parallel with the optical axis from a point on the object-side surface 152 of the fifth lens, through which the optical axis passes,

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to a point at the maximum effective radius of the object-side surface 152 of the fifth lens; InRS52 is a displacement in parallel with the optical axis from a point on the image-side surface 154 of the fifth lens, through which the optical axis passes, to a point at the maximum effective radius of the image-side surface 154 of the fifth lens; and TP5 is a central thickness of the fifth lens 150 on the optical axis. It may control the positions of the maximum effective radius on both surfaces of the fifth lens, correct the aberration of the spherical field of view, and reduce the size.

The optical image capturing system of the first preferred embodiment further satisfies NA5/NA2=2.5441, where NA2 is an Abbe number of the second lens 120, and NA5 is an Abbe number of the fifth lens 150. It may correct the aberration of the system.

The optical image capturing system of the first preferred embodiment further satisfies |TDT|=0.6343% and |ODT|=2.5001%, where TDT is TV distortion; and ODT is optical distortion.

The parameters of the lenses of the first embodiment are listed in Table 1 and Table 2.

TABLE 1

f = 3.73172 mm; f/HEP = 2.05; HAF = 37.5 deg; tan(HAF) = 0.7673						
Surface		Radius of curvature (mm)	Thickness (mm)	Material	Refractive index	Abbe number
0	Object	plane	infinity			
1	Aperture	plane	-0.30784			
2	1 <sup>st</sup> lens	1.48285	0.587988	plastic	1.5441	56.1
3		4.54742	0.511659			
4	2 <sup>nd</sup> lens	-9.33807	0.306624	plastic	1.6425	22.465
5		-12.8028	0.366935			
6	3 <sup>rd</sup> lens	-1.02094	0.308255	plastic	1.6425	22.465
7		-1.2492	0.05			
8	4 <sup>th</sup> lens	2.18916	0.512923	plastic	1.5441	56.1
9		-31.3936	0.44596			
10	5 <sup>th</sup> lens	-2.86353	0.328302	plastic	1.514	57.1538
11		5.75188	0.3			
12	Filter	plane	0.2		1.517	64.2
13		plane	0.58424			
14	Image plane	plane	-0.00289			

Reference wavelength: 555 nm

TABLE 2

Coefficients of the aspheric surfaces					
Surface	2	3	4	5	6
k	-1.83479	-20.595808	16.674705	11.425456	-4.642191
A4	6.89867E-02	2.25678E-02	-1.11828E-01	-4.19899E-02	-7.09315E-02
A6	2.35740E-02	-6.17850E-02	-6.62880E-02	-1.88072E-02	9.65840E-02
A8	-4.26369E-02	5.82944E-02	-3.35190E-02	-6.98321E-02	-7.32044E-03
A10	5.63746E-03	-2.73938E-02	-7.28886E-02	-1.13079E-02	-8.96740E-02
A12	7.46740E-02	-2.45759E-01	4.05955E-02	6.79127E-02	-3.70146E-02
A14	-6.93116E-02	3.43401E-01	1.60451E-01	2.83769E-02	5.00641E-02
A16	-2.04867E-02	-1.28084E-01	1.24448E-01	-2.45035E-02	7.50413E-02
A18	1.99910E-02	-2.32031E-02	-1.94856E-01	2.90241E-02	-5.10392E-02
A20					
Surface	7	8	9	10	11
k	-1.197201	-20.458388	-50	-2.907359	-50
A4	3.64395E-02	-1.75641E-02	-7.82211E-04	-1.58711E-03	-2.46339E-02
A6	2.22356E-02	-2.87240E-03	-2.47110E-04	-3.46504E-03	6.61804E-04
A8	7.09828E-03	-2.56360E-04	-3.78130E-04	4.52459E-03	1.54143E-04
A10	5.05740E-03	7.39189E-05	-1.22232E-04	1.05841E-04	-2.83264E-05
A12	-4.51124E-04	-5.53116E-08	-1.50294E-05	-5.57252E-04	-5.78839E-06
A14	-1.84003E-03	8.16043E-06	-5.41743E-07	4.41714E-05	-2.91861E-07
A16	-1.28118E-03	2.10395E-06	2.98820E-07	1.80752E-05	8.25778E-08

TABLE 2-continued

Coefficients of the aspheric surfaces				
A18	4.09004E-04	-1.21664E-06	2.73321E-07	-2.27031E-06
A20				-9.87595E-09

The detail parameters of the first preferred embodiment are listed in Table 1, in which the unit of radius of curvature, thickness, and focal length are millimeter, and surface 0-14 indicates the surfaces of all elements in the system in sequence from the object side to the image side. Table 2 is the list of coefficients of the aspheric surfaces, in which A1-A20 indicate the coefficients of aspheric surfaces from the first order to the twentieth order of each aspheric surface. The following embodiments have the similar diagrams and tables, which are the same as those of the first embodiment, so we do not describe it again.

#### Second Embodiment

As shown in FIG. 2A and FIG. 2B, an optical image capturing system of the second preferred embodiment of the present invention includes, along an optical axis from an object side to an image side, an aperture **200**, a first lens **210**, a second lens **220**, a third lens **230**, a fourth lens **240**, a fifth lens **250**, an infrared rays filter **270**, an image plane **280**, and an image sensor **290**.

The first lens **210** has positive refractive power, and is made of plastic. An object-side surface thereof, which faces the object side, is a convex aspheric surface, and an image-side surface thereof, which faces the image side, is a concave aspheric surface, and each of them has an inflection point respectively. The first lens **210** satisfies  $SGI111=0.289597$  mm;  $SGI121=0.0365023$  mm;  $|SGI111|/(|SGI111|+TP1)=0.373529438$ ; and  $|SGI121|/(|SGI121|+TP1)=0.06990042$ , where  $SGI111$  is a displacement in parallel to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI121$  is a displacement in parallel to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The first lens further satisfies  $HIF111=0.905831$  mm;  $HIF121=0.652682$  mm;  $HIF111/HOI=0.308788478$ ; and  $HIF121/HOI=0.222492586$ , where  $HIF111$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis, and  $HIF121$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens **220** has positive refractive power, and is made of plastic. An object-side surface thereof, which faces the object side, is a concave aspheric surface, and an image-side surface thereof, which faces the image side, is a convex aspheric surface.

The third lens **230** has negative refractive power, and is made of plastic. An object-side surface **232**, which faces the object side, is a concave aspheric surface, and an image-side surface **234**, which faces the image side, is a convex aspheric surface, and the image-side surface **234** has an inflection

point. The third lens **230** satisfies  $SGI321=-0.127948$  mm;  $|SGI321|/(|SGI321|+TP3)=0.357448568$ , where  $SGI321$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The third lens **230** further satisfies  $HIF321=0.764648$  mm;  $HIF321/HOI=0.260660644$ , where  $HIF321$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the closest to the optical axis, and the optical axis.

The fourth lens **240** has positive refractive power, and is made of plastic. Both an object-side surface **242**, which faces the object side, and an image-side surface **244**, which faces the image side, thereof are convex aspheric surfaces. The object-side surface **242** has an inflection point. The fourth lens **240** satisfies  $SGI411=0.0450907$  mm and  $|SGI411|/(|SGI411|+TP4)=0.069192674$ , where  $SGI411$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The fourth lens **240** further satisfies  $HIF411=0.614636$  mm;  $HIF411/HOI=0.209523095$ , where  $HIF411$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fifth lens **250** has negative refractive power, and is made of plastic. Both an object-side surface **252**, which faces the object side, and an image-side surface **254**, which faces the image side, thereof are concave aspheric surfaces. The image-side surface **254** has an inflection point. The fifth lens **250** satisfies  $SGI521=0.0335164$  mm and  $|SGI521|/(|SGI521|+TP5)=0.142482679$ , where  $SGI521$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fifth lens **250** further satisfies  $HIF521=0.548451$  mm and  $HIF521/HOI=0.186961309$ , where  $HIF521$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The infrared rays filter **270** is made of glass, and between the fifth lens **250** and the image plane **280**. The infrared rays filter **270** gives no contribution to the focal length of the system.

The optical image capturing system of the second preferred embodiment has the following parameters, which are  $|f2|+|f3|+|f4|=10.9023$  mm;  $|f1|+|f5|=6.1640$  mm; and  $|f2|+|f3|+|f4|>|f1|+|f5|$ , where  $f1$  is a focal length of the first lens **210**;  $f2$  is a focal length of the second lens **220**;  $f3$  is a focal length of the third lens **230**;  $f4$  is a focal length of the fourth lens **240**; and  $f5$  is a focal length of the fifth lens **250**.

The optical image capturing system of the second preferred embodiment further satisfies  $TP4=0.6066$  mm and  $TP5=0.2017$  mm, where  $TP4$  is a thickness of the fourth lens on the optical axis, and  $TP5$  is a thickness of the fifth lens on the optical axis.

In the second embodiment, the first, the second, and the fourth lenses **210**, **220**, and **240** are positive lenses, and their focal lengths are  $f_1$ ,  $f_2$ , and  $f_4$ . The optical image capturing system of the second preferred embodiment further satisfies  $\Sigma PP = f_1 + f_2 + f_4 = 11.2567$  mm and  $f_1/(f_1 + f_2 + f_4) = 0.3351$ , where  $\Sigma PP$  is a sum of the focal lengths of each positive lens. It is helpful to sharing the positive refractive powers of the first lens **210** to the other positive lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the second preferred embodiment further satisfies  $\Sigma NP = f_3 + f_5 = -5.8096$  mm and  $f_5/(f_3 + f_5) = 0.4117$ , where  $f_3$  and  $f_5$  are focal lengths of the third and the fifth lenses, and  $\Sigma NP$  is a sum of the focal lengths of each negative lens. It is helpful to sharing the negative refractive powers of the fifth lens **250** to the other negative lenses to avoid the significant aberration caused by the incident rays.

The parameters of the lenses of the second embodiment are listed in Table 3 and Table 4.

TABLE 3

f = 3.73617 mm; f/HEP = 2.05; HAF = 37.5 deg; tan(HAF) = 0.7673						
Surface		Radius of curvature (mm)	Thickness (mm)	Material	Refractive index	Abbe number
0	Object	plane	infinity			
1	Aperture	plane	-0.29314			
2	1 <sup>st</sup> lens	1.55019	0.485702	plastic	1.5441	56.1
3		5.57808	0.573897			
4	2 <sup>nd</sup> lens	-4.51338	0.431526	plastic	1.5441	56.1
5		-1.72725	0.104831			
6	3 <sup>rd</sup> lens	-1.02096	0.23	plastic	1.6425	22.465
7		-2.06286	0.393512			
8	4 <sup>th</sup> lens	3.40929	0.606578	plastic	1.6142	25.59
9		-2.88795	0.385878			
10	5 <sup>th</sup> lens	-2.18563	0.201715	plastic	1.5441	56.1
11		3.34847	0.3			
12	Filter	plane	0.2		1.517	64.2
13		plane	0.594835			
14	Image plane	plane	-0.00847			

Reference wavelength: 555 nm

TABLE 4

Coefficients of the aspheric surfaces					
Surface	2	3	4	5	6
k	-0.014137	-9.617622	-6.992485	-3.9719	-2.261144
A4	3.50872E-03	5.26325E-03	-1.02501E-01	-9.08359E-02	2.14378E-02
A6	3.73889E-03	-9.55385E-03	-2.18613E-02	7.98399E-02	7.05677E-02
A8	-4.63034E-03	-2.66210E-02	-9.76049E-02	-1.29003E-01	-1.02874E-01
A10	3.10388E-03	-8.42124E-03	1.97474E-02	-4.53549E-02	-1.35856E-03
A12	-4.70632E-02	1.32845E-01	6.53677E-02	-8.17092E-03	-2.88475E-02
A14	8.89250E-02	-3.91880E-01	-4.33721E-02	3.50727E-02	1.63909E-02
A16	-6.77938E-02	4.02388E-01	-1.41837E-01	2.04185E-02	4.87130E-02
A18	2.52211E-03	-1.56641E-01	1.11366E-01	-1.71945E-02	-4.56600E-02
A20					
Surface	7	8	9	10	11
k	-1.066389	-15.633165	-23.312562	-0.140216	-49.59024
A4	3.03418E-02	-3.36733E-02	-1.37877E-03	2.55377E-04	-2.40682E-02
A6	6.17927E-03	-2.46620E-03	-6.62558E-04	5.33694E-03	5.23907E-04
A8	8.46591E-03	-1.24603E-04	-3.78081E-04	1.88047E-03	8.11577E-05
A10	1.38731E-02	-1.01770E-05	-6.46074E-05	-7.89433E-05	-5.45660E-05
A12	2.17513E-03	-3.52464E-05	-7.88480E-06	-1.95736E-04	-5.51843E-06
A14	-5.76279E-03	-2.72652E-06	-3.67304E-06	-1.17001E-05	4.55719E-08
A16	-6.16033E-03	1.62638E-06	-7.08326E-07	6.26770E-06	1.22706E-07
A18	4.34621E-03	5.46949E-08	6.90943E-08	5.64306E-07	-2.48651E-08
A20					

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An equation of the aspheric surfaces of the second embodiment is the same as that of the first embodiment, and the definitions are the same as well.

The exact parameters of the second embodiment based on Table 3 and Table 4 are listed in the following table:

TDT	0.3739%	InRS51	-0.8039
ODT	2.5%	InRS52	-0.5513
$\Sigma PP$	11.2567	InRS51 /TP5	3.9853
$\Sigma NP$	-5.8096	InRS52 /TP5	2.7332
f1/ $\Sigma PP$	0.3351	HIF511	0
f5/ $\Sigma NP$	0.4117	HIF512	0
IN12/f	0.1536	HIF521	0.5485
HOS/f	1.2044	HIF522	0
HOS	4.5	HIF311	0
InTL	3.4136	HIF312	0
HOS/HOI	1.5340	HIF321	0.7646
InS/HOS	0.9349	HIF322	0
InTL/HOS	0.7586	f/f1	0.9905
$\Sigma TP$ /InTL	0.5729	f/f2	0.7687
(TP1 + IN12)/TP2	2.4555	f/f3	1.0932
(TP5 + IN45)/TP4	0.9687	f/f4	1.4236
(TP2 + TP3 + TP4)/ $\Sigma TP$	0.6485	f/f5	1.5620

## Third Embodiment

As shown in FIG. 3A and FIG. 3B, an optical image capturing system of the third preferred embodiment of the present invention includes, along an optical axis from an object side to an image side, an aperture **300**, a first lens **310**, a second lens **320**, a third lens **330**, a fourth lens **340**, a fifth lens **350**, an infrared rays filter **370**, an image plane **380**, and an image sensor **390**.

The first lens **310** has positive refractive power, and is made of plastic. An object-side surface **312** thereof, which faces the object side, is a convex aspheric surface, and an image-side surface **314** thereof, which faces the image side, is a concave aspheric surface, and the image-side surface **314** has an inflection point. The first lens **310** satisfies  $SGI121=0.0358931$  mm and  $|SGI121|/(|SGI121|+TP1)=0.063758371$ , where  $SGI121$  is a displacement in parallel to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The first lens further satisfies  $HIF121=0.613321$  mm and  $HIF121/HOI=0.209074825$ , where  $HIF121$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens **320** has positive refractive power, and is made of plastic. Both an object-side surface **322**, which faces the object side, and an image-side surface **324**, which faces the image side, thereof are convex aspheric surfaces, and the object-side surface **322** has two inflection points. The second lens **320** satisfies  $SGI211=0.00003$  mm and  $|SGI211|/(|SGI211|+TP2)=0.0000569$ , where  $SGI211$  is a displacement in parallel to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The second lens further satisfies  $SGI212=-0.116102$  mm and  $|SGI212|/(|SGI212|+TP2)=0.267770943$ , where  $SGI212$  is a displacement in parallel to the optical axis from a point on the object-side surface of the second lens, through

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which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis.

The second lens further satisfies  $HIF211=0.0902456$  mm and  $HIF211/HOI=0.030763798$ , where  $HIF211$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens further satisfies  $HIF212=0.919918$  mm and  $HIF212/HOI=0.313590591$ , where  $HIF212$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the second the closest to the optical axis.

The third lens **330** has positive refractive power, and is made of plastic. An object-side surface **332**, which faces the object side, is a concave aspheric surface, and an image-side surface **334**, which faces the image side, is a convex aspheric surface, and the image-side surface **334** has an inflection point. The third lens **330** satisfies  $SGI321=-0.238578$  mm and  $|SGI321|/(|SGI321|+TP3)=0.378170002$ , where  $SGI321$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The third lens **330** further satisfies  $HIF321=0.854181$  mm;  $HIF321/HOI=0.291181524$ , where  $HIF321$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the closest to the optical axis, and the optical axis.

The fourth lens **340** has a positive refractive power, and is made of plastic. An object-side surface **342**, which faces the object side, is a concave aspheric surface, and an image-side surface **344**, which faces the image side, is a convex aspheric surface.

The fifth lens **350** has negative refractive power, and is made of plastic. Both an object-side surface **352**, which faces the object side, and an image-side surface **354**, which faces the image side, thereof are concave aspheric surfaces. The object-side surface **352** has three inflection points, and the image-side surface **354** has an inflection point. The fifth lens **350** satisfies  $SGI511=-0.419938$  mm;  $SGI521=0.0343486$  mm;  $|SGI511|/(|SGI511|+TP5)=0.677387094$ ; and  $|SGI521|/(|SGI521|+TP5)=0.146570536$ , where  $SGI511$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI521$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fifth lens **350** further satisfies  $SGI512=-0.632485$  mm and  $|SGI512|/(|SGI512|+TP5)=0.759755431$ , where  $SGI512$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second the closest to the optical axis.

The fifth lens **350** further satisfies  $SGI513=-0.659028$  mm and  $|SGI513|/(|SGI513|+TP5)=0.767178718$ , where  $SGI513$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through

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which the optical axis passes, to the inflection point on the object-side surface, which is the third the closest to the optical axis.

The fifth lens 350 further satisfies  $HIF511=1.41761$  mm;  $HIF521=0.574215$  mm;  $HIF511/HOI=0.483248679$ ; and  $HIF521/HOI=0.195743992$ , where  $HIF511$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis, and  $HIF521$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fifth lens 350 further satisfies  $HIF512=1.86371$  mm and  $HIF512/HOI=0.635319584$ , where  $HIF512$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the second the closest to the optical axis, and the optical axis.

The fifth lens 350 further satisfies  $HIF513=1.92106$  mm and  $HIF513/HOI=0.65486961$ , where  $HIF513$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the third the closest to the optical axis, and the optical axis.

The infrared rays filter 370 is made of glass, and between the fifth lens 350 and the image plane 380. The infrared rays filter 370 gives no contribution to the focal length of the system.

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The parameters of the lenses of the third preferred embodiment are  $|f2|+|f3|+|f4|=134.5847$  mm;  $|f1|+|f5|=6.3780$  mm; and  $|f2|+|f3|+|f4|>|f1|+|f5|$ , where  $f1$  is a focal length of the first lens 310;  $f2$  is a focal length of the second lens 320;  $f3$  is a focal length of the third lens 330; and  $f4$  is a focal length of the fourth lens 340; and  $f5$  is a focal length of the fifth lens 350.

The optical image capturing system of the third preferred embodiment further satisfies  $TP4=0.5810$  mm and  $TP5=0.2000$  mm, where  $TP4$  is a thickness of the fourth lens 340 on the optical axis, and  $TP5$  is a thickness of the fifth lens 350 on the optical axis.

The optical image capturing system of the third preferred embodiment further satisfies  $\Sigma PP=f1+f2+f3+f4=138.4992$  mm and  $f1/(f1+f2+f3+f4)=0.0283$ , where  $\Sigma PP$  is a sum of the focal lengths of each positive lens. It is helpful to sharing the positive refractive powers of the first lens 310 to the other positive lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the third preferred embodiment further satisfies  $\Sigma NP=f5=-2.4635$  mm, where  $\Sigma NP$  is a sum of the focal lengths of each negative lens.

The parameters of the lenses of the third embodiment are listed in Table 5 and Table 6.

TABLE 5

$f = 3.73358$ mm; $f/HEP = 2.05$ ; $HAF = 37.5$ deg; $\tan(HAF) = 0.7673$						
Surface	Radius of curvature (mm)	Thickness (mm)	Material	Refractive index	Abbe number	Focal length (mm)
0	Object plane	infinity				
1	Aperture plane	-0.28783				
2	1 <sup>st</sup> lens	1.5409	0.527062 plastic	1.5441	56.0936	3.9145
3		4.85792	0.489361			
4	2 <sup>nd</sup> lens	115.1264	0.317485 plastic	1.5441	56.0936	31.0086
5		-19.8251	0.398047			
6	3 <sup>rd</sup> lens	-1.27512	0.392297 plastic	1.6425	22.465	100
7		-1.40172	0.05			
8	4 <sup>th</sup> lens	-25.1813	0.581038 plastic	1.5441	56.0936	3.57607
9		-1.8264	0.459379			
10	5 <sup>th</sup> lens	-2.06778	0.2 plastic	1.5346	56.07	-2.46346
11		3.78326	0.3			
12	Filter	plane	0.2	1.517	64.2	
13		plane	0.590802			
14	Image plane	plane	-0.00547			

Reference wavelength: 555 nm

TABLE 6

Coefficients of the aspheric surfaces					
Surface	2	3	4	5	6
k	-0.25951	9.415402	50	-49.897066	0.470805
A4	4.78151E-03	-1.90620E-02	-8.68067E-02	-6.70132E-02	8.08562E-02
A6	1.61140E-02	-2.85554E-02	-1.03967E-01	-7.81192E-02	4.01965E-02
A8	-3.62587E-02	-1.77557E-02	2.73175E-02	-4.56985E-02	-2.67176E-02
A10	1.86146E-02	-3.43074E-03	-2.25781E-02	-6.85619E-03	2.26771E-02
A12	4.82498E-03	5.11491E-02	-5.39131E-02	2.50775E-02	6.05700E-03
A14	-1.56659E-02	-1.56407E-01	-1.42712E-02	5.83725E-04	-3.67741E-02
A16	-4.21928E-03	1.06095E-01	9.38904E-02	-2.66081E-02	6.85779E-02
A18	-2.03231E-03	-1.06315E-02	3.24556E-03	2.71042E-02	-3.52185E-02
A20					
Surface	7	8	9	10	11
k	0.021118	50	-2.556424	-0.798246	-32.242001
A4	7.80579E-02	-3.04939E-02	4.44007E-03	2.43426E-02	-3.17486E-02



TABLE 6-continued

Coefficients of the aspheric surfaces					
A6	1.31945E-02	3.63840E-03	1.04533E-03	-6.96291E-03	2.66213E-03
A8	7.14122E-03	-5.23017E-04	-1.57310E-04	2.33553E-03	-1.02965E-04
A10	1.62027E-02	7.39189E-05	-1.22232E-04	1.05841E-04	-2.83264E-05
A12	1.09523E-02	-5.53116E-08	-1.50294E-05	-5.57252E-04	-5.78839E-06
A14	-5.18479E-03	8.16043E-06	-5.41743E-07	4.41714E-05	-2.91861E-07
A16	-1.13291E-02	2.10395E-06	2.98820E-07	1.80752E-05	8.25778E-08
A18	5.63487E-03	-1.21664E-06	2.73321E-07	-2.27031E-06	-9.87595E-09
A20					

An equation of the aspheric surfaces of the third embodiment is the same as that of the first embodiment, and the definitions are the same as well.

The exact parameters of the third embodiment based on Table 5 and Table 6 are listed in the following table:

[TDT]	0.5361%	InRS51	-0.71349
[ODT]	2.5%	InRS52	-0.574799
$\Sigma$ PP	138.4992	InRS51 /TP5	3.5675
$\Sigma$ NP	-2.4635	InRS52 /TP5	2.8740
f1/ $\Sigma$ PP	0.0283	HIF511	1.41761
f5/ $\Sigma$ NP	1	HIF512	1.86371
IN12/f	0.1311	HIF521	0.574215
HOS/f	1.2053	HIF522	0
HOS	4.5	HIF311	0
InTL	3.4147	HIF312	0
HOS/HOI	1.5340	HIF321	0.854181
InS/HOS	0.9360	HIF322	0
InTL/HOS	0.7588	f/f1	0.9538
$\Sigma$ TP/InTL	0.5909	f/f2	0.1204
(TP1 + IN12)/TP2	3.2015	f/f3	0.0373
(TP5 + IN45)/TP4	1.1348	f/f4	1.0440
(TP2 + TP3 + TP4)/ $\Sigma$ TP	0.6397	f/f5	1.5156

#### Fourth Embodiment

As shown in FIG. 4A and FIG. 4B, an optical image capturing system of the fourth preferred embodiment of the present invention includes, along an optical axis from an object side to an image side, an aperture **400**, a first lens **410**, a second lens **420**, a third lens **430**, a fourth lens **440**, a fifth lens **450**, an infrared rays filter **470**, an image plane **480**, and an image sensor **490**.

The first lens **410** has positive refractive power, and is made of plastic. An object-side surface **412** thereof, which faces the object side, is a convex aspheric surface, and an image-side surface **414** thereof, which faces the image side, is a concave aspheric surface, and each of them has an inflection point respectively. The first lens **410** satisfies  $SGI111=0.200123$  mm;  $SGI121=0.00212328$  mm;  $|SGI111|/(|SGI111|+TP1)=0.246038147$ ; and  $|SGI121|/(|SGI121|+TP1)=0.003450343$ , where  $SGI111$  is a displacement in parallel to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis, and  $SGI121$  is a displacement in parallel to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The first lens **410** further satisfies  $HIF111=0.815455$  mm;  $HIF121=0.225965$  mm;  $HIF111/HOI=0.277980228$ ; and  $HIF121/HOI=0.077029146$ , where  $HIF111$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the first lens, through which the

optical axis passes, to the inflection point, which is the closest to the optical axis, and  $HIF121$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens **420** has negative refractive power, and is made of plastic. An object-side surface thereof, which faces the object side, is a convex aspheric surface, and an image-side surface thereof, which faces the image side, is a concave aspheric surface.

The third lens **430** has positive refractive power, and is made of plastic. An object-side surface **432**, which faces the object side, is a concave aspheric surface, and an image-side surface **434**, which faces the image side, is a convex aspheric surface, and each has two inflection points. The third lens **430** satisfies  $SGI311=0.032962$  mm;  $SGI321=0.0207769$  mm;  $|SGI311|/(|SGI311|+TP3)=0.089989298$ ; and  $|SGI321|/(|SGI321|+TP3)=0.058674752$ , where  $SGI311$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis, and  $SGI321$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The third lens **430** further satisfies  $SGI312=0.05311$  mm;  $SGI322=-0.0196993$  mm;  $|SGI312|/(|SGI312|+TP5)=0.137435436$ ; and  $|SGI322|/(|SGI322|+TP3)=0.055801383$ , where  $SGI312$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second the closest to the optical axis, and  $SGI322$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second the closest to the optical axis.

The third lens **430** further satisfies  $HIF311=0.451205$  mm;  $HIF321=0.448495$  mm;  $HIF311/HOI=0.153811147$ ; and  $HIF321/HOI=0.152887336$ , where  $HIF311$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the closest to the optical axis, and the optical axis, and  $HIF321$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the closest to the optical axis, and the optical axis.

The third lens **430** further satisfies  $HIF312=0.903949$  mm;  $HIF322=1.0168$  mm;  $HIF312/HOI=0.308146923$ ; and  $HIF322/HOI=0.34661667$ , where  $HIF312$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the second closest to the optical axis, and the optical axis, and  $HIF322$

is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the second closest to the optical axis, and the optical axis.

The fourth lens **440** has positive refractive power, and is made of plastic. An object-side surface **442**, which faces the object side, is a convex aspheric surface, and an image-side surface **444**, which faces the image side, is a concave aspheric surface. The image-side surface **444** has two inflection points. The fourth lens **440** satisfies  $SGI421 = -0.288516$  mm and  $|SGI421|/(|SGI421|+TP4) = 0.379394186$ , where  $SGI421$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The fourth lens **440** further satisfies  $SGI422 = -0.483235$  mm and  $|SGI422|/(|SGI422|+TP4) = 0.505907762$ , where  $SGI422$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis.

The fourth lens **440** further satisfies  $HIF421 = 0.821549$  mm and  $HIF421/HOI = 0.28005761$ , where  $HIF421$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fourth lens **440** further satisfies  $HIF422 = 1.29988$  mm and  $HIF422/HOI = 0.443115732$ , where  $HIF422$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis.

The fifth lens **450** has negative refractive power, and is made of plastic. Both an object-side surface **452**, which faces the object side, and an image-side surface **454**, which faces the image side, thereof are concave aspheric surfaces, and each of them has two inflection points. The fifth lens **450** satisfies  $SGI511 = 0.00669328$  mm;  $SGI521 = 0.0960792$  mm;  $|SGI511|/(|SGI511|+TP5) = 0.013155102$ ; and  $|SGI521|/(|SGI521|+TP5) = 0.160618352$ , where  $SGI511$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI521$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fifth lens **450** further satisfies  $SGI512 = -0.111977$  mm;  $SGI522 = -0.0598915$  mm;  $|SGI512|/(|SGI512|+TP5) = 0.182348908$ ;  $|SGI522|/(|SGI522|+TP5) = 0.106569359$ , where  $SGI512$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis, and  $SGI522$  is a displacement in parallel to the optical axis from a point on the image-side surface of the

fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis.

The fifth lens **450** further satisfies  $HIF511 = 0.270916$  mm;  $HIF521 = 0.506464$  mm;  $HIF511/HOI = 0.09235248$ ; and  $HIF521/HOI = 0.172648372$ , where  $HIF511$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis, and  $HIF521$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fifth lens **450** further satisfies  $HIF512 = 1.25206$  mm;  $HIF522 = 2.15071$  mm;  $HIF512/HOI = 0.426814386$ ; and  $HIF522/HOI = 0.733154934$ , where  $HIF512$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis, and  $HIF522$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis.

The infrared rays filter **470** is made of glass, and between the fifth lens **450** and the image plane **480**. The infrared rays filter **470** gives no contribution to the focal length of the system.

The optical image capturing system of the fourth preferred embodiment has the following parameters, which are  $|f2|+|f3|+|f4| = 20.3329$  mm;  $|f1|+|f5| = 6.0723$  mm; and  $|f2|+|f3|+|f4| > |f1|+|f5|$ , where  $f1$  is a focal length of the first lens **410**;  $f2$  is a focal length of the second lens **420**;  $f3$  is a focal length of the third lens **430**;  $f4$  is a focal length of the fourth lens **440**; and  $f5$  is a focal length of the fifth lens **450**.

The optical image capturing system of the fourth preferred embodiment further satisfies  $TP4 = 0.4719$  mm and  $TP5 = 0.5021$  mm, where  $TP4$  is a thickness of the fourth lens on the optical axis, and  $TP5$  is a thickness of the fifth lens on the optical axis.

In the fourth embodiment, the first, the third, and the fourth lenses **410**, **430**, and **440** are positive lenses, and their focal lengths are  $f1$ ,  $f3$ , and  $f4$ . The optical image capturing system of the fourth preferred embodiment further satisfies  $\Sigma PP = f1+f3+f4 = 17.4948$  mm and  $f1/(f1+f3+f4) = 0.2089$ , where  $\Sigma PP$  is a sum of the focal lengths of each positive lens. It is helpful to sharing the positive refractive powers of the first lens **410** to the other positive lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the fourth preferred embodiment further satisfies  $\Sigma NP = f2+f5 = -8.9104$  mm and  $f5/(f2+f5) = 0.2713$ , where  $f2$  and  $f5$  are focal lengths of the second and the fifth lenses, and  $\Sigma NP$  is a sum of the focal lengths of each negative lens. It is helpful to sharing the negative refractive powers of the fifth lens **450** to the other negative lenses to avoid the significant aberration caused by the incident rays.

The parameters of the lenses of the fourth embodiment are listed in Table 7 and Table 8.

TABLE 7

$f = 3.68765$ mm; $f/HEP = 2.05$ ; $HAF = 38$ deg; $\tan(HAF) = 0.7813$						
Surface	Radius of curvature (mm)	Thickness (mm)	Material	Refractive index	Abbe number	Focal length (mm)
0	Object	plane	infinity			
1		plane	0			

TABLE 7-continued

f = 3.68765 mm; f/HEP = 2.05; HAF = 38 deg; tan(HAF) = 0.7813							
Surface	Radius of curvature (mm)	Thickness (mm)	Material	Refractive index	Abbe number	Focal length (mm)	
2	1 <sup>st</sup> lens/Aperture	1.661715	0.613259	plastic	1.535	56.1	3.65523
3		9.5	0.03841				
4	2 <sup>nd</sup> lens	4.410298	0.3	plastic	1.643	22.5	-6.4933
5		2.095114	0.3				
6	3 <sup>rd</sup> lens	2.565918	0.333326	plastic	1.535	56.1	11.1432
7		4.292405	0.502411				
8	4 <sup>th</sup> lens	-2.11857	0.471949	plastic	1.535	56.1	2.69636
9		-0.92632	0.158316				
10	5 <sup>th</sup> lens	4.440027	0.502104	plastic	1.535	56.1	-2.41708
11		0.963795	0.340348				
12	Filter	plane	0.21	1.517	64.2		
13		plane	0.709877				
14	Image plane	plane	0				

Reference wavelength: 555 nm

TABLE 8

Coefficients of the aspheric surfaces					
Surface	2	3	4	5	6
k	-5.64626E+00	-3.74029E+01	-1.08126E+02	-1.01530E+01	-2.07310E+01
A4	1.40603E-01	-2.43992E-01	-1.05391E-01	-1.39433E-02	-4.00093E-02
A6	-9.40997E-02	6.85672E-01	3.72195E-01	3.04690E-01	6.41498E-02
A8	-1.13170E-02	-7.86656E-01	1.79723E-01	-4.48499E-01	-8.91312E-01
A10	1.87365E-01	-7.48882E-01	-2.21677E+00	6.08376E-01	2.41287E+00
A12	-4.06461E-01	2.37324E+00	3.53652E+00	-8.55515E-01	-3.28858E+00
A14	3.99062E-01	-1.93760E+00	-2.28768E+00	8.36620E-01	2.25240E+00
A16	-2.29569E-01	5.47090E-01	5.41358E-01	-3.23940E-01	-5.89713E-01
A18	5.85201E-02	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
A20	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
Surface	7	8	9	10	11
k	1.01980E+01	1.28599E+00	-3.10422E+00	-8.21767E+01	-6.39094E+00
A4	-5.81996E-02	1.78350E-01	-2.23010E-02	-2.04418E-01	-1.28257E-01
A6	-1.53316E-01	-4.57068E-01	-1.88600E-01	2.01606E-01	8.64602E-02
A8	1.52353E-01	1.65829E+00	7.08455E-01	-2.03429E-01	-4.98270E-02
A10	-2.37631E-01	-4.08668E+00	-1.22197E+00	1.48407E-01	1.96872E-02
A12	2.42492E-01	6.41709E+00	1.28265E+00	-6.64032E-02	-5.28849E-03
A14	-1.60049E-01	-6.35179E+00	-8.06529E-01	1.81506E-02	9.72957E-04
A16	5.73563E-02	3.79979E+00	2.93593E-01	-2.98191E-03	-1.21454E-04
A18	0.00000E+00	-1.24581E+00	-5.70956E-02	2.71548E-04	9.53845E-06
A20	0.00000E+00	1.71017E-01	4.59424E-03	-1.05608E-05	-3.54660E-07

An equation of the aspheric surfaces of the fourth embodiment is the same as that of the first embodiment, and the definitions are the same as well.

The exact parameters of the fourth embodiment based on Table 7 and Table 8 are listed in the following table:

TDT	0.6919%	InRS51	-0.217564
ODT	2.8921%	InRS52	-0.166513
ΣPP	17.4948	InRS51 /TP5	0.4333
ΣNP	-8.9104	InRS52 /TP5	0.3316
f1/ΣPP	0.2089	HIF511	0.270916
f5/ΣNP	0.2713	HIF512	1.25206
IN12/f	0.0104	HIF521	0.506464
HOS/f	1.2149	HIF522	2.15071
HOS	4.48	HIF311	0.451205
InTL	3.21977	HIF312	0.903949
HOS/HOI	1.5272	HIF321	0.448495
InS/HOS	0.9470	HIF322	1.0168
InTL/HOS	0.7187	f/f1	1.0089
ΣTP/InTL	0.6897	f/f2	0.5679
(TP1 + IN12)/TP2	2.1722	f/f3	0.3309

-continued

50	(TP5 + IN45)/TP5	1.3993	f/f4	1.3676
	(TP2 + TP3 + TP4)/ΣTP	0.4977	f/f5	1.5257

## Fifth Embodiment

As shown in FIG. 5A and FIG. 5B, an optical image capturing system of the fifth preferred embodiment of the present invention includes, along an optical axis from an object side to an image side, an aperture **500**, a first lens **510**, a second lens **520**, a third lens **530**, a fourth lens **540**, a fifth lens **550**, an infrared rays filter **570**, an image plane **580**, and an image sensor **590**.

The first lens **510** has positive refractive power, and is made of plastic. Both an object-side surface **512**, which faces the object side, and an image-side surface **514** thereof, which faces the image side, are convex aspheric surfaces, and the object-side surface **512** has an inflection point. The

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first lens **510** satisfies  $SGI111=0.0767781$  mm and  $|SGI111|/(|SGI111|+TP1)=0.141136187$ , where  $SGI111$  is a displacement in parallel to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The first lens further satisfies  $HIF111=0.571706$  mm and  $HIF111/HOI=0.248892468$ , where  $HIF111$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens **520** has negative refractive power, and is made of plastic. An object-side surface **522** thereof, which faces the object side, is a convex aspheric surface, and an image-side surface **524** thereof, which faces the image side, is a concave aspheric surface, and each of them has an inflection point. The second lens **520** satisfies  $SGI211=0.00453749$  mm;  $SGI221=0.0802085$  mm;  $|SGI211|/(|SGI211|+TP2)=0.009618227$ ; and  $|SGI221|/(|SGI221|+TP2)=0.250488354$ , where  $SGI211$  is a displacement in parallel to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI221$  is a displacement in parallel to the optical axis from a point on the image-side surface of the second lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The second lens further satisfies  $HIF211=0.403308$  mm;  $HIF221=0.582844$  mm;  $HIF211/HOI=0.175580322$ ; and  $HIF221/HOI=0.253741402$ , where  $HIF211$  is a displacement perpendicular to the optical axis from a point on the image-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The third lens **530** has positive refractive power, and is made of plastic. An object-side surface **532**, which faces the object side, is a convex aspheric surface, and an image-side surface **534**, which faces the image side, is a concave aspheric surface, and each of them has two inflection points. The third lens **530** satisfies  $SGI311=0.051302$  mm;  $SGI321=0.0132421$  mm;  $|SGI311|/(|SGI311|+TP3)=0.122577223$ ; and  $|SGI321|/(|SGI321|+TP3)=0.034804758$ , where  $SGI311$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI321$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The third lens **530** further satisfies  $SGI312=0.0878365$  mm;  $SGI322=0.0185546$  mm;  $|SGI312|/(|SGI312|+TP5)=0.193020739$ ; and  $|SGI322|/(|SGI322|+TP3)=0.04809625$ , where  $SGI312$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis, and  $SGI322$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis.

The third lens **530** further satisfies  $HIF311=0.486251$  mm;  $HIF321=0.491163$  mm;  $HIF311/HOI=0.211689595$ ;

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and  $HIF321/HOI=0.213828037$ , where  $HIF311$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the closest to the optical axis, and the optical axis, and  $HIF321$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the closest to the optical axis, and the optical axis.

The third lens **530** further satisfies  $HIF312=0.738394$  mm;  $HIF322=0.806132$  mm;  $HIF312/HOI=0.321460165$ ; and  $HIF322/HOI=0.350949935$ , where  $HIF312$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the second closest to the optical axis, and the optical axis, and  $HIF322$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the second closest to the optical axis, and the optical axis.

The fourth lens **540** has a positive refractive power, and is made of plastic. An object-side surface **542**, which faces the object side, is a concave aspheric surface, and an image-side surface **544**, which faces the image side, is a convex aspheric surface, and each of them has two inflection points. The fourth lens **540** satisfies  $SGI411=-0.12685$  mm;  $SGI421=-0.301629$  mm;  $|SGI411|/(|SGI411|+TP4)=0.207360014$ ; and  $|SGI421|/(|SGI421|+TP4)=0.383499657$ , where  $SGI411$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI421$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fourth lens **540** further satisfies  $SGI412=-0.229331$  mm;  $SGI422=-0.482163$  mm;  $|SGI412|/(|SGI412|+TP4)=0.32109339$ ; and  $|SGI422|/(|SGI422|+TP4)=0.498591077$ , where  $SGI412$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis, and  $SGI422$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis.

The fourth lens **540** further satisfies  $HIF411=0.584829$  mm;  $HIF421=0.710318$  mm;  $HIF411/HOI=0.254605572$ ; and  $HIF421/HOI=0.309237266$ , where  $HIF411$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis, and  $HIF421$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fourth lens **540** further satisfies  $HIF412=0.935364$  mm;  $HIF422=1.0617$  mm;  $HIF412/HOI=0.407211145$ ; and  $HIF422/HOI=0.46221158$ , where  $HIF412$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis, and  $HIF422$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis.

The fifth lens **550** has negative refractive power, and is made of plastic. An object-side surface **552**, which faces the

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object side, is a convex aspheric surface, and an image-side surface **554**, which faces the image side, thereof is a concave aspheric surface, and each of them has an inflection point. The fifth lens **550** satisfies  $SGI511=0.0421076$  mm;  $SGI521=0.128996$  mm;  $|SGI511|/(|SGI511|+TP5)=0.068110522$ ; and  $|SGI521|/(|SGI521|+TP5)=0.182943727$ , where  $SGI511$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI521$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fifth lens **550** further satisfies  $HIF511=0.447148$  mm;  $HIF521=0.520736$  mm;  $HIF511/HOI=0.194666086$ ; and  $HIF521/HOI=0.226702656$ , where  $HIF511$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis, and  $HIF521$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The infrared rays filter **570** is made of glass, and between the fifth lens **550** and the image plane **580**. The infrared rays filter **570** gives no contribution to the focal length of the system.

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The parameters of the lenses of the fifth preferred embodiment are  $|f2|+|f3|+|f4|=9.4560$  mm;  $|f1|+|f5|=5.2532$  mm; and  $|f2|+|f3|+|f4|>|f1|+|f5|$ , where  $f1$  is a focal length of the first lens **510**;  $f2$  is a focal length of the second lens **520**;  $f3$  is a focal length of the third lens **530**; and  $f4$  is a focal length of the fourth lens **540**; and  $f5$  is a focal length of the fifth lens **550**.

The optical image capturing system of the fifth preferred embodiment further satisfies  $TP4=0.4849$  mm and  $TP5=0.5761$  mm, where  $TP4$  is a thickness of the fourth lens **540** on the optical axis, and  $TP5$  is a thickness of the fifth lens **550** on the optical axis.

The optical image capturing system of the fifth preferred embodiment further satisfies  $\Sigma PP=f1+f3+f4=9.1580$  mm and  $f1/(f1+f3+f4)=0.2904$ , where  $\Sigma PP$  is a sum of the focal lengths of each positive lens. It is helpful to sharing the positive refractive powers of the first lens **510** to the other positive lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the fifth preferred embodiment further satisfies  $\Sigma NP=f2+f5=-5.5513$  mm; and  $f5/(f2+f5)=0.4673$ , where  $\Sigma NP$  is a sum of the focal lengths of each negative lens.

The parameters of the lenses of the fifth embodiment are listed in Table 9 and Table 10.

TABLE 9

$f = 2.5865$ mm; $f/HEP = 1.84$ ; $HAF = 40.5023$ deg; $\tan(HAF) = 0.8542$						
Surface	Radius of curvature (mm)		Thickness (mm)	Material	Refractive index	Abbe number
0	Object	plane	infinity			
1	Aperture	plane	600			
2	1 <sup>st</sup> lens	1.97767	0.467222	plastic	1.5346	56.0493
3		-4.60888	0.059668			
4	2 <sup>nd</sup> lens	9.84426	0.24	plastic	1.6425	22.4554
5		1.57135	0.163865			
6	3 <sup>rd</sup> lens	1.80017	0.367226	plastic	1.5346	56.0493
7		8.81208	0.346631			
8	4 <sup>th</sup> lens	-1.10175	0.484888	plastic	1.5346	56.0493
9		-0.67415	0.027			
10	5 <sup>th</sup> lens	1.92949	0.576117	plastic	1.5346	56.0493
11		0.7222	0.325091			
12	Filter	plane	0.21			
13		plane	0.57			
14	Image plane	plane	0			

Reference wavelength: 555 nm

TABLE 10

Coefficients of the aspheric surfaces					
Surface	2	3	4	5	6
k	-17.548	20.72007	-1458.5	-10.102	-30.452
A4	2.16810E-01	-1.91737E-02	-7.79360E-02	-1.89220E-01	1.77640E-01
A6	-4.05220E-01	5.62482E-01	4.35910E-01	9.27040E-01	-8.13350E-01
A8	4.94800E-01	-2.44628E+00	-1.10450E+00	-2.31830E+00	2.04860E+00
A10	-1.31620E+00	2.87229E+00	1.45050E+00	3.46340E+00	-3.53560E+00
A12	2.41040E+00	-8.31653E-01	-1.26780E+00	-3.48440E+00	3.46920E+00
A14	-2.12010E+00	-5.92440E-01	6.94020E-01	2.14430E+00	-1.57340E+00
A16	-5.78930E-01	9.56615E-02	-1.70820E-01	-5.88790E-01	2.34740E-01
A18	8.56960E-01		7.99370E-01	9.04260E-01	9.32410E-01
A20					
Surface	7	8	9	10	11

TABLE 10-continued

Coefficients of the aspheric surfaces					
k	-220.47	-0.2298	-3.7604	-13.45	-5.0734
A4	3.52410E-02	3.56040E-01	-1.01020E+00	-4.70200E-01	-1.93170E+00
A6	-7.57280E-03	6.39890E-02	3.41410E+00	-5.25100E+00	3.72680E+00
A8	-4.54180E-01	-1.64550E+00	-9.10050E+00	2.62670E+01	-5.76430E+00
A10	1.44980E+00	5.97970E+00	1.65970E+01	-6.61760E+01	4.90790E+00
A12	-2.46040E+00	-9.44460E+00	-1.55700E+01	9.47930E+01	-2.30280E+00
A14	2.02280E+00	7.06870E+00	6.60480E+00	-7.14380E+01	8.23710E-01
A16	-5.92280E-01	-2.05660E+00	-9.53720E-01	2.18430E+01	-4.04360E-01
A18	9.47530E-01	1.00130E+00	1.18040E+00	1.74380E+00	2.07930E+00
A20					

An equation of the aspheric surfaces of the fifth embodiment is the same as that of the first embodiment, and the definitions are the same as well.

The exact parameters of the fifth embodiment based on Table 9 and Table 10 are listed in the following table:

TDT	0.6919%	InRS51	-0.038646
ODT	2.8921%	InRS52	0.141591
ΣPP	9.1580	InRS51 /TP5	0.0671
ΣNP	-5.5513	InRS52 /TP5	0.2458
f1/ΣPP	0.2904	HIF511	0.447148
f5/ΣNP	0.4673	HIF512	0
IN12/f	0.0231	HIF521	0.520736
HOS/f	1.4837	HIF522	0
HOS	3.83771	HIF311	0.486251
InTL	2.73262	HIF312	0.738394
HOS/HOI	1.6707	HIF321	0.491163
InS/HOS	0.9726	HIF322	0.806132
InTL/HOS	0.7120	f/f1	0.9726
ΣTP/InTL	0.7815	f/f2	0.8746
(TP1 + IN12)/TP2	2.1954	f/f3	0.6211
(TP5 + IN45)/TP5	1.2438	f/f4	1.1080
(TP2 + TP3 + TP4)/ΣTP	0.5114	f/f5	0.9971

### Sixth Embodiment

As shown in FIG. 6A and FIG. 6B, an optical image capturing system of the sixth preferred embodiment of the present invention includes, along an optical axis from an object side to an image side, an aperture 600, a first lens 610, a second lens 620, a third lens 630, a fourth lens 640, a fifth lens 650, an infrared rays filter 670, an image plane 680, and an image sensor 690.

The first lens 610 has positive refractive power, and is made of plastic. Both an object-side surface 612, which faces the object side, and an image-side surface 614 thereof, which faces the image side, thereof are convex aspheric surfaces, and the object-side surface 612 has an inflection point. The first lens 610 satisfies  $SGI111=0.13282$  mm and  $|SGI111|/(|SGI111|+TP1)=0.249633031$ , where  $SGI111$  is a displacement in parallel to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The first lens 610 further satisfies  $HIF111=0.557356$  mm and  $HIF111/HOI=0.242328696$ , where  $HIF111$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the first lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens 620 has negative refractive power, and is made of plastic. Both an object-side surface thereof, which faces the object side, and an image-side surface thereof, which faces the image side, thereof are concave aspheric

surfaces, and each of them has three inflection points. The second lens 620 satisfies  $SGI211=-0.006689$  mm and  $|SGI211|/(|SGI211|+TP2)=0.016478211$ , where  $SGI211$  is a displacement in parallel to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The second lens 620 further satisfies  $SGI212=-0.013634$  mm and  $|SGI212|/(|SGI212|+TP2)=0.059791165$ , where  $SGI212$  is a displacement in parallel to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis.

The second lens 620 further satisfies  $SGI213=-0.025093$  mm and  $|SGI213|/(|SGI213|+TP2)=0.104778567$ , where  $SGI213$  is a displacement in parallel to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the third closest to the optical axis.

The second lens 620 further satisfies  $HIF211=0.230075$  mm and  $HIF211/HOI=0.100032609$ , where  $HIF211$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis.

The second lens 620 further satisfies  $HIF212=0.406523$  mm and  $HIF212/HOI=0.17674913$ , where  $HIF212$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the second closest to the optical axis.

The second lens 620 further satisfies  $HIF213=0.599935$  mm and  $HIF213/HOI=0.260841304$ , where  $HIF213$  is a displacement perpendicular to the optical axis from a point on the object-side surface of the second lens, through which the optical axis passes, to the inflection point, which is the third closest to the optical axis.

The third lens 630 has positive refractive power, and is made of plastic. An object-side surface 632, which faces the object side, is a convex aspheric surface, and an image-side surface 634, which faces the image side, is a concave aspheric surface, and the object-side surface 632 has three inflection points. The third lens 630 satisfies  $SGI311=0.008926$  mm;  $SGI321=0.007233$  mm;  $|SGI311|/(|SGI311|+TP3)=0.040333476$ ; and  $|SGI321|/(|SGI321|+TP3)=0.032935359$ , where  $SGI311$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis, and  $SGI321$  is a displacement in parallel to the optical axis from a point on

the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The third lens **630** further satisfies  $SGI312=0.016027$  mm;  $SGI322=0.009358$  mm;  $|SGI312|/(|SGI312|+TP3)=0.07016891$ ; and  $|SGI322|/(|SGI322|+TP3)=0.042203151$ , where  $SGI312$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis, and  $SGI322$  is a displacement in parallel to the optical axis from a point on the image-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis.

The third lens **630** further satisfies  $SGI313=0.027532$  mm and  $|SGI313|/(|SGI313|+TP3)=0.114759223$ , where  $SGI313$  is a displacement in parallel to the optical axis from a point on the object-side surface of the third lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the third closest to the optical axis.

The third lens **630** further satisfies  $HIF311=0.242051$  mm;  $HIF321=0.260156$  mm;  $HIF311/HOI=0.105239565$ ; and  $HIF321/HOI=0.113111304$ , where  $HIF311$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the closest to the optical axis, and the optical axis, and  $HIF321$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the closest to the optical axis, and the optical axis.

The third lens **630** further satisfies  $HIF312=0.516971$  mm;  $HIF322=0.580997$  mm;  $HIF312/HOI=0.22477$ ; and  $HIF322/HOI=0.252607391$ , where  $HIF312$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the second closest to the optical axis, and the optical axis, and  $HIF322$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the third lens, which is the second closest to the optical axis, and the optical axis.

The third lens **630** further satisfies  $HIF313=0.707384$  mm and  $HIF313/HOI=0.307558261$ , where  $HIF313$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the third lens, which is the third closest to the optical axis.

The fourth lens **640** has positive refractive power, and is made of plastic. An object-side surface **642**, which faces the object side, is a concave aspheric surface, and an image-side surface **644**, which faces the image side, is a convex aspheric surface, and the image-side surface **644** has two inflection points. The fourth lens **640** satisfies  $SGI421=-0.169119$  mm and  $|SGI421|/(|SGI421|+TP4)=0.271054011$ , where  $SGI421$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis.

The fourth lens **640** further satisfies  $SGI422=-0.315768$  mm and  $|SGI422|/(|SGI422|+TP4)=0.409779647$ , where  $SGI422$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fourth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the second closest to the optical axis.

The fourth lens **640** further satisfies  $HIF421=0.538907$  mm and  $HIF421/HOI=0.234307391$ , where  $HIF421$  is a distance perpendicular the optical axis between the inflec-

tion point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fourth lens **640** further satisfies  $HIF422=0.891673$  mm and  $HIF422/HOI=0.387683913$ , where  $HIF422$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis.

The fifth lens **650** has negative refractive power, and is made of plastic. An object-side surface **652**, which faces the object side, is a concave aspheric surface, and an image-side surface **654**, which faces the image side, thereof is a convex aspheric surface. The object-side surface **652** has an inflection point, and the image-side surface **654** has three inflection points. The fifth lens **650** satisfies  $SGI511=-0.322008$  mm;  $SGI521=-0.003418$  mm;  $|SGI511|/(|SGI511|+TP5)=0.495992114$ ; and  $|SGI521|/(|SGI521|+TP5)=0.01033784$ , where  $SGI511$  is a displacement in parallel to the optical axis from a point on the object-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the object-side surface, which is the closest to the optical axis, and  $SGI521$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the closest to the optical axis.

The fifth lens **650** further satisfies  $SGI522=-0.004481$  mm and  $|SGI522|/(|SGI522|+TP5)=0.01350948$ , where  $SGI522$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the second closest to the optical axis.

The fifth lens **650** further satisfies  $SGI523=-0.349841$  mm and  $|SGI523|/(|SGI523|+TP5)=0.516711395$ , where  $SGI523$  is a displacement in parallel to the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point on the image-side surface, which is the third closest to the optical axis.

The fifth lens **650** further satisfies  $HIF511=0.97271$  mm;  $HIF521=0.226561$  mm;  $HIF511/HOI=0.422917391$ ; and  $HIF521/HOI=0.098504783$ , where  $HIF511$  is a distance perpendicular the optical axis between the inflection point on the object-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis, and  $HIF521$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the closest to the optical axis, and the optical axis.

The fifth lens **650** further satisfies  $HIF522=0.641323$  mm and  $HIF522/HOI=0.278836087$ , where  $HIF522$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the second closest to the optical axis, and the optical axis.

The fifth lens **650** further satisfies  $HIF523=1.694681$  mm and  $HIF523/HOI=0.736817826$ , where  $HIF523$  is a distance perpendicular the optical axis between the inflection point on the image-side surface of the fourth lens, which is the third closest to the optical axis, and the optical axis.

The infrared rays filter **670** is made of glass, and between the fifth lens **650** and the image plane **680**. The infrared rays filter **670** gives no contribution to the focal length of the system.

The optical image capturing system of the sixth preferred embodiment has the following parameters, which are  $|f2|+|f3|+|f4|=19.7606$  mm;  $|f1|+|f5|=3.2700$  mm; and  $|f2|+|f3|+|f4|>|f1|+|f5|$ , where  $f1$  is a focal length of the first lens **610**;  $f2$  is a focal length of the second lens **620**;  $f3$  is a focal length

of the third lens **630**;  $f_4$  is a focal length of the fourth lens **640**; and  $f_5$  is a focal length of the fifth lens **650**.

The optical image capturing system of the sixth preferred embodiment further satisfies  $TP_4=0.4548$  mm and  $TP_5=0.3272$  mm, where  $TP_4$  is a thickness of the fourth lens 5 on the optical axis, and  $TP_5$  is a thickness of the fifth lens on the optical axis.

In the sixth embodiment, the first, the third, and the fourth lenses **610**, **630**, and **640** are positive lenses, and their focal lengths are  $f_1$ ,  $f_3$ , and  $f_4$ . The optical image capturing system of the sixth preferred embodiment further satisfies  $\Sigma PP=f_1+f_3+f_4=19.0837$  mm and  $f_1/(f_1+f_3+f_4)=0.0886$ , where  $\Sigma PP$  is a sum of the focal lengths of each positive lens.

It is helpful to sharing the positive refractive powers of the first lens **610** to the other positive lenses to avoid the significant aberration caused by the incident rays.

The optical image capturing system of the sixth preferred embodiment further satisfies  $\Sigma NP=f_2+f_5=-3.9469$  mm and  $f_5/(f_2+f_5)=0.4000$ , where  $f_2$  and  $f_5$  are focal lengths of the second and the fifth lenses, and  $\Sigma NP$  is a sum of the focal lengths of each negative lens. It is helpful to sharing the negative refractive powers of the fifth lens **650** to the other negative lenses to avoid the significant aberration caused by the incident rays.

The parameters of the lenses of the sixth embodiment are listed in Table 11 and Table 12.

TABLE 11

$f = 2.83773$ mm; $f/HEP = 2.4$ ; $HAF = 38.6605$ deg; $\tan(HAF) = 0.8000$							
Surface		Radius of curvature (mm)	Thickness (mm)	Material	Refractive index	Abbe number	Focal length (mm)
0	Object	plane	600				
1	Aperture	1.18456	0.399241				
2	1 <sup>st</sup> lens	-3.68537	0	plastic	1.5441	56.09	3.355
3		plane	0.045033				
4	2 <sup>nd</sup> lens	-3.14358	0.214393	plastic	1.6355	23.89	-8.053
5		3.00699	0.167286				
6	3 <sup>rd</sup> lens	2.68802	0.212379	plastic	1.5441	56.09	-589.708
7		3.82951	0.296565				
8	4 <sup>th</sup> lens	-2.1967	0.454812	plastic	1.5441	56.09	-3.85
9		-0.75354	0.458295				
10	5 <sup>th</sup> lens	-0.74066	0.327212	plastic	1.5441	56.09	6.661
11		-6.08962	0.08				
12	Filter	plane	0.175				
13		plane	0.513913				
14	Image plane	plane	0				

Reference wavelength: 555 nm

TABLE 12

Coefficients of the aspheric surfaces					
Surface	2	3	4	5	6
k	1.9568E+00	2.0334E+00	5.0243E+00	1.7812E+00	-9.1494E+00
A4	-2.1502E-01	4.6222E-01	7.1996E-01	2.2114E-01	-5.7323E-01
A6	8.2675E-01	-8.7735E-01	-1.4073E+00	-1.3082E+00	1.2032E+00
A8	-1.2625E+01	-4.2271E+00	-2.5992E+00	8.3507E+00	-7.8450E+00
A10	7.3550E+01	3.3447E+01	3.3806E+01	-2.7786E+01	3.2645E+01
A12	-2.5114E+02	-1.3617E+02	-1.5306E+02	4.9437E+01	-6.0054E+01
A14	4.4130E+02	2.6247E+02	3.1396E+02	-3.9448E+01	5.8411E+01
A16	-3.3548E+02	-1.8954E+02	-2.3240E+02	6.4543E+00	-2.8187E+01
A18					
A20					
Surface	7	8	9	10	11
k	-8.7625E+00	-6.6969E+01	-5.9109E-01	-2.8337E+00	2.0824E+00
A4	-3.7080E-01	-7.6309E-01	3.5851E-01	4.7034E-01	3.2928E-01
A6	8.1877E-01	3.2225E+00	-3.8194E-02	-7.4425E-01	-5.1245E-01
A8	-4.6973E+00	-7.1789E+00	1.3339E+00	5.0757E-01	4.0799E-01
A10	1.3632E+01	9.1544E+00	-2.3424E+00	-1.2456E-01	-2.0641E-01
A12	-1.9159E+01	-7.0084E+00	1.7126E+00	-1.9061E-02	6.4248E-02
A14	1.7693E+01	2.9268E+00	-6.2160E-01	1.4992E-02	-1.1187E-02
A16	-8.2859E+00	-8.5757E-01	1.1434E-01	-2.0511E-03	8.3703E-04
A18					
A20					



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An equation of the aspheric surfaces of the sixth embodiment is the same as that of the first embodiment, and the definitions are the same as well.

The exact parameters of the sixth embodiment based on Table 11 and Table 12 are listed in the following table:

TDT	0.5643%	InRS51	-0.488487
ODT	1.01225%	InRS52	-0.395252
$\Sigma PP$	19.0837	InRS51 /TP5	1.4929
$\Sigma NP$	-3.9469	InRS52 /TP5	1.2079
f1/ $\Sigma PP$	0.0886	HIF511	0.97271
f6/ $\Sigma NP$	0.4000	HIF521	0.226561
IN12/f	0.0159	HIF522	0.641323
HOS/f	1.1784	HIF523	1.694681
HOS	3.344097	HIF311	0.242051
InTL	2.655183	HIF312	0.516971
HOS/HOI	1.4540	HIF321	0.260156
InS/HOS	0.9558	HIF322	0.580997
InTL/HOS	0.7940	f/f1	1.6780
$\Sigma TP/InTL$	0.6056	f/f2	1.1983
(TP1 + IN12)/TP2	2.0721	f/f3	0.1831
(TP5 + IN45)/TP4	1.7271	f/f4	1.5008
(TP2 + TP3 + TP4)/ $\Sigma TP$	0.5482	f/f5	1.7974

It must be pointed out that the embodiments described above are only some preferred embodiments of the present invention. All equivalent structures which employ the concepts disclosed in this specification and the appended claims should fall within the scope of the present invention.

What is claimed is:

1. An optical image capturing system, in order along an optical axis from an object side to an image side, comprising:

- a first lens having positive refractive power;
- a second lens having refractive power;
- a third lens having refractive power;
- a fourth lens having refractive power;
- a fifth lens having refractive power; and
- an image plane;

wherein the optical image capturing system consists of the five lenses with refractive power; at least two of the five lenses each has at least an inflection point on a surface thereof; at least one of the lenses from the second lens to the fifth lens has positive refractive power; the fifth lens has an object-side surface, which faces the object side, and an image-side surface, which faces the image side, and both the object-side surface and the image-side surface of the fifth lens are aspheric surfaces;

wherein the optical image capturing system satisfies:

$$1.2 \leq f/HEP \leq 2.8 \text{ and } 0.5 \leq HOS/f \leq 2.5;$$

where f is a focal length of the optical image capturing system; HEP is an entrance pupil diameter of the optical image capturing system; and HOS is a distance in parallel with the optical axis from an object-side surface of the first lens to the image plane;

wherein the optical image capturing system further satisfies:

$$|TDT| < 1.5\%; \text{ and } |ODT| < 2.5\%; \text{ and}$$

$$39 \text{ deg} \leq HAF \leq 70 \text{ deg};$$

where HAF is a half of a view angle of the optical image capturing system; TDT is a TV distortion; and ODT is an optical distortion.

2. The optical image capturing system of claim 1, wherein the third lens has at least an inflection point on each surface thereof, and the fifth lens has at least an inflection point on each surface thereof.

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3. The optical image capturing system of claim 1, wherein the optical image capturing system further satisfies:

$$0 \text{ mm} < HIF \leq 5 \text{ mm};$$

where HIF is a distance perpendicular to the optical axis between any inflection point and the optical axis.

4. The optical image capturing system of claim 3, wherein the optical image capturing system further satisfies:

$$0 < HIF/InTL \leq 5;$$

where InTL is a distance in parallel with the optical axis between the object-side surface of the first lens and the image-side surface of the fifth lens.

5. The optical image capturing system of claim 3, wherein the optical image capturing system further satisfies:

$$0 < SGI \leq 1 \text{ mm};$$

where SGI is a displacement in parallel with the optical axis from a point on each surface of each of the first lens to the fifth lens, through which the optical axis passes, to the inflection point on said surface.

6. The optical image capturing system of claim 1, wherein the fourth lens has positive refractive power, and the fifth lens has negative refractive power.

7. The optical image capturing system of claim 1, wherein the optical image capturing system further satisfies:

$$0.6 \leq InTL/HOS \leq 0.9;$$

where InTL is a distance in parallel with the optical axis between an object-side surface, which faces the object side, of the first lens and the image-side surface of the fifth lens.

8. The optical image capturing system of claim 4, further comprising an aperture and an image sensor on the image plane, wherein the optical image capturing system further satisfies:

$$0.6 \leq InS/HOS \leq 1.1 \text{ and } 0 < HIF/HOI \leq 0.9;$$

where InS is a distance in parallel with the optical axis between the aperture and the image plane; and HOI is a height for an image formation of the optical image capturing system.

9. An optical image capturing system, in order along an optical axis from an object side to an image side, comprising:

- a first lens having positive refractive power;
- a second lens having refractive power;
- a third lens having refractive power;
- a fourth lens having refractive power;
- a fifth lens having refractive power; and
- an image plane;

wherein the optical image capturing system consists of the five lenses with refractive power; at least two of the five lenses each has at least an inflection point on a surface thereof; at least one of the lenses from the second lens to the fourth lens has positive refractive; the fifth lens has an object-side surface, which faces the object side, and an image-side surface, which faces the image side, and both the object-side surface and the image-side surface of the fifth lens are aspheric surfaces;

wherein the optical image capturing system satisfies:

$$1.2 \leq f/HEP \leq 2.8;$$

$$0.5 \leq HOS/f \leq 2.5;$$

$$0.81 \leq |\tan(HAF)| \leq 1.5;$$

$$|TDT| < 1.5\%; \text{ and } |ODT| \leq 2.5\%;$$

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where  $f$  is a focal length of the optical image capturing system; HEP is an entrance pupil diameter of the optical image capturing system; HOS is a distance in parallel with the optical axis between an object-side surface, which face the object side, of the first lens and the image plane; HAF is a half of a view angle of the optical image capturing system; TDT is a TV distortion; and ODT is an optical distortion.

10. The optical image capturing system of claim 9, wherein the first lens has at least an inflection point on each surface thereof, the third lens has at least an inflection point on each surface thereof, and the fifth lens has at least an inflection point on each surface thereof.

11. The optical image capturing system of claim 9, wherein the third lens has a plurality of inflection points on at least a surface thereof.

12. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$0 \text{ mm} < \text{HOS} \leq 5 \text{ mm}.$$

13. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$0 < \text{InTL} \leq 4 \text{ mm};$$

where InTL is a distance in parallel with the optical axis between an object-side surface, which face the object side, of the first lens and the image-side surface of the fifth lens.

14. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$0 < \Sigma \text{TP} \leq 3 \text{ mm};$$

where  $\Sigma \text{TP}$  is a sum of central thicknesses of the lenses on the optical axis.

15. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$0 < \text{SGI521}/(\text{TP5} + \text{SGI521}) \leq 0.5;$$

where SGI521 is a displacement in parallel with the optical axis from a point on the image-side surface of the fifth lens, through which the optical axis passes, to the inflection point, which is the closest to the optical axis, on the image-side surface of the fifth lens; and TP5 is a thickness of the fifth lens on the optical axis.

16. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$\text{IN12}/f \leq 0.2;$$

where IN12 is a distance on the optical axis between the first lens and the second lens.

17. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$0.01 \leq f1/(f1+f3+f4) \leq 0.8;$$

where  $f1$  is a focal length of the first lens;  $f3$  is a focal length of the third lens; and  $f4$  is a focal length of the fourth lens.

18. The optical image capturing system of claim 9, wherein the optical image capturing system further satisfies:

$$0 < |f/f1| \leq 2; 0 < |f/f2| \leq 2; 0 < |f/f3| \leq 2; 0 < |f/f4| \leq 2; \text{ and } 0 < |f/f5| \leq 2;$$

where  $f2$  is a focal length of the second length; and  $f5$  is a focal length of the fifth lens.

19. An optical image capturing system, in order along an optical axis from an object side to an image side, comprising:

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a first lens having positive refractive power, and having at least an inflection point on an image-side surface, which faces the image side;

a second lens having refractive power;

a third lens having refractive power, and having at least an inflection point on an image-side surface, which faces the image side, and an object-side surface, which faces the object side, respectively;

a fourth lens having refractive power;

a fifth lens having refractive power, and having at least an inflection point on an image-side surface, which faces the image side, and an object-side surface, which faces the object side, respectively; and

an image plane;

wherein the optical image capturing system consists of the five lenses having refractive power; the fifth lens has an object-side surface, which faces the object side, and an image-side surface, which faces the image side, and both the object-side surface and the image-side surface of the fifth lens are aspheric surfaces;

wherein the optical image capturing system satisfies:

$$1.2 \leq f/\text{HEP} \leq 2.8;$$

$$0.81 \leq |\tan(\text{HAF})| \leq 1.5;$$

$$0.5 \leq \text{HOS}/f \leq 2.5;$$

$$|\text{TDT}| < 1.5\%; \text{ and}$$

$$|\text{ODT}| \leq 2.5\%;$$

where  $f$  is a focal length of the optical image capturing system; HEP is an entrance pupil diameter of the optical image capturing system; HAF is a half of a view angle of the optical image capturing system; HOS is a distance in parallel with the optical axis between an object-side surface, which face the object side, of the first lens and the image plane; TDT is a TV distortion; and ODT is an optical distortion.

20. The optical image capturing system of claim 19, wherein the optical image capturing system further satisfies:

$$0 \text{ mm} < \text{HIF} \leq 5 \text{ mm};$$

where HIF is a distance perpendicular to the optical axis between the inflection points and the optical axis.

21. The optical image capturing system of claim 19, wherein the optical image capturing system further satisfies:

$$0.6 \leq \text{InTL}/\text{HOS} \leq 0.9;$$

where InTL is a distance in parallel with the optical axis between an object-side surface, which faces the object side, of the first lens and the image-side surface of the fifth lens.

22. The optical image capturing system of claim 19, wherein the third lens has at least two inflection points on an object-side surface, which faces the object side, and the fifth lens has at least an inflection point on each surface thereof; and the optical image capturing system further satisfies:

$$0.01 \leq f1/(f1+f3+f4) \leq 0.8 \text{ and } 0.01 \leq f5/(f2+f5) \leq 0.8;$$

where  $f1$  is a focal length of the first lens;  $f2$  is a focal length of the second length;  $f3$  is a focal length of the third lens; and  $f4$  is a focal length of the fourth lens; and  $f5$  is a focal length of the fifth lens.

23. The optical image capturing system of claim 22, wherein the optical image capturing system further satisfies:

$$0.45 < \Sigma \text{TP}/\text{InTL} \leq 0.95;$$

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where  $\Sigma TP$  is a sum of central thicknesses of the lenses on the optical axis; and  $InTL$  is a distance between an object-side surface, which face the object side, of the first lens and the image-side surface of the fifth lens.

24. The optical image capturing system of claim 22, 5  
further comprising an aperture and an image sensor on the image plane, wherein the optical image capturing system further satisfies:

where  $InS$  is a distance in parallel with the optical axis between the aperture and the image plane. 10

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