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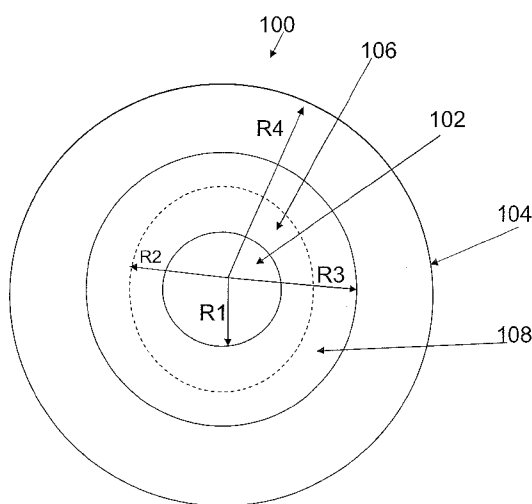


Fig. 1

(57) Abstract: Few mode optical fibers with small delay differences between the propagating modes are disclosed. In one embodiment, an optical fiber includes a glass core and a glass cladding surrounding and in direct contact with the glass core. The glass core may include a radius R_1 from about $8\text{ }\mu\text{m}$ to about $13\text{ }\mu\text{m}$; a graded refractive index profile with an α value between about 1.9 and 2.1 at a wavelength of 1550 nm ; and a maximum relative refractive index $\Delta_{1\text{MAX}}$ from about 0.6% to about 0.95% relative to the glass cladding. The effective area of the LP₀₁ mode at 1550 nm may be between $80\text{ }\mu\text{m}^2$ and $105\text{ }\mu\text{m}^2$ such that the core supports the propagation and transmission of an optical signal with X LP modes at a wavelength of 1550 nm , wherein X is an integer greater than 1 and less than 10. The glass cladding may include a maximum relative refractive index $\Delta_{4\text{MAX}}$ such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}}$. The optical fiber has DGD of less than or equal to about 150 ps/km at a wavelength of 1550 nm .

FEW-MODED OPTICAL FIBERS**BACKGROUND*****Cross-reference to Related Application***

[0001] This application claims the benefit of priority of U.S. Application Serial No. 13/164,971 filed on June 21, 2011 the contents of which are relied upon and incorporated herein by reference in its entirety.

Field

[0002] The present specification generally relates to optical fibers and, more specifically, to few-moded optical fibers with low loss and small differential group delays.

[0003] Technical Background

Few-moded fibers (10 or fewer LP modes at 1550 nm) have been designed to transmit optical signals in two or more LP modes. Spatial mode converters can be used to multiplex the optical signals into the fiber and the signals can be decomposed at the receiver using electronic dispersion compensation. The few-moded fibers previously proposed for WDM communications systems have step index cores in which the diameter is increased relative to the single mode fibers in order to support additional modes. One problem with these designs is that there are large delay differences between the fundamental mode and the higher order modes (HOMs). If there is even a small amount of mode mixing in the fiber, the pulses arriving at the detector are degraded due to multipath interference, and this can lead to unsurmountable bit error rate penalties. Another problem is that increasing the core diameter leads to high microbending losses, and although the higher order modes (HOMs) can be designed to have theoretical cutoffs above the 1550 window, these modes are leaky and are not suitable for long transmission spans. A third problem is that the large effective area of the step index fiber is achieved by reducing the refractive index of the core, and this reduces the numerical aperture (NA) of the fiber. This smaller NA can increase both the coupling losses and alignment sensitivity between the spatial mode converter or optical transceiver and the fiber.

[0004] Accordingly, a need exists for alternative designs for few-moded optical fibers with low loss, small differential group delays (DGD) and large numerical aperture.

SUMMARY

[0005] According to one embodiment an optical fiber may include a glass core and a glass cladding surrounding and in direct contact with the glass core. The glass core may have a radius R_1 from about 8 μm to about 13 μm and a graded refractive index profile with an alpha value greater than or equal to about 1.8 and less than about 2.2 at a wavelength of 1550 nm. The maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core may be from about 0.6% to about 0.95% relative to the glass cladding. An effective area of the LP01 mode may be greater than 80 μm^2 , for example between 80 μm^2 and 110 μm^2 , or between 85 μm^2 and 105 μm^2 , or between 85 μm^2 and 100 μm^2 . The numerical aperture of the fiber is greater than 0.15 and less than 0.22, for example between 0.15 and 0.20, between 0.15 and 0.17 or between 0.18 and 0.20. The glass core may support the propagation and transmission of an optical signal with X LP modes at a wavelength of 1550 nm, wherein X is an integer greater than 1 and less than 10, for example X = 9, X = 6, X = 4 or X = 2. The glass cladding may have a maximum relative refractive index $\Delta_{4\text{MAX}}$ such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}}$, wherein the optical fiber has a maximum differential group delay (DGD) less than or equal to about 150 ps/km, preferably less than 100 ps/km, more preferably less than 50 ps/nm and even more preferably less than 10 ps/nm at a wavelength of 1550 nm. The attenuation of the LP01 mode is less than 0.20 dB/km, preferably less than 0.19 dB/km.

[0006] In another embodiment, an optical fiber includes a glass core and a glass cladding surrounding and in direct contact with the glass core. The glass core may have a radius R_c from about 10 μm to about 13 μm and a graded refractive index profile with an alpha value greater than or equal to about 1.8 and less than or equal to about 2.2 at a wavelength of 1550 nm. A maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core may be from about 0.7% to about 0.95% relative to an outer cladding layer of the glass cladding. An effective area of the LP01 mode may be between 80 and 120 μm^2 , for example between 80 and 110 μm^2 , or between 80 and 105 μm^2 , or between 85 and 100 μm^2 . The glass core may support the propagation and transmission of an optical signal with X number of LP modes at a wavelength of 1550 nm, wherein X is an integer greater than 1 and less than 10, for example X = 9, X = 6, X = 4 or X

= 2. The numerical aperture of the fiber is greater than 0.15 and less than 0.22, for example between 0.15 and 0.20 or between 0.18 and 0.20. The glass cladding includes a low index ring layer and may include an optional inner cladding layer surrounding and in direct contact with the glass core. The inner cladding layer may have a relative refractive index Δ_2 such that $\Delta_{1MAX} \geq \Delta_2$. A low index ring may surround and directly contact the inner cladding layer, or alternatively may surround and directly contact the core. The outer cladding layer may surround and directly contact the low index ring. The low index ring has a minimum relative refractive index Δ_{3MIN} relative to the outer cladding layer and the outer cladding layer has a maximum relative refractive index Δ_{4MAX} relative to pure silica glass such that $\Delta_{1MAX} > \Delta_{4MAX} > \Delta_{3MIN}$. The optical fiber may have a maximum DGD less than or equal to about 150 ps/km, preferably less than 100 ps/km, more preferably less than 50 ps/nm, more preferably less than 20 ps/nm, and even more preferably less than 10 ps/nm at a wavelength of 1550 nm. The attenuation of the LP01 mode is less than 0.20 dB/km, preferably less than 0.19 dB/km.

[0007] In yet another embodiment an optical fiber includes a glass core and a glass cladding surrounding and in direct contact with the glass core. The glass core may have a radius R_1 from about 8 μm to about 10 μm and a graded refractive index profile with an alpha value greater than or equal to about 1.8 and less than or equal to about 2.2 at a wavelength of 1550 nm. A maximum relative refractive index Δ_{1MAX} of the core may be from about 0.6% to about 0.7% relative to an outer cladding layer of the glass cladding. An effective area of the LP01 mode may be between 80 and 120 μm^2 , for example between 80 and 110 μm^2 , or between 85 and 105 μm^2 , or between 85 and 100 μm^2 . The glass core may support the propagation and transmission of an optical signal with X LP modes at a wavelength of 1550 nm, wherein X = 2. The numerical aperture of the fiber is greater than 0.15 and less than 0.20, and preferably between 0.15 and 0.17. The glass cladding may include an optional inner cladding layer surrounding and in direct contact with the glass core. The inner cladding layer may have a relative refractive index Δ_2 such that $\Delta_{1MAX} > \Delta_2$. A low index ring may surround and directly contact the inner cladding layer, or alternatively may surround and directly contact the core. The outer cladding layer may surround and directly contact the low index ring. The low index ring has a minimum relative refractive index Δ_{3MIN} relative to the outer cladding layer and the outer cladding layer has a maximum relative refractive index Δ_{4MAX} relative to pure silica glass

such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}} > \Delta_{3\text{MIN}}$. The optical fiber may have a maximum DGD less than or equal to about 150 ps/km, preferably less than 100 ps/km, more preferably less than 50 ps/nm and even more preferably less than 10 ps/nm at a wavelength of 1550 nm. The attenuation of the LP01 mode is less than 0.20 dB/km, preferably less than 0.19 dB/km.

[0008] Additional features and advantages of the invention will be set forth in the detailed description which follows, and in part will be readily apparent to those skilled in the art from that description or recognized by practicing the embodiments described herein, including the detailed description which follows, the claims, as well as the appended drawings.

[0009] It is to be understood that both the foregoing general description and the following detailed description describe various embodiments and are intended to provide an overview or framework for understanding the nature and character of the claimed subject matter. The accompanying drawings are included to provide a further understanding of the various embodiments, and are incorporated into and constitute a part of this specification. The drawings illustrate the various embodiments described herein, and together with the description serve to explain the principles and operations of the claimed subject matter.

BRIEF DESCRIPTION OF THE DRAWINGS;

[0010] FIG. 1 schematically depicts a cross section of an optical fiber according to one or more embodiments described herein

[0011] FIGS. 2A, 2B and 2C schematically depict relative refractive index profiles of optical fibers with low index rings according to one or more embodiments shown and described herein;

[0012] FIG. 3 depicts the refractive index profile of one embodiment of the invention and the derivative of the normalized refractive index profile with respect to the normalized radius;

[0013] FIG. 4 depicts minimum relative delays vs. Mode Group for one or more embodiments described herein;

[0014] FIG. 5 depicts relative delays of the LP11 mode as a function of the core alpha for one or more embodiments described herein.

DETAILED DESCRIPTION

[0015] Reference will now be made in detail to embodiments of optical fibers for use as long haul transmission fibers, examples of which are illustrated in the accompanying drawings. Whenever possible, the same reference numerals will be used throughout the drawings to refer to the same or like parts. One embodiment of an optical fiber for use as a long haul transmission fiber is schematically depicted in cross section in **FIG. 1**. The optical fiber generally has a glass core surrounded by a glass cladding. The glass core generally has a radius R_1 from about 8 μm to about 13 μm (for example, between 9 μm and 12.5 μm) and a maximum relative refractive index $\Delta_{1\text{MAX}}$ from about 0.6% to about 0.95% relative to the glass cladding. An effective area of the LP01 mode is between about 80 and 120 μm^2 , for example between 80 and 110 μm^2 , between 85 and 105 μm^2 or between 85 μm^2 and 100 μm^2 . The glass core is generally able to support the transmission and propagation of an optical signal with X LP modes at a wavelength of 1550 nm, wherein X is an integer greater than 1 and less than 10, for example X = 9, X = 6, X = 4 or X = 2. The glass cladding generally comprises a maximum relative refractive index $\Delta_{4\text{MAX}}$ such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}}$. The optical fiber may have a maximum DGD less than or equal to about 150 ps/km, for example less than 100 ps/km, preferably less than 50 ps/nm and even more preferably less than 10 ps/nm at a wavelength of 1550 nm.. The numerical aperture NA of the fiber **100** is greater than 0.15 and less than 0.22, for example between 0.15 and 0.20, between 0.15 and 0.17 or between 0.18 and 0.20. The attenuation of the LP01 mode is less than 0.20 dB/km, preferably less than 0.19 dB/km. The optical fibers and the properties of the optical fibers will be described in more detail herein with specific reference to the appended drawings.

[0016] The following terminology will be used herein to described the optical fibers:

[0017] The term “refractive index profile,” as used herein, is the relationship between the refractive index or the relative refractive index and the radius of the fiber.

[0018] The term “relative refractive index,” as used herein, is defined as:

$$\Delta(r) = 100 \times [n(r)^2 - n_{\text{REF}}^2] / 2n(r)^2,$$

where $n(r)$ is the refractive index at radius r , unless otherwise specified. The relative refractive index is defined at 1550 nm unless otherwise specified. In one aspect, the reference index n_{REF} is silica glass. In another aspect, n_{REF} is the maximum refractive index of the cladding. In another aspect, n_{REF} is the average refractive index of the cladding. As used herein, the relative refractive index is represented by Δ and its values are given in units of “%”, unless otherwise specified. In cases where the refractive index of a region is less than the reference index n_{REF} , the relative index percent is negative and is referred to as having a depressed region or depressed-index, and the minimum relative refractive index is calculated at the point at which the relative index is most negative unless otherwise specified. In cases where the refractive index of a region is greater than the reference index n_{REF} , the relative index percent is positive and the region can be said to be raised or to have a positive index.

[0019] The term “updopant,” as used herein, refers to a dopant which raises the refractive index of glass relative to pure, undoped SiO_2 . The term “downdopant,” as used herein, is a dopant which has a propensity to lower the refractive index of glass relative to pure, undoped SiO_2 . An updopant may be present in a region of an optical fiber having a negative relative refractive index when accompanied by one or more other dopants which are not updopants. Likewise, one or more other dopants which are not updopants may be present in a region of an optical fiber having a positive relative refractive index. A downdopant may be present in a region of an optical fiber having a positive relative refractive index when accompanied by one or more other dopants which are not downdopants. Likewise, one or more other dopants which are not downdopants may be present in a region of an optical fiber having a negative relative refractive index.

[0020] As used herein, the “effective area” of an optical fiber is the area of the optical fiber in which light is propagated and is defined as:

$$A_{\text{eff}} = 2\pi \frac{(\int_0^\infty E^2 r dr)^2}{\int_0^\infty E^4 r dr},$$

where E is the electric field associated with light propagated in the fiber and r is the radius of the fiber. The effective area is determined at the specified mode (e.g., LP01), at a wavelength of 1550 nm, unless otherwise specified.

[0021] The normalized wave number, or V-number of a fiber is defined as $V = k \cdot R_1 \cdot \text{NA}$, where k is the free space wave number, $2\pi/\lambda$, λ is the wavelength, R_1 is the radius of the core, and NA is the numerical aperture of the fiber. The NA is given by $(n_{\text{core}}^2 - n_{\text{clad}}^2)^{1/2} = n_{\text{core}} [2\Delta_{1\text{MAX}} / (1 - 2\Delta_{1\text{MAX}})]^{1/2}$, where n_{core} is the maximum refractive indices of the core, n_{clad} is the refractive index of the cladding and $\Delta_{1\text{MAX}}$ is the maximum relative refractive index of the core with respect to the cladding.

[0022] Chromatic dispersion or dispersion of a fiber is the sum of the material dispersion, the waveguide dispersion, and the inter-modal dispersion.

[0023] Unless otherwise specified herein, the above-referenced properties of the optical fiber are at 1550 nm.

[0024] The cutoff wavelength of a mode is the minimum wavelength beyond which a mode ceases to propagate in the optical fiber. The cutoff wavelength of a single mode fiber is the minimum wavelength at which an optical fiber will support only one propagating mode. The cutoff wavelength of a single mode fiber corresponds to the highest cutoff wavelength among the higher order modes. Typically the highest cutoff wavelength of a single mode fiber corresponds to the cutoff wavelength of the LP₁₁ mode. If the operative wavelength is below the cutoff wavelength, multimode operation may take place and the introduction of additional sources of dispersion may limit a fiber's information carrying capacity. A mathematical definition can be found in Single Mode Fiber Optics, Jeunhomme, pp. 39-44, Marcel Dekker, New York, 1990 wherein the theoretical fiber cutoff is described as the wavelength at which the mode propagation constant becomes equal to the plane wave propagation constant in the outer cladding. This theoretical wavelength is appropriate for an infinitely long, perfectly straight fiber that has no diameter variations.

[0025] As used herein, the term "few moded fiber" refers to a fiber supporting the propagation of more modes than a single mode fiber but fewer modes than a normal multimode fiber. In particular, the term "few moded fiber", as used herein means that the fiber supports 2 to 9 LP modes in a fiber length longer than 22 meters as defined by the cable cutoff measurement. The number of propagating modes and their characteristics in a cylindrically symmetric optical fiber with an arbitrary refractive index profile is obtained by solving the scalar wave equation [see for example T.A. Lenahan, "Calculation of modes in an optical fiber using a finite element

method and EISPACK,” Bell Syst. Tech. J., vol. 62, no. 1, p. 2663, Feb. 1983]. Light travelling in an optical fiber or other dielectric waveguide forms hybrid-type modes, which are usually referred to as LP (linear polarization) modes. The LP_{0p} modes have two polarization degrees of freedom and are two-fold degenerate, the LP_{1p} modes are four-fold degenerate and the LP_{mp} modes with $m > 1$ are four-fold degenerate. We do not count these degeneracies when we designate the number of LP modes propagating in the fiber. For example, an optical fiber in which only the LP₀₁ mode propagates is a single-mode fiber, even though the LP₀₁ mode has two possible polarizations. A few-moded optical fiber in which the LP₀₁ and LP₁₁ modes propagate supports three spatial modes since the LP₁₁ mode is two-fold degenerate, and each mode also has two possible polarizations, giving a total of 6 modes. We designate this fiber as having two LP modes, and by this we mean that it supports the propagation of all of the LP₀₁ and LP₁₁ modes. Similarly, a few-modes fiber designated as having 4 LP modes supports the propagation of all of the LP₀₁, LP₁₁, LP₀₂ and LP₂₁ modes, and a few-modes fiber designated as having 6 LP modes supports the propagation of all of the LP₀₁, LP₁₁, LP₀₂, LP₂₁, LP₁₂ and LP₃₁ modes.

[0026] The term graded index, “ α -profile” or “alpha profile,” as used herein, refers to a relative refractive index profile, expressed in terms of Δ which is in units of “%”, where r is the radius and which follows the equation,

$$\Delta(r) = \Delta_0 \left[1 - \left(\frac{r}{R_1} \right)^\alpha \right],$$

where Δ_0 is the relative refractive index extrapolated to $r = 0$, R_1 is the radius of the core, and α is an exponent which is a real number. For a step index profile, the alpha value is greater than or equal to 10. For a graded index profile, the alpha value is less than 10, for example less than 4, less than 3, less than 2.2, or less than or equal to 2.1. The term “parabolic,” as used herein, includes substantially parabolically shaped refractive index profiles which may vary slightly from an α value of 2.0 at one or more points in the core, as well as profiles with minor variations and/or a centerline dip. In most cases, accurate parameters of an alpha profile are obtained by numerically fitting a measured relative refractive index profile from $0.05 R_1 \leq r \leq 0.95 R_1$. In ideal graded index fibers with no imperfections such as dips or

spikes at the centerline, $\Delta_0 = \Delta_{1MAX}$, but in other cases, the value from Δ_0 obtained from the numerical fit from $0.05 R_1 \leq r \leq 0.95 R_1$ may be greater or less than Δ_{1MAX} .

[0027] Referring to **FIG. 1**, a cross section of the glass portion of an optical fiber **100** is schematically depicted according to one or more embodiments described herein. The optical fiber **100** generally comprises a core **102** surrounded by and in direct contact with a cladding **104**. In the embodiments shown and described herein, the core **102** and the cladding **104** generally comprise silica, specifically silica glass. The cross section of the optical fiber **100** may be generally circular-symmetric with respect to the center of the core **102** and the core **102** may have a radius R_1 . In the embodiments described herein, the radius R_1 of the core **102** is greater than or equal to about 8 μm and less than or equal to about 13 μm (for example, 8 μm , 8.5 μm ; 9 μm ; 9.5 μm ; 10 μm ; 10.5 μm ; 11 μm ; 11.5 μm ; 12 μm ; 12.5 μm , or any number therebetween). In some embodiments described herein, the radius R_4 (i.e., the radius of the glass portion of the optical fiber **100**) is about 125 μm . However, it should be understood that the dimensions of the cladding **104** may be adjusted such that the radius R_4 may be greater than 125 μm or less than 125 μm .

[0028] In the embodiments described herein, the core **102** has a maximum relative refractive index Δ_{1MAX} relative to the cladding **104** and the cladding **104** has a maximum relative refractive index percent Δ_{4MAX} relative to pure silica glass, and $\Delta_{1MAX} > \Delta_{4MAX}$.

[0029] In the embodiments shown and described herein, the core **102** comprises pure silica glass (SiO_2) or silica glass with one or more dopants which increases the index of refraction of the glass core relative to pure, undoped silica glass. Suitable dopants for increasing the index of refraction of the core include, without limitation, GeO_2 , Al_2O_3 , P_2O_5 , TiO_2 , ZrO_2 , Nb_2O_5 , Ta_2O_5 , and/or combinations thereof. In the embodiments described herein, the core **102** contains a sufficient amount of dopant such that the maximum relative refractive index Δ_{1MAX} of the core **102** is from about 0.6% to about 0.95%, more preferably from about 0.6% to about 0.8%, for example from about 0.6% to about 0.7%, or from about 0.7% to about 0.8%, or from about 0.7 % to about 0.9%.

[0030] In some embodiments, the core **102** may have a graded refractive index with an alpha profile with an alpha value greater than or equal to 1 and less than 10, preferably greater than or equal to about 1.8 and less than or equal to about 2.2, more preferably greater than or equal

to about 1.9 and less than or equal to about 2.1 or less than or equal to 2.05, at a wavelength of 1550 nm, as depicted in **FIGs. 2A, 2B and 2C**.

[0031] In the embodiment of the optical fiber **100** depicted in **FIG. 1**, the cladding **104** may comprise pure silica glass (SiO_2), silica glass with one or more dopants which increase the index of refraction (e.g., GeO_2 , Al_2O_3 , P_2O_5 , TiO_2 , ZrO_2 , Nb_2O_5 and/or Ta_2O_5), such as when the cladding **104** is “up-doped,” or silica glass with a dopant which decreases the index of refraction, such as fluorine, such as when the inner cladding is “down-doped”, so long as the maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core **102** is greater than the maximum relative refractive index $\Delta_{4\text{MAX}}$ of the cladding **104**. For example, in one embodiment, the cladding **104** is pure silica glass. In yet another embodiment, the inner cladding may comprise silica glass up-doped with Cl, GeO_2 , TiO_2 , or a similar up-dopant.

[0032] More specifically, Referring now to **FIGS. 1 and 2A-2C** the optical fiber **100** generally comprises a core **102** with a graded refractive index profile and a cladding **104** that comprises at least a low index ring **108** and an outer cladding layer **110**. The cladding **104** may also optionally include an inner cladding layer **106**, as depicted schematically in **FIG. 1**. The low index ring **108** may be spaced apart from the core **102** by the inner cladding layer **106**, as is schematically illustrated in **FIGS. 1 and 2A**. Alternatively, the low index ring **108** may surround and directly contact the core portion, as is schematically depicted in **FIG. 2B**. In some embodiments, the inner cladding layer **106** is an extension of the graded index core, as is schematically depicted in **FIG. 2C**.

[0033] The low index ring **108** is an annular region of silica-based glass which surrounds the core **102**. The low index ring **108** assists in further improving the bend performance of the optical fiber **100**, as will be described in more detail herein. In embodiments where the cladding **104** comprises an inner cladding layer **106**, the inner cladding layer **106** is positioned between the core **102** and the low index ring **108** such that the low index ring **108** is spaced apart from the core **102** (i.e., the low index ring **108** is not in direct contact with the core **102**). The width of inner cladding layer, $W_2 = R_2 - R_1$, is greater than $0.5\text{ }\mu\text{m}$ and less than $4.0\text{ }\mu\text{m}$, preferably greater than $0.5\text{ }\mu\text{m}$ and less than $2.0\text{ }\mu\text{m}$, and more preferably greater than $0.5\text{ }\mu\text{m}$ and less than $1.5\text{ }\mu\text{m}$. In embodiments where the low index ring **108** is spaced apart from the core **102** with the inner cladding layer **106** and the core has a graded refractive index

with an alpha profile, the alpha value of the core may be greater than or equal to about 1.8 and less than about 2.2 at a wavelength of 1550 nm, more preferably greater than or equal to about 1.9 and less than or equal to about 2.1 at a wavelength of 1550 nm, even more preferably greater than or equal to about 1.9 and less than or equal to about 2.05 at a wavelength of 1550 nm.

[0034] However, in embodiments where the low index ring **108** surrounds and is in direct contact with the core **102**, the width of the inner cladding layer is very small but not zero due to the transition between the two regions (i.e., $0 \mu\text{m} \leq R_2 - R_1 < 0.5 \mu\text{m}$, with radial width $W_2 < 0.5 \mu\text{m}$). In embodiments where the low index ring **108** surrounds and is in direct contact with the core **102** and the core has a graded refractive index with an alpha profile, the alpha value of the core may be greater than or equal to about 1.8 and less than about 2.2 at a wavelength of 1550 nm, more preferably greater than or equal to about 1.9 and less than or equal to about 2.1 at a wavelength of 1550 nm, even more preferably greater than or equal to about 1.9 and less than or equal to about 2.05 at a wavelength of 1550 nm.

[0035] In the embodiments described herein, R_2 is defined as the radius at which the derivative of the normalized refractive index profile with respect to the normalized radius, $d(\Delta/\Delta_{1\text{MAX}})/d(r/R_1)$, has a local minimum, as shown in **FIG. 3**.

[0036] In the embodiments described herein, the low index ring **108** comprises $\Delta_3(r)$ with minimum relative refractive index $\Delta_{3\text{MIN}}$ and extends from the radius R_2 to the radius R_3 , wherein R_3 is the radius at which $\Delta_3(r)$ first reaches a value of greater than -0.05%, going radially outwardly from the radius at which $\Delta_3(r) = \Delta_{3\text{MIN}}$. The low index ring **108** has a radial width $W_3 = R_3 - R_2$. In some embodiments the radial width W_3 of the low index ring **108** is from about 2 μm to about 10 μm , for example from about 2 μm to about 8 μm or from about 3 μm to about 7 μm .

[0037] The low index ring **108** generally comprises silica glass down-doped to reduce the index of refraction of the low index ring **108** with respect to pure silica glass. For example, the low index ring **108** may be down doped with fluorine, boron and/or combinations thereof in order to decrease the index of refraction of the low index ring **108** with respect to pure silica glass. In the embodiments described herein, the low index ring is formed with a sufficient amount of down-dopant such that the minimum relative refractive index percent ($\Delta_{3\text{MIN}}$) of the

low index ring **108** is from about -0.1 % to about -0.7%, more preferably from about -0.25% to about -0.6%, even more preferably about -0.3% to about -0.55% relative to pure silica glass, for example $-0.5\% \leq \Delta_{3\text{MIN}} \leq -0.3\%$.

[0038] The inner cladding **106** may comprise pure silica glass (SiO_2), silica glass with one or more dopants which increase the index of refraction (e.g., GeO_2 , Al_2O_3 , P_2O_5 , TiO_2 , ZrO_2 , Nb_2O_5 and/or Ta_2O_5), such as when the inner cladding **106** is “up-doped,” or silica glass with a dopant which decreases the index of refraction, such as fluorine, such as when the inner cladding is “down-doped.” In the embodiments of the optical fiber **100** described herein, the relative refractive index Δ_2 of the inner cladding **106** is less than the maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core **102**, as shown in **FIG. 2A-2C**. In some preferred embodiments, the relative refractive index Δ_2 of the inner cladding may be from about -0.6% to about 0.1%. In other preferred embodiments, the relative refractive index Δ_2 of the inner cladding may be from about -0.5% to about 0.0%. The inner cladding **106** is also characterized by the maximum and minimum relative refractive index values $\Delta_{2\text{MAX}}$, $\Delta_{1\text{MIN}}$ respectively, where $\Delta_{2\text{MAX}} > \Delta_{2\text{MIN}}$. In at least some embodiments of the optical fiber **100**, $\Delta_{2\text{MIN}} > -0.6\%$; for example $\Delta_{2\text{MIN}} > -0.5\%$; or $\Delta_{2\text{MIN}} \geq -0.4\%$. In at least some embodiments of the optical fiber **100**, $\Delta_{2\text{MAX}} < 0.1\%$; for example $\Delta_{2\text{MAX}} \leq -0.0\%$. In at least some embodiments of the optical fiber **100**, $\Delta_{2\text{MIN}} > -0.6\%$; and $\Delta_{2\text{MAX}} < 0.1\%$; for example $\Delta_{2\text{MAX}} \leq -0.0\%$, and $\Delta_{2\text{MAX}} > \Delta_{2\text{MIN}}$.

[0039] The outer cladding layer **110** surrounds and is in direct contact with the low index ring **108**. The outer cladding **110** generally extends from the radius R_3 to the radius R_4 such that the outer cladding layer has a radial width $W_4 = R_4 - R_3$. The outer cladding layer **110** generally has a relative refractive index Δ_4 relative to pure silica glass which is greater than the minimum relative refractive index $\Delta_{3\text{MIN}}$ of the low index ring **108** and less than the maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core **102**. In some embodiments, $\Delta_4 \geq \Delta_{2\text{MAX}}$; in other embodiments, $\Delta_4 \leq \Delta_{2\text{MAX}}$. Accordingly, the outer cladding **108** may comprise pure silica glass (SiO_2), silica glass with one or more dopants which increase the index of refraction (e.g., GeO_2 , Al_2O_3 , P_2O_5 , TiO_2 , ZrO_2 , Nb_2O_5 and/or Ta_2O_5), such as when the outer cladding **108** is “up-doped,” or silica glass with a dopant which decreases the index of refraction, such as fluorine, such as when the outer cladding is “down-doped,” so long as the relative refractive index Δ_4 of the outer cladding **108** is less than the maximum relative refractive index $\Delta_{1\text{MAX}}$ of

the core **102** and greater than the minimum relative refractive index $\Delta_{3\text{MIN}}$ of the low index ring **108**. For example, the outer cladding layer **110** may be up-doped such that the relative refractive index Δ_4 of the outer cladding layer **110** is from about 0.02% to about 0.2% relative to pure silica glass.

[0040] Referring to specifically to **FIG. 2A**, the refractive index profile of one specific embodiment of an optical fiber is graphically depicted. In this embodiment the core of the fiber has a graded refractive index profile with a maximum relative refractive index $\Delta_{1\text{MAX}}$. The cladding of the optical fiber is formed with an inner cladding layer having a maximum relative refractive index $\Delta_{2\text{MAX}}$ which is less than the maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core. A low index ring **108** is positioned directly adjacent to and in contact with the inner cladding layer **106**. The low index ring has **108** a minimum relative refractive $\Delta_{3\text{MIN}}$ which is less than or equal to $\Delta_{2\text{MAX}}$ and less than $\Delta_{1\text{MAX}}$. In some preferred embodiments, outer cladding layer **110** surrounds and is in direct contact with the low index ring and has a relative refractive index Δ_4 which is greater than $\Delta_{2\text{MAX}}$ and greater than $\Delta_{3\text{MIN}}$ and less than $\Delta_{1\text{MAX}}$. Accordingly, $\Delta_{1\text{MAX}} > \Delta_4 > \Delta_{2\text{MAX}} > \Delta_{3\text{MIN}}$ in this embodiment. However, it should be understood that other embodiments are possible. For example, Δ_4 may be equal to $\Delta_{2\text{MAX}}$. Alternatively, $\Delta_{2\text{MAX}}$ may be greater than Δ_4 .

[0041] In the embodiments of the optical fibers described herein, the combination of the core radius R_1 and the maximum relative refractive index $\Delta_{1\text{MAX}}$ of the core increase the theoretical cutoff wavelength of the higher order modes of an optical signal propagating in the optical fiber. Increasing the theoretical cutoff wavelength of these higher order modes has the effect of increasing the number of modes which can propagate in the core of the optical fiber and, as a result, the optical fiber becomes few-moded (i.e., the optical fiber supports the propagation and transmission of more modes than a single-mode fiber and fewer modes than a multi-moded fiber, for example the fiber that propagates less than 10 LP modes (e.g., 2-9 LP modes). For example, in the embodiments described herein, the theoretical cutoff wavelength of the LP11 mode of an optical signal having is greater than or equal to 2000 nm, preferably greater than 2200 nm, for example 2200 nm to 4000 nm. Similarly, the theoretical cutoff wavelength of the LP02 mode is greater than or equal to 1200 nm, preferably greater than 1400 nm, for example between 1400 nm and 3000 nm. The theoretical cutoff wavelength of the LP12 mode

of an optical signal having a wavelength of 1550 nm is greater than or equal to 1000 nm, preferably greater than 1100 nm, for example between 1100 nm and 2000 nm.

[0042] In the embodiments described herein, forming the optical fibers with a core radius in the range of 8 μm to 13 μm (for example, 8 μm , 8.5 μm ; 9 μm ; 9.5 μm ; 10 μm ; 10.5 μm ; 11 μm ; 11.5 μm ; 12 μm ; 12.5 μm , 13 μm , or any number therebetween) and a relative refractive index Δ_{IMAX} greater than or equal to about 0.6% and less than or equal to about 0.95% produces an optical fiber which supports X LP modes, where X is an integer. In the embodiments described herein, X is greater than 1 and less than 10. For example, in embodiments where the core of the optical fiber has a graded refractive index profile with an alpha value of about 2, Δ_{IMAX} from 0.6 to 0.95%, and a radius from about 9 μm to 13 μm , X may be an integer from 2 to 9, for example X = 2, X = 4, X = 6 or X = 9.

[0043] In addition to increasing the number of higher order modes which can propagate in the core of the optical fiber, optical fibers formed with the structure and properties described above and shown in **FIGS. 1, 2A and 2B** generally have an increased numerical aperture (NA) and, as such, the optical fibers generally have lower coupling losses to the optical source. Specifically, the combination of a core with a radius from about 8 μm to about 13 μm and a relative refractive index Δ_{IMAX} greater than or equal to about 0.6% and less than or equal to about 0.95% produces an NA greater than about 0.15, preferably greater than about 0.16 and even more preferably between 0.16 and 0.20.

[0044] The optical fibers disclosed herein also have a chromatic dispersion value greater than or equal to about 18 ps/nm/km and less than or equal to about 23 ps/nm/km at 1550 nm. At least some of the exemplary embodiments of the optical fiber **100** propagate at least 2 but fewer than 10 LP modes (e.g., 2, 4, or 6 LP modes), have numerical apertures between 0.15 and 0.22; a DGD less than or equal to about 150 ps/km; LP01 mode dispersion between 18 and 22 ps/nm/km (for example, 20 to 21 ps/nm/km); and attenuation (loss of LP01 mode) at 1550nm below 0.2 dB/km (for example, 0.16 dB/km to 0.2 dB/km, or 0.18 dB/km to 0.19 dB/km..

[0045] Referring now to **FIG. 4**, the DGD between the fundamental and higher order modes may be reduced by forming the optical fiber with a core having a graded refractive index profile with an alpha value less than 10, as described above. In general, lowering the alpha

value from a step index profile alpha value decreases the time delays between modes propagating in the optical fiber. The mode delays in an optical fiber with an arbitrary refractive index profile may be calculated using the method T.A. Lenahan, "Calculation of modes in an optical fiber using a finite element method and EISPACK," Bell Syst. Tech. J., vol. 62, no. 1, p. 2663, Feb. 1983, which is incorporated herein by reference. Equation 47 of this reference is used to calculate the modal delays; however note that the term $dk_{\text{clad}}/d\omega^2$ must be replaced with $dk_{\text{clad}}^2/d\omega^2$, where $k_{\text{clad}} = 2\pi n_{\text{clad}}/\lambda$ and $\omega = 2\pi/\lambda$. The modal delays are typically normalized per unit length and given in units of ns/km. The inventor has discovered that reducing the alpha value from about 10 to about 2 reduces the DGD by more than two orders of magnitude. Specifically, it has been determined that DGD between higher order modes at 1550 nm can be minimized when the core of the optical fiber has a graded refractive index profile with an alpha value between 1.9 and 2.05. **FIG. 4** illustrates the differential group delays of the LP modes (with respect to the LP01 mode) of one exemplary fiber embodiment (Example 1). The magnitudes of the differential group delays are all less than 50 ps/km, which means that signals launched into the different mode groups travel at approximately the same velocities.

[0046] Referring now to **FIG. 5**, the graded index profile of each embodiment also enables the the differential group delays of the LP modes to be tuned by a predetermined amount by varying the alpha of the core. Specifically, **FIG. 5** illustrates that an alpha value of 1.98 yields a differential group delay between the LP01 and LP11 modes of less than 1 ps/km, so the signals launched into these mode groups travel at almost exactly the same velocities. Decreasing the alpha of the core to a value less than 1.98 to decreases the relative delay of the LP11 mode, which means that it travels faster than the LP01 mode. Increasing the alpha of the core to a value greater than 1.98 to increases the relative delay of the LP11 mode, which means that it travels slower than the LP01 mode.

[0047] According to some embodiments the optical fibers **100** propagate fewer than 10 LP modes (for example 2, 4, 6 or 9 LP modes) and have one or more of the following advantageous features: low attenuation (<0.2 dB/km), low microbending losses (wire mesh drum < 0.8 dB for the LP01 mode), low dispersion differences between the LP01 mode and higher order modes HOMs (magnitude less than 1 ps/nm/km), and low differential group delays (< 150 ps/km). A few-moded optical fiber **100** that propagates between 2 and 6 LP

modes at 1550 nm with low attenuation and small differential group delays may be advantageously used for spatial-division multiplexing transmission systems.

Examples

[0048] The invention will be further clarified by the following examples.

[0049] A plurality of optical fibers were mathematically modeled to determine the effect of variations of α , Δ_{MAX} and core radius R_1 on the effective area of LP01 mode, DGD, fiber attenuation at 1550 nm (for the LP01 mode), and the cut off wavelengths and dispersion at 1550 nm for the different modes. **Table 1** contains data for the optical fibers Examples 1-4 with graded refractive index profiles. Specifically, **Table 1** contains data for Examples 1-4 which were modeled with cores having graded refractive index profiles with α values of between 1.9 and 2.1. The numerical apertures NA of the fiber cores **102** of the optical fibers Examples 1-4 are between 0.18 and 0.205. As shown in **Table 1**, Examples 1-4 each support the propagation and transmission of at least 4 LP modes (example 1 and 2 fibers support 6 LP modes) and have effective areas between $85 \mu\text{m}^2$ and $110 \mu\text{m}^2$, for example between $85 \mu\text{m}^2$ to $100 \mu\text{m}^2$. Each of these exemplary fibers has low LP01 mode attenuation below 0.2 dB/km at 1550 nm. Each of these exemplary fibers has small differential group delays (less than 50 ps/nm). For example, **FIG. 4** illustrates differential mode delays of the LP modes with respect to LP01 mode for the optical fiber of Example 1. **FIG. 5** depicts differential mode delays of the LP11 mode as a function of core delta for a fiber that similar to that of Example 4 (all of the parameters for this exemplary fiber were the same as that of Example 4, except for α , which was changed to observe the impact of such change on the differential mode delays. **FIG. 5** illustrates that decreasing the α of the core to a value less than 1.98 to decreases the relative delay of the LP11 mode, which means that it travels faster than the LP01 mode. Increasing the α of the core to a value greater than 1.98 to increases the relative delay of the LP11 mode, which means that it travels slower than the LP01 mode.

Table 1

	Example 1	Example 2	Example 3	Example 4
Delta 1MAX (%) (Δ_{1MAX})	0.893	0.907	0.779	0.777
R1 (microns)	12.43	12.34	10.27	10.27
Alpha	1.993	1.994	1.988	1.983
R2 (microns)	13.41	13.54	11.18	10.90
W2 (microns)	0.98	1.20	0.91	0.63
Delta3MIN (%)	-0.4	-0.5	-0.4	-0.32
R3 (microns)	17	17	15	15.5
W3 (microns)	3.59	3.47	3.82	4.60
LP Modes at 1550nm	6	6	4	4
LP01 Attn 1550 (dB/km)	0.186	0.186	0.186	0.186
LP01 Aeff (sq. microns)	98	97.3	87.7	87.9
NA	0.195	0.196	0.182	0.181
LP01 Cutoff (microns)	> 5	> 5	> 5	> 5
LP11 Cutoff (microns)	3.882	3.822	2.924	2.922
LP02 Cutoff (microns)	2.543	2.511	1.928	1.924
LP21 Cutoff (microns)	2.515	2.492	1.919	1.915
LP12 Cutoff (microns)	1.886	1.870	<1.5	<1.5
LP31 Cutoff (microns)	1.881	1.866	<1.5	<1.5
LP01 Disp (ps/nm/km)	20.13	20.13	20.45	20.46
LP11 Disp (ps/nm/km)	20.37	20.37	20.72	20.72
LP02 Disp (ps/nm/km)	20.54	20.54	20.24	19.88
LP21 Disp (ps/nm/km)	20.61	20.62	20.74	20.60
LP12 Disp (ps/nm/km)	20.36	20.70	N/A	N/A
LP31 Disp (ps/nm/km)	20.75	20.85	N/A	N/A
DGD (ps/km)	16.5	22.6	13.2	13.0

[0050] **Table 2** contains data for Examples 5-8 which were modeled with cores having graded refractive index profiles with alpha values of between 1.9 and 2.1. The numerical apertures NA of the fiber cores **102** of the optical fibers Examples 5-8 are between 0.15 and 0.18. As shown in **Table 2**, Examples 5-8 each support the propagation and transmission of two LP modes and have effective areas between $85 \mu\text{m}^2$ and $110 \mu\text{m}^2$, for example areas between $85 \mu\text{m}^2$ and $100 \mu\text{m}^2$. Each of these exemplary fibers has low LP01 mode attenuation below 0.2 dB/km at 1550 nm. Each of these exemplary fibers has DGD values less than 5 ps/nm. Also included in **Table 2** is a comparative example step index fiber which also supports the propagation and transmission of 2 LP modes. The DGD comparative example is between the LP01 and LP11 modes is approximately 2000 ps/nm, which is three orders of magnitude greater than the DGDs of Examples 5-8 (see below). Each of these exemplary fibers has modeled DGD values less than 10 ps/nm, for example less than 5 ps/nm.

Table 2

	Example 5	Example 6	Example 7	Example 8	Comparative
Delta 1MAX (%) (Δ_{1MAX})	0.606	0.606	0.606	0.606	0.350
R1 (microns)	9.25	9.27	9.01	9.11	8.00
Alpha	1.976	1.978	1.982	1.987	20
R2 (microns)	10.29	10.47	10.08	9.58	
W2 (microns)	1.04	1.20	1.07	0.47	
Delta3MIN (%)	-0.4	-0.45	-0.4	-0.25	
R3 (microns)	14.5	14.5	14.5	15	
W3 (microns)	4.21	4.04	4.43	5.42	
LP Modes at 1550nm	2	2	2	2	2
LP01 Attn 1550 (dB/km)	0.186	0.186	0.187	0.186	0.186
LP01 Aeff (sq. microns)	89.8	90.2	87.5	88.5	154
NA	0.160	0.160	0.160	0.160	0.121
LP01 Cutoff (microns)	> 5	> 5	> 5	> 5	> 5
LP11 Cutoff (microns)	2.290	2.293	2.225	2.268	2.443
LP02 Cutoff (microns)	< 1.55	< 1.55	< 1.55	< 1.55	< 1.55
LP21 Cutoff (microns)	< 1.55	< 1.55	< 1.55	< 1.55	< 1.55
LP01 Disp (ps/nm/km)	20.85	20.85	20.88	20.86	22.18
LP11 Disp (ps/nm/km)	21.06	21.13	21.10	20.73	19.22
DGD (ps/km)	0.190	0.260	0.860	0.030	2000

[0051] **Table 3** contains data for Examples 9-10 which were modeled with cores having graded refractive index profiles with alpha values of between 1.9 and 2.1. The inner annular segment in these examples is an extension of the graded index core, as shown in **Figure 2B**. The numerical apertures NA of the fiber cores **102** of the optical fibers Examples 9-10 are between 0.15 and 0.20. As shown in Table 1, Examples 9 and 10 support the propagation and transmission of 2 and 4 LP modes, respectively, and have effective areas between $85 \mu\text{m}^2$ and $110 \mu\text{m}^2$. Each of these exemplary fibers has low LP01 mode attenuation below 0.2 dB/km at 1550 nm. Each of these exemplary fibers has modeled DGD values less than 50 ps/nm, for example less than 30 ps/nm.

Table 3

	Example 9	Example 10
Delta 1MAX (%) (Δ_{1MAX})	0.603	0.757
R1 (microns)	9.05	11.01
Alpha	2.013	2.011
R2 (microns)	11.35	13.41
W2 (microns)	2.30	2.40
Delta3MIN (%)	-0.4	-0.424
R3 (microns)	15	16.7
W3 (microns)	3.66	3.30
LP Modes at 1550nm	2	4
LP01 Attn 1550 (dB/km)	0.186	0.186
LP01 Aeff (sq. microns)	88.5	95.6
NA	0.160	0.179
LP11 Cutoff (microns)	2.255	3.080
LP02 Cutoff (microns)	< 1.5	2.032
LP21 Cutoff (microns)	< 1.5	2.024
LP12 Cutoff (microns)	< 1.5	< 1.53
LP31 Cutoff (microns)	< 1.5	< 1.53
LP01 Disp (ps/nm/km)	20.85	20.50
LP11 Disp (ps/nm/km)	20.84	20.70
LP02 Disp (ps/nm/km)	N/A	20.31
LP21 Disp (ps/nm/km)	N/A	20.74
DGD (ps/km)	0.030	27.7

[0052] In particular, Examples 2-10 demonstrate that the differential group delays can be reduced to less than 150 ps/km while having a numerical aperture greater than 0.15 when the optical fiber is formed with a low index ring and a graded index core.

[0053] It should be understood that the optical fibers described herein support the propagation and transmission of more than one mode of an optical signal. Moreover, the increase in the NA decreases the non-linearity of the optical fiber thereby improving the performance of the optical fiber in long-haul optical communications systems.

[0054] It should also be understood that the optical fibers described herein with cores having graded refractive index profiles may be used to minimize time delays between higher order modes of optical signals propagating in the core of the optical fiber. Such optical fibers are suitable for use in WDM communications systems where digital signal processing may be readily used to compensate for the minimized time delays in the optical fiber.

[0055] It will be apparent to those skilled in the art that various modifications and variations can be made to the embodiments described herein without departing from the spirit and scope of the claimed subject matter. Thus it is intended that the specification cover the modifications and variations of the various embodiments described herein provided such modification and variations come within the scope of the appended claims and their equivalents.

What is claimed is:

1. An optical fiber comprising a glass core and a glass cladding surrounding and in direct contact with the glass core, wherein:

the glass core comprises:

a radius R_1 from about 8 μm to about 13 μm ;

a graded refractive index profile with an alpha value greater than or equal to about 1.8 and less than about 2.2 at a wavelength of 1550 nm;

a maximum relative refractive index $\Delta_{1\text{MAX}}$ from about 0.6 to about 0.95 relative to the glass cladding;

an effective area of LP01 mode between 80 μm^2 and 110 μm^2 , the glass core supporting the propagation and transmission of an optical signal with X LP modes at a wavelength of 1550 nm, wherein X is an integer greater than 1 and less than 10; and

the glass cladding comprises a maximum relative refractive index $\Delta_{1\text{MAX}}$ such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}}$, wherein the optical fiber has a maximum DGD of less than or equal to about 150 ps/km at a wavelength of 1550 nm.

2. The optical fiber of claim 1 wherein:

the radius R_c is from about 10 μm to about 13 μm ; the alpha value is between 1.95 and 2.1 at a wavelength of 1550 nm; the maximum relative refractive index $\Delta_{1\text{MAX}}$ is from about 0.7% to about 0.95% relative to an outer cladding layer of the glass cladding; the effective area of LP01 mode between 85 and 100 μm^2 ; and

the glass cladding comprises:

a low index ring surrounding said core; and

the outer cladding layer that surrounds and is in direct contact with the low index ring, wherein the low index ring has a minimum relative refractive index $\Delta_{3\text{MIN}}$ relative to the outer cladding layer and the outer cladding layer has a maximum relative refractive index $\Delta_{4\text{MAX}}$ relative to pure silica glass such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}} > \Delta_{3\text{MIN}}$, wherein the optical fiber has a maximum DGD of less than or equal to about 150 ps/km at a wavelength of 1550 nm.

3. The optical fiber of claim 1, wherein:

the radius R_c is from about 8 μm to about 10 μm ;
 the alpha value between is 1.95 and 2.1 at a wavelength of 1550 nm;
 the maximum relative refractive index $\Delta_{1\text{MAX}}$ from about 0.6% to about 0.7% relative to an outer cladding layer of the glass cladding;
 the effective area of LP01 mode between 85 and 100 μm^2 ; and
 the glass cladding comprises:
 a low index ring surrounding the core; and
 the outer cladding layer that surrounds and is in direct contact with the low index ring, wherein the low index ring has a minimum relative refractive index $\Delta_{3\text{MIN}}$ relative to the outer cladding layer and the outer cladding layer has a maximum relative refractive index $\Delta_{4\text{MAX}}$ relative to pure silica glass such that $\Delta_{1\text{MAX}} > \Delta_{4\text{MAX}} > \Delta_{3\text{MIN}}$, wherein the optical fiber has a maximum DGD of less than or equal to about 150 ps/km at a wavelength of 1550 nm.

4. The optical fiber of claim 1-3, further comprising an inner cladding layer surrounding and in direct contact with the glass core, the inner cladding layer having a maximum relative refractive index $\Delta_{2\text{MAX}}$ such that $\Delta_{1\text{MAX}} > \Delta_{2\text{MAX}} \geq \Delta_{3\text{MIN}}$; said low index ring surrounding and in direct contact with the inner cladding layer.

5. The optical fiber according to claim 1-4, wherein the optical fiber has a numerical aperture NA where $0.15 \leq \text{NA} \leq 0.2$.

6. The optical fiber according to claim 1-3, wherein the optical fiber has a maximum DGD of less than or equal to about 50 ps/km at a wavelength of 1550 nm.

7. The optical fiber according to claim 6, wherein the optical fiber has a maximum DGD of less than or equal to about 10 ps/km at a wavelength of 1550 nm.

8. The optical fiber according to claim 1-3, wherein $X = 2$.

9. The optical fiber according to claim 1-3, wherein the optical fiber has a core with an alpha value greater than or equal to about 1.8 and less than about 2.1, the numerical aperture NA is

$0.15 \leq \text{NA} \leq 0.2$; and a maximum DGD of less than or equal to about 50 ps/km at a wavelength of 1550 nm.

10. The fiber of claims 1-3 , wherein the alpha value is greater than or equal to about 1.95 and less than or equal to about 2.05 at a wavelength of 1550 nm.

11. The optical fiber of claim 1-3, wherein the glass cladding comprises a low index ring which is spaced apart from the core by an inner cladding layer.

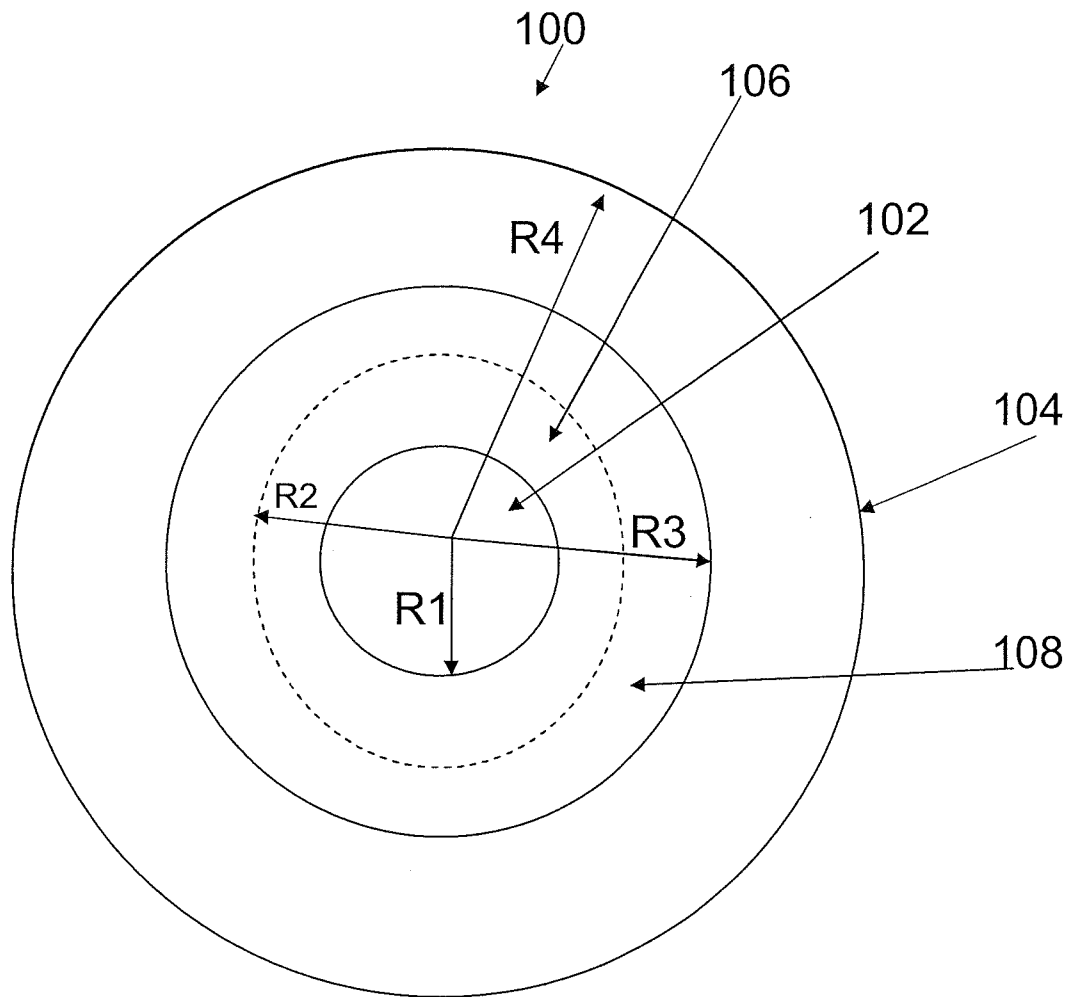


Fig. 1

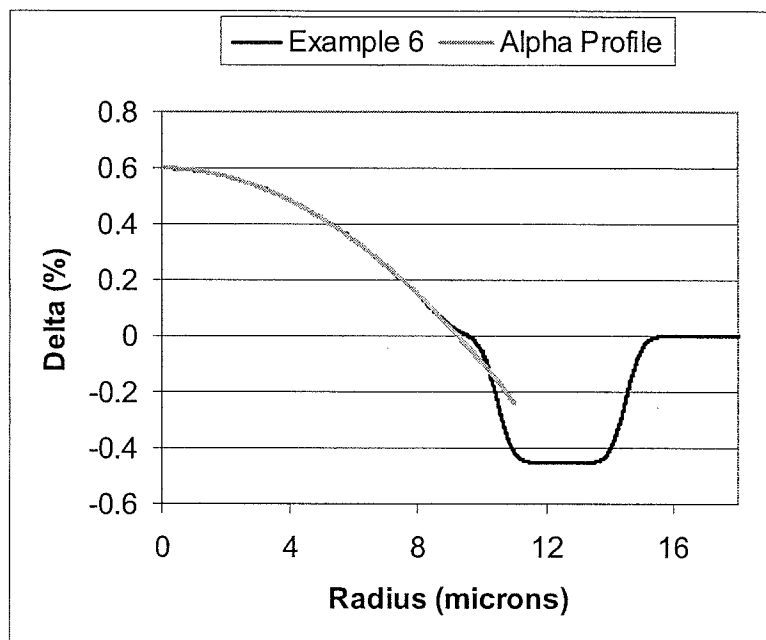


Fig. 2A

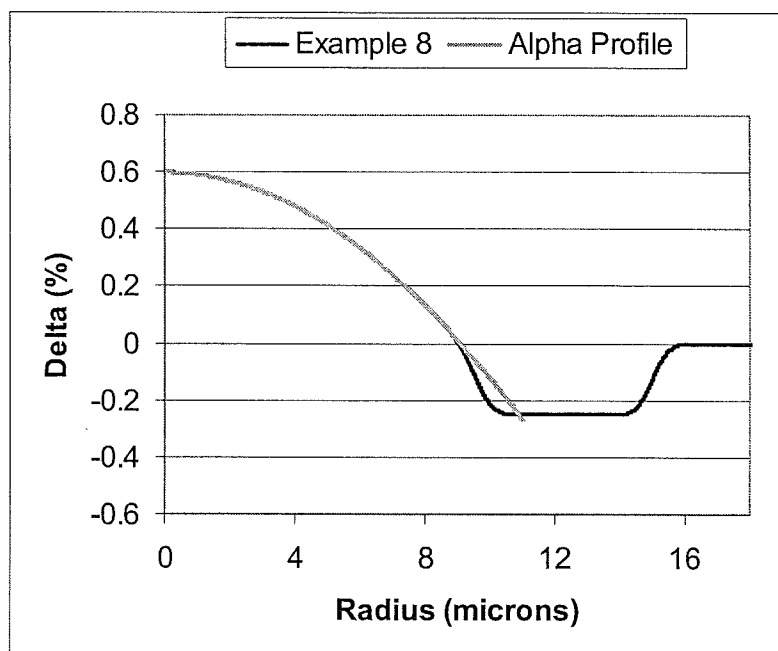


Fig. 2B

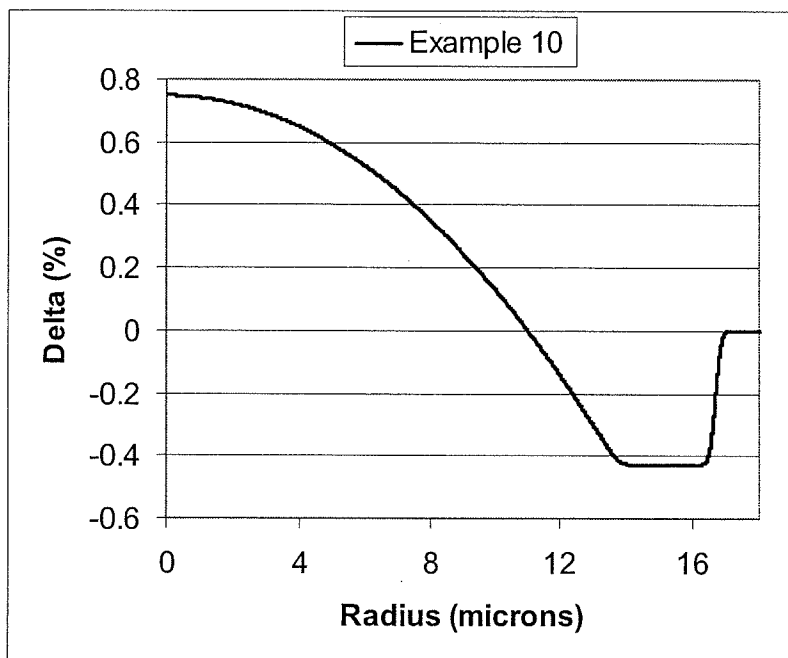


Fig. 2C

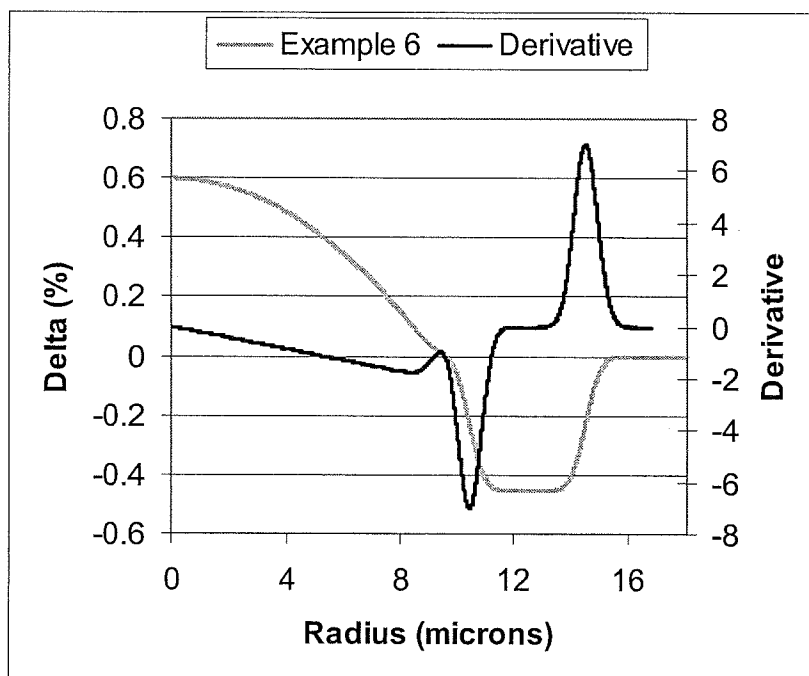


Fig. 3

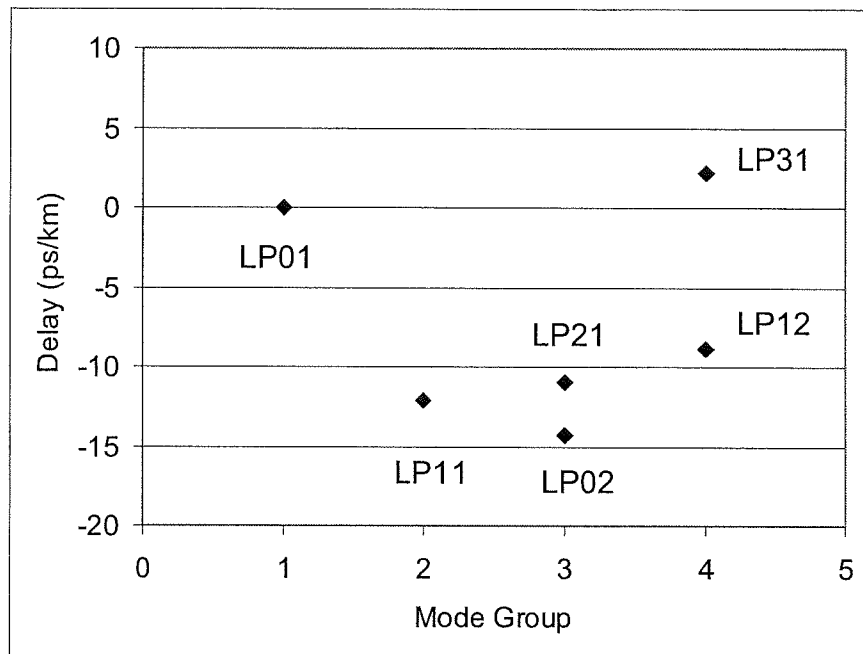


Fig. 4

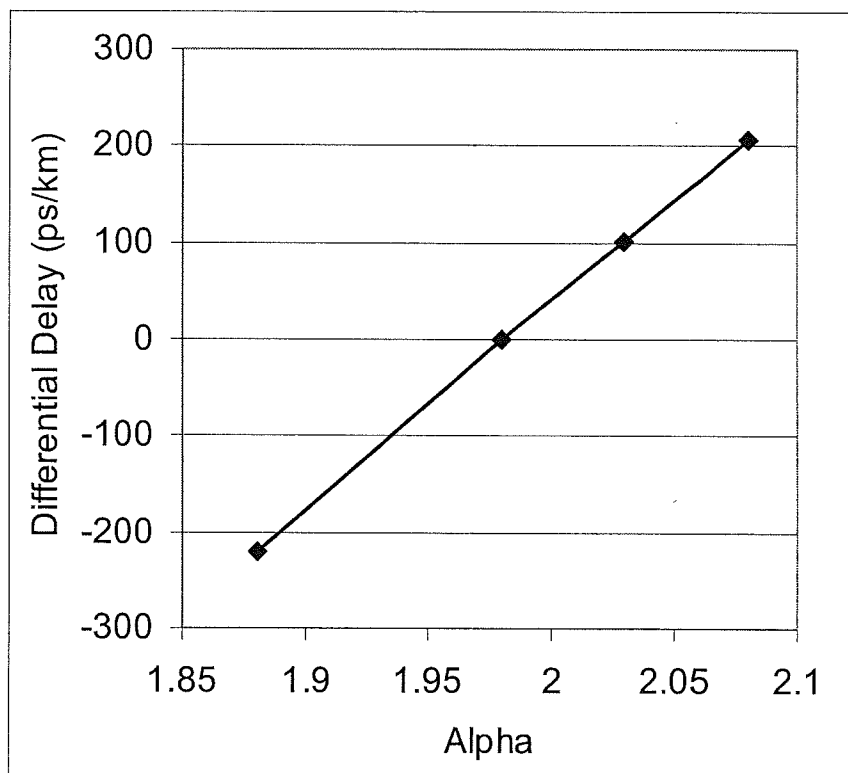


Fig. 5

INTERNATIONAL SEARCH REPORT

International application No

PCT/US2012/037186

A. CLASSIFICATION OF SUBJECT MATTER

INV. G02B6/028

ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 2010/019222 A1 (CORNING INC [US]; CHEN XIN [US]; LI MING-JUN [US]; NOLAN DANIEL A [US]) 18 February 2010 (2010-02-18) abstract; figures 1,2,4,6,8,10,12,14,16 paragraphs [0031], [0041] - [0042], [0045], [0047], [0049], [0056] - [0058] -----	1-11
A	US 2008/166094 A1 (BOOKBINDER DANA CRAIG [US] ET AL) 10 July 2008 (2008-07-10) abstract; figures 1,3,5 paragraphs [0049], [0051] -----	1,4,11



Further documents are listed in the continuation of Box C.



See patent family annex.

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