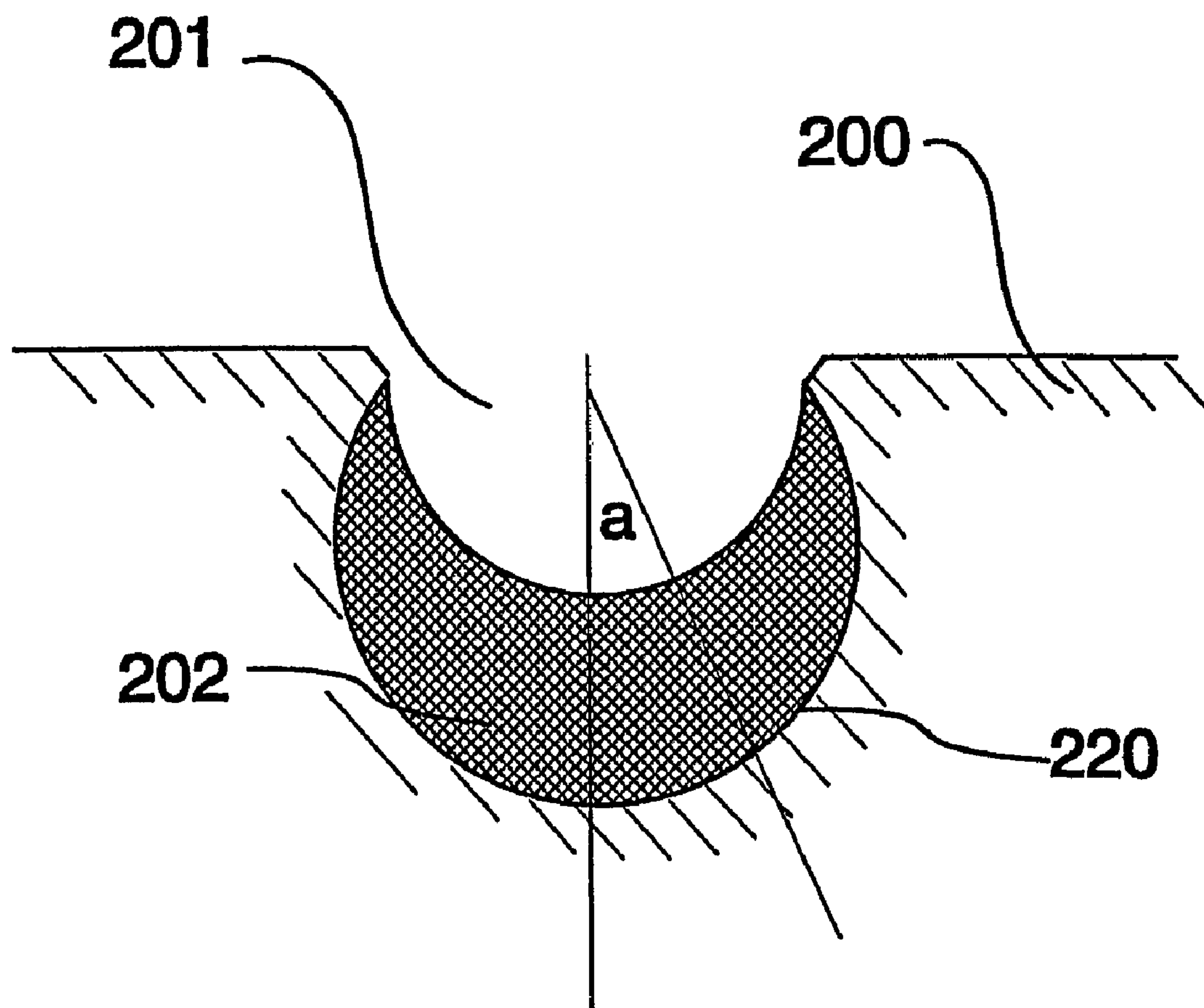




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(54) Title: ELEVATOR AND TRACTION SHEAVE OF AN ELEVATOR



(57) Abrégé/Abstract:

A counterweight and an elevator car are suspended on a set of hoisting ropes. The elevator comprises one or more rope pulleys provided with rope grooves, one of said pulleys being a traction sheave driven by a drive machine and moving the set of hoisting



(57) **Abrégé(suite)/Abstract(continued):**

ropes. At least one of the rope pulleys has against the hoisting rope a coating adhesively bonded to the rope pulley and containing the rope grooves, said coating having an elasticity that is greater in the edge portions of the rope groove than at the bottom of the rope groove. In a preferred solution, the traction sheave is a rope pulley like this.

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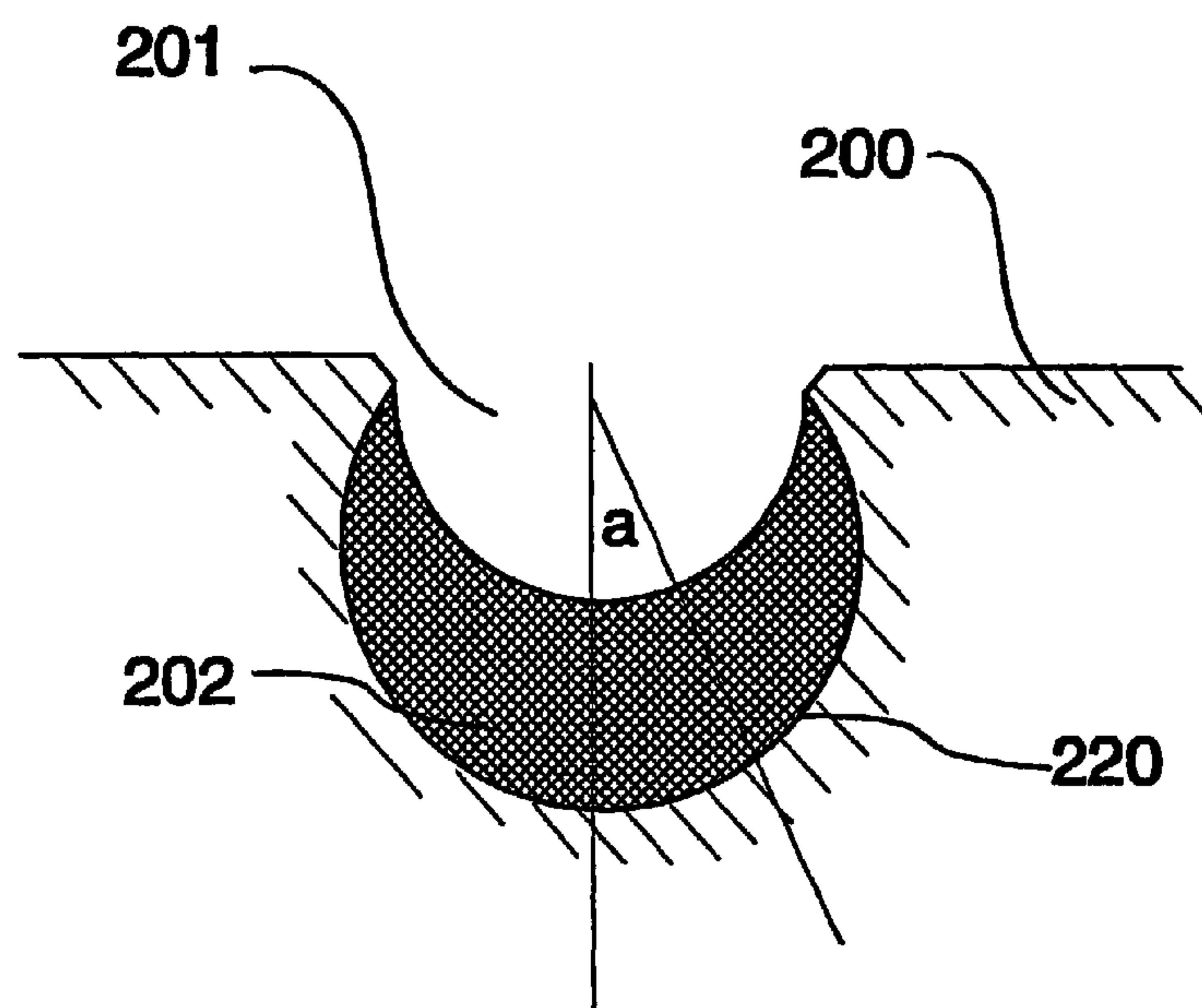
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(54) Title: ELEVATOR AND TRACTION SHEAVE OF AN ELEVATOR



(57) Abstract: A counterweight and an elevator car are suspended on a set of hoisting ropes. The elevator comprises one or more rope pulleys provided with rope grooves, one of said pulleys being a traction sheave driven by a drive machine and moving the set of hoisting ropes. At least one of the rope pulleys has against the hoisting rope a coating adhesively bonded to the rope pulley and containing the rope grooves, said coating having an elasticity that is greater in the edge portions of the rope groove than at the bottom of the rope groove. In a preferred solution, the traction sheave is a rope pulley like this.

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ELEVATOR AND TRACTION SHEAVE OF AN ELEVATOR

The present invention relates to an elevator as defined in the preamble of claim 1 and to an elevator
5 traction sheave as defined in the preamble of claim 7.

The operation of a conventional traction sheave elevator is based on a solution in which steel wire ropes serving as hoisting ropes and also as suspension ropes
10 are moved by means of a metallic traction sheave, often made of cast iron, driven by an elevator drive machine. The motion of the hoisting ropes produces a motion of a counterweight and elevator car suspended on them. The tractive force from the traction sheave to
15 the hoisting ropes, as well as the braking force applied by means of the traction sheave, is transmitted by the agency of the friction between the traction sheave and the ropes.

20 The coefficient of friction between the steel wire ropes and the metallic traction sheaves used in elevators is often insufficient in itself to maintain the required grip between the traction sheave and the hoisting rope in normal situations during elevator operation. The friction and the forces transmitted by
25 the rope are increased by modifying the shape of the rope grooves on the traction sheave. The traction sheaves are provided with undercut or V-shaped rope grooves, which create a strain on the hoisting ropes
30 and therefore also cause more wear of the hoisting ropes than rope grooves of an advantageous semi-circular cross-sectional form as used e.g. in diverting pulleys. The force transmitted by the rope can also be increased by increasing the angle of bite between the traction sheave and the ropes, e.g. by using
35 a so-called "double wrap" arrangement.

In the case of a steel wire rope and a cast-iron or cast-steel traction sheave, a lubricant is almost always used in the rope to reduce rope wear. A lubricant especially reduces the internal rope wear resulting from the interaction between rope strands. External wear of the rope consists of the wear of surface wires mainly caused by the traction sheave. The effect of the lubricant is also significant in the contact between the rope surface and the traction sheave.

10

To provide a substitute for the rope groove shape that causes rope wear, inserts placed in the rope groove to achieve a greater friction coefficient have been used. Such prior-art inserts are disclosed e.g. in specifications US3279762 and US4198196. The inserts described in these specifications are relatively thick. The rope grooves of the inserts are provided with a transverse or nearly transverse corrugation creating additional elasticity in the surface portion of the insert and in a way softening its surface. The inserts undergo wear caused by the forces imposed on them by the ropes, so they have to be replaced at intervals. Wear of the inserts occurs in the rope grooves, at the interface between insert and traction sheave and internally.

25

It is an object of the invention to achieve an elevator in which the traction sheave has an excellent grip on a steel wire rope and in which the traction sheave is durable and of a design that reduces rope wear. Another object of the invention is to eliminate or avoid the above-mentioned disadvantages of prior-art solutions and to achieve a traction sheave that provides an excellent grip on the rope and is durable and reduces rope wear. A specific object of the invention is to disclose a new type of engagement between the traction sheave and the rope in an elevator. It is also an object of the invention to apply said engagement be-

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tween the traction sheave and the rope to possible diverting pulleys of the elevator.

As for the features characteristic of the invention,
5 reference is made to the claims.

In an elevator provided with hoisting ropes of substantially round cross-section, the direction of deflection of the hoisting ropes can be freely changed
10 by means of a rope pulley. Thus, the basic layout of the elevator, i.e. the disposition of the car, counterweight and hoisting machine can be varied relatively freely. Steel wire ropes or ropes provided with a load-bearing part twisted from steel wires constitute a tried way of composing a set of hoisting ropes
15 for suspending the elevator car and counterweight. An elevator driven by means of a traction sheave may comprise other diverting pulleys besides the traction sheave. Diverting pulleys are used for two different
20 purposes: diverting pulleys are used to establish a desired suspension ratio of the elevator car and/or counterweight, and diverting pulleys are used to guide the passage of the ropes. Each diverting pulley may be mainly used for one of these purposes, or it may have
25 a definite function both regarding the suspension ratio and as a means of guiding the ropes. The traction sheave driven by the drive machine additionally moves the set of hoisting ropes. The traction sheave and other eventual diverting pulleys are provided with
30 rope grooves, each rope in the set of hoisting ropes being thus guided separately.

When a rope pulley has against a steel wire rope a coating containing rope grooves and giving great friction,
35 tion, a practically non-slip contact between rope pulley and rope is achieved. This is advantageous especially in the case of a rope pulley used as a traction

sheave. If the coating is relatively thin, the force difference arising from the differences between the rope forces acting on different sides of the rope pulley will not produce a large tangential displacement of the surface that would lead to a large extension or compression in the direction of the tractive force when the rope is coming onto the pulley or leaving it. The greatest difference across the pulley occurs at the traction sheave, which is due to the usual difference of weight between the counterweight and the elevator car and to the fact that the traction sheave is not a freely rotating pulley but produces, at least during acceleration and braking, a factor either adding to or detracting from the rope forces resulting from the balance difference, depending on the direction of the balance difference and that of the elevator motion. A thin coating is also advantageous in that, as it is squeezed between the rope and the traction sheave, the coating can not be compressed so much that the compression would tend to evolve to the sides of the rope groove. As such compression causes lateral spreading of the material, the coating might be damaged by the great tensions produced in it. By making the coating thicker in the bottom area of the groove than in its lateral parts, a groove bottom portion having a greater elasticity than the edges is achieved. In this way, the surface pressure imposed on the rope can be more evenly distributed over the rope surface and the surface of the rope groove. Thus, the rope groove also provides more uniform support to the rope, and the pressure imposed on the rope maintains the cross-sectional form of the rope better. However, the coating must have a thickness sufficient to receive the rope elongations resulting from tension so that no rope slip fraying the coating occurs. At the same time, the coating has to be soft enough to allow the structural roughness of the rope, in other words,

the surface wires to sink at least partially into the coating, yet hard enough to ensure that the coating will not substantially escape from under the roughness of the rope.

5

For steel wire ropes less than 10 mm thick, in which the surface wires are of a relatively small thickness, a coating hardness ranging from below 60 shoreA up to about 100 shoreA can be used. For ropes having surface
10 wires thinner than in conventional elevator ropes, i.e. ropes having surface wires only about 0.2 mm thick, a preferable coating hardness is in the range of about 80...90 shoreA or even harder. A relatively hard coating can be made thin. When a rope with some-
15 what thicker surface wires (about 0.5...1 mm) is used, a good coating hardness is in the range of about 70...85 shoreA and a thicker coating is needed. In other words, for thinner wires a harder and thinner coating is used, and for thicker wires a softer and thicker
20 coating is used. As the coating is firmly attached to the sheave by an adhesive bond comprising the entire area resting against the sheave, there will occur between the coating and the sheave no slippage causing wear of these. An adhesive bond may be made e.g. by
25 vulcanizing a rubber coating onto the surface of a metallic rope sheave or by casting polyurethane or similar coating material onto a rope sheave with or without an adhesive or by applying a coating material on the rope sheave or gluing a coating element fast onto
30 the rope sheave.

Thus, on the one hand, due to the total load or average surface pressure imposed on the coating by the rope, the coating should be hard and thin, and on the
35 other hand, the coating should be sufficiently soft and thick to permit the rough surface structure of the rope to sink into the coating to a suitable degree to

produce sufficient friction between the rope and the coating and to ensure that the rough surface structure will not pierce the coating.

5 A highly advantageous embodiment of the invention is the use of a coating on the traction sheave. Thus, a preferred solution is to produce an elevator in which at least the traction sheave is provided with a coating. A coating is also advantageously used on the di-
10 verting pulleys of the elevator. The coating functions as a damping layer between the metallic rope pulley and the hoisting ropes.

The coating of the traction sheave and that of a rope
15 pulley may be differently rated so that the coating on the traction sheave is designed to accommodate a larger force difference across the sheave. The properties to be rated are thickness and material properties of the coating. Preferable coating materials are rubber and polyurethane. The coating is required to be
20 elastic and durable, so it is possible to use other durable and elastic materials as far as they can be made strong enough to bear the surface pressure produced by the rope. The coating may be provided with
25 reinforcements, e.g. carbon fiber or ceramic or metallic fillers, to improve its capacity to withstand internal tensions and/or the wearing or other properties of the coating surface facing the rope.

30 The invention provides the following advantages, among other things:

- great friction between traction sheave and hoisting rope
- a coating having a greater thickness in the bottom
35 area of the groove distributes the load evenly in the transverse direction of the rope groove, so the

groove bottom is not subjected to a greater strain than the edge portions

- uniform support of the rope reduces the strain on the internal portions of the rope
- 5 - the coating reduces abrasive wear of the ropes, which means that less wear allowance is needed in the surface wires of the rope, so the ropes can be made entirely of thin wires of strong material
- since the ropes can be made of thin wires, and since
10 thin wires can be made relatively stronger, the hoisting ropes may be correspondingly thinner, smaller rope pulleys can be used, which again allows a space saving and more economical layout solutions
- the coating is durable because in a relatively thin
15 coating no major internal expansion occurs
- in a thin coating, deformations are small and therefore also the dissipation resulting from deformations and producing heat internally in the coating is low and heat is easily removed from the thin
20 coating, so the thermal strain produced in the coating by the load is small
- as the rope is thin and the coating on the rope pulley is thin and hard, the rope pulley rolls lightly against the rope
- 25 - no wear of the coating occurs at the interface between the metallic part of the traction sheave and the coating material
- the great friction between the traction sheave and the hoisting rope allows the elevator car and counterweight to be made relatively light, which means a
30 cost saving.

In the following, the invention will be described in detail with reference to the attached drawings,
35 wherein

- Fig. 1 presents a diagram representing an elevator according to the invention,
- Fig. 2 presents a rope pulley applying the invention,
- 5 Fig. 3 presents a coating solution according to the invention, and
- Fig. 4 and 5 present alternative coating solutions according to the invention.
- 10 Fig. 1 is a diagrammatic representation of the structure of an elevator. The elevator is preferably an elevator without machine room, in which the drive machine 6 is placed in the elevator shaft, although the invention is also applicable for use in elevators with
- 15 machine room. The passage of the hoisting ropes 3 of the elevator is as follows: One end of the ropes is immovably fixed to an anchorage 13 located in the upper part of the shaft above the path of a counterweight 2 moving along counterweight guide rails 11.
- 20 From the anchorage, the ropes run downward and are passed around diverting pulleys 9 suspending the counterweight, which diverting pulleys 9 are rotatably mounted on the counterweight 2 and from which the ropes 3 run further upward to the traction sheave 7 of
- 25 the drive machine 6, passing around the traction sheave along rope grooves on the sheave. From the traction sheave 7, the ropes 3 run further downward to the elevator car 1 moving along car guide rails 10, passing under the car via diverting pulleys 4 used to
- 30 suspend the elevator car on the ropes, and going then upward again from the elevator car to an anchorage 14 in the upper part of the elevator shaft, to which anchorage the second end of the ropes 3 is fixed. Anchorage 13 in the upper part of the shaft, the traction sheave 7 and the diverting pulley 9 suspending
- 35 the counterweight on the ropes are preferably so dis-

posed in relation to each other that both the rope portion going from the anchorage 13 to the counterweight 2 and the rope portion going from the counterweight 2 to the traction sheave 7 are substantially parallel to the path of the counterweight 2. Similarly, a solution is preferred in which anchorage 14 in the upper part of the shaft, the traction sheave 7 and the diverting pulleys 4 suspending the elevator car on the ropes are so disposed in relation to each other that the rope portion going from the anchorage 14 to the elevator car 1 and the rope portion going from the elevator car 1 to the traction sheave 7 are substantially parallel to the path of the elevator car 1. With this arrangement, no additional diverting pulleys are needed to define the passage of the ropes in the shaft. The rope suspension acts in a substantially centric manner on the elevator car 1, provided that the rope pulleys 4 supporting the elevator car are mounted substantially symmetrically relative to the vertical center line passing via the center of gravity of the elevator car 1.

The drive machine 6 placed in the elevator shaft is preferably of a flat construction, in other words, the machine has a small depth as compared with its width and/or height, or at least the machine is slim enough to be accommodated between the elevator car and a wall of the elevator shaft. The machine may also be placed differently. Especially a slim machine can be fairly easily fitted above the elevator car. The elevator shaft can be provided with equipment required for the supply of power to the motor driving the traction sheave 7 as well as equipment for elevator control, both of which can be placed in a common instrument panel 8 or mounted separately from each other or integrated partly or wholly with the drive machine 6. The drive machine may be of a geared or gearless type. A

preferable solution is a gearless machine comprising a permanent magnet motor. The drive machine may be fixed to a wall of the elevator shaft, to the ceiling, to a guide rail or guide rails or to some other structure, such as a beam or frame. In the case of an elevator with machine below, a further possibility is to mount the machine on the bottom of the elevator shaft. Fig. 1 illustrates the economical 2:1 suspension, but the invention can also be implemented in an elevator using a 1:1 suspension ratio, in other words, in an elevator in which the hoisting ropes are connected directly to the counterweight and elevator car without diverting pulleys, or in an elevator implemented using some other suspension arrangement suited for a traction sheave elevator.

Fig. 2 presents a partially sectioned view of a rope pulley 100 applying the invention. The rope grooves 101 are in a coating 102 placed on the rim of the rope pulley. The rope pulley is preferably made of metal or plastic. Provided in the hub of the rope pulley is a space 103 for a bearing used to support the rope pulley. The rope pulley is also provided with holes 105 for bolts, allowing the rope pulley to be fastened by its side to an anchorage in the hoisting machine 6, e.g. to a rotating flange, to form a traction sheave 7, in which case no bearing separate from the hoisting machine is needed.

Fig. 3 presents a solution in which the rope groove 201 is in a coating 202 which is thinner at the sides of the rope groove than at the bottom. In such a solution, the coating is placed in a basic groove 220 provided in the rope pulley 200 so that deformations produced in the coating by the pressure imposed on it by the rope will be small and mainly limited to the rope surface texture sinking into the coating. Such a solu-

tion often means in practice that the rope pulley coating consists of rope groove-specific sub-coatings separate from each other, but the inventive idea does not exclude an alternative in which the rope pulley
5 coating extends continuously over a number of grooves.

By making the coating thinner at the edges of the groove than at its bottom, the strain imposed by the rope on the bottom of the rope groove while sinking into the groove is avoided or at least reduced. As the
10 pressure cannot be discharged laterally but is directed by the combined effect of the shape of the basic groove 220 and the thickness variation of the coating 202 to support the rope in the rope groove 201, lower maximum surface pressures acting on the
15 rope and the coating are also achieved. One method of making a grooved coating 202 like this is to fill the round-bottomed basic groove 220 with coating material and then form a half-round rope groove 201 in this coating material in the basic groove. The shape of the
20 rope grooves is well supported and the load-bearing surface layer under the rope provides a better resistance against lateral propagation of the compression stress produced by the ropes. The lateral spreading or rather adjustment of the coating caused by the pres-
25 sure is promoted by thickness and elasticity of the coating and reduced by hardness and eventual reinforcements of the coating. The coating thickness on the bottom of the rope groove can be made large, even as large as half the rope thickness, in which case a
30 hard and inelastic coating is needed. On the other hand, if a coating thickness corresponding to only about one tenth of the rope thickness is used, then the coating material may be clearly softer. An elevator for eight persons could be implemented using a
35 coating thickness at the bottom of the groove equal to about one fifth of the rope thickness if the ropes and

the rope load are chosen appropriately. The coating thickness should equal at least 2-3 times the depth of the rope surface texture formed by the surface wires of the rope. Such a very thin coating, having a thickness even less than the thickness of the surface wire of the rope, will not necessarily endure the strain imposed on it. In practice, the coating must have a thickness larger than this minimum thickness because the coating will also have to receive rope surface variations rougher than the surface texture. Such a rougher area is formed e.g. where the level differences between rope strands are larger than those between wires. In practice, a suitable minimum coating thickness is about 1-3 times the surface wire thickness. In the case of the ropes normally used in elevators, which have been designed for a contact with a metallic rope groove and which have a thickness of 8-10 mm, this thickness definition leads to a coating at least about 1 mm thick. Since a coating on the traction sheave, which causes more rope wear than the other rope pulleys of the elevator, will reduce rope wear and therefore also the need to provide the rope with thick surface wires, the rope can be made smoother. The use of thin wires allows the rope itself to be made thinner, because thin steel wires can be manufactured from a stronger material than thicker wires. For instance, using 0.2 mm wires, a 4 mm thick elevator hoisting rope of a fairly good construction can be produced. A traction sheave coating well suited for such a rope is already clearly below 1 mm thick. However, the coating should be thick enough to ensure that it will not be very easily scratched away or pierced e.g. by an occasional sand grain or similar particle having got between the rope groove and the hoisting rope. Thus, a desirable minimum coating thickness, even when thin-wire hoisting ropes are

used, would be about 0.5...1 mm. For hoisting ropes having small surface wires and an otherwise relatively smooth surface, a coating having a thickness of the form $A+B\cos a$ is well suited. However, such a coating is also applicable to ropes whose surface strands meet the rope groove at a distance from each other, because if the coating material is sufficiently hard, each strand meeting the rope groove is in a way separately supported and the supporting force is the same and/or as desired. In the formula $A+B\cos a$, A and B are constants so that A+B is the coating thickness at the bottom of the rope groove 201 and the angle a is the angular distance from the bottom of the rope groove as measured from the center of curvature of the rope groove cross-section. Constant A is larger than or equal to zero, and constant B is always larger than zero. The thickness of the coating growing thinner towards the edges can also be defined in other ways besides using the formula $A+B\cos a$ so that the elasticity decreases towards the edges of the rope groove. Fig. 4 and 5 present cross-sectional views of rope grooves in which the elasticity of the middle portion of the rope groove has been specially increased. The rope groove in Fig. 4 is an undercut groove. In Fig. 5, the coating on the bottom of the rope groove comprises a particularly elastic area 221 of a different material, where the elasticity has been increased, in addition to increasing the material thickness, by the use of a material that is softer than the rest of the coating.

In the foregoing, the invention has been described by way of example with reference to the attached drawing while different embodiments of the invention are possible within the scope of the inventive idea defined in the claims. In the scope of the inventive idea, it is obvious that a thin rope increases the average surface pressure imposed on the rope groove if the rope

tension remains unchanged. This can be easily taken into account by adapting the thickness and hardness of the coating, because a thin rope has thin surface wires, so for instance the use of a harder and/or
5 thinner coating will not cause any problems. It is also obvious to a skilled person that the bearing surface of a rope groove of semi-circular cross-section may be less than 180 degrees.

THE EMBODIMENTS OF THE INVENTION IN WHICH AN EXCLUSIVE PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS FOLLOWS:

1. An elevator, in which a counterweight and an elevator car are suspended on a set of hoisting ropes consisting of hoisting ropes of substantially round cross-section, the elevator comprising one or more rope pulleys provided with rope grooves, one of said pulleys being a traction sheave driven by a drive machine and moving the set of hoisting ropes, and at least one of said rope pulleys has against the hoisting rope a coating adhesively bonded to the rope pulley and containing the rope grooves, said coating having an elasticity that is smaller in the edge parts of the rope groove than near the bottom of the rope groove, wherein said rope groove contains a round-bottomed basic groove area to which the coating is bonded and that the thickness of the coating varies in the area where it is bonded to the round-bottomed basic groove area.
2. The elevator according to claim 1, wherein the traction sheave is provided with the coating.
3. The elevator according to claim 1, wherein all rope pulleys are provided with the coating.
4. The elevator according to claim 1, wherein the coating is thinner in the edge parts of the rope groove than at the bottom of the rope groove.
5. The elevator according to any one of claims 1 to 4, wherein the thickness of the coating in the bottom area of the rope groove is substantially less than half the thickness of the rope running in the rope groove and a hardness less than 100 shoreA and greater than 60 shoreA.

6. The elevator according to any one of claims 1 to 5, wherein the hoisting ropes have a load-bearing part twisted from steel wires.

7. A traction sheave of an elevator, designed for hoisting ropes of substantially round cross-section, whereby the traction sheave has, against the hoisting rope, a coating bonded to the traction sheave and provided with rope grooves, said coating having an elasticity that is smaller in the edge parts of the rope groove than near the bottom of the rope groove, wherein said rope groove contains a round-bottomed basic groove area to which the coating is bonded and wherein the thickness of the coating varies in the area where it is bonded to the round-bottomed basic groove area.

8. The traction sheave according to claim 7, wherein the coating has a thickness that, at the bottom of the rope groove, is substantially less than half the thickness of the rope running in the rope groove, and a hardness less than 100 shoreA and greater than 60 shoreA.

9. The traction sheave according to claim 7 or 8, wherein the coating is made of rubber or polyurethane.

10. The traction sheave according to any one of claims 7 to 9, wherein the coating is thinner in the edge parts of the rope groove than at the bottom of the rope groove.

11. The traction sheave according to any one of claims 7 to 10, wherein the thickness of the coating is defined according to the formula $A + B \cos a$, in which formula A and B are constants and the angle a is the angular distance from the bottom center of the rope groove.

12. A coating for the rope groove of the traction sheave of an elevator, whereby the coating is adhesively bonded to the rope groove on the traction sheave and that the thickness of the coating is largest at the center of the bottom of the rope groove and diminishes gradually toward the edges of the rope groove, wherein the thickness of the coating being defined according to the formula $A + B \cos a$, in which formula A and B are constants and the angle a is the angular distance from the bottom center of the rope groove.

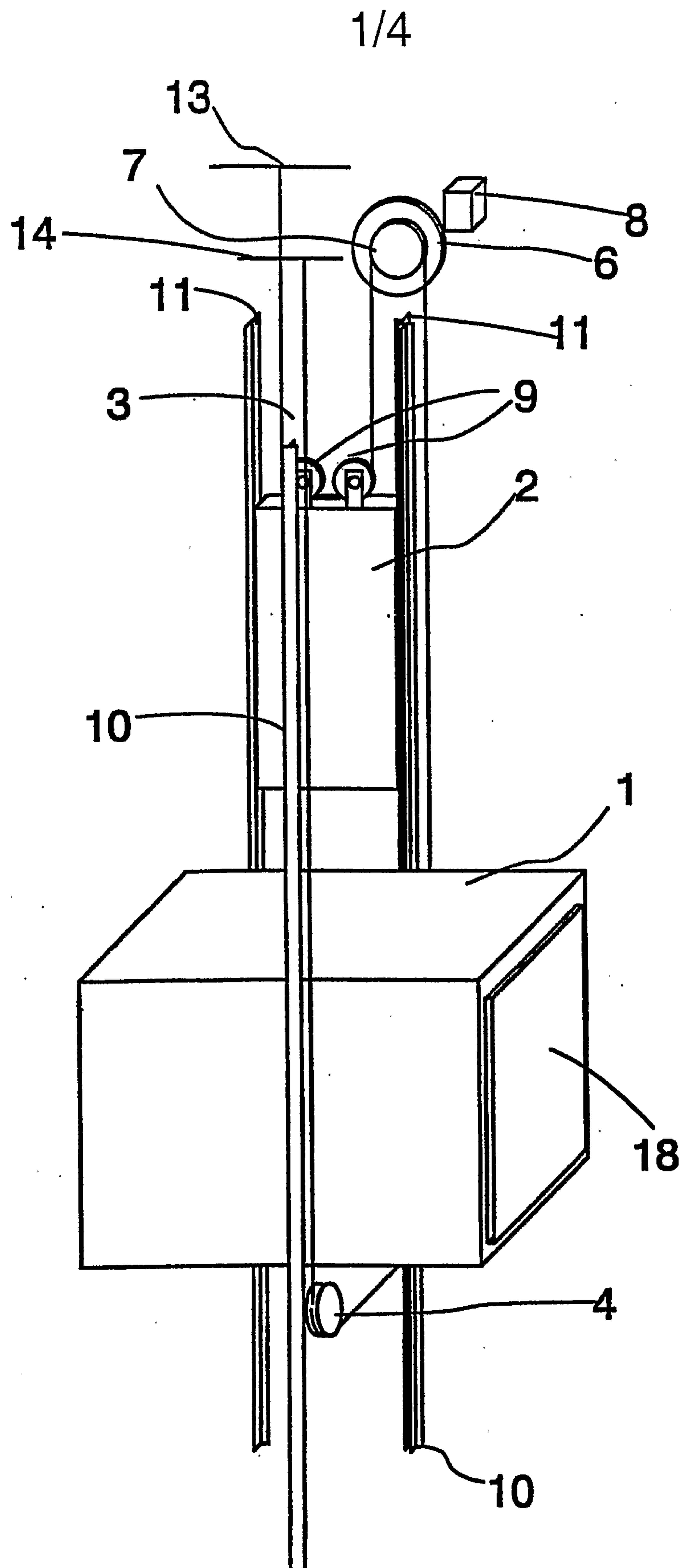


Fig. 1

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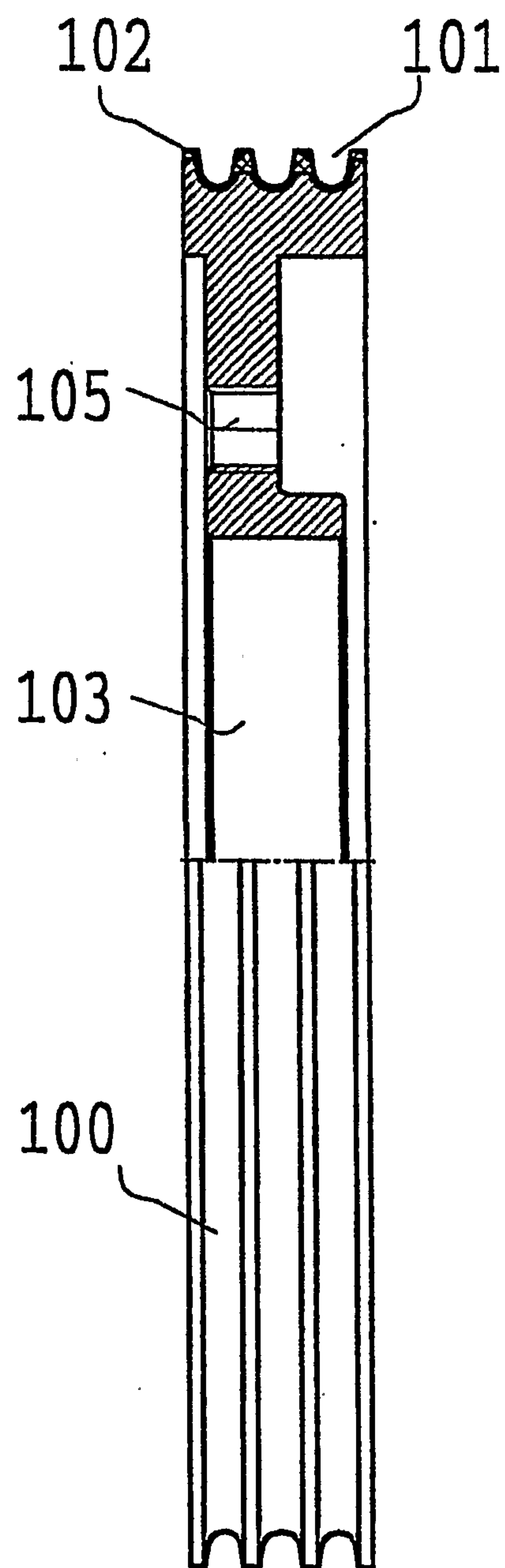


Fig. 2

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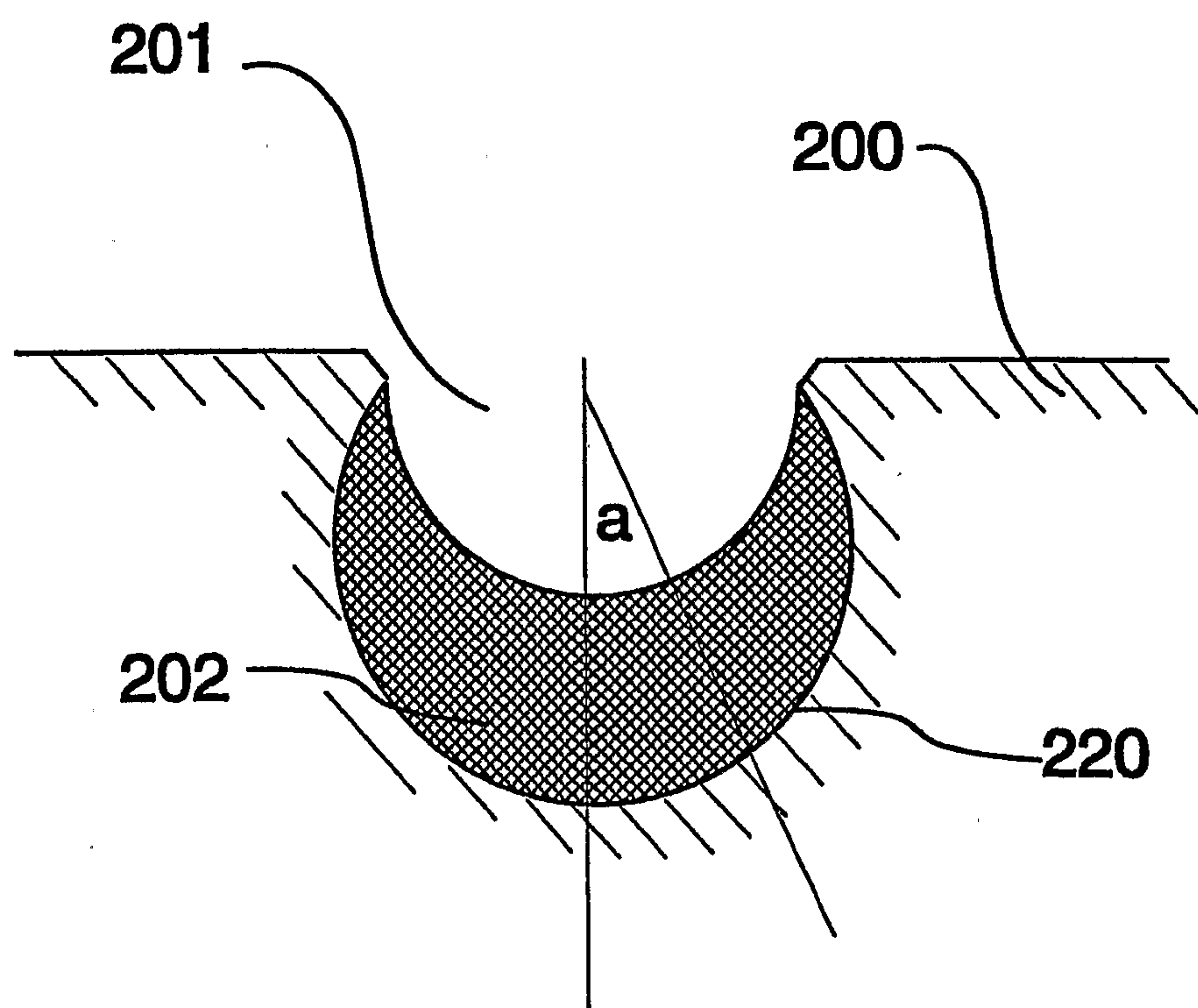


Fig. 3

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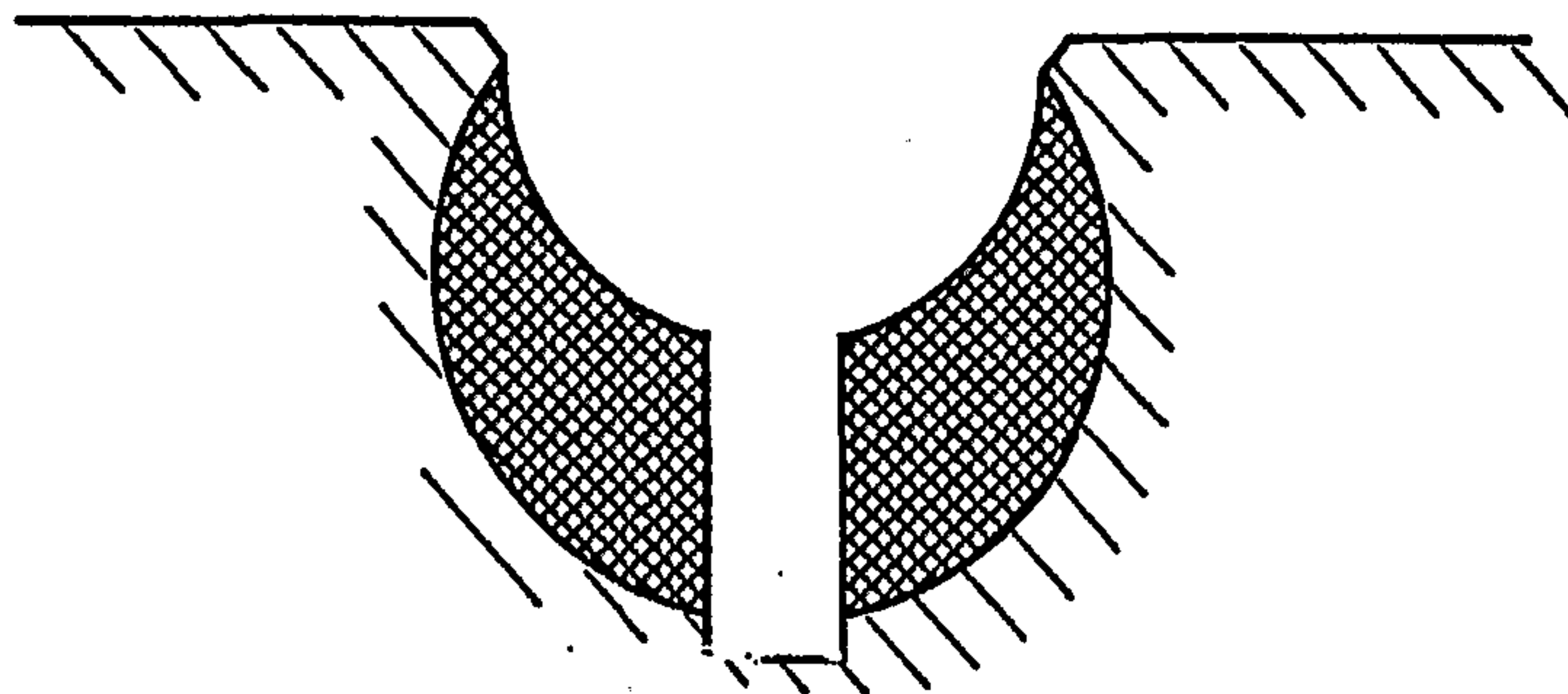


Fig. 4

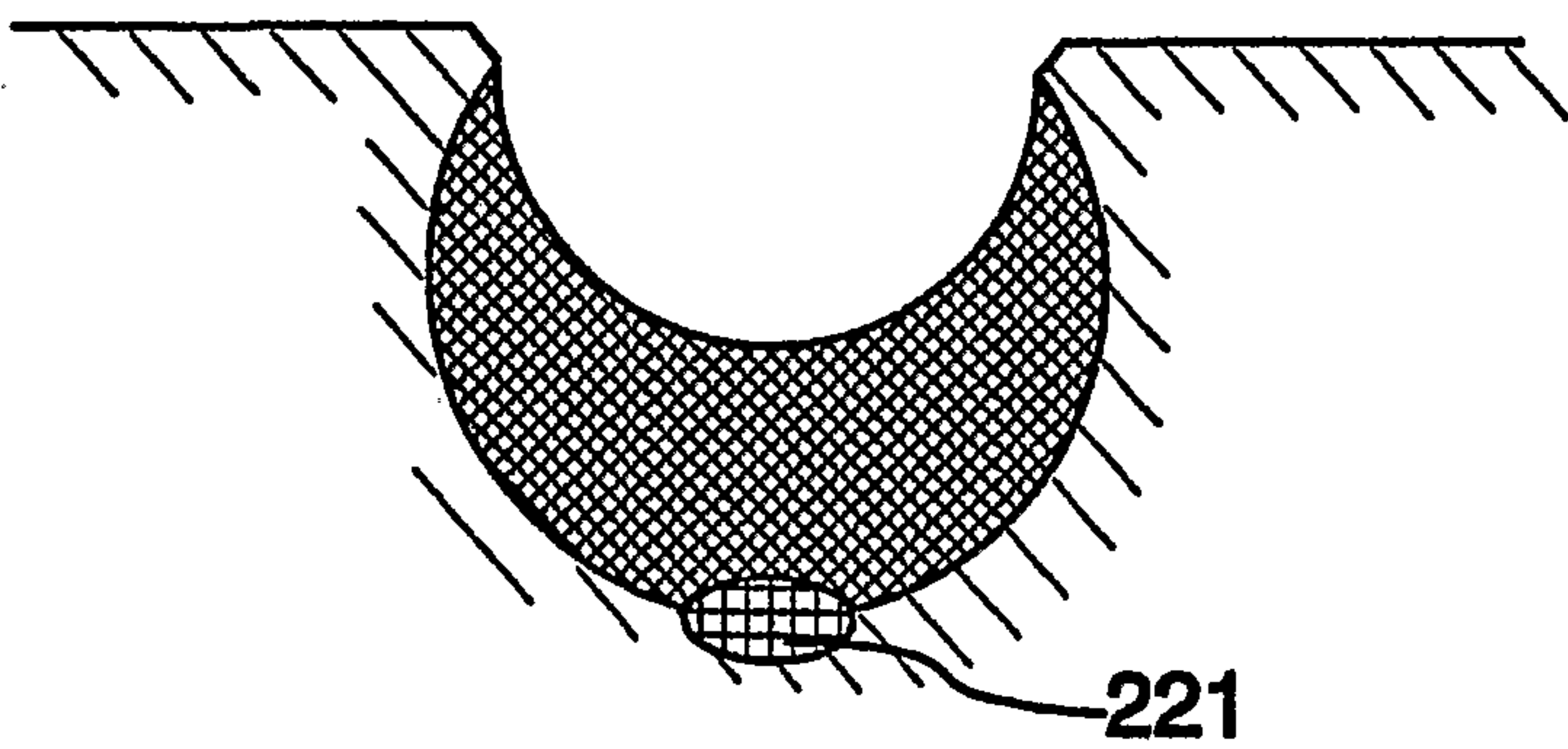


Fig. 5

