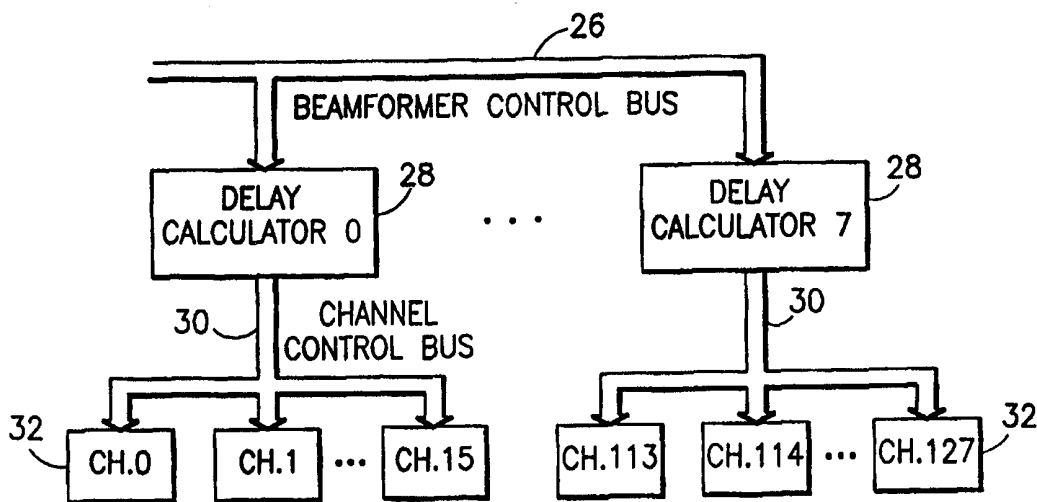




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(54) Title: METHOD AND APPARATUS FOR DISTRIBUTED, AGILE CALCULATION OF BEAMFORMING TIME DELAYS AND APODIZATION VALUES



(57) Abstract

An architecture in which a plurality of delay calculators (28) are distributed throughout the beamformer. Each delay calculator (28) provides beamforming delays and apodization values for a plurality of channels (32)/elements (34). The delay calculators (28) are initialized with element position coordinates. Then, while imaging, focal coordinates and steering angles are broadcast to all delay calculators (28). The delay calculator (28) uses a cordic rotator to perform the aperture projections and calculate the hypotenuse. The cordic rotator performs successive coordinate transformations, in two dimensions, using coefficients that are simple powers of two. The resulting apodization values and time delays are then provided by a channel control bus (30) to a plurality of channels (32).

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METHOD AND APPARATUS FOR DISTRIBUTED,  
AGILE CALCULATION OF BEAMFORMING  
TIME DELAYS AND APODIZATION VALUES

FIELD OF THE INVENTION

5           This invention generally relates to coherent imaging methods which apply a phased array antenna. In particular, the invention relates to beamforming techniques for use in ultrasound imaging systems.

BACKGROUND OF THE INVENTION

10           A medical ultrasound system forms an image by acquiring individual ultrasound lines (or beams). The lines are adjacent to each other and cover the target area to be imaged. Each line is formed by transmitting an ultrasonic pulse in a particular spatial  
15           direction and receiving the reflected echoes from that direction. The spatial characteristics of the transmitted wave and the characteristics of the receive sensitivity determine the quality of the ultrasound image. It is desirable that the ultrasound line  
20           gathers target information only from the intended direction and ignores targets at other directions.

          Conventional ultrasound imaging systems comprise an array of ultrasonic transducer elements which are used to transmit an ultrasound beam and then receive  
25           the reflected beam from the object being studied. Such scanning comprises a series of measurements in which the focused ultrasonic wave is transmitted, the system switches to receive mode after a short time interval, and the reflected ultrasonic wave is  
30           received, beamformed and processed for display. Typically, transmission and reception are focused in the same direction during each measurement to acquire data from a series of points along an acoustic beam or

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scan line. The receiver is dynamically focused at a succession of ranges along the scan line as the reflected ultrasonic waves are received.

For ultrasound imaging, the array typically has  
5 a multiplicity of transducer elements arranged in one or more rows and driven with separate voltages. By selecting the time delay (or phase) and amplitude of the applied voltages, the individual transducer elements in a given row can be controlled to produce  
10 ultrasonic waves which combine to form a net ultrasonic wave that travels along a preferred vector direction and is focused in a selected zone along the beam. The beamforming parameters of each of the firings may be varied to provide a change in maximum  
15 focus or otherwise change the content of the received data for each firing, e.g., by transmitting successive beams along the same scan line with the focal zone of each beam being shifted relative to the focal zone of the previous beam. In the case of a phased array, by  
20 changing the time delays and amplitudes of the applied voltages, the beam with its focal zone can be moved in a plane to scan the object. In the case of a linear array, a focused beam directed normal to the array is scanned across the object by translating the aperture  
25 across the array from one firing to the next.

The same principles apply when the transducer probe is employed to receive the reflected sound in a receive mode. The voltages produced at the receiving transducer elements are summed so that the net signal  
30 is indicative of the ultrasound reflected from a single focal zone in the object. As with the transmission mode, this focused reception of the ultrasonic energy is achieved by imparting separate time delay (and/or phase shifts) and gains to the signal from  
35 each receiving transducer element. The time delays

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are adjusted with increasing depth of the returned signal to provide dynamic focusing on receive.

In a typical ultrasound system the beamformer control is a significant contributor to the performance and cost of the system. Dynamic receive delay and apodization control must be generated for each beam and channel at a high rate. Often as many as 512 beam channels are required for a high-end system with an update rate as high as 10 MHz. Calculating delays and apodization for an ultrasound beamformer during dynamic reception requires complex calculations including transcendental functions. Normally image quality is traded off for cost by using second or third-order approximations for these functions. Additionally large memories are frequently used to store precalculated controls for predetermined beam positions and parameters. Using stored precalculated values limits the ability of the system to optimally readjust beam position or parameters dependent on scanning situations. Thus image quality is compromised to achieve faster control response times.

There are a wide variety of beamformer control designs currently in use. All use some combination of large parameter random access memories (RAMs), state machines, complex calculations and approximations. Thus they fall short in one or more areas: agility, cost or precision.

Agility means the ability to change the beamforming setup for an entire imaging configuration in a time much less than 1 sec, where the setup includes vector phase center (aperture) positions, steering angles, f-numbers, and focal positions, and the imaging configuration includes all vectors (beams) displayed on the imaging console. Agility also means the ability to begin receive delay computation in mid-

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flight, i.e., immediately before a deep region of interest.

The controllers described in many patents use state machines. Unfortunately these state machines must begin running immediately after transmit. They cannot easily be reloaded for a different receive focus significantly after transmission. For some high-frame-rate applications, particularly for volumetric imaging, it is desirable to start reception just before echoes from a deep region of interest are received. In addition, at least one prior art method uses parameters which are beam and element dependent. This results in an extremely large number of parameters, involving functions such as square root and sine. This makes agility impossible.

Other systems include inherent approximation, which limits the precision of the beamforming time delays. This results in a loss in image quality, most often manifested by poor contrast resolution, i.e., poor ability to detect very subtle differences in tissue-reflected intensities, or in cystic clearing.

More accurate systems use complicated logic to perform the required calculations. Since these circuits must be duplicated according to the number of channels, they can become a significant portion of the cost of high-channel-count systems.

There is a need for a new beamforming architecture which does not require large memories for storing precalculated beamforming values, which works equally well with transducer arrays of any geometry, and which is agile, precise and low in cost.

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## SUMMARY OF THE INVENTION

The present invention is an architecture for calculating beamformer time delays and apodization values in real-time by using a cordic rotator (hereinafter "cordic"), a simple multiplier-less device used for polar-Cartesian conversions. The use of the cordic to directly calculate the root-sum-of-squares without approximation or complex logic provides ideal performance and flexibility at low cost. The system may quickly re-optimize the beam positions and parameters without the need to recalculate large pre-stored memories or use rough approximations.

In accordance with the preferred embodiments of the invention, cordic rotators are utilized in a very agile, efficient and precise method and means for calculating ultrasonic beamforming apodization weightings and time delays. Apodization weightings and time delays are calculated in a real-time, distributed and pipelined manner without the need for large memories or complex state machines. There are no inherent approximations. Precision may be easily controlled to be within the accuracy of the delay apparatus. When a transducer array is attached to the ultrasonic imaging system, the element positions are written into relatively small distributed memories. The element positions do not need to be reloaded except when the array geometry is changed. While imaging, a small number of parameters are broadcast before each transmission and during each reception. These parameters may include: focal position(s), multiplexer state(s), aperture position(s), aperture size(s) and vector angle(s). Simple logic, including cordics, combines these parameters to produce beamforming time delays and apodization. Focal position and apertures may be

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changed very quickly for an entire image, in milli-seconds. The receive focal positions do not need to start at the skin-line or follow a straight line, as required by state machine approaches. Reception focus  
5 can begin in mid-flight, and be warped to compensate for parallel beamforming methods. In addition, the array geometry may take any form; it is not restricted to the conventional linear, convex and phase arrays.

#### BRIEF DESCRIPTION OF THE DRAWINGS

10 FIG. 1 is a block diagram showing a conventional ultrasound imaging system having a beamformer.

FIG. 2 is schematic showing the geometry of an ultrasound transducer array.

15 FIG. 3 is a block diagram showing an agile delay and apodization control architecture in accordance with the preferred embodiments of the invention.

FIG. 4 is a schematic showing coordinate rotation for hypotenuse calculation.

20 FIG. 5 is a schematic showing coordinate rotation for apodization projection.

FIG. 6 is a block diagram showing an  $N$ -stage cordic rotator.

FIG. 7 is a block diagram showing a stage of a cordic rotator.

25 FIG. 8 is a block diagram in two parts (FIGS. 8-1 and 8-2) showing a delay calculator in accordance with the preferred embodiment of the invention.

30 FIG. 9 is a block diagram showing a delay calculator arithmetic logic unit (ALU) in accordance with the preferred embodiment.

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## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention can be incorporated in any ultrasound imaging system employing beamforming. One example of the foregoing is a B-mode ultrasound imaging system, which will be generally described before disclosing in detail the preferred embodiment of the invention.

A conventional B-mode ultrasound imaging system is generally depicted in FIG. 1. The system comprises a transducer array 2 consisting of a plurality of separately driven transducer elements 34, each of which produces a burst of ultrasonic energy when energized by a pulsed waveform produced by a transmitter 8 and sent through a set of transmit/receive (T/R) switches 6 switched to a transmit state and respective switches of a multiplexer 4 switched to a MUX state. The ultrasonic energy reflected back to transducer array 2 from the object under study is converted to an electrical signal by each receiving transducer element 34 and applied separately to a receive beamformer 10 through the multiplexer switches 4 switched to the MUX state and the T/R switches 6 switched to a receive state. Transmitter 8 and receive beamformer 10 are operated under control of a host computer (master controller) 24. A complete scan is performed by acquiring a series of echoes in which transmitter 8 is gated ON momentarily to energize each transducer element 34 in the transmit aperture, and the subsequent echo signals produced by each transducer element 34 are applied to receive beamformer 10. The receive beamformer 10 combines the separate echo signals from each transducer element 34 to produce a single echo signal which is used to produce a line in an image on a display monitor 22.

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The receive beamformer's signal inputs are the low-level analog RF signals from the transducer elements 34. The receive beamformer is responsible for analog-to-digital conversion and for receive beamforming. In baseband imaging systems, the beamsummed signal is output to a demodulator 12, which converts the beamsummed signal into baseband in-phase  $I$  and quadrature  $Q$  receive beams. The  $I$  and  $Q$  acoustic data vectors from the demodulator 12 are sent to respective FIR filters 14 which are programmed with filter coefficients to pass a band of frequencies preferably centered at the fundamental frequency  $f_0$  of the transmit waveform or a (sub)harmonic frequency thereof.

In the case of a B-mode imaging system, vectors of filtered  $I$  and  $Q$  acoustic data are sent to a B-mode processor 16, which converts the  $I$  and  $Q$  acoustic data into a log-compressed version of the signal envelope. The B-mode function images the time-varying amplitude of the envelope of the signal as a gray scale. The envelope of a baseband signal is the magnitude of the vector which  $I$  and  $Q$  represent. The  $I, Q$  phase angle is not used in the B-mode display. The magnitude (i.e., intensity) of the signal is the square root of the sum of the squares of the orthogonal components, i.e.,  $(I^2 + Q^2)^{1/2}$ .

The B-mode amplitude data is output to a scan converter 18 comprising an acoustic line memory followed by an X-Y display memory. The acoustic line memory accepts the processed vectors of amplitude data and interpolates where necessary, and also performs the coordinate transformation of the amplitude data from polar coordinate ( $R-\theta$ ) sector format or Cartesian coordinate linear format to appropriately scaled Cartesian coordinate display pixel intensity data, which is stored in the X-Y display memory.

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The scan-converted frames are passed to a video processor 20, which converts the pixel intensity data to the video frame rate and then maps the pixel intensity data to a gray-scale mapping for video display. A conventional ultrasound imaging system typically employs a variety of gray maps, which are simple transfer functions of the raw intensity data to display gray-scale levels. The gray-scale image frames are then sent to the display monitor 22 for display.

The ultrasound image produced by the system shown in FIG. 1 is composed of multiple image scan lines. A single scan line (or small localized group of scan lines) is acquired by transmitting focused ultrasound energy at a point in the region of interest, and then receiving the reflected energy over time. The focused transmit energy is referred to as a transmit beam. During the time after transmit, one or more receive beamformers coherently sum the energy received by each channel, with dynamically changing phase rotation or delays, to produce peak sensitivity along the desired scan lines at ranges proportional to the elapsed time. The resulting focused sensitivity pattern is referred to as a receive beam. A scan line's resolution is a result of the directivity of the associated transmit and receive beam pair.

The purpose of the beamformer is to provide maximum transmitted intensity and receive sensitivity at the desired focal point(s) in space with minimum intensity/sensitivity away from the focal point(s). To do this, a beamformer must precisely calculate time delays which correspond to the difference in the propagation time of sound between the focal point(s) and elements of a transducer array. Typically the receive beamforming time delays are adjusted dynam-

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ically during reception. This allows the focal points to track the depth of the objects producing the received echoes. This depth is proportional to the time after transmission.

5 A typical transducer array geometry is shown in FIG. 2. In this example the elements of the array and the focal points all lie within a single plane in three-dimensional space. Thus one can describe the geometry in two dimensions:  $x$  and  $z$ , where the  $x$  axis  
10 is tangential to the center of the array face and the  $z$  axis is orthogonal to the  $x$  axis. The elements in the array are indexed by the letter "i". The position of each  $i$ -th element is indicated by its coordinates in  $x$  (azimuthal) and  $z$  (axial):  $Elx_i$  and  $Elz_i$ , respec-  
15 tively. The vector along which the focal points lie may be described by an angle  $\beta$ , relative to the  $z$  axis. The position of the focal point, as a function of time, is indicated by coordinates  $Focx(t)$  and  $Focz(t)$ . According to the Pythagoras Theorem, the  
20 propagation path length  $D_i(t)$  is then:

$$D_i(t) = \text{hypot}[(Elx_i - Focx(t)), (Elz_i - Focz(t))] \quad (1)$$

where  $\text{hypot}(x,y)$  is a function that calculates the hypotenuse of the two orthogonal lengths as defined below:

$$\text{hypot}(x,y) \equiv \sqrt{x^2 + y^2} \quad (2)$$

Some transducer arrays, referred to as 2D arrays, have  
25 elements out of the  $x$ - $z$  plane, in the elevational or  $y$  direction. For these arrays the geometry must be extended with a  $y$  axis orthogonal to the  $x$ - $z$  plane, with the positive direction pointing out of the plane of FIG. 1. The element position needs the additional  
30 coordinate of  $Ely_i$ . In addition, some modern systems acquire data in a 3D volume where focal points may

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also be out of the x-z plane. Thus the additional coordinate of  $Focy(t)$  is required. In this more generalized case, the propagation path length  $D_i(t)$  is

$$D_i(t) = \text{hypot}(\text{hypot}[(Elx_i - Focx(t)), (Elz_i - Focz(t))], (Ely_i - Focy(t))) \quad (3)$$

When an ultrasound imaging system is scanning, the receive focal point progresses from a point on the array face, along a line through the volume being imaged. This line is called a vector or beam. The point on the array face, at the intersection of the vector and the array, is called the vector phase center. The distance from the phase center to the focal point is  $r(t)$ .

The beamformer delays the signals at each transducer element by a time  $T_i(t)$  to compensate for the differences in propagation times. The propagation time is simply the propagation path distance divided by the speed of sound  $c$  (approximately 1.54 mm/ $\mu$ sec in tissue). Because the focal point is a function of time in reception, the delays are also a function of time. However, the delay at the phase center is kept constant to ensure a linear relationship between the depth of an object along the vector and the output of the corresponding echo signal from the beamformer. In addition, an offset delay is added to ensure the applied beamforming time delays are positive, a requirement to be causal. The beamforming delays are thus:

$$T_i(t) = T_{\text{offset}} + \frac{r(t)}{c} - \frac{D_i(t)}{c} \quad (4)$$

or

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$$T_i(t) = R_{\text{offset}}(t) + - \frac{D_i(t)}{C} \quad (5)$$

where

$$R_{\text{offset}}(t) = T_{\text{offset}} + \frac{r(t)}{C} \quad (6)$$

In addition to delays, the beamformer must provide apodization weightings or values which control the size and shading of the array active aperture. Apodization is applied according to the projection of the array onto a plane orthogonal to the vector. The apodization value for a particular element is determined by the projected distance from the center of the aperture divided by the projected aperture size. The aperture size and center may be controlled according to desired effective f-numbers and acceptance angles.

A preferred embodiment of the invention, shown in FIG. 3, includes a plurality of delay calculators 28 distributed throughout the beamformer. Each delay calculator provides beamforming delays and apodization for a plurality of channels (32)/elements (34) via a channel control bus 30. The delay calculators are initialized with element position coordinates. Then, while imaging, focal coordinates and steering angles are broadcast to all delay calculators. All parameters may be provided to the delay calculators over a single beamformer control bus 26. The delay calculator uses a cordic to perform the aperture projections and carry out the hypot function. The cordic provides a very efficient and accurate means of performing the projection and calculating the hypotenuse. It performs successive coordinate transformations, in two dimensions, using coefficients that are simple powers of two. Thus it requires a small number of bit shifts and adds. It is pipelined, allowing

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high throughput. The resulting apodization values and time delays are then provided by a channel control bus 30 to a plurality of channels 32.

Referring to FIG. 4, a hypotenuse can be calculated by first taking the absolute value of the coordinates, to put it in the first quadrant, then using the cordic to rotate it onto the  $x'$  axis (aligned with the hypotenuse to be calculated) and output the resulting  $x'$  value.

An apodization projection can be performed by simply rotating the coordinate system (see FIG. 5) about the origin by an angle  $-\beta$ , so that the  $z'$  axis is parallel with the vector. The transformed element  $x$  coordinates,  $Elx'_i$ , then provide the element position in the projection plane.

The necessary calculation for apodization is the distance of an element from the aperture center,  $ACx'$ , in the projection. Referring to FIG. 5, this distance is:

$$Ap_{x_i} = ACx' + Elx_i \quad (7)$$

The aperture center  $ACx'$  and the inverse aperture  $iAp$  are other parameters broadcast to all delay calculators. The product of  $Ap_{x_i}$  and the inverse aperture  $iAp$  is used to index a window function comprising a table of shading (apodization) values.

A hypotenuse in three dimensions may be calculated by two successive cordics. The first transforms  $x$  and  $z$  to a rotated coordinate system,  $x'$  and  $z'$ . The second then rotates  $x'$  and  $y$  to  $x''$  and  $y''$ . The first cordic calculates the hypotenuse in the  $x$ - $z$  plane by rotating it onto  $x'$ , and the second cordic calculates the three-dimensional hypotenuse, now in the  $x'$ - $y$  plane, by rotating it onto  $x''$ . Similarly the apodization projection may be provided by first rotating the

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x and z axes about the y axes, and then rotating the y and x' axes about the z axis.

A cordic is composed of N stages as seen in FIG. 6. Given a stage index k = 0 to N-1, the coordinate transformation performed by each stage 36 of a cordic is:

$$\begin{bmatrix} x_{k+1} \\ z_{k+1} \end{bmatrix} = \begin{bmatrix} 1 & s_k 2^{-k} \\ -s_k 2^{-k} & 1 \end{bmatrix} \begin{bmatrix} x_k \\ z_k \end{bmatrix} \quad (8)$$

where  $s_k = \pm 1$ . This matrix multiplication is easily implemented with two adder/subtractors, as shown in FIG. 7. It produces a coordinate rotation of

$$\theta_k = -s_k \arctan(2^{-k}) \quad (9)$$

and a magnification by

$$M_k = \text{hypot}(1, 2^{-k}) \quad (10)$$

The total rotation after N stages is

$$\theta = \sum_{k=0}^{N-1} \theta_k \quad (11)$$

and the total magnification is

$$M = \prod_{k=0}^{N-1} M_k \quad (12)$$

The cordic shown in FIG. 7 can perform two functions: rotation of any input coordinates to the x' axis and rotation by a desired angle. The "rotate" control signal in FIG. 7 selects which of the two functions is performed.

When "rotate" is set to 1, the cordic rotates the inputs by an angle corresponding to the N sign bits,  $s_0$  through  $s_{N-1}$ , provided at the input. This is used to project element positions onto a rotated axis for

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apodization. The rotate sign bits may be calculated according to the vector angle  $\beta$  prior to transmit and broadcast, as AngS, to all delay calculators 28 via the beamformer control bus 32 (see FIG. 3).

5       When "rotate" is zero, the cordic rotates the coordinates to the  $x'$  axis to provide the hypotenuse as  $x'$ . This is done by setting the sign bit  $s_k$  at each stage to the sign bit of the input  $z_k$ . Thus the direction of rotation is always toward the  $x'$  axis.  
10 With each successive stage the angle of rotation becomes smaller and the hypotenuse asymptotically approaches the  $x'$  axis. The final  $x'$  output will be equal to the hypotenuse magnified by  $M$ , with the maximum remaining error determined by the smallest  
15 angle:

$$E_{\max} = h_{\max} \times (1 - \cos(\theta_{N-1})) \approx h_{\max} \times 2^{-2N+1} \quad (13)$$

where  $E_{\max}$  is the maximum remaining error and  $h_{\max}$  is the maximum hypotenuse. Given a maximum hypotenuse of 200  $\mu$ sec and a maximum delay error of 6.25 nsec, an  $N = 8$  stage cordic is sufficient. The magnification factor  
20 is constant, independent of the angle of rotation; prescaling the inputs by  $1/M$  provides an output with the correct scale.

This invention provides all of the advantages of the prior art with none of the disadvantages. It is  
25 agile, simple, and accurate. There are no vector- and element-dependent parameters. Vector-dependent parameters are element independent. Element-dependent parameters are vector independent. The resulting small number of parameters allow for quick reprogram-  
30 ming. In addition, because there is no state machine, delay computation may begin anywhere along the vector. The cordic is inherently pipelined and extremely simple. It requires only a small number of adds/sub-

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tracts. Its precision is determined by the number of stages with no underlying approximation.

In accordance with the preferred embodiment shown in FIG. 3, the delay calculators 28 receive all the  
5 required parameters over a beamformer control bus 26. This control bus requires at least 16 data bits, 13 address bits and a "Start" bit. The "Start" signal resets the calculators for the beginning of a new vector. Transducer array geometry parameters are  
10 written before scanning, while vector parameters are written synchronous with scanning. For dynamic reception, this bus should run at 15 MHz. (For dual parallel beam reception, a 30-MHz bus or separate 15-MHz busses are required). Separate, but nearly  
15 identical, control structures and busses may be used for transmit and receive.

There are three element position parameters required per element/channel combination, when a transducer is activated:  $(Elx_i, Elz_i, Ely_i)$ . There are  
20 eight vector parameters which are updated during scanning: the focus position  $(FocX, FocZ, FocY)$ , the range offset  $(R_{offset})$ , the aperture center  $(ACx')$ , the inverse aperture size  $(iAp)$ , the multiplexer state (MUX State), and the vector angle sign bits (AngS).  
25 For dynamic receive beamforming, the first six are updated during reception. If they are updated at a 2.5 MHz rate, then the resulting 2.5-MHz beamforming delay output can be linearly interpolated with adequate precision. This dictates the 15-MHz bus speed.

30 The MUX State is required when a multiplexer is used to connect different physical element(s) to individual channels. This is typical for large linear or convex transducers where the number of elements exceeds the number of beamforming channels. The  
35 element position corresponding to each delay channel

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then depends on the MUX State.

Each delay calculator 28 outputs delay and apodization information to a respective plurality of beamformer channels 32 through a respective channel control bus 30. For a 16-channel, single-beam delay calculator, this bus should have 16 data bits, 5 address bits and a "Strt" signal. The delay calculator outputs delay and apodization data interleaved by channel. Providing a 2.5 MHz update per channel, for 16 channels, requires a 40-MHz bus. Four address bits index the channels and one address bit indicates delay or apodization.

A preferred embodiment of the delay calculator is shown in composite FIG. 8 (consisting of FIGS. 8-1 and 8-2). This embodiment of the delay calculator provides delay and apodization for 16 channels. Four relatively small random access memories (RAMs) are used to store information about the activated array. This delay calculator provides 256 possible MUX states with a maximum of four physical elements associated with each channel. A "MUX" RAM 64 stores a 2-bit value to indicate which of the four available elements is connected to each channel per MUX state. Three "Chn" RAMs 66, 68 and 70 contain the coordinates for each of the four associated physical elements per channel. This two-step structure provides complete flexibility for multiplexer designs without large memories.

The delay calculator loops through 16 channels at a 40 MHz rate so that delays for all channels may be calculated at the required 2.5 MHz rate. This is done with a 4-bit up counter 58 (see FIG. 8-1), initialized with the "Start" signal. The "Start" signal is also received by a delay circuit 60. The up counter 58 outputs a 4-bit channel index (labeled "Channel" in

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FIG. 8) to the "Chn" RAMs 66, 68 and 70 and to another delay circuit 62. The delay circuits 60 and 62 respectively output delayed versions of the "Start" and "Channel" signals (labeled "Strt" and "Chn", respectively, in FIG. 8-1). The "Strt" and "Chn" signals are output aligned with the corresponding delay and apodization data.

The 4-bit channel index is combined with an 8-bit MUX State signal to look up the element index from the "MUX" RAM 64. The resulting two-bit element index is combined with the 4-bit channel index to look up the physical element coordinates in the "Chn" RAMs 66, 68 and 70.

The "Start" signal triggers a brief initialization, followed by the pipelined delay and apodization calculation. The initialization provides for setup of the "MUX" RAM 64 and an element projection ("PROJ") RAM 92 (see FIG. 8-2).

The first loop through the 16 channels, after "Start", is used to setup the element projection RAM 92 for apodization. During initialization the element positions from "Chn" RAMs 66, 68 and 70 are passed directly to the cordics via line B and multiplexer 110 (see FIG. 9) of the respective ALUs 78, 80 and 82, and the controls for the cordics 84 and 86 are set to perform a fixed-angle rotation according to AngS. The results are stored in the projection RAM 92. A second loop through the 16 channels may be used to prepare the pipes for dynamic calculations. The total initialization time is less than 0.5  $\mu$ sec. Synchronizing the cordic controls with the pipeline can eliminate the need for the extra loop, reducing initialization to 0.25  $\mu$ sec.

After initialization the delay calculator begins updating the dynamic parameters and producing dynamic

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delays and apodization. For delay (see FIG. 8-1), the focus coordinates from registers 72 and 74 are respectively subtracted in ALUs 78 and 80 from the element coordinates from "ChnX" RAM 66 and "ChnZ" RAM 68 and the absolute values of the coordinate differences  $x$  and  $z$  are fed to cordic 84, and the focus coordinates from register 76 are subtracted in ALU 82 from the element coordinates from "ChnY" RAM 70 and the absolute value of the difference  $\bar{y}$  is fed to cordic 88, along with the output of cordic 84. These operations performed by each ALU are depicted in FIG. 9 by adder/subtractor 106 and absolute value block 108. The adder/subtractor 106 receives the focus coordinate via line A and the element position coordinate via line B. The multiplexer 110 is switched to pass the absolute value to the respective cordic.

The first cordic 84 transforms  $x$  and  $z$  to a rotated coordinate system,  $x'$  and  $z'$ . The second cordic 86 then rotates  $x'$  and  $y$  to  $x''$  and  $y''$ . The first cordic 84 calculates the hypotenuse in the  $x$ - $z$  plane by rotating it onto  $x'$ , and the second cordic 86 calculates the three-dimensional hypotenuse, now in the  $x'$ - $y$  plane, by rotating it onto  $x''$ . The calculated hypotenuse corresponds to the propagation time. The range offset time ( $R_{\text{offset}}$ ) from register 88 is subtracted from the output of cordic 86 in adder 90 to produce the delay.

For apodization, the aperture center ( $A_{px'}$ ) from register 94 is subtracted in adder 96 from the element positions read from the projection RAM 92, in accordance with Eq. (7). The absolute value (block 98) of the resulting distance  $A_{px'}$  is multiplied by the inverse aperture size ( $iAP$ ) from register 100 by multiplier 102. The resulting product is used to index a window function table in "window" RAM 104,

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which produces an 8-bit shading (i.e., apodization) value. The "window" RAM 104 preferably stores a bank of window function tables, with one table be selected by the input "BANK".

5       The focus and element coordinates should all be expressed in 6.25 nsec units, pre-scaled by  $1/M$ . Providing additional fractional bits can help maintain precision. The  $R_{\text{offset}}$  is not prescaled by  $1/M$  since it is after the cordics.

10       Although the preferred embodiment has been disclosed in the context of a receive beamformer, it will be readily appreciated that the invention also has application in transmit beamforming. To generally depict a transmit beamformer in accordance with  
15 another preferred embodiment of the invention, one need merely substitute pulsing circuits for the receive channels shown in FIG. 3.

      The foregoing preferred embodiments have been disclosed for the purpose of illustration. Variations  
20 and modifications of the basic concept of the invention will be readily apparent to those skilled in the art. All such variations and modifications are intended to be encompassed by the claims set forth hereinafter.

25       The phrase "as a function of", as used in the claims, is not to be construed to mean "as a function of only" what follows. For example, in accordance with the foregoing definition, the phrase "determine  
30  $y$  as a function of  $x$ " would read on all cases where  $y$  was determined as a function of  $x$  alone or as a function of  $x$  and one or more other variables, e.g.,  $z$ .

## CLAIMS

1. A beamforming system comprising:  
a transducer array comprising a multiplicity of transducer elements arranged in a plane having x and z coordinate axes; and  
5 a beamformer comprising a multiplicity of receive channels respectively operatively coupled to said multiplicity of transducer elements, first memory storing x and z coordinates of a focal position, second memory storing respective sets of coordinates  
10 of respective positions of said multiplicity of transducer elements, each coordinate set comprising an x coordinate and a z coordinate, a first adding/subtracting circuit connected to said first and second memories for forming respective x coordinate differ-  
15 ences between said x coordinate of said focal position and respective x coordinates of said element positions, a second adding/subtracting circuit connected to said first and second memories for forming respec-  
20 tive z coordinate differences between said z coordinate of said focal position and respective z coordinates of said element positions, a cordic rotator connected to said first and second adding/subtracting circuits for performing coordinate transformations of the outputs of said first and second adding/subtract-  
25 ing circuits, and a time delay generator for applying respective time delays to respective receive channels, each time delay being a function of a respective output of said cordic rotator.
2. The beamforming system as recited in claim 1, wherein said cordic rotator calculates a respective hypotenuse as a function of respective x and z coordinate differences and respective sign bits of

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5    respective  $z$  coordinates when said cordic rotator is  
      in a first state.

      3. The beamforming system as recited in claim 1,  
      wherein said cordic rotator performs a respective  
      apodization projection as a function of respective  $x$   
      and  $z$  element positions and respective rotate sign  
5    bits which are a function of a vector angle  $\beta$  when  
      said cordic rotator is in a second state.

      4. The beamforming system as recited in claim 2,  
      wherein said time delay generator applies time delays  
      which are a function of respective hypotenuses and a  
      range offset.

      5. The beamforming system as recited in claim 3,  
      further comprising an apodization value generator for  
      applying respective apodization values to respective  
      receive channels, each apodization value being a  
5    function of a respective apodization projection, an  
      aperture center and an inverse aperture size.

      6. The beamforming system as recited in claim 5,  
      wherein said apodization value generator comprising  
      third memory storing at least one window function  
      table.

      7. The beamforming system as recited in claim 1,  
      further comprising a counter for reading said respec-  
      tive sets of  $x$  and  $z$  element position coordinates out  
      of said second memory in succession.

      8. The beamforming system as recited in claim 1,  
      wherein said cordic rotator comprises a plurality of  
      successive stages, each stage performing a coordinate

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transformation that rotates the inputs to that stage,  
 5 the angle of rotation becoming smaller for each successive stage.

9. The beamforming system as recited in claim 8, wherein the number of stages in said cordic rotator is  $N$ , and given a stage index  $k = 0$  to  $N - 1$ , each stage performs the coordinate transformation:

$$\begin{bmatrix} x_{k+1} \\ z_{k+1} \end{bmatrix} = \begin{bmatrix} 1 & s_k 2^{-k} \\ -s_k 2^{-k} & 1 \end{bmatrix} \begin{bmatrix} x_k \\ z_k \end{bmatrix}$$

5 where  $s_k = \pm 1$ .

10. The beamforming system as recited in claim 1, further comprising a multiplexer comprising a multiplicity of multiplexing switches having switching states determined by a MUX state, wherein said beam-  
 5 former further comprises third memory for storing said MUX state, said second memory having inputs operatively coupled to outputs from said third memory.

11. A beamforming system comprising:  
 a transducer array comprising a multiplicity of transducer elements arranged in a three-dimensional space having  $x$ ,  $y$  and  $z$  coordinate axes; and  
 5 a beamformer comprising a multiplicity of receive channels respectively operatively coupled to said multiplicity of transducer elements, first memory storing  $x$ ,  $y$  and  $z$  coordinates representing a focal position, second memory storing respective sets of  
 10 coordinates representing the respective positions of said multiplicity of transducer elements, each coordinate set comprising an  $x$  coordinate, a  $y$  coordinate and a  $z$  coordinate, a first adding/subtracting circuit connected to said first and second memories for form-

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15 ing respective x coordinate differences between said  
x coordinate of said focal position and respective x  
coordinates of said element positions, a second  
adding/subtracting circuit connected to said first and  
second memories for forming respective y coordinate  
20 differences between said y coordinate of said focal  
position and respective y coordinates of said element  
positions, a third adding/subtracting circuit con-  
nected to said first and second memories for forming  
respective z coordinate differences between said z  
25 coordinate of said focal position and respective z  
coordinates of said element positions, a first cordic  
rotator connected to said first and second adding/sub-  
tracting circuits for performing coordinate trans-  
formations of the outputs of said first and second  
30 adding/subtracting circuits, a second cordic rotator  
connected to said first cordic rotator and to said  
third adding/subtracting circuits for performing  
coordinate transformations of the outputs of said  
first cordic rotator and said third adding/subtracting  
35 circuit, and a time delay generator for applying  
respective time delays to respective receive channels,  
each time delay being a function of a respective  
output of said second cordic rotator.

12. The beamforming system as recited in claim  
11, further comprising an apodization value generator  
for applying respective apodization values to  
respective receive channels, each apodization value  
5 being a function of a respective output of said second  
cordic rotator.

13. A beamforming system comprising:  
a transducer array comprising a multiplicity of  
transducer elements arranged in a plane having x and

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z coordinate axes; and

5 a beamformer comprising a multiplicity of pulsing circuits respectively operatively coupled to said multiplicity of transducer elements, first memory storing x and z coordinates of a focal position, second memory storing respective sets of coordinates  
10 of respective positions of said multiplicity of transducer elements, each coordinate set comprising an x coordinate and a z coordinate, a first adding/subtracting circuit connected to said first and second memories for forming respective x coordinate differ-  
15 ences between said x coordinate of said focal position and respective x coordinates of said element positions, a second adding/subtracting circuit connected to said first and second memories for forming respective z coordinate differences between said z coordi-  
20 nate of said focal position and respective z coordinates of said element positions, a cordic rotator connected to said first and second adding/subtracting circuits for performing coordinate transformations of the outputs of said first and second adding/subtract-  
25 ing circuits, and a time delay generator for applying respective time delays to respective pulsing circuits, each time delay being a function of a respective output of said cordic rotator.

14. The beamforming system as recited in claim 13, further comprising an apodization value generator for applying respective apodization values to  
5 respective pulsing circuits, each apodization value being a function of a respective output of said cordic rotator.

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15. A beamforming system comprising:  
a transducer array comprising a multiplicity of  
transducer elements arranged in a three-dimensional  
space having  $x$ ,  $y$  and  $z$  coordinate axes; and  
5 a beamformer comprising a multiplicity of pulsing  
circuits respectively operatively coupled to said  
multiplicity of transducer elements, first memory  
storing  $x$ ,  $y$  and  $z$  coordinates representing a focal  
position, second memory storing respective sets of  
10 coordinates representing the respective positions of  
said multiplicity of transducer elements, each coordinate set comprising an  $x$  coordinate, a  $y$  coordinate  
and a  $z$  coordinate, a first adding/subtracting circuit  
connected to said first and second memories for forming  
15 respective  $x$  coordinate differences between said  
 $x$  coordinate of said focal position and respective  $x$   
coordinates of said element positions, a second  
adding/subtracting circuit connected to said first and  
second memories for forming respective  $y$  coordinate  
20 differences between said  $y$  coordinate of said focal  
position and respective  $y$  coordinates of said element  
positions, a third adding/subtracting circuit connected to said first and second memories for forming  
respective  $z$  coordinate differences between said  $z$   
25 coordinate of said focal position and respective  $z$   
coordinates of said element positions, a first cordic  
rotator connected to said first and second adding/sub-  
tracting circuits for performing coordinate trans-  
formations of the outputs of said first and second  
30 adding/subtracting circuits, a second cordic rotator  
connected to said first cordic rotator and to said  
third adding/subtracting circuits for performing  
coordinate transformations of the outputs of said  
first cordic rotator and said third adding/subtracting  
35 circuit, and a time delay generator for applying

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respective time delays to respective pulsing circuits, each time delay being a function of a respective output of said second cordic rotator.

16. The beamforming system as recited in claim 11, further comprising an apodization value generator for applying respective apodization values to respective pulsing circuits, each apodization value  
5 being a function of a respective output of said second cordic rotator.

17. An imaging system comprising:  
a transducer array comprising a multiplicity of transducer elements arranged in a plane having x and z coordinate axes;  
5 a first delay calculator for calculating a first set of respective receive time delays as a function of a focal position and respective positions of a first set of said transducer elements;  
a transmit beamformer programmed to activate said  
10 transducer array to transmit a focused ultrasound beam;  
a receive beamformer comprising a first set of receive channels for converting respective analog signals from said first set of transducer elements  
15 into respective vectors of digital samples, a first channel control bus for applying said first set of respective receive time delays to said respective vectors of digital samples in said first set of receive channels, and a beamsummer for summing at  
20 least said time-delayed vectors of digital samples from said first set of receive channels to produce a net receive signal;  
a processor for deriving an image signal from said net receive signal; and

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25 a display device for displaying an image having  
an image portion which is a function of said image  
signal,  
wherein said first delay calculator comprises a  
first cordic rotator for calculating respective  
30 hypotenuses as a function of said focal position and  
said respective positions of said first set of  
transducer elements in a first cordic rotator state,  
and a first time delay generator for outputting said  
first set of respective receive time delays to said  
35 first channel control bus, each receive time delay of  
said first set being a function of a respective  
hypotenuse output by said first cordic rotator.

18. The imaging system as recited in claim 17,  
further comprising a second delay calculator for  
calculating a second set of respective receive time  
delays as a function of said focal position and  
5 respective positions of a second set of said trans-  
ducer elements, wherein said receive beamformer  
further comprises a second set of receive channels for  
converting respective analog signals from said second  
set of transducer elements into respective vectors of  
10 digital samples, and a second channel control bus for  
applying said second set of respective receive time  
delays to said respective vectors of digital samples  
in said second set of receive channels, and said  
second delay calculator comprises a second cordic  
15 rotator for calculating respective hypotenuses as a  
function of said focal position and said respective  
positions of said second set of transducer elements,  
and a second time delay generator for outputting said  
second set of respective receive time delays to said  
20 second channel control bus, each receive time delay of  
said second set being a function of a respective

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hypotenuse output by said second cordic rotator.

19. The imaging system as recited in claim 18, further comprising a computer for generating a set of vector parameters, and a beamformer control bus for distributing said set of vector parameters to said  
5 first and second time delay calculators, said first and second sets of receive time delays being a function of said vector parameters.

20. The imaging system as recited in claim 17, wherein said first cordic rotator performs respective apodization projections as a function of said focal position and said respective positions of said first  
5 set of transducer elements in a second cordic rotator state, and said first delay calculator further comprises an apodization value generator for applying respective receive apodization values to said first set of respective receive channels, each receive  
10 apodization value being a function of a respective apodization projection.

21. An imaging system comprising:  
a transducer array comprising a multiplicity of transducer elements arranged in a three-dimensional space having  $x$ ,  $y$  and  $z$  coordinate axes; and  
5 a first delay calculator for calculating a first set of respective receive time delays as a function of a focal position and respective positions of a first set of said transducer elements;  
a transmit beamformer programmed to activate said  
10 transducer array to transmit a focused ultrasound beam;  
a receive beamformer comprising a first set of receive channels for converting respective analog

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signals from said first set of transducer elements  
15 into respective vectors of digital samples, a first  
channel control bus for applying said first set of  
respective receive time delays to said respective  
vectors of digital samples in said first set of  
receive channels, and a beamsummer for summing at  
20 least said time-delayed vectors of digital samples  
from said first set of receive channels to produce a  
net receive signal;

a processor for deriving an image signal from  
said net receive signal; and

25 a display device for displaying an image having  
an image portion which is a function of said image  
signal,

wherein said first delay calculator comprises  
first and second cordic rotators connected in series  
30 for calculating respective hypotenuses as a function  
of said focal position and said respective positions  
of said first set of transducer elements in a first  
cordic rotator state, and a first time delay generator  
for applying said first set of respective receive time  
35 delays to said first channel control bus, each receive  
time delay of said first set being a function of a  
respective hypotenuse output by said second cordic  
rotator.

22. The imaging system as recited in claim 21,  
further comprising a second delay calculator for  
calculating a second set of respective receive time  
delays as a function of said focal position and  
5 respective positions of a second set of said trans-  
ducer elements, wherein said receive beamformer fur-  
ther comprises a second set of receive channels for  
converting respective analog signals from said second  
set of transducer elements into respective vectors of

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10 digital samples, and a second channel control bus for  
applying said second set of respective receive time  
delays to said respective vectors of digital samples  
in said second set of receive channels, and said  
second delay calculator comprises a second cordic  
15 rotator for calculating respective hypotenuses as a  
function of said focal position and said respective  
positions of said second set of transducer elements,  
and a second time delay generator for outputting said  
second set of respective receive time delays to said  
20 second channel control bus, each receive time delay of  
said second set being a function of a respective  
hypotenuse output by said second cordic rotator.

23. The imaging system as recited in claim 22,  
further comprising a computer for generating a set of  
vector parameters, and a beamformer control bus for  
distributing said set of vector parameters to said  
5 first and second time delay calculators, said first  
and second sets of receive time delays being a func-  
tion of said vector parameters.

24. The imaging system as recited in claim 21,  
wherein said first cordic rotator performs respective  
apodization projections as a function of said focal  
position and said respective positions of said first  
5 set of transducer elements in a second cordic rotator  
state, and said first delay calculator further com-  
prises an apodization value generator for applying  
respective receive apodization values to said first  
channel control bus, each receive apodization value  
10 being a function of a respective apodization  
projection.

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25. An imaging system comprising:
- a transducer array comprising a multiplicity of transducer elements arranged in a plane having x and z coordinate axes;
  - 5 a delay calculator for calculating a set of respective transmit time delays as a function of a focal position and respective positions of said transducer elements;
  - a transmit beamformer programmed with transmit  
10 time delays to activate said transducer array to transmit an ultrasound beam focused at said focal position, said transmit beamformer comprising a multiplicity of pulsing circuits for activating respective transducer elements, and a channel control  
15 bus for applying said set of respective transmit time delays to respective pulsing circuits;
  - a receive beamformer comprising a multiplicity of receive channels for converting respective analog signals from respective transducer elements into  
20 respective vectors of digital samples and applying respective time delays to respective vectors, and a beamsummer for summing said time-delayed vectors of digital samples from said multiplicity of receive channels to produce a net receive signal;
  - 25 a processor for deriving an image signal from said net receive signal; and
  - a display device for displaying an image having an image portion which is a function of said image signal,
  - 30 wherein said delay calculator comprises a cordic rotator for calculating respective hypotenuses as a function of said focal position and said respective positions of said transducer elements in a first cordic rotator state, and a time delay generator for  
35 outputting said set of respective transmit time delays

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to said channel control bus, each transmit time delay being a function of a respective hypotenuse output by said cordic rotator.

26. The imaging system as recited in claim 25, wherein said cordic rotator performs respective apodization projections as a function of said focal position and said respective positions of said transducer elements in a second cordic rotator state, and said delay calculator further comprises an apodization value generator for applying respective transmit apodization values to said channel control bus, each transmit apodization value being a function of a respective apodization projection.

27. An imaging system comprising:  
a transducer array comprising a multiplicity of transducer elements arranged in a three-dimensional space having x, y and z coordinate axes; and  
a delay calculator for calculating a set of respective transmit time delays as a function of a focal position and respective positions of said transducer elements;  
a transmit beamformer programmed with transmit time delays to activate said transducer array to transmit an ultrasound beam focused at said focal position, said transmit beamformer comprising a multiplicity of pulsing circuits for activating respective transducer elements, and a channel control bus for applying said set of respective transmit time delays to respective pulsing circuits;  
a receive beamformer comprising a multiplicity of receive channels for converting respective analog signals from respective transducer elements into respective vectors of digital samples and applying

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respective time delays to respective vectors, and a beamsummer for summing said time-delayed vectors of digital samples from said multiplicity of receive channels to produce a net receive signal;

25 a processor for deriving an image signal from said net receive signal; and

a display device for displaying an image having an image portion which is a function of said image signal,

30 wherein said delay calculator comprises first and second cordic rotators connected in series for calculating respective hypotenuses as a function of said focal position and said respective positions of said transducer elements in a first cordic rotator state, and a time delay generator for outputting said  
35 set of respective transmit time delays to said channel control bus, each transmit time delay being a function of a respective hypotenuse output by said second cordic rotator.

28. The imaging system as recited in claim 27, wherein said first and second cordic rotators perform respective apodization projections as a function of said focal position and said respective positions of  
5 said transducer elements in a second cordic rotator state, and said delay calculator further comprises an apodization value generator for applying respective transmit apodization values to said channel control bus, each transmit apodization value being a function  
10 of a respective apodization projection.

29. A beamforming system comprising:  
a transducer array comprising a multiplicity of transducer elements arranged in a plane having x and z coordinate axes; and

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5 a delay calculator for calculating a set of  
respective time delays as a function of a focal  
position and respective positions of said transducer  
elements; and

10 a beamformer comprising a multiplicity of  
channels operatively coupled to said multiplicity of  
transducer elements and a channel control bus for  
applying said set of respective time delays to signals  
in said respective channels;

15 wherein said delay calculator comprises a cordic  
rotator for calculating respective hypotenuses as a  
function of said focal position and said respective  
positions of said transducer elements in a first  
cordic rotator state, and a time delay generator for  
outputting said set of respective time delays to said  
20 channel control bus, each time delay being a function  
of a respective hypotenuse output by said cordic  
rotator.

30. The beamforming system as recited in claim  
29, wherein said cordic rotator performs respective  
apodization projections as a function of said focal  
position and said respective positions of said trans-  
5 ducer elements in a second cordic rotator state, and  
said delay calculator further comprises an apodization  
value generator for applying respective apodization  
values to said channel control bus, each apodization  
value being a function of a respective apodization  
10 projection.

31. A beamforming system comprising:

a transducer array comprising a multiplicity of  
transducer elements arranged in a three-dimensional  
space having  $x$ ,  $y$  and  $z$  coordinate axes; and

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5 a delay calculator for calculating a set of  
respective time delays as a function of a focal  
position and respective positions of said transducer  
elements; and

10 a beamformer comprising a multiplicity of  
channels operatively coupled to said multiplicity of  
transducer elements and a channel control bus for  
applying said set of respective time delays to signals  
in said respective channels;

15 wherein said delay calculator comprises first and  
second cordic rotators connected in series for  
calculating respective hypotenuses as a function of  
said focal position and said respective positions of  
said transducer elements in a first cordic rotator  
state, and a time delay generator for outputting said  
20 set of respective time delays to said channel control  
bus, each time delay being a function of a respective  
hypotenuse output by said second cordic rotator.

32. The beamforming system as recited in claim  
31, wherein said first and second cordic rotators  
perform respective apodization projections as a  
function of said focal position and said respective  
5 positions of said transducer elements in a second  
cordic rotator state, and said delay calculator  
further comprises an apodization value generator for  
applying respective apodization values to said channel  
control bus, each apodization value being a function  
10 of a respective apodization projection.

33. A method for ultrasound beamforming,  
comprising the steps of:

storing geometry parameters of a transducer array  
having a multiplicity of transducer elements;

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5 storing vector parameters for forming a focused  
beam having a focal position;  
calculating respective hypotenuses representing  
the distances from said focal position to said  
respective transducer elements as a function of said  
10 geometry parameters and said vector parameters using  
multiple stages of cordic rotation to derive each  
hypotenuse;  
generating respective time delays as a function  
of said respective calculated hypotenuses; and  
15 forming a beam using said respective time delays.

34. The method as recited in claim 33, further  
comprising the steps of:

performing respective apodization projections for  
said respective transducer elements as a function of  
5 said geometry parameters and said vector parameters  
using multiple stages of cordic rotation to perform  
each projection;  
generating respective shading values as a func-  
tion of said respective apodization projections; and  
10 using said respective shading values during  
forming of said beam.

35. The method as recited in claim 33, wherein  
each stage of cordic rotation comprises bit shifts and  
additions.

36. The method as recited in claim 33, wherein  
each stage of cordic rotation comprises a coordinate  
transformation using coefficients which are powers of  
two.

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37. A method for ultrasound apodization, comprising the steps of:

storing geometry parameters of a transducer array having a multiplicity of transducer elements;

5 storing vector parameters for forming a focused beam having a focal position;

performing respective apodization projections for said respective transducer elements as a function of said geometry parameters and said vector parameters  
10 using multiple stages of cordic rotation to perform each projection;

generating respective shading values as a function of said respective apodization projections; and

15 applying said respective shading values to respective signals in respective channels of a beamformer.

38. The method as recited in claim 37, wherein each stage of cordic rotation comprises a coordinate transformation using coefficients which are powers of two.

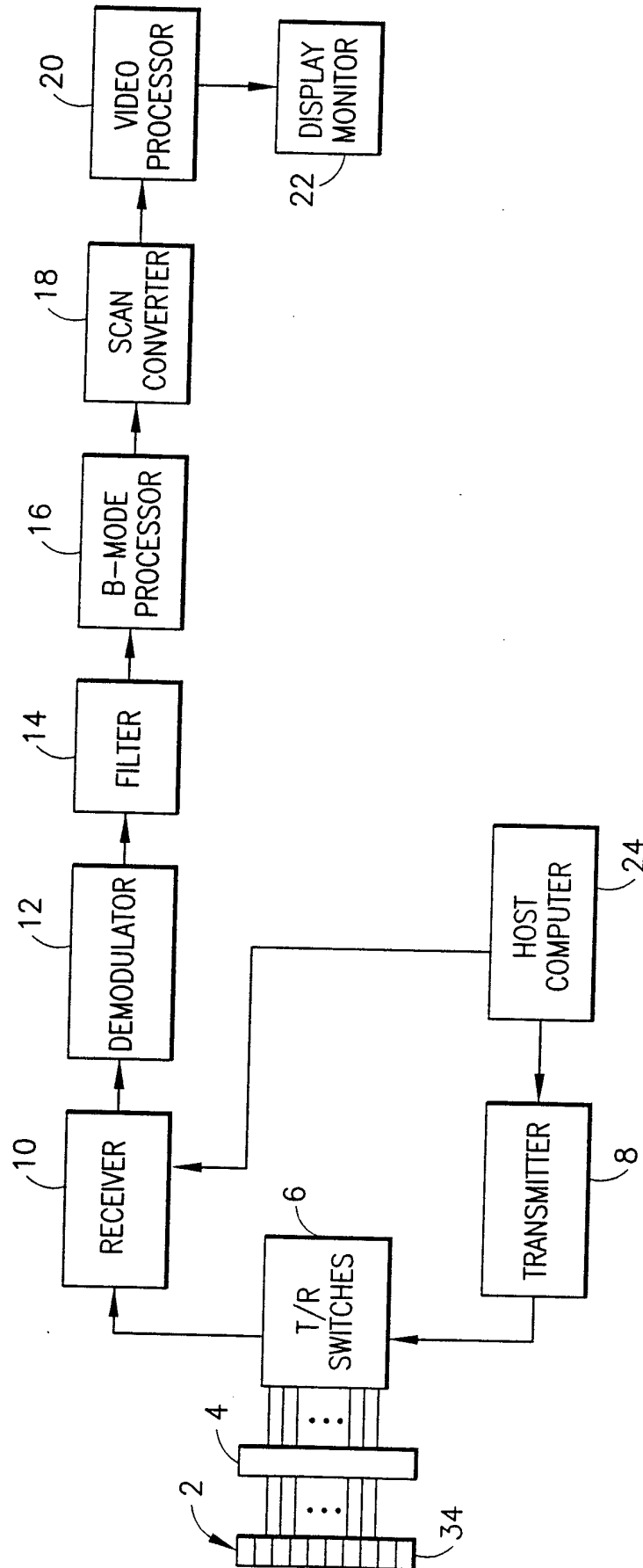


FIG. 1

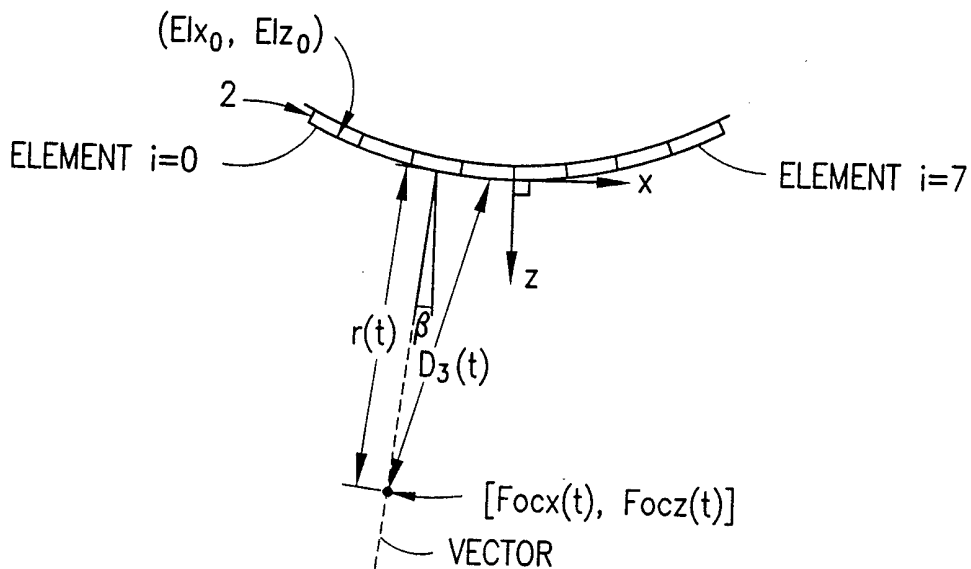


FIG.2

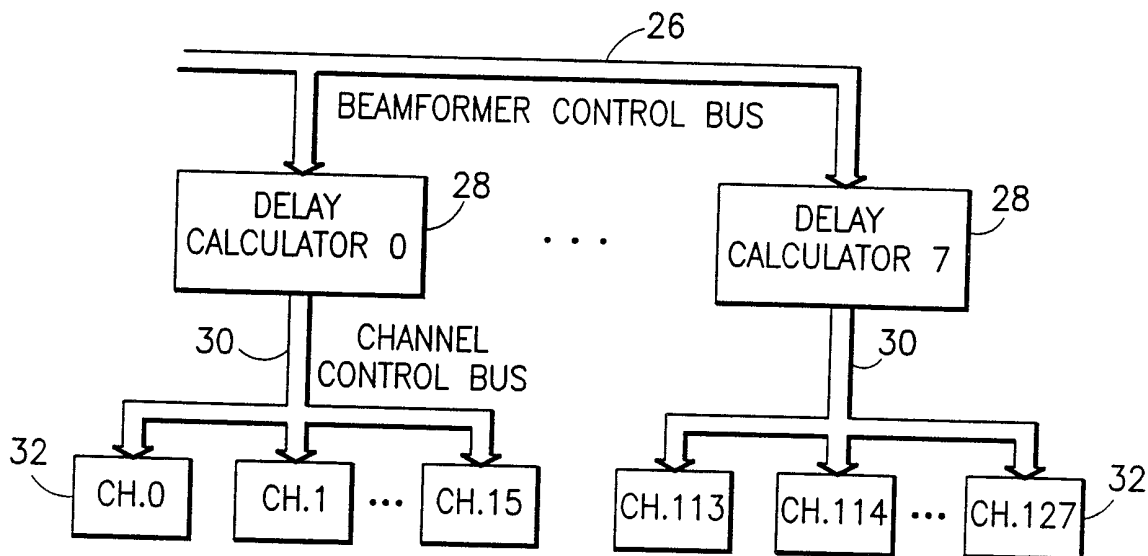


FIG.3

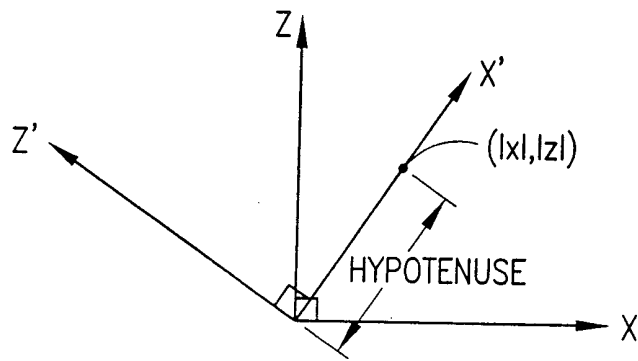


FIG.4

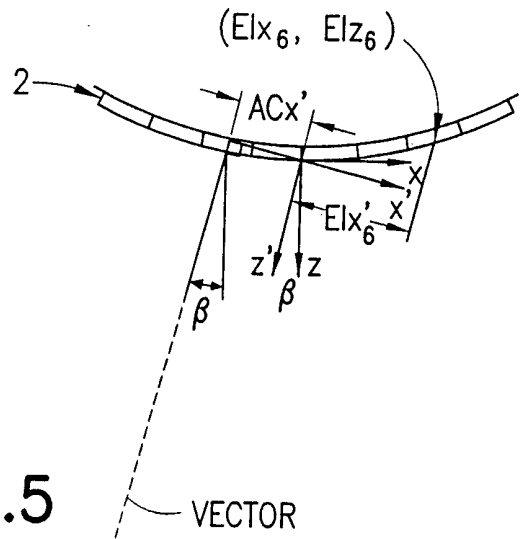


FIG.5

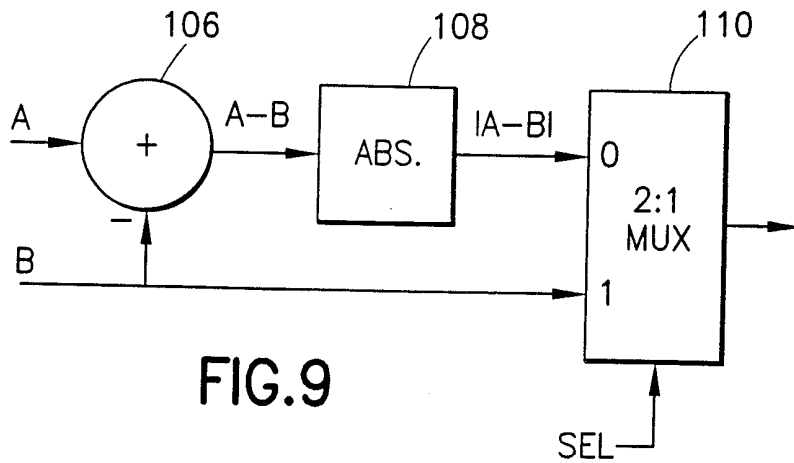


FIG.9

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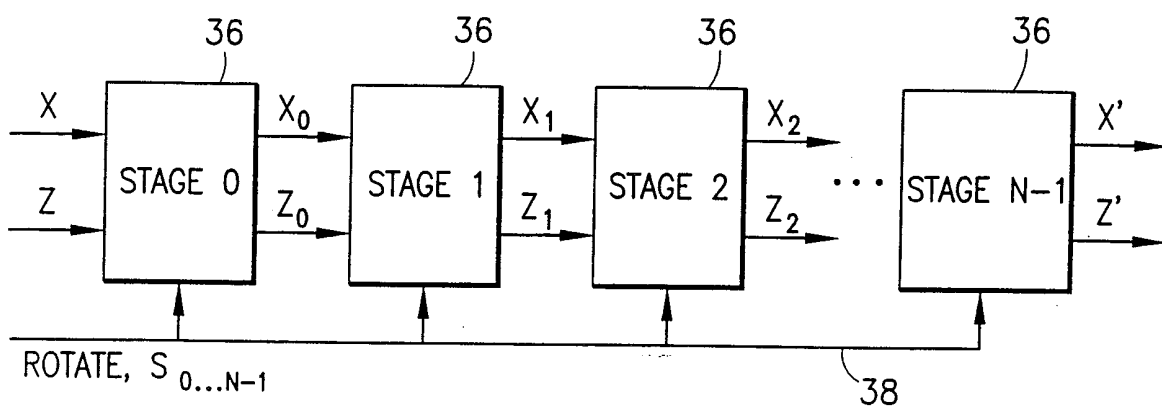


FIG. 6

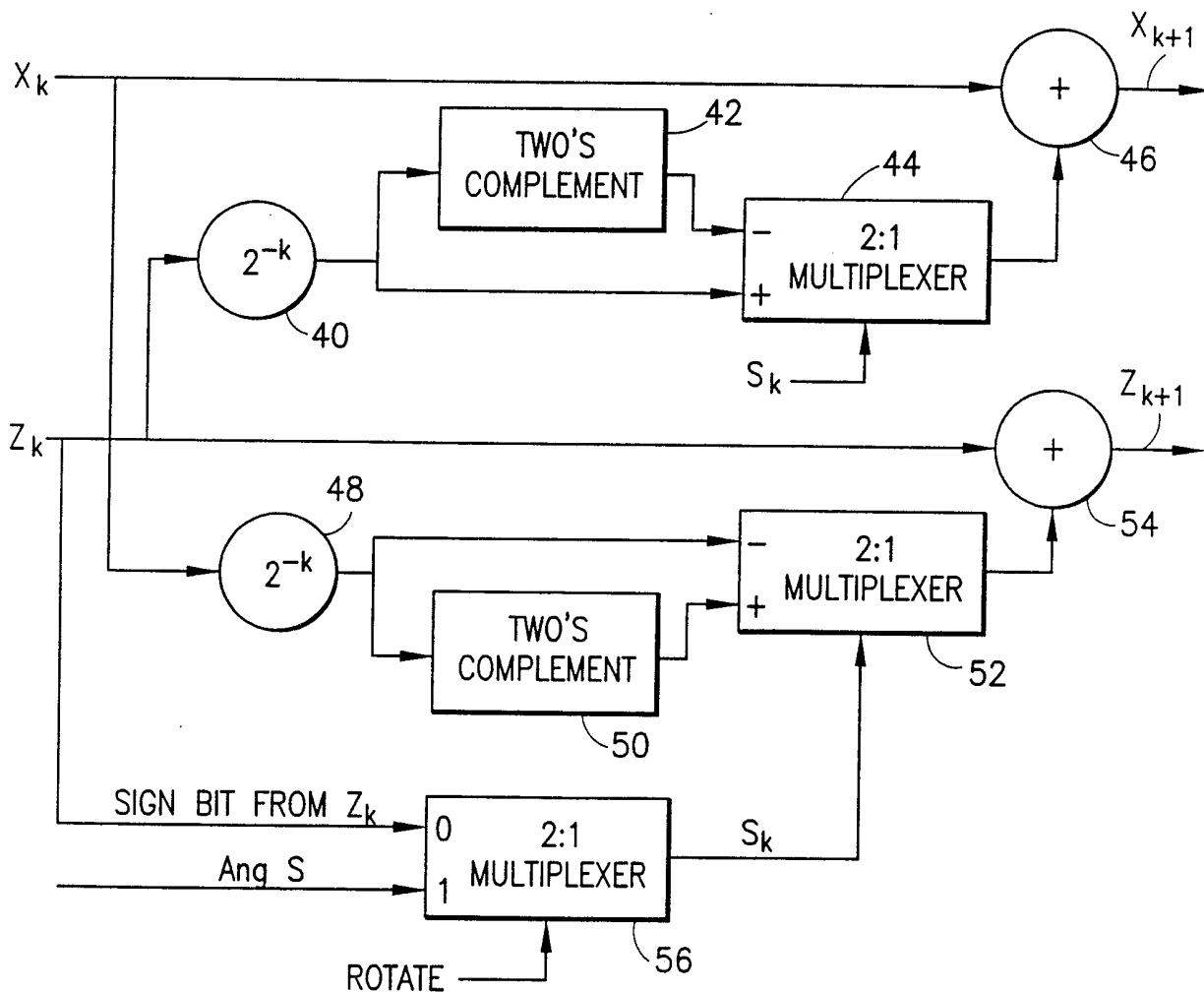


FIG. 7



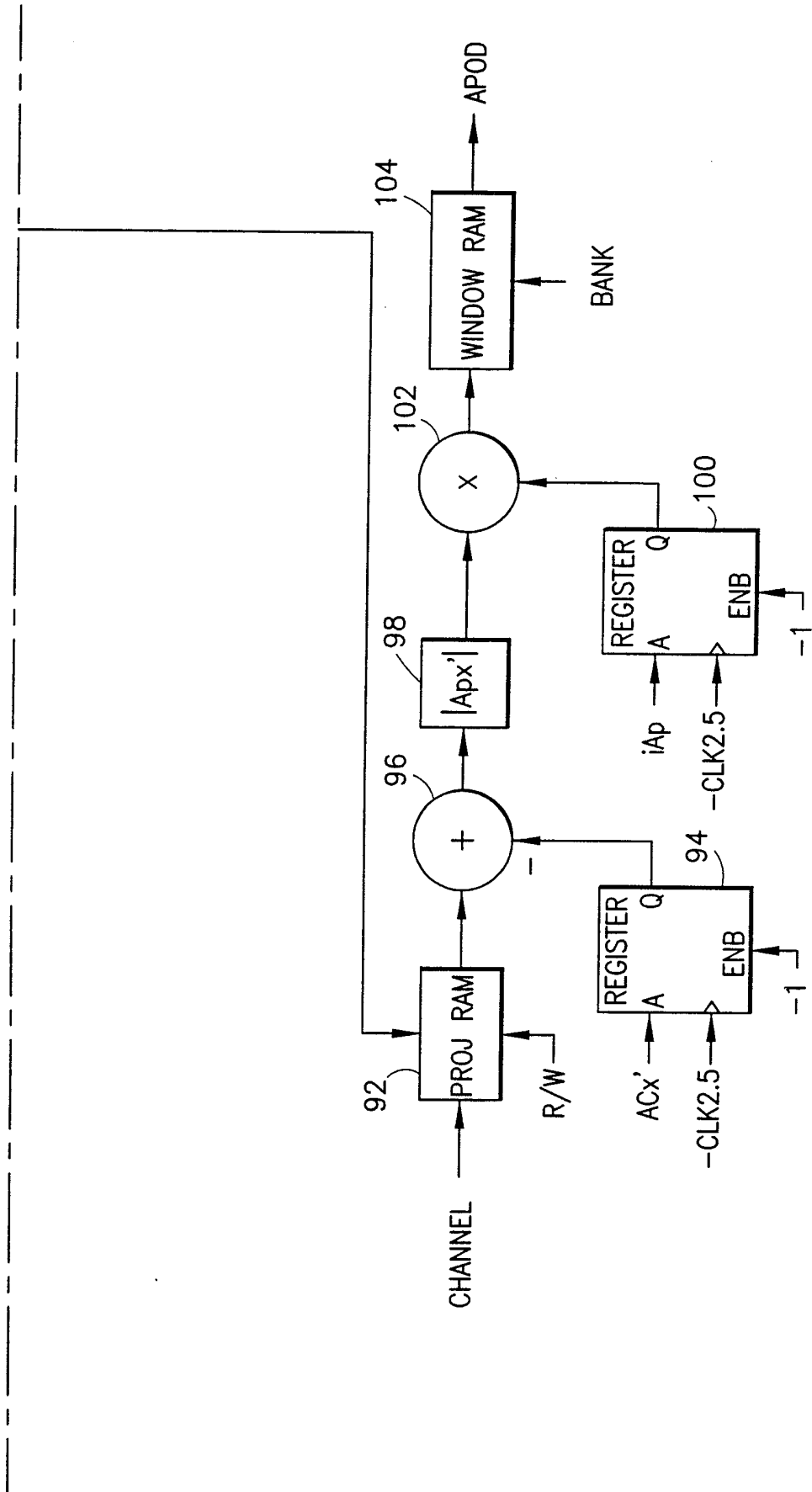


FIG. 8-2

# INTERNATIONAL SEARCH REPORT

In tional Application No  
PCT/US 99/28652

**A. CLASSIFICATION OF SUBJECT MATTER**

IPC 7 G10K11/34 G01S7/52 G01S15/89 G06F7/544 G06F7/552

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G10K G01S H01Q G06F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>EP 0 782 126 A (GEN ELECTRIC) 2 July 1997 (1997-07-02)</p> <p style="text-align: center;">---</p> <p>page 2, line 35 -page 4, line 11</p>	<p>1, 11, 13, 15, 17, 21, 25, 27, 29, 31, 33, 37</p>
A	<p>US 5 501 219 A (YAO LIN X ET AL) 26 March 1996 (1996-03-26)</p> <p style="text-align: center;">---</p> <p>column 2, line 61 -column 3, line 56</p> <p style="text-align: center;">--- -/--</p>	<p>1, 11, 15, 17, 21, 27, 31</p>

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

° Special categories of cited documents :

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Date of the actual completion of the international search

26 April 2000

Date of mailing of the international search report

04/05/2000

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INTERNATIONAL SEARCH REPORT

International Application No  
PCT/US 99/28652

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>ELDON J A ET AL: "FROM POLAR TO RECTANGULAR AND BACK" PROCEEDINGS OF THE ASILOMAR CONFERENCE ON SIGNALS, SYSTEMS AND COMPUTERS,US,NEW YORK, IEEE, vol. CONF. 23, 1989, pages 431-435, XP000217688 page 432, left-hand column -page 433, right-hand column</p>	<p>1,13,17, 25,29, 33,37</p>
A	<p>EP 0 365 226 A (RAYTHEON CO) 25 April 1990 (1990-04-25)</p> <p>claim 1</p>	<p>1,13,17, 25,29, 33,37</p>
A	<p>SHEN-FU HSIAO ET AL: "THE CORDIC HOUSEHOLDER ALGORITHM" PROCEEDINGS OF THE SYMPOSIUM ON COMPUTER ARITHMETIC,US,LOS ALAMITOS, IEEE COMP. SOC. PRESS, vol. SYMP. 10, 1991, pages 256-263, XP000222178 page 256 -page 257</p>	<p>11,15, 21,27,31</p>

# INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 99/28652

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EP 0782126	A	02-07-1997	US 5653236 A JP 9318733 A	05-08-1997 12-12-1997
US 5501219	A	26-03-1996	NONE	
EP 0365226	A	25-04-1990	JP 2037639 C JP 2170274 A JP 7075019 B US 4945505 A	28-03-1996 02-07-1990 09-08-1995 31-07-1990