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(54) Title: FLAME RESISTANT SPUN STAPLE YARNS MADE FROM BLENDS OF FIBERS DERIVED FROM DIAMINO DIPHENYL SULFONE AND MODACRYLIC FIBERS AND FABRICS AND GARMENTS MADE THEREFROM AND METHODS FOR MAKING SAME

(57) Abstract: The invention concerns a flame-resistant spun staple yarns and fabrics and garments comprising these yarns and methods of making the same. The yarns have 25 to 80 parts by weight of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and 20 to 75 parts by weight of a modacrylic fiber, based on 100 parts by weight of the polymeric fiber and the modacrylic fiber in the yarn.

TITLE OF INVENTION

5 FLAME RESISTANT SPUN STAPLE YARNS MADE FROM BLENDS OF
FIBERS DERIVED FROM DIAMINO DIPHENYL SULFONE AND
MODACRYLIC FIBERS AND FABRICS AND GARMENTS MADE
THEREFROM AND METHODS FOR MAKING SAME

10 **FIELD OF THE INVENTION**

The invention relates to flame-resistant spun staple yarns, and fabrics and garments comprising these yarns, and methods of making the same. The yarns have at least 25 parts by weight of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of
15 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and 20 to 75 parts by weight of a modacrylic fiber, based on 100 parts by weight of the polymeric fiber and the modacrylic fiber in the yarn.

BACKGROUND OF THE INVENTION

Workers that can be potentially exposed to electrical arcs and the like need
20 protective clothing and articles made from thermally resistant fabrics. Any increase in the effectiveness of these protective articles, or any increase in the comfort of these articles while maintaining arc protection performance, is welcomed.

A fiber known as polysulfonamide fiber (PSA) is made from a poly
25 (sulfone-amide) polymer and has good thermal resistance due to its aromatic content and also has low modulus, which imparts more flexibility to fabrics made from the fiber; however, the fiber has low tensile break strength. This low tensile strength in fibers has a major impact on the mechanical properties of fabrics made from these fibers, including the ability of the fabrics and garments made with
30 these fabrics to provide adequate arc protection. Therefore what is needed is a way of incorporating PSA into yarns for use in protective apparel that utilizes the benefits of the PSA fiber while compensating for the limitations of the fiber.

SUMMARY OF THE INVENTION

In some embodiments, this invention relates to a flame-resistant spun yarn, 5 woven fabric, and protective garment, comprising at least 25 parts by weight (i.e., 25 to 80 parts) of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and 20 to 75 parts by weight of a modacrylic fiber, based on the total amount (100 10 total parts) of the polymeric fiber and the modacrylic fiber in the yarn.

In some embodiments, this invention relates to a flame-resistant spun yarn comprising at least 25 parts by weight (i.e., 25 to 80 parts) of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; 20 to 69 parts by weight of a modacrylic fiber; 5 to 15 parts by weight of a para-aramid fiber; and 1 to 5 parts by weight of an antistatic fiber based on the total amount (100 total parts) of polymeric fiber, modacrylic fiber, para-aramid fiber, and antistatic fiber in the yarn.

In some other embodiments, this invention concerns a method of 20 producing a flame-resistant spun yarn comprising forming a fiber mixture of at least 25 parts by weight (i.e., 25 to 80 parts) of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and 20 to 75 parts by weight of a modacrylic fiber, based on the 25 total amount (100 total parts) of the polymeric fiber and the modacrylic fiber in the yarn; and spinning the fiber mixture into a spun staple yarn.

DETAILED DESCRIPTION

30 This invention concerns a flame-resistant spun staple yarn made from a mixture of polymeric staple fiber derived from a diamino diphenyl sulfone monomer and modacrylic staple fiber. By "flame resistant" it is meant the spun staple yarn, or fabrics made from the yarn, will not support a flame in air. In

preferred embodiments the fabrics have a limiting oxygen index (LOI) of 26 and higher.

For purposes herein, the term "fiber" is defined as a relatively flexible, macroscopically homogeneous body having a high ratio of length to the width of the cross-sectional area perpendicular to that length. The fiber cross section can be any shape, but is typically round. Herein, the term "filament" or "continuous filament" is used interchangeably with the term "fiber."

As used herein, the term "staple fibers" refers to fibers that are cut to a desired length or are stretch broken, or fibers that occur naturally with or are made having a low ratio of length to the width of the cross-sectional area perpendicular to that length when compared with filaments. Man made staple fibers are cut or made to a length suitable for processing on cotton, woolen, or worsted yarn spinning equipment. The staple fibers can have (a) substantially uniform length, (b) variable or random length, or (c) subsets of the staple fibers have substantially uniform length and the staple fibers in the other subsets have different lengths, with the staple fibers in the subsets mixed together forming a substantially uniform distribution.

In some embodiments, suitable staple fibers have a length of 0.25 centimeters (0.1 inches) to 30 centimeters (12 inches). In some embodiments, the length of a staple fiber is from 1 cm (0.39 in) to 20 cm (8 in). In some preferred embodiments the staple fibers made by short staple processes have a staple fiber length of 1 cm (0.39 in) to 6 cm (2.4 in).

The staple fibers can be made by any process. For example, the staple fibers can be cut from continuous straight fibers using a rotary cutter or a guillotine cutter resulting in straight (i.e., non crimped) staple fiber, or additionally cut from crimped continuous fibers having a saw tooth shaped crimp along the length of the staple fiber, with a crimp (or repeating bend) frequency of preferably no more than 8 crimps per centimeter.

The staple fibers can also be formed by stretch breaking continuous fibers resulting in staple fibers with deformed sections that act as crimps. Stretch broken staple fibers can be made by breaking a tow or a bundle of continuous filaments during a stretch break operation having one or more break zones that are a prescribed distance creating a random variable mass of fibers having an average cut length controlled by break zone adjustment.

Spun staple yarn can be made from staple fibers using traditional long and short staple ring spinning processes that are well known in the art. For short staple, cotton system spinning fiber lengths from 1.9 to 5.7 cm (0.75 in to 2.25 in) are typically used. For long staple, worsted or woolen system spinning, fibers up 5 to 16.5 cm (6.5 in) are typically used. However, this is not intended to be limiting to ring spinning because the yarns may also be spun using air jet spinning, open end spinning, and many other types of spinning which converts staple fiber into useable yarns.

Spun staple yarns can also be made directly by stretch breaking using 10 stretch-broken tow to top staple processes. The staple fibers in the yarns formed by traditional stretch break processes typically have length of up to 18 cm (7 in) long. However spun staple yarns made by stretch breaking can also have staple fibers having maximum lengths of up to 50 cm (20 in) through processes as described for example in PCT Patent Application No. WO 0077283. Stretch 15 broken staple fibers normally do not require crimp because the stretch-breaking process imparts a degree of crimp into the fiber.

The term continuous filament refers to a flexible fiber having relatively 20 small-diameter and whose length is longer than those indicated for staple fibers. Continuous filament fibers and multifilament yarns of continuous filaments can be made by processes well known to those skilled in the art.

By polymeric fibers containing a polymer or copolymer derived from an amine monomer selected from the group consisting of 4,4'-diaminodiphenyl sulfone, 3,3'-diaminodiphenyl sulfone, and mixtures thereof, it is meant the polymer fibers were made from a monomer generally having the structure:

25



wherein Ar₁ and Ar₂ are any unsubstituted or substituted six-membered aromatic 30 group of carbon atoms and Ar₁ and Ar₂ can be the same or different. In some preferred embodiments Ar₁ and Ar₂ are the same. Still more preferably, the six-membered aromatic group of carbon atoms has *meta*- or *para*-oriented linkages versus the SO₂ group. This monomer or multiple monomers having this general structure are reacted with an acid monomer in a compatible solvent to create a polymer. Useful acids monomers generally have the structure of



wherein Ar_3 is any unsubstituted or substituted aromatic ring structure and can be 5 the same or different from Ar_1 and/or Ar_2 . In some preferred embodiments Ar_3 is a six-membered aromatic group of carbon atoms. Still more preferably, the six-membered aromatic group of carbon atoms has *meta*- or *para*-oriented linkages. In some preferred embodiments Ar_1 and Ar_2 are the same and Ar_3 is different 10 from both Ar_1 and Ar_2 . For example, Ar_1 and Ar_2 can be both benzene rings having *meta*-oriented linkages while Ar_3 can be a benzene ring having *para*-oriented linkages. Examples of useful monomers include terephthaloyl chloride, isophthaloyl chloride, and the like. In some preferred embodiments, the acid is terephthaloyl chloride or its mixture with isophthaloyl chloride and the amine monomer is 4,4'-diaminodiphenyl sulfone. In some other preferred embodiments, 15 the amine monomer is a mixture of 4,4'-diaminodiphenyl sulfone and 3,3'-diaminodiphenyl sulfone in a weight ratio of 3:1, which creates a fiber made from a copolymer having both sulfone monomers.

In still another preferred embodiment, the polymeric fibers contain a 20 copolymer, the copolymer having both repeat units derived from sulfone amine monomer and an amine monomer derived from paraphenylene diamine and/or metaphenylene diamine. In some preferred embodiments the sulfone amide repeat units are present in a weight ratio of 3:1 to other amide repeat units. In some 25 embodiments, at least 80 mole percent of the amine monomers is a sulfone amine monomer or a mixture of sulfone amine monomers. For convenience, herein the abbreviation "PSA" will be used to represent all of the entire classes of fibers made with polymer or copolymer derived from sulfone monomers as previously described.

In one embodiment, the polymer and copolymer derived from a sulfone 30 monomer can preferably be made via polycondensation of one or more types of diamine monomer with one or more types of chloride monomers in a dialkyl amide solvent suchs as N-methyl pyrrolidone, dimethyl acetamide, or mixtures thereof. In some embodiments of the polymerizations of this type an inorganic salt such as lithium chloride or calcium chloride is also present. If desired the polymer can be isolated by precipitation with non-solvent such as water, neutralized,

washed, and dried. The polymer can also be made via interfacial polymerization which produces polymer powder directly that can then be dissolved in a solvent for fiber production.

The polymer or copolymer can be spun into fibers via solution spinning, 5 using a solution of the polymer or copolymer in either the polymerization solvent or another solvent for the polymer or copolymer. Fiber spinning can be accomplished through a multi-hole spinneret by dry spinning, wet spinning, or dry-jet wet spinning (also known as air-gap spinning) to create a multi-filament yarn or tow as is known in the art. The fibers in the multi-filament yarn or tow 10 after spinning can then be treated to neutralize, wash, dry, or heat treat the fibers as needed using conventional technique to make stable and useful fibers.

Exemplary dry, wet, and dry-jet wet spinning processes are disclosed U.S. Patent Nos. 3,063,966; 3,227,793; 3,287,324; 3,414,645; 3,869,430; 3,869,429; 3,767,756; and 5,667,743.

15 Specific methods of making PSA fibers or copolymers containing sulfone amine monomers are disclosed in Chinese Patent Publication 1389604A to Wang et al. This reference discloses a fiber known as polysulfonamide fiber (PSA) made by spinning a copolymer solution formed from a mixture of 50 to 95 weight percent 4,4'diaminodiphenyl sulfone and 5 to 50 weight percent 3,3'diaminodiphenyl sulfone copolymerized with equimolar amounts of terephthaloyl chloride in dimethylacetamide. Chinese Patent Publication 1631941A to Chen et al. also discloses a method of preparing a PSA copolymer spinning solution formed from a mixture of 4,4'diaminodiphenyl sulfone and 3,3'diaminodiphenyl sulfone in a mass ratio of from 10:90 to 90:10 20 copolymerized with equimolar amounts of terephthaloyl chloride in dimethylacetamide. Still another method of producing copolymers is disclosed in United States Patent No. 4,169,932 to Sokolov et al. This reference discloses preparation of poly(paraphenylene) terephthalamide (PPD-T) copolymers using tertiary amines to increase the rate of polycondensation. This patent also discloses 25 the PPD-T copolymer can be made by replacing 5 to 50 mole percent of the paraphenylene diamine (PPD) by another aromatic diamine such as 4,4'diaminodiphenyl sulfone.

The polymeric staple fiber containing derived from the sulfone monomers is combined with 20 to 75 parts by weight of a modacrylic staple fiber, based on

the total amount of the polymeric fiber and the modacrylic fiber in the yarn. By modacrylic fiber it is meant acrylic synthetic fiber made from a polymer comprising acrylonitrile. Preferably the polymer is a copolymer comprising 30 to 70 weight percent of an acrylonitrile and 70 to 30 weight percent of a halogen-containing vinyl monomer. The halogen-containing vinyl monomer is at least one monomer selected, for example, from vinyl chloride, vinylidene chloride, vinyl bromide, vinylidene bromide, etc. Examples of copolymerizable vinyl monomers are acrylic acid, methacrylic acid, salts or esters of such acids, acrylamide, methylacrylamide, vinyl acetate, etc.

5 The preferred modacrylic fibers used in this invention are copolymers of acrylonitrile combined with vinylidene chloride. The copolymer can have, in addition, an antimony oxide or antimony oxides for improved fire retardancy. Such useful modacrylic fibers include, but are not limited to, fibers disclosed in United States Patent No. 3,193,602 having 2 weight percent antimony trioxide,

10 fibers disclosed in United States Patent No. 3, 748,302 made with various antimony oxides that are present in an amount of at least 2 weight percent and preferably not greater than 8 weight percent, and fibers disclosed in United States Patent Nos. 5,208,105 & 5,506,042 having 8 to 40 weight percent of an antimony compound. The preferred modacrylic fiber is commercially available from

15 Kaneka Corporation, Japan, in various forms, some containing no antimony oxides while others such as Protex C are said to contain 10 to 15 weight percent of those compounds.

20 In some preferred embodiments the modacrylic fiber has a break tenacity greater than the break tenacity of the PSA staple fiber, which is generally 3 grams per denier (2.7 grams per dtex). In some embodiments, the modacrylic fiber has a break tenacity of at least 3.5 grams per denier (3.2 grams per dtex). In some other embodiments the modacrylic fiber has a break tenacity of at least 4 grams per denier (3.6 grams per dtex) or greater. When exposed to high heat flux, such as a flame, modacrylic fiber releases a flame suppressing gas, providing higher

25 protection during arc events. It is believed, therefore, that fabrics made from the PSA and modacrylic fiber spun yarn have a higher level of protection during arc events. It is believed that at least 20 percent by weight of the modacrylic staple yarn is required to provide adequate arc protection, and that amounts greater than

75 percent by weight the amount of modacrylic fiber becomes detrimental to the fabric char length.

In one embodiment, the fiber mixture comprises para-aramid fibers in an amount of 5 to 15 parts by weight. By aramid is meant a polyamide wherein at least 85% of the amide (-CONH-) linkages are attached directly to two aromatic rings, and "para-aramid" means the two rings or radicals are para oriented with respect to each other along the molecular chain. Additives can be used with the aramid. In fact, it has been found that up to as much as 10 percent, by weight, of other polymeric material can be blended with the aramid or that copolymers can be used having as much as 10 percent of other diamine substituted for the diamine of the aramid or as much as 10 percent of other diacid chloride substituted for the diacid chloride of the aramid. In the practice of this invention, the preferred para-aramid is poly(paraphenylene terephthalamide). Methods for making para-aramid fibers useful in this invention are generally disclosed in, for example, US Patent Nos. 3,869,430; 3,869,429; and 3,767,756. Such aromatic polyamide organic fibers and various forms of these fibers are available from E. I. du Pont de Nemours & Company, Wilmington, Delaware sold under the trademark Kevlar® fibers and from Teijin Ltd. of Japan sold under the trademark Twaron® fibers. For the purposes herein, Technora® fiber, which is available from Teijin Ltd. of Tokyo, Japan, and is made from copoly(p-phenylene/3,4'diphenyl ester terephthalamide), is considered a para-aramid fiber.

Para-aramid fiber has low thermal shrinkage. By "low thermal shrinkage" it is meant that the fiber does not excessively shrink when exposed to a high heat flux or a flame; that is, the length of the fiber will not shorten more than five percent when exposed to a flame. In some preferred embodiments, the fiber actually lengthens when exposed to a flame. In some preferred embodiments, the fiber retains 90 percent of its fiber weight when heated in air to 500 C at a rate of 20 degrees C per minute. Para-aramid fibers are flame resistant organic fibers, and fabric made solely from these fibers has a high Limiting Oxygen Index (LOI) such that the fiber or fabric will not support a flame in air, the preferred LOI range being greater than 26. Fabrics made with spun yarns containing at least 5 percent by weight such low thermal shrinkage fibers, when combined with the other fibers in this mixture, have limited amount of cracks and openings or break open when burned by an impinging flame. Larger amounts of para-aramid fibers provide

more protection to break open up to a practical limit of 15 percent by weight. Above this amount the affect on shrinkage reaches a point of diminishing returns.

If desired, the staple fiber blend and the spun staple yarns can have, in addition, 1 to 5 parts by weight of an antistatic fiber that reduces the propensity 5 for static buildup in the staple yarns, fabric, and garments. In some preferred embodiments the fiber for imparting this antistatic property is a sheath-core staple fiber having a nylon sheath and a carbon core. Suitable materials for supplying antistatic properties are described in United States Patent Nos. 3,803,453 and 4,612,150.

10 In some embodiments, this invention concerns a flame-resistant spun yarn, woven fabric, and protective garment, comprising at least 25 parts by weight (i.e., 25 to 80 parts) of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; 15 and 20 to 75 parts by weight of a modacrylic fiber, based on the total amount (100 total parts) of the polymeric fiber and the modacrylic fiber in the yarn. Based on this combination, the polymeric staple fiber in the yarn can be up to and include 80 parts by weight of the combination of polymeric and modacrylic fiber. In some preferred embodiments the polymeric staple fiber is present in an amount of 50 to 20 75 parts by weight, and the modacrylic fiber is present in an amount of 25 to 50 parts by weight, based on the total amount (100 total parts) of the polymeric staple fiber and the modacrylic fiber in the yarn. In some other preferred embodiments the polymeric staple fiber is present in an amount of 60 to 70 parts by weight, and the modacrylic fiber is present in an amount of 30 to 40 parts by weight, based on 25 the total amount (100 total parts) of the polymeric staple fiber and the modacrylic fiber in the yarn.

In still some other embodiments, the flame-resistant spun yarn, woven fabric, and protective garment, have at least 25 parts by weight of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected 30 from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; 20 to 69 parts by weight of a modacrylic fiber, 5 to 15 parts by weight of a para-aramid fiber, and 1 to 5 parts by weight of an antistatic fiber based on the total amount (100 total parts) of the polymeric fiber, the modacrylic fiber, the para-aramid fiber, and antistatic fiber in the yarn. Based

on this combination, the polymeric staple fiber in the yarn can be up to and include 74 parts by weight of the combination of polymeric, modacrylic, para-aramid, and antistatic fiber.

In some preferred embodiments the various types of staple fibers are 5 present as a staple fiber blend. By fiber blend it is meant the combination of two or more staple fiber types in any manner. Preferably the staple fiber blend is an “intimate blend”, meaning the various staple fibers in the blend form a relatively uniform mixture of the fibers. In some embodiments the two or more staple fiber types are blended prior to or while the yarn is being spun so that the various staple 10 fibers are distributed homogeneously in the staple yarn bundle.

The modacrylic, PSA, and para-aramid fibers all have high flame retardancy, therefore, the combination of the highly flexible PSA fiber with high-arc performance modacrylic fiber ensures the resulting flame-retardant fabric gives a garment a flexible fabric shell for environments where are protection and 15 comfort are required.

Fabrics can be made from the spun staple yarns and can include, but is not limited to, woven or knitted fabrics. General fabric designs and constructions are well known to those skilled in the art. By “woven” fabric is meant a fabric usually formed on a loom by interlacing warp or lengthwise yarns and filling or crosswise 20 yarns with each other to generate any fabric weave, such as plain weave, crowfoot weave, basket weave, satin weave, twill weave, and the like. Plain and twill weaves are believed to be the most common weaves used in the trade and are preferred in many embodiments.

By “knitted” fabric is meant a fabric usually formed by interlooping yarn 25 loops by the use of needles. In many instances, to make a knitted fabric spun staple yarn is fed to a knitting machine which converts the yarn to fabric. If desired, multiple ends or yarns can be supplied to the knitting machine either plied of unplied; that is, a bundle of yarns or a bundle of plied yarns can be co-fed to the knitting machine and knitted into a fabric, or directly into a article of apparel 30 such as a glove, using conventional techniques. In some embodiments it is desirable to add functionality to the knitted fabric by co-feeding one or more other staple or continuous filament yarns with one or more spun staple yarns having the intimate blend of fibers. The tightness of the knit can be adjusted to meet any

specific need. A very effective combination of properties for protective apparel has been found in for example, single jersey knit and terry knit patterns.

In some particularly useful embodiments, the spun staple yarns can be used to make flame-resistant garments. In some embodiments the garments can 5 have essentially one layer of the protective fabric made from the spun staple yarn. Exemplary garments of this type include jumpsuits and coveralls for fire fighters or for military personnel. Such suits are typically used over the firefighters clothing and can be used to parachute into an area to fight a forest fire. Other garments can include pants, shirts, gloves, sleeves and the like that can be worn in 10 situations such as chemical processing industries or industrial electrical/utility where an extreme thermal event might occur. In some preferred embodiments the fabrics have an arc resistance of at least 0.8 calories per square centimeter per ounce per square yard.

In another embodiment, this invention relates to a method of producing a 15 flame-resistant spun yarn comprising forming a fiber mixture of at least 25 parts by weight (i.e., 25 to 80 parts) of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and 20 to 75 parts by weight of a modacrylic fiber, based on the total amount (100 20 total parts) of the polymeric fiber and the modacrylic fiber in the yarn; and spinning the fiber mixture into a spun staple yarn. In some preferred embodiments the polymeric staple fiber is present in an amount of 50 to 75 parts by weight, and the modacrylic fiber is present in an amount of 25 to 50 parts by weight, based on 100 parts by weight of the polymeric staple fiber and the modacrylic fiber in the 25 yarn. In some other embodiments, the polymeric staple fiber is present in an amount of 60 to 70 parts by weight, and the modacrylic fiber is present in an amount of 30 to 40 parts by weight, based on 100 parts by weight of the polymeric staple fiber and the modacrylic fiber in the yarn. In some embodiments the fiber mixture includes 5 to 15 parts by weight of a para-aramid fiber, and in 30 some embodiments the fiber mixture includes 1 to 5 parts by weight of an antistatic fiber.

In one embodiment the fiber mixture is formed by making an intimate blend of the fibers. If desired, other staple fibers can be combined in this relatively uniform mixture of staple fibers. The blending can be achieved by any number of

ways known in the art, including processes that creel a number of bobbins of continuous filaments and concurrently cut the two or more types of filaments to form a blend of cut staple fibers; or processes that involve opening bales of different staple fibers and then opening and blending the various fibers in openers, blenders, and cards; or processes that form slivers of various staple fibers which are then further processed to form a mixture, such as in a card to form a sliver of a mixture of fibers. Other processes of making an intimate fiber blend are possible as long as the various types of different fibers are relatively uniformly distributed throughout the blend. If yarns are formed from the blend, the yarns have a relatively uniform mixture of the staple fibers also. Generally, in most preferred embodiments the individual staple fibers are opened or separated to a degree that is normal in fiber processing to make a useful fabric, such that fiber knots or slubs and other major defects due to poor opening of the staple fibers are not present in an amount that detract from the final fabric quality.

15 In a preferred process, the intimate staple fiber blend is made by first mixing together staple fibers obtained from opened bales, along with any other staple fibers, if desired for additional functionality. The fiber blend is then formed into a sliver using a carding machine. A carding machine is commonly used in the fiber industry to separate, align, and deliver fibers into a continuous 20 strand of loosely assembled fibers without substantial twist, commonly known as carded sliver. The carded sliver is processed into drawn sliver, typically by, but not limited to, a two-step drawing process.

Spun staple yarns are then formed from the drawn sliver using techniques including conventional cotton system or short-staple spinning processes such as 25 open-end spinning and ring-spinning; or higher speed air spinning techniques such as Murata air-jet spinning where air is used to twist the staple fibers into a yarn. The formation of spun yarns can also be achieved by use of conventional woolen system or long-staple processes such as worsted or semi-worsted ring-spinning or stretch-break spinning. Regardless of the processing system, ring-spinning is the 30 generally preferred method for making the spun staple yarns.

TEST METHODS

Basis weight values were obtained according to FTMS 191A; 5041.

Abrasion Test. The abrasion performance of fabrics is determined in accordance with ASTM D-3884-01 “Standard Guide for Abrasion Resistance of Modacrylic Fabrics (Rotary Platform, Double Head Method)”.

Instrumented Thermal Manikin Test. Burn protection performance is 5 determined using “Predicted Burn Injuries for a Person Wearing a Specific Garment or System in a Simulated Flash Fire of Specific Intensity” in accordance with ASTM F 1930 Method (1999) using an instrumented thermal mannequin with standard pattern coverall made with the test fabric.

Arc Resistance Test. The arc resistance of fabrics is determined in 10 accordance with ASTM F-1959-99 “Standard Test Method for Determining the Arc Thermal Performance Value of Materials for Clothing”. The Arc Thermal Performance Value (ATPV) of each fabric, which is a measure of the amount of energy that a person wearing that fabric could be exposed to that would be equivalent to a 2nd degree burn from such exposure 50% of the time.

15 Grab Test. The grab resistance of fabrics (the break tensile strength) is determined in accordance with ASTM D-5034-95 “Standard Test Method for Breaking Strength and Elongation of Fabrics (Grab Test)”.

Tear Test. The tear resistance of fabrics is determined in accordance with 20 ASTM D-5587-03 “Standard Test Method for Tearing of Fabrics by Trapezoid Procedure”.

Thermal Protection Performance (TPP) Test. The thermal protection performance of fabrics is determined in accordance with NFPA 2112 “Standard on Flame Resistant Garments for Protection of Industrial Personnel Against Flash Fire”. The thermal protective performance relates to a fabric’s ability to provide 25 continuous and reliable protection to a wearer’s skin beneath a fabric when the fabric is exposed to a direct flame or radiant heat.

Vertical Flame Test. The char length of fabrics is determined in accordance with ASTM D-6413-99 “Standard Test Method for Flame Resistance of Modacrylics (Vertical Method)”.

30 Limiting Oxygen Index (LOI) is the minimum concentration of oxygen, expressed as a volume percent, in a mixture of oxygen and nitrogen that will just support the flaming combustion of a material initially at room temperature under the conditions of ASTM G125 / D2863.

Examples

The invention is illustrated by, but is not intended to be limited by the following examples. All parts and percentages are by weight unless otherwise 5 indicated.

Example 1

This example illustrates flame-resistant spun yarns and fabrics of intimate blends of PSA fiber and modacrylic fiber. The PSA staple fiber is made from a 10 polymer made from 4,4'diaminodiphenyl sulfone and 3,3'diaminodiphenyl sulfone copolymerized with equimolar amounts of terephthaloyl chloride in dimethylacetamide and is known under the common designation of Tanlon®; the modacrylic fiber is made by Kaneka under the trade name of Protex C®, and Kevlar®29 is poly(p-phenylene terephthalamide) fiber (referred to as PPD-T 15 fiber) and is marketed by E. I. du Pont de Nemours & Company.

A picker blend sliver of 23 weight percent of the PSA, 10 weight percent of PPD-T, and 65% of modacrylic fiber is prepared and processed by the conventional cotton system equipment and is then spun into a flame resistant spun staple yarn having twist multiplier 4.0 and a single yarn size of 21 tex (28 cotton 20 count) using a ring spinning frame. Two such single yarns are then plied on a plying machine to make a two-ply flame resistant yarn for use as a fabric warp yarn. Using a similar process and the same twist and blend ratio, a 24 tex (24 cotton count) singles yarn is made and two of these single yarns are plied to form a two-ply fabric fill yarn. These combination plied yarns have a tenacity greater 25 than the tenacity of a 100% PSA fiber yarn, i. e., they have a tenacity of at least 3 grams per denier (2.7 grams per dtex).

The ring spun yarns are then used as the warp and fill yarns and are woven into a fabric on a shuttle loom, making a greige fabric having a 2x1 twill weave and a construction of 26 ends x 17 picks per cm (72 ends x 52 picks per inch), and 30 a basis weight of 215 g/m² (6.5 oz/yd²). The greige twill fabric is then scoured in hot water and is dried under low tension. The scoured fabric is then jet dyed using basic dye. The resulting fabric has a basis weight of 231 g/m² (7 oz/yd²) and an LOI in excess of 28. Table 1 illustrates properties of the resulting fabric. A “+” indicates superior properties to those of the control fabric, while the notation

“0” indicates the performance of the control fabric or performance equivalent to the control fabric.

Table 1

Property	100%PSA	Example 1
Nominal Basis Weight (opsy)	7	7
Grab Test Break Strength (lbf) W/F	0	+
Trap Tear (lbf) W/F	0	+
Taber Abrasion (Cycles)CS-10/1000 g	0	+
TPP (cal/cm²)	0	0
Vertical Flame (in) W/F	0	0
Instrumented Thermal Manikin Test (% of body burn)	0	0/+
ARC rating(cal/cm²)	0	+

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Example 2

Example 1 is repeated except that the fiber blend includes an antistatic fiber and the proportions of the fibers are as follows: 23 weight percent PSA fiber, 10 weight percent modacrylic fiber, 10 weight percent p-aramid fiber, and 2 weight percent of the antistatic fiber. Spun staple yarns and fabrics having improved performance are made using this fiber blend.

Example 3

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The fabrics of Example 1 and 2 are made into protective articles, including garments, by cutting the fabrics into fabric shapes per a pattern and sewing the shapes together to form a protective coverall for use as protective apparel in industry. Likewise, the fabrics are cut into fabric shapes and the shapes sewn

together to form a protective apparel combination comprising a protective shirt and a pair of protective pants. If desired, the fabrics are cut and sewn to form other protective apparel components such as, coveralls, hoods, sleeves, and aprons.

CLAIMS**What is Claimed:**

5 1. A flame-resistant spun yarn comprising:

10 a) 25 to 80 parts by weight of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and

15 b) 20 to 75 parts by weight of a modacrylic fiber; based on 100 parts by weight of the polymeric fiber and the modacrylic fiber in the yarn.

20 2. The flame-resistant spun yarn of claim 1 wherein the polymeric staple fiber is present in an amount of 50 to 75 parts by weight, and the modacrylic fiber is present in an amount of 25 to 50 parts by weight, based on 100 parts by weight of the polymeric staple fiber and the modacrylic fiber in the yarn.

25 3. The flame-resistant spun yarn of claim 2 wherein the polymeric staple fiber is present in an amount of 60 to 70 parts by weight, and the modacrylic fiber is present in an amount of 30 to 40 parts by weight, based on 100 parts by weight of the polymeric staple fiber and the modacrylic fiber in the yarn.

4. The flame-resistant spun yarn of claim 1 wherein at least 80 mole percent of the polymer or copolymer used in the polymeric staple fiber is derived from a sulfone amine monomer or a mixture of sulfone amine monomers.

30 5. The flame-resistant spun yarn of claim 1 wherein the polymeric polymer further contains a polymer or copolymer derived from the monomer selected from the group of terephthaloyl chloride, isophthaloyl chloride, and mixtures thereof.

6. A woven fabric comprising the yarn of claim 1.

7. A protective garment comprising the yarn of claim 1.

8. A flame-resistant spun yarn comprising:
 - a) 25 to 80 parts by weight of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof;
 - b) 20 to 69 parts by weight of a modacrylic fiber;
 - c) 5 to 15 parts by weight of a para-aramid fiber; and
 - d) 1 to 5 parts by weight of an antistatic fiber;
- 10 based on 100 parts by weight of polymeric fiber, modacrylic fiber, para-aramid fiber, and antistatic fiber in the yarn.
9. The flame-resistant spun yarn of claim 8 wherein at least 80 mole percent of the polymer or copolymer used in the polymeric staple fiber is derived from a sulfone amine monomer or a mixture of sulfone amine monomers.
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10. The flame-resistant spun yarn of claim 8 wherein the para-aramid fiber is poly(paraphenylene terephthalamide) fiber.
11. A woven fabric comprising the yarn of claim 8.
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12. A protective garment comprising the yarn of claim 8.
13. A method of producing a flame-resistant spun yarn comprising:
 - a) forming a fiber mixture of at 25 to 80 parts by weight of a polymeric staple fiber containing a polymer or copolymer derived from a monomer selected from the group consisting of 4,4'diaminodiphenyl sulfone, 3,3'diaminodiphenyl sulfone, and mixtures thereof; and 20 to 75 parts by weight of a modacrylic fiber, based on 100 parts by weight of the polymeric fiber and the modacrylic fiber in the yarn; and
 - b) spinning the fiber mixture into a spun staple yarn.
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14. The method of producing the flame-resistant spun yarn of claim 13 wherein the polymeric staple fiber is present in an amount of 50 to 75 parts by

weight, and the modacrylic fiber is present in an amount of 25 to 50 parts by weight, based on 100 parts by weight of the polymeric staple fiber and the modacrylic fiber in the yarn.

5 15. The method of producing the flame-resistant spun yarn of claim 14 wherein the polymeric staple fiber is present in an amount of 60 to 70 parts by weight, and the modacrylic fiber is present in an amount of 30 to 40 parts by weight, based on 100 parts by weight of the polymeric staple fiber and the modacrylic fiber in the yarn.

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16. The method of producing the flame-resistant spun yarn of claim 13 wherein at least 80 mole percent of the polymer or copolymer used in the polymeric staple fiber is derived from a sulfone amine monomer or a mixture of sulfone amine monomers.

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17. The method of producing the flame-resistant spun yarn of claim 13 wherein the polymeric polymer further contains a polymer or copolymer derived from the monomer selected from the group of terephthaloyl chloride, isophthaloyl chloride, and mixtures thereof.

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18. The method of producing the flame-resistant spun yarn of claim 13 wherein the fiber mixture further comprises 5 to 15 parts by weight para-aramid fiber, based on 100 parts by weight of polymeric fiber, modacrylic fiber, and para-aramid fiber in the yarn.

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INTERNATIONAL SEARCH REPORT

International application No
PCT/US2008/073941

A. CLASSIFICATION OF SUBJECT MATTER INV. D01F6/76 D01F6/80 D02G3/04		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) D01F D02G		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used). EPO-Internal, WPI Data		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	CN 1 389 604 A (SHANGHAI TEXTILE HOLDING GROUP [CN]) 8 January 2003 (2003-01-08) cited in the application abstract	1-18
A	GB 875 068 A (ICI LTD) 16 August 1961 (1961-08-16) the whole document	1-18
A	US 3 621 646 A (BOBKOWICZ EMILIAN ET AL) 23 November 1971 (1971-11-23) the whole document	1-18
<input type="checkbox"/> Further documents are listed in the continuation of Box C.		<input checked="" type="checkbox"/> See patent family annex.
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A document defining the general state of the art which is not considered to be of particular relevance		
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Y document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.		
& document member of the same patent family		
Date of the actual completion of the international search 27 October 2008		Date of mailing of the international search report 14/11/2008
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016		Authorized officer Lux, Rudolf

INTERNATIONAL SEARCH REPORT

Information on patent family members

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Patent document cited in search report	Publication date	Patent family member(s)	Publication date
CN 1389604	A 08-01-2003	NONE	
GB 875068	A 16-08-1961	NONE	
US 3621646	A 23-11-1971	BE 751703 A1 16-11-1970 CA 880988 A 14-09-1971 CH 519594 A 29-02-1972 DE 2042762 A1 27-05-1971 FR 2057698 A5 21-05-1971 GB 1285003 A 09-08-1972 JP 49009424 B 04-03-1974 NL 7013252 A 17-03-1971	