

[54] **MICROWAVE DRYING APPARATUS
AND METHOD**

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[51] Int. Cl.H05b 9/06
[58] Field of Search34/1, DIG. 19; 219/10.55

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[57] **ABSTRACT**

Apparatus and method for drying moisture-laden dielectric materials by microwave energy and including directing microwave energy from a generator to opposite sides of material to be dried. Means is provided for protecting the generator from microwave energy reflected by the material. It is preferable to include means for controlling the output of the generator in accordance with the moisture content of the portion of the material exposed to the microwave energy. This is accomplished by measuring energy transmitted through the material, and controlling the output of the generator inversely relative to the level of the transmitted energy.

18 Claims, 10 Drawing Figures

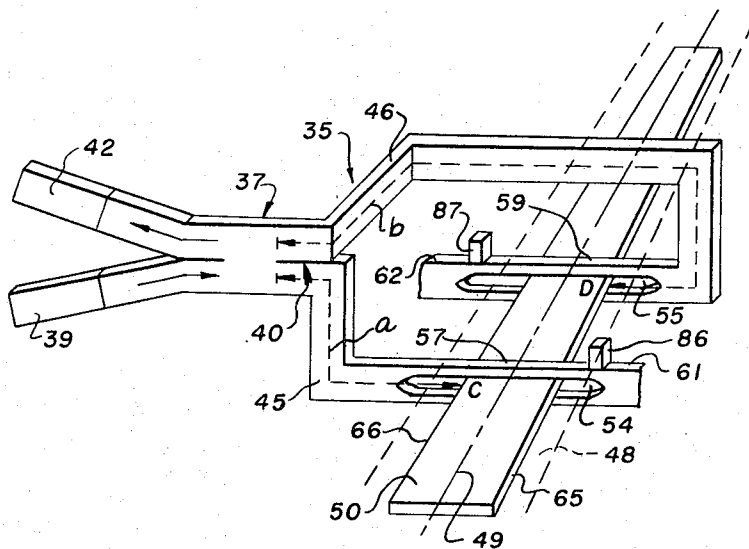


Fig. 1.

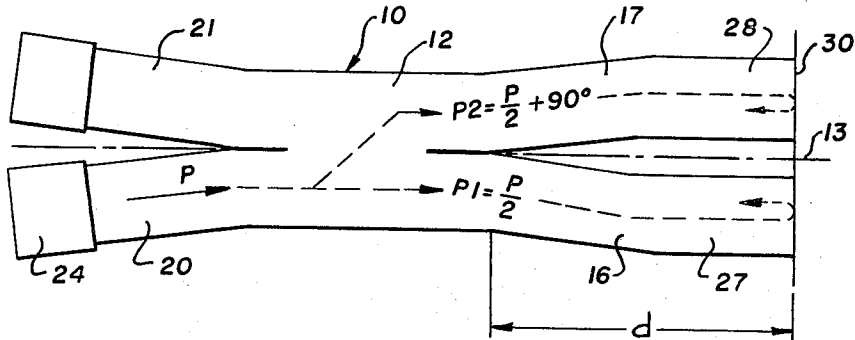


Fig. 2.

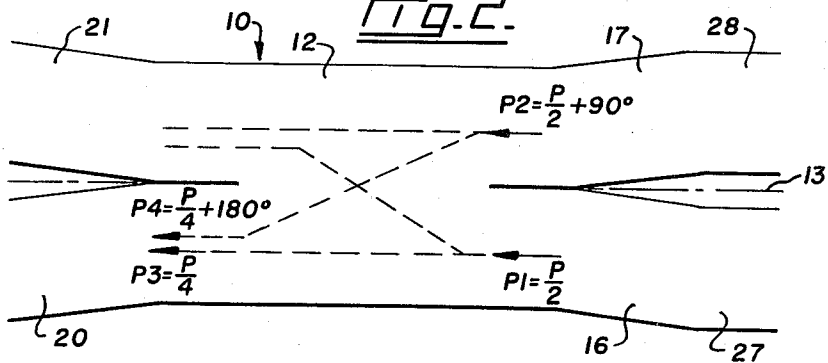
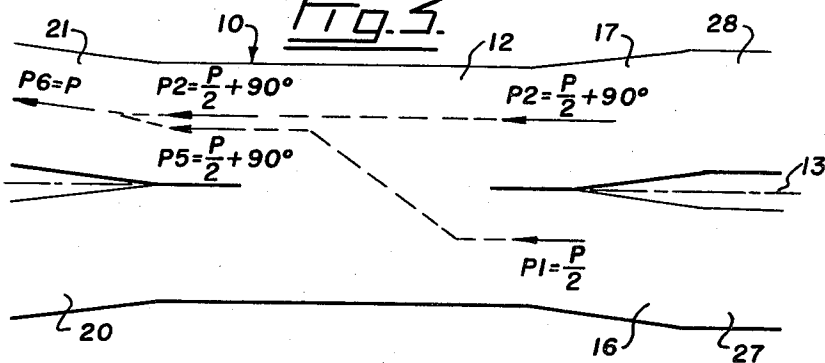


Fig. 3.



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Fig. 4.

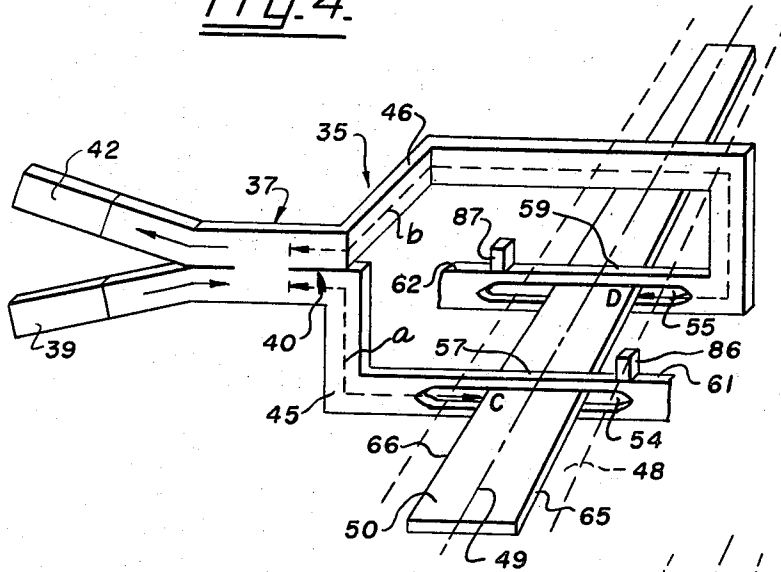


Fig. 6.

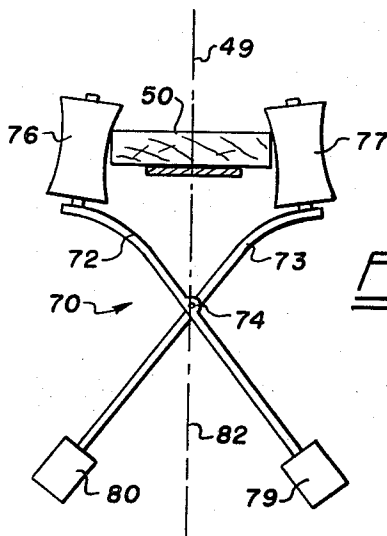
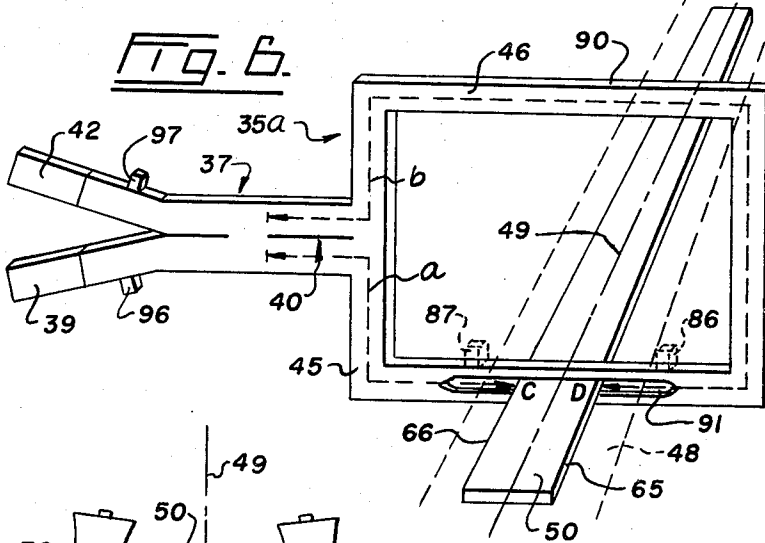
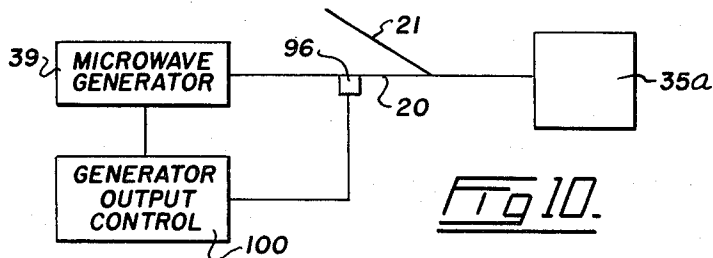
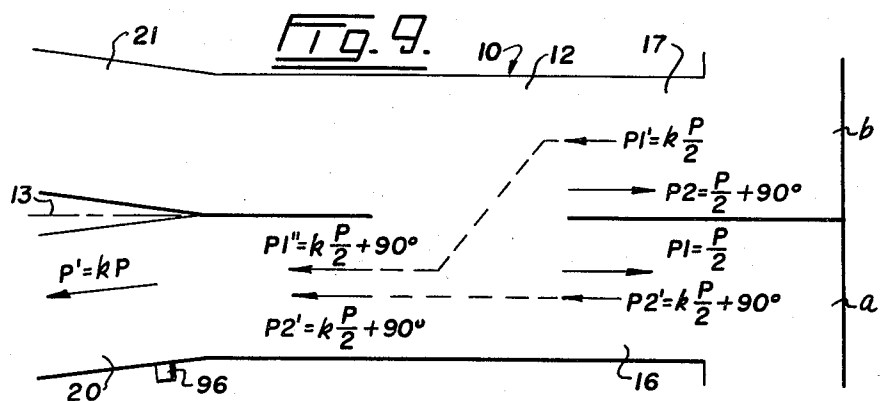
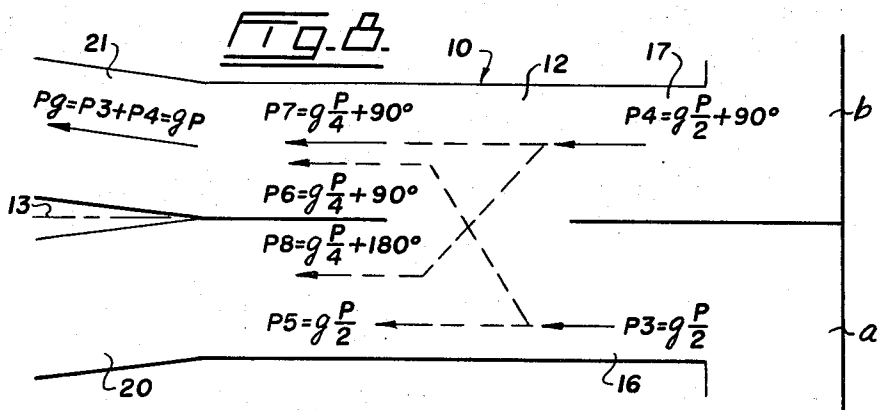
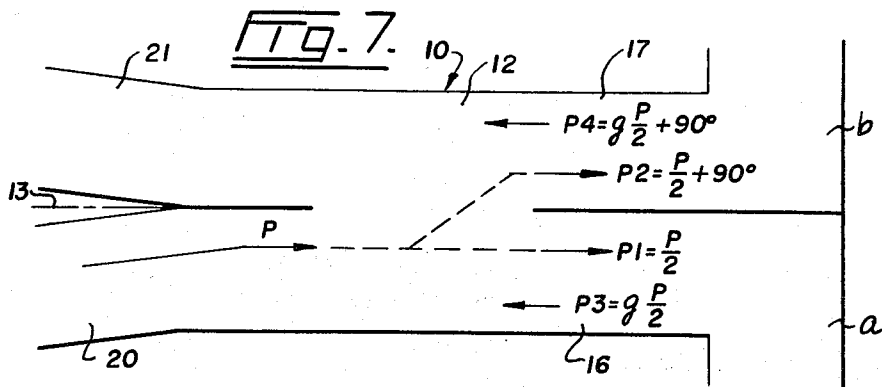


Fig. 5.

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MICROWAVE DRYING APPARATUS AND METHOD

This invention relates to apparatus and methods for drying moisture-laden materials, such as lumber, wood based materials, bagasse, paper and the like by means of microwave energy.

Different types of materials can be dried by the present apparatus and methods, but for the sake of convenience the invention is described herein relative to the drying of lumber.

Heretofore the drying of lumber by means of microwave energy has been difficult and not practical in a commercial sense. The main difficulty is caused by the fact that the moisture content of lumber varies greatly from piece to piece and very often throughout the length of each piece. As the cost of microwave generating equipment and the amount of power consumed are very high, it has not been thought practical economically to dry by means of microwave energy. Another problem is caused by the fact that some microwave energy is reflected by the lumber back to the generator, and this causes serious problems.

The present invention greatly reduces these problems by directing microwave energy from a generator to opposite sides of the lumber, preferably in directly opposed areas. This means that the microwave generator "sees" portions of the board which have substantially the same moisture content. If the output of the generator is controlled in accordance with the moisture content of the lumber exposed to the microwave energy, this energy will increase and decrease in accordance with the moisture content. This is contemplated by the present invention, and includes means for measuring the microwave energy transmitted by the lumber and controlling the output of the generator inversely relative to the transmitted energy. The invention also includes a stopper or means for protecting the microwave generator from microwave energy reflected by the lumber.

The microwave drying method according to this invention comprises dividing microwave energy from a microwave generator into two equal parts, and directing said energy parts through two separated channels to opposite sides of the lumber to be dried, the distance of travel through one of said channels to the longitudinal centerline or to a side of the lumber being equal to the distance of travel through the other of said channels to said centerline or lumber side plus a whole number of half wavelengths of the microwaves from said generator. It is preferable according to this method to direct the two parts of the microwave energy to directly opposite areas of the lumber. The method also includes measuring the microwave energy transmitted through the lumber and controlling the output of the microwave generator inversely relative to the level of the transmitted microwave energy.

The microwave energy from the generator is preferably divided by a four-port hybrid which directs the energy to the two channels and, at the same time, protects the generator from microwave energy reflected by the lumber.

Apparatus according to the present invention comprises a microwave generator, means for dividing microwave energy from the generator into two equal parts, and separate channels for directing said two energy parts to opposite sides of lumber to be dried, the length of one of said channels to the longitudinal centerline or the side of the lumber being equal to the length of the other of said channels to the center line or lumber side plus a whole number of half wavelengths of the microwaves from said generator. These channels are preferably located to direct the two energy parts against directly opposite areas of the lumber. The apparatus also includes means for measuring the microwave energy transmitted through the lumber, and controlling means for regulating the output of the generator inversely relative to the level of the transmitted energy.

In the preferred form of the apparatus, a waveguide system having two channels is used, and the channels of this waveguide system are coupled to the generator by a four-port hybrid. In the preferred form of the invention, the two waveguide channels are in the form of a closed loop or ring, and the lumber travels through a slot in the loop or ring. Guide

means is provided for maintaining the longitudinal center line of the lumber on an electromagnet center line. The length of one of the channels to this electromagnetic center line is equal to the length of the other of the channels plus a whole number of half wavelengths of the microwaves from the generator. With this arrangement, the microwave energy transmitted through the lumber travels back through the channels towards the hybrid. This transmitted energy is measured and the output of the generator is controlled inversely relative to the transmitted energy.

It has been found that the transmitted energy levels are mainly related to the moisture content of the transmitting lumber. As the amount of moisture in the lumber increases so increases the amount of microwave energy absorbed in the drying process and vice versa. The transmitted power represents the amount of power or energy which the lumber was unable to absorb. In this way, lumber of high moisture content and therefore very low in transmitting power, receives automatically maximum microwave energy, while lumber of lower moisture content receives less energy. This ensures maximum power being applied to wet areas without applying too much power to dryer areas, even though these areas are in the same piece of lumber or in adjacent different pieces.

The method and apparatus of the present invention will be understood from the following description in connection with the accompanying drawings, in which

FIGS. 1, 2 and 3 diagrammatically illustrate the operation of a four-port hybrid,

FIG. 4 illustrates one form of microwave drying apparatus in accordance with this invention,

FIG. 5 illustrates an example of guide means for lumber being dried in this apparatus,

FIG. 6 illustrates a preferred form of microwave drying apparatus according to this invention,

FIGS. 7, 8 and 9 illustrate the operation of the four-port hybrid when used in the drying apparatus of FIG. 4 or FIG. 6, and

FIG. 10 illustrates a control system for the drying apparatus.

When a microwave generator is directly coupled to a slotted waveguide through which lumber travels to be dried, all microwave power or energy reflected from the lumber face returns to the generator. This endangers the generator and interferes with its proper operation. This situation is avoided by the use of a four-port hybrid between the generator and the slotted waveguide.

FIG. 1 illustrates the basic working of a four-port hybrid 10. This hybrid is formed with a central section 12 and has a longitudinal center line 13. A first pair of arms 16 and 17 project from one end of the central section on opposite sides of center line 13 at an angle to each other, and a second pair of arms 20 and 21 project from the opposite end of the central section of the hybrid on opposite sides of said center line and at an angle to each other. These arms constitute the four ports of the hybrid. A microwave generator 24 is coupled to arm 20, and arm 21 is connected to suitable microwave energy absorbing means, such as a waterload or another system utilizing microwave energy. Channels 27 and 28 are connected to arms 16 and 17, respectively, and for the purpose of this illustration, a reflector plate 30 extends across the two channels 27 and 28.

When microwave energy or power P comes from generator 24 into port 20 then P1 equalling P/2 continues through port 16, and P2 equalling P/2 will cross the center line 13 and continue through port 17. The crossing of the center line gives an automatic 90° phase shift to P2. If P1 and P2 both travel the same distance d before being reflected by reflector 30, their phase relationship does not change by the time they re-enter ports 16 and 17.

The powers P1 and P2 in FIG. 2 represent their returning or reflected powers, and each one has the tendency to split again into two equal parts, each one of them being equal to P/4. If P3 is that half of P1 which does not cross over the center line, and P4 is that half of P2 which does cross over the center line

and therefore has a further 90° phase shift, then there are in port 20 two electromagnetic waves of equal power but with a phase shift of 180° or half a wavelength. These two waves cancel each other completely and therefore prohibit propagation in port 20, thereby protecting the microwave generator.

FIG. 3 illustrates the results of the above-mentioned cancellation. Since no power from ports 16 and 17 can enter port 20, and since it has to go somewhere, the only way open is port 21, that is, P2 does not cross over the centerline therefore maintains its 90° phase shift while P5 has crossed over the center line and therefore has a 90° phase shift. There are now in port 21 two electromagnetic waves of equal power and of identical phase and therefore they reinforce each other and travel as one wave of power P6 which equals P through port 21 towards the absorption means.

If the total reflection surface 30 is replaced by a surface with a partial reflection coefficient of g , such as the surface of moist lumber, then the same reasoning holds as above, the only difference being in the various power levels, for example, P6 equalling $g \times P$.

FIG. 4 illustrates one form of microwave drying apparatus 35 in accordance with this invention. This apparatus includes a four-port hybrid 37 similar to hybrid 10 described above, and which couples a microwave generator 39 to a waveguide system 40. Suitable microwave absorption means, such as a waterload 42, is coupled to the hybrid.

Waveguide system 40 has a pair of arms or channels 45 and 46 which extend to opposite sides of a path 48 having an electromagnetic center line 49 and along which lumber 50 travels with its longitudinal center line coinciding with centerline 49. Channels 45 and 46 of the waveguide have slots 54 and 55 therein through which path 48 extends. As far as this invention is concerned, the effective parts of channels 45 and 46 terminate in ends 57 and 59 substantially at center line 49. However, the channels 45 and 46 may continue on beyond the lumber path in section 61 and 62 so that microwave energy transmitted through the lumber may be used for any desired purpose.

If the path lengths of FIG. 4 indicated by a and b are not both equal to d of FIG. 1, the distance from the hybrid to a reflecting surface, but is

$a = d$, and $b = d + m \lambda/2$ where m is an integer and λ is the wavelength of the microwaves, then the above reasoning still holds because the distance

$b - a = m \lambda/2$ is being traveled twice, therefore a phase shift of

$2 \times m \lambda/2 = m \lambda$ takes place so that no extra phase shift has been introduced.

If the condition $b - a = m \lambda/2$ is realized for a board of width w then the center line of that board coincides with the electromagnetic center line (EMCL) 49. If now a board of any other width is placed with its center line on the EMCL, then the pathlengths of a and b are changed into a' and b' respectively but in identical ways therefore the term $b' - a' = m \lambda/2$ still holds.

Summarizing, it can be said that independent of power level P , reflection coefficient g or lumber width w , the microwave generator will receive no reflected power if all boards are centered on the EMCL. As an example, with a frequency of 915 MHz, a wavelength results in the guide system of 17.2 inches, there is an EMCL every 4.3 inches (or $\lambda/4$) across the width of the waveguide slot. Therefore within approximately 2 inches of the physical center line of the system there is an EMCL.

In order the comply with this reasoning, the effective length of channel 46 to the edge 65 of lumber 50 or center line 49 equals the effective length of channel 45 to edge 66 of the lumber or center line 49 plus a whole number of half wavelengths of the microwaves from generator 39.

It is clear that when drying lumber of varying widths in apparatus 35, it is not possible to use a one-sided guide rail, and therefore, it is necessary to provide means for keeping the longitudinal center lines of the lumber on the electromagnetic center line 49. FIG. 5 illustrates one way of accomplishing

this. A scissor type guide 70 can be used for this purpose. Guide 70 includes a pair of arms 72 and 73 pivotally connected at 74 to each other said arms carrying rollers 76 and 77 at upper ends thereof equally spaced from pivot 74, and weights 79 and 80 at lower ends thereof, also equally spaced from the pivot. Guide 70 has a vertical center line 82 which extends through pivot 74 and coincides with the electromagnetic center line 49 of apparatus 35.

Lumber 50 to be dried by this apparatus is directed between rollers 76 and 77 which apply substantially equal pressure to opposite edges of the lumber and so positions the longitudinal centerline thereof on the electromagnetic center line.

As stated above, a certain percentage of the microwave energy directed against the opposite edges of the lumber is transmitted therethrough, and the amount transmitted depends upon the moisture content of the lumber. As the moisture content of the lumber is constantly changing, it is desirable to control the power from the microwave generator in accordance with the changed moisture contents. This can be accomplished by positioning detectors 86 and 87 on the outer end sections 61 and 62 of waveguide channels 45 and 46, respectively. These detectors also known as directional power meters are well known and do not need description herein. These detectors are connected to a controller for the microwave generator 39 in the manner described hereinafter.

FIG. 6 illustrates a preferred form of drying apparatus 35a in accordance with this invention. In this example, the arms or channels 45 and 46 of waveguide system 40 are formed in a closed loop 90 having a single slot 91 therein through which path 48 extends. The same relationship as above exists between the effective lengths of channels 45 and 46 to the edges 66 and 65 of lumber 50 or to the electromagnetic center line 49. If in this case, the detector 86 for channel 45 were located in arm 46 and the detector 87 for channel 46 were located in arm 45, as indicated in broken line in FIG. 6, then there would be completed the transformation of FIG. 4 to FIG. 6 by squeezing all waveguide system components into one plane. However, if this were done a difficulty arises because the detector 86 not only measures that part of the power flowing through arm 45 that is transmitted through the lumber from C to D and beyond but also that part of the power flowing through arm 46 that is reflected at the lumber face D. Therefore the detectors 86 and 87 have been replaced by a single detector 96 in arm 20 which detector will measure, as will be shown later, the sum of the two transmitted powers flowing back to generator 39. For convenience another detector 97 can be added in arm 21 for the measurement of the reflected power flowing to waterload 42.

As stated above, all of the reflected microwave power or energy is directed back to waterload 42 and so the microwave generator 39 is protected against this. In actual practice, this happens only if the areas C and D of the lumber have the same reflection coefficient. Since C and D in FIG. 4 are spaced apart, the generator is protected only if the moisture content of the boards to be dried is relatively constant. If the moisture content in different areas of a given board or if the moisture content of successive boards is different, the reflection coefficient in apparatus 35 will be different, and the microwave generator can be exposed to reflected power. However, apparatus 35 can be used for lumber in which the moisture content does not vary greatly within boards or successive boards.

Apparatus 35a eliminates this problem since C and D are directly opposite each other or, in other words, the microwave generator "sees" substantially the same portion of each board.

When the energy or power transmitted through the lumber is used to control the output of the generator, the same problem arises with apparatus 35 since the power transmitted in channel 45 may be different from that transmitted in channel 46 at any given instance. Apparatus 35a also eliminates this problem.

The loop or ring waveguide system of apparatus 35a in FIG. 6 is considered to be much better than apparatus 35 for general purposes. If, in apparatus 35a, the path lengths a and b fulfill the following condition:

$$b = a + m \lambda / 2 \quad (1)$$

where λ is the MW wavelength in the waveguide and m is an integer, then all reflected power from the lumber faces C and D will flow to the waterload and all transmitted power exiting from the lumber faces D and C will flow to the generator.

FIG. 7 shows how the energy P flowing from the generator through port 20 is split into two equal parts P1 and P2, but P2 also obtained a 90° phase shift because it crossed the center line of the four-port hybrid. After travelling through the respective waveguides a and b , part of the energy is reflected back. Since both P1 and P2 "see" the same portion of the lumber (albeit from two different sides) the same part g of P1 and P2 is reflected back as P3 and P4, respectively. Since both arms a and b have been travelled twice by the time the four-port hybrid is reached, any additional phase shift due to $b \neq a$ amounts to a whole number of full wavelengths therefore has no influence. The only phase shift between P3 and P4 is that P4 is still 90° ahead of P3 (as was the case between P2 and P1).

In FIG. 8 illustrates what happens when P3 and P4 enter the four-port hybrid and try to split into two equal parts. In port 20 you then have P5 (or half of P3) and P8 (or the crossed over half of P4 which gets another 90° phase shift for crossing). These are now two electromagnetic wave systems of equal magnitude but with a 180° phase shift between them, therefore cancellation between the two wave systems will take place, thus prohibiting propagation towards the generator. In port 21 the two wave systems P6 and P7 from ports 16 and 17 are of the same magnitude and phase when they meet, therefore, they will reinforce each other and flow to the water load.

Since P5 and P8 have to go somewhere, they will act and reinforce each other in a manner identical to P6 and P7, respectively, and will also flow through port 21 to the water load. Therefore the amount of reflected power ending up in the water load is $P9 = P3 + P4 = gP$ or the total amount of the original P which has been reflected by the lumber.

As far as the transmitted power is concerned, there is a completely different result. In FIG. 9 P results in P1 flowing through arm a and P2 flowing through arm b (P2 has already a 90° phase shift). Those equal parts of P1 and P2 that are not reflected at the lumber faces C and D will enter the lumber where a certain fraction will be absorbed (the fraction depending on the lumber portion CD in the wave guide) and the remainder P1' and P2' will continue on their way through the wave guides b respectively a . If the transmission coefficient for the portion CD of the lumber is h and $(1-h) = k$ then you have:

$$P \rightarrow P1 = (P/2) \text{ through arm } a \rightarrow P1' = k P/2 \text{ through arm } b$$

and

$$P \rightarrow P2 = (P/2) + 90^\circ \text{ through arm } b \rightarrow P2' = k (P/2) + 90^\circ \text{ through arm } a$$

In FIG. 9 you find now (through an identical exercise as in FIG. 8) that the only way the transmitted power P2' and P1' can go is through port 20 towards the generator since port 21 is a prohibited area due to cancellation.

Since the transmitted power P' represents the amount of power which the lumber was unable to absorb and therefore is going to waste (in the generator) it should be kept to a tolerable minimum ΔP , depending on the wood properties. Therefore P' should be measured with detector 96 and used to control the output of the generator so that $P' \leq \Delta P$. In this way lumber of high moisture content and therefore very low in transmitted power, receives automatically maximum power while lumber of lower moisture content gradually receives less power, thus resulting in a slowdown of the drying process when the lumber reaches its desired final moisture content.

FIG. 10 diagrammatically illustrates a system for controlling the power output of microwave generator 39 in accordance with the moisture content of the lumber being subjected to the drying action of microwaves at any given instant. The detector or measurer 96 of transmitted microwave energy P' is operatively connected to an output control unit 100 for generator 39. The arrangement is such that as the moisture content of

the wood being "viewed" increases, the transmitted energy decreases and the output of the generator is increased, and vice versa.

I claim:

1. Microwave drying apparatus for moisture-laden dielectric material comprising a microwave generator, means for dividing microwave energy from the generator into two equal parts, and separate channels for directing said two energy parts to opposite sides of material to be dried, the length of one of said channels to the longitudinal center line of the material being equal to the length of the other of said channels plus a whole number of half wavelengths of the microwaves from said generator.

2. Microwave drying apparatus as claimed in claim 1 in which said channels are located to direct said two energy parts against directly opposite areas on said material.

3. Microwave drying apparatus as claimed in claim 1 including means for detecting the microwave energy that is transmitted through said material, and controlling means for regulating the output of the microwave generator inversely relative to the level of the transmitted energy.

4. Microwave drying apparatus for moisture-laden dielectric material comprising a waveguide having two channels extending to outer ends on opposite sides of a path along which material to be dried travels, said path having an electromagnetic center line and said material being guided to travel with its center line on said electromagnetic center line and between said two channel ends, a microwave generator, a four-port hybrid coupling the waveguide channels to the generator, the length of one of said channels to the electromagnetic center line being equal to the length of the other of said channels plus a whole number of half wavelengths of the microwaves from said generator, said waveguide channels directing microwave energy from the generator to opposite sides of material moving along said path.

5. Microwave drying apparatus as claimed in claim 4 in which said two channel ends are located close to each other.

6. Microwave drying apparatus as claimed in claim 4 in which said channel ends are located directly opposite from each other.

7. Microwave drying apparatus as claimed in claim 4 including control means operated by microwave energy transmitted through said material to control the output of the microwave generator inversely relative to the level of the transmitted energy.

8. Microwave drying apparatus as claimed in claim 4 in which said channel ends are located directly opposite from each other whereby microwave energy transmitted through said material travels back through said channels, and control means operated by said transmitted energy to control the output of the microwave generator inversely relative to the level of the transmitted energy.

9. Microwave drying apparatus as claimed in claim 4 including microwave energy absorption means coupled to one of the ports of said hybrid.

10. Microwave drying apparatus for moisture-laden dielectric material comprising a hybrid having a common central section and a longitudinal center line, a first pair of arms projecting from one end of the central section on opposite sides of the center line, a second pair of arms projecting from an opposite end of the central section on opposite sides of the hybrid center line, a microwave generator coupled to one arm of said second pair of arms so that microwave energy therefrom is directed through both of the arms of the first pair, a waveguide having two channels, one connected to each arm of said first pair, said two channels extending to outer ends on opposite sides of a path along which said material travels, said path having an electromagnetic center line and said material being guided to travel with its center line on said electromagnetic center line and between said two channel ends, the length of one of said channels to the electromagnetic center line being equal to the length of the other of said channels plus a whole number of half wavelengths of the microwaves from

said generator, said waveguide channels directing microwave energy from the generator to opposite sides of the material moving along said path.

11. Microwave drying apparatus as claimed in claim 10 in which said two channel ends are located close to each other.

12. Microwave drying apparatus as claimed in claim 10 in which said channel ends are located directly opposite from each other.

13. Microwave drying apparatus as claimed in claim 10 including control means operated by microwave energy transmitted through the said material to control the output of the microwave generator inversely relative to the level of the transmitted energy.

14. Microwave drying apparatus as claimed in claim 10 in which said channel ends are located directly opposite from each other whereby microwave energy transmitted through said material travels back through said channels, and control means operated by said transmitted energy to control the output of the microwave generator inversely relative to the level of the transmitted energy.

15. Microwave drying apparatus as claimed in claim 10 including microwave energy absorption means coupled to the other of said second pair of arms.

16. The microwave drying method which comprises dividing microwave energy from a microwave generator into two equal parts, and directing said energy parts through two separate channels to opposite sides of material to be dried, the distance of travel through one of said channels to the longitudinal center line of the material being equal to the distance of travel through the other of said channels to said center line plus a whole number of half wavelengths of the microwaves from said generator.

17. The method according to claim 16 in which said two microwave energy parts are directed by the channels to directly opposite areas on said material.

18. The method according to claim 16 including detecting the microwave energy transmitted through said material, and controlling the output of the microwave generator inversely relative to the level of the transmitted microwave energy.

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