The present invention relates to a method for compensating DC offset in a signal path comprising a plurality of stages, wherein for each stage a fine DC compensation is performed by introducing a fine DC compensation signal into the signal path of said stage by means of the compensation analog to digital converter, wherein said fine DC compensation signal is determined by setting the total gain of said stage to a value that equals the product of a first total gain of the preceding stage(s) and a first gain of said stage, setting at least two different DC compensation signals for said stage and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a first linear relationship between DC compensation signal and DC offset residual at the output of said signal path, setting the total gain of said stage to a value that equals the product of a second total gain of the preceding stage(s) and a second gain of said stage, setting at least two different DC compensation signals and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a second linear relationship between DC compensation signal and DC offset residual at the output of said signal path, setting the total gain of said stage to a value that equals the product of a second total gain of the preceding stage(s) and a second gain of said stage, setting at least two different DC compensation signals and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a second linear relationship between DC compensation value and gain, and determining an interception point of said first linear relationship and said second linear relationship, wherein the DC compensation signal of said interception point is the fine DC compensation signal.
The present invention relates to a method and device for compensating DC offset in RF transceivers. The present invention specifically relates to a method for performing fine DC offset compensation.

Integrated direct conversion RF transceiver architectures became popular in the last decade for many different RF applications. They require a minimal set of building blocks, see Fig. 1. Each RX or TX signal path requires only one mixer with associated local oscillator which also simplifies the synthesizer. An IF filter is no longer needed.

Direct conversion RF transceivers, e.g. for WLAN, did use more than one point to enter components like amplifier, mixer, filter etc. It may distort the signal, and directly limits the available dynamic range. Strong offsets can saturate the signal path and also violate the digital signal processing. It became common to compensate this DC offset by adding DC voltages opposite to the occurring DC offset. Several different solutions have been developed in the past.

One typical approach is providing additional hardware blocks as disclosed in US 6,756,924 B2 or US 7,271,649 B2 or Tanaka, T. Yamawaki, K. Takikawa, N. Hayashi, I. Ohno, T.Wakuta, S. Takahashi, M. Kasahara, and B. Henshaw, "GSM/DCS 1800 Dual Band Direct-Conversion Transceiver IC With a DC Offset Calibration System," in 01 ESSCIRC Session 3.3, 2001. These blocks are typically dedicated to individual building blocks. The DC offset is measured and compensated. This approach requires additional elements not only for compensation, e.g. DACs, but also for measuring the DC offset and for determining the value needed for compensation. These blocks are running permanently. They increase the system complexity and consume additional power and space.

Other approaches determine the DC offset and the resulting DC compensation values permanently in the digital domain as disclosed in Marko Mailand and Hans-Joachim Jentschel, "Compensation of DC-Offsets and RF-Self-Mixing in Products in Six-Port-Based Analog Direct Receivers," in 14th IST Mobile & Wireless Communication Summit, Dresden, June 2005; or Russell Hoppenstein, "DC Offset Auto-Calibration of TRF371x," Texas Instruments, 2010; or I.-H. Sohn, E.-R. Jeong, and Y. H. Lee, "Data-Aided Approach to I/Q Mismatch and DC Offset Compensation in Communication Receivers," IEEE COMMUNICATIONS LETTERS, vol. 6, no. 12, December 2002. The compensation values are introduced by a DAC in the analog section. But this concept prepares only one set of compensation values. This is working well if the system gain is fixed. But systems with variable gain make the DC offset variably as well. Therefore every new gain configuration requires new DC offset values to be measured and new compensation values to be set. This increases the steps to be done to change the gain as additional calibration steps must be executed as well for every new gain setting. Setting the gain becomes more complex and time consuming.

Fig. 1 shows a state-of-the-art direct conversion receiver comprising a plurality of components like low noise amplifier 12, mixer 13, filter 14, VGA 15, ADC 16, digital DC offset compensation 17 between radio frequency (RF) input 11 and baseband (BB) output. Direct conversion RF transceivers, e.g. for WLAN, did use more than one point to enter DC compensation voltages by additional DACs 18, 19. These DC compensation voltages (the calibration parameters) were typically determined from different measurements and from calculations in the digital domain, e.g. by a signal processor. It is common to add short cut and bypass switches to the individual transceiver/receiver components to measure the DC offset that occurs at each individual stage separately. Therefore, some of the components were operated under debug/test conditions (bypass or short cut mode) instead of the real operation conditions while the DC offset is measured. This introduces additional errors, e.g. due to different bias or temperature conditions, and increases the system complexity.

It is generally intended to find a set of calibration parameters that covers the complete gain control range. But this is not common in present implementations as the accuracy of the determined calibration parameters is insufficient. Therefore, the complete gain control range is split into several different sub ranges. Each different sub range has an own set of set of calibration parameters. Changing the gain from one sub range to another requires also the calibration parameters to be changed which is still complex and time consuming. The transceiver (Rx path) with DC offset sources and compensation DACs (digital to analog converters) given in Fig. 1, can be simplified, see Fig.2, to a set of variable gain stages 23 corresponding to mixer 13, 24 corresponding to filter 14, 25 corresponding to VGA 15 between RF input 21 and BB output 210, where the DC offset 211, 212, 213 and the compensation DACs 28 and 29 are connected to the input of each individual stage. This remaining voltage nonzero DC voltage
becomes amplified by the gain stages that follow. As this gain is variable the resulting DC offset at the output of said signal path directly depends on the following total gain and the DC offset residual:

\[
\text{mean}\left(BB_{out}(A_{tot,k})\right) = A_{tot,k} \ast (DC_{off,k} + DC_{comp,k})
\]

[0009] The total gain for the gain stage k (k>0) is given by:

\[
A_{tot,k} = \prod_{j=1}^{k} A_{j,i}
\]

[0010] Therefore, a good calibration algorithm should find values DC_{comp,k} that meet the relation:

\[
0 \approx DC_{off,k} + DC_{comp,k}
\]

[0011] The essential part of the calibration routines is therefore to determine DC_{off,k} accurately from different measured mean (BB_{out}) values so that

\[
DC_{comp,k} = -DC_{off,k}
\]

[0012] Throughout this document the following notation will be used:

- number of total gain stages: \( n \)
- DC offset of gain stage k: \( DC_{off,k} \)
- DC compensation parameter of gain stage k: \( DC_{comp,k} \)
- DC offset residual of gain stage k: DC_{off,k} + DC_{comp,k}
- gain control range R of gain stage k: \( A_{k,R} \)
- gain i of stage k, were \( A_{k,i} \) element of \( A_{k,R} \): \( A_{k,i} \)
- total gain for gain stage k: \( A_{tot,k} \)
- DC offset residual at ADC output (BB_{out}): \( DC_{res} \)

Disclosure of the Invention

[0013] It is therefore an objective of the present invention to provide a method for compensating DC offset in radio frequency transceiver architectures having an improved efficiency. It is specifically an objective of the present invention to provide an improved DC offset calibration method for RF transceivers with variable gain that provide multiple points with compensation DACs (digital to analog converters) for DC offset compensation.

[0014] This objective is achieved by a method according to the independent claim. Dependent claims relate to further aspects of the present invention.

[0015] The present invention relates to a method for compensating DC offset in a signal path comprising a plurality of stages, each stage k having an individual gain \( A_k \) and a total gain \( A_{tot,k} \) that is the product of the gains of all preceding stages and the gain of said stage:

\[
A_{tot,k} = A_k \ast A_{tot,k-1}.
\]

[0016] For each stage a fine DC calibration is performed by introducing a raw DC compensation signal \( DC_{comp,k} \) into the signal path of said stage by means of an compensation analog to digital converter that is electrically coupled to said...
The procedure is based on finding intersection points were the intersection points found represent the best compensation values. At least two lines, e.g. four points are required for obtaining one DC compensation signal. One line represents a set of different compensation DAC values for the dedicated gain of the stage behind the compensation DAC. Measurement values for at least two gain configurations are mandatory. More gains are possible. More measurement points for one gain configuration may help to increase the accuracy and eliminate nonlinearities of the compensation DACs.

A fine DC compensation signal is determined by setting the total gain of said stage to a value that equals the product of a first total gain of the preceding stage(s) and a first gain of said stage, setting at least two different DC compensation signals for said stage and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a first linear relationship between DC compensation signal and DC offset residual at the output of said signal path, setting the total gain of said stage to a value that equals the product of a second total gain of the preceding stage(s) and a second gain of said stage, setting at least two different DC compensation signals and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a second linear relationship between DC compensation value and gain, and determining an interception point of said first linear relationship and said second linear relationship, wherein the DC compensation signal of said interception point is the fine DC compensation signal.

The fine DC compensation may be performed stage by stage starting with the stage that is closest to the input of said signal path, i.e. closest to RF input, \( k=n \).

The fine DC compensation may be performed stage by stage starting with the stage that is closest to the output of said signal path. Here, several iterations are required.

One aspect of the fine DC calibration relates to the setting of the total gain of the preceding stages. The first and/or the second total gain of the preceding stages are preferably set to the mean total gain of the preceding stages. Therefore, the total gain of the preceding gain stages are constant and approximately in the middle of the used control range.

One aspect of the fine DC calibration relates to the setting of the gain of said stage. The first gain of said stage is preferably set to the minimum gain of said stage. The second gain of said stage is preferably set to the maximum gain of said stage.

The calibration coefficients obtained by the fine DC compensation keep the gain dependency of the DC offset residuum small.

One aspect of the present invention relates to performing a raw DC calibration prior to the fine DC calibration. The raw DC calibration increases the stability of the calibration process so that the entire calibration procedure works for huge DC offsets. Raw DC calibration can be hardware supported and comprise any method referred to in the prior art section. Raw DC calibration methods have a broader error tolerance range compared to fine DC calibration methods. Usually raw DC calibration methods also converge faster.

For each stage a raw DC calibration may be performed by introducing a raw DC compensation signal \( DC_{\text{comp},k} \) into the signal path of said stage by means of a compensation digital to analog converter that is electrically coupled to said stage.

The raw DC compensation is performed stage by stage starting with the stage that is closest to the output of said signal path. Said raw DC compensation signal for said stage is determined by performing the steps:

(a) setting the total gain of said stage,
(b) measuring a DC offset residual at the output of said signal path,
(c) setting the raw DC compensation signal to a value that is the negative of the DC offset residual divided by the total gain of said stage.

For each stage a raw DC calibration may be performed by introducing a raw DC compensation signal \( DC_{\text{comp},k} \) into the signal path of said stage by means of a compensation digital to analog converter that is electrically coupled to said stage.

(a) setting the total gain of said stage,
(b) measuring a DC offset residual at the output of said signal path,
(c) setting the raw DC compensation signal to a value that is the negative of the DC offset residual divided by the total gain of said stage.

One aspect of the raw DC calibration relates to augmenting the method by one calibration loop comprising the steps:

(d) setting the total gain of said stage
(e) measuring a DC offset residual at the output of said signal path,
(f) setting the raw DC compensation signal to a value that is the difference between the previously set raw DC compensation signal and the DC offset residual divided by the total gain of said stage.

One aspect of the raw DC calibration relates to iteratively determining the raw DC compensation signals for m
calibration iterations. The DC compensation parameter of gain stage \( k \), \( \text{DC}_{\text{comp},k} \) can be calculated from the known total gain \( A_{\text{tot},k} \) and the measured DC offset residual \( \text{DC}_{\text{res}} \) by the formula:

\[
\text{DC}_{\text{comp},k,m} = \text{DC}_{\text{comp},k,m-1} - \frac{\text{DC}_{\text{res},m}}{A_{\text{tot},k}}
\]

where \( \text{DC}_{\text{comp},k,0} = 0 \).

[0029] One aspect of the raw DC calibration relates to the selection of the total gain \( A_{\text{tot},k} \) of each gain stage. It is preferably selected to be approximately in the middle between its minimum and maximum:

\[
A_{\text{tot},k} \approx \frac{A_{\text{tot},k,\text{max}} - A_{\text{tot},k,\text{min}}}{2}
\]

[0030] The computed calibration coefficients obtained by the raw DC calibration are good enough to prevent the system from saturation while the fine DC calibration is performed.

[0031] Therefore, the present invention provides a method for determining a set of calibration parameters \( \text{DC}_{\text{comp},k} \) having the advantage of covering the complete gain control range from \( A_{\text{tot},n,\text{min}} \) to \( A_{\text{tot},n,\text{max}} \) so that changing the gain does not require any additional calibration tasks or calibration parameter changes.

[0032] It is another advantage of the present invention that the transceiver operates close to regular operation mode during calibration. Thus, unwanted measurement errors due to different device states, e.g., different bias and temperature conditions are avoided. Only loop back functionality might be needed. Power down or feed trough operation is not required.

[0033] It is yet another advantage of the present invention that only DC offset compensation elements, e.g., DACs that are common in present RF transceivers are required.

Brief Description of the Drawings

[0034] The method and the device according to the invention are described in more detail herein below by way of exemplary embodiments and with reference to the attached drawings, in which:

- Fig. 1 shows a state-of-the-art direct conversion receiver architecture,
- Fig. 2 shows a simplified receiver model,
- Fig. 3 shows a mathematical receiver model,
- Fig. 4 shows a flow chart of a raw DC offset calibration algorithm,
- Fig. 5 shows a diagram of functional relationships between DC offset compensation parameters and DC offset residuals, and
- Fig. 6 shows a flow chart of an algorithm for gain independent offset calibration.

Embodiments of the Invention

[0035] Fig. 5 shows a diagram of a functional relationship of fine DC compensation signal and DC residual for one specific embodiment of the fine DC calibration procedure, wherein for each of the channels I and Q a calibration result is obtained by determining the first linear relationship for I and Q and the second linear relationship for I and Q and intersecting them in order to find the optimal DC compensation signal for I and Q.

[0036] Fig. 6 shows a flow chart of an embodiment of the fine DC calibration algorithm. In step 61 the stage index \( k \) is set to \( n+1 \), wherein \( n \) is the number of stages. The loop for a single stage comprises the steps 62 to 612, wherein the loop is left in step 613 in case all stages have been computed. In the following step 62 the stage index \( k \) is decremented by 1. Therefore, the following steps that relate to a single gain stage start with stage \( k=n \), which is the stage closest to RF input. The total gain of the preceding stages \( A_{\text{tot},k-1} \) and the first gain \( A_{k,1} \) of stage \( k \) is set in step 63. The first gain \( A_{k,1} \) is set to the minimum of \( A_{k} \). In the first inner loop having loop index \( i \) and comprising the steps 64 and 65 the first linear relationship is determined for gain \( A_{k,1} \). At least two points are needed, but up to \( x \) points may be computed, step 66. In step 64 the DC compensation signal \( \text{DC}_{\text{comp},k,1} \) is set. In step 65 the DC offset residual \( \text{DC}_{\text{res},i} \) is measured at the output of the signal path. In the first inner loop the first DC compensation signal is set to its maximum and the second DC compensation signal is set to its minimum. Further DC compensation signals may be set somewhere in between. In step 67 the total gain of the preceding stages \( A_{\text{tot},k-1} \) and the second gain \( A_{k,m} \) of stage \( k \) is set. The second gain \( A_{k,m} \)
is set to its maximum value. In the second inner loop having loop index i and comprising the steps 68 and 69 the second linear relationship is determined for gain $A_{k,m}$. At least two points are needed, but up to $x$ points may be computed, step 66. In step 64 the DC compensation signal $DC_{comp,k,i}$ is set. In step 65 the DC offset residual $DC_{Res,l,i}$ is measured at the output of the signal path. In the first inner loop the first DC compensation signal is set to its maximum and the second DC compensation signal is set to its minimum. Further DC compensation signals may be set somewhere in between. In step 611 the DC compensation signal $DC_{comp,k}$ for stage $k$ is computed. In step 612 the DC compensation signal $DC_{comp,k}$ is set.

**Fig. 4** shows a flow chart of an embodiment of a raw DC compensation algorithm that is executed before the fine DC compensation is performed. In step 41 the algorithm is initialized by setting the stage index and the calibration iteration index to zero. The outer loop comprising steps 42 to 49 refers to the computation of raw DC offset compensation signals for all stages. In step 42 the stage index $k$ is incremented by one. In step 49 the outer loop is left in case all stages have been computed. The inner loop comprising steps 43 to 48 refers to the computation of raw DC compensation signals for a single stage $k$. In step 43 the calibration index $m$ is incremented by one. In step 44 the gain of stage $k$ is set. In step 45 the resulting DC offset residual $DC_{RES,m}$ is measured. In step 46 the DC compensation signal $DC_{comp,k,m}$ is computed. In step 47 the DC compensation signal $DC_{comp,k,m}$ is set. The inner loop is executed three times according to step 48.

While the invention has been illustrated and described in detail in the drawings and foregoing description, such illustration and description are to be considered illustrative or exemplary and not restrictive. It will be understood that changes and modifications may be made by those of ordinary skill within the scope and spirit of the following claims.

**Claims**

1. Method for compensating DC offset in a signal path comprising a plurality of stages, wherein for each stage a fine DC compensation is performed by introducing a fine DC compensation signal into the signal path of said stage by means of the compensation digital to analog converter, wherein said fine DC compensation signal is determined by setting the total gain of said stage to a value that equals the product of a first total gain of the preceding stage(s) and a first gain of said stage, setting at least two different DC compensation signals for said stage and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a first linear relationship between DC compensation signal and DC offset residual at the output of said signal path, setting the total gain of said stage to a value that equals the product of a second total gain of the preceding stage(s) and a second gain of said stage, setting at least two different DC compensation signals and measuring a DC residual signal at the output of the signal path for each of the two different DC compensation signals in order to determine a second linear relationship between DC compensation signal and DC offset residual at the output of said signal path, and determining an interception point of said first linear relationship and said second linear relationship, wherein the DC compensation signal of said interception point is the fine DC compensation signal.

2. Method according to claim 1, wherein the fine DC compensation is performed stage by stage starting with the stage that is closest to the input of said signal path.

3. Method according to claim 1, wherein the fine DC compensation is performed stage by stage starting with the stage that is closest to the output of said signal path.

4. Method according to any of claims 1 to 3, wherein the first total gain of the preceding stage(s) is the mean total gain of the preceding stage(s).

5. Method according to any of claims 1 or 4, wherein the second total gain of the preceding stage(s) is the mean total gain of the preceding stages.

6. Method according to any of claims 1 to 5, wherein the first gain of said stage is the minimum gain of said stage.

7. Method according to any of claims 1 to 6, wherein the second gain of said stage is the maximum gain of said stage.

8. Method according to any of claims 1 to 7, wherein one of said different DC compensation signals is a minimum DC compensation signal and/or one of said different compensation signals is a maximum DC compensation signal.
9. Method according to any of claims 1 to 8 wherein prior to the fine DC compensation a raw DC compensation is performed.

10. Method according to claim 9, wherein for each stage the raw DC compensation is performed by introducing a raw DC compensation signal into the signal path of said stage by means of a compensation digital to analog converter that is electrically coupled to said stage; wherein the raw DC compensation is performed stage by stage starting with the stage that is closest to the output of said signal path; wherein said raw DC compensation signal for said stage is determined by performing the steps:

   (a) setting the total gain of said stage
   (b) measuring a DC offset residual at the output of said signal path,
   (c) setting the raw DC compensation signal to a value that is the negative of the DC offset residual divided by the total gain of said stage.

11. Method according to claim 10, wherein said raw DC compensation signal for said stage is determined by further performing the following steps:

   (d) setting the total gain of said stage
   (e) measuring a DC offset residual at the output of said signal path,
   (f) setting the raw DC compensation signal to a value that is the difference between the previously set raw DC compensation signal and the DC offset residual divided by the total gain of said stage.

12. Method according to claim 11, wherein said raw DC compensation signal for said stage is determined by further performing the following step:

   (g) repeating steps (d) to (f).

13. Method according to claim 10 to 12, wherein the total gain of said stage is set to a value that is arithmetic mean of a maximum total gain of said stage and a minimum total gain of said stage.
FIG 1

Typical direct conversion receiver architecture.
FIG 2  Simplified receiver model with DC offset sources, compensation DACs and variable gain blocks.
FIG 3  Mathematical receiver model with variable gain blocks, DC offset and DC compensation sources.
FIG 4

Simple algorithm for raw DC offset calibration.

start calibration

41 \[ k=0, m=0 \]

42 \[ k=k+1, m=0 \]

single gain stage

43 \[ m=m+1 \]

44 \[ \text{set } A_{\text{tot},k} \]

45 \[ \text{measure } DC_{\text{RES}, m} \text{ at ADC output} \]

46 \[ \text{calculate } DC_{\text{comp}, k, m} \text{ from } DC_{\text{RES}, m} \text{ and } A_{\text{tot}, k} \]

47 \[ \text{set } DC_{\text{comp}, k, m} \]

48 \[ m<3 \]

49 \[ k<n \]

yes

no

yes

no

calibration finished
FIG 5

Determination of the compensation parameters $DC_{\text{comp}, k}$ for gain stage $k$. 

- Mean $|BB_{\text{out}}|$
- $DC_{\text{comp}, k}$
- Calibration result, I
- Calibration result, Q

$Ak, i$
$Ak, m$
$51q$
$52q$
$53q$
$51i$
$53i$
Algorithm for gain independent DC offset calibration.

1. Start calibration
2. $k = n + 1$
3. $k = k - 1$
4. Set $A_{tot, k-1, A_k, i}$
5. Set $DC_{comp, k, i}$
6. Measure $DC_{RES, i, i}$ at ADC output
7. For $i = 1: x$
8. Set $A_{tot, k-1, A_k, m}$
9. Set $DC_{comp, k, i}$
10. Measure $DC_{RES, m, i}$ at ADC output
11. For $i = 1: x$
12. Calculate $DC_{comp, k}$
13. Set $DC_{comp, k}$
14. $k > 1$? Yes, go back to 1. No, calibration finished.
## DOCUMENTS CONSIDERED TO BE RELEVANT

<table>
<thead>
<tr>
<th>Category</th>
<th>Citation of document with indication, where appropriate, of relevant passages</th>
<th>Relevant to claim</th>
<th>CLASSIFICATION OF THE APPLICATION (IPC)</th>
</tr>
</thead>
</table>

The present search report has been drawn up for all claims.

**Place of search:** The Hague  
**Date of completion of the search:** 25 May 2012  
**Examiner:** Niederholz, Jürgen
This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

25-05-2012

<table>
<thead>
<tr>
<th>Patent document cited in search report</th>
<th>Publication date</th>
<th>Patent family member(s)</th>
<th>Publication date</th>
</tr>
</thead>
<tbody>
<tr>
<td>US 2007184803 A1</td>
<td>09-08-2007</td>
<td>NONE</td>
<td></td>
</tr>
<tr>
<td>US 2006284671 A1</td>
<td>21-12-2006</td>
<td>CN 1881788 A</td>
<td>20-12-2006</td>
</tr>
<tr>
<td></td>
<td></td>
<td>JP 4628881 B2</td>
<td>09-02-2011</td>
</tr>
<tr>
<td></td>
<td></td>
<td>JP 2006352401 A</td>
<td>28-12-2006</td>
</tr>
<tr>
<td></td>
<td></td>
<td>US 2006284671 A1</td>
<td>21-12-2006</td>
</tr>
<tr>
<td>US 7239199 B1</td>
<td>03-07-2007</td>
<td>NONE</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>JP 2002217762 A</td>
<td>02-08-2002</td>
</tr>
<tr>
<td></td>
<td></td>
<td>US 2002094792 A1</td>
<td>18-07-2002</td>
</tr>
<tr>
<td></td>
<td></td>
<td>EP 1949715 A2</td>
<td>17-09-2008</td>
</tr>
<tr>
<td></td>
<td></td>
<td>JP 2009522936 A</td>
<td>11-06-2009</td>
</tr>
<tr>
<td></td>
<td></td>
<td>KR 20080084852 A</td>
<td>19-09-2008</td>
</tr>
<tr>
<td></td>
<td></td>
<td>WD 2007081795 A2</td>
<td>19-07-2007</td>
</tr>
<tr>
<td></td>
<td></td>
<td>JP 2008535377 A</td>
<td>28-08-2008</td>
</tr>
<tr>
<td></td>
<td></td>
<td>KR 20088002806 A</td>
<td>04-01-2008</td>
</tr>
<tr>
<td></td>
<td></td>
<td>US 2006222117 A1</td>
<td>05-10-2006</td>
</tr>
<tr>
<td></td>
<td></td>
<td>WD 2006107466 A2</td>
<td>12-10-2006</td>
</tr>
</tbody>
</table>

For more details about this annex: see Official Journal of the European Patent Office, No. 12/82
REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader’s convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

- US 6756924 B2 [0004]
- US 7271649 B2 [0004]

Non-patent literature cited in the description

- TANAKA, T. YAMAWAKI; K. TAKIKAWA; N. HAYASHI; I. OHNO; T.WAKUTA, S. TAKAHASHI; M. KASAHARA; B. HENSHAW. GSM/DCS 1800 Dual Band Direct-Conversion Transceiver IC With a DC Offset Calibration System. 01 ESSCIRC Session 3.3, 2001 [0004]
- MARKO MAILAND; HANS-JOACHIM JENTSCHEL. Compensation of DC-Offsets and RF-Self-Mixing Products in Six-Port-Based Analog Direct Receivers. 14th IST Mobile & Wireless Communication Summit, June 2005 [0005]
- RUSSELL HOPPENSTEIN. DC Offset Auto-Calibration of TRF371x. Texas Instruments, 2010 [0005]