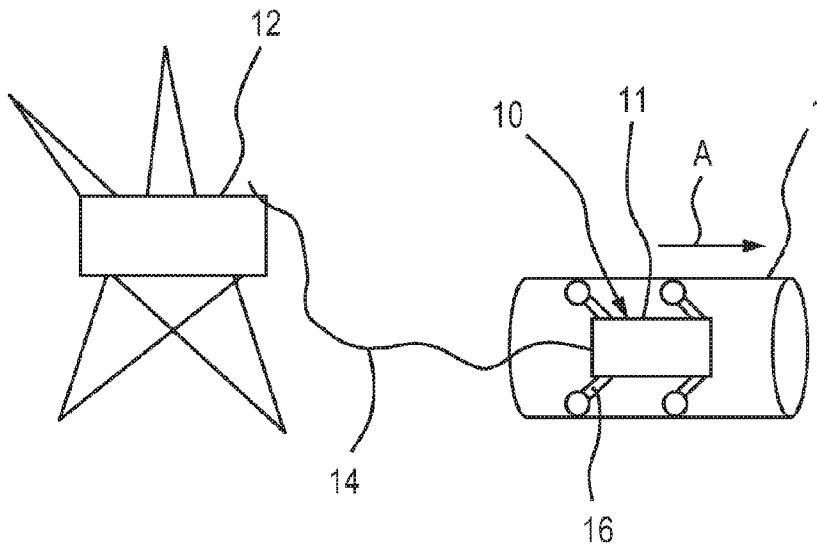




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 (54) Title: METHOD AND APPARATUS FOR ACOUSTIC ASSESSMENT FROM THE INTERIOR OF FLUID CONDUITS



(57) **Abrégé/Abstract:**

The invention provides a method and apparatus for assessing a condition of a fluid conduit from its interior. The method comprises providing a measurement apparatus comprising at least one wideband acoustic transducer within the fluid conduit and transmitting a wideband acoustic signal from the measurement apparatus to excite a broadside resonance in at least a portion of the fluid conduit. A wideband acoustic signal is received in the measurement apparatus due to a broadside resonant response of the fluid conduit to obtain a wideband acoustic data set; and the data set is analysed to assess the condition of the fluid conduit.

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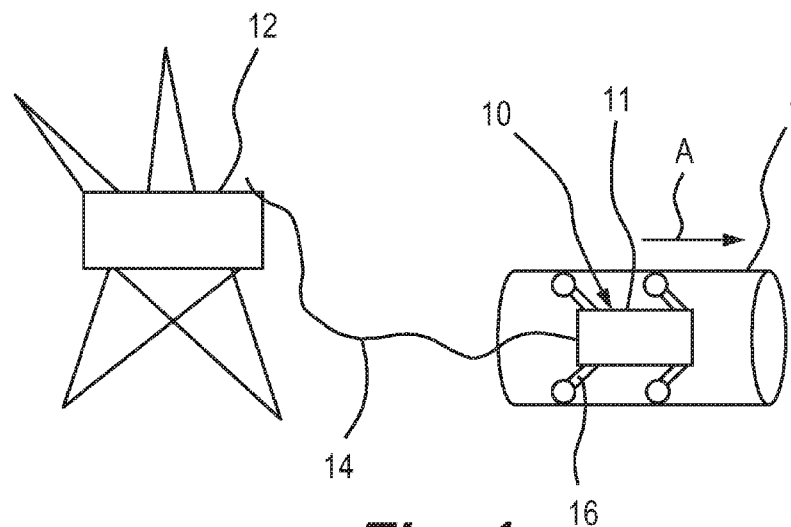
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(54) Title: METHOD AND APPARATUS FOR ACOUSTIC ASSESSMENT FROM THE INTERIOR OF FLUID CONDUITS

**Fig. 1**

(57) Abstract: The invention provides a method and apparatus for assessing a condition of a fluid conduit from its interior. The method comprises providing a measurement apparatus comprising at least one wideband acoustic transducer within the fluid conduit and transmitting a wideband acoustic signal from the measurement apparatus to excite a broadside resonance in at least a portion of the fluid conduit. A wideband acoustic signal is received in the measurement apparatus due to a broadside resonant response of the fluid conduit to obtain a wideband acoustic data set; and the data set is analysed to assess the condition of the fluid conduit.

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**METHOD AND APPARATUS FOR ACOUSTIC ASSESSMENT FROM THE
INTERIOR OF FLUID CONDUITS**

1

2

3 The present invention relates to methods and apparatus for the acoustic assessment of
4 fluid conduits or their features from their interiors, particularly but not exclusively to
5 methods and apparatus assessing the condition of features of surface, subsea or
6 subterranean pipelines, risers including marine and/or flexible risers, tubing including
7 subterranean well tubing, and other fluid conduits used in the hydrocarbon exploration,
8 production and transportation industries.

9

10 Aspects of the invention are methods and apparatus which use acoustic techniques for the
11 assessment and monitoring of the internal condition of fluid conduits from their interiors,
12 including the build-up and deposition of scale, sand, waxes and other materials on the
13 interior surface of conduits. Alternative aspects of the invention are methods and
14 apparatus which use acoustic techniques for the assessment, monitoring and inspection of
15 the physical condition of a fluid conduit from its interior including defects, wall thickness,
16 damage, holes, cracks and corrosion of a conduit or its layers.

17

18

1 Background to the invention

2

3 Ultrasound transducers have been used in pipeline pigging applications to measure or
4 map the profile of the inner diameter of a pipeline using single frequency pulses.

5

6 Wideband acoustic measurement techniques, which may be referred to as bio-sonar
7 acoustic or bio-acoustic measurement techniques have been used in applications to detect
8 and/or characterise buried objects. Examples are described in Y. Pailhas et al. (2010)
9 (reference [1]) and P. Moore et al. (reference [2]).

10

11 WO 2007/123418 (reference [3]) describes an acoustic method and apparatus for
12 detecting a hydrate presence in a hydrocarbon pipeline. The technique relies on acoustic
13 resonance frequencies of the pipeline walls, which imposes limitations on the application
14 of the method to the detection or assessment of a wide range of fluid conduit conditions
15 and on the manner in which the apparatus can be deployed.

16

17 US 7,246,522 (reference [4]) discloses a device and method for multiparameter acoustic
18 inspection of containers. The methods utilise dual acoustic signatures to discriminate
19 between various fluids and materials for identification purposes. The methods rely on
20 excitation of point resonances from the outside of the containers being inspected.

21

22 WO 2010/107712 (reference [5]) describes a method and apparatus for ultrasonic
23 inspection of a wall of a mechanical structure. The techniques are stated to use low power
24 consumption equipment to facilitate remote operation. The methods are external, non-
25 invasive techniques.

26

27 US 2007/0019506 (reference [6]) describes an ultrasonic imaging method for wells and
28 tubulars using a wideband acoustic pulse fired at a wall to measure wall thickness.

29

30 It is amongst the aims and objects of the invention to provide a method of assessing a fluid
31 conduit condition from the interior of the conduit which is improved with respect to prior art
32 methods and apparatus for acoustic assessment. It is another aim of invention to apply
33 bio-inspired acoustic pulses to the assessment of fluid conduit conditions from their
34 interiors. Further aims and objects of the invention will become apparent from the
35 following description.

1

2 Summary of the invention

3

4 According to a first aspect of the invention there is provided a method of assessing a
5 condition of a fluid conduit from its interior, the method comprising:

6 providing a measurement apparatus comprising at least one wideband acoustic transducer
7 within the fluid conduit;

8 transmitting a wideband acoustic signal from the measurement apparatus to excite a
9 broadside resonance in at least a portion of the fluid conduit;

10 receiving a wideband acoustic signal in the measurement apparatus due to a broadside
11 resonant response of the fluid conduit to obtain a wideband acoustic data set; and

12 analysing the wideband acoustic data set to assess the condition of the fluid conduit.

13

14 In the context of this specification, broadside resonance of the fluid conduit is defined as a
15 resonance excited by a plane acoustic wave incident on the inner surface of the wall of the
16 fluid conduit at an angle of substantially 90 degrees (substantially perpendicular) to the
17 axis of symmetry of the conduit (or longitudinal axis). Broadside resonant response is the
18 response elicited by a plane acoustic wave incident on the inner surface of the wall of the
19 fluid conduit at an angle of substantially 90 degrees (substantially perpendicular) to the
20 axis of symmetry of the conduit (or longitudinal axis).

21

22 Using a broadside resonant response gives more effective echo energy capture and thus
23 the received signal contains more information across a wide range of frequencies. The
24 invention in this aspect differs from the traditional spot acoustic techniques of the prior art,
25 in which the frequency is chosen to resonate a very localised area. Typically in the prior art
26 systems the frequency is a function of wall thickness. In contrast, the method of the
27 present invention may select frequencies which resonate the fluid conduit, or at least a
28 portion of the fluid conduit, by exciting lamb waves in the fluid conduit structure. Other
29 methods use narrowband analysis to arrive at a measurement, by 'tuning' between
30 frequency and thickness of a fluid conduit wall, rather than a genuine wideband acoustic
31 approach.

32

33 The method may comprise using beam forming transmission and/or reception techniques.

34

1 At least one of the transmitted or received wideband acoustic signals may be transmitted
2 or received with an axial beamwidth corresponding to a maximum angle of deviation of the
3 longitudinal axis of the measurement apparatus with the longitudinal or along track axis of
4 the fluid conduit.

5

6 Thus the axial beamwidth is selected to compensate for axial misalignment of the
7 measurement apparatus in the fluid conduit by maintaining a substantially perpendicular
8 acoustic wave incident on an inner wall of the fluid conduit, throughout the range of
9 possible misalignment of the measurement apparatus in the fluid conduit.

10

11 In the context of this specification, the term "assessing the condition of a fluid conduit" is
12 used to generally to refer to the overall state of the flow path defined by fluid conduit
13 (primarily the effective flow area of the conduit), including one or more features of its
14 internal condition which may be affected for example by build-up and deposition of scale,
15 sand, waxes and other materials on the interior surface, and its inherent physical condition
16 which may include the presence of defects, damage, holes, cracks, wall thickness and
17 corrosion of the conduit or a part thereof.

18

19 The invention has particular application to detecting the presence of, measuring the extent
20 of, and/or identifying the composition of deposits, debris and foreign bodies within fluid
21 conduits.

22

23 The wideband acoustic signal may comprise at least one frequency in the range of
24 approximately 150 kHz to approximately 10 MHz, and may comprise a distribution of
25 frequencies between 150 kHz and 10 MHz.

26

27 The wideband acoustic signal may comprise a lower frequency of approximately 150 kHz,
28 and an upper frequency of approximately 1 MHz, and may comprise a distribution of
29 frequencies between the upper and lower frequencies. Preferably, the wideband acoustic
30 signal comprises a lower frequency greater than 150 kHz, an upper frequency of less than
31 1MHz, and comprises a distribution of frequencies between the upper and lower
32 frequencies. In another embodiment, the wideband acoustic signal comprises a lower
33 frequency of at least 150 kHz, an upper frequency which is at least twice the lower
34 frequency, and comprises a distribution of frequencies between the upper and lower
35 frequencies. The upper frequency may therefore be at least one octave above the lower

1 frequency. In another embodiment, the upper frequency is at least two octaves above the
2 lower frequency, and in another is at least three octaves above the lower frequency. The
3 upper frequency may be less than four octaves above the lower frequency.

4

5 Frequencies above 150kHz facilitate plane wave formation and mitigate against near-field
6 corruption of measurements.

7

8 Preferably, the method comprises transmitting a wideband acoustic signal from the
9 measurement apparatus, through a fluid which couples the measurement apparatus to at
10 least a portion of the fluid conduit. The method may therefore be a non-contact method, in
11 which a transmission transducer does not physically contact the fluid conduit directly. The
12 fluid conduit may therefore be a fluid-filled conduit.

13

14 Preferably, the method comprises maintaining a distance between the at least one
15 transducer and the fluid conduit to avoid near-field interference effects. This has the
16 advantage of avoiding interference with the fluid conduit or any material on the interior of
17 the fluid conduit, and enables the measurement apparatus to be translated within the fluid
18 conduit at a desirable (higher or more consistent) speed.

19

20 The measurement apparatus may comprise a pipeline pig. Preferably the method
21 comprises translating the measurement apparatus within the fluid conduit.

22

23 Preferably the measurement apparatus is translated within the fluid conduit (which may be
24 a pipeline) at a speed between 0 m/s and 6 m/s during measurement operations.

25 Translation speeds may be selected according to measurement precision demanded for a
26 particular application: for a given beamwidth and pulse length, a higher the translation
27 speed will insonify a greater area of the fluid conduit inner wall with a single pulse, and
28 therefore a larger area will contribute to the measured response. A consequence is a less
29 precise localisation of any measurement made.

30

31 The method may comprise transmitting a plurality of wideband acoustic pulses separated
32 in time. The method may comprise transmitting a plurality of wideband acoustic pulses at
33 a fixed transmission rate, i.e. at regular time intervals. The transmission rate may be
34 determined by the fluid conduit diameter and/or the speed of sound in a medium within the

1 fluid conduit. The transmission rate may be less than 2 kHz, and preferably is 1.8 kHz or
2 less.

3

4 Alternatively, or in addition, the method may comprise triggering the transmission and/or
5 sampling of subsequent wideband acoustic pulses according to a distance translated by
6 the measurement apparatus in the fluid conduit. For example, the method may comprise
7 triggering the transmission and/or sampling of subsequent wideband acoustic pulses when
8 a fixed distance is travelled by the measurement apparatus. The distance may be less
9 than 100mm, and preferable is less than 20mm. In preferred embodiments the distance is
10 10mm or 3.3 mm. The transmission and/or sampling rate may be less than 2 kHz, and
11 preferably is 1.8 kHz or less.

12

13 The fluid conduit may be an elastic conduit, for example (without limitation) a carbon steel
14 pipe, a plastic or polymeric pipe, or a flexible pipe or flexible riser.

15

16 Preferably, the method comprises transmitting a wideband acoustic pulse with a duration
17 of at least 10 times the acoustic wave period (or in other words, a pulse comprising at least
18 10 acoustic wavelengths λ). The method may comprise transmitting a wideband
19 acoustic pulse with a duration of less than 100 μ S, and may comprise transmitting a
20 wideband acoustic pulse with a duration of less than 70 μ S. For higher frequencies,
21 shorter pulse durations may be used. For example, the method may comprise transmitting
22 a wideband acoustic pulse with a duration of less than 20 μ S, and may comprise
23 transmitting a wideband acoustic pulse with a duration of less than 5 μ S.

24

25 Preferably, the pulse duration is selected to have a maximum (upper) constraint according
26 to the free space within the fluid conduit, in order to preclude reception of the response
27 signal while transmission is still in progress. Where the fluid conduit is a pipe, with
28 diameter D, and free space between the transducer and the pipe wall d, the pulse may be
29 selected such that 10 times the acoustic wavelength λ is less than d.

30

31 The measurement apparatus may comprise a transmission wideband acoustic transducer
32 and a receiving wideband acoustic transducer. Alternatively, the wideband acoustic signal
33 may be transmitted and received from a single wideband acoustic transducer.

34

1 Preferably, the measurement apparatus comprises a plurality of acoustic transducers, and
2 most preferably comprises a plurality of pairs of transmitting/receiving wideband acoustic
3 transducers.

4

5 Preferably, the at least one wideband acoustic transducer comprises a composite
6 transducer. The composite transducer preferably comprises a composite element as the
7 active component of the transducer. The composite element may comprise a matrix of
8 piezo-electric material pillars embedded in a polymer matrix. Preferably, at least one
9 transmitting transducer comprises a composite transducer.

10

11 A receiving transducer may comprise a solid piezo-electric transducer or may comprise a
12 composite transducer.

13

14 At least one receiving wideband acoustic transducer may be configured to operate in a
15 resonant mode. Alternatively, at least one receiving wideband acoustic transducer may be
16 configured to operate in a non-resonant mode.

17

18 The at least one wideband acoustic transducer may be configured to operate in
19 conventional or parametric modes.

20

21 The wideband acoustic transducer preferably has a low Q-factor, and may in preferred
22 embodiments have a Q-factor of less than 5.0. In particular embodiments the Q-factor is
23 less than 3.0 and more preferably is less than 1.5.

24

25 The wideband acoustic transducer is preferably selected to have a high transmit and/or
26 receive sensitivity. Preferably, the efficiency of the wideband acoustic transducer is
27 greater than 50%, and more preferably is greater than 65%.

28

29 Preferred embodiments of the invention use a plurality of wideband acoustic transducers
30 with similar, substantially identical, or identical specifications as defined above.

31

32 The method may comprise transmitting a wideband acoustic signal wideband acoustic
33 signal which comprises frequencies in the range of approximately 150 kHz to
34 approximately 1MHz. Preferably, the method comprises transmitting a wideband acoustic
35 signal wideband acoustic signal which comprises a lower frequency greater than 150 kHz,

1 and an upper frequency of less than 1MHz, and comprises a distribution of frequencies
2 between the upper and lower frequencies.

3

4 The method may comprise transmitting a wideband acoustic signal comprising a frequency
5 chirp. Preferably, the method comprises transmitting a wideband acoustic signal
6 comprising a plurality of frequency chirps. Preferably, the method comprises transmitting
7 a wideband acoustic signal comprising a plurality of stacked frequency chirps. The
8 transmitted wideband acoustic signal may therefore comprise a complex-stacked chirped
9 signal.

10

11 The frequency chirps may comprise down chirps. Alternatively or in addition the frequency
12 chirps may comprise up chirps.

13

14 In one example, the wideband acoustic signal comprises a first chirp having a first
15 frequency range, and a second chirp having a second frequency range. The second
16 frequency range is preferably different from the first frequency range, and may be for
17 example slightly higher than the first frequency range.

18

19 Preferably the first and second chirps overlap in time, and they may overlap for greater
20 than 50% of the duration of the first chirp. More preferably the first and second chirps
21 overlap for greater than 70% of the duration of the first chirp, and may overlap for greater
22 than 80% of the duration of the first chirp. In a particular embodiment the first and second
23 chirps overlap for around 90% of the duration of the first chirp.

24

25 The measurement apparatus may comprise a segmented annular wideband transmit
26 and/or receive array of transducers, and the method may comprise transmitting and/or
27 receiving over a segmented annular wideband receiver array. The number of segments
28 may be selected according to factors including required precision, quality of signal
29 response and influence of ambient and radiated noise sources. In one example, the
30 measurement apparatus comprises a segmented array comprising 12 segments, each
31 having a maximum radial beamwidth of 60 degrees. This provides overlap of adjacent
32 beams and measurement redundancy which enables measurements to be
33 compared/verified across adjacent array segments. In another example, the measurement
34 apparatus comprises a segmented array comprising 4 segments, each having a maximum

1 radial beamwidth of 90 degrees. This avoids overlap between adjacent segments.

2 Alternative embodiments may comprise greater or fewer numbers of segments.

3

4 Preferably, the method comprises analysing the wideband acoustic data set, by comparing
5 the data set with the database of wideband acoustic data signatures. Preferably, the
6 method comprises analysing the frequency content of the wideband acoustic data set.

7 The method may comprise comparing the frequency content of the wideband acoustic
8 data set with the frequency content of previously acquired acoustic data.

9

10 Preferably, analysing the wideband acoustic data set is performed in a computer
11 apparatus executing a computer program. Preferably a computer program comprises
12 software algorithms for the analysis for wideband acoustic signals. The method may
13 comprise of interrogating a database of wideband acoustic data. The wideband acoustic
14 data may be data collected from one or more tests performed on a sample fluid conduit of
15 known condition.

16

17 The method may comprise assessing or detecting the presence of a layer or volume of
18 material in the fluid conduit. The layer or volume of material may be a layer or deposit of
19 material on the inner wall or surface of the fluid conduit. The layer or deposit of material
20 may comprise the build-up and/or deposition of scale, sand, waxes, hydrates, or other
21 solids.

22

23 Alternatively, or in addition, the layer or volume of material may be volume of fluid in the
24 fluid conduit. The layer or volume of fluid may be between two layers of a multi-layer fluid
25 conduit, for example in an annulus between adjacent layers. The fluid conduit may be a
26 flexible conduit, for example a flexible riser, and the method may comprise assessing or
27 detecting the presence of a volume of fluid in between different layers in the flexible riser.
28 The method may therefore comprise a method of determining or inspecting the condition
29 of a flexible riser.

30

31 The method may comprise analysing the wideband acoustic data set to assess one or
32 more acoustic properties or attributes of the layer or volume of material.

33

1 The method may comprise assessing a physical condition of the fluid conduit. The physical
2 condition may comprise the presence of one or defects, damage, holes, cracks, wall
3 thickness and/or corrosion of a conduit or its layers.

4

5 The method may comprise analysing the wideband acoustic data set to assess one or
6 more acoustic properties or attributes a physical condition of the fluid conduit.

7

8 The fluid conduit may be selected from the group consisting of: surface, subsea or
9 subterranean pipelines, risers including marine and/or flexible risers, and tubing including
10 subterranean well tubing.

11

12 The fluid conduit may be a fluid conduit used in the hydrocarbon exploration, production
13 and transportation industries.

14

15 The method may comprise modelling a fluid conduit response, and selecting one or more
16 characteristics of a transmitted or received wideband acoustic signal based on the
17 modelled fluid conduit response. Modelling a fluid conduit response may comprise
18 modelling one or more physical parameters of the fluid conduit, including (but not limited
19 to) diameter, wall thickness, fluid conduit material, internal or external coating or cladding
20 material and/or thickness, speed of sound in a fluid medium, and/or deposits or debris
21 located in the fluid conduit.

22

23 Preferably, selecting one or more characteristics of a transmitted or received wideband
24 acoustic signal based on the modelled fluid conduit response comprises selecting one or
25 more frequency characteristics of the acoustic signal.

26

27 The method may comprise designing a wideband acoustic signal having one or more
28 acoustic characteristics and simulating a wideband acoustic signal response based on a
29 fluid conduit model to obtain a (first) simulated wideband acoustic data set. The method
30 may comprise analysing the simulated wideband acoustic data set.

31

32 The method may comprise perturbing at least one acoustic characteristic of the wideband
33 acoustic signal, and simulating a second wideband acoustic signal response based on a
34 fluid conduit model to obtain a second simulated wideband acoustic data set. The method
35 may comprise analysing the second simulated wideband acoustic data set, which may

1 comprise comparing the second simulated wideband acoustic data set with the first
2 simulated wideband acoustic data set. The method may comprise optimising the
3 wideband acoustic signal by repeating the steps of perturbing at least one acoustic
4 characteristic of the wideband acoustic signal; simulating a wideband acoustic signal
5 response based on the wideband acoustic signal with the perturbed characteristic; and
6 analysing a resulting simulated wideband acoustic data set.

7

8 The method may comprise using empirical measurements to design a wideband acoustic
9 signal. The method may comprise the step of designing a wideband acoustic signal
10 having one or more acoustic characteristics and measuring a wideband acoustic signal
11 response from a sample fluid conduit to obtain a (first) training wideband acoustic data set.
12 The method may comprise analysing the training wideband acoustic data set.

13

14 The method may comprise perturbing at least one acoustic characteristic of the wideband
15 acoustic signal, and measuring a second wideband acoustic signal response from the
16 sample fluid conduit model to obtain a second training wideband acoustic data set. The
17 method may comprise analysing the second training wideband acoustic data set, which
18 may comprise comparing the second training wideband acoustic data set with the first
19 training wideband acoustic data set. The method may comprise optimising the wideband
20 acoustic signal by repeating the steps of perturbing at least one acoustic characteristic of
21 the wideband acoustic signal; measuring a wideband acoustic signal response based on
22 the wideband acoustic signal with the perturbed characteristic; and analysing a resulting
23 training wideband acoustic data set.

24

25 Preferably the wideband acoustic signal is designed to excite a broadside or bulk
26 resonance in at least a portion of the fluid conduit (as opposed to a point resonance or
27 highly localised resonance).

28

29 The method may comprise perturbing an acoustic characteristic of the wideband acoustic
30 signal to excite a broadside or bulk resonance in a simulated wideband acoustic data set
31 or measured training wideband acoustic dataset.

32

33 The sample fluid conduit may comprise a fluid conduit having known condition, selected
34 from (but not limited to) diameter, wall thickness, fluid conduit material, internal or external

1 coating or cladding material and/or thickness, speed of sound in a fluid medium, and/or
2 deposits or debris located in the fluid conduit.

3

4 The method may comprise generating a library or database of wideband acoustic data
5 sets and/or signal responses corresponding to range of fluid conduit characteristics and/or
6 conditions. According to a further aspect of the invention, there is provided a method of
7 generating a library or database of wideband acoustic data sets and/or signal responses
8 using at least some of the steps above for generating simulated and/or empirical data sets.

9

10 According to a second aspect of the invention there is provided measurement apparatus
11 for assessing a condition of a fluid conduit from its interior, the measurement apparatus
12 comprising:

13 a body and at least one wideband acoustic transducer disposed on the body;
14 wherein the body is configured to be disposed within a fluid conduit to be assessed;
15 and wherein the apparatus is operable to:
16 transmit a wideband acoustic signal from the at least one wideband acoustic transducer
17 into a fluid volume in the fluid conduit to excite a broadside resonance in at least a portion
18 of the fluid conduit; and
19 receive a wideband acoustic signal due to a broadside resonant response of the fluid
20 conduit at the at least one wideband acoustic transducer to obtain a wideband acoustic
21 data set.

22

23 The apparatus may comprise one or more segmented arrays of transducers.

24

25 The transducers may comprise backward or rearward facing transducers, which may be
26 arranged to insonify the fluid conduit and/or receive a signal from a region of the fluid
27 conduit behind the apparatus in the direction of travel. The transducers may be positioned
28 behind one or more seals, discs and/or cups of the apparatus.

29

30 The transducers may comprise forward facing transducers, which may be arranged to
31 insonify the fluid conduit and/or receive a signal from a region of the fluid conduit head of
32 the apparatus in the direction of travel. The transducers may be positioned in front of one
33 or more seals, discs and/or cups of the apparatus.

34

1 The transducers may comprise rear mounted transducers, which may be arranged to
2 transmit a wideband acoustic signal generally in a tangential or radially perpendicular
3 direction.

4

5 The transducers may comprise mid-mounted transducers, which are arranged to transmit
6 a wideband acoustic signal generally in between the forward and rearward discs, seals or
7 cups of the apparatus.

8

9 Embodiments of the second aspect of the invention may include one or more features of
10 the first aspect of the invention or its embodiments, or vice versa.

11

12 According to a third aspect of the invention there is provided a method of assessing a
13 condition of a fluid conduit from its interior, the method comprising:

14 providing a measurement apparatus comprising at least one wideband acoustic transducer
15 within the fluid conduit;

16 transmitting a wideband acoustic signal from the measurement apparatus to excite at least
17 a portion of the fluid conduit;

18 receiving a wideband acoustic signal in the measurement apparatus to obtain a wideband
19 acoustic data set; and

20 analysing the wideband acoustic data set to assess the condition of the fluid conduit;

21 wherein at least one of the transmitted or received wideband acoustic signals is

22 transmitted or received with an axial beamwidth corresponding to a maximum angle of
23 deviation of the longitudinal axis of the measurement apparatus with the longitudinal or
24 along track axis of the fluid conduit.

25

26 Thus the axial beamwidth is selected to compensate for axial misalignment of the
27 measurement apparatus in the fluid conduit by maintaining a substantially perpendicular
28 acoustic wave incident on an inner wall of the fluid conduit, throughout the range of
29 possible misalignment of the measurement apparatus in the fluid conduit.

30

31 In the context of this specification, axial beamwidth is taken to be the width of a radially
32 propagating beam in an axial direction or long-track axis of the fluid conduit, measured at
33 the position of the at least one transducer in the fluid conduit. Thus it is a measure of the
34 incidence of the beam on an inner surface of the wall in the axial or longitudinal direction
35 along the fluid conduit

1

2 In one embodiment, at least one of the transmitted or received wideband acoustic signals
3 is transmitted or received with an axial beamwidth of at least 2 degrees.

4

5 In one embodiment, at least one of the transmitted or received wideband acoustic signals
6 is transmitted or received with an axial beamwidth of at least 4 degrees.

7

8 In one embodiment, at least one of the transmitted or received wideband acoustic signals
9 is transmitted or received with an axial beamwidth of at least 6 degrees.

10

11 In one embodiment, at least one of the transmitted or received wideband acoustic signals
12 is transmitted or received with an axial beamwidth of at least 8 degrees.

13

14 In one embodiment, at least one of the transmitted or received wideband acoustic signals
15 is transmitted or received with an axial beamwidth of approximately 8 to 12 degrees.

16

17 In one embodiment, at least one of the transmitted or received wideband acoustic signals
18 is transmitted or received with an axial beamwidth corresponding to a maximum angle of
19 deviation of the longitudinal axis of the measurement apparatus with the longitudinal or
20 along track axis of the fluid conduit.

21

22 Preferably, the transmitted wideband acoustic signal is transmitted with an axial
23 beamwidth of least 2 degrees, and more preferably within a range of approximately 6 to 14
24 degrees.

25

26 The method may comprise transmitting a wideband acoustic signal wideband acoustic
27 signal which comprises frequencies in the range of approximately 150 kHz to
28 approximately 1MHz. Preferably, the method comprises transmitting a wideband acoustic
29 signal wideband acoustic signal which comprises a lower frequency greater than 150 kHz,
30 and an upper frequency of less than 1MHz, and comprises a distribution of frequencies
31 between the upper and lower frequencies.

32

33 The method may comprise transmitting a wideband acoustic signal from the measurement
34 apparatus to excite a broadside resonance at least in the portion of the fluid conduit. The

1 wideband acoustic signal received in the measurement apparatus may be due to a
2 broadside resonant response of the fluid conduit to obtain a wideband acoustic data set.

3

4 Embodiments of the third aspect of the invention may include one or more features of the
5 first or second aspects of the invention or their embodiments, or vice versa.

6

7 According to a fourth aspect of the invention there is provided a method of assessing a
8 condition of a fluid conduit from its interior, the method comprising:

9 providing a measurement apparatus comprising at least one wideband acoustic transducer
10 within the fluid conduit;

11 transmitting a wideband acoustic signal from the measurement apparatus to excite at least
12 a portion of the fluid conduit;

13 receiving a wideband acoustic signal in the measurement apparatus to obtain a wideband
14 acoustic data set; and

15 analysing the wideband acoustic data set to assess the condition of the fluid conduit;

16 wherein at least one of the transmitted or received wideband acoustic signals is

17 transmitted or received with a radial beamwidth greater than 10 degrees.

18

19 In the context of this specification, radial beamwidth is taken to be the angular width of a
20 radially propagating beam in a circumferential direction of the fluid conduit, measured at
21 the position of the at least one transducer in the fluid conduit. Thus it is a measure of the
22 incidence of the beam on an inner surface of the wall in the circumferential direction
23 around the fluid conduit.

24

25 At least one of the transmitted or received wideband acoustic signals may be transmitted
26 or received with a radial beamwidth greater than 20 degrees.

27

28 At least one of the transmitted or received wideband acoustic signals may be transmitted
29 or received with a radial beamwidth in a range of approximately 10 degrees to
30 approximately 90 degrees.

31

32 The method may comprise transmitting a wideband acoustic signal which comprises
33 frequencies in the range of approximately 150 kHz to approximately 1MHz. Preferably,
34 the method comprises transmitting a wideband acoustic signal which comprises a lower

1 frequency greater than 150 kHz, and an upper frequency of less than 1MHz, and
2 comprises a distribution of frequencies between the upper and lower frequencies.

3

4 The method may comprise transmitting a wideband acoustic signal from the measurement
5 apparatus to excite a broadside resonance at least in the portion of the fluid conduit. The
6 wideband acoustic signal received in the measurement apparatus may be due to a
7 broadside resonant response of the fluid conduit to obtain a wideband acoustic data set.

8

9 Embodiments of the fourth aspect of the invention may include one or more features of the
10 first to third aspects of the invention or their embodiments, or vice versa.

11

12 According to a fifth aspect of the invention there is provided a method of analysing data
13 acquired according to any previous aspect of the invention.

14

15 Embodiments of the fifth aspect of the invention may include one or more features of the
16 first to fourth aspects of the invention or their embodiments, or vice versa.

17

18 According to a sixth aspect of the invention there is provided a method of acquiring data
19 using an apparatus according to the second aspect of the invention.

20

21 According to a seventh aspect of the invention there is provided a measurement apparatus
22 for assessing a condition of a fluid conduit, the apparatus comprising:

23 a body and at least one wideband acoustic transducer disposed on the body;

24 wherein the apparatus is operable to:

25 transmit a wideband acoustic signal from the at least one transducer into a fluid volume
26 coupled to the at least a portion of the fluid conduit;

27 receive a wideband acoustic signal at the at least one wideband acoustic transducer to
28 obtain a wideband acoustic data set.

29

30 Embodiments of the seventh aspect of the invention may include one or more features of
31 the first to sixth aspects of the invention or their embodiments, or vice versa.

32

33

1 Brief description of the drawings

2

3 There will now be described, by way of example only, various embodiments of the
4 invention with reference to the drawings, of which:

5

6 Figure 1 is a schematic representation of an internal fluid conduit measurement apparatus
7 according to a first embodiment of the invention, shown in situ in a fluid conduit;

8

9 Figure 2 is a schematic representation of the functional components of the fluid conduit
10 measurement apparatus of Figure 1;

11

12 Figure 3 is a schematic representation of an internal fluid conduit measurement apparatus
13 according to a second embodiment of the invention, shown in situ in a fluid conduit;

14

15 Figure 4 is a schematic representation of an internal fluid conduit measurement apparatus
16 according to a third embodiment of the invention, shown in situ in a fluid conduit;

17

18 Figure 5 is a schematic representation of internal components of a fluid conduit
19 measurement apparatus according to an embodiment of the invention;

20

21 Figure 6 is a schematic representation of internal components of a fluid conduit
22 measurement apparatus according to an alternative embodiment of the invention;

23

24 Figure 7 is a schematic representation of internal components of a fluid conduit
25 measurement apparatus according to a further alternative embodiment of the invention;

26

27 Figures 8A to 8E are schematic representations of transducer configurations of
28 measurement apparatus according to various alternative embodiments of the invention;

29

30 Figures 9A and 9B are respectively schematic representations from plan and cross-
31 sectional views depicting axial and radial beamwidths according to embodiments of the
32 invention;

33

34 Figure 10 is a plot of a bio-inspired wideband acoustic signal, as may be used in preferred
35 embodiments of the invention; and

1

2 Figures 11A, 11B; 12A, 12B; and 13A to 13B are plots of bio-inspired wideband acoustic
3 pulses, as may be used in preferred embodiments of the invention; and

4

5 Figure 14 is a flow diagram representing steps of a training method according to an
6 embodiment of the invention.

7

8 Detailed description of preferred embodiments

9

10 There will now be described, by way of example only, various embodiments of the
11 invention with reference to the drawings, of which:

12

13 Figure 1 shows schematically an apparatus 10 according to a first embodiment of the
14 invention which is used to perform an assessment method on a fluid conduit, in this case a
15 hydrocarbon pipeline 1, from its interior.

16

17 The apparatus 10 is configured to be operated inside the pipeline (and is effectively a
18 pipeline pig). The apparatus comprises a body 11 on which are located a plurality of
19 wideband acoustic transducers (not shown). The body 11 is centralised in the pipeline by
20 contact arms 16, which comprise measurement callipers and optionally comprise mounted
21 for wheels. The apparatus 10 is operated from a hydrocarbon production platform 12, and
22 is tethered to the platform by tether 14. In this embodiment, the tether 14 is an umbilical
23 and provides power and data communication between the apparatus and the deployment
24 point (in this case the platform 12). This enables real-time viewing of the data remotely
25 from the apparatus, as well as data storage on the pig itself. The apparatus 10 is driven
26 through the pipeline 1 by fluid flowing in the pipeline, and tether 14 can be used to pull the
27 apparatus 10 back to the platform 12 after running. Where wheels are provided on the
28 contact arms 16, the wheels can be used to drive the apparatus along the pipeline and/or
29 reverse the direction of the apparatus to return the apparatus to the platform. The wheels
30 may also be coupled to an odometer to provide an accurate measurement of the speed
31 and distance travelled in the fluid conduit. A 6-axis inertial measurement unit (IMU) is also
32 provided (not shown) to provide data relating to the pitch, roll a yaw or heading of the pig.

33

34 Figure 2 shows schematically (as a block diagram) a system 40 of functional components
35 of the fluid conduit measurement apparatus 10 of Figure 1. The system 40 comprises

1 transducers 41, which include an array of transmitting transducers and an array of
2 receiving transducers. The transducers 41 can be mounted in a number of ways
3 depending on system requirements. For example, the transmitting and receiving
4 transducers can be operated in either conventional or parametric modes depending upon
5 application. The acoustic transducers may be configured and distributed in a number of
6 ways on the body of the apparatus. These include (without limitation);

7

- 8 i. Separate transmit and receive transducer elements spatially distributed around the
9 body.
- 10 ii. Integrated transmit and receive transducer elements spatially distributed around the
11 body.
- 12 iii. Separate transmit and receive ring segments spatially distributed around the body.
- 13 iv. Integrated transmit and receive ring segments spatially distributed around the body.
- 14 v. Separate transmit and receive transducer elements configured as an acoustic array
15 for the purpose of beam forming spatially distributed around a body.
- 16 vi. Integrated transmit and receive transducer elements configured as an acoustic array
17 for the purpose of beam forming spatially distributed around a body (i.e. multi-
18 element arrays).
- 19 vii. Multiple and varying combinations of the above configurations depending upon the
20 application, for example 3 transmit ring segments each at 120° and a 360° multi-
21 element receive array.

22

23 In this embodiment, the transducers are arranged in a helical path on the body. The
24 transmitting transducers are designed to work in a resonant mode and across a broad
25 range of frequencies with a low Q factor (which is less than 3).

26

27 To achieve the desired low transmission Q factor, the transmitting acoustic transducers
28 comprise a composite element as the active component of the transducer. The composite
29 transduction materials comprise a matrix of piezo-electric material pillars embedded in a
30 polymer matrix.

31

32 The receiving acoustic transducers are designed to work either in a resonant or non-
33 resonant mode. The receiving acoustic transducer can comprise either a solid piezo-
34 electric material as the receiving element or composite material depending upon

1 application and mode of operation (i.e. whether operated in resonant or non-resonant
2 modes).

3

4 The system comprises electronics 43 for signal matching and/or signal conditioning. The
5 electronics 43 comprise application-specific tailored networks of passive electronic
6 components, and function to maximise efficiency in the process of transferring electrical
7 energy generated by the system into acoustic energy and maximise efficiency in the
8 process of transferring acoustic energy returning to the apparatus from fluid conduit into
9 electrical energy for computation. The electronics 43 are designed to preserve the fidelity
10 of the transmitted and received wideband broadband signals across the chosen frequency
11 bandwidth.

12

13 Storage module 47 is typically be a large volume solid state drive or card to enable the
14 large amounts of data generated by the system to be stored and recovered. Alternatively,
15 standard hard drives may be used. The storage is mounted onboard the apparatus 10
16 itself in a pressure vessel on the pig. The storage module 47 stores data during the run
17 and allows data recovery once the operation is complete. Alternatively (or in addition) data
18 storage could be remote to the apparatus. For example, in a tethered implementation of
19 Figure 1, the data are transmitted to a remote location from the pig location to be stored
20 and viewed.

21

22 The system comprises signal processing electronics 45, and a software module 49 running
23 software algorithms for the analysis for wideband acoustic signals. Information derived
24 from the signal processing may be provided visually and/or audibly via the display module
25 51.

26

27 In use, a transmitting transducer transmits a wideband acoustic signal. The signal is
28 coupled to the pipeline via fluid or slurry contained in the pipeline to excite the pipeline and
29 generate broadside resonance of the fluid conduit. A broadside resonance is a resonance
30 excited by a plane acoustic wave incident on the inner surface of the wall of the fluid
31 conduit at an angle of substantially 90 degrees (i.e. substantially perpendicular) to the axis
32 of symmetry of the conduit (or longitudinal axis).

33

34 When travelling through a fluid filled conduit the apparatus can be used for a range of fluid
35 assessment operations. These include (but are not limited to:

1

- 2 • Detecting the presence of and measuring the extent of debris and deposits within fluid
- 3 filled conduits, for example the thickness and distribution of wax;
- 4 • Identifying the nature and composition of debris and deposits within fluid filled conduits,
- 5 for example characterising the wax deposits into soft, medium, hard;
- 6 • Assessing the degree of strain in conduits, for example bends in flexible risers;
- 7 • Assessing the extent of structural disturbance in conduits, for example water ingress in
- 8 flexible risers following a breach in external protective coatings;
- 9 • Assessing the structural integrity of fluid filled conduits, for example the presence of
- 10 defects and changes in geometry through time;
- 11 • Assessing the nature and composition of the fluid phase within the conduit, for example
- 12 discriminating between fluid and multiphase flows;
- 13 • Assessing the nature of the conduit to environment interface, for example is the fluid
- 14 filled conduit in contact with water, sediment or rock.

15

16 More details of the transducer configuration and measurement operations according this
17 embodiment and alternative embodiments will be described below.

18

19 Referring now to Figure 3, there is shown a measurement apparatus 60 according to an
20 alternative embodiment of the invention. The apparatus 60 is a pipeline pig. The
21 apparatus 60 is similar to the apparatus 10 and will be understood from Figures 1 and 2
22 and the accompanying description. However, the apparatus 60 is a modified cup or seal
23 disc pig comprising a body 61 mounted with discs or cups 66. The wideband acoustic
24 transducers are mounted on the body 61. The apparatus 60 is designed to be driven by
25 differential pressure developed across the pig due to product flow. Data are acquired with
26 limited processing and stored on board for post-processing and analysis after the
27 operation is complete. This apparatus 60 is particularly applicable to oil, gas, water and
28 multiphase pipelines.

29

30 Referring now to referring now to Figure 4, there is shown a measurement apparatus 70
31 according to an alternative embodiment of the invention. The apparatus 70 is similar to
32 the apparatus 60 and will be understood from Figure 3 and the accompanying description.
33 However, the apparatus 70 is a free floating neutrally buoyant pipeline pig. The wideband
34 acoustic transducers and other electronics components are mounted in the body 71. The
35 apparatus 70 is designed to be neutrally buoyant and be driven by product flow. Data are

1 acquired with limited processing and stored on board for post-processing and analysis
2 after the operation is complete. This apparatus 70 is particularly applicable to oil, water
3 and multiphase pipelines.

4

5 Figure 5 shows schematically an arrangement 80 of internal components of the apparatus
6 according to an embodiment of the invention. In this embodiment, a pressure vessel (or
7 pressure resistant electronics pod) 81 contained within a pig body houses the electronics
8 modules and components (items 43, 45, 47, 49 in Figure 2), and the transducers are
9 located separately from the pressure vessel 81. Communication between the transducers
10 and the electronics is via data line 85.

11

12 Figure 6 shows schematically an alternative arrangement 90 of internal components of the
13 apparatus. In this embodiment, the transducers are mounted on and form part of the
14 pressure housing 91. This option has a more limited scope for transducer mounting but
15 may have useful benefits in some applications.

16

17 Figure 7 shows schematically an alternative arrangement 100 of internal components of
18 the apparatus, shown in situ in a fluid conduit 1. In this embodiment, the apparatus is a
19 modified cup or seal pig (similar to the pig 60 of Figure 3), and a pressure housing 101
20 forms the body of the pig itself. The electronics are mounted on a chassis inside the pig
21 and the transducers located in the appropriate place on the body to give the most suitable
22 view of the pipeline/ pipeline wall. This embodiment is most suited (without limitation) to
23 small diameter pipelines, e.g. an inner diameter of less than 300mm (12 inches).

24

25 As noted above, there are a number of different ways in which the transducers may be
26 configured depending on application. In particular in certain applications there may be
27 benefit to moving the location of the transducers on the pig and altering their incident angle
28 on the pipe wall. Figures 8A to 8E illustrate examples of transducer configurations in the
29 context of a cup or seal pig (similar to the pig 60 of Figure 3).

30

31 Figure 8A shows a pig 120 which comprises backward or rearward facing transducers,
32 which are arranged to transmit a wideband acoustic signal generally in the direction of
33 arrows 121a and 121b. This configuration will insonify the fluid conduit and receive a
34 signal from a region of the fluid conduit behind the pig in the direction of travel (and behind
35 the seals and cups) of the pig. This configuration may provide an effective assessment of

1 the fluid conduit after the pig has had some cleaning or dislodging effect on any material
2 present in the fluid conduit.

3

4 Figure 8B shows a pig 130 which comprises forward facing transducers, which are
5 arranged to transmit a wideband acoustic signal generally in the direction of arrows 131a
6 and 131b. This configuration will insonify the fluid conduit and receive a signal from a
7 region of the fluid conduit ahead the pig in the direction of travel (and ahead of the seals
8 and cups) of the pig. This configuration may provide an effective assessment of the fluid
9 conduit before the pig has dislodged or disrupted any material present in the fluid conduit.

10

11 Figure 8C shows a pig 140 which comprises rear mounted transducers, which are
12 arranged to transmit a wideband acoustic signal generally in the direction of arrows 141a
13 and 141b in a tangential or radially perpendicular direction. This configuration will insonify
14 the fluid conduit and receive a signal from a region of the fluid conduit behind the pig in the
15 direction of travel (and behind the seals and cups) of the pig, similar to the configuration of
16 Figure 8A, but may have the advantage of an improved excitation of a broadside resonant
17 response in the fluid conduit.

18

19 Figure 8D shows a pig 150 which comprises forward mounted transducers, which are
20 arranged to transmit a wideband acoustic signal generally in the direction of arrows 151a
21 and 151b in a tangential or radially perpendicular direction. This configuration will insonify
22 the fluid conduit and receive a signal from a region of the fluid conduit ahead of the pig in
23 the direction of travel (and ahead of the seals and cups) of the pig, similar to the
24 configuration of Figure 8B, but may have the advantage of an improved excitation of a
25 broadside resonant response in the fluid conduit.

26

27 Figure 8E shows a pig 160 which comprises mid-mounted transducers, which are
28 arranged to transmit a wideband acoustic signal generally in the direction of arrows 161a
29 and 161b in a tangential or radially perpendicular direction. This configuration will insonify
30 the fluid conduit and receive a signal from a region of the fluid conduit between the forward
31 and rearward cups of the pig.

32

33 Alternatively, or in addition, in some applications the fluid conduit volume behind the pig
34 may contain a fluid which provides improved acoustic coupling between the transducers
35 and the fluid conduit (i.e. fluid volumes present behind the pig, in front of the pig, or

1 between the forward and rearward cups. The different transducer configurations allow
2 effective acoustic coupling through the preferred fluid.

3

4 As described above, embodiments of the present invention excite broadside resonances in
5 the fluid conduit using the wideband acoustic techniques. One factor which improves the
6 broadside resonant response is directing the transmitted wideband acoustic beam towards
7 the inner surface of the wall of the fluid conduit at an angle of substantially 90 degrees
8 (substantially perpendicular) to the axis of symmetry of the conduit (or longitudinal axis).

9

10 Typically, an apparatus in accordance with the invention will be designed to remain aligned
11 with the along track (or longitudinal) axis of the fluid conduit in which it is being run. In the
12 case of a cup and disc seal pig, this is achieved by the symmetrical centralising force
13 applied by the cups and discs. In some applications, it may not be possible to guarantee
14 alignment of the pig with the along track axis.

15

16 Figure 9A shows schematically a measurement apparatus in the form of a pig 180 in situ in
17 a fluid conduit 1, shown in plan view. The pig is designed to have its longitudinal axis
18 aligned with the along track axis of the fluid conduit, but has an operational deviation from
19 alignment of $\pm\theta_1$. This translates to a misalignment of the normal to the pig body from the
20 normal to the inner wall of the fluid conduit. Thus, a radial beam transmitted from the pig
21 body at an angle normal to the body, will not be incident on the inner wall at a
22 perpendicular angle.

23

24 The present embodiment mitigates against this deviation by transmitting the acoustic
25 signal with a beamwidth in the axial direction of the fluid conduit. The axial beamwidth,
26 shown in Figure 9A as θ_2 is taken to be the width of a radially propagating beam in an axial
27 direction or long-track axis of the fluid conduit, measured at the position of the at least one
28 transducer in the fluid conduit. Thus it is a measure of the incidence of the beam on an
29 inner surface of the wall in the axial or longitudinal direction along the fluid conduit

30

31 If the axial beamwidth θ_2 is designed to be equal to or greater than $2\theta_1$, the acoustic beam
32 will always have a component incident on the inner wall fluid conduit at an angle of
33 substantially 90 degrees (substantially perpendicular) to the axis of symmetry of the
34 conduit (or longitudinal axis), throughout the operational deviation of the pig from
35 alignment with the fluid conduit.

1

2 A typical cup and disc seal pig may have a maximum deviation of $\pm 5^\circ$ from the along track
3 axis, and therefore a preferred embodiment may have an axial beamwidth of 10° . Other
4 pig designs may have greater or lesser operational deviations, and therefore the radial
5 beamwidth may be selected accordingly.

6

7 Figure 9B shows the same apparatus 180 in situ in a fluid conduit 1 from an end view.

8 The apparatus has an array of transducers arranged around the surface of the apparatus
9 in a ring. Each transducer is designed to transmit a wideband acoustic signal with a radial
10 beamwidth ϕ in the circumferential dimension of the apparatus and the fluid conduit.

11

12 The apparatus therefore provides a segmented annular wideband transmit and/or receive
13 array of transducers 181. The number of segments may be selected according to factors
14 including required precision, quality of signal response and influence of ambient and
15 radiated noise sources. In the example shown, the measurement apparatus comprises a
16 segmented array comprising eight segments, each having a radial beamwidth ϕ of 45° .
17 This avoids overlap of adjacent beams.

18

19 Variations are of course possible within the scope of the invention. A minimal four segment
20 system might have 90° beamwidths per segment to ensure full radial coverage of the pipe,
21 but with limited resolution. However, an alternative embodiment comprises a 72-segment
22 system with 10° beamwidths per segment providing 50% overlap with adjacent segments.
23 Such a configuration guarantees 2:1 redundancy in measurements, which would have
24 benefits for profiling and verification. However, such a system is relatively costly and has
25 higher power-consumption. Alternative embodiments may comprise greater or fewer
26 numbers of segments: there are of course any number of potential variants in between all
27 of which could work well under different constraints/conditions.

28

29 Figure 10 is a graphical diagram 200 showing an example of the design of a bio-inspired
30 wideband acoustic signal, as may be used in preferred embodiments of the invention. The
31 graph 200 plots frequency against time. The signal comprises a pair of overlapping down
32 chirps 202, 204, which overlap in time to generate the acoustic excitation pulse.

33

34 Figures 11A, 11B; 12A, 12B; and 13A to 13B are examples of plots of bio-inspired
35 wideband acoustic pulses, as may be used in preferred embodiments of the invention. In

1 each case, the first plot in each drawing (suffixed "A") shows the pulse in the time domain,
2 and the second plot (suffixed "B") shows the pulse in the frequency domain.

3

4 In Figures 11A and 11B, the plots 300a, 300b, show a wideband acoustic signal 302a,
5 302b with a frequency range of approximately 150 kHz to over 300 kHz, and a distribution
6 of frequencies across that range. Thus the signal has a bandwidth greater than one
7 octave.

8

9 In Figures 12A and 12B, the plots 500a, 500b, show a wideband acoustic signal 502a,
10 502b with a frequency range of approximately 200 kHz to about 800 kHz, and a
11 distribution of frequencies across that range. Thus the signal has a bandwidth spanning
12 around two octaves.

13

14 In Figures 13A and 13B, the plots 600a, 600b, show a wideband acoustic signal 602a,
15 602b with a frequency range of approximately 200 kHz to about 1.6 MHz, and a
16 distribution of frequencies across that range. Thus the signal has a bandwidth spanning
17 around three octaves.

18

19 The design of wideband acoustic signals in accordance with Figures 10 to 13B (i.e. with a
20 frequency range of approximately 150 kHz to about 1.6 MHz, overcomes limitations of the
21 technique of the prior art including WO2007/123418, which is reliant on 'tuning' resonant
22 frequencies of pipeline walls. The selection of frequencies in the range of 150 kHz to
23 about 1.6 MHz facilitates a range of applications to fluid conduit assessment or inspection.

24

25 Prior to use of the measurement apparatus of the invention, it is beneficial to educate or
26 train the system using modelling and empirical data collection. Figure 14 shows
27 schematically a method 900 by which the system is educated or trained.

28

29 As a first step, a model of the fluid conduit system to be assessed is generated, and may
30 include (without limitation) parameters such as diameter, wall thickness, fluid conduit
31 material, internal or external coating or cladding material and/or thickness, speed of sound
32 in a fluid medium, and/or deposits or debris located in the fluid conduit. This generated
33 model (step 901) is used with a preliminary transmission signal designed or selected (step
34 902) according to the modelled conditions. The signal from 902 is run in a computer
35 model (step 903) to generate a simulated data set which is output (step 904) for storage

1 (step 905) and/or data analysis (step 906). The data analysis 906 determines the
2 effectiveness of the designed transmission pulse for the model. The designed signal can
3 then be optimised by modifying the signal and repeating the data simulation. This may for
4 example comprise perturbing at least one acoustic characteristic of the wideband acoustic
5 signal, and simulating a second wideband acoustic signal response based on the fluid
6 conduit model to obtain a second simulated wideband acoustic data set. This data set can
7 be compared with the first, and it can be determined whether the second signal is more
8 effective for the fluid conduit modelled.

9

10 As an alternative to the above, or as a subsequent method, a designed signal can be used
11 in a measurement operation in a sample fluid conduit having one or more known
12 characteristics. The signal from 902 (which may be optimised by a modelling method as
13 described above) may be used in the sample fluid conduit (step 908) and a training data
14 set may be output (step 909) from the apparatus for storage (905) and/or analysis (906).
15 The results of the data analysis may be used in further optimise the designed signal by
16 perturbing a characteristic and repeating the measurement.

17

18 The above-described simulated and/or empirical data can be used to help design a signal
19 and pulse which is tailored to the particular characteristics of the conduit. In particular, the
20 techniques may be used to generate a pulse which is likely to generate a strong broadside
21 resonant response (by modelling or actual detection of a broadside response in a sample
22 conduit).

23

24 In addition, the data may be stored to generate a library of acoustic profiles associated
25 with the known condition of the sample conduit. The database of acoustic profiles can be
26 referenced during real measurement operations in order to characterise fluid conduit
27 features. This may be by recognition of, for example, a fluid conduit with no debris or with
28 a substantial amount of debris, or may be by inferring an intermediate fluid conduit
29 condition by comparison with the data.

30

31 In practice as the systems are run a database of responses from specific conduits, specific
32 types of conduit and related pipe types are collated. From these knowledge of known and
33 expected responses of pipes under 'normal' operating conditions are built up. This
34 knowledge will iteratively improve with each run (system education). Once the known
35 normal responses have been logged, anomalies are readily recognisable. With additional

1 data gathered against known defects, these anomalies will become associated with known
2 problem conditions or known structural observations (for example, field joints). A database
3 of known anomalies can then be built up (further system education), so that anomalies,
4 which may include flaws, debris, sand, wax may be detected.

5

6 A method of use will now be described by way of example. The measurement system has
7 previously been "educated" to allow features and material compositions of interest to be
8 identified. This relates to both the transmitted signal and how the algorithms process the
9 received data.

10

11 The measurement apparatus is a modified pig such cup pig. The apparatus is self-
12 powered using onboard batteries and activated either by the operator via a switch, by the
13 pipeline pressure using a pressure activated switch or remotely using a wireless interface.

14

15 The invention is placed in the pipeline using a standard pig launcher and is driven down
16 the pipeline by the fluid flow in the pipeline. The transducers of the apparatus are
17 maintained at a distance between the at least one transducer and the fluid conduit to avoid
18 near-field interference effects. This enables the measurement apparatus to be translated
19 within the fluid conduit at a desirable (higher or more consistent) speed. Typically the
20 measurement apparatus is translated within the fluid conduit speed of between 0 and 5
21 m/s. As the pig moves in the pipe, multi-axis position, velocity and acceleration sensors
22 are used to log the position, rotation and orientation of the pig relative to the pipe axis. This
23 enables distribution estimation for deposits and debris from any differential responses
24 measured in different segments of the annular array.

25

26 The system transmits wideband acoustic pulses into the fluid medium into the conduit as
27 the conduit is traversed. With any acoustic measurement the speed of sound is critical in
28 determining range. If the speed of sound is not known it can be measured using a fixed
29 baseline and pulse echo measurement. The transmitted pulses have frequencies typically
30 in the range of 150 kHz and 1 MHz, and span around 1 to 2 octaves.

31

32 The measurement apparatus records data as it traverses the pipeline. This data
33 acquisition could be time based (for example every 0.01 seconds a sample is taken) or
34 distance based (for example every 0.01m the pig travels a sample is taken). Distance is
35 determined using odometer wheels that output a signal at fixed distance intervals. Data

1 stored is raw data converted from analogue signals or part-processed data. The return
2 signal is affected by the acoustic properties experienced between transmission and
3 detection, including acoustic properties of the pipeline and any layer deposited on the
4 inside of the pipeline. Analysing the return data set enables the presence of a layer or
5 deposit to be detected by the apparatus.

6

7 When the pig reaches the end of the pipeline it is received in to a pig receiver and
8 removed from the pipeline. The apparatus will de-activate either by operator intervention,
9 pressure switch de-activation, or remote control by wireless interface. Once removed from
10 the pipeline data is downloaded from the invention and post-processing carried out that
11 specifically relates to the type of features/material composition etc that is of interest. The
12 data can then be viewed and conclusions/inferences made from that data. For example, by
13 comparison with acoustic signatures collected from layers or deposits of known thickness,
14 profile and/or composition enables a detected layer or deposit to be characterised. The
15 method therefore enables characteristics of the layer or deposit to be inferred from the
16 detected acoustic wideband signal.

17

18 Such analysis can be performed using software algorithms, and the acoustic signatures
19 may be stored as a data set within a database. The frequency content of the return signal
20 can also be analysed, and may be compared with the frequency content of such signature
21 acoustic data sets.

22

23 The invention provides a method of and apparatus for assessing a condition of a fluid
24 conduit from its interior. The method comprises providing a measurement apparatus
25 comprising at least one wideband acoustic transducer within the fluid conduit and
26 transmitting a wideband acoustic signal from the measurement apparatus to excite a
27 broadside resonance in at least a portion of the fluid conduit. A wideband acoustic signal
28 is received in the measurement apparatus due to a broadside resonant response of the
29 fluid conduit to obtain a wideband acoustic data set; and the data set is analysed to assess
30 the condition of the fluid conduit.

31

32 The method and apparatus of the invention may be used to detect layers attached to the
33 wall of a fluid conduit. Using the bulk response from the wideband signal of the attached
34 layers, it is possible to map hydrate and wax build-up. In addition, annular layers attached

1 to the wall, e.g. wax build-up, will alter the measured wideband response. The response
2 will be linked to material type and distribution.

3

4 The invention also enables detection of debris lying in a fluid conduit. Debris echoes can
5 be used to map position of debris deposits in the fluid conduit, as debris will affect the
6 broadside wideband responses of the fluid conduit. The differences will vary between
7 segments of the annular receive array depending on distribution of the debris. The
8 responses will be affected most greatly towards the bottom of the fluid conduit and the
9 response changes will be expected to depend on the type of debris present.

10

11 An evaluation the condition of the fluid conduit may also be performed using the wideband
12 signal returns to characterise the fluid conduit condition. Corrosion, thinning and structural
13 flaws will all affect the broadside resonance properties of the pipe. The precise
14 configuration of the transducer arrays and speed of the pig platform determine the
15 resolution with which these condition 'changes' can be measured.

16

17 The invention also has application to gas-filled fluid conduits. In such applications a wave
18 guide would be used to facilitate acoustic propagation to the pipe wall/debris. This could
19 for example be a gel, fluid bag or other.

20

21 Various modifications may be made within the scope of the invention as herein intended,
22 and embodiments of the invention may include combinations of features other than those
23 expressly described above. For example, where the apparatus is described above as
24 performing an assessment method on a hydrocarbon pipeline, it will be appreciated that
25 the apparatus (and the assessment method) is equally applicable to other fluid conduits
26 including surface, subsea or subterranean pipelines, risers including marine and/or flexible
27 risers, and tubing including subterranean well tubing.

28

1 References

2

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15 [5] WO 2010/107712

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17 [6] US 2007/0019506

18

19

20

1 Claims

2

3 1. A method of assessing a condition of a fluid conduit from its interior, the method
4 comprising:
5 providing a measurement apparatus comprising at least one wideband acoustic
6 transducer within the fluid conduit;
7 transmitting a wideband acoustic signal from the measurement apparatus to excite a
8 broadside resonance in at least a portion of the fluid conduit; wherein the broadside
9 resonance is resonance excited by a plane acoustic wave incident on an inner
10 surface of a wall of the fluid conduit at an angle of substantially 90 degrees to a
11 longitudinal axis of the conduit;
12 receiving a wideband acoustic signal in the measurement apparatus due to a
13 broadside resonant response of the fluid conduit to obtain a wideband acoustic data
14 set; wherein the broadside resonant response is the response elicited by the plane
15 acoustic wave incident on the inner surface of the wall of the fluid conduit at an angle
16 of substantially 90 degrees to the longitudinal axis of the conduit; and
17 analysing the wideband acoustic data set to assess a state of a flow path defined by
18 the fluid conduit.

19

20 2. The method according to claim 1, wherein at least one of the transmitted or received
21 wideband acoustic signals is transmitted or received with an axial beamwidth
22 corresponding to a maximum angle of deviation of the longitudinal axis of the
23 measurement apparatus with the longitudinal axis of the fluid conduit.

24

25 3. The method according to claim 1 or claim 2, comprising detecting the presence of,
26 measuring the extent of, and/or identifying the composition of deposits, debris and
27 foreign bodies within fluid conduits.

28

29 4. The method according to any one of claims 1 to 3, wherein the wideband acoustic
30 signal comprises at least one frequency in the range of 150 kHz to 10 MHz, and
31 comprises a distribution of frequencies between 150 kHz and 10 MHz.

32

33 5. The method according to any one of claims 1 to 4, wherein the wideband acoustic
34 signal comprises a lower frequency of 150 kHz, and an upper frequency of 1 MHz,

- 1 and comprises a distribution of frequencies between the upper and lower
2 frequencies.
3
- 4 6. The method according to any one of claims 1 to 5, comprising transmitting a
5 wideband acoustic signal from the measurement apparatus, through a fluid which
6 couples the measurement apparatus to at least a portion of the fluid conduit.
7
- 8 7. The method according to any one of claims 1 to 6, comprising maintaining a distance
9 between the at least one transducer and the fluid conduit to avoid near-field
10 interference effects.
11
- 12 8. The method according to any one of claims 1 to 7, comprising translating the
13 measurement apparatus within the fluid conduit.
14
- 15 9. The method according to any one of claims 1 to 8, comprising transmitting a plurality
16 of wideband acoustic pulses separated in time.
17
- 18 10. The method according to any one of claims 1 to 9, comprising transmitting a plurality
19 of wideband acoustic pulses at a fixed transmission rate.
20
- 21 11. The method according to any one of claims 1 to 10, comprising triggering a
22 transmission and/or sampling of subsequent wideband acoustic pulses according to
23 a distance translated by the measurement apparatus in the fluid conduit.
24
- 25 12. The method according to any one of claims 1 to 11, comprising transmitting a
26 wideband acoustic pulse with a duration of at least 10 times an acoustic wave
27 period.
28
- 29 13. The method according to any one of claims 1 to 12, comprising transmitting a
30 wideband acoustic pulse with a duration of less than 100 μ S.
31
- 32 14. The method according to any one of claims 1 to 13, comprising transmitting a
33 wideband acoustic signal comprising a frequency chirp.
34

- 1 15. The method according to any one of claims 1 to 14, comprising transmitting a
2 wideband acoustic signal comprising a plurality of frequency chirps.
3
- 4 16. The method according to any one of claims 1 to 15, comprising transmitting a
5 wideband acoustic signal comprising a plurality of stacked frequency chirps.
6
- 7 17. The method according to any one of claims 1 to 16, wherein the transmitted
8 wideband acoustic signal comprises a complex-stacked chirped signal.
9
- 10 18. The method according any one of claims 1 to 17, wherein the wideband acoustic
11 signal comprises a first chirp having a first frequency range, and a second chirp
12 having a second frequency range.
13
- 14 19. The method according to claim 18, wherein the first and second chirps overlap in
15 time.
16
- 17 20. The method according to claim 18 or claim 19, wherein the first and second chirps
18 overlap in time for greater than 50% of the duration of the first chirp.
19
- 20 21. The method according to any one of claims 1 to 20, comprising transmitting and/or
21 receiving over a segmented annular wideband receiver array.
22
- 23 22. The method according to any one of claims 1 to 21, comprising analysing the
24 wideband acoustic data set, by comparing the data set with a database of wideband
25 acoustic data signatures.
26
- 27 23. The method according to any one of claims 1 to 22, comprising comparing the
28 frequency content of the wideband acoustic data set with the frequency content of
29 previously acquired acoustic data.
30
- 31 24. The method according to any one of claims 1 to 23, comprising interrogating a
32 database of wideband acoustic data, wherein the acoustic data is data collected from
33 one or more tests performed on a sample fluid conduit of known condition.
34

- 1 25. The method according to any one of claims 1 to 24, comprising analysing the
2 wideband acoustic data set to assess one or more acoustic properties or attributes of
3 a physical condition of the fluid conduit.
4
- 5 26. The method according to any one of claims 1 to 25, comprising modelling a fluid
6 conduit response, and
7 selecting one or more characteristics of a transmitted or received wideband acoustic
8 signal based on the modelled fluid conduit response.
9
- 10 27. The method according to any one of claims 1 to 26, comprising:
11 designing a wideband acoustic signal having one or more acoustic characteristics
12 and
13 simulating a wideband acoustic signal response based on a fluid conduit model to
14 obtain a first simulated wideband acoustic data set.
15
- 16 28. The method according to claim 27, comprising perturbing at least one acoustic
17 characteristic of the wideband acoustic signal, and
18 simulating a second wideband acoustic signal response based on a fluid conduit
19 model to obtain a second simulated wideband acoustic data set.
20
- 21 29. The method according to claim 28, comprising analysing the second simulated
22 wideband acoustic data set.
23
- 24 30. The method according to claim 29, comprising optimising the wideband acoustic
25 signal by repeating the steps of perturbing at least one acoustic characteristic of the
26 wideband acoustic signal;
27 simulating a wideband acoustic signal response based on the wideband acoustic
28 signal with the perturbed characteristic; and
29 analysing a resulting simulated wideband acoustic data set.
30
- 31 31. The method according to any one of claims 1 to 30, comprising the step of designing
32 a wideband acoustic signal having one or more acoustic characteristics and
33 measuring a wideband acoustic signal response from a sample fluid conduit to
34 obtain a first training wideband acoustic data set.

1

2 32. The method according to claim 31, comprising analysing the training wideband
3 acoustic data set.

4

5 33. The method according to claim 31 or claim 32, comprising perturbing at least one
6 acoustic characteristic of the wideband acoustic signal, and
7 measuring a second wideband acoustic signal response from a sample fluid conduit
8 model to obtain a second training wideband acoustic data set.

9

10 34. The method according to claim 33, comprising analysing the second training
11 wideband acoustic data set.

12

13 35. The method according to claim 34, comprising optimising the wideband acoustic
14 signal by repeating the steps of perturbing at least one acoustic characteristic of the
15 wideband acoustic signal;
16 measuring a wideband acoustic signal response based on the wideband acoustic
17 signal with the perturbed characteristic; and
18 analysing a resulting training wideband acoustic data set.

19

20 36. The method according to any one of claims 1 to 35, comprising using empirical
21 measurements to design a wideband acoustic signal.

22

23 37. The method according to any one of claims 1 to 36, comprising perturbing an
24 acoustic characteristic of the wideband acoustic signal to excite a broadside or bulk
25 resonance in a simulated wideband acoustic data set or measured training wideband
26 acoustic dataset.

27

28 38. The method according to any one of claims 1 to 37, comprising generating a library
29 or database of wideband acoustic data sets and/or signal responses corresponding
30 to range of fluid conduit characteristics and/or conditions.

31

32 39. A measurement apparatus for assessing a state of a flow path of a fluid conduit from
33 its interior, the measurement apparatus comprising:
34 a body and at least one wideband acoustic transducer disposed on the body;

- 1 wherein the body is configured to be disposed within a fluid conduit to be assessed;
2 and wherein the apparatus is operable to:
3 transmit a wideband acoustic signal from the at least one wideband acoustic
4 transducer into a fluid volume in the fluid conduit to excite a broadside resonance in
5 at least a portion of the fluid conduit; wherein the broadside resonance is resonance
6 excited by a plane acoustic wave incident on an inner surface of a wall of the fluid
7 conduit at an angle of substantially 90 degrees to a longitudinal axis of the conduit
8 and
9 receive a wideband acoustic signal due to a broadside resonant response of the fluid
10 conduit at the at least one wideband acoustic transducer to obtain a wideband
11 acoustic data set for analysis of the state of the flow path of the fluid conduit; wherein
12 the broadside resonant response is the response elicited by the plane acoustic wave
13 incident on the inner surface of the wall of the fluid conduit at an angle of
14 substantially 90 degrees to the longitudinal axis of the conduit.
15
- 16 40. The apparatus according to claim 39, wherein the transducers comprise backward or
17 rearward facing transducers, which are arranged to insonify the fluid conduit and/or
18 receive a signal from a region of the fluid conduit behind the apparatus in the
19 direction of travel.
20
- 21 41. The apparatus according to claim 39 or claim 40, wherein the transducers comprise
22 forward facing transducers, which are arranged to insonify the fluid conduit and/or
23 receive a signal from a region of the fluid conduit ahead of the apparatus in the
24 direction of travel.
25
- 26 42. The apparatus according to any of claims 39 to 41, wherein the transducers
27 comprise rear mounted transducers, which are arranged to transmit a wideband
28 acoustic signal in a tangential or radially perpendicular direction.
29
- 30 43. The apparatus according to any of claims 39 to 42, wherein the transducers
31 comprise mid-mounted transducers, which are arranged to transmit a wideband
32 acoustic signal in between forward and rearward discs, seals or cups of the
33 apparatus.
34

- 1 44. The apparatus according to any of claims 39 to 43, wherein the apparatus comprises
2 a plurality of pairs of transmitting/receiving wideband acoustic transducers.
3
- 4 45. The apparatus according to any of claims 39 to 44, wherein the wideband acoustic
5 transducer has a Q-factor of less than 5.0.
6
- 7 46. The apparatus according to any of claims 39 to 45, wherein the efficiency of the
8 wideband acoustic transducer is greater than 50%.
9
- 10 47. The apparatus according to any of claims 39 to 46, wherein the apparatus comprises
11 one or more segmented arrays of transducers.
12
- 13 48. The apparatus according to any of claims 39 to 47, wherein the apparatus comprises
14 a pipeline pig.

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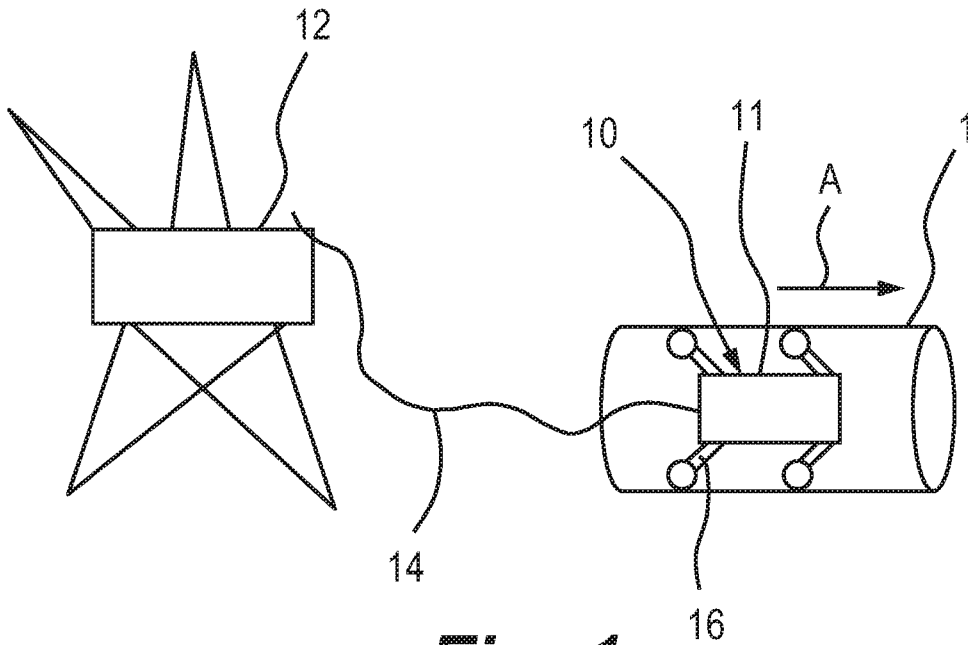


Fig. 1

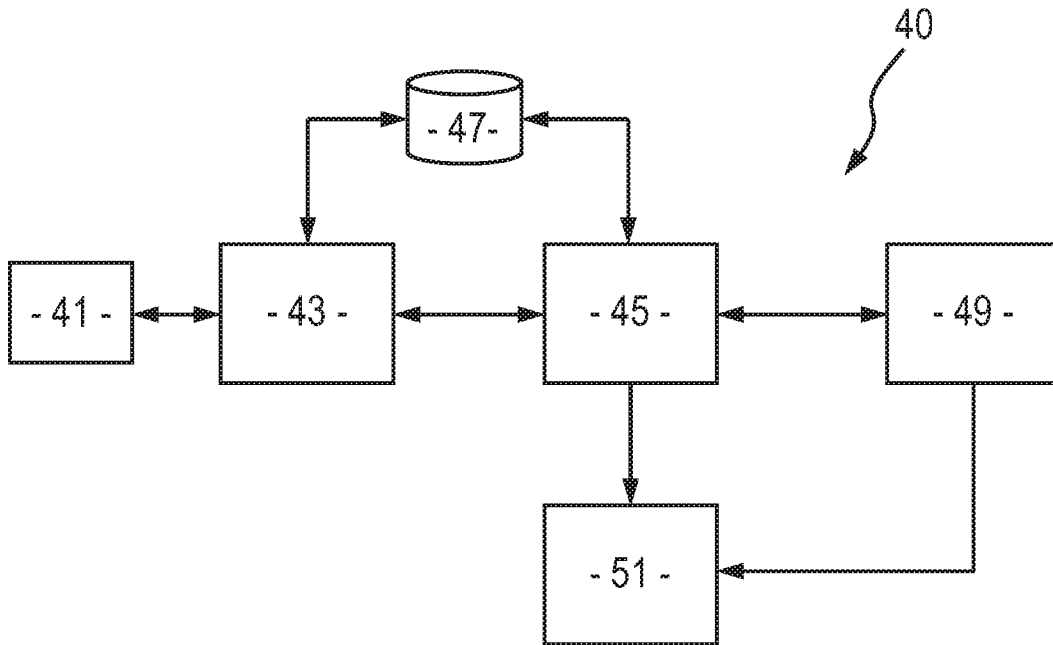
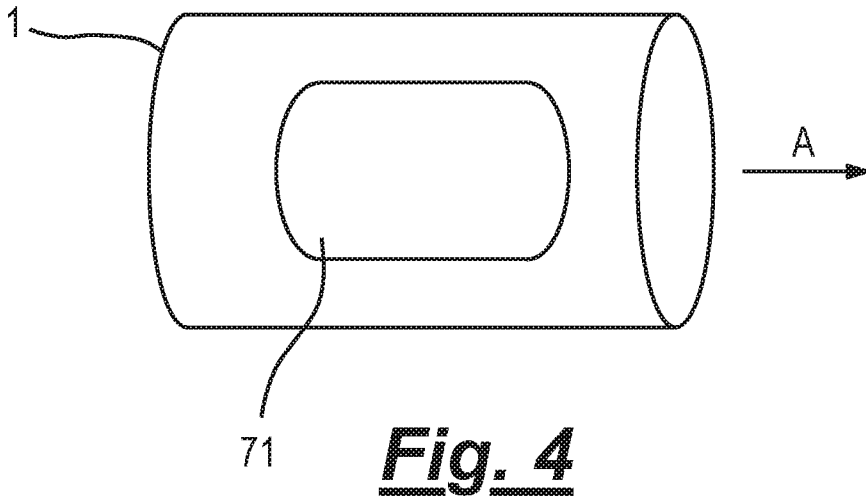
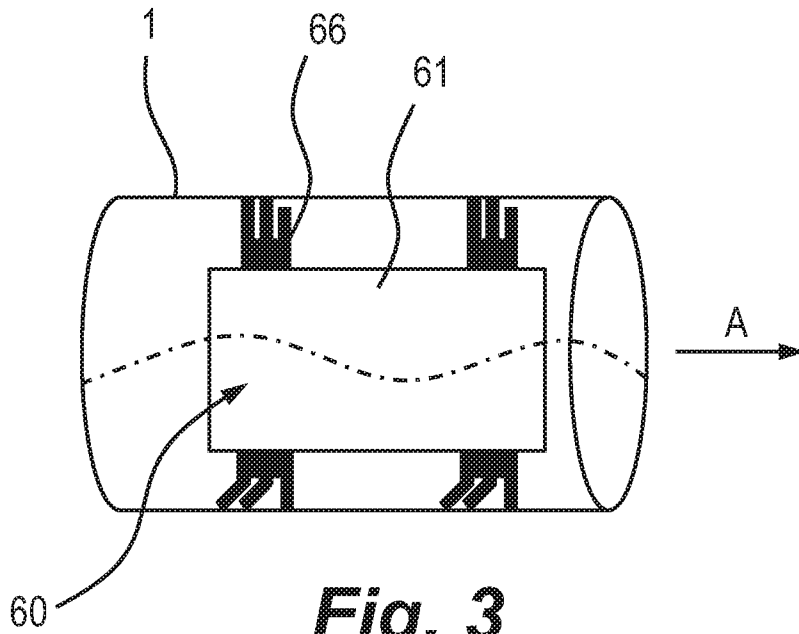


Fig. 2

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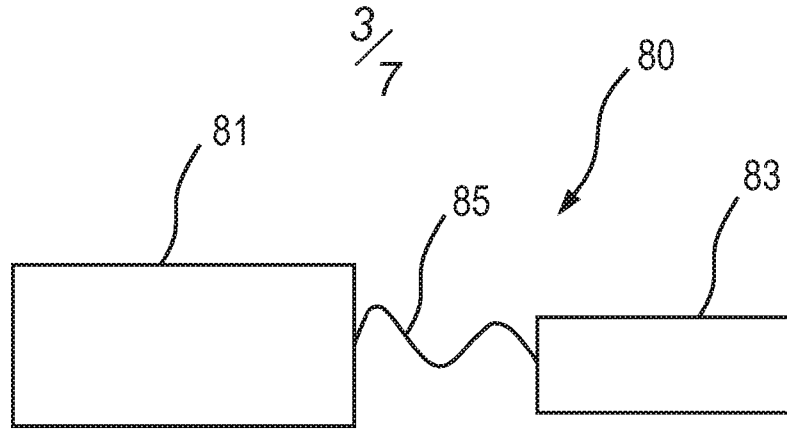


Fig. 5

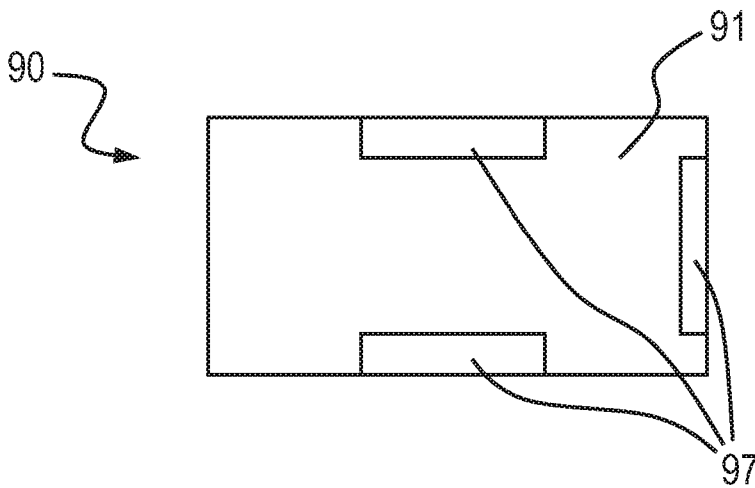


Fig. 6

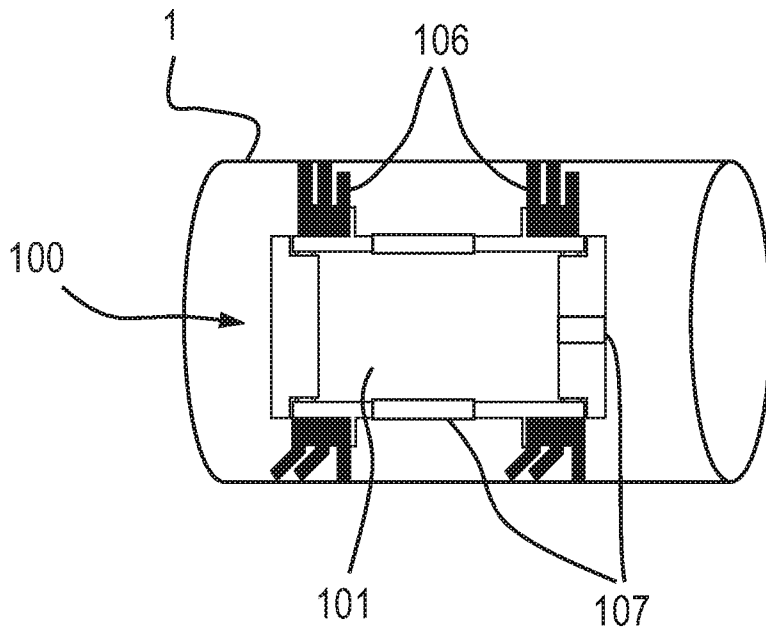
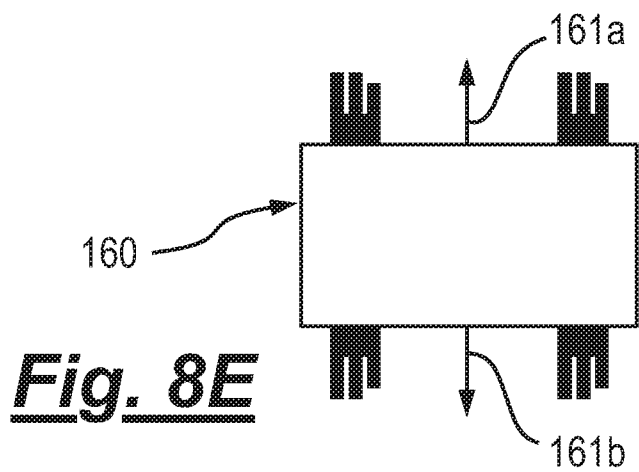
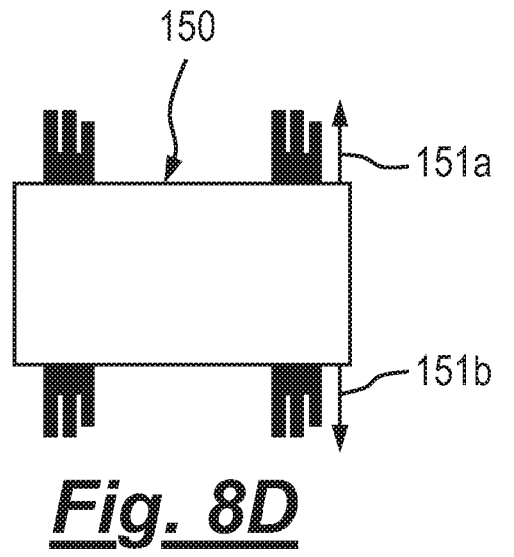
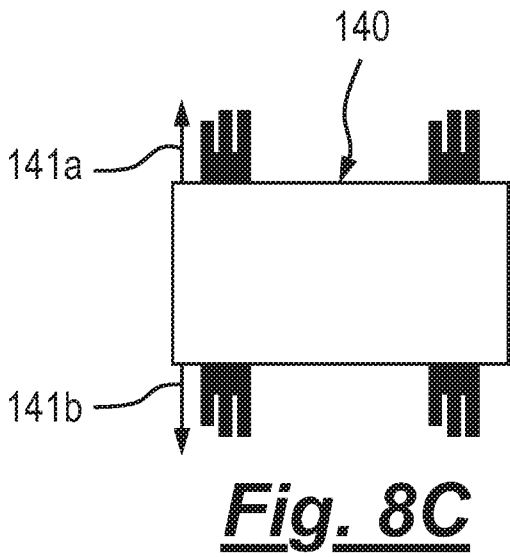
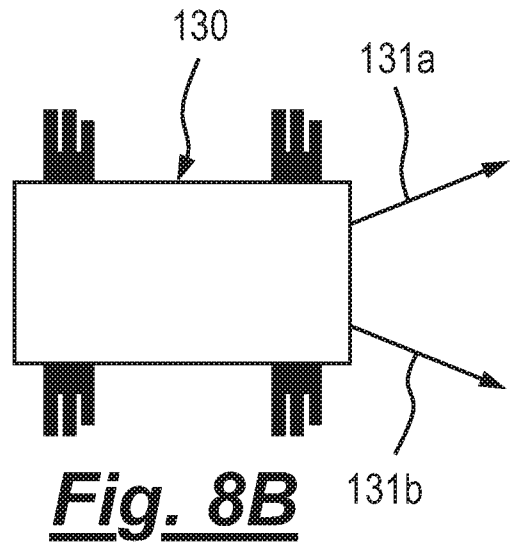
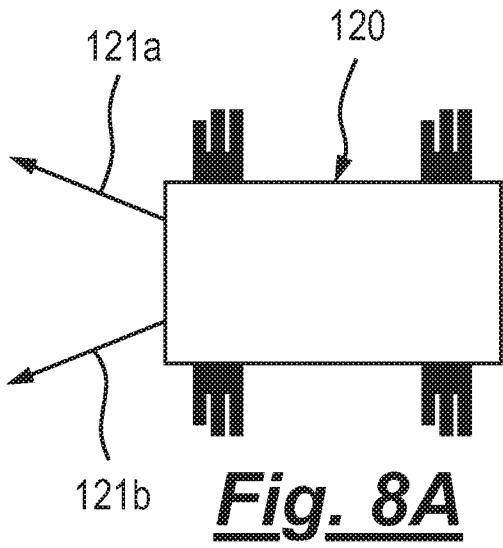


Fig. 7

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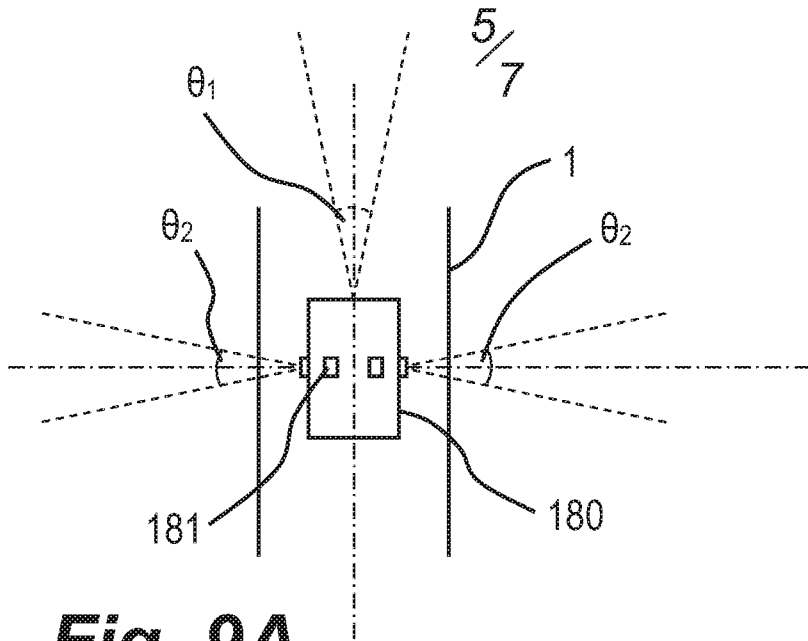


Fig. 9A

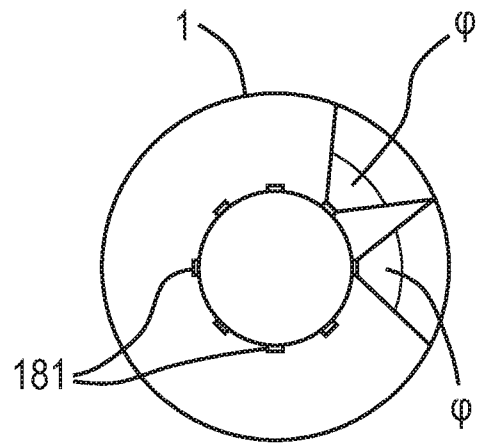


Fig. 9B

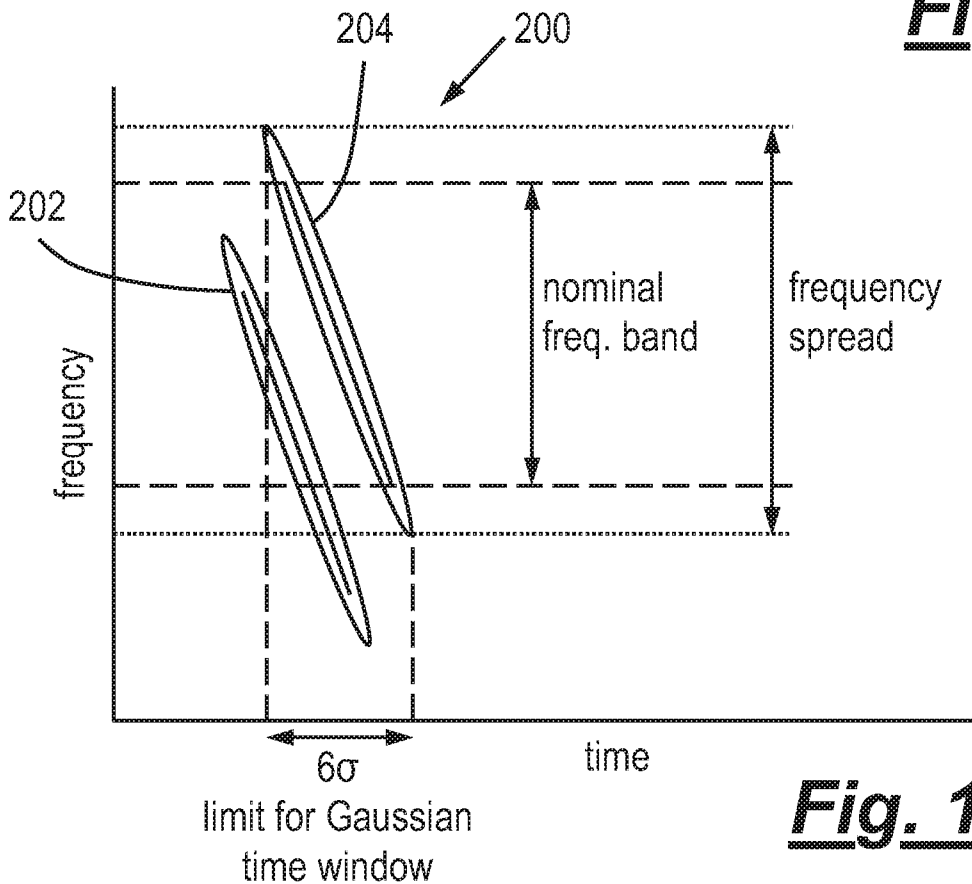


Fig. 10

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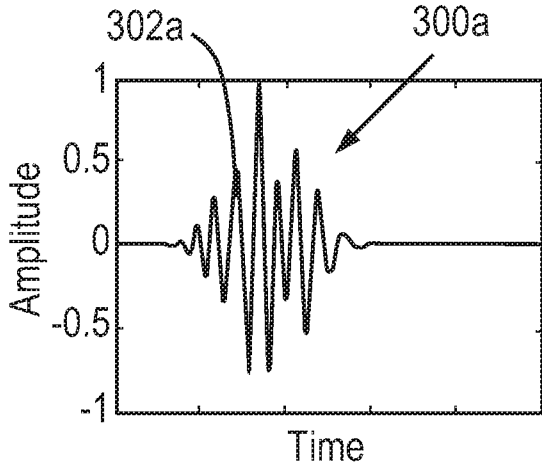


Fig. 11A

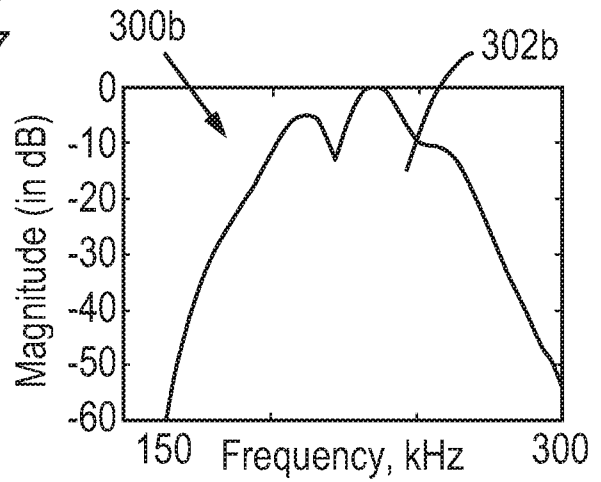


Fig. 11B

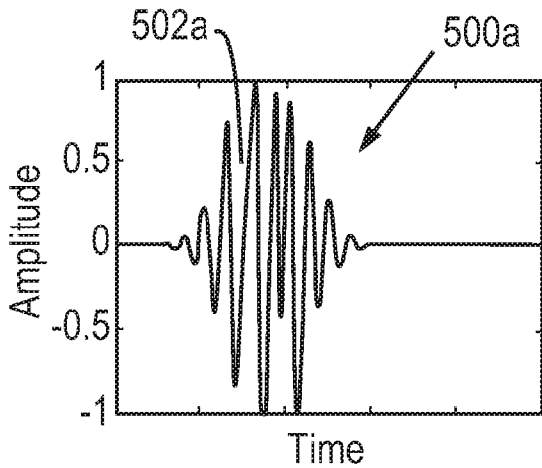


Fig. 12A

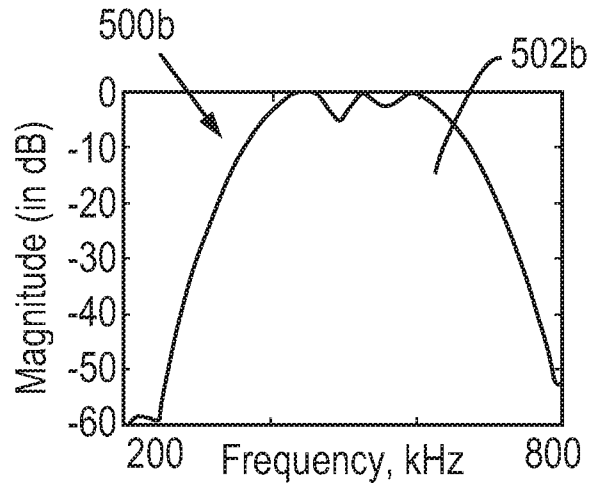


Fig. 12B

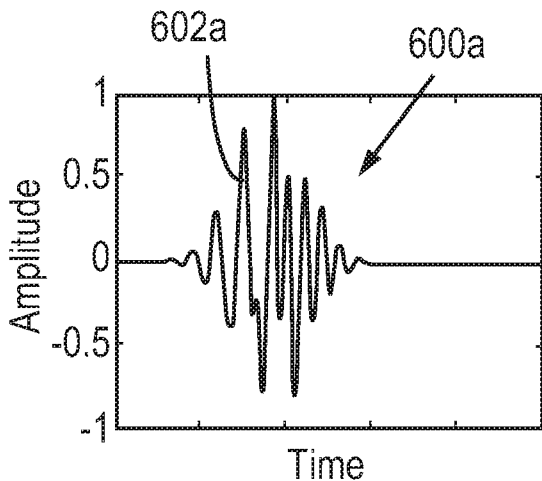


Fig. 13A

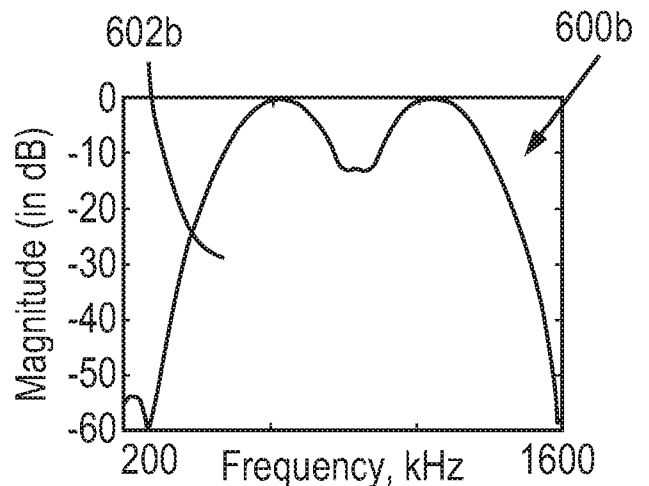


Fig. 13B

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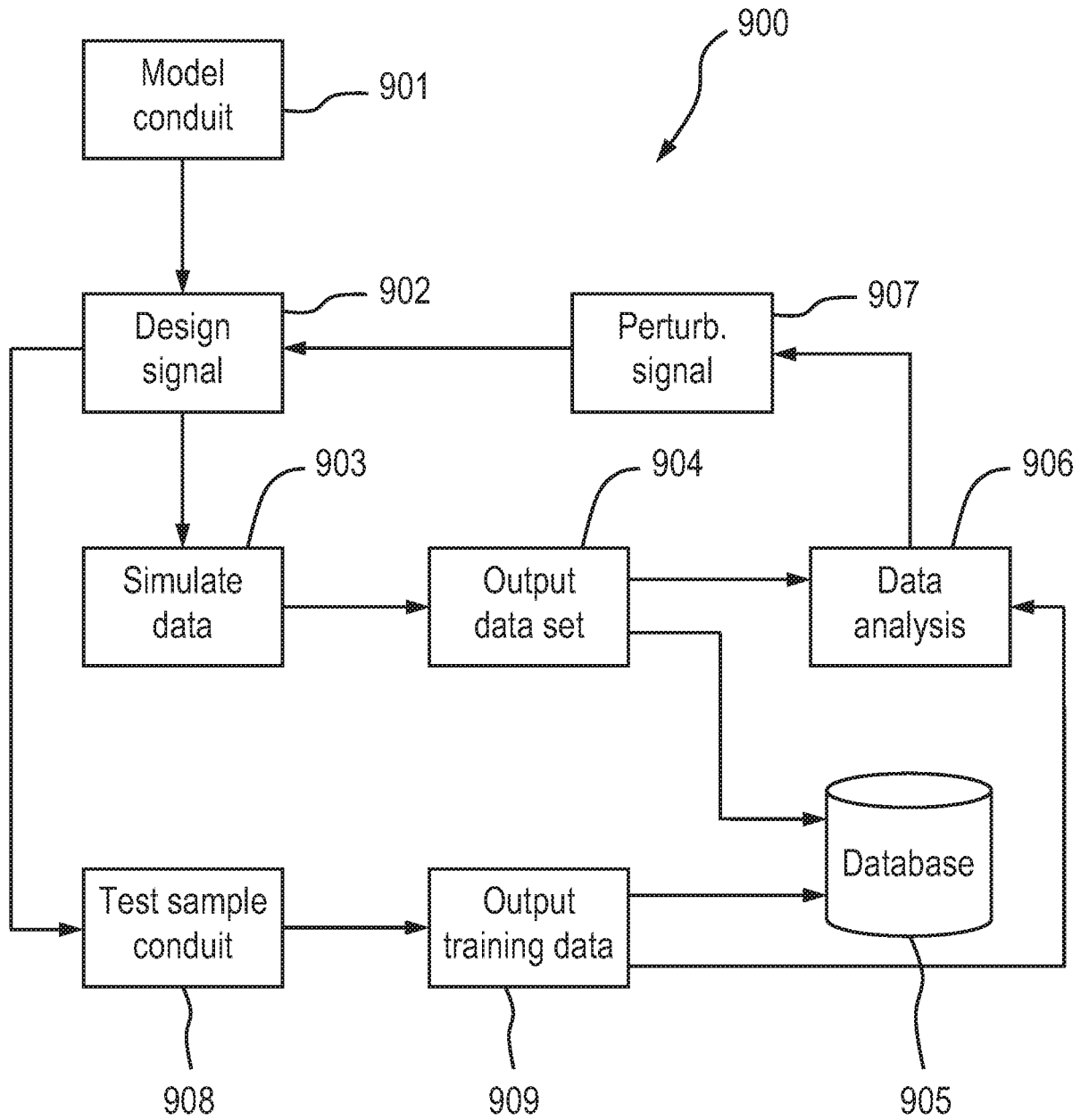


Fig. 14

