



(22) Date de dépôt/Filing Date: 2011/03/17

(41) Mise à la disp. pub./Open to Public Insp.: 2011/10/01

(45) Date de délivrance/Issue Date: 2014/01/21

(30) Priorité/Priority: 2010/04/01 (US12/752,417)

(51) Cl.Int./Int.Cl. *F15B 20/00* (2006.01),
B64C 13/00 (2006.01)

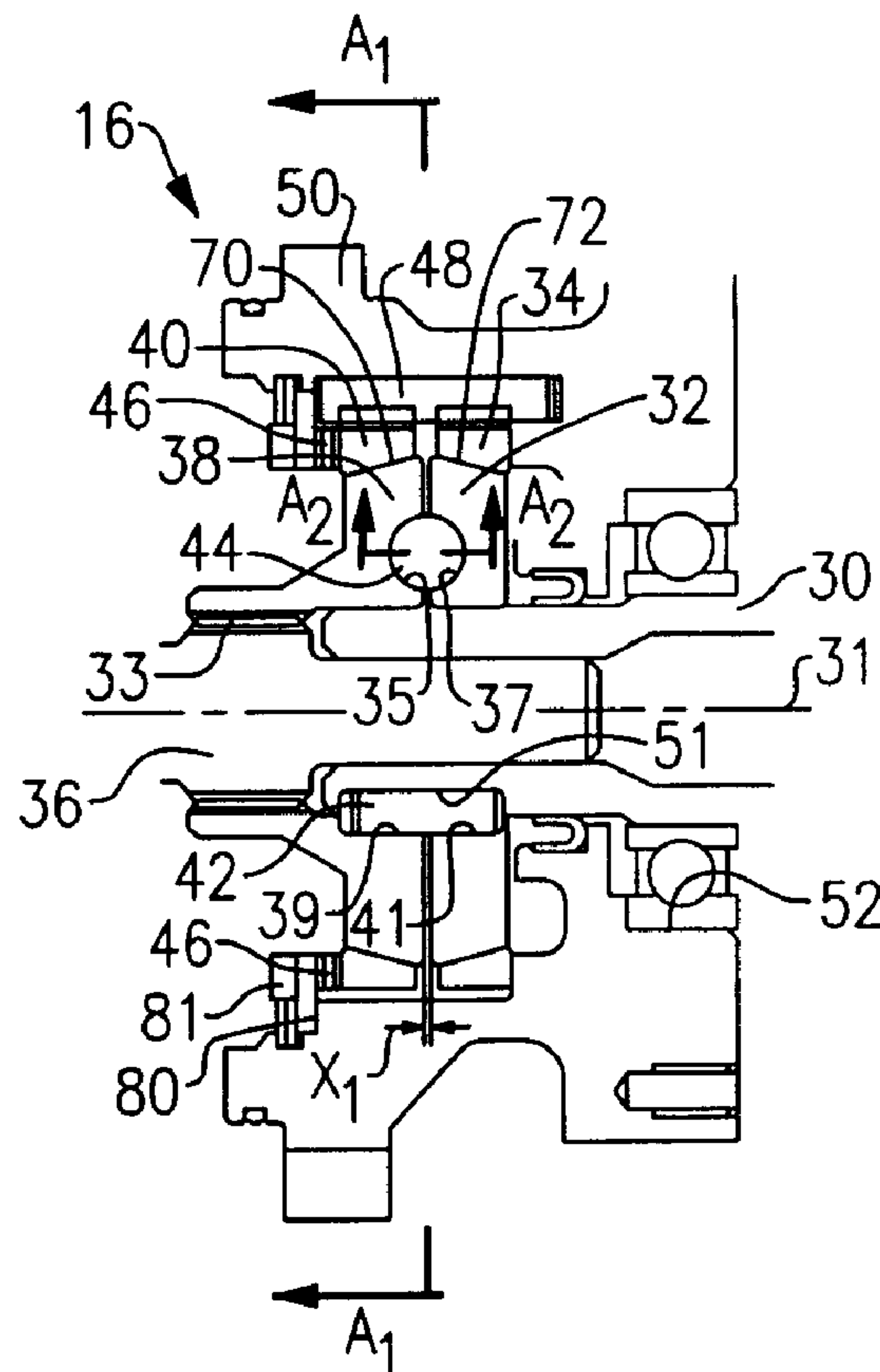
(72) Inventeurs/Inventors:
LANG, DAVID J., US;
REGAN, JAMES M., US;
MILLER, MARK D., US

(73) Propriétaire/Owner:
HAMILTON SUNDSTRAND CORPORATION, US

(74) Agent: NORTON ROSE FULBRIGHT CANADA
LLP/S.E.N.C.R.L., S.R.L.

(54) Titre : FREIN A CONE SANS FLASQUE

(54) Title: CONE BRAKE NO-BACK



(57) Abrégé/Abstract:

Disclosed is a cone brake no-back for use with an actuation system. The actuation system may be an aircraft actuation system, for example. The no-back may include cone brakes capable of preventing undesired displacement of an aircraft surface (such as a flap, a leading edge, or a trailing edge of a wing) in the event that an actuator input becomes disconnected or is otherwise insufficient to oppose the load created by the aircraft surface.



ABSTRACT OF THE DISCLOSURE

Disclosed is a cone brake no-back for use with an actuation system. The actuation system may be an aircraft actuation system, for example. The no-back may include cone brakes capable of preventing undesired displacement of an aircraft surface (such as a flap, a leading edge, or a trailing edge of a wing) in the event that an actuator input becomes disconnected or is otherwise insufficient to oppose the load created by the aircraft surface.

CONE BRAKE NO-BACK

BACKGROUND

This disclosure relates to a no-back for use with an actuation system.

5 No-backs are typically used with aircraft actuators, which may be used to
displace an aircraft surface, such as a flap, a leading edge, or a trailing edge of a
wing. Multiple actuators may be positioned on opposing sides of an aircraft, and are
typically driven by an input, which may be a drive line torque shaft. In the event of
failure or disconnect of the drive line torque shaft, for example, a no-back will
10 prevent an associated aircraft surface from being displaced from a desired position.

SUMMARY

Disclosed is a no-back assembly including first and second discs coupled to
respective first and second shafts. The first and second discs are arranged radially
15 outward of respective first and second shafts. The no-back assembly also includes
first and second brakes arranged radially outward of respective first and second
discs. The first and second brakes are configured to prevent the first and second
discs from rotating when in a no-back condition.

Also disclosed is a system including an actuator with a shaft receiving an
20 input and being coupled to a load. The system further includes a disc in
communication with the shaft. When in a no-back condition, the disc is brought into
contact with a brake disposed about the outer periphery of the disc such that the
shaft is substantially prevented from rotating.

Further disclosed is a method wherein a disc is rotated in a first rotational
25 direction when in a first operational state. The disc is then moved in a first axial
direction when in a second operational state. A brake is urged in a second axial
direction, opposite the first axial direction, in the second operational state such that
the brake is wedged into the disc and thus prevents the disc from rotating.

These and other features can be best understood from the following
30 specification and drawings, the following of which is a brief description.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic representative of an aircraft's actuation system;

Figure 2 is a typical rotary actuator including a cone brake no-back;

Figure 3a is a view of area A from Figure 2 depicting the cone brake no-back
 5 in a no-load, or opposing load, condition;

Figure 3b is a section taken along line A1-A1 from Figure 3a;

Figure 3c is a section taken along line B-B from Figure 3b;

Figure 3d is a view of area A from Figure 2 depicting the cone brake no-back
 in a no-back condition;

10 Figure 3e is a section taken along line A2-A2 from Figure 3a;

Figure 3f is a section taken along line C-C from Figure 3d;

Figure 4 is a schematic representative of the no-back in a no-load condition;

Figure 5 is a schematic representative of the no-back in an opposing load
 condition;

15 Figure 6 is a schematic representative of the no-back in a no-back condition;
 and

Figure 7 is a schematic representative of the no-back in an aiding load
 condition.

20 DETAILED DESCRIPTION

Referring to Figure 1, a schematic representative of an aircraft's actuation system is shown. Multiple actuators 11 may be arranged about a centerline 10 of the aircraft. Each of the actuators 11 are driven by an input (shown generically as actuator input 20 in Figure 2) from the drive line torque shaft 12, and may be
 25 coupled to a load 17 by way of a linkage mechanism 15. The drive line torque shaft 12 is driven by a PDU, or power drive unit, 14. The load 17 may be a movable aircraft surface, such as a flap, leading edge, or trailing edge of a wing. The load 17 generally imparts a torque, or load, on respective actuators 11. This load imparted onto the actuators 11 generally opposes the torque generated by the input from the
 30 drive line torque shaft 12. In a system without no-backs 16, an input insufficient to oppose the load 17 (e.g., if the drive line torque shaft or the PDU were to fail) may cause the actuator 11 to back-drive, thus causing the load 17 to displace from a

desired position. Thus, each of the actuators 11 include no-backs 16 to prevent back-drive of the actuators 11 and to prevent unwanted displacement of the load 17. In this regard, the no-backs 16 help maintain overall aircraft control. The system may further include position sensors 18 at either end of the drive line torque shaft 12 to monitor system position.

Referring to Figure 2, an actuator 11 including a no-back 16 is shown. As explained, the no-back 16 may be driven by an actuator input 20, which may be the drive line torque shaft 12. The drive line torque shaft 12 may rotate in forward and reverse directions. The drive line torque shaft 12 drives the no-back input shaft 30 which, in turn, drives the no-back output shaft 36. The no-back output shaft 36 is operatively coupled to the actuator output 22. The actuator output 22 may include input and output planetary gears 26 and 28, respectively, in communication with the no-back output shaft 36. The actuator output 22 is coupled to the load 17 by way of a linkage mechanism 15 (represented in Figure 1). The elements included within the no-back 16 are generally within area A. Area A is shown in detail in Figure 3a.

Figure 3a, is representative of the arrangement of the no-back 16 in a no-load condition, and in an opposing-load condition (schematically represented in Figures 4 and 5, respectively). In the opposing load condition, for example, the no-back 16 is positioned such that it allows the no-back input shaft 30 to transfer rotation to the no-back output shaft 36. The no-back input shaft 30, which may be supported by bearing 52, is coupled to the no-back output shaft 36 by way of input and output discs 32, 38 arranged about the outer periphery of input and output shafts 30, 36. The input and output discs 32, 38 may be made of a hardened steel or bronze and may be coated with Teflon®, for example. Notably, as shown, the no-back output shaft 36 is only coupled to the output disc 38, whereas the no-back input shaft 30 is operatively coupled to both of the input and output discs 32, 38.

The input and output discs 32, 38 are rotatably coupled to the no-back input shaft 30 by way of pins 42 arranged about the outer diameter of the no-back input shaft 30, for example. The no-back input shaft 30 may include recesses 51 about its outer diameter, each of which may receive a portion of a pin 42. The input and output discs 32, 38 may also include recesses 41 and 39, respectively. Each of the recesses 39, 41 are aligned with the recesses 51 to receive a portion of the pins 42.

Further, the output disc 38 may be coupled to the no-back output shaft 36 by way of a geared, or splined, connection 33.

Cone brakes 34, 40 are arranged about the outer periphery of (or, radially outward of) the input and output discs 32, 38, respectively. The cone brakes 34, 40 may be made of a known steel, for example. In the example shown, the cone brakes 34, 40 are coupled to a housing 50 by way of pins 48. The cone brakes 34, 40 may be coupled to the housing 50 such that they are rotatably fixed with respect to the input and output discs 32, 38, but can axially slide in the direction of the pins 48. The pins 48 may extend generally parallel to the axis 31, and thus the cone brakes 34, 40 may axially slide in the direction of the axis 31. A spring 46 may be disposed on one axial side of the cone brake 40 (in Figure 3a, the spring 46 is disposed to the left of the cone brake 40) and may bias (or preload, or urge) the cone brake 40 to the other axial side (in Figure 3a, the spring 46 biases the cone brake 40 to the right). Alternatively, the spring 46 may be disposed on the right side of the input disc 32 and may bias the cone brake 34 to the left (again, with reference to Figure 3a). The spring 46 may be a single compression spring, or a set of compression springs, and may be selected of an appropriate material, which may be a hardened steel, for example.

In the no-load and opposing load conditions, the spring 46 may contact the disc 40, which in turn contacts output disc 38, but it does not do so with sufficient force to prevent the input and output discs 32, 38 from rotating relative to respective cone brakes 34, 40. The spring 46 is utilized to urge (or, preload) the cone brake 40 and the output disc 38 into alignment with input disc 32 and cone brake 34, such that the balls 44 are positioned in the deep center portions 62 of the ballramps 35 and 37 (explained in detail below). The inner periphery of the cone brakes 34, 40 may include sloped, or angled, surfaces (generally represented at 70, 72). The outer periphery of the input and output discs 32, 38 also include sloped, or angled, surfaces (generally represented at 70, 72) such that the sloped surfaces of the cone brakes 34, 40 correspond with the sloped surfaces of a respective input disc 32, 38. Respective sloped surfaces of output disc 38 and cone brake 40 are generally represented by reference numeral 70. The sloped surfaces of input disc 32 and cone brake 34 are generally represented by reference numeral 72. As seen in Figure 3a,

respective sloped surfaces 70, 72 of the input and output discs 32, 38 and the cone brakes 34, 40 are sloped such that they extend generally parallel to one another. One will further appreciate that the sloped surfaces 70, 72 are sloped, or angled, relative to the axis 31.

5 The input and output discs 32, 38 are spaced apart by a distance X1 when in the no-load, or opposing load, condition shown in Figure 3a. The spacing of the input and output discs 32, 38 with respect to one another is regulated, in part, by the position of the balls 44 between the input and output discs 32, 38. Each of the input and output discs 32, 38 includes a ballramp 37, 35, respectively. The ballramps 35,
10 37 may extend into the input and output discs 32, 38 at a varying depth. The relationship of the position of the balls 44 within the ballramps 35, 37 to the spacing of the input and output discs 32, 38 is explained in detail below.

Referring to Figure 3b, a view taken along line A1-A1, from Figure 3a, is shown. As explained, the recesses 39 formed in the output disc 38 may be arranged
15 to correspond with the recesses 51 formed in the no-back input shaft 30. As shown, each of the recesses 39 and 51 receives a portion of a pin 42. In this manner, the no-back input shaft 30 is rotatably (or, operatively) coupled to the output disc 38 such that rotation of the no-back input shaft 30 is transferred to the output disc 38. Pins 48 may be arranged about the outer periphery of the cone brake 40. The pins 48
20 may be grounded to the housing 50, thereby preventing the cone brake 40 from rotating, but allowing it to slide axially. Kidney-shaped ballramps 35 are formed within the output disc 38, and are sized to receive at least a portion of a ball 44 therein. The ballramps 35 are explained in detail below.

Figure 3c is a view taken along line B-B, from Figure 3b, and is
25 representative of the varying depth of the ballramps 35, 37 as they extend into the input and output discs 32, 38. As shown, the ballramp 35 may include a deep center portion 62, which is the deepest portion of the ballramp 35. Shallow ends 60, 64 of the ballramp 35 may be sloped, or may taper, downwardly from an outer surface 61 of the output disc 38 toward the deep center portion 62. When the no-back 16 is in
30 the no-load and opposing-load conditions (as shown in Figure 3a and as schematically represented in Figures 4 and 5), the balls 44 may generally be positioned in the deep center portion 62 of respective ballramps 35, 37. This

position may be referred to as a neutral position, shown in Figure 3e. In this way, the balls 44 are positioned such that they extend into the input and output discs 32, 38 relatively deeply, and thus the distance X1 between the input and output discs 32, 38 is relatively small. That is, the input and output discs 32, 38 may be positioned
 5 such that the deep center portions 62 of the ballramps 35, 37 are in alignment, and such that the balls 44 are positioned between respective deep center portions 62 of the ballramps 35, 37. In the no-load and opposing-load conditions, the spring 46 generally urges the brake 40 such that the input and output discs 32, 38 are aligned, thus causing the balls 44 to settle in the deep center portions 62.

10 Referring to Figure 3d, the no-back 16 is shown in a no-back (or, holding-load) condition (schematically represented in Figure 6). Such a no-back condition may be created when the actuator input 20 is insufficient to oppose the load 17, or when the actuator input 20 fails (due to a failure of the PDU 14 or the drive line torque shaft 12, for example). In absence of actuator input 20, or when the actuator
 15 input 20 is insufficient to oppose the load 17, the load 17 may cause reverse rotation of the no-back output shaft 36, which in turn may cause output disc 38 to rotate relative to input disc 32 (because the no-back output shaft 36 is only coupled to the output disc 38, and not both of the input and output discs 32, 38). In this regard, the deep center portions 62 of the ballramps 35, 37 will also rotate out of alignment, and
 20 the balls 44 will be moved toward the shallow ends 60, 64 of the ballramps 35, 37, as shown in Figure 3f. Because the shallow ends 60, 64 do not extend as deeply into the respective input and output discs 32, 38 as the deep center portion 62, the positioning of the balls 44 causes the output disc 38 to become axially spaced from input disc 32 by a distance X2 (this position may be referred to as an extended
 25 position, shown in Figure 3f), which is greater than the distance X1. This positioning of the balls 44 generates an axial load on the input and output discs 32, 38 greater than the preload (or biasing force) generated by the spring 46.

As the balls 44 are positioned toward the shallow ends 60, 64 of the ballramps 35, 37, the output disc 38 engages the cone brake 40 (by way of their
 30 respective sloped surfaces 70) and causes the cone brake 40 to axially slide with the output disc 38 (to the left in Figure 3d). Again, as the load 17 is applied to the no-back output shaft 36, and then to the output disc 38, an axial load is generated by the

balls 44 that is transferred to both discs 32 and 38. This axial load generated by the balls 44 passes from the input and output discs 32, 38 to the cone brakes 34, 40, thus displacing output disc 38 and cone brake 40 (to the left in Figure 3d) relative to their position in the no-load and opposing-load conditions shown in Figure 3a. The cone
5 brake 40 thus compresses the spring 46 against the spacer 80 and retaining ring 81, both of which are fixed to the housing 50. By way of the compression of the spring 46, the cone brake 40 is urged toward the output disc 38 against the axial load generated by the positioning of the balls 44. In this manner, the cone brake 40 is wedged into the output disc 38 by way of the respective sloped surfaces 70. This
10 wedging action thus creates a frictional force between the cone brake 40 and the output disc 38 and between cone brake 34 and the input disc 32, respectively, creating a combined resistance torque (T_r) sufficient to overcome the torque created by load 17 on the no-back output shaft 36 (T_{load}). In this manner, the no-back input and output shafts 30, 36 and the input and output discs 32, 38 are prevented from
15 rotating. Thus, the load 17 is prevented from being displaced, and the no-back condition is effectively provided.

The following relationship may be referred to as gain (G).

$$G = \frac{T_r}{T_{load}}$$

One of ordinary skill will appreciate that several factors may affect gain (G)
20 including: the materials chosen for the input and output discs 32, 38 and the cone brakes 34, 40; the slope of the sloped surfaces 70, 72; the dimensions of the ballramps 35, 37, etc. In order for the no-back 16 to work properly, the gain (G) must be greater than 1 when in the no-back condition. That is, the above-mentioned factors must be set such that $T_r > T_{load}$ when in the no-back condition.

25 Figure 3e is a view taken along line A2-A2 from Figure 3a and shows the balls 44 arranged between the ballramps 35, 37 of the input and output discs 32, 38 such that the discs are spaced apart by a distance X1. Figure 3e is representative of a neutral position. The neutral position may be present during a no-load condition (schematically represented in Figure 4) and an opposing load condition
30 (schematically represented in Figure 5). The neutral position exists when the deep

center portions 62 of the respective input and output discs 32, 38 are in alignment, and the balls 44 are positioned between respective deep center portions 62.

Figure 3f is a view taken along line C-C from Figure 3d and shows the balls 44 arranged between the ballramps 35, 37 of the input and output discs 32, 38 such that input and output discs 32, 38 are spaced apart by a distance X2. Figure 3f is representative of an extended position. The extended position may be present during the no-back condition or during an aiding-load condition (schematically represented in Figures 6 and 7, respectively). The extended position exists when the deep center portions 62 of the respective input and output discs 32, 38 are out of alignment, and the balls 44 are positioned between respective shallow ends 60, 64 of the ballramps 35, 37. This positioning of the balls 44 creates an axial load on the input and output discs 32, 38 sufficient to overcome the preload (or biasing force) of the spring 46.

Referring to Figure 4, the no-back 16 is schematically represented in a no-load condition. The no-load condition is also represented in Figure 3a. Notably, in the no-load condition, the load 17 may be present, but may be positioned in a rest position so as to not impart a torque, or load (such as Tload), on the no-back output shaft 36. Thus, there may be no input (e.g., from actuator input 20), as there is no load for the input to oppose. As can be seen in Figure 4, the ball 44 is positioned in the center (shown as the deep center portion 62 in Figure 3c) of respective ballramps 35, 37. That is, the input and output discs 32, 38 are aligned such that the center of the ballramps 35, 37 are in alignment. Cone brakes 34, 40 are positioned outside of, or about the outer periphery of, the input and output discs 32, 38. As shown, spring 46 is positioned between the cone brake 40 and the housing 50 (the spring 46 may actually be in operative connection with the housing 50 by way of the spacer 80 and retaining ring 81, as shown in Figure 3a, for example).

Referring to Figure 5, the no-back 16 is schematically represented in an opposing-load condition (which is also represented in Figure 3a). In this condition, a forward input, Iforward, is sufficient to oppose, or overcome a load, L. That is, the forward input, Iforward, drives the no-back output shaft 36 in a forward rotational direction, such that the load L, which generally urges the no-back output shaft 36 in a reverse rotational direction, is opposed. In this manner, the load 17 is generally maintained in a desired position by virtue of the forward input, Iforward. Note that

the forward input, $I_{forward}$, is shown as engaging the input and output discs 32, 38 by way of a pin 42 (as described above).

Referring to Figure 6, the no-back 16 is shown in a no-back condition (also depicted in Figure 3d). The no-back condition, which is generally described above, may be caused by the failure of the drive line torque shaft 12 or the PDU 14, for example. In either case, the no-back input shaft 30 would not impart a forward input $I_{forward}$ sufficient to oppose the load L . In fact, when in the no-back condition there may be no input present at all (as the drive line torque shaft may have completely failed, for example). Regardless, when the forward input $I_{forward}$ is insufficient to oppose the load L , the no-back output shaft 36 is urged in a reverse rotational direction. Since the no-back output shaft 36 is only coupled to the output disc 38, rather than both of the input and output discs 32, 38, the input and output discs 32, 38 are brought out of alignment. That is, the ballramps 35, 37 of the input and output discs 32, 38 are brought out of alignment with one another. As explained above, this misalignment causes the balls 44 to be positioned away from the center of the ballramps 35, 37 and toward the shallow end portions 60, 64, for example (see Figure 3c). Because of this positioning of the balls 44 within the ballramps 35, 37, the input and output discs 32, 38 are spaced relative to one another (generally indicated as the distance $X2$ in Figures 3d and 3f). In Figure 6, this relative movement of the input and output discs 32, 38 is represented by downward movement of the output disc 38. Movement of the output disc 38 also causes the cone brake 40 to move toward the spring 46 and the housing 50 (the spring 46 may contact the housing 50 by way of the spacer 80 and retaining ring 81). The axial load that is generated by the positioning of the balls 44 within the ballramps 35 and 37 is sufficient to generate friction between the cone brake 40 and the output disc 38 and between the cone brake 34 and the input disc 32. This friction between the input and output discs 32, 38 and the cone brakes 34, 40 generates a combined resistance torque (T_r) sufficient to overcome the torque imparted onto the no-back output shaft 36 by the load L , defined above as T_{load} . Thereby, no-back 16 prevents the load 17 from being displaced, and the no-back condition is effectively provided.

Referring to Figure 7, the no-back 16 is shown in an aiding-load condition, wherein the no-back 16 may be released from the no-back condition. Essentially,

the no-back 16 can be released by adjusting the resistance torque (T_r). This may be accomplished by applying, a reverse input, $I_{reverse}$, to the no-back input shaft 30 of a sufficient magnitude to reduce the gain (G) to less than 1. In this way, the resistance torque (T_r) is reduced and rotation of the input and output discs 32, 38 and input and output shafts 30, 36 is again possible.

A worker of ordinary skill in this art would recognize that certain modifications of the instant disclosure would come within the scope of the claims. For example, although the no-back 16 has been described with reference to cone brakes 34, 40, alternate brake designs are contemplated within the scope of this disclosure. That is, the cone brakes 34, 40 may be representative of any brake arranged radially outward of the input and output discs 32, 38. Further, while the no-back 16 has been described with reference to use in aircrafts, one of ordinary skill would recognize that the no-back 16 need not be limited to use in aircrafts, and indeed may be applicable for use in other settings. Accordingly, the following claims should be studied to determine their true scope and content.

CLAIMS:

1. A no-back assembly comprising:
 - a first disc coupled to a first shaft and arranged radially outward of the first shaft;
 - a first brake arranged radially outward of the first disc, the first brake being configured to prevent the first disc from rotating when in a no-back condition; and
 - a spring adjacent the first brake, the spring configured to urge the first brake toward the first disc to prevent the first disc from rotating when in the no-back condition.
2. The no-back assembly of claim 1 further including:
 - a second disc coupled to a second shaft and arranged radially outward of the second shaft; and
 - a second brake arranged radially outward of the second disc, the second brake being configured to prevent the second disc from rotating when in the no-back condition.
3. The no-back assembly of claim 2 further including that the first disc is an output disc, the first shaft is an output shaft, the second disc is an input disc, and the second shaft is an input shaft; and
 - wherein the first disc is arranged radially outward of the first and second shafts.
4. The no-back assembly of claim 2 wherein, when in the no-back condition, the first and second brakes are brought into contact with respective first and second discs, and thereby the first and second shafts are substantially prevented from rotating.
5. The no-back assembly of claim 4 wherein the first shaft is urged in forward rotational direction by a forward input and is urged in a reverse rotational direction by

a load, the reverse rotational direction opposite the forward rotational direction, the first shaft being operatively coupled to the second shaft.

6. The no-back assembly of claim 5 wherein, when in the no-back condition, there is no input.

7. The no-back assembly of claim 6 wherein each of the first and second brakes are rotatably fixed relative to the first and second discs and include a sloped surface on an inner periphery thereof, the sloped surfaces of the first and second brakes being inclined relative to an axis of the first and second shafts, each of the first and second discs including a sloped surface about the outer periphery thereof, the sloped surfaces of the first and second discs inclined to be substantially parallel to the sloped surfaces of respective first and second brakes.

8. The no-back assembly of claim 7 wherein, when in the no-back condition, the sloped surfaces of the first and second brakes are brought into contact with respective sloped surfaces of the first and second discs such that a resistance torque is generated that is larger than a torque created by the load urging the first shaft in the reverse rotational direction.

9. The no-back assembly of claim 8 further including that each of the first and second discs include a ballramp formed therein, respective ballramps of the first and second discs being generally aligned with and facing one another.

10. The no-back assembly of claim 9 further including that a ball is positioned between the first and second discs such that the ball is supported partially by the ballramp of the first disc and partially by the ballramp of the second disc.

11. The no-back assembly of claim 10 wherein each of the ballramps are formed with a varying depth, the ballramps being deepest at a center portion, ends of the

ballramps including sloped portions such that the ballramps taper downwardly from the ends to the center portion.

12. The no-back assembly of claim 11 wherein the first brake is axially slidable and rotatably fixed relative to a housing, the first brake is in contact with the spring on a first side of the first brake and is in contact with the first disc on a second side of the first brake, the second side of the first brake being generally opposite the first side of the first brake.

13. The no-back assembly of claim 12 wherein, when in the no-back condition, the ball is positioned such that it contacts the sloped portion of the ballramp of the first disc and the sloped portion of the ballramp of the second disc, and thereby the first disc is displaced in a first axial direction and causes the first brake to slide axially in the first axial direction toward the spring, the spring urges the first brake in a second axial direction opposite the first axial direction such that the sloped surfaces of the first and second brakes are brought into contact with the sloped surfaces of respective first and second discs, thereby substantially preventing the first and second discs and the first and second shafts from rotating.

14. A system comprising:

- an actuator including a shaft receiving an input and coupled to a load;
- a disc in communication with the shaft;
- a brake disposed about an outer periphery of the disc;
- a spring adjacent the brake; and

when in a no-back condition, the brake is urged, by way of the spring, to contact the disc such that the disc and the shaft are substantially prevented from rotating.

15. A method of controlling rotation of a disc, comprising the steps of:

- a) rotating a disc in a first rotational direction when in a first operational state;

- b) moving the disc in a first axial direction when in a second operational state; and
- c) when in the second operational state, urging a brake in a second axial direction opposite the first axial direction such that the brake is wedged into the disc and thus prevents the disc from rotating.

16. The no-back assembly of claim 1 wherein the first brake is disposed about the outer periphery of the first disc.

17. The no-back assembly of claim 1 wherein at least one of the first brake and the first disc includes a sloped surface on a periphery thereof, the sloped surface being inclined relative to an axis of the first shaft.

18. The no-back assembly of claim 17 including a sloped surface on an outer periphery of the first disc, and a sloped surface on an inner periphery of the first brake.

19. The system of claim 14 wherein at least one of the disc and the brake includes a sloped surface on a periphery thereof, the sloped surface included relative to an axis of the shaft.

20. The system of claim 19 wherein the disc includes a sloped surface on an outer periphery thereof, and the brake includes a sloped surface on an inner periphery thereof.

21. The method of claim 15 wherein at least one of the disc and the brake includes a sloped surface on a periphery thereof, the sloped surface included relative to the first axial direction.

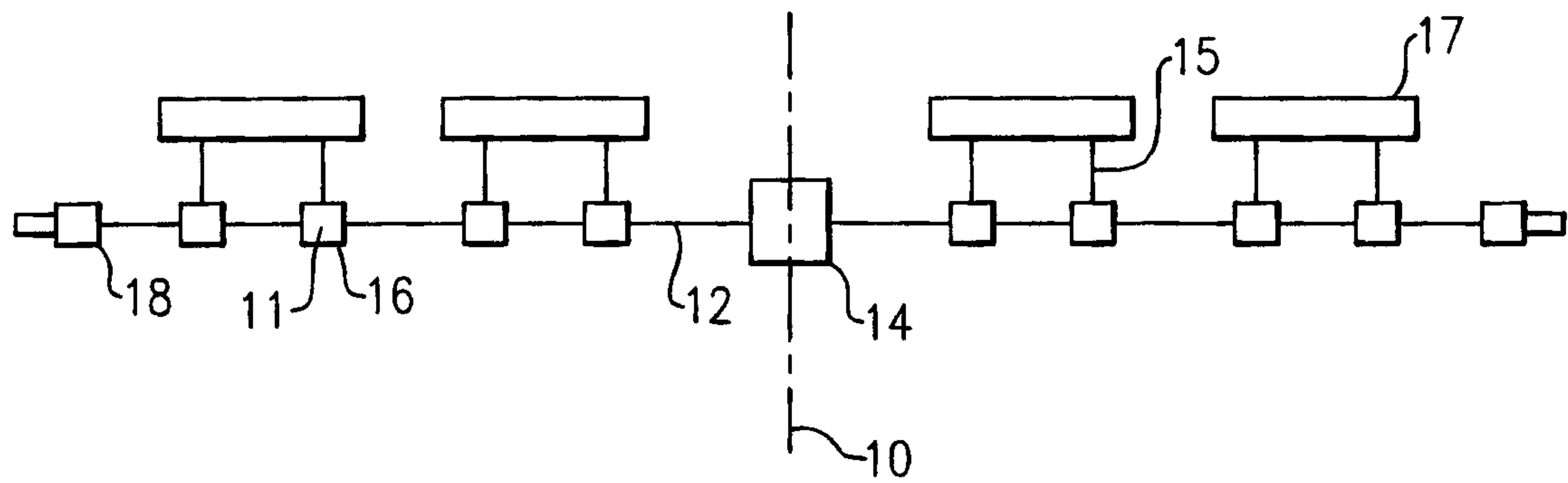
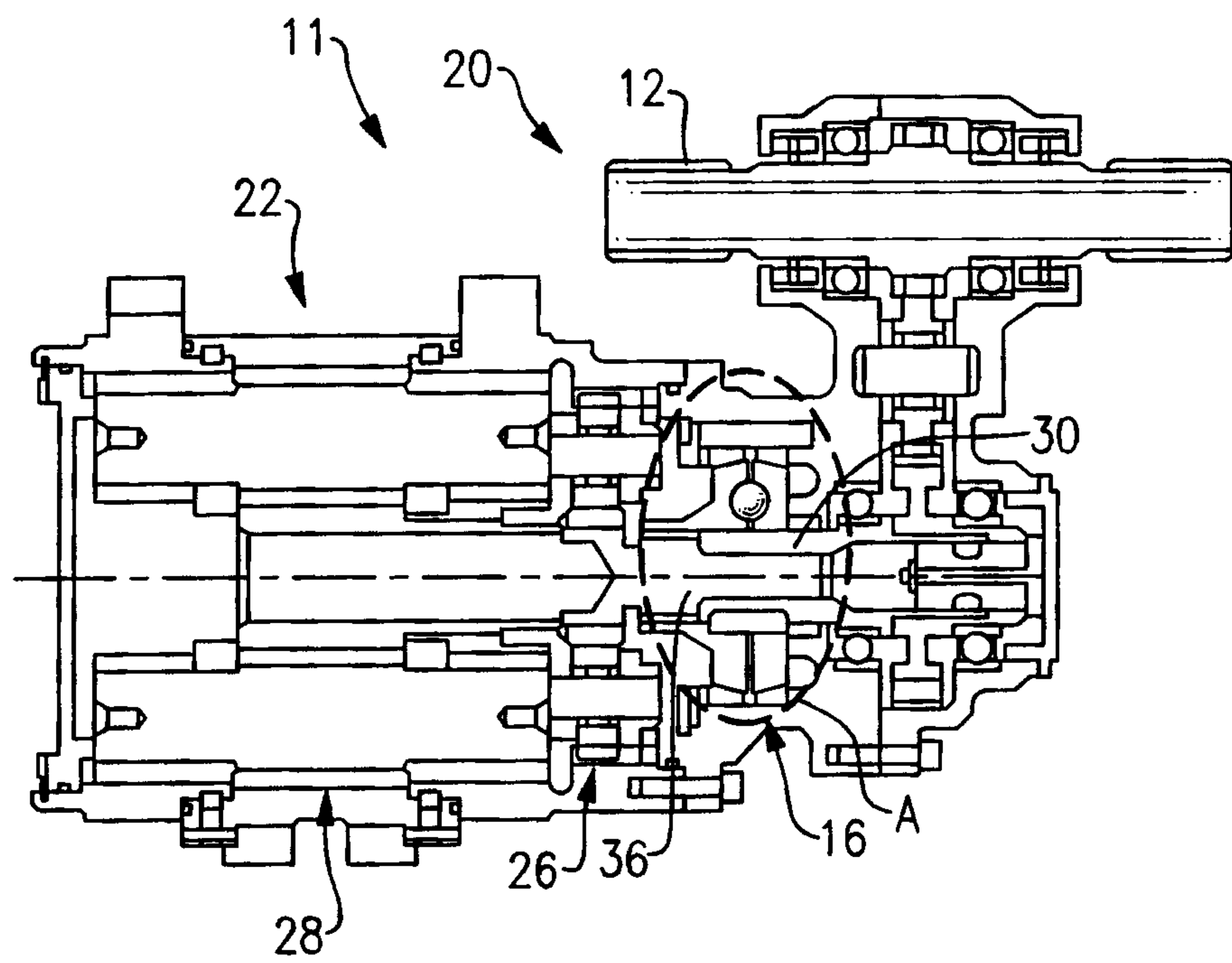
22. The no-back assembly of claim 1 wherein, when in the no-back condition, the first disc is urged in a first axial direction and the first brake is urged by the spring in

a second axial direction opposite the first axial direction such that the brake is wedged into the disc, thereby preventing the disc from rotating.

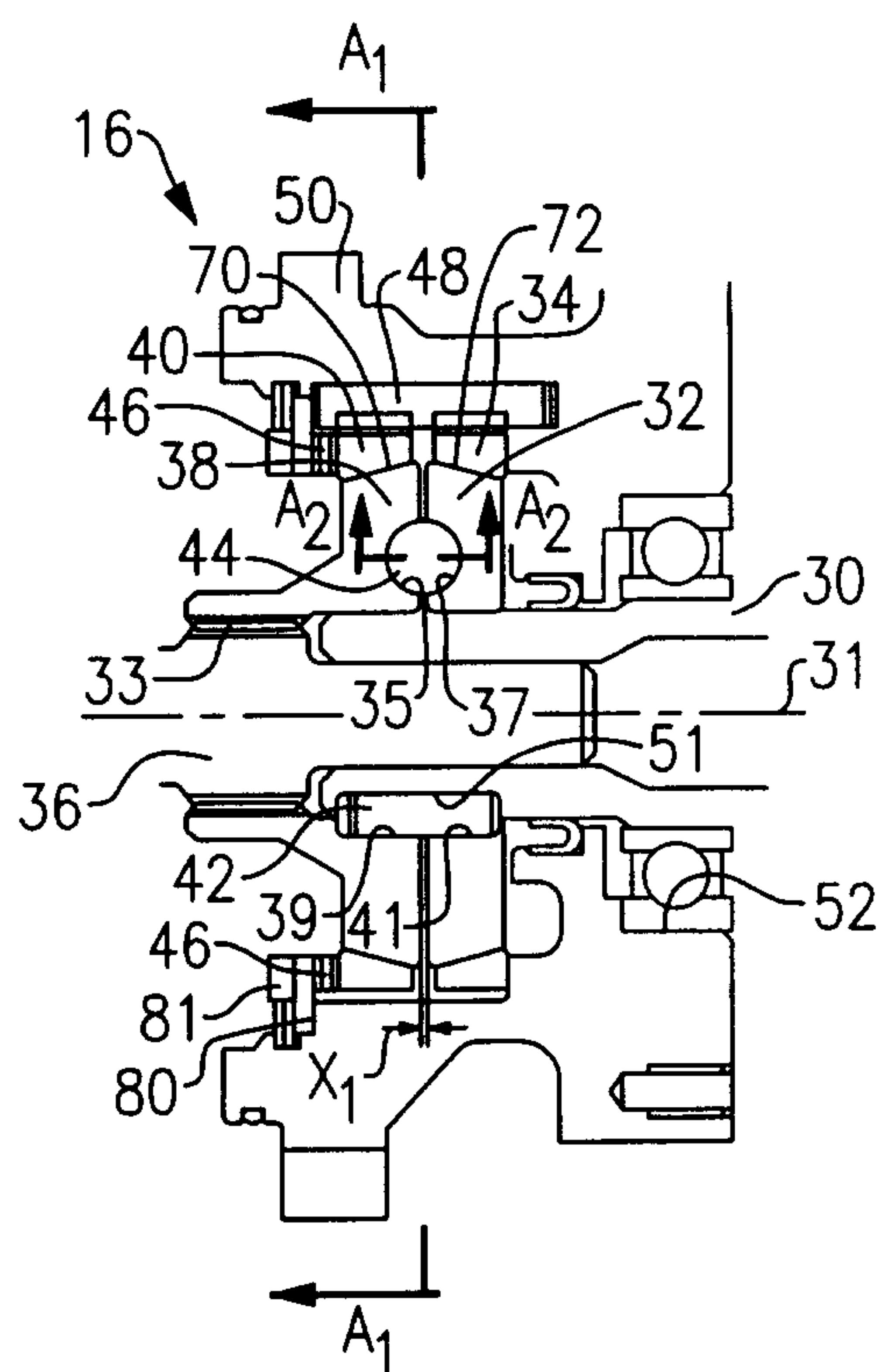
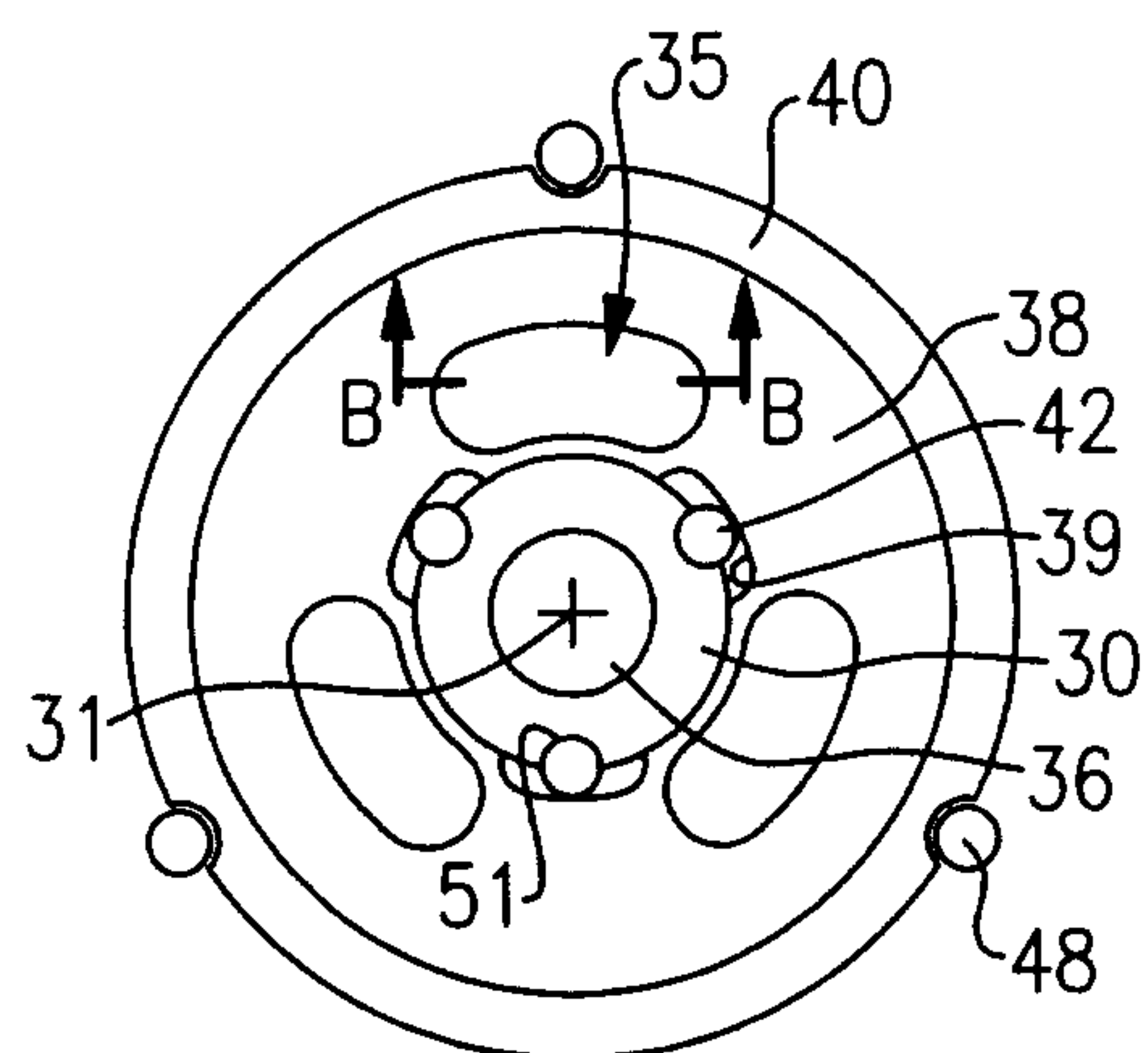
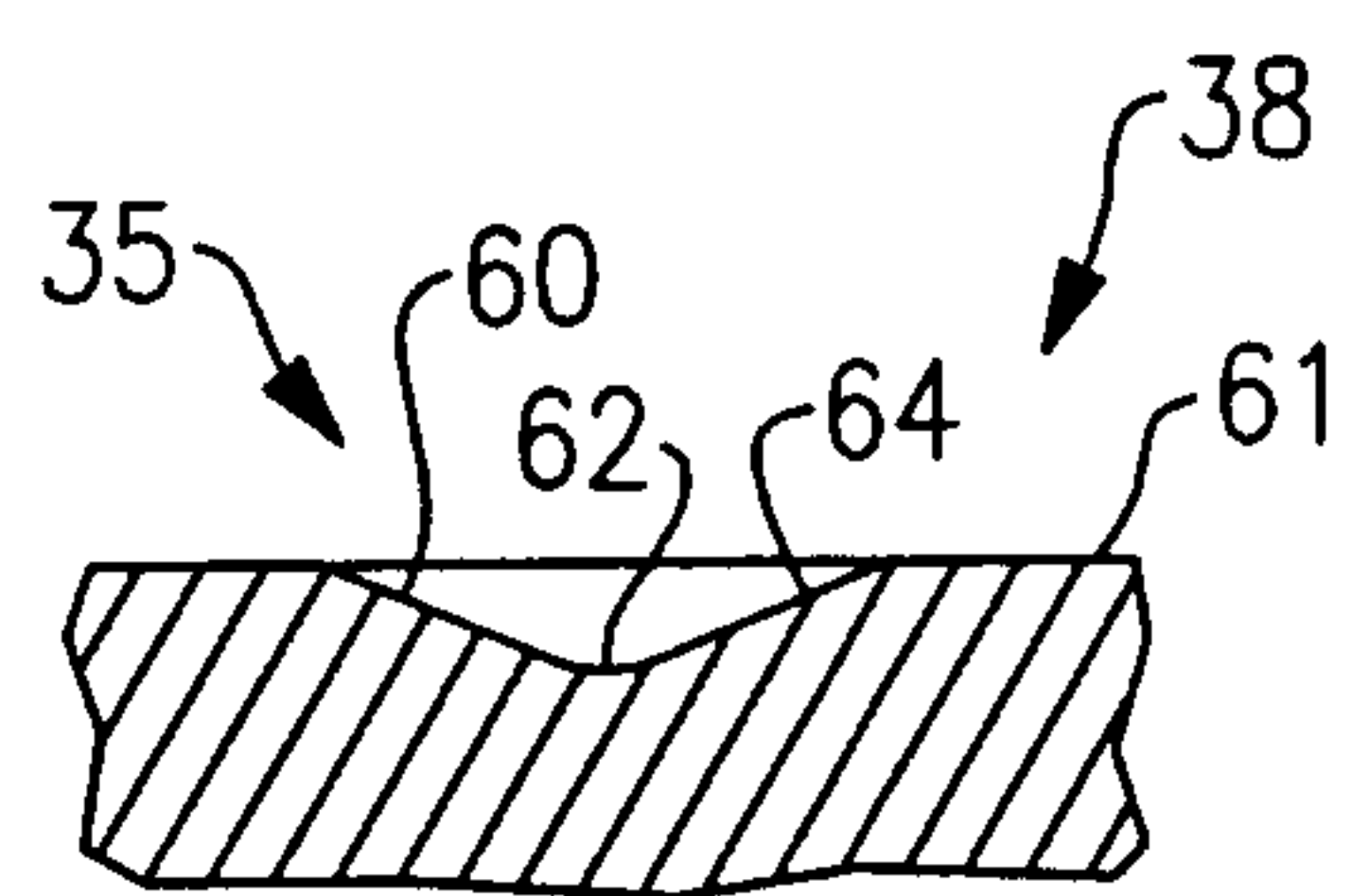
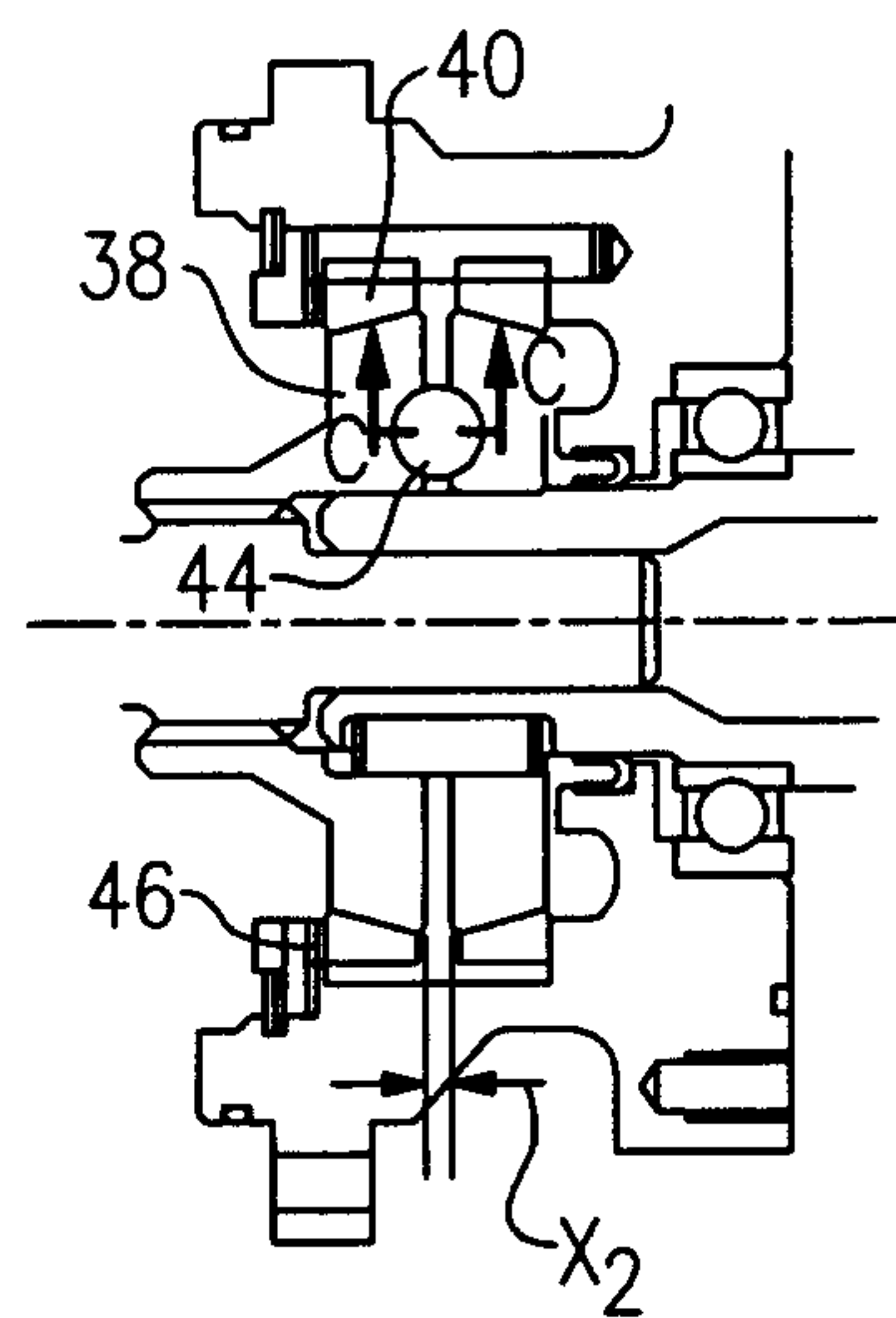
23. The system of claim 20 wherein, when in the no-back condition, the disc is urged in a first axial direction and the brake is urged by the spring in a second axial direction opposite the first axial direction such that the brake is wedged into the disc, thereby preventing the disc from rotating.

24. The method of claim 15 wherein the brake is urged in the second axial direction by way of a spring.

1/3

**FIG.1****FIG.2**

2/3

**FIG. 3a****FIG. 3b****FIG. 3c****FIG. 3d**

3/3

