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DESCRIPTION

Field of the Invention

[0001] The present invention relates to fuel cell systems, and more particularly, to apparatus' for generating a gas which may be used for startup and shutdown of a fuel cell.

Background

[0002] Fuel cell systems, such as fuel cell based power plants and mobile fuel cell based power generation equipment, generate electrical power via electrochemical reactions, and are coming into greater use because the exhaust byproducts are typically cleaner than traditional power plants, and because fuel cells may generate electricity more efficiently than traditional power plants. Fuel cell systems often employ stacks of individual fuel cells, each fuel cell typically including an anode, a cathode, and an electrolyte positioned between the anode and the cathode. The electrical load is coupled to the anode and the cathode. The anode and cathode are electrically conductive and permeable to the requisite gases, such as hydrogen and oxygen, respectively. In a solid oxide fuel cell (SOFC), the electrolyte is configured to pass oxygen ions, and has little or no electrical conductivity so as to prevent the passage of free electrons from the cathode to the anode. In order for the electrochemical reactions to take place efficiently, some fuel cells are operated at elevated temperatures, e.g., with anode, cathode and electrolyte temperatures in the vicinity of 700°C to 1000°C or greater for an SOFC.

[0003] During normal operation, a synthesis gas is supplied to the anode, and an oxidant, such as air, is supplied to the cathode. Some fuel cell systems include an internal reformer that catalytically reforms the fuel into a synthesis gas (syngas) by use of an oxidant. The fuel may be a conventional fuel, such as natural gas, gasoline, diesel fuel, or an alternative fuel, such as bio-gas, etc. The synthesis gas typically includes hydrogen (H₂), which is a gas frequently used in fuel cells of many types. The synthesis gas may contain other gases suitable as a fuel, such as carbon monoxide (CO), which serves as a reactant for some fuel cell types, e.g., SOFC fuel cells, although carbon monoxide may be detrimental to other fuel cell types, such as PEM (proton exchange membrane) fuel cells. In addition, the synthesis gas typically includes other reformer byproducts, such as water vapor and other gases, e.g., nitrogen and carbon dioxide (CO₂), methane (typically 1 %), as well as trace amounts of higher hydrocarbon slip, such as ethane.

[0004] In any event, the synthesis gas is oxidized in an electrochemical reaction in the anode with oxygen ions received from the cathode via migration through the electrolyte. The reaction creates water vapor and electricity in the form of free electrons in the anode that are used to power the electrical load. The oxygen ions are created via a reduction of the cathode oxidant using the electrons returning from the electrical load into the cathode.

[0005] Once the fuel cell is started, internal processes maintain the required temperature for operation. However, in order to start the fuel cell, the primary fuel cell system components must be heated, and some fuel cell system components must be protected from damage during the startup. For example, the anode may be subjected to oxidation damage in the presence of oxygen at temperatures below the normal operating temperature in the absence of the synthesis gas. Also, the reformer may require a specific chemistry in addition to heat, in order to start the catalytic reactions that generate the synthesis gas. Further, the startup of the fuel cell system should be accomplished in a safe manner, e.g., so as to prevent a flammable mixture from forming during the starting process. Still further, it is desirable to purge the fuel cell with a non-explosive and non-oxidizing gas during the initial stage of startup.

[0006] WO 2008/091801 A2 discloses a multistage combustor for starting a fuel cell system the combustor including a partial oxidation burner.

[0007] US 5928805 A discloses a cover and startup gas supply system for a solid oxide fuel cell power generator.

[0008] What is needed in the art is an improved apparatus and method for startup and shutdown of a fuel cell.

Summary

[0009] The present invention provides a reducing gas generator according to independent claim 1 for startup and shutdown of a fuel cell. Furthermore the invention provides a fuel cell system according to independent claim 14. For example, embodiments of the present invention may employ a nitrogen generator to generate a nitrogen-rich stream, e.g., using a nitrogen separation membrane, that may be used to purge one or more auxiliary subsystem components or other components of a fuel cell power plant.

[0010] In addition, the same and/or other embodiments of the present invention may include generating a low oxygen content oxidant, combining the oxidant with fuel to yield a feed mixture, and then catalytically converting the feed mixture to a reducing gas.

[0011] Also, the same and/or other embodiments of the present invention may include varying the oxygen content of the oxidant and also varying the oxidant/fuel ratio of the feed mixture in order to maintain the reducing gas at a desired temperature, e.g., a reaction temperature or a temperature downstream of the reactor.

[0012] Further, the same and/or different embodiments of the present invention may include controlling the oxygen content of the oxidant and also controlling the oxidant/fuel ratio of the feed mixture in order to maintain a desired catalyst exit temperature, while providing a desired reducing strength of the reducing gas, e.g., by varying the combustibles content of the reducing gas, while providing a desired flow rate of reducing gas.

[0013] Still further, the same and/or different embodiments of the present invention may include controlling the oxygen content of the oxidant and also controlling the oxidant/fuel ratio of the feed mixture in order to maintain a desired catalyst exit temperature, while providing a desired reducing strength of the reducing gas, e.g., by varying the combustibles content of the reducing gas, while varying the reducing gas flow.

[0014] Yet further, the same and/or different embodiments of the present invention may include controlling the oxygen content of the oxidant and also controlling the oxidant/fuel ratio of the feed mixture in order to maintain a desired reducing gas catalyst exit temperature, while varying, e.g., changing, the reducing strength of the reducing gas, e.g., by varying the combustibles content of the reducing gas.

[0015] Still yet further, the same and/or different embodiments of the present invention may include maintaining a temperature, e.g., of a heating device, at or above the catalyst light-off temperature of the feed mixture in order to reduce the amount of time required to begin producing reducing gas.

Brief Description of the Drawings

[0016] The description herein makes reference to the accompanying drawings, wherein like reference numerals refer to like parts throughout the several views, and wherein:

FIG. 1 schematically depicts a fuel cell system in accordance with an embodiment of the present invention.

FIG. 2 schematically depicts the fuel cell system of FIG. 1 in greater detail, including a reducing gas generator in accordance with an embodiment of the present invention.

FIGS. 3A-3D are a flowchart depicting a method for startup and shutdown of a fuel cell using a reducing gas generator in accordance with an embodiment of the present invention.

FIG. 4 is a plot depicting catalytic conversion parameters in a catalytic reactor of a reducing gas generator in accordance with an embodiment of the present invention.

Detailed Description

[0017] For purposes of promoting an understanding of the principles of the invention, reference will now be made to the embodiments illustrated in the drawings, and specific language will be used to describe the same. It will nonetheless be understood that no limitation of the scope of the invention is intended by the illustration and description of certain embodiments of the invention. In addition, any alterations and/or modifications of the illustrated and/or described embodiment(s) are contemplated

as being within the scope of the present invention. Further, any other applications of the principles of the invention, as illustrated and/or described herein, as would normally occur to one skilled in the art to which the invention pertains, are contemplated as being within the scope of the present invention.

[0018] Referring now to the figures, and in particular, FIG. 1, a schematic of a fuel cell system 10 in accordance with an embodiment of the present invention is depicted. Fuel cell system 10 includes one or more of a fuel cell 12, and includes a reducing gas generator 14. Fuel cell system 10 is configured to provide power to an electrical load 16, e.g., via electrical power lines 18. In the present embodiment, fuel cell 12 is a solid oxide fuel cell (SOFC), although it will be understood that the present invention is equally applicable to other types of fuel cells, such as alkali fuel cells, molten-carbonate fuel cells (MCFC), phosphoric acid fuel cells (PAFC), and proton exchange membrane (PEM) fuel cells. In the present embodiment, fuel cell system 10 is suitable, but not limited to, use in a fuel cell turbine hybrid system where high-pressure feed streams are employed.

[0019] Reducing gas generator 14 of the present embodiment is configured to generate a reducing gas having a combustibles content (which is primarily hydrogen - H₂ and carbon monoxide - CO) that may be varied within a compositional range of approximately 3% combustibles content to approximately 45% combustibles content. In other embodiments, different compositional ranges may be employed, for example, a range of approximately 2% combustibles content to approximately 50% combustibles content in some embodiments, and approximately 1% combustibles content to approximately 60% combustibles content in other embodiments. As set forth below, reducing gas generator 14 of the present embodiment is tailored to yield a start gas in the form of a reducing gas having a primary function of protecting the anode of fuel cell 12 from oxidation during startup of fuel cell 12, e.g., during system heat-up prior to power generation. As power generation is started, the reducing gas is transitioned off.

[0020] In the embodiment of FIG. 1, various features, components and interrelationships therebetween of aspects of an embodiment of the present invention are depicted. However, the present invention is not limited to the particular embodiment of FIG. 1 and the components, features and interrelationships therebetween as are illustrated in FIG. 1 and described herein. For example, other embodiments encompassed by the present invention, the present invention being manifested by the principles explicitly and implicitly described herein via the present Figures and Detailed Description and set forth in the Claims, may include a greater or lesser number of components, features and/or interrelationships therebetween, and/or may employ different components and/or features having the same and/or different nature and/or interrelationships therebetween, which may be employed for performing similar and/or different functions relative to those illustrated in FIG. 1 and described herein.

[0021] Referring now FIG. 2, fuel cell 12 and reducing gas generator 14 are described in greater detail. Fuel cell 12 includes at least one each of an anode 20, an electrolyte 22, a cathode 24, and a reformer 26. Anode 20, electrolyte 22 and cathode 24 are considered part of fuel cell 12. Reformer 26 is an internal steam reformer that receives steam as a constituent of a recycled fuel cell product gas stream, and heat for operation from fuel cell 12 electro chemical reactions. Reducing gas generator 14 is not a part of fuel cell 12, but rather, is configured for generating gases for use in starting up and shutting down fuel cell 12.

[0022] Anode 20 is electrically coupled to electrical load 16 via electrical power line 18, and cathode 24 is also electrically coupled to electrical load 16 via the other electrical power line 18. Electrolyte 22 is disposed between anode 20 and cathode 24. Anode 20 and cathode 24 are electrically conductive, and are permeable to oxygen, e.g., oxygen ions. Electrolyte 22 is configured to pass oxygen ions, and has little or no electrical conductivity, e.g., so as to prevent the passage of free electrons from cathode 24 to anode 20.

[0023] Reformer 26 is coupled to anode 20, and is configured to receive a fuel and an oxidant and to reform the fuel/oxidant mixture into a synthesis gas (syngas) consisting primarily of hydrogen (H₂), carbon monoxide (CO), as well as other reformer by-products, such as water vapor in the form of steam, and other gases, e.g., nitrogen and carbon-dioxide (CO₂), methane slip (CH₄), as well as trace amounts of hydrocarbon slip. In the present embodiment, the oxidant employed by fuel cell 12 during normal operations, i.e., in power production mode to supply electrical power to electrical load 16, is air, and the fuel is natural gas, although it will be understood that other oxidants and/or fuels may be employed without departing from the scope of the present invention.

[0024] The synthesis gas is oxidized in an electro-chemical reaction in anode 20 with oxygen ions received from cathode 24 via migration through electrolyte 22. The electro-chemical reaction creates water vapor and electricity in a form of free electrons on the anode that are used to power electrical load 16. The oxygen ions are created via a reduction of the cathode oxidant using the electrons returning from electrical load 16 into cathode 24.

[0025] Once fuel cell 12 is started, internal processes maintain the required temperature for normal power generating

operations. However, in order to start the fuel cell, the primary fuel cell system components must be heated, including anode 20, electrolyte 22, cathode 24 and reformer 26.

[0026] In addition, some fuel cell 12 components may be protected from damage during the start-up, e.g., due to oxidation. For example, anode 20 may be subjected to oxidative damage in the presence of oxygen at temperatures above ambient but below the normal operating temperature of fuel cell 12 in the absence of the synthesis gas. Also, reformer 26 may need a specific chemistry, e.g. H₂O in the form of steam in addition to the heat provided during start-up of fuel cell 12, in order to start the catalytic reactions that generate the synthesis gas. Further, it is desirable that fuel cell 12 be started in a safe manner, e.g., so as to prevent a combustible mixture from forming during the starting process. Thus, it may be desirable to purge anode 20 with a nonflammable reducing gas during the initial startup as the temperature of anode 20 increased. In one aspect, a characteristic of reducing gas generator 14 is that the reducing gas may be made sufficiently dilute in combustibles to prevent the potential formation of a flammable (i.e., potentially explosive) mixture upon mixing with air. This may be desirable during the low temperature portion of heat-up of fuel cell 12 where any combustibles mixing with air are below auto-ignition temperature, and therefore, can potentially build up to form dangerous quantities of potentially pressurized flammable gases within the vessel that contains fuel cell 12.

[0027] The reducing gas strength for protecting anode 20 of fuel cell 12 from oxygen migration can be quite high, e.g., up to 45% combustibles content in the present embodiment, up to 50% in other embodiments, and up to 60% combustibles content in still other embodiments. Mechanisms that cause the migration of oxygen through electrolyte 22 to the anode 20 side of the fuel cell 12 are often temperature dependent and include oxygen permeation through electrolyte 22 or oxygen transfer induced by short circuit currents. Also, physical leakage mechanisms may become worse with temperature as materials differentially expand. Thus, the ability of reducing gas generator 14 to increase combustibles content at high fuel cell 12 temperatures during startup may be particularly useful in protecting anode 20 from oxidation damage.

[0028] From a safety perspective, it may be possible to step to a greater reducing strength at higher temperatures during fuel cell 12 startup, since the possibility of mixing the reducing gas with a pressurized volume of air to form an combustible mixture in or near fuel cell 12 is reduced if the reducing gas is above auto-ignition temperature, because the reducing gas would tend to immediately burn upon mixing with air. In addition, this may prevent build-up of a flammable mixture that can potentially deflagrate if the mixture were to suddenly come in contact with an ignition source, since any such mixture would tend to burn immediately when above the auto-ignition temperature, rather than build up a large quantity of the mixture.

[0029] Thus, in some embodiments, it may be desirable to operate reducing gas generator 14 in a manner by which the reducing gas is initially weakly reducing and well below the flammability limit, e.g., 3% combustibles content in the present embodiment, although other values may be employed, for example, 2% combustibles content in some embodiments and 1 % combustibles content or less in other embodiments. In still other embodiments, the combustibles content may be greater than 3%. The combustibles content may subsequently be changed to a strongly reducing (i.e., higher combustibles) condition (higher reducing strength) when temperature conditions in fuel cell 12, e.g., anode 20, are high enough to ensure that the reducing gas is far above its lower flammability limit. For example, the strongly reducing condition may be up to 45% combustibles content in the present embodiment, up to 50% combustibles content in other embodiments, and up to 60% combustibles content or greater in yet other embodiments, depending upon the conditions in fuel cell 12. The increased energy input to the system with a stronger reducing gas may be offset by decreasing fuel flow to the fuel cell power plant's Off-Gas Burner for such plants so equipped.

[0030] Accordingly, embodiments of the present invention may employ reducing gas generator 14 to generate a purging gas to purge fuel cell 12 of oxidants, in particular, cathode 24, as well as to generate a safe gas, i.e., a weak reducing gas having a relatively low level of combustibles.

[0031] In addition, embodiments of the present invention may also employ reducing gas generator 14 to produce a variable-reducing-strength reducing gas. The reducing gas composition provided by reducing gas generator 14 may also be configured to contain adequate steam to initiate the operation of the internal reformer 26 as the normal fuel cell 12 fuel stream flow, e.g., natural gas, is started. Accordingly, the reducing gas supplied to fuel cell 12 from reducing gas generator 14 may be considered a transition gas as power production by fuel cell 12 is ramped up. Additionally, reducing gas generator 14 of the present embodiment may be capable of rapid start-up, e.g., for protecting anode 20 in the event of emergency fuel cell 12 shutdown events, for example, by maintaining certain elements of reducing gas generator 14 at elevated temperatures in order to speed up initiation of the catalytic reactions that yield the reducing gas.

[0032] In the present embodiment, as illustrated in FIG. 2, reducing gas generator 14 includes a fuel system 28, an oxidant system 30, a merging chamber 32, and a catalytic reactor 34 having a catalyst 36. In the present embodiment, the outputs of fuel

system 28 and oxidant system 30 are combined in merging chamber 32 and directed to fuel cell 12 via catalytic reactor 34 to selectively provide purging gas, safe gas, and variable strength reducing gas to anode 20 and reformer 26.

[0033] In the embodiment depicted in FIG. 2, various features, components and interrelationships therebetween of aspects of an embodiment of the present invention are depicted. However, the present invention is not limited to the particular embodiment of FIG. 2 and the components, features and interrelationships therebetween as are illustrated in FIG. 2 and described herein. For example, other embodiments encompassed by the present invention, the present invention being manifested by the principles explicitly and implicitly described herein via the present Figures and Detailed Description and set forth in the Claims, may include a greater or lesser number of components, features and/or interrelationships therebetween, and/or may employ different components and/or features having the same and/or different nature and/or interrelationships therebetween, which may be employed for performing similar and/or different functions relative to those illustrated in FIG. 2 and described herein.

[0034] In any event, in the embodiment of Fig. 2, fuel system 28 includes a fuel input 38, a pressure regulator 40, a sulfur capture sorbent 42, a fuel flow controller 44, and a variable position/output fuel control valve 46. Fuel input 38 is configured to receive a hydrocarbon fuel, e.g., natural gas, and serves as a source of the hydrocarbon fuel used by reducing gas generator 14. Pressure regulator 40 is fluidly coupled to fuel inlet 38, and regulates the pressure of the hydrocarbon fuel. Sulfur capture sorbent 42 is fluidly coupled to pressure regulator 40, and is configured to capture sulfur from the fuel stream received from pressure regulator 40. Fuel flow controller 44 and fuel control valve 46 are coupled to the output of sulfur capture sorbent 42, and are configured to control the amount of fuel delivered to merging chamber 32.

[0035] Oxidant system 30 functions as an oxidant source for reducing gas generator 14, and includes an air intake 48, an air compressor 50 as a pressurized air source, a pressure regulator 52, a nitrogen generator 54 having a nitrogen separation membrane 56, a variable position/output air control valve 58, an air flow controller 60, a variable position/output oxidant control valve 62, an oxidant flow controller 64 and an oxygen sensor 66.

[0036] Air intake 48 may be any structure or opening capable of providing air, and is fluidly coupled to air compressor 50, which compresses ambient air received from the atmosphere. Pressure regulator 52 is fluidly coupled to air compressor 50, and regulates the air pressure delivered to reducing gas generator 14. Air control valve 58 is part of an air charging system structured to variably add air to the nitrogen-rich gas received from nitrogen generator 54 to yield an oxidant having a variable O₂ content.

[0037] The O₂ content may be sensed by oxygen sensor 66, which may be used by the control system of reducing gas generator 14 to vary the O₂ content of the oxidant supplied to merging chamber 32. For example, under normal operating conditions, the O₂ content is controlled based on a control temperature, e.g., the temperature of catalyst 36 in the present embodiment, although other temperatures may be used in other embodiments, e.g., the temperature of the reducing gas output by reducing gas generator 14. However, during startup of reducing gas generator 14, oxygen sensor 66 may be used to provide feedback until the temperature is available as a feedback. The amount or flow of the oxidant having the variable O₂ content is controlled by oxidant control valve 62 and oxidant flow controller 64.

[0038] Nitrogen generator 54 is configured to generate a nitrogen-rich stream, which may be used as a purging gas, and which may also be combined with air to form a low oxygen (O₂) content oxidant stream, e.g., a nitrogen-diluted air stream, used by reducing gas generator 14 to form a reducing gas. The purity of the nitrogen-rich stream may vary with the needs of the particular application, for example, and may consist essentially of nitrogen. Alternatively, it is considered that in other embodiments, other gases may be employed in place of or in addition to nitrogen, such as argon or helium, for use as a purging gas and/or as a constituent of a low O₂ content oxidant stream, e.g., as a dilutant (diluent) of air. As used herein, "low O₂ content oxidant" means that the oxygen content of the oxidant stream is less than that of atmospheric air under the same pressure and temperature conditions.

[0039] Nitrogen generator 54 and air control valve 58 are fluidly coupled in parallel to pressure regulator 52, and receive pressurized air from air compressor 50 for use in reducing gas generator 14 operations. Nitrogen generator 54 has an output 54A, e.g., an opening or passage structured to discharge the products of nitrogen generator 54. Nitrogen generator 54 is structured to receive air from air intake 48, extract oxygen (O₂) from the air, and to discharge the balance in the form of a nitrogen-rich gas from the outlet. The extracted O₂ is discharged from nitrogen generator 54 to the atmosphere in the present embodiment, although it will be understood that in other embodiments, the extracted O₂ may be employed for other purposes related to fuel cell 12 and/or reducing gas generator 14, e.g., as part of an oxidant stream.

[0040] Nitrogen separation membrane 56 of nitrogen generator 54 is configured to separate oxygen out of the air received from

air intake 48, and provides the nitrogen-rich stream, which is then combined with the air supplied by air control valve 58 to yield the low O₂ content oxidant, which is delivered to oxidant control valve 62. Oxidant control valve 62 is fluidly coupled to the outputs of both nitrogen generator 54 and air control valve 58. Oxygen sensor 66, which may be in the form of an O₂ analyzer, is fluidly coupled downstream to oxidant control valve 62, and provides a control signal via control line 68 that communicatively couples oxygen sensor 66 with air flow controller 60. Air flow controller 60 provides control signals to air control valve 58 to control the amount of air added to the nitrogen-rich stream based on the control input from oxygen sensor 66.

[0041] Merging chamber 32 is in fluid communication with the output of nitrogen generator 54 and fuel input 38, and is structured to receive and combine the hydrocarbon fuel and nitrogen-rich gas and discharge a feed mixture containing both the fuel and the oxidant including the nitrogen-rich gas to catalytic reactor 34. Catalytic reactor 34 is structured to receive the feed mixture and to catalytically convert the feed mixture into a reducing gas. The form of merging chamber 32 is a simple plumbing connection joining the oxidant stream with the fuel stream in the present embodiment, although any arrangement that is structured to combine an oxidant stream with a fuel stream may be employed without departing from the scope of the present invention. For example, a dedicated mixing chamber having swirler vanes to mix the streams may be employed.

[0042] Reducing gas generator 14 includes a start control valve having a valve element 70 and a valve element 72; and a feed mixture heater 74, which may be used to start the process of generating reducing gas. In one form, valve elements 70 and 72 are part of a combined valving element. The inlets of valve elements 70 and 72 are fluidly coupled to merging chamber 32 downstream thereof. The outlet of valve element 70 is fluidly coupled to catalytic reactor 34 for providing the feed mixture to catalyst 36 of catalytic reactor 34. The outlet of valve element 72 is fluidly coupled to the inlet of feed mixture heater 74. In one form, the start control valve is a three-way valve that operates valve elements 70 and 72 to direct flow entering the start control valve into catalytic reactor 34 directly or via feed mixture heater 74. It is alternatively considered that other valve arrangements may be employed, such as a pair of individual start control valves in place of the start control valve with valve elements 70 and 72.

[0043] Feed mixture heater 74 includes a heating body 76 and a flow coil 78 disposed adjacent to heating body 76. The outlet of feed mixture heater 74 is fluidly coupled to catalytic reactor 34 for providing heated feed mixture to catalyst 36 of catalytic reactor 34. In the normal operating mode, valve elements 70 and 72 direct all of the feed mixture directly to the catalytic reactor 34. In the startup mode, the feed mixture is directed through feed mixture heater 74. In one form, all of the feed mixture is directed through feed mixture heater 74, although in other embodiments, lesser amounts may be heated.

[0044] Feed mixture heater 74 is configured to "light" the catalyst 36 of catalytic reactor 34 (initiate the catalytic reaction of fuel and oxidant) by heating the feed mixture, which is then supplied to catalytic reactor 34. In one form, the feed mixture is heated by feed mixture heater 74 to a preheat temperature above the catalyst light-off temperature of the feed mixture (the catalyst light-off temperature is the temperature at which reactions are initiated over the catalyst, e.g., catalyst 36). Once catalyst 36 is lit, the exothermic reactions taking place at catalyst 36 maintain the temperature of catalytic reactor 34 at a controlled level, as set forth below. Also, once catalyst 36 is lit it may no longer be necessary to heat the feed mixture, in which case valve elements 70 and 72 are positioned to direct all of the feed mixture directly to the catalytic reactor 34, bypassing feed mixture heater 74.

[0045] In order to provide for a quick supply of reducing gas in the event of a sudden shutdown of fuel cell 12, heating body 76 is configured to continuously maintain a temperature sufficient to light catalyst 36 during normal power production operations of fuel cell 12. That is, while fuel cell 12 is operating in power production mode to supply power to electrical load 16, which is the normal operating mode for fuel cell 12, heating body 76 maintains a preheat temperature sufficient to heat the feed mixture in order to be able to rapidly light the catalyst for startup of reducing gas generator 14 so that reducing gas may be supplied to fuel cell 12 during shutdown.

[0046] In addition, one or more catalyst heaters 80 are disposed adjacent to catalytic reactor 34, and are configured to heat catalyst 36 and maintain catalyst 36 at a preheat temperature that is at or above the catalyst light-off temperature for the feed mixture supplied to catalytic reactor 34. This preheat temperature is maintained during normal operations of fuel cell 12 in power production mode in the event of a sudden need for reducing gas, e.g., in the event of the need for a shutdown of fuel cell 12.

[0047] In other embodiments, it is alternatively considered that another heater 82 may be used in place of or in addition to heaters 74 and 80, e.g., a heater 82 positioned adjacent to catalytic reactor 34 on the upstream side. Such an arrangement may be employed to supply heat more directly to catalyst 36 in order to initiate catalytic reaction of the feed mixture in an upstream portion of catalytic reactor 34.

[0048] In the present embodiment, heaters 74, 80 and 82 are electrical heaters, although it is alternatively considered that in

other embodiments, indirect combustion heaters may be employed in addition to or in place of electrical heaters. Also, although the present embodiment employs both feed mixture heater 74 and heaters 80 to rapidly light the feed mixture on the catalyst, it is alternatively considered that in other embodiments, only one such heater may be employed, or a greater number of heaters may be employed, without departing from the scope of the present invention.

[0049] A control temperature sensor 84 is positioned adjacent catalyst 36 of catalytic reactor 34, and is structured to measure the temperature of catalyst 36. In one form, control temperature sensor 84 is structured to provide a signal indicating the temperature of a portion of catalyst 36 via a sense line 92 that communicatively couples air flow controller 60 with control temperature sensor 84. The control temperature is a temperature employed by control system 96 in regulating the output of reducing gas generator 14. Air flow controller 60 is configured to direct the operations of air control valve 58 based on the signal received from control temperature sensor 84 in conjunction with the signal received from oxygen sensor 66. In another form, other temperatures may be sensed for purposes of controlling reducing gas generator 14. For example, in one such embodiment, the temperature of the reducing gas produced by reducing gas generator 14, e.g., as output by catalytic reactor 34, may be measured and used as a control temperature feedback to direct the operations of air control valve 58.

[0050] A reducing gas combustibles detection sensor 86, which in the present embodiment is in the form of a hydrogen (H₂) sensor or H₂ analyzer, is configured to determine the quantity of one or more combustibles, e.g., percent mole, present in the reducing gas output by catalytic reactor 34. In other embodiments, reducing gas combustibles detection sensor 86 may be in the form of a carbon monoxide (CO) sensor or analyzer in addition to or in place of the H₂ sensor/analyzer. In any case, a control line 94 communicatively couples fuel flow controller 44 and reducing gas combustibles detection sensor 86. Reducing gas combustibles detection sensor 86 is configured to supply a signal reflecting the combustibles content of the reducing gas to fuel flow controller 44. Fuel flow controller 44 is configured to control the amount of fuel delivered to merging chamber 32.

[0051] The reducing gas output by catalytic reactor 34 is cooled using a heat exchanger 88. In one form, heat exchanger 88 is an indirect heat exchanger. In other embodiments, other types of heat exchangers may be employed. In one form, reducing gas combustibles detection sensor 86 is positioned downstream of heat exchanger 88. In other forms, reducing gas combustibles detection sensor 86 may be positioned in other locations, for example, upstream of heat exchanger 88 or inside of or mounted on heat exchanger 88.

[0052] The pressure output of catalytic reactor 34 is maintained by a backpressure regulator 90 downstream of heat exchanger 88. Heat exchanger 88 maintains the temperature of the reducing gas downstream of catalytic reactor 34 at a suitable level to prevent damage to backpressure regulator 90. In one form, the reducing gas is cooled to between 100°C and 150°C using cooling air. In other embodiments, other suitable fluids may be used as the heat sink, and other temperatures may be used. In one form, a control loop (not shown) may be used to control the temperature of the reducing gas exiting heat exchanger 88 by varying the flow of cooling air or other cooling fluid.

[0053] The output of reducing gas generator 14 is fluidly coupled to catalytic reactor 34, and is in fluid communication with anode 20, e.g., either directly or via reformer 26. The output of backpressure regulator 90 serves as a reducing gas output in the present embodiment, and is operative to direct the reducing gas to anode 20 and reformer 26. The "reducing gas output" is the output of reducing gas generator 14 that discharges the product of reducing gas generator 14 into fuel cell 12, and may be one or more of any opening or passage structured to discharge the products of reducing gas generator 14.

[0054] Fuel flow controller 44, air flow controller 60 and oxidant flow controller 64 form a control system 96 that is structured to control the temperature and chemical makeup of the product mixture supplied from catalytic reactor 34 based on the signals output by oxygen sensor 66 (during startup in the present embodiment), control temperature sensor 84 and reducing gas combustibles detection sensor 86. In particular, air control valve 58 is controlled by air flow controller 60 to regulate the O₂ content of the oxidant stream supplied to merging chamber 32, e.g., the amount of O₂ expressed as a mole percentage of the O₂ in the oxidant stream. Oxidant control valve 62 is controlled by oxidant flow controller 64 to regulate flow of the oxidant stream formed of nitrogen-rich gas and air supplied to merging chamber 32. Fuel control valve 46 is controlled by fuel flow controller 44 to regulate the amount of hydrocarbon fuel supplied to merging chamber 32.

[0055] Thus, in the present embodiment, control system 96 is configured to control the oxygen (O₂) content of the oxidant stream, and to also control the oxidant/fuel ratio of the feed mixture, which is defined by a ratio of the amount of the oxidant in the feed mixture to the amount of hydrocarbon fuel in the feed mixture, e.g., the mass flow rate of the oxidant stream relative to the mass flow rate of the hydrocarbon fuel stream. In particular, the O₂ content of the oxidant stream supplied to merging chamber 32 is controlled by air control valve 58 via the output of air flow controller 60 based on the signal received from oxygen sensor 66. In addition, the oxidant/fuel ratio of the feed mixture supplied to catalytic reactor 34 is controlled by fuel control valve 46 and oxidant

control valve 62 under the direction of fuel flow controller 44 and oxidant flow controller 64, respectively. In one form, the flow of reducing gas output by reducing gas generator 14 is controlled by oxidant control valve 62, e.g., including an offset or other compensation to account for the amount of fuel in the feed mixture, whereas the oxidant/fuel ratio is then controlled using fuel control valve 46. In other embodiments, other control schemes may be employed.

[0056] In the present embodiment, each of fuel flow controller 44, air flow controller 60 and oxidant flow controller 64 are microprocessor-based, and execute program instructions in the form of software in order to perform the acts described herein. However, it is alternatively contemplated that each such controller and the corresponding program instructions may be in the form of any combination of software, firmware and hardware, and may reflect the output of discreet devices and/or integrated circuits, which may be co-located at a particular location or distributed across more than one location, including any digital and/or analog devices configured to achieve the same or similar results as a processor-based controller executing software or firmware based instructions, without departing from the scope of the present invention. Further, it will be understood that each of fuel flow controller 44, air flow controller 60 and oxidant flow controller 64 may be part of a single integrated control system, e.g., a microcomputer, without departing from the scope of the present invention.

[0057] In any event, control system 96 is configured to execute program instructions to both vary the O₂ content of the oxidant stream and vary the oxidant/fuel ratio of the feed mixture while maintaining a selected temperature of the reducing gas in order to achieve a selected combustibles content at desired flow rate. The flow rate may be varied, e.g., depending upon the particular application or operational phase. Control system 96 varies the O₂ content of the oxidant stream and the oxidant/fuel ratio of the feed mixture based on the output of control temperature sensor 84, oxygen sensor 66 and reducing gas combustibles detection sensor 86.

[0058] Reducing gas generator 14 may be employed during startup and shutdown of fuel cell 12, e.g., to provide reducing gas of various reducing strengths, including reducing gas in the form of a safe (non-flammable) gas, and in some embodiments, to provide a purging gas with no combustibles.

[0059] The reducing gas is generated by combining the nitrogen-rich stream with air supplied via air control valve 58 to form the oxidant stream, which is regulated by oxidant control valve 62 and combined with the hydrocarbon fuel supplied via fuel control valve 46 to form the feed mixture that is catalytically converted in catalytic reactor 34 into the reducing gas. As set forth herein, the O₂ content of the oxidant stream and the oxidant fuel ratio of the feed mixture are varied by control system 96 in order to both regulate the control temperature, e.g., at catalytic reactor 34, while also controlling the reducing strength of the reducing gas to achieve the selected combustibles content at the desired flow rate.

[0060] The combustibles content may be selected in order to provide the appropriate reducing gas chemical configuration during various phases in the fuel cell 12 startup and shut down processes. In the present embodiment, control system 96 is structured to maintain the control temperature, e.g., the catalyst 36 temperature, while varying the combustibles content. For example, the reducing strength may be varied from weakly reducing, i.e., a low reducing strength, for purposes of forming a safe gas, to a high reducing strength having greater combustibles content. The combustibles content is primarily in the form of hydrogen (H₂) and carbon monoxide (CO).

[0061] The safe gas may be supplied to fuel cell 12 during ramp up to fuel cell 12 operating temperature. In one form, the reducing gas may be supplied to fuel cell 12 in the form of a safe gas to transition reformer 26 into service. In another form, as the operating temperature of fuel cell 12 increases, e.g., the temperature of anode 20 and reformer 26, the strength of the reducing gas may be increased by increasing the combustibles content of the reducing gas, which may thus protect anode 20 at the higher temperatures at which a significant amount of oxidation damage may otherwise occur, e.g., due to oxygen migration through electrolyte 22 or other leakages. In addition, as anode 20 (and/or reformer 26, in some embodiments) approaches normal operating temperatures, the combustibles content of the reducing gas may be further increased to achieve combustibles content levels similar to that of the synthesis gas that is produced by reformer 26 during normal power generation operations of fuel cell 12, which may help initiate the normal electrical power-producing reactions of anode 20. In embodiments where supplied to reformer 26, this may help initiate the normal operating catalytic reactions of reformer 26.

[0062] Regarding the purging gas, in some embodiments, a noncombustible purging gas may be generated by nitrogen generator 54 in the form of a nitrogen-rich stream, e.g., consisting primarily of nitrogen, which may be supplied to fuel cell 12 via back pressure regulator 90, although other plumbing schemes to direct the output of nitrogen generator 54 to fuel cell 12 may alternatively be employed. In one form, the purging gas may be supplied to fuel cell 12, e.g., to purge one or more of cathode 24 and/or other fuel cell 12 components, e.g., when a cold start of fuel cell 12 is desired. In another form, the purging gas may be supplied to fuel cell 12 to purge fuel cell 12 before maintenance. In yet another form, nitrogen generator 54 and/or a second

nitrogen generator may be employed to create a purge gas. For example, in the event of a loss of the power plant's main air supply during an emergency shut-down, a nitrogen rich cathode purge may be supplied to cathode 24 with, e.g., using nitrogen generator 54 and/or a second nitrogen generator, while nitrogen generator 54 is used to generate the reducing gas supplied to the anode 20 loop. Such embodiments may be used to ensure that "safe" non-flammable mixtures reside in the fuel cell 12 vessel.

[0063] Having thus described exemplary means for varying the combustibles content of the reducing gas output by catalytic reactor 34 while maintaining a constant reducing gas output temperature from catalytic reactor 34, including means for varying the O₂ content in oxidant supplied to merging chamber 32 and means for varying the oxidant/fuel ratio of feed mixture exiting merging chamber 32, an exemplary embodiment of a method for generating a purging gas and a reducing gas for startup and shutdown of a fuel cell is described as follows. The exemplary embodiment is described with respect to FIGS. 3A-3D, which form a flowchart having control blocks B100-B146 depicting a method for starting up and shutting down a fuel cell. Although a particular sequence of events is illustrated and described herein, it will be understood that the present invention is not so limited, and that other sequences having the same or different acts in lesser or greater numbers and in the same or different order may be employed without departing from the scope of the present invention.

[0064] Referring now to FIG. 3A, at block B100, a command to start fuel cell 12 is received by control system 96, e.g., via an operator of fuel cell 12.

[0065] At block B102, a bypass system is engaged. The bypass system opens a vent line to vent the output of reducing gas generator 14, and closes the flowpath to fuel cell 12. The output of reducing gas generator is vented until the control loop, e.g., control system 96, holds process parameters within their prescribed bounds, at which point the bypass system closes the vent line and opens the flowpath to fuel cell 12.

[0066] Air is then supplied to reducing gas generator 14, e.g., via air intake 48, by initiating operation of air compressor 50.

[0067] At block B104, air compressor 50 compresses the air received from air intake 48. In one form, the air is compressed to a pressure in a range from 5 bar absolute to 14 bar absolute. In other embodiments, the pressure of the compressed air may fall within a different range, for example, in a range from 2 bar absolute to 25 bar absolute in some embodiments, and in other embodiments, 1 bar absolute to 30 bar absolute. The pressure supplied by air compressor 50 may vary, for example, depending upon the characteristics of nitrogen separation membrane 56 and nitrogen generator 54.

[0068] At block B106, the nitrogen-rich gas stream is generated in nitrogen generator 54 of reducing gas generator 14 by supplying the compressed air to nitrogen separation membrane 56. The O₂ removed from the air by nitrogen separation membrane 56 as a byproduct of the nitrogen generation process is directed offboard, e.g., for use elsewhere, or simply vented, whereas the resulting nitrogen-rich stream is directed toward oxidant control valve 62. In the present embodiment, the nitrogen-rich stream contains oxygen, albeit at levels lower than that of ambient air. In other embodiments, the nitrogen stream may consist essentially of nitrogen (e.g., <1% O₂).

[0069] At block B110, compressed air is added to the nitrogen-rich stream in a controlled manner by air control valve 58 under the direction of air flow controller 60 to form a low oxygen (O₂) content oxidant stream, i.e., an oxidant stream having less O₂ than ambient atmospheric air.

[0070] At block B112, a flow of hydrocarbon fuel to reducing gas generator 14 is initiated by fuel control valve 46 under the direction of fuel flow controller 44. Fuel flow may be initially set to a default value anticipated to achieve the desired combustibles content of the reducing gas and the control temperature, and may be subsequently adjusted.

[0071] At block B114, the oxidant stream is combined with the hydrocarbon fuel stream in merging chamber 32 to form the feed mixture having an oxidant/fuel ratio, e.g., defined by a ratio of the mass flow rate of the oxidant stream in the feed mixture to the mass flow rate of the hydrocarbon fuel stream in the feed mixture.

[0072] Referring now to FIG. 3B, at block B116, heating devices are operated at a temperature at or above the catalyst light-off temperature of the feed mixture, and the heat output by the heating devices is supplied to the feed mixture. In one form, the heating devices are turned on immediately after receiving the command to start the fuel cell 12, e.g., immediately after block B100. In other embodiments, the heating devices may be turned on at other times suitable to the application, e.g., depending upon how much time it takes the heaters to reach the desired temperature. In the present embodiment, the heating devices are feed mixture heater 74 and heater 80, although in other embodiments, only one heater may be employed or a plurality of heaters may be employed in place of or in addition to one or both of feed mixture heater 74 and heater 80. The types or forms of heaters

used in other embodiments may vary with the needs of the application.

[0073] Heating body 76 and flow coil 78 are maintained at or above the catalyst light-off temperature of the feed mixture. The heat from heating body 76 and flow coil 78 is supplied to the feed mixture by diverting feed mixture through feed mixture heater 74, in particular, flow coil 78. In one form, all of the feed mixture is diverted through feed mixture heater 74. In another form, a portion of the feed mixture is diverted through feed mixture heater 74. The feed mixture is diverted to flow coil 78 by controlling the output of the start control valve to operate valve elements 70 and 72. The resulting heated feed mixture is directed to catalyst 36 of catalytic reactor 34 to help initiate the catalytic reactions that yield reducing gas. Once the catalytic reactions in catalytic reactor 34 have been started, the three-way start control valve is re-oriented to direct all of the feed mixture directly to catalytic reactor 34, bypassing feed mixture heater 74. While the present application is described using a feed mixture heater 74 with heating body 76 and flow coil 78, it will be understood that other types of heaters may be employed in embodiments that utilize a flow mixture heater.

[0074] Heater 80 of the present embodiment is in the form an electric band heater, and maintains catalyst 36 at or above the catalyst light-off temperature of the feed mixture, thereby promoting rapid lighting (hence, re-lighting) of catalyst 36. It will be understood that other types of heaters may be employed without departing from the scope of the present invention.

[0075] In other embodiments, heater 82 may be employed to heat catalyst 36 at or near the location where the feed mixture is supplied to catalyst 36 in order to initiate the catalytic reactions. In various other embodiments, one or more heaters 82 may be used in place of or in addition to heaters 74 and 80.

[0076] At block B118, the heated feed mixture is directed to catalyst 36, where catalytic reactions are initiated. In one form, the catalytic reactions are initiated based on the heat received from feed mixture heater 74. In various other forms, the reactions may be initiated based on heat received from feed mixture heater 74 and/or heater 80 and/or heater 82).

[0077] At block B120, the feed mixture is catalytically converted to reducing gas in catalytic reactor 34 of reducing gas generator 14.

[0078] At block B122, the O₂ content of the oxidant stream and the oxidant/fuel ratio of the feed mixture are each controlled by control system 96 to maintain the selected control temperature of the reducing gas and to yield the reducing gas in the form of a safe gas. In one form, the O₂ content of the oxidant stream is controlled by air flow controller 60 directing the operations of air control valve 58, although in other embodiments, the O₂ content of the oxidant stream may be controlled differently. In one form, the oxidant/fuel ratio is controlled by fuel flow controller 44 directing the operations of respective fuel control valve 46, although in other embodiments, the oxidant/fuel ratio may be controlled differently. Prior to reaching the control temperature, control of the O₂ content may be based on the output of oxygen sensor 66. Once a temperature indicating catalytic combustion is achieved, the control algorithm switches to feedback based on control temperature sensor 84. The control temperature in some embodiments may be, for example, a function of reducing gas flow rate (catalyst load), time at service, or some other operating parameter. In other embodiments, the output of either or both of oxygen sensor 66 and control temperature sensor 84 may be employed during system startup and/or normal operation.

[0079] The flow rate of the feed mixture is controlled primarily by oxidant flow controller 64 directing the operations of oxidant control valve 62. In the form of a safe gas, i.e., a weakly reducing gas mixture, the reducing gas may have a combustibles content (e.g., predominantly CO+H₂) of approximately 4.5%. Other reducing gases having greater or lesser percentages of combustibles content may be employed without departing from the scope of the present invention.

[0080] Because the mass flow of the feed mixture is based predominantly on the flow rate of the oxidant flow stream, the total flow of the feed mixture, and hence the reducing gas output by reducing gas generator 14, is based primarily on the flow rate of the oxidant control flow stream as governed by oxidant flow controller 64. The selected control temperature in the present embodiment is 800°C, which is measured at one of the hottest points in catalyst 36, and which in the present embodiment yields a bulk average temperature of 770°C. The selected temperature in the present embodiment is a predetermined temperature value selected based on life considerations for components of reducing gas generator 14 and fuel cell 12, as well as catalytic conversion efficiency. Other temperature values and measurement locations may be employed in other embodiments.

[0081] At block B124, the bypass system is disengaged from the bypass mode, and the reducing gas in the form of a safe gas is thus directed from reducing gas generator 14 to anode 20 of fuel cell 12. In other embodiments, the safe gas may be directed to reformer 26.

[0082] Referring now to FIG. 3C, a block B126 is illustrated. In one form, block B126 is bypassed, and process flow proceeds directly to block B128. In another form, at block B126 the O₂ content of the oxidant stream and the oxidant/fuel ratio of the feed mixture are controlled to selectively vary the reducing strength of the reducing gas by selectively varying the combustibles content of the reducing gas while maintaining the selected temperature of the reducing gas of block B122. As set forth above with respect to block B122, in one form, the O₂ content of the oxidant stream is controlled by air flow controller 60 directing the operations of air control valve 58. In other forms, the O₂ content of the oxidant stream may be controlled differently. In one form, the oxidant/fuel ratio is primarily controlled by fuel flow controller 44, and the reducing gas flow is primarily controlled by oxidant flow controller 64 directing the operations of oxidant control valve 62. In other forms, the oxidant/fuel ratio and reducing gas flow rate may be controlled differently.

[0083] Control of the O₂ content of the oxidant stream and of the oxidant/fuel ratio of the feed mixture to selectively vary the reducing strength of the reducing gas while maintaining the selected temperature and flow rate of the reducing gas output by catalytic reactor 34 in the present embodiment is now described.

[0084] Reducing gas generator 14 catalytically converts the low O₂ content oxidant and hydrocarbon fuel to form the reducing gas with sufficient combustibles content to protect fuel cell anode 20 of fuel cell 12 during start-up and shutdown of the fuel cell system 10 power plant. By adjusting the O₂ content of the oxidant gas in combination with changing the oxidant/fuel ratio, the reducing gas strength may be changed while the catalyst operating temperature is held constant, e.g., at an ideal conversion temperature. This temperature is sensed by control temperature sensor 84 and used as input to control system 96 for use in maintaining the output temperature of catalytic reactor 34 at the selected temperature.

[0085] Referring now to FIG. 4, an example of catalytic reactor 34 parameters is depicted. The illustrated parameters include oxidant stream mass flow rate 100; hydrocarbon fuel stream mass flow rate 102; percent (%) stoichiometric air 104, which represents the percentage amount of air in the oxidant stream relative to the amount of air required for complete combustion of the hydrocarbon fuel stream; and the oxygen/carbon ratio (O₂/C) 106. In the plot of FIG. 4, the abscissa is H₂ content of the reducing gas, the left-hand ordinate is in units of percent and also grams per second (g/s), against which % stoichiometric air 104 and oxidant stream mass flow rate 100 are plotted. The right-hand ordinate is in units of both molar fraction and g/s, against which O₂/C ratio 106 and hydrocarbon fuel stream mass flow rate 102 are plotted.

[0086] FIG. 4 illustrates catalytic reactor 34 operating parameters over a reducing gas compositional range of 2% to 20% H₂ and 1% to 10% CO (3% to 30% CO+H₂). To produce higher combustibles content (CO+H₂), the O₂ content in the oxidant is raised. At a constant oxidant/fuel ratio of the feed mixture, e.g., air to fuel ratio, raising the O₂ content in the oxidant stream reduces combustibles and raises operating temperature. However, in the present embodiment, as the O₂ content in the oxidant stream is increased, the oxidant/fuel ratio of the feed mixture is simultaneously decreased, i.e., made more fuel rich, in order to achieve higher combustibles content at the same operating temperature.

[0087] By varying both the O₂ content in the oxidant stream and the oxidant/fuel ratio of the feed mixture, a broad range of reducing gas strengths may be achieved at a selected catalyst operating temperature, e.g., 770°C in the present embodiment. For example, in one form, the range may extend from a reducing gas strength that represents normal operating conditions for reformer 26 (~45% CO+H₂) to weakly reducing conditions (~3% CO+H₂). In other forms, different ranges may be employed, e.g., as set forth herein.

[0088] As 20% H₂ content in the reducing gas is approached, conditions in catalytic reactor 34 may approach that normally occurring in reformer 26 in power production mode as the oxidant approaches air with respect to %O₂ content and the O₂ to C molar ratio reaches 0.65. As the reducing gas becomes richer in combustibles, the fuel flow may increase by a factor of about 4 at 20% H₂ relative to weakly reducing conditions. The percentage of the fuel burned may decrease significantly as conditions approach those in the reformer 26. The temperature may be sustained because the lower percentage of combustion oxygen is offset by the combination of the elevated fuel flow rate and the decreased heat dissipation through less N₂ dilution in the oxidant. Thus, even though the O₂ concentration in the oxidant increases for increased reducing strength, as a percentage of oxygen required to completely consume the fuel, the oxygen level decreases. In the present embodiment, percent CO content is about ½ of the percent of H₂ content at the desired operating temperature, and hence the combustibles content of the reducing gas is approximately 1.5 times the percent of H₂ content in the reducing gas. While described in the present application with respect to a fuel cell system, it will be understood that reducing gas generator 14 is equally applicable to other systems, such as systems for generating reducing gas for other purposes.

[0089] Referring again to FIG. 3C, at block B128, the reducing gas is supplied to reformer 26, and to anode 20, e.g., via reformer 26.

[0090] At block B130, a transition of fuel cell 12 into power production mode is initiated, which includes supplying to fuel cell 12 flows of the primary fuel and the primary oxidant that are normally provided to fuel cell 12 for operation in power production mode, in contrast to the oxidant and hydrocarbon fuel provided to reducing gas generator 14 to generate reducing gas for use during startup or shutdown of fuel cell 12. The transition into power production mode also includes heating portions of fuel cell 12, including anode 20 and reformer 26, to normal operating temperature in a controlled fashion so as to reduce mechanical stresses that might result from thermal gradients within and between such components. The heating of fuel cell 12 may be performed prior to, during and after the provision of reducing gas to fuel cell 12, and may be performed until satisfactory operating temperatures in such portions, e.g., anode 20 and reformer 26, are achieved. During the transition into power production mode, the bypass system may be transitioned into bypass mode.

[0091] At block B132, fuel cell 12 is operated in power production mode, i.e., normal operating mode, to supply power to electrical load 16.

[0092] At block B134, the airflow and fuel flow supplied to reducing gas generator 14 are terminated, ending the production of reducing gas by reducing gas generator 14.

[0093] Referring now to FIG. 3D, at block B136, the temperature of the heating device is maintained at or above the temperature required to initiate catalytic reaction of the feed mixture at catalyst 36. This temperature is maintained during operation of the fuel cell in the power production mode, e.g., in order to provide for rapid restart of reducing gas generator 14, including rapid restart of catalyst 36, in the event of a need to shut down fuel cell 12.

[0094] At block B138, a command to shut down fuel cell 12 from the power production mode is received by control system 96, e.g., via a human input or an automated process. It will be noted that in some embodiments, block B136 may be performed subsequent to receiving the command to shut down fuel cell 12. For example, in some embodiments, the heating device may not be heated to a temperature at or above the catalytic light-off temperature until the command to shutdown fuel cell 12 is received.

[0095] At block B140, reducing gas generator 14 generates reducing gas in response to the command, e.g., by performing some or all of the actions indicated above with respect to blocks B102 to B128, including controlling the O₂ content of the oxidant stream and the oxidant/fuel ratio of the feed mixture to selectively vary the reducing strength of the reducing gas by selectively varying the combustibles content of the reducing gas to a desired level while maintaining a selected temperature, e.g., the selected temperature of block B122, above.

[0096] At block B142, the reducing gas generated by reducing gas generator 14 is supplied to anode 20 of fuel cell 12 by disengaging the bypass system from the bypass mode. This may help to prevent oxidation damage to anode 20 during shutdown of fuel cell 12. Initially, the reducing gas may have a high reducing strength, which may be decreased as the temperature of fuel cell 12 decreases.

[0097] At block B144, a transition of fuel cell 12 out of the power production mode is initiated, including gradually reducing the flow to anode 20 of the primary fuel that is normally provided during operation in power production mode.

[0098] At block B146, the airflow and fuel flow supplied to reducing gas generator 14 are terminated, ending the production of reducing gas by reducing gas generator 14. Block B146 may be executed after anode 20 is sufficiently cooled to a temperature at which oxidative damage is not a concern, which may vary with the materials used to manufacture anode 20.

[0099] A reducing gas generator in accordance with some embodiments of the present application may include a compressed air supply that feeds a polymer nitrogen-separation membrane, which uses the high pressure to segregate oxygen from nitrogen across a polymer fiber. Such embodiments may preclude the need for bottled nitrogen. In other embodiments, other nitrogen sources may be employed. The product gas is a nitrogen-rich stream that is depleted in oxygen. A variable-position bypass valve may divert a relatively small stream of the feed air around the nitrogen generator for blending with the nitrogen-rich stream. In some embodiments, the bypass airflow is directly proportional to the final oxygen content of the blended streams. The blended stream of nitrogen-rich product gas and bypass air may be referred to as an oxidant stream, which passes through a flow control device that sets the flow of oxidant to the process. The bypass valve controls the proportions of bypass air and nitrogen-rich gas to achieve the desired oxygen content of the oxidant stream.

[0100] A relatively small quantity of hydrocarbon fuel may be metered into the oxidant stream through a flow control device. In a steady state flow mode, the premixed oxidant and fuel blend is fed directly into a catalytic reactor that converts the feed mixture into the reducing gas. Compared with ordinary combustion in air, the reduced oxygen content oxidant stream may translate to less fuel per unit combustibles yield in the reducing gas. Thus, the required chemical energy input (i.e., the thermal load due to the input of fuel) per unit production of combustibles (e.g., H₂ and CO) may also be decreased, and therefore, less heat may need to be extracted from the process gas to cool the product stream to a required temperature. The nitrogen dilution of the oxidant stream may also decrease the reaction temperature into the range that may be preferable for the catalyst, and may not exceed the material limits in the downstream heat exchanger. In contrast to embodiments of the present invention, a reactor designed for combustion with normal air (in contrast to the nitrogen-rich oxidant employed in embodiments of the present invention) at the required scale might be complex, and might require cooling jackets that would likely require a liquid coolant, or otherwise a very high volumetric flow of coolant gas, and therefore, would have a relatively large heat duty in order to protect reactor materials from excessive temperature. In contrast, the catalytic reactor of some embodiments of the present invention may be designed to operate at a lower temperature without the need for external cooling.

[0101] Fuel oxidation with an oxygen-depleted oxidant may yield a given range of combustibles concentration (or molar flow) over a much wider range of air to fuel ratio relative to ordinary combustion with air, which makes control of the combustibles content easier to achieve.

[0102] Thermocouple(s) may monitor the exit temperature at the catalyst exit. The thermocouple may act as the control input for the air bypass valve. If the exit temperature were to fall too far below the set point, a control signal would open the bypass by some amount since an oxidant stream having a higher proportion of O₂ elevates the exit temperature (by oxidizing more fuel) and vice versa. The set point temperature is set high enough to achieve complete conversion of the flammable feed mixture to the equilibrated gas composition, but not too high as to approach the operational material limit temperatures for either the catalyst or the downstream heat exchanger.

[0103] An oxygen sensor 66 may measure the oxygen content on a volume basis of the oxidant stream downstream of the mix point for the bypass air and the nitrogen-rich stream exiting the nitrogen generator. An alternative embodiment may employ the measured oxygen concentration rather than the exit temperature to position air bypass control valve so that the exit temperature is maintained to a set point value. This may be preferable at start-up before a representative steady state reactor exit temperature is available to set the bypass valve position.

[0104] The oxygen sensor may be a small zirconia sensor maintained at a high temperature, e.g., around 600°C for some embodiments, which develops a Nernst potential when exposed to oxygen, which is related to the oxygen content of the gas. The sensor can be located in-situ. However, the sensor may alternatively be submerged in a controlled small slip stream that is blown down off the main process line through a critical flow orifice. The control software may dictate the relationship between the deviation of the measured oxygen content from the targeted value, and the incremental amount the bypass valve is opened as a result. The sensor may have a rapid response to changes in the oxygen content of the process gas, and therefore, the optimized tuning parameters on the air bypass valve control loop may provide more reliable control over a broader range of conditions.

[0105] The downstream heat exchanger cools the reducing gas to a temperature that is required for introduction of the reducing gas into the downstream process. A temperature control loop may vary a flow of cooling air or other cooling medium to the heat exchanger based on the deviation of the catalyst exit temperature from the temperature set point of the outlet gas. The heat exchanger may be a compact alloy steel or ceramic design to withstand the temperature of the gas exiting the catalyst.

[0106] A hydrogen or combustibles sensor may extract a slipstream of the process gas downstream of the heat exchanger to measure the percent by volume hydrogen or combustibles as a constituent of the reducing gas. The control software may compare the measured %H₂ to a set point value, and based on the difference sends a control signal to fuel control valve. If the measured %H₂ deviates too far below the set point, the fuel feed would be increased, and vice versa. The control software may dictate the relationship between the deviation of the measured %H₂ with the targeted % H₂, and the incremental amount the fuel valve is opened or closed.

[0107] One approach for continuously measuring hydrogen uses a thermal conductivity hydrogen sensor calibrated over the permissible range of hydrogen content for the reducing gas. Similar to the oxygen sensor, a critical flow orifice may be used as a relatively inexpensive and simple way to meter a very small slipstream of the reducing gas at the correct sample gas flow to the sensor.

[0108] A method for rapid restart of the catalyst from a standby condition to bring the reducing gas generator back on-line as quickly as possible for unforeseen events within the fuel cell system that will require an immediate supply of safe reducing gas may also be provided by embodiments of the present invention. A rapid restart capability may avoid the need for a bottled storage of reducing-gas necessary to bridge the gap between the time that the gas is demanded and the time required to bring the reducing gas generator on-line. A rapid restart method may employ a heater with a high thermal mass located just upstream of the catalyst reactor and, e.g., a pair of valves or a three-way valve for diverting feed mixture flow through the heater. During normal operation the valve directs the mixture directly into the catalytic reactor, bypassing the heater. At start-up, flow may be diverted through the heater. In the absence of flow, e.g., under idle conditions of the reducing gas generator, the heater is continuously supplied sufficient power to sustain the metal at the desired preheat temperature while balancing a relatively small heat loss, and thus, this power demand may be small. Within the heater, a flow coil may be engulfed with a metallic body. The heater may contain sufficient thermal mass so that when flow is initiated upon a re-start attempt, the process stream immediately acquires the targeted ignition temperature.

[0109] Such a design may be relatively safe because it may achieve good electrical isolation between the flammable mixture and the power supply that acts on the metallic body. Prior to a re-start sequence, the heater regulates power to the internal metal to the required temperature prior to the introduction of flow, and must only maintain power to offset heat loss through the surrounding insulation at this condition.

[0110] On a start-up attempt, power may be immediately ramped up to sustain or elevate the set-point preheat temperature until reaction of the catalyst feed mixture is achieved. Once this is achieved, e.g., as indicated by a sufficient rise in temperature at the catalyst exit, the flow may be diverted around the ignition heater directly into the catalyst (normal operating flow mode) to prevent overheating of the catalyst.

[0111] To further promote rapid re-start, band heaters may provide an additional heat source. The band heaters may surround the catalyst reactor to hold the catalyst at or above the catalyst light-off temperature before flow is initiated at start-up. Prior to start-up, the band heaters would preferably provide the energy to offset heat loss through the insulation surrounding the band heaters. Once the catalyst is lit, the band heaters may turn off as the skin temperature rises above the set point temperature of the heaters. Power to the heater may be either turned off or turned down to sustain the heater's thermal mass at the temperature set point for the next restart.

[0112] Other alternative embodiments would simplify the heat-up scheme by employing a closely coupled heater at the catalyst inlet. This approach may use a low thermal mass heater that would locally initiate reaction near the front side of the catalyst by close thermal coupling, which in such embodiments may potentially reduce the reducing gas generator's part count and cost.

[0113] In an additional embodiment, the reducing gas generator may replace the internal reformer for the fuel cell system for those embodiments where the reducing gas generator is structured to produce a reducing gas that is suitable for power production in the fuel cell system. In some such embodiments, the reduced gas generator may be used for producing a reducing gas of one composition for startup and shutdown of the fuel cell system, and for producing a reducing gas of an alternate composition for the normal operation of the fuel cell system.

[0114] Embodiments of the present invention include a reducing gas generator for startup and shutdown of a fuel cell including an oxidant source structured to supply a low oxygen (O_2) content oxidant, the low O_2 content oxidant having an O_2 content less than that of atmospheric air. The reducing gas generator of the present invention also includes a fuel input configured to receive a hydrocarbon fuel, a merging chamber in fluid communication with said oxidant source and in fluid communication with the fuel inlet, the merging chamber structured to receive the hydrocarbon fuel and the low oxygen (O_2) content oxidant, and to discharge a feed mixture containing both the hydrocarbon fuel, and the low oxygen (O_2) content oxidant. The reducing gas generator also includes a catalytic reactor in fluid communication with the merging chamber, the catalytic reactor structured to receive the feed mixture and to catalytically convert the feed mixture into a reducing gas. The reducing gas generator also includes a reducing gas output fluidly coupled to the catalytic reactor and in fluid communication with at least one of an anode and a reformer of the fuel cell, the reducing gas output operative to direct the reducing gas to at least one of the anode and the reformer of the fuel cell, the reducing gas generator further including a control system configured to execute program instructions to regulate a control temperature by varying both the O_2 content of the low O_2 content oxidant and the oxidant/fuel ratio of the feed mixture.

[0115] One refinement of the embodiment may include a nitrogen generator operable to extract oxygen (O_2) from air and to discharge the balance in the form of a nitrogen-rich gas, the nitrogen-rich gas forming at least a part of the low O_2 content oxidant.

[0116] Another refinement of the embodiment may include an air charging system coupled to the nitrogen generator output. The air charging system is structured to variably add air to the nitrogen-rich gas to vary the O₂ content of the low O₂ content oxidant.

[0117] Another refinement of the embodiment may include a valve structured to add a controlled amount of air to one of the nitrogen-rich gas and the feed mixture.

[0118] Another refinement of the embodiment may include the nitrogen generator which may include a nitrogen separation membrane configured to separate nitrogen out of air.

[0119] The reducing gas generator of the present invention includes a control system configured to execute program instructions to regulate a control temperature by varying both the O₂ content of the low O₂ content oxidant and the oxidant/fuel ratio of the feed mixture.

[0120] Another refinement of the embodiment may include a control temperature sensor and an O₂ sensor communicatively coupled to the control system.

[0121] Another refinement of the embodiment may include an oxidant control valve communicatively coupled to the control system. The oxidant control valve may be structured to control a flow of the oxidant as directed by the control system and a fuel control valve communicatively coupled to the control system. The fuel control valve may be structured to control a flow of the hydrocarbon fuel as directed by the control system, wherein the control system is configured to execute program instructions to vary the oxidant/fuel ratio by controlling the output of at least one of the fuel control valve and the oxidant control valve.

[0122] Another refinement of the embodiment may include a control system configured to execute program instructions to selectively vary a combustibles content of the reducing gas while maintaining a selected temperature of the reducing gas by varying both the O₂ content of the oxidant and the oxidant/fuel ratio of the feed mixture.

[0123] Another refinement of the embodiment may include at least two of a control temperature sensor, an oxygen sensor and a reducing gas combustibles detection sensor communicatively coupled to the control system.

[0124] Another refinement of the embodiment may include a heat exchanger fluidly coupled downstream of the catalytic reactor, wherein the heat exchanger may be configured to control a temperature of the reducing gas.

[0125] Another refinement of the embodiment may include a heater upstream of the catalytic reactor, wherein the heater may be configured to initiate a catalytic reaction at the catalyst of the catalytic reactor by heating at least a portion of the feed mixture and supplying the heated mixture to the catalytic reactor.

[0126] In another refinement of the embodiment the heater may include a body configured to continuously maintain a temperature one of at and above the catalyst light-off temperature of the feed mixture during normal operations of the fuel cell.

[0127] Another refinement of the embodiment may include at least one of a catalyst heater configured to maintain the catalyst of the catalytic reactor at a temperature one of at and above a catalyst light-off temperature of the feed mixture during normal operations of the fuel cell or an other heater disposed adjacent the inlet of the catalytic reactor and structured to initiate catalytic reaction of the feed mixture in an upstream portion of the catalytic reactor.

[0128] Another refinement of the embodiment may include means for varying a combustibles content of the reducing gas while maintaining a constant control temperature.

[0129] In another refinement of the embodiment the feed mixture includes an oxidant having an O₂ content. The means for varying may include a means for varying the O₂ content in the oxidant or a means for varying an oxidant/fuel ratio of the feed mixture.

[0130] Another embodiment of the present invention is a fuel cell system which includes a fuel cell, including an anode, a cathode, an electrolyte coupled to the anode and the cathode, and a reformer, the fuel cell system including a reducing gas generator configured for startup and shutdown of the fuel cell, the reducing gas generator including an oxidant source structured to supply a low oxygen (O₂) content oxidant stream, the low O₂ content oxidant stream having an O₂ content less than that of atmospheric air. The reducing gas generator also includes a fuel input configured to receive a hydrocarbon fuel and a merging chamber in fluid communication with the oxidant source and in fluid communication with the fuel inlet, the merging chamber

structured to receive the hydrocarbon fuel and the low O₂ content oxidant stream and to discharge a feed mixture containing both the hydrocarbon fuel and the low O₂ content oxidant stream. The reducing gas generator also includes a catalytic reactor in fluid communication with the merging chamber, the catalytic reactor structured to receive the feed mixture and catalytically convert the feed mixture into a reducing gas, the reducing gas generator also including a reducing gas output fluidly coupled to the catalytic reactor and in fluid communication with at least one of the anode and the reformer, the reducing gas output operative to direct the reducing gas to the at least one of the anode and the reformer, the reducing gas generator further including a control system configured to execute program instructions to regulate a control temperature by varying both the O₂ content of the low O₂ content oxidant and the oxidant/fuel ratio of the feed mixture.

[0131] One refinement of the embodiment may include an air intake or a nitrogen generator in fluid communication with the air intake. The nitrogen generator may have a nitrogen generator output and structured to receive air from the air intake to extract O₂ from the air received from the air intake, and to discharge from the nitrogen generator output the balance in the form of a nitrogen-rich gas. The nitrogen-rich gas may form at least a part of the low O₂ oxidant stream.

[0132] Also disclosed is a reducing gas generator which may include an oxidant source structured to supply a low-oxygen (O₂) content oxidant stream. The low O₂ oxidant stream may have an O₂ content less than that of atmospheric air. The reducing gas generator may also include a fuel source fluidly coupled to the oxidant source and structured to supply a hydrocarbon fuel. The reducing gas generator may also include a merging chamber fluidly coupled to the fuel source and the oxidant source. The merging chamber may be structured to combine the oxidant and the hydrocarbon fuel into a feed mixture. The feed mixture may have an oxidant/fuel ratio defined by a ratio of the amount of the oxidant in the feed mixture to the amount of the hydrocarbon fuel in the feed mixture. The reducing gas generator may also include a catalytic reactor fluidly coupled to the merging chamber and structured to catalytically convert the feed mixture to generate a reducing gas. The reducing gas generator may also include a control system configured to execute program instructions to control the flow rate of feed mixture and both the O₂ content of the oxidant stream and the oxidant/fuel ratio of the feed mixture to maintain a predetermined control temperature while varying a combustibles content of the reducing gas output by the catalytic reactor.

[0133] In one refinement of the embodiment the oxidant source employs a nitrogen generator to supply a nitrogen-rich gas.

[0134] In another refinement of the embodiment the nitrogen generator includes a nitrogen separation polymer.

[0135] In another refinement of the embodiment the reducing gas generator may be structured to supply the reducing gas to a fuel cell having at least one of an anode and a reformer. In accordance with the invention, the reducing gas generator may include a reducing gas output fluidly coupled to the catalytic reactor and in fluid communication with at least one of the anode and the reformer, the reducing gas output operative to direct the reducing gas to the at least one of said anode and the reformer.

[0136] Disclosed herein is a reducing gas generator which may include a means for providing an oxidant stream, a means for supplying a hydrocarbon fuel, and a means for combining the oxidant and the hydrocarbon fuel into a feed mixture. The feed mixture may have an oxidant/fuel ratio defined by a ratio of the amount of the oxidant in the feed mixture to the amount of the hydrocarbon fuel in the feed mixture. The reducing gas generator may also include a means for catalytically converting the feed mixture into a reducing gas. The reducing gas generator may also include a means for controlling both the O₂ content of the oxidant stream and the oxidant/fuel ratio of the feed mixture to selectively vary a combustibles content of the reducing gas while maintaining a selected control temperature.

[0137] Also disclosed is a system for purging a fuel cell which may include an air intake structured to receive atmospheric air. The system for purging a fuel cell may also include a compressor fluidly coupled to the air intake. The compressor may be structured to compress atmospheric air received from the air intake to a pressure above ambient atmospheric pressure. The system for purging a fuel cell may also include a nitrogen generator fluidly coupled to the compressor and fluidly coupled to the fuel cell. The nitrogen generator may be structured to generate a nitrogen-rich stream from the compressed air and to provide the nitrogen-rich stream to purge at least one component associated with the fuel cell.

[0138] The nitrogen generator may include a nitrogen separation membrane structured to separate oxygen from the compressed air using the pressure of the compressed air to supply the nitrogen-rich stream.

[0139] A pressure regulator may be included fluidly coupled between the compressor and the nitrogen generator. The pressure regulator may be structured to automatically regulate the pressure of the compressed air to the desired level.

[0140] Also disclosed is a fuel cell system which may include a fuel cell and a purging system coupled to the fuel cell. The purging system may include an air intake structured to receive atmospheric air. The purging system may also include a compressor fluidly coupled to the air intake. The compressor may be structured to compress atmospheric air received from the air intake to a pressure above ambient atmospheric pressure. The purging system may also include a nitrogen generator fluidly disposed between the compressor and the fuel cell. The nitrogen generator may be structured to generate a nitrogen-rich stream from the compressed air and to provide the nitrogen-rich stream to purge at least one component associated with the fuel cell.

[0141] Disclosed herein is a control system structured to execute program instructions to control a flow rate of a feed mixture and both the O₂ content of an oxidant stream and the oxidant/fuel ratio of the feed mixture to maintain a predetermined control temperature in one of a catalytic reactor and a reducing gas output by the catalytic reactor.

[0142] The control system may be structured to execute program instructions to maintain the predetermined control temperature while varying a combustibles content of the reducing gas output by the catalytic reactor.

[0143] The control system may be structured to execute program instructions to selectively discharge the reducing gas into one or both of an anode of a fuel cell and a reformer of a fuel cell.

[0144] In another refinement of the embodiment the amount of reducing gas discharged to each of the anode and reformer varies between 0% and 100% of the total amount discharged from the catalytic reactor.

[0145] While the invention has been described in connection with what is presently considered to be the most practical and preferred embodiment, it is to be understood that the invention is not to be limited to the disclosed embodiment(s), but on the contrary, is intended to cover various modifications and equivalent arrangements included within the scope of the appended claims. Furthermore it should be understood that while the use of the word preferable, preferably, or preferred in the description above indicates that feature so described may be more desirable, it nonetheless may not be necessary and any embodiment lacking the same may be contemplated as within the scope of the invention, that scope being defined by the claims that follow. In reading the claims it is intended that when words such as "a," "an," "at least one" and "at least a portion" are used, there is no intention to limit the claim to only one item unless specifically stated to the contrary in the claim. Further, when the language "at least a portion" and/or "a portion" is used the item may include a portion and/or the entire item unless specifically stated to the contrary.

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- [WO2008091801A2 \[0006\]](#)
- [US5926805A \[0007\]](#)

ANORDNING TIL GENERERING AF EN GAS, DER KAN ANVENDES TIL OPSTART OG
LUKNING AF EN BRÆNDELSCELLE

PATENTKRAV

1. Reduktionsgasgenerator (14) til opstart og lukning af en brændselscelle (12), hvilken generator
5 omfatter:
 - en oxideringsmiddelkilde, der er struktureret til at tilføre et oxideringsmiddel med et lavt oxygen-
(O₂) indhold, hvilket oxideringsmiddel med lavt O₂-indhold har et O₂-indhold, der er mindre end indholdet i
den atmosfæriske luft;
 - en brændstofindgang (38), der er konfigureret til at modtage et carbonhybridbrændstof;
 - 10 et blandekammer (32), der står i fluidforbindelse med oxideringsmiddelkilden og i fluidforbindelse
med brændstofindgangen, hvilket blandekammer er struktureret til at modtage carbonhybridbrændstoffet og
oxideringsmidlet med lavt O₂-indhold og til at udlede en tilførselsblanding, der både indeholder
carbonhybridbrændstoffet og oxideringsmidlet med lavt O₂-indhold;
 - en katalytisk reaktor (34), der står i fluidforbindelse med blandekammeret, hvilken katalytisk
15 reaktor er struktureret til at modtage tilførselsblandingen og til katalytisk at omdanne tilførselsblandingen til
en reduktionsgas; og
 - en reduktionsgasudgang, der fluidmæssigt er koblet til den katalytiske reaktor og står i
fluidforbindelse med mindst én af en anode (20) og en reformer (26) for brændselscellen, hvilken
reduktionsgasudgang kan dirigere reduktionsgassen til den mindst én af brændselscellens anode og
20 reformer,
 - hvilken reduktionsgasgenerator endvidere indbefatter et styresystem (96), der er konfigureret til at
eksekvere programinstruktioner for at regulere en styretemperatur ved at variere både O₂-indholdet i
oxideringsmidlet med lavt O₂-indhold og forholdet mellem tilførselsblandingsens oxideringsmiddel og
brændstof.
- 25 2. Reduktionsgasgenerator (14) ifølge krav 1, hvilken generator endvidere omfatter en
nitrogengenerator (54), der kan udlede oxygen (O₂) fra luft og udlede det resterende i form af en nitrogenrig
gas, hvilken nitrogenrig gas udgør mindst en del af oxideringsmidlet med lavt O₂-indhold.
3. Reduktionsgasgenerator (14) ifølge krav 2, hvilken generator endvidere omfatter et
luftindføringsystem, der er koblet til nitrogengeneratorens udgang, hvilket luftindføringsystem er
30 struktureret til variabelt at tilføre luft til den nitrogenrige gas for at variere O₂-indholdet i oxideringsmidlet
med lavt O₂-indhold.
4. Reduktionsgasgenerator (14) ifølge krav 2, hvilken generator endvidere indbefatter en ventil, der er
struktureret til at tilføre en styret mængde luft til en af den nitrogenrige gas og tilførselsblandingen.
5. Reduktionsgasgenerator (14) ifølge krav 2, hvor nitrogengeneratoren indbefatter en
35 nitrogenseparationsmembran (56), der er konfigureret til at separere nitrogen fra luft.
6. Reduktionsgasgenerator (14) ifølge krav 1, hvilken generator endvidere omfatter en
styretemperatursensor (84) og en O₂-sensor (66), der forbindelsesmæssigt er koblet til styresystemet (96).
7. Reduktionsgasgenerator (14) ifølge krav 1, hvilken generator endvidere omfatter:

en oxideringsmiddelreguleringsventil (62), der forbindelsesmæssigt er koblet til styresystemet (96), hvilken oxideringsmiddelreguleringsventil er struktureret til at styre en strøm af oxideringsmidlet, der dirigeres ved hjælp af styresystemet; og

5 en brændstofreguleringsventil (46), der forbindelsesmæssigt er koblet til styresystemet, hvilken brændstofreguleringsventil er struktureret til at styre en strøm af carbonhybridbrændstoffet, der dirigeres ved hjælp af styresystemet,

hvor styresystemet er konfigureret til at eksekvere programinstruktioner for at variere forholdet mellem oxideringsmiddel og brændstof ved at styre udgangen fra mindst én af brændstofreguleringsventilen og oxideringsmiddelreguleringsventilen.

10 8. Reduktionsgasgenerator (14) ifølge krav 1, hvor styresystemet (96) er konfigureret til at eksekvere programinstruktioner for selektivt at variere et indhold af brændbare stoffer i reduktionsgassen, mens der opretholdes en udvalgt temperatur på reduktionsgassen ved både at variere oxideringsmidlets O₂-indhold og forholdet mellem tilførselsblandings oxideringsmiddel og brændstof.

9. Reduktionsgasgenerator (14) ifølge krav 8, hvilken generator endvidere omfatter mindst to af en
15 styretemperatursensor (84), en oxygensensor (66) og en sensor (86) til detektering af brændbare stoffer i reduktionsgassen, hvilke sensorer er forbindelsesmæssigt koblet til styresystemet (96).

10. Reduktionsgasgenerator (14) ifølge krav 1, hvilken generator endvidere omfatter en varmeveksler (88), der fluidmæssigt er tilkoblet på nedstrømsiden af den katalytiske reaktor (34), hvilken varmeveksler er konfigureret til at styre en temperatur på reduktionsgassen.

20 11. Reduktionsgasgenerator (14) ifølge krav 1, hvilken generator endvidere omfatter en varmeanordning (74) på opstrømsiden af den katalytiske reaktor (34), hvilken varmeanordning er konfigureret til at initiere en katalytisk reaktion ved den katalytiske reaktors katalysator (36) ved at opvarme mindst en del af tilførselsblandingen og tilføre den opvarmede blanding til den katalytiske reaktor.

12. Reduktionsgasgenerator (14) ifølge krav 11, hvor varmeanordningen (74) indbefatter et legeme
25 (76), der er konfigureret til kontinuerligt at opretholde en temperatur ved én af ved og over en katalysator- (36) driftstemperatur for tilførselsblandingen under normale anvendelser af brændselscellen (12).

13. Reduktionsgasgenerator (14) ifølge krav 1, hvilken generator endvidere omfatter mindst én af:
30 en katalysatorvarmeanordning (80), der er konfigureret til at bevare den katalytiske reaktors (34) katalysator (36) ved en temperatur på én af ved og over en katalysatordriftstemperatur for tilførselsblandingen under normale anvendelser af brændselscellen (12); og

en anden varmeanordning (82), der er placeret stødende op til indgangen til den katalytiske reaktor og struktureret til at initiere katalytisk reaktion af tilførselsblandingen i en opstrømsdel af den katalytiske reaktor.

14. Brændselscellesystem (10), der omfatter:
35 en brændselscelle (12), der indbefatter en anode (20), en katode (24), en elektrolyt (22), der er koblet til anoden og katoden, og en reformer (26); og

en reduktionsgasgenerator (14), der er konfigureret til opstart og lukning af brændselscellen, hvilken reduktionsgasgenerator indbefatter:

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en oxideringsmiddelkilde, der er struktureret til at tilføre en oxideringsmiddelstrøm med lavt oxygen- (O_2) indhold, hvilken oxideringsmiddelstrøm med lavt O_2 -indhold har et O_2 -indhold, der er mindre end indholdet i den atmosfæriske luft;

en brændstofindgang (38), der er konfigureret til at modtage et carbonhybridbrændstof;

5 et blandekammer (32), der står i fluidforbindelse med oxideringsmiddelkilden og i fluidforbindelse med brændstofindgangen, hvilket blandekammer er struktureret til at modtage carbonhybridbrændstoffet og oxideringsmiddelstrømmen med lavt O_2 -indhold og til at udlede en tilførselsblanding, der indeholder både carbonhybridbrændstoffet og oxideringsmiddelstrømmen med lavt O_2 -indhold;

10 en katalytisk reaktor (34), der står i fluidforbindelse med blandekammeret, hvilken katalytisk reaktor er struktureret til at modtage tilførselsblandingen og til katalytisk at omdanne tilførselsblandingen til en reduktionsgas; og

en reduktionsgasudgang, der fluidmæssigt er koblet til den katalytiske reaktor og står i fluidforbindelse med mindst én af anoden og reformeren, hvilken reduktionsgasudgang kan dirigere reduktionsgassen til den mindst ene af anoden og reformeren,

15 hvilken reduktionsgasgenerator endvidere indbefatter et styresystem (96), der er konfigureret til at eksekvere programinstruktioner for at regulere en styretemperatur ved at variere både O_2 -indholdet i oxideringsmidlet med lavt O_2 -indhold og forholdet mellem tilførselsblandingens oxideringsmiddel og brændstof.

DRAWINGS

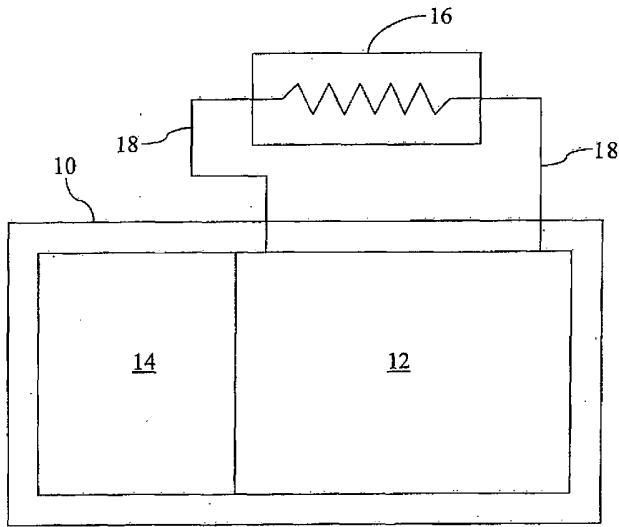


FIG. 1

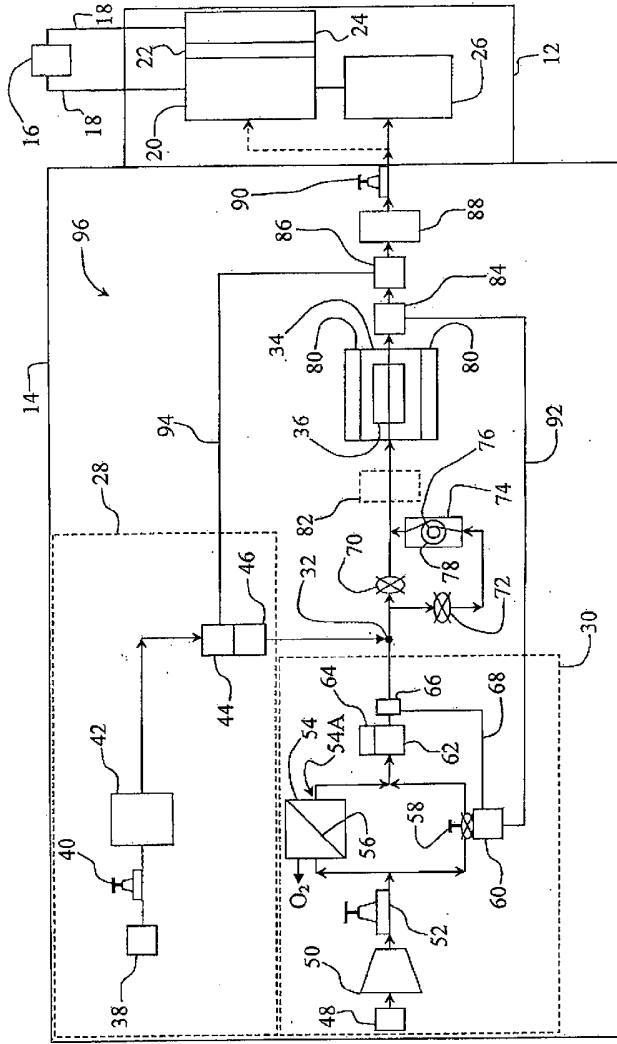


FIG. 2

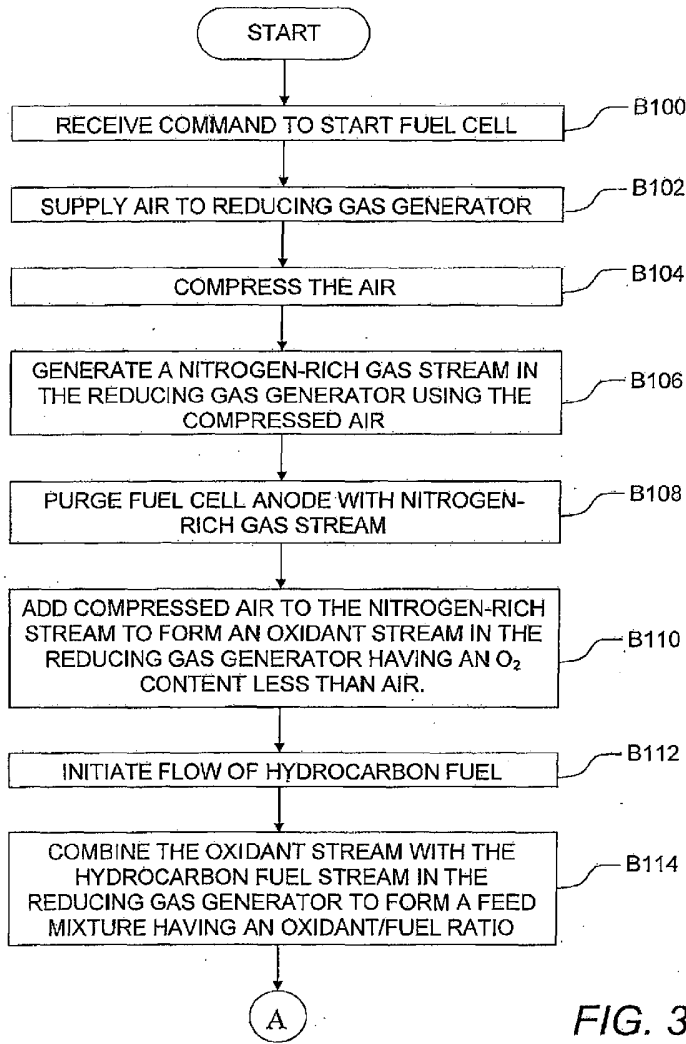


FIG. 3A

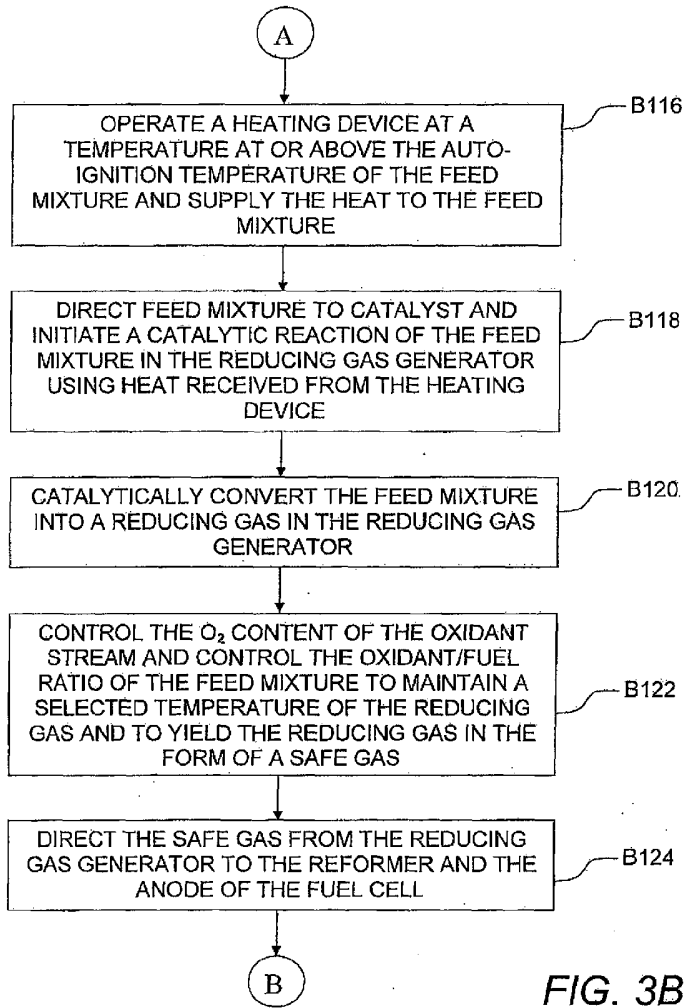


FIG. 3B

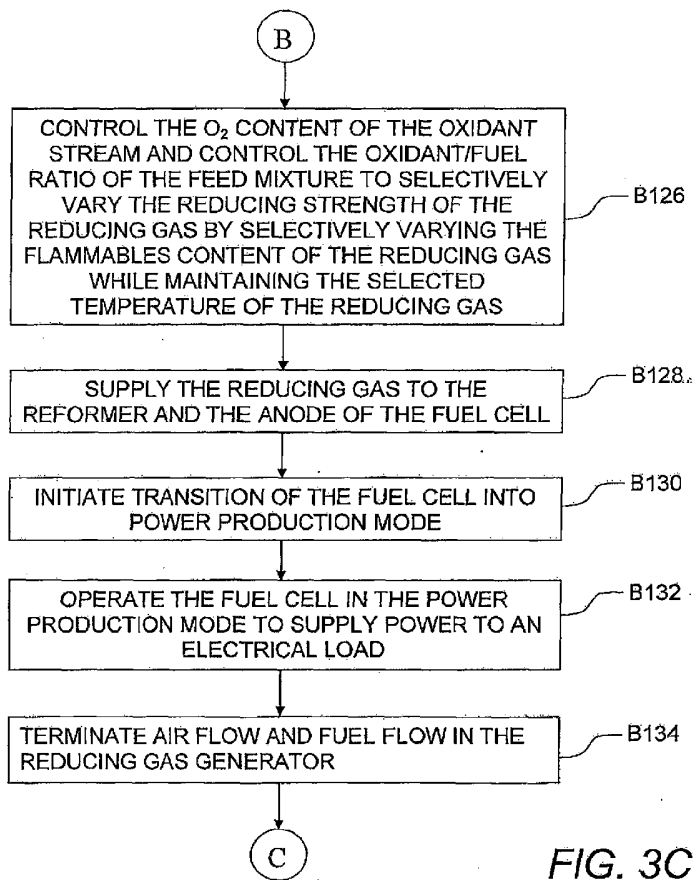


FIG. 3C

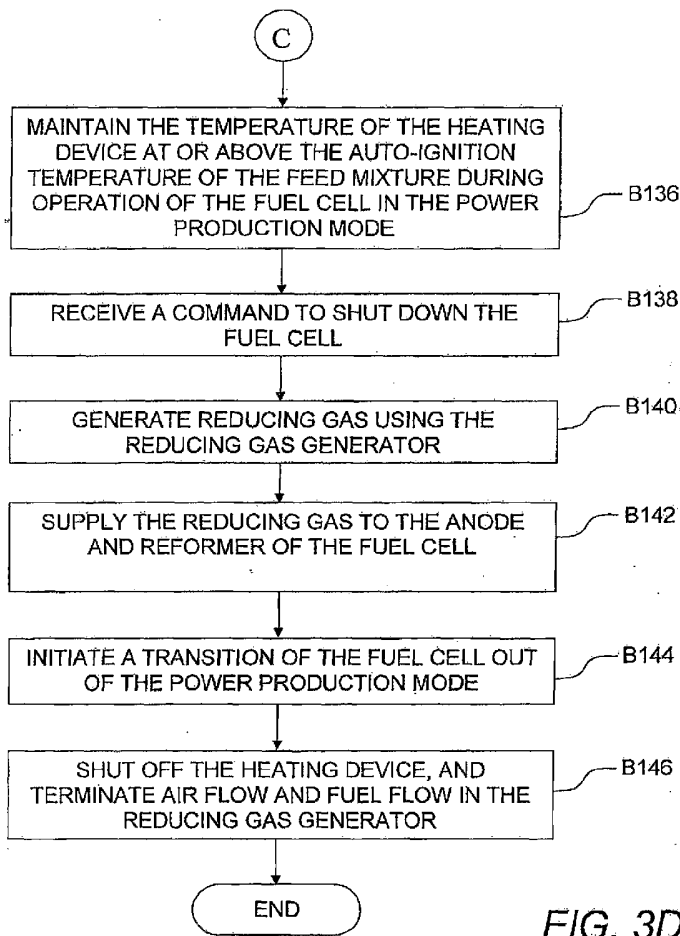


FIG. 3D

10 g/s Reducing Gas Flow, Texit = 770C

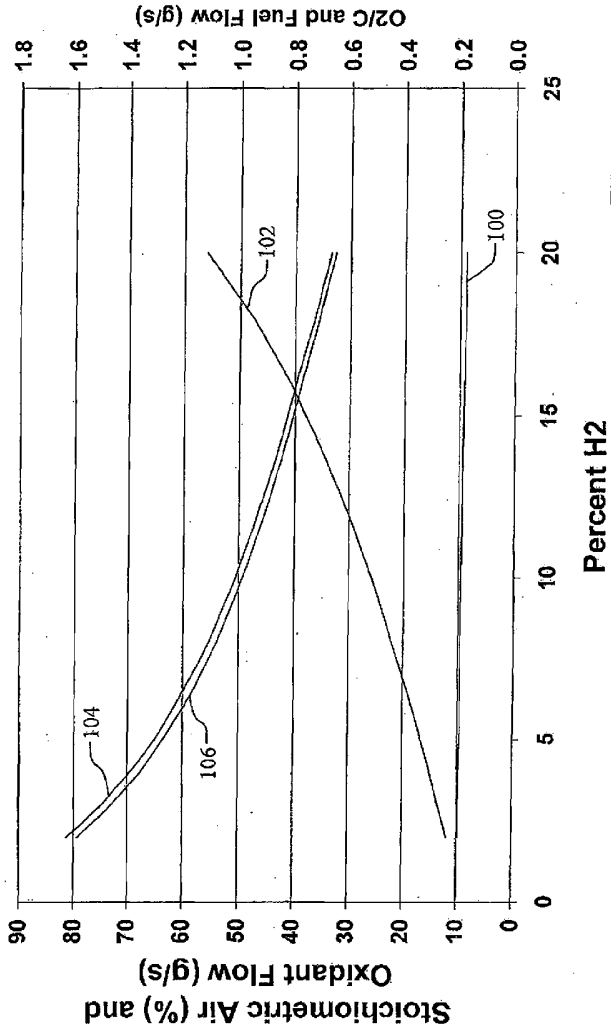


FIG. 4